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3DFEMWATER: A Three-Dimensional Finite Element Model of WATER Flow Through Saturated-Unsaturated Media

G. T. Yeh

Environmental Sciences Division
Publication No. 2904



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of WATER Flow through Saturated-Unsaturated Media**

G. T. Yeh

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NUCLEAR AND CHEMICAL WASTE PROGRAMS
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ABSTRACT

YEH, G. T. 1987. 3DFEMWATER: A Three-Dimensional Finite Element Model of WATER Flow through Saturated-Unsaturated Media. ORNL-6386. Oak Ridge National Laboratory, Oak Ridge, TN. 304 pp.

This report presents the development and verification of a three-dimensional finite element model of water flow through saturated-unsaturated media (3DFEMWATER). The special features of 3DFEMWATER are its flexibility and versatility in modeling as wide a range of real-world problems as possible. The model is designed to: (1) treat heterogeneous and anisotropic media consisting of as many geologic formations as desired, (2) consider both distributed and point sources/sinks that are spatially and temporally dependent, (3) accept the prescribed initial conditions or obtain them by simulating a steady state version of the system under consideration, (4) deal with a transient head distributed over the Dirichlet boundary, (5) handle time-dependent fluxes due to pressure gradient varying along the Neumann boundary, (6) treat time-dependent total fluxes distributed over the Cauchy boundary, (7) automatically determine variable boundary conditions of evaporation, infiltration, or seepage on the soil-air interface, (8) include the off-diagonal hydraulic conductivity components in the modified Richards equation for dealing with cases when the coordinate system does not coincide with the principal directions of the hydraulic conductivity

tensor, (9) give three options for estimating the nonlinear matrix, (10) include two options (successive subregion block iterations and successive point iterations) for solving the linearized matrix equations, (11) automatically reset time step size when boundary conditions or source/sinks change abruptly, and (12) check the mass balance computation over the entire region for every time step. The model is verified with analytical solutions or other numerical models for three examples.

1. INTRODUCTION

To study the transport of dissolved constituents in a subsurface flow system, the velocity field, pressure distribution, and moisture content must be determined. Numerous models by finite differences and finite elements have been reported in the literature for simulating the flow variables in saturated-unsaturated porous media (Freeze 1972; Neuman et al. 1974; Reeves and Duguid 1975; Segol 1976; van Genuchten et al. 1977; Narasimhan and Witherspoon 1977; van Genuchten and Pinder 1978; Yeh and Ward 1980; Reisenauer et al. 1982; Huyakorn 1986). While the Richards equation (Richards 1931) or its modified form has been the common basis for the development of practically all numerical models, the variations among these models lie mainly in the number of space dimensions, the choice of numerical methods, the treatment of initial and boundary conditions, and the consideration of source/sink.

The vast majority of subsurface flow models in saturated-unsaturated media are limited to two-dimensional and/or one-dimensional problems. Only a few three-dimensional models have appeared in the report and open literature (Segol 1976; Reisenauer, et al. 1982; Huyakorn 1986). In nature, water movement in the surface system occurs in all directions (three-dimensional problems) under saturated-unsaturated flow conditions. This report presents the development and verification of a three-dimensional model of water flow through saturated-unsaturated media to

deal with naturally occurring or artificially disturbed flow systems. The model can handle completely saturated, completely unsaturated, or partially saturated and partially unsaturated flows. It can be applied to confined or unconfined aquifer regimes. The most difficult task in modeling unconfined aquifer flows is locating the moving phreatic surfaces under transient conditions. This difficulty can be alleviated by treating the media as being under combined saturated-unsaturated conditions. The surface of the zero pressure head, which is a function of time, can then be considered as the moving phreatic surface.

The most common numerical methods used to solve the Richards equations are the finite difference methods (FDMs) and finite element methods (FEMs) (Forsythe and Wasow 1960; Huebner 1975; Lapidus and Pinder 1982). The fundamental distinction between FEM and FDM is that the former is based directly upon approximating the function, whereas the latter is based on approximating the derivatives. Thus, the FEM provides spatially continuous solutions, whereas the FDM yields solutions only at discrete points. In addition, FEM has several advantages over FDM: (1) a better description of irregular boundaries, without the need for special formulas, (2) the ease of employing irregular grid to provide different levels of spatial discretization in different regions of the aquifers, (3) easy handling of aquifer heterogeneity and anisotropy, (4) need (sometimes) for fewer node points to represent the aquifer to the same level of accuracy, resulting in savings of computational time and computer

storage, and (5) the natural result of flux types of boundary conditions from the integral formulation. Hence the FEM is used in the 3D FEMWATER code because it is believed that the FEM is the best method, especially when it is used in conjunction with point or block iteration (Yeh 1985; Yeh et al. 1985) for the solution of matrix equations, as far as the Richards equation is concerned.

Most of the existing models assume that initial conditions are known and hence are the inputs to the model (Freeze 1972; Neumann et al 1974; Segol 1976; Reisenauer et al. 1982). A few models, however, do provide the option of obtaining the initial conditions by simulating the steady-state version of the Richards equation subject to time-invariant boundary conditions (Reeves and Duguid 1975; Yeh and Ward 1980).

As far as boundary conditions are concerned, four types may be prescribed for the most general cases: (1) Dirichlet, (2) Neumann, (3) Cauchy, and (4) variable conditions. For the Dirichlet conditions, the pressure head is prescribed on the boundary. These conditions are normally applied to the soil-water interfaces such as streams, rivers, lakes, artificial impoundments, and coastal lines. For the Neumann conditions, the pressure gradient is prescribed on the boundary. These conditions do not occur or may not be specified very often in real-world problems. They may be applied to the bottom of the media where natural drainage takes place. For the Cauchy conditions, the total normal flux on

the boundary due to pressure gradient and gravity is prescribed. These conditions are normally applied to surface water bodies with known infiltration rates through their bottom layers of sediments or liners into subsurface media. On the variable boundary, either Cauchy or Dirichlet conditions prevail depending on the conductivity of the media, the availability of water such as rainfall rates, and the potential evapotranspiration. These conditions normally occur at the soil-air interface. Most of the existing large computational codes have not included all four types of boundary conditions. Many considered only two or, at the most, three types. Furthermore, most of these were not designed to treat boundary values that are time dependent either gradually or abruptly and that vary along the boundary. Concerning the treatment of source/sinks, existing computational codes fare much better since quite a few include transient, point, as well as distributed source/sink terms (Neumann et al. 1974).

In real-world problems, the recharge and pumping due to rainfall and artificial withdrawals are likely to be time dependent and distributed over the region of interest. The given boundary pressure heads, with rare exception, vary with time and along Dirichlet segments at the surface water bodies, which inevitably have their water levels fluctuating along the soil-water interfaces. The prescribed pressure gradients along Neumann boundary segments are, in general, time dependent. The known total water fluxes on Cauchy boundary segments are transient in nature;

for example, the infiltration rate from the bottom of surface water bodies into subsurface media depends on the depth of water, which, of course, varies with time. Furthermore, on the air-soil interface, the rainfall is intermittent and its intensity is not constant with time, resulting in transient total fluxes if the soil is capable of taking all the throughfall. Thus, for field applications, a computational model must have the capability to deal with these aspects simultaneously. This report presents the development of such a model to achieve these purposes.

In addition to its versatility and flexibility to treat transient source/sinks and boundary conditions and to provide options to obtain initial conditions, 3DFEMWATER also includes several special features. By including the off-diagonal hydraulic conductivity components, the model can be applied to anisotropic and nonuniform media. For an anisotropic uniform medium, one can imbed the coordinate system to coincide with the principal directions of the hydraulic conductivity tensor. However, for anisotropic and heterogeneous media, the inclusion of off-diagonal conductivities becomes necessary since the principal directions of the hydraulic conductivity tensor vary with space, prohibiting the imbedance of a unique coordinate system.

The Richards equation is nonlinear and its numerical solution exhibits fluctuations in iterations for many situations. Underrelaxation is thus provided in 3DFEMWATER to reduce the fluctuations. When certain

sets of system parameters such as hydraulic retention and hydraulic conductivity are variable, the rate of numerical convergence is very slow. Hence, an overrelaxation technique is given as an option to speed up the convergence.

In solving the linearized matrix equation to obtain the iterates, practically all finite element models use the direct elimination methods to solve the system of algebraic equations simultaneously. When the region of interest requires a large number of nodes for discretization, the use of a direct elimination solution to the matrix equation becomes impractical because of excessive requirements on the central process unit (CPU) memory. For example, an 80 x 40 x 20 node discretization in a three-dimensional problem would need a CPU memory of about 960 megabytes for the banded coefficient matrix alone. These plus other overhead CPU memory are beyond the capacity of any of the mainframe computers today. To alleviate this problem, two options are provided in solving the matrix equation which will greatly reduce the CPU memory requirement: successive subregional block iteration and successive point iteration.

Finally, for abrupt change of external conditions, small time step size is needed to yield accurate and stable solutions. Automatic resetting of the time step size is built into 3DFEMWATER to facilitate the computations. This alleviates the troublesome external manipulations.

2. MATHEMATICAL STATEMENTS

2.1 Derivation of the Governing Equations

The mathematical formulation of the conservation of mass and Darcy's law extended to three-dimensional flow have been described in detail elsewhere (Bear 1972). Using (1) the continuity of fluid, (2) the continuity of solid, (3) the motion of fluid (Darcy's law), (4) equation of the state, and (5) the law of consolidation of media, one can derive a governing equation for the distribution of pressure head in the saturated-unsaturated subsurface media. The derivation of this combined equation is described below.

The continuity of fluid is expressed in integral form as:

$$\frac{D}{Dt} \int_{\nu} S n_e \rho_f d\nu = - \int_{\Gamma} n \cdot (\rho_f V_{fs}) d\Gamma + \int_{\nu} \rho_f q d\nu, \quad (1)$$

where

t - time (T),

$D()/Dt$ - total derivative of () with respect to time,

n_e - effective porosity (L^3/L^3),

S - degree of saturation (dimensionless),

ρ_f - fluid density (M/L^3),

n - outward unit vector normal to the surface,

V_{fs} - Darcy's velocity relative to the solid matrix (L^3),

ν - volume of material containing constant amount of

- solids (Fig. 1) (L^3),
- q - internal source/sink [$(L^3/T)/L^3$],
- Γ - surface enclosing the volume v (Fig. 1) (L^2).

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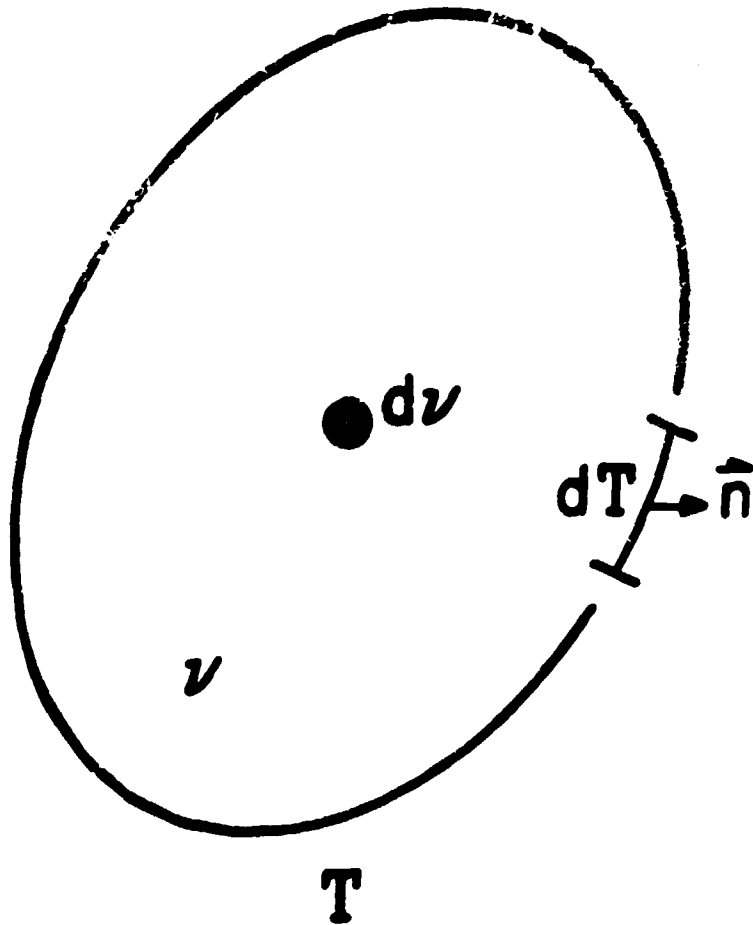


Fig. 1. An element volume containing constant amount of solids

By the Reynolds transport theorem (Owczarek 1964), Eq. (1) can be written as

$$\int_{\nu} \frac{\partial \rho_{f_e} n S}{\partial t} d\nu + \int_{\Gamma} n \cdot (S \rho_{f_e} n V_s) d\Gamma + \int_{\Gamma} n \cdot (\rho_f V_{fs}) d\Gamma - \int_{\nu} \rho_f q d\nu, \quad (2)$$

where

V_s -- velocity of the deformable surface Γ due to consolidation (L/T).

Applying the Gaussian divergence theorem to Eq. (2) and using the fact that ν is arbitrary, one can obtain the following continuity equation of fluid in differential form:

$$\frac{\partial \rho_{f_e} n S}{\partial t} + \nabla \cdot (\rho_{f_e} n S V_s) + \nabla \cdot (\rho_f V_{fs}) = \rho_f q. \quad (3)$$

The granular skeleton of the media is considered compressible under pressure, but the grains themselves are considered incompressible. The continuity statement of incompressible solids but a compressible skeleton is

$$\frac{D}{Dt} \int_{\nu} \rho_s (1 - n_e) d\nu = 0, \quad (4)$$

where

ρ_s -- density of solid grains (M/L³).

Again applying the Reynolds transport theorem to Eq. (4), we obtain:

$$\int_V \frac{\partial(1 - n_e)\rho_s}{\partial t} dv + \int_{\Gamma} n_e [(1 - n_e)\rho_s V_s] d\Gamma = 0 . \quad (5)$$

Using the Gaussian divergence theorem and the fact that ξ is arbitrary, we can write Eq. (5) in the differential form as:

$$\frac{\partial(1 - n_e)\rho_s}{\partial t} + \nabla \cdot [(1 - n_e)\rho_s V_s] = 0 . \quad (6)$$

However, since the solid grains are incompressible, we have

$$\frac{\partial \rho_s}{\partial t} + V_s \cdot \nabla \rho_s = 0 . \quad (7)$$

Combining Eqs. (6) and (7), we have:

$$\frac{\partial(1 - n_e)}{\partial t} + \nabla \cdot [(1 - n_e)V_s] = 0 . \quad (8)$$

Equations (3) and (8) are derived based on the continuity law of fluid and solid grains, with the assumptions that the grains are incompressible. These two equations involve five state variables, ρ_f , n_e , V_{fs} , V_s , and S . Up to this point, no empiricism has been introduced in the derivation of the governing equations [Eqs. (3) and (8)]. However, the number of state variables exceeds the number of equations. Thus, constitutive relationships must be empirically or theoretically established among n_e , ρ_f , V_{fs} , V_s , and S .

The first constitutive relationship is the empirical Darcy's law, stating that the relative Darcy's velocity V_{fs} is proportional to the gradient of hydraulic head. The proportionality constant is termed the hydraulic conductivity. This empirical law, in fact, can be derived theoretically from the continuity of momentum with the assumptions of neglecting the inertial forces and linearizing the frictional force (Polubarinova-Kochina 1962). The extension of Darcy's law to anisotropic media may be written in the form of

$$V_{fs} = -K \cdot \nabla H, \quad (9)$$

$$H = h + z, \quad (10)$$

where

H = total head (L),

h = pressure head (L),

z = potential head (L),

K = hydraulic conductivity tensor (L/T).

The hydraulic conductivity tensor is a function of fluid and medium properties and is defined as

$$K = \frac{\rho_f g}{\mu_f} P, \quad (11)$$

where

P = intrinsic permeability tensor of the media (L^2),

μ_f - dynamic viscosity of the fluid $(ML/T^2, L_2/T)$,
 g - acceleration of gravity (L/T^2) .

A new state variable h in Eqs. (9) and (10) has been introduced. Thus, we will need a constitutive relationship to take care of the new state variable h . Thus, the second constitutive relationship will be the empirical, thermodynamic equation of state. We will assume that the fluid density ρ_f is either constant or a function of the pressure p only; that is,

$$\rho_f = \rho(p) , \quad (12)$$

where

p - pressure $[(ML/T^2)/L^2]$.

With the assumption of Eq. (12), we can now relate the pressure head to the pressure as

$$h = \frac{p - p_0}{\rho_f g} = \frac{\sigma}{\rho_f g} , \quad (13)$$

where

p_0 - the datum pressure $[(ML/T^2)/L^2]$,

σ - the incremental pressure of the fluid.

The third constitutive relationship will be derived based on the consolidation law of the media to relate the solid velocity V_s to the

pressure head h in this paragraph. The three-dimensional consolidation equation developed by Biot (1940) is

$$(\lambda_s + 2\mu_s)\nabla^2 e - \nabla^2 \sigma, \quad (14)$$

where

$$\lambda_s = \text{Lame' first constant } [(ML/T^2)/L^2],$$

$$\mu_s = \text{Lame' second constant } [(ML/T^2)/L^2],$$

e = dilatation of the media (dimensionless).

The dilatation e and the solid velocity V_s are defined by:

$$e = \nabla \cdot U \quad \text{and} \quad V_s = \frac{\partial U}{\partial t}, \quad (15)$$

where

U = displacement of the media (L).

Taking the divergence of V_s , and from Eq. (15), we have

$$\nabla \cdot V_s = \frac{\partial}{\partial t}(\nabla \cdot U) = \frac{\partial e}{\partial t}. \quad (16)$$

Equations (13), (14), and (16) have implicitly established the constitutive relationship between V_s and the pressure head h . To explicitly express this relationship, we integrate Eq. (14) to yield

$$(\lambda_s + 2\mu_s)e = \sigma + f. \quad (17)$$

where

f - integration function.

The integration function f must satisfy the Laplace's equation for all time. To simplify the matter further, we will only consider vertical consolidation. Under this condition, it has been shown (Verruijt 1969) that the integration function f is equal to 0. It then follows from Eq. (17) that

$$\frac{\partial e}{\partial t} = \alpha \frac{\partial \sigma}{\partial t} \quad (18)$$

where

$$\alpha = \frac{1}{(\lambda_s + 2\mu_s)} \quad (19)$$

in which

α - the coefficient of consolidation of the media.

Substituting Eqs. (13) and (18) into Eq. (16), we obtain

$$\nabla \cdot \mathbf{v}_s = \frac{\partial e}{\partial t} = \alpha \frac{\partial \sigma}{\partial t} = \alpha \rho_f g \frac{\partial h}{\partial t} = \alpha' \frac{\partial h}{\partial t} \quad (20)$$

where α' is the modified compressibility of the media.

To complete the final, fourth constitutive relationship, we shall assume that the moisture content is a unique function of the pressure head. This function is termed the retention curve in the soil physics literature and expressed mathematically as:

$$\theta = n_e S = \theta(h) , \quad (21)$$

where θ is the moisture content. When the media are under saturated conditions, θ is equal to the effective porosity, n_e , and S is equal to 1.

Equations (3), (8), (9), (13), (20), and (21) (representing continuity of fluid, continuity of solids, Darcy's law, the equation of state, vertical consolidation of the solid matrix, and retention characteristics of the media, respectively) contain six variables ρ_f , n_e , V_{fs} , h , V_s , and S . Hence the number of equations is equal to the number of unknowns. The system is complete, and a mathematical statement is posed. However, we can combine these six equations into a single one to simplify the problem. The simplification is demonstrated below.

Expanding Eqs. (3) and (8), we have

$$\begin{aligned} S\rho_f \left[\frac{\partial n_e}{\partial t} + \nabla \cdot (n_e V_s) \right] + n_e S \frac{\partial \rho_f}{\partial t} + n_e \rho_f \frac{\partial S}{\partial t} = \\ - (n_e V_s) \cdot \nabla (S\rho_f) - \nabla \cdot (\rho_f V_{fs}) + \rho_f q , \end{aligned} \quad (22)$$

and

$$\frac{\partial n_e}{\partial t} = -\nabla \cdot (n_e V_s) + \nabla \cdot V_s , \quad (23)$$

respectively. Neglecting the second-order term, $(n_e V_s) \cdot \nabla (S\rho_f)$, and

substituting Eq. (23) into (22), we obtain

$$n_e \rho_f \frac{\partial S}{\partial t} + n_e S \frac{\partial \rho_f}{\partial t} + S \rho_f \nabla \cdot \mathbf{V}_s - \nabla \cdot (\rho_f \mathbf{V}_{fs}) + \rho_f q . \quad (24)$$

From Eq. (12), a compressibility of the fluid, β , is defined by

$$\beta = \frac{1}{\rho_f} \frac{d\rho_f}{dp} . \quad (25)$$

Rewriting Eq. (25) in the following form,

$$d\rho_f = \beta \rho_f dp , \quad (26)$$

and using Eq. (13), we have

$$\frac{\partial \rho_f}{\partial t} = \rho_f \beta \frac{\partial p}{\partial t} - \rho_f \beta' \frac{\partial h}{\partial t} , \quad (27)$$

where

$$\beta' = \rho_f \beta \beta \quad (28)$$

is the modified compressibility of water. From Eq. (21), we can define a specific moisture capacity as

$$\frac{d\theta}{dh} = n_e \frac{dS}{dh} , \quad (29)$$

from which

$$\frac{d\theta}{dh} \frac{\partial h}{\partial t} = n_e \frac{\partial S}{\partial t} \quad (30)$$

Substituting Eqs. (9), (20), (24), and (30) into (24), we obtain:

$$\rho_f \frac{d\theta}{dh} \frac{\partial h}{\partial t} + \rho_f \theta \beta' \frac{\partial h}{\partial t} + S \rho_f \alpha' \frac{\partial h}{\partial t} = \nabla \cdot (\rho_f \mathbf{K} \cdot \nabla H) + \rho_f q \quad (31)$$

Expanding the fourth term of Eq. (31) and neglecting the second-order term $[(\mathbf{K} \cdot \nabla H) \cdot (\nabla \rho_f)]$, we finally have the following governing equation for saturated-unsaturated media:

$$F \frac{\partial h}{\partial t} = \nabla \cdot [\mathbf{K} \cdot (\nabla h + \nabla z)] + q \quad (32)$$

in which

$$F = \alpha' \frac{\theta}{n_e} + \beta' \theta + \frac{d\theta}{dh} \quad (33)$$

The first two terms in Eq. (33) make Eq. (32) a modified form of the Richards equation.

2.2 Initial and Boundary Conditions

To completely define the problem, Eq. (32) must be constrained by initial and boundary conditions. It is assumed that an initial distribution of pressure head can be described in the region of interest, R (Fig. 2):

$$h = h_I(x, y, z) \quad \text{in } R, \quad (34)$$

where h_I is the prescribed initial condition, which can be defined or obtained by solving the steady state version of Eq. (32).

The specification of boundary conditions is the most difficult and intricate task in groundwater flow modeling. From the dynamic point of view, a segment of boundary may be classified as flow-through or impervious. From the physical point of view, it may be considered as a soil-air interface, a soil-soil interface, or a soil-water interface. From the mathematical point of view, it may be treated as a Dirichlet boundary on which the functional values are prescribed, a Neumann boundary on which the gradients of the function are known, or a Cauchy boundary on which the total fluxes are given. An even more difficult mathematical boundary is the variable conditions on which the boundary conditions are not known a priori but are themselves the solution to be sought. In other words, on the mathematically variable boundary, either Dirichlet or Cauchy conditions may prevail and change with time. As to which condition prevails at a particular time can only be determined in the cyclic process of solving the governing equations (Freeze 1972; Reeves and Duguid 1975; Yeh and Ward 1980).

Whatever point of view is taken, all boundary conditions must be transformed into mathematical equations for quantitative simulation.

Thus, we will specify the boundary condition from the mathematical point of view in concert with dynamic and physical considerations. The boundary conditions imposed on any segment of the boundary are taken to be either Dirichlet, Neumann, Cauchy, or variable. Thus, the boundary may be split into four parts, B_D , B_N , B_C , and B_V (Fig. 2), denoting Dirichlet, Neumann,

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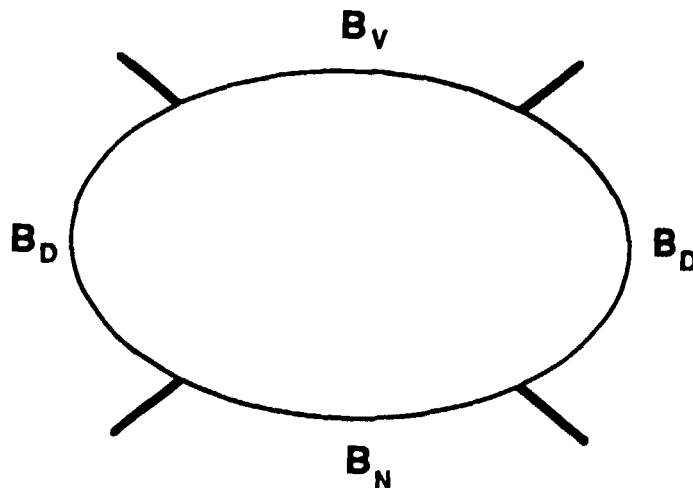


Fig. 2. Region of interest and its boundaries

Cauchy, and variable boundaries, respectively. The conditions imposed on the first three types of boundaries are given as follows:

$$h = h_D(x_b, y_b, z_b, t) \quad \text{on } B_D, \quad (35)$$

$$-n \cdot K \cdot \nabla h = q_N(x_b, y_b, z_b, t) \quad \text{on } B_N, \quad (36)$$

and

$$-n \cdot (K \cdot \nabla h + K \cdot \nabla z) = q_C(x_b, y_b, z_b, t) \quad \text{on } B_C, \quad (37)$$

where (x_b, y_b, z_b) is the spatial coordinate on the boundary; and h_D , q_N , and q_C are the prescribed Dirichlet functional value, Neumann flux, and Cauchy flux, respectively.

The conditions imposed on the variable-type boundary, which is normally the soil-air or soil-water interface, are treated separately for precipitation and nonprecipitation periods. During precipitation periods, we impose

$$h = h_p(x_b, y_b, z_b, t) \quad \text{on } B_V, \quad (38)$$

or

$$-n \cdot (K \cdot \nabla h + K \cdot \nabla z) = q_p(x_b, y_b, z_b, t) \quad \text{on } B_V, \quad (39)$$

where h_p is the allowed ponding depth and q_p is the throughfall of precipitation. Either Eq. (38) or Eq. (39) is applied to the boundary B_V

when the exact boundary conditions cannot in general be predicted a priori. Such a case would arise at the ground surface where either Dirichlet (ponding) or Cauchy (infiltration) conditions could prevail. The changeover from Dirichlet conditions specified by Eq. (38) to Cauchy conditions specified by Eq. (39) or vice versa is determined in the cyclic process of solving Eq. (32). Numerical implementation of this type of boundary conditions is treated in Sect. 3.3.

During nonprecipitation periods, we imposed

$$h = h_p(x_b, y_b, z_b, t) \quad \text{on } B_V, \quad (40)$$

or

$$h = h_m(x_b, y_b, z_b, t) \quad \text{on } B_V, \quad (41)$$

or

$$-n \cdot K \cdot (\nabla h + \nabla z) = q_e(x_b, y_b, z_b, t) \quad \text{on } B_V, \quad (42)$$

where h_m is the allowed minimum pressure on the air-soil interface and q_e is the allowed maximum evaporation rate, which is the potential evaporation. Again, only one of Eqs. (40) through (42) is used at any point on the variable boundary.

Equations (32) and (35) through (42) constitute a general mathematical statement of physical problems of flow in saturated-unsaturated subsurface media. Analytical solutions for this general system do not exist. Numerical algorithms have to be devised to solve the problem. The

finite element method rather than the finite difference method will be used in this report because of its ability to treat compound regions with complex boundaries and its simplicity in handling flux-type boundary conditions, whereas the FDM has to use a regular grid system and to interpolate the flux-type boundary conditions.

3. NUMERICAL APPROXIMATIONS

Equations (32) and (35) through (42) constitute an initial-boundary value problem governing the hydrological flow problems in subsurface systems. Analytical solution to the system in general is beyond the capability of present day applied mathematics. Numerical methods are the only tools that can be used to achieve a solution. A large number of numerical approximations can be used to reduce the partial differential equation governing the subsurface flow to a system of algebraic equations. The most common numerical methods used to approximate Eq. (32) are finite difference methods (FDMs) and finite element methods (FEMs) (Forsythe and Wasow 1960; Huebner 1975; Lapidus and Pinder 1982). Many other numerical techniques such as the integrated finite difference method (IFDM) (Narasimhan and Witherspoon 1977) or the integrated compartment method (ICM) (Yeh and Luxmoore 1983), have been employed to deal with special cases of the Richards equation. Only finite differences and finite elements can be applied to the most generalized form of the transport equations. The advantages of the FEM are its inherent ability to discretize complex boundaries, ease in dealing with flux-type boundary conditions, and flexibility in including cross-derivative terms. The disadvantages of the FEM are the requirements of CPU time to obtain element matrices, and the inflexibility of using iteration methods to solve the resulting matrix equation. On the other hand, the FDM offers great economy because of simple interpolation for the derivatives, and it

provides flexibility in solving the resulting matrix equation with various iteration methods. However, it suffers from the problems that the regular rectangular grid system must be used, the flux-type boundary conditions must be extrapolated, and the cross-derivative terms cannot be consistently approximated. The most severe limitations of the IFDM are its inability to treat anisotropic media and its usage of the Jacobian iteration method, in which the rate of convergency is extremely slow, but it offers even more flexibility than the FEM in discretizing the complex boundaries, and the physical representation of the method is most clearly understood. The ICM, while retaining the advantage of the IFDM, can deal with anisotropic media by defining new variables but at the expense of having to solve a large number of simultaneous field equations (Yeh and Luxmoore 1983). In addition, ICM provides options of using the direct elimination method and iteration methods with the Gauss-Seidel or successive overrelaxation schemes to solve the matrix equation (Yeh and Luxmoore 1983). In light of these discussions and the fact that great progress has been made in using the iteration methods to solve finite element equations (Yeh 1985; Yeh 1986) and that influence coefficient methods have been proposed to analytically and thus economically compute the element matrices (Huyakorn and Thomas 1984), the FEM is used in this report to approximate the Richards equation.

3.1 Finite Element Approximations in Space

Equation (32) will be integrated in the spatial dimensions by the weighted residual method in conjunction with finite elements. Because the formulation and use of the finite element method has been well documented (Lapidus and Pinder 1982), the theoretical basis will not be presented here. Only the numerical procedures are summarized in the following. The region of interest is subdivided into an assemblage of smaller subdomains called elements, which are interconnected by nodes that may be either on the vertices or the boundaries of the elements. Following the procedure of the finite element, weighted-residual method, approximate formulation of the distribution of the pressure head in Eq. (32) will be obtained. Thus, let the variable h be approximated by

$$h = \sum_{j=1}^N h_j(t) N_j(x, y, z), \quad (43)$$

where

N_j - the basis function of the spatial coordinate
for the j -th node,

h_j - the value of h at node j ,

N - number of nodes in the region.

Upon substituting Eq. (43) into Eq. (32) and applying the principle of weighted-residual, we obtain the following matrix equation:

$$[M] \frac{dh}{dt} + [S](h) = (G) + (Q) + (B), \quad (44)$$

where (dh/dt) and (h) are the column vectors containing the values of dh/dt and h , respectively, at all nodes; $[M]$ is the mass matrix resulting from the storage term; $[S]$ is the stiff matrix resulting from the action of conductivity; and (G) , (Q) , and (B) are the load vectors from the gravity force, internal source/sink, and boundary conditions, respectively. The matrices $[M]$ and $[S]$ are given by

$$M_{ij} = \sum_{e \in M_e} \int_{R_e} N_{\alpha}^e F N_{\beta}^e dR, \quad (45)$$

$$S_{ij} = \sum_{e \in M_e} \int_{R_e} [(\nabla N_{\alpha}^e) \cdot K \cdot (\nabla N_{\beta}^e)] dR, \quad (46)$$

where

R_e - the region of element e ,

M_e - the set of elements that have a local side α - β coinciding with the global side i - j ,

N_{α}^e - the α -th local basis function of element e .

Similarly, the load vectors (G) , (Q) and (B) are given by

$$G_i = - \sum_{e \in M_e} \int_{R_e} (\nabla N_{\alpha}^e) \cdot K \cdot \nabla z dR, \quad (47)$$

$$Q_i = \sum_{e \in M_e} \int_{R_e} N_{\alpha}^e q dR, \quad (48)$$

and

$$B_i = - \sum_{e \in N_{se}} \int_{B_e} N_{\alpha}^e (-K \cdot \nabla H) dB \quad (49)$$

where

B_e - the length of boundary segment e ,

N_{se} - the set of boundary segments that have a local node α coinciding with the global node i .

It should be noted that in applying the weighted-residual finite element method to Eq. (32), we have used the Galerkin finite element method, in which the set of basis functions is chosen as the set of weighting functions for all terms.

The reduction of the partial differential equation (PDE), Eq. (32), to the set of ordinary differential equations (ODE), Eq. (44), simplifies to the evaluation of integrals on the right-hand side of Eqs. (45) through (49) for every element or boundary segment e . The major tasks that remain are the specification of basis and weighting functions and the performance of integration to yield the element matrices. Linear hexahedron elements are employed in this report.

For a hexahedron element with eight corner nodes, a trilinear polynomial base function for the α -th node may be written in terms of local normalized coordinate as

$$N_{\alpha}^e = (1 + \xi_{\alpha} \xi)(1 + \eta_{\alpha} \eta)(1 + \zeta_{\alpha} \zeta) / 8, \quad \alpha = 1, 2, \dots, 8, \quad (50)$$

where ξ_α , η_α , and ζ_α are the local coordinates of the corner nodes, which are numbered 1 to 4 progressing around the bottom face of the element in a counterclockwise direction and 5 to 8 around the top face of the element also counterclockwise direction, as shown in Fig. 3. The transformation from local coordinate (ξ, η, ζ) to the global coordinate (x, y, z) is achieved by

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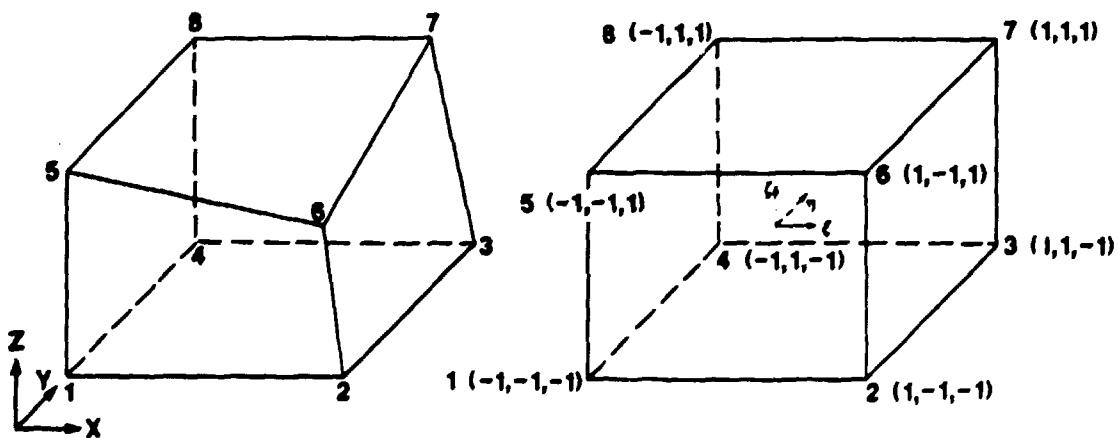


Fig. 3. Global coordinate vs local coordinate for a typical element

$$\begin{aligned}
 x &= \sum_{\alpha=1}^8 x_{\alpha} N_{\alpha}^e(\xi, \eta, \zeta) , & y &= \sum_{\alpha=1}^8 y_{\alpha} N_{\alpha}^e(\xi, \eta, \zeta) , & \text{and} \\
 z &= \sum_{\alpha=1}^8 z_{\alpha} N_{\alpha}^e(\xi, \eta, \zeta) . & & & (51)
 \end{aligned}$$

To complete the reduction of the PDE [Eq. (32)] to the ODE [Eq. (44)], one has to evaluate the integrals on the right-hand sides of Eqs. (45) through (49) for every element to yield the element mass matrix $[M^e]$ and stiff matrix $[S^e]$ as well as the element gravity column vector $[G^e]$, source/sink column vector $[Q^e]$, and boundary column vector $[B^e]$ as

$$M_{\alpha\beta}^e = \int_{R_e} N_{\alpha}^e F N_{\beta}^e dR , \quad (52)$$

$$S_{\alpha\beta}^e = \int_{R_e} (\nabla N_{\alpha}^e) \cdot K \cdot (\nabla N_{\beta}^e) dR , \quad (53)$$

$$G_{\alpha}^e = - \int_{R_e} (\nabla N_{\alpha}^e) \cdot K \cdot \nabla z dR , \quad (54)$$

$$Q_{\alpha}^e = \int_{R_e} N_{\alpha}^e q dR , \quad (55)$$

and

$$B_{\alpha}^e = - \int_{B_e} N_{\alpha}^e n \cdot (-K \cdot \nabla H) dB , \quad (56)$$

where the superscript or subscript e denotes the element and $\alpha, \beta = 1, 2, 3, 4, 5, 6, 7, \text{ or } 8$.

For a hexahedron element, Eqs. (52) through (55) are computed by Gaussian quadrature (Conte 1965) because it is not easy to solve Eq. (51) for ξ, η , and ζ in terms of x, y , and z . The computation of Eqs. (52) through (55) with the Gaussian quadrature is straightforward. However, the computation of Eq. (56) will need further elaboration, which will be described in Sect. 3.3.

3.2 Finite Difference Approximation in Time

An important advantage of finite element approximation over finite difference approximation is its inherent ability to handle complex boundaries and obtain the normal derivatives therein. In the time dimension, such advantages are not evident. Thus, finite difference methods are typically used in the approximation of the time derivative. Using a time weighting factor w , we obtain from Eq. (44) the following matrix equation:

$$[C](h)_{t+\Delta t} = (L) + (B) , \quad (57)$$

where $(h)_{t+\Delta t}$ is the column vector representing the values of (h) at time $(t + \Delta t)$ with Δt being the time step size, and the stiff matrix (C) and the load vector (L) are given as

$$[C] = [M]/\Delta t + w[S] , \quad (58)$$

and

$$\{L\} = \{D\} + \{Q\} + ([M]/\Delta t - (1 - w)[S])\{h\}_t , \quad (59)$$

in which w is the time weighting factor and $\{h\}_t$ is the values of $\{h\}$ at time t . When $w = 0$, the time integration is explicit. When $w = 0.5$, it is the Crank-Nicolson central difference. For the implicit (or backward) difference, w is equal to 1.0.

3.3 Numerical Implementation of Boundary Conditions

To incorporate the boundary conditions, we have to evaluate Eq. (56) for every boundary segment e to yield the load vector $\{B^e\}$. For the Cauchy boundary condition given by Eq. (37), we simply substitute Eq. (37) into Eq. (56) to yield a boundary-element column vector $\{B_C^e\}$ for a Cauchy segment:

$$\{B_C^e\} = \{q_C^e\} , \quad (60)$$

where $\{q_C^e\}$ is the Cauchy boundary flux vector given by

$$q_{c\alpha}^e = - \int_{B_e} N_\alpha^e q_C dB, \quad \alpha = 1, 2, 3, 4. \quad (61)$$

This Cauchy boundary flux vector represents the normal fluxes through the two nodal points of the segment B_e on B_C .

The surface integration of Eq. (61) in three-dimensional space is not as straightforward as the line integration in two-dimensional space. This integration requires further elaboration. Any surface integral of a continuous function $F(x,y,z)$ specified on the surface S (Fig. 4) can be reduced to the area integration. Let I represent the surface integral:

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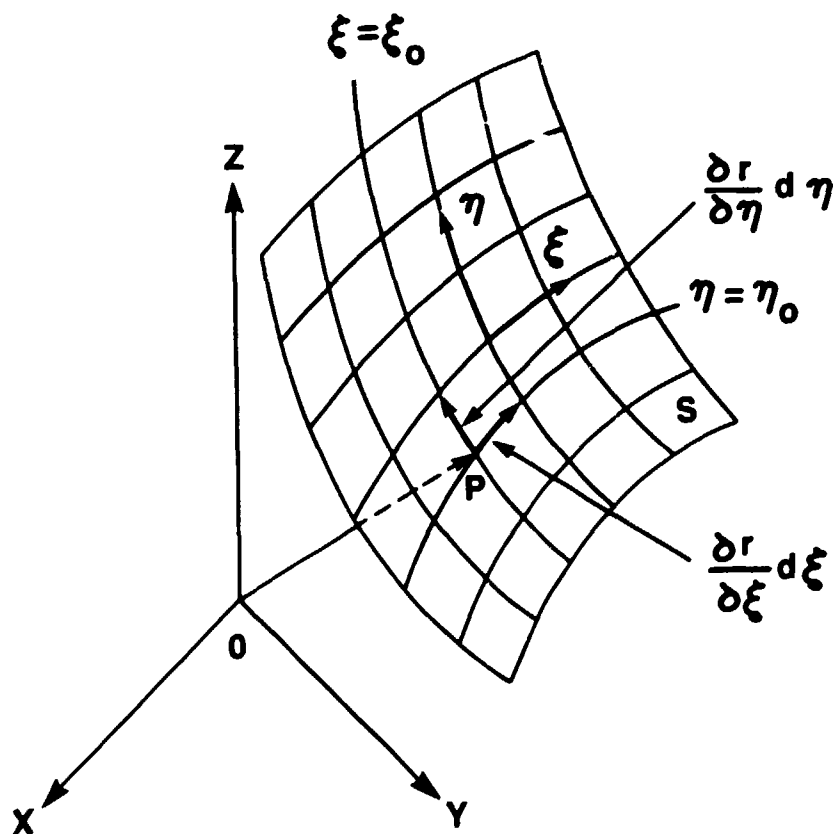


Fig. 4. A surface area and its imbedded local coordinate

$$I = \int_S F(x,y,z) dS \quad , \quad (62)$$

where

$$z = f(x,y) \quad (63)$$

is the equation for the surface S . Also, let P be any point on the surface S with coordinates (x,y,z) or (ξ,η) (Fig. 4). Then the vector r from O to P is given by

$$r = x i + y j + z k \quad . \quad (64)$$

The tangent vectors to the coordinate curves $\xi = \xi_0$ and $\eta = \eta_0$ on the surface S are $\partial r / \partial \eta$ and $\partial r / \partial \xi$, respectively (Fig. 4). The area dS of Fig. 4 is given by

$$dS = \left| \frac{\partial r}{\partial \xi} \times \frac{\partial r}{\partial \eta} \right| d\xi d\eta \quad , \quad (65)$$

where \times represents vector multiplication. But

$$\frac{\partial r}{\partial \xi} \times \frac{\partial r}{\partial \eta} = \begin{vmatrix} i & j & k \\ \frac{\partial x}{\partial \xi} & \frac{\partial y}{\partial \xi} & \frac{\partial z}{\partial \xi} \\ \frac{\partial x}{\partial \eta} & \frac{\partial y}{\partial \eta} & \frac{\partial z}{\partial \eta} \end{vmatrix} \quad (66)$$

so that

$$dS = \sqrt{J_x^2 + J_y^2 + J_z^2} d\xi d\eta \quad , \quad (67)$$

where

$$J_z = \begin{vmatrix} \frac{\partial x}{\partial \xi} & \frac{\partial y}{\partial \xi} \\ \frac{\partial x}{\partial \eta} & \frac{\partial y}{\partial \eta} \end{vmatrix} \quad (68a)$$

$$J_y = \begin{vmatrix} \frac{\partial x}{\partial \xi} & \frac{\partial z}{\partial \xi} \\ \frac{\partial x}{\partial \eta} & \frac{\partial z}{\partial \eta} \end{vmatrix} \quad (68b)$$

$$J_x = \begin{vmatrix} \frac{\partial z}{\partial \xi} & \frac{\partial y}{\partial \xi} \\ \frac{\partial z}{\partial \eta} & \frac{\partial y}{\partial \eta} \end{vmatrix} \quad (68c)$$

Substituting Eq. (67) into Eq. (62), we obtain

$$\int_S F(x,y,z) \, dS = \int_S \Phi(\xi,\eta) \left(J_x^2 + J_y^2 + J_z^2 \right)^{1/2} \, d\xi \, d\eta \quad (69)$$

where

$$\Phi(\xi,\eta) = F[x(\xi,\eta), y(\xi,\eta), z(\xi,\eta)] \quad (70)$$

Using Eq. (69), we can easily evaluate Eq. (61) with the Gaussian quadrature to yield the numerical value of q_c^e .

For the Neumann boundary condition given by Eq. (36), we substitute Eq. (36) into Eq. (56) to yield a boundary-element column vector $\{B_n^e\}$ for a Neumann segment:

$$\{B_n^e\} = \{q_n^e\}, \quad (71)$$

where $\{q_n^e\}$ is the Neumann boundary flux vector given by

$$q_{n\alpha}^e = \int_{B_e} (N_\alpha^e n \cdot K \cdot \nabla z - N_\alpha^e q_N^e) dB; \quad \alpha = 1, 2, 3, 4, \quad (72)$$

which is independent of the pressure head. Again using Eq. (69), we can easily compute the integral in Eq. (72) to obtain the Neumann boundary flux $q_{n\alpha}^e$.

The implementation of a variable-type boundary condition is more involved. It normally occurs at the air-soil interface. During a precipitation period, we will assume that only seepage or infiltration can occur for any point on the air-soil interface. No evapotranspiration is allowed since it is not likely to happen. If seepage occurs, the Dirichlet boundary condition, Eq. (38), must be imposed. On the other hand, if infiltration occurs, either the Dirichlet boundary condition, Eq. (38), or the Cauchy boundary condition, Eq. (39), may be specified,

depending on the soil properties and throughfall rate q_p in Eq. (39). The problem is which equation, Eq. (38) or Eq. (39), should be prescribed for a point on the boundary. This problem is settled by iteration. The procedure adopted is as follows. At each iteration, we examine the solution at each node along the variable boundary and test whether the existing boundary condition is still consistent. Specifically, if the existing condition is Eq. (39) (Cauchy boundary condition), we compute the pressure head at the boundary node. If the head is greater than the allowed ponding depth h_p in Eq. (38), too much water has been forced into the region through the node. In other words, the throughfall rate is greater than that which the medium can absorb. To account for this, the boundary condition is changed to Eq. (38), which in practice should result in infiltration at a rate less than q_p in Eq. (39) or result in seepage. If the computed head is less than the ponding depth, the medium is capable of absorbing all throughfall and no change of boundary condition is required. On the other hand, if the existing boundary condition is Eq. (38) (Dirichlet boundary condition), we compute Darcy's flux at the node. If the computed Darcy flux is going out of the region (seepage) or into the region (infiltration) but its magnitude is less than q_p in Eq. (39), no change of boundary condition is needed. However, if the computed Darcy flux is directed into the region (infiltration) with a rate greater than the throughfall rate q_p , a change of boundary condition to Eq. (39) is required since Eq. (38) would force more water than available into the region. By changing the boundary condition to Eq. (39), it should in practice result in a pressure head less than h_p . The iteration outlined

above is discontinued when no changeover of boundary condition is encountered along the entire boundary.

Similarly, during a nonprecipitation period, we will assume that only evapotranspiration or seepage can occur and no infiltration is allowed. If seepage actually occurs at a node, Eq. (40) (Dirichlet boundary condition) must be specified at the node. On the other hand, if evapotranspiration happens, either Eq. (41) (Dirichlet boundary condition) or Eq. (42) (Cauchy boundary condition) may be imposed at the node. The problem is again to determine which of the three equations should be used as boundary conditions. Iteration procedure is used to solve the problem. If the existing boundary condition is Eq. (40), we calculate Darcy's flux. When the computed Darcy flux is going out of the region, the existing boundary condition is consistent and no change on boundary condition is necessary. When the Darcy flux is directed into the region (remember no infiltration is allowed), the application of Eq. (40) implies the infiltration and prohibits evapotranspiration. Hence, the boundary condition is changed to Eq. (42), which in practice would generate evapotranspiration and would result in a pressure head lower than the ponding depth in Eq. (40). If the existing boundary condition is Eq. (41), we compute the Darcy flux. Since the minimum pressure is prescribed on the boundary, it is unlikely that this computed Darcy flux will be directed into the region. Thus, when the computed outgoing Darcy flux is less than q_e in Eq. (42), the existing boundary condition is consistent and no change on boundary condition is needed. When the computed Darcy

flux is greater than q_e in Eq. (42), the application of Eq. (41) implies the imposition of too much suction at the node. Hence, the boundary condition is changed to Eq. (42), which in practice should result in a pressure head greater than h_m in Eq. (41). If the existing boundary condition is Eq. (42), we calculate pressure head at the node. If this computed pressure head is not lower than h_m in Eq. (41), the boundary condition is consistent and no change is required. However, if the computed head is lower than h_m in Eq. (41), the application of Eq. (42) implies that too much water is removed through the node yielding too low a pressure head. Hence, the boundary condition is changed to Eq. (41), which should yield an evapotranspiration rate less than q_e in Eq. (42). This iteration process is completed only when consistent boundary conditions have been applied to all nodes on the variable boundary.

During the iteration of boundary conditions on the variable boundary, one of the Eqs. (38) through (42) is used at a node. If either Eq. (39) or (42) is used, we substitute it into Eq. (56) to yield a boundary element column vector $\{B_v^e\}$ for a variable boundary segment:

$$\{B_v^e\} = \{q_v^e\}, \quad (73)$$

where $\{q_v^e\}$ is the variable boundary flux given by

$$q_{v\alpha}^e = - \int_{B_e} N_{\alpha}^e q_p dB, \quad \text{or} \quad q_{v\alpha}^e = - \int_{B_e} N_{\alpha}^e q_e dB; \quad \alpha = 1, 2, 3, 4. \quad (74)$$

Assembling over all Neumann, Cauchy, and variable boundary segments, we obtain the global boundary column vector (B) as

$$(B) = (q) , \quad (75)$$

in which

$$(q) = \sum_{e \in N_{ne}} (q_n^e) + \sum_{e \in N_{ce}} (q_c^e) + \sum_{e \in N_{ve}} (q_v^e) , \quad (76)$$

where N_{ne} , N_{ce} , and N_{ve} are the number of Neumann boundary segments, Cauchy boundary segment, and variable boundary segments with flux conditions imposed on them, respectively.

Substituting Eq. (75) into Eq. (57) and dropping the subscript $(t + \Delta t)$ to simplify the notation, we obtain

$$[C](h) = (R) , \quad (77)$$

where (R) is given by

$$(R) = (L) + (q) . \quad (78)$$

At nodes where Dirichlet boundary conditions are applied, an identity equation is generated for each node and included in the matrices of Eq. (77). The detailed method of applying this type of boundary condition can

be found elsewhere (Wang and Connor, 1975). The Dirichlet nodes include the nodes on the Dirichlet boundary and the nodes on the variable boundary to which either Eq. (38), (40), or (41) is applied.

3.4 Solution of the Matrix Equations

The matrix equation, Eq. (77), is linear only when the entire region of interest is under saturated conditions. If part of the region is unsaturated, the governing equation, Eq. (32), is nonlinear, hence Eq. (77) is a nonlinear matrix equation. To solve it, some type of iterative procedure is required. The approach taken here is to make an initial estimate of the unknown (h^k) . Using this estimate, we then compute the coefficient matrix $[C]$ and solve the linearized matrix equation by the method of linear algebra. The new estimate is now obtained by the weighted average of the new solution and the previous estimate:

$$\{h^{(k+1)}\} = \{h\} + (1 - \omega)\{h^k\}, \quad (79)$$

where $\{h^{(k+1)}\}$ is the new estimate, $\{h^k\}$ is the previous estimate, $\{h\}$ is the new solution, and ω is the iteration parameter. The procedure is repeated until the new solution $\{h\}$ is within a tolerance error. When the iteration parameter is greater than or equal to 0 but is less than 1, the iteration is termed under-relaxation. If $\omega = 1$, the method is the exact relaxation. For the cases when ω is greater than 1 but less than or equal to 2, the iteration is termed overrelaxation. The underrelaxation option should be used to overcome cases when nonconvergency or the slow

convergence rate is due to fluctuation rather than due to "blowup" computations. Overrelaxation should be used to speed up the convergence rate when the rate of convergence decreases monotonically.

Two options are employed to solve the linearized matrix equation: one is the direct elimination method and the other is pointwise iteration. When the direct elimination method is used to solve the matrix equation, a single iteration loop is used to iterate the nonlinearity. However, when pointwise iterations are used, a double loop is required: the inner loop to solve the linearized equation and the outer loop to iterate the nonlinearity. Three options have been employed when the pointwise iteration method is used to solve the linearized matrix equation. These are the successive under-relaxation (SUR), Gauss-Seidel (G-S) iteration, and successive over-relaxation (SOR). These three methods are unified by a relaxation parameter, Ω . When the relaxation parameter is less than 1 but greater than or equal to 0, the method is termed SUR iteration. When Ω is equal to 1, the method is termed G-S iteration. If the relaxation parameter is greater than 1 but less than or equal to 2, the method is termed SOR iteration.

There are six options in 3DFEMWATER to solve the finite element equations. These are the combination of two ways to solve a given set of linearized algebraic equations and three ways of estimating the coefficient matrix.

3.5 Computation of Mass Balance

One of the most important aspects in numerical modeling of subsurface flow is to check the mass balance over the whole region. The error in mass balance provides a crude index on the accuracy and convergence of numerical computations. The mass balance over a region R enclosed by the boundary $B(x,y,z) = 0$ can be obtained by integrating Eq. (32):

$$F_V = \int_R \left(F \frac{\partial h}{\partial t} - q \right) dR \quad , \quad (80)$$

and

$$F_B = \int_B F_n dB \quad , \quad (81)$$

where F_V represents the net volumetric increasing rate of water in the region, F_B is the net volumetric flow rate through the entire boundary out from the region, and F_n is the outward normal flux. In fact, F_n can be defined as

$$F_n = -n \cdot K \cdot \nabla H \quad (82)$$

Having obtained the pressure head field by solving Eq. (77), one can integrate Eqs. (80) and (81) independently. If the solution for h is free of error, one would expect the sum of two integrals equal to zero. In the present report, the integral of Eq. (82) is broken into two parts:

$$F_P = \int_R F \frac{\partial h}{\partial t} dR \quad , \quad (83a)$$

and

$$F_S = \int_R q \, dR , \quad (83b)$$

where F_p and F_S represent the volumetric rates due to head change and artificial sources, respectively. Similarly, the integral in Eq. (82) is broken into six parts:

$$F_D = \int_{B_D} F_n \, dB , \quad (84a)$$

$$F_C = \int_{B_C} F_n \, dB , \quad (84b)$$

$$F_N = \int_{B_N} F_n \, dB , \quad (84c)$$

$$F_{VO} = \int_{B_{VO}} F_n \, dB , \quad (84d)$$

$$F_{VI} = \int_{B_{VI}} F_n \, dB , \quad (84e)$$

and

$$F_L = \int_{B - B_D - B_C - B_N - B_V} F_n \, dB , \quad (84f)$$

in which F_D , F_C , F_N , F_{VO} , F_{VI} , and F_L represent fluxes through the

Dirichlet boundary B_D , the Cauchy boundary B_C , the Neumann boundary B_N , the part of the variable boundary B_{V0} with flow going out from the region, the part of the variable boundary B_{V1} with flow going into the region, and the unspecified boundary $B-B_D-B_C-B_N-B_V$.

For an exact solution, the sum of the net outgoing flux F_B across the entire boundary and the total volumetric increase rate F_V should be equal to zero. In addition, F_L should theoretically be equal to zero. However, in any practical simulation, F_B plus F_V will not be equal to zero, and F_L will be nonzero. Nevertheless, the mass balance computation should provide a means to check the numerical scheme and the consistency in the computer code.

4. DESCRIPTION OF THE COMPUTER PROGRAM

4.1 Purpose of 3DFEMWATER

There are two source codes for 3DFEMWATER. Both of these two codes are designed to solve the initial and boundary value problems given by Eqs. (32) and (34) through (42). We have used the subregional block iteration methods (Yeh et al. 1985) in one code (referred to as code BLI), which is listed in Appendix A. For the other code (referred to as code PTI), listed in Appendix B, we have used the point iteration method. The differences between BLI and PTI are: (1) in BLI two subroutines BLKTR and SOLVE are used to solve the matrix equation, whereas in PTI the subroutine PISS is used to solve the matrix equation; (2) for BLI five pointer arrays are generated in subroutine PAGEN, whereas for PTI only one pointer array is generated in subroutine PAGEN; (3) the controlling subroutine GW3D for BLI contains more variables than for PTI; and (4) the subroutine DATAIN for BLI needs to read additional data about subregional information, whereas that for PTI does not need to read those data.

To refresh our memory, we restate the governing equation and initial and boundary conditions that 3DFEMWATER is designed to solve:

Governing Equation

$$F \frac{\partial h}{\partial t} = \nabla \cdot [K_s K_r (\nabla h + \nabla z)] + q \quad (85)$$

where h is the pressure head, t is time, K_s is the saturated hydraulic conductivity tensor, K_r is the relative hydraulic conductivity or relative permeability, z is the potential head, q is the source and/or sink, and F is the water capacity given by

$$F = d\theta/dh \quad (86)$$

after we have neglected the compressibility of the water and media. In Eq. (86) θ is the moisture content.

Initial Conditions

$$h = h_1(x, y, z) \quad \text{in } R, \quad (87)$$

where R is the region of interest and h_1 is the prescribed initial condition, which can be defined or obtained by solving the steady state version of Eq. (85).

Boundary Conditions

Dirichlet Conditions:

$$h = h_d(x_b, y_b, z_b, t) \quad \text{on } B_d. \quad (88)$$

Neumann Conditions:

$$-n \cdot K_s K_r \cdot \nabla h = q_n(x_b, y_b, z_b, t) \quad \text{on } B_r \quad (89)$$

Cauchy Conditions:

$$-n \cdot (K_s K_r \cdot \nabla h + K_s K_r \cdot \nabla z) = q_c(x_b, y_b, z_b, t) \quad \text{on } B_c \quad (90)$$

Variable Conditions - During Precipitation Period:

$$h = h_p(x_b, y_b, z_b, t) \quad \text{on } B_v \quad (91a)$$

or

$$-n \cdot (K_s K_r \cdot \nabla h + K_s K_r \cdot \nabla z) = q_p(x_b, y_b, z_b, t) \quad \text{on } B_v \quad (91b)$$

Variable Conditions - During Nonprecipitation Period:

$$h = h_p(x_b, y_b, z_b, t) \quad \text{on } B_v \quad (91c)$$

or

$$h = h_m(x_b, y_b, z_b, t) \quad \text{on } B_v \quad (91d)$$

or

$$-n \cdot K_s K_r \cdot (\nabla h + \nabla z) = q_e(x_b, y_b, z_b, t) \quad \text{on } B_v \quad (91e)$$

where (x_b, y_b, z_b) is the spatial coordinate on the boundary; n is an

outward unit vector normal to the boundary; h_d , q_n , and q_c are the prescribed Dirichlet functional value, Neumann flux, and Cauchy flux, respectively; B_d , B_n , and B_c are the Dirichlet, Neumann, and Cauchy boundary, respectively; B_v is the variable boundary; h_p is the allowed ponding depth and q_p is the throughfall of precipitation, respectively, on the variable boundary; h_m is the allowed minimum pressure on the variable boundary; and q_e is the allowed maximum evaporation rate on the variable boundary, which is the potential evaporation. Only one of Eqs. (91a) through (91e) is used at any point on the variable boundary at any one time.

4.2 Program Structure

The description in this section is for the computer code that employs the subregional block iteration method (BLI). Whenever the description is not valid for the code that uses the point iteration method (PTI), it is noted.

3DFEMWATER consists of a MAIN program, a section of BLOCK DATA for specifying the size of array dimensions, and 22 subroutines for Code BLI or 21 subroutines for Code PTI. The MAIN is used to specify the sizes of all arrays. The control and coordinate activity are performed by the subroutine GW3D. Figure 5 shows the structure of the program. The functions of these subroutines are described below.

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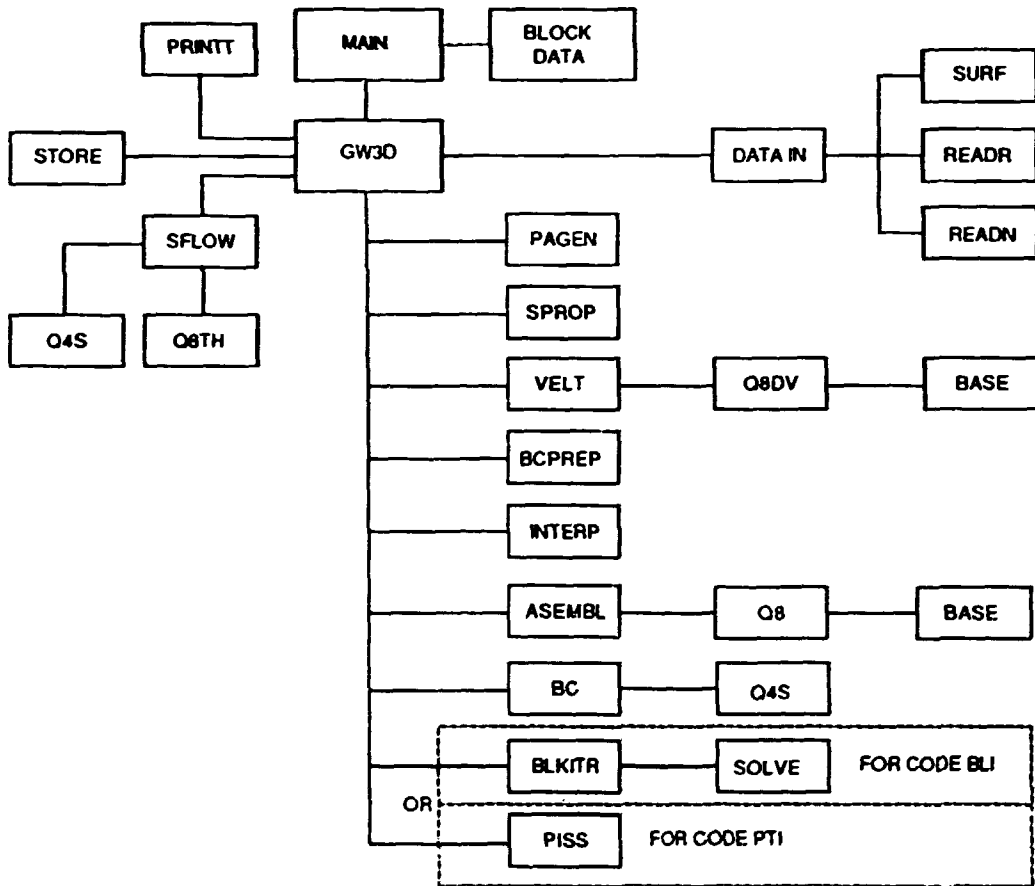


Fig. 5. Program structure of 3DFEMWATER

Subroutine GW3D

The subroutine GW3D controls the entire sequence of operations, a function generally performed by the MAIN program. It is, however, preferable to keep a short MAIN and several subroutines with variable storage allocation. This makes it possible to place most of the FORTRAN deck on a permanent file and to deal with a site-specific problem without making changes in array dimensions throughout all subroutines.

The subroutine GW3D will perform either the steady state computation alone ($KSS = 0$ and $NTI = 0$), or a transient state computation using the steady-state solution as the initial conditions ($KSS = 0$, $NTI > 0$), or a transient computation using user-supplied initial conditions ($KSS = 1$, $NTI > 0$). The flow chart of this subroutine is given in Fig. 6.

GW3D calls to subroutine DATAIN to read and print input data; subroutine PAGEN to generate pointer arrays; subroutine INTERP to obtain sources/sinks and boundary values; subroutine SPROP to obtain the relative hydraulic conductivity, water capacity, and moisture content from the pressure head; subroutine VELT to compute Darcy's velocity; subroutine BCPREP to determine if a change of boundary conditions is required; subroutine ASEMBL to assemble the element matrices over all elements; subroutine BC to implement the boundary conditions; subroutine BLKTR to form and solve the subregional block matrix equations for BLI or subroutine PISS to solve the matrix equation for PTI; subroutine SFLOW to

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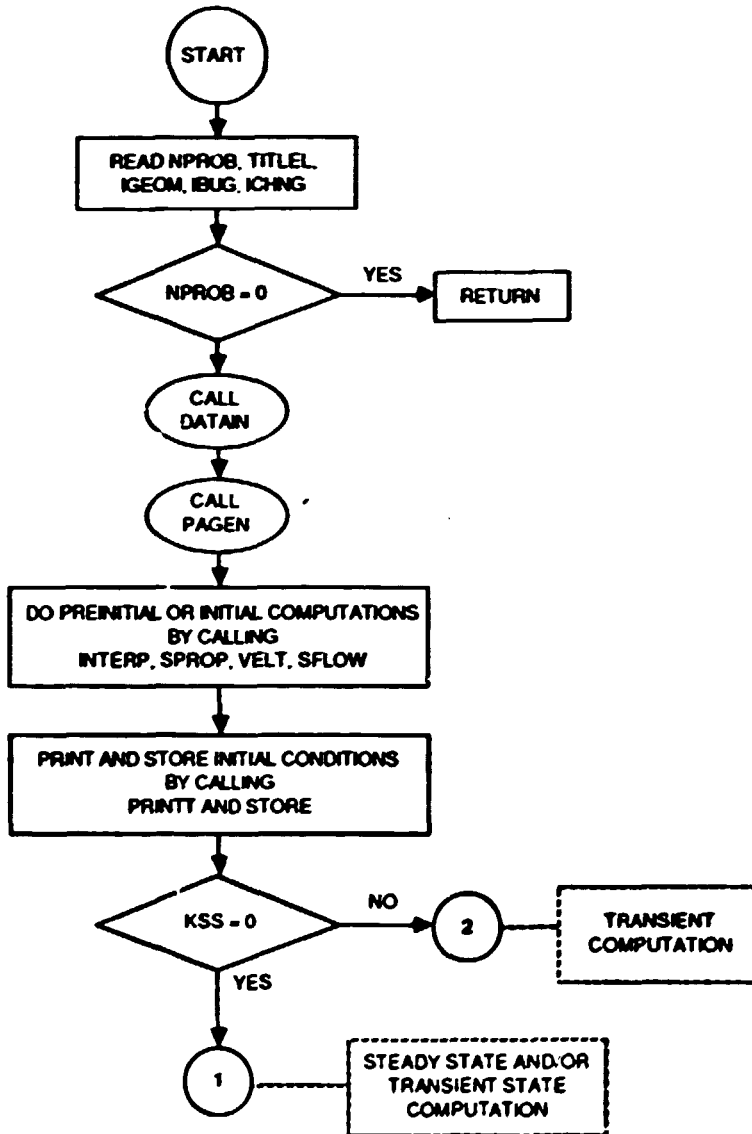


Fig. 6. Flow chart of subroutine GW3D (the first of three parts).

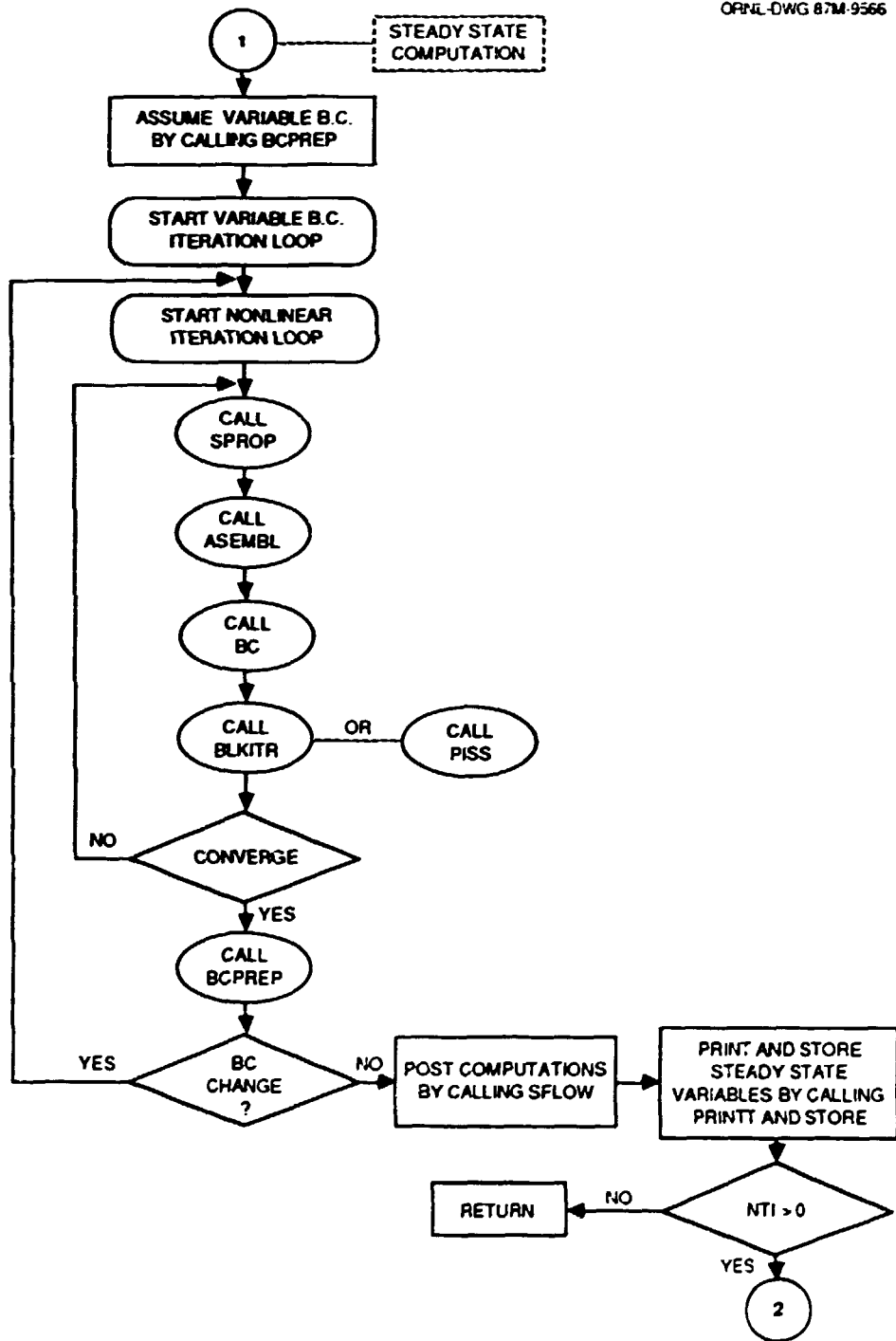


Fig. 6. Flow chart of subroutine GW3D (the second of three parts).

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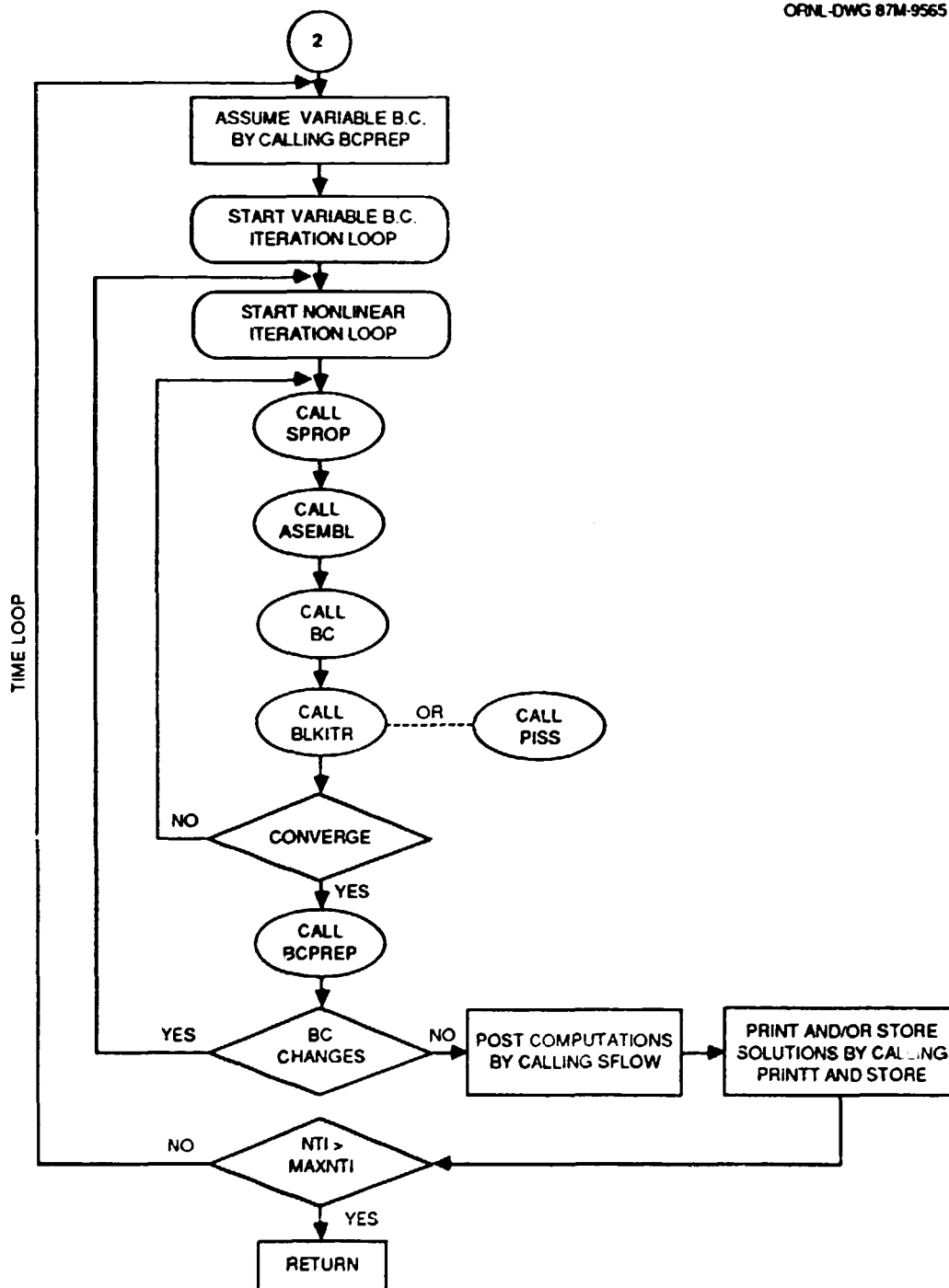


Fig. 6. Flow chart of subroutine GW3D (3 of 3)
(the third of three parts).

calculate flux through all types of boundaries and water accumulated in the media; subroutine PRINTT to print out the results; and subroutine STORE to store the flow variables for input to a 3DFEMWASTE or for plotting (Fig. 5).

Subroutine DATAIN

Subroutine DATAIN reads all data input described in Sect. 5.3 except the card group 1. It also prints all the input information, and calls subroutine SURF to identify the surface elements and boundary nodes and subroutines READR and READN, respectively, to automatically generate real and integer numbers.

Subroutine SURF

Subroutine SURF identifies the boundary sides, sequences the boundary nodes, and computes the directional cosine of the surface sides. The mappings from boundary nodes to global nodes are stored in NPBB(I) (where NPBB(I) is the global node number of i-th boundary node). The boundary node numbers of the four nodes for each boundary side are stored in ISB(I,J) (where ISB(I,J) is the boundary node number of I-th node of J-th side, I = 1 to 4). There are six sides for each element. Which of these six sides is the boundary side is determined automatically in the subroutine SURF and is stored in ISB(5,J). The global element number, to which the J-th boundary side belongs, is also preprocessed in the subroutine SURF and is stored in ISB(6,J). The directional cosines of the J-th boundary side are computed and stored in DCOSB(I,J) (where DCOSB(I,J)

is the directional cosine of the J-th surface with I-th coordinate, I = 1 to 3). The information contained in NPBB, ISB, and DOSB, along with the number of boundary nodes and the number of boundary sides is returned to subroutine DATAIN for other users.

Subroutine READR

This subroutine is called by the subroutine DATAIN to generate real numbers for data sets 7, 14(e), and 14(f) of Sect. 5.3. Automatic generation of regularly patterned data is built into this subroutine.

Subroutine READN

This subroutine is also called by the subroutine DATAIN to generate integer data sets 8, 9, 12(c), 12(f), 14(b) through 14(d), 15(c), 16(b), 16(c), 17(b), and 17(c) of Sect. 5.3.

Subroutine PAGEN

This subroutine is called by the controlling subroutine GW3D to preprocess pointer arrays that are needed to store the global matrix in compressed form and to construct the subregional block matrices. The pointer arrays automatically generated in this subroutine include the global node connectivity (stencil) GNOJCN(J,N), regional node connectivity LNOJCN(J,I,K), total node number for each subregion NTNPLR(K), bandwidth indicator for each subregion LMAXDF(K), and partial fill-up for the mapping array between global node number and local subregion node number GNPLR(I,k) with I = NNPLR(K) + 1 to NTNPLR(K). Here GNOJCN(J,N) is the

global node number of J-th node connected to the global node N; LNOJN(J,I,K) is the local node number of J-th node connected to the local node I in K-th subregion; NTNPLR(K) is the total number of nodes in the K-th subregion, including the interior nodes, the global boundary nodes, and intra-boundary nodes; LMAXDF(K) is the maximum difference between any two nodes of any element in K-th subregion; and GNPLR(I,K) is the global node number of I-th local-region node in the K-th subregion. These pointer arrays are generated based on the element connectivity IE(M,J), the number of node for each subregion NNPLR(K), and the mapping between global node and local-region node GNLR(I,K) with $I = 1, NNPLR(K)$. Here IE(M,J) is the global node number of J-th node of element M; NNPLR(K) is the number of nodes in the K-th subregion including the interior nodes and the global boundary nodes but not the intraboundary nodes.

Subroutine INTERP

This subroutine is called by the subroutine GW3D to compute the functional values (such as the Dirichlet total head, element source/sink, point source/sink, Neumann fluxes, Cauchy fluxes, and rainfall) at a particular time for all profiles. It uses the linear interpolation of the tabular data.

Subroutine SPROP

This subroutine calculates the values of moisture content, relative hydraulic conductivity, and the water capacity. Analytical functions are

used. Thus, the users must supply the functional form.

Subroutine VELT

This subroutine calls Q8DV to evaluate the element matrices and the derivatives of the total head. It then sums over all element matrices to form a matrix equation governing the velocity components at all nodal points. To save computational time, the matrix is diagonalized by lumping. The velocity components can thus be solved point by point. The computed velocity field is then returned to GW3D through the argument. This velocity field is also passed to subroutine BCPREP to evaluate the Darcy flux across the seepage-infiltration-evapotranspiration surfaces.

Subroutine Q8DV

Subroutine Q8DV is called by the subroutine VELT to compute the element matrices given by

$$QB(I,J) = \int_{R_e} N_i^e N_j^e dR \quad , \quad (92a)$$

where N_i^e and N_j^e are the basis functions for nodal point i and j of element e , respectively. Subroutine Q8DV also evaluates the element load vector:

$$QRX(I) = - \int_{R_e} N_i^e i \cdot K_s K_r \cdot (\nabla N_j^e) H_j dR \quad , \quad (92b)$$

$$QRZ(I) = - \int_{R_e}^r N_i^e j \cdot K_s K_r \cdot (\nabla N_j^e) H_j dR , \quad (92c)$$

$$QRZ(I) = - \int_{R_e}^r N_i^e k \cdot K_s K_r \cdot (\nabla N_j^e) H_j dR , \quad (92d)$$

where

H_j - the total head at nodal point j ,

i - the unit vector along the x-coordinate,

j - the unit vector along the y-coordinate,

k - the unit vector along the z-coordinate,

K_s - the saturated hydraulic conductivity tensor,

K_r - the relative hydraulic conductivity.

Subroutine BCPREP

This subroutine is called by GW3D to prepare the infiltration-seepage boundary conditions during a rainfall period or the seepage-evapotranspiration boundary conditions during non-rainfall periods. It decides the number of nodal points on the variable boundary to be considered as Dirichlet or Cauchy points. It computes the number of points that change boundary conditions from ponding depth (Dirichlet types) to infiltration (Cauchy types), or from infiltration to ponding depth, or from minimum pressure (Dirichlet types) to infiltration during rainfall periods. It also computes the number of points that change boundary conditions from potential evapotranspiration (Cauchy types) to

minimum pressure, or from ponding depth to potential evapotranspiration, or from minimum pressure to potential evapotranspiration during non-rainfall periods. Upon completion, this subroutine returns the Darcy flux (DCYFLX), infiltration/potential evapotranspiration rate (FLX), the ponding depth nodal index (NPCON), the flux-type nodal index (NPFLX), the minimum pressure nodal index (NPMIN), and the number of nodal points (NCHG) that have changed boundary conditions.

Subroutine ASEMBL

This subroutine calls Q8 to evaluate the element matrices. It then sums over all element matrices to form a global matrix equation governing the pressure head at all nodes.

Subroutine Q8

This subroutine is called by the subroutine ASEMBL to compute the element matrix given by

$$QA(I,J) = \int_{R_e} N_1^e F N_j^e dR, \quad (93a)$$

$$QB(I,J) = \int_{R_e} (\nabla N_1^e) \cdot K_s K_r \cdot (\nabla N_j^e) dR, \quad (93b)$$

where F is the soil property function. Subroutine Q8 also calculates the element load vector given by

$$RQ(I) = \int_{R_e} [(\nabla N_i^e) \cdot K_S K_T \cdot (\nabla z) - N_i^e q] dR \quad , \quad (93c)$$

where q is the source/sink.

Subroutine BASE

This subroutine is called by subroutines Q8DV and Q8 to evaluate the value of the base function at a Gaussian point. The computation is straightforward.

Subroutine BC

This subroutine incorporates Dirichlet, Cauchy, Neumann, and variable boundary conditions. For a Dirichlet boundary condition, an identity algebraic equation is generated for each Dirichlet nodal point. Any other equation having this nodal variable is modified accordingly to simplify the computation. For a Cauchy surface, the integration of the surface source is obtained by calling the subroutine Q4S, and the result is added to the load vector. For a Neumann surface, the integrations of both the gradient and gravity fluxes are obtained by calling the subroutine Q4S. These fluxes are added to the load vector. The subroutine BC also implements the variable boundary conditions. First, it checks all infiltration-evapotranspiration-seepage points, identifying any of them that are Dirichlet points. If there are Dirichlet points, the method of incorporating Dirichlet boundary conditions mentioned above is used. If a given point is not the Dirichlet point, the point is bypassed. Second, it

checks all rainfall-evaporation-seepage points again to see if any of them is a Cauchy point. If it is a Cauchy point, then the computed flux by infiltration or potential evapotranspiration is added to the load vector. If a given point is not a Cauchy point, it is bypassed. Because the infiltration-evaporation-seepage points are either Dirichlet or Cauchy points, all points are taken care of in this manner.

Subroutine Q4S

This subroutine is called by the subroutines BC and SFLOW to compute the surface node flux of the type

$$RQ(I) = \int_{R_e} N_1^e q \, dB, \quad (94)$$

where q is either the Cauchy flux, Neumann flux, or gravity flux.

Subroutine BLKTR

This subroutine is called by the subroutine GW3D to solve the matrix equation with block iteration methods. For each subregion, a block matrix equation is constructed based on the global matrix equation and two pointer arrays GNPLR and LNOJCN (see subroutine PAGEN), and the resulting block matrix equation is solved with the direct band matrix solver by calling subroutine SOLVE. This is done for all subregions for each iteration until a convergent solution is obtained. This subroutine and the subroutine SOLVE, to be described in the next paragraph, are needed only for the code BLI.

Subroutine SOLVE

This subroutine is called by the subroutine BLKTR to solve for the matrix equation of the type

$$[C](x) = (y) . \quad (95)$$

where [C] is the coefficient matrix and (x) and (y) are two vectors. (x) is the unknown to be solved, and (y) is the known load vector. The computer returns the solution (y) and stores it in (y). The computation is a standard banded Gaussian direct elimination procedure.

Subroutine PISS

This subroutine is called by the subroutine GW3D to solve the matrix equation with point iteration methods. This subroutine is needed only for the code PTI.

Subroutine PRINTI

This subroutine is used to line-print the flow variables. These include the fluxes through variable boundary surfaces, the pressure head, total head, moisture content, and Darcy's velocity components.

Subroutine STORE

This subroutine is used to store the flow variables on Logical Unit 1. It is intended for use with a subsequent computer model 3DFEMWASTE, or for plotting. The information stored includes region geometry, subregion data, and hydrological variables such as pressure head, total head,

moisture content, and Darcy's velocity components.

Subroutine SFLOW

This subroutine is used to compute the fluxes through various types of boundaries and the increasing rate of water content in the region of interest. The function of FRATE(7) is to store the flux through the whole boundary enclosing the region of interest. It is given by

$$\text{FRATE}(7) = \int_B (V_x n_x + V_y n_y + V_z n_z) dB, \quad (96)$$

where B is the global boundary of the region of interest; V_x , V_y , and V_z are Darcy's velocity components; and n_x , n_y , and n_z are the directional cosines of the outward unit vector normal to the boundary B . FRATE(1) through FRATE(5) store the flux through Dirichlet boundary B_D , Cauchy boundary B_C , Neumann boundary B_N , the seepage/evapotranspiration boundary B_S , and infiltration boundary B_R , respectively, and are given by

$$\text{FRATE}(1) = \int_{B_D} (V_x n_x + V_y n_y + V_z n_z) dB, \quad (97a)$$

$$\text{FRATE}(2) = \int_{B_C} (V_x n_x + V_y n_y + V_z n_z) dB, \quad (97b)$$

$$\text{FRATE}(3) = \int_{B_N} (V_x n_x + V_y n_y + V_z n_z) dB, \quad (97c)$$

$$\text{FRATE}(4) = \int_{B_S} (v_x n_x + v_y n_y + v_z n_z) dB , \quad (97d)$$

$$\text{FRATE}(5) = \int_{B_R} (v_x n_x + v_y n_y + v_z n_z) dB . \quad (97e)$$

FRATE(6), which is related to the numerical loss, is given by

$$\text{FRATE}(6) = \text{FRATE}(7) - \sum_{I=1}^5 \text{FRATE}(I) . \quad (98)$$

FRATE(8) and FRATE(9) are used to store the source/sink and increased rate of water within the media, respectively:

$$\text{FRATE}(8) = - \int_R q dR , \quad (99)$$

and

$$\text{FRATE}(9) = \int_R F \frac{\partial h}{\partial t} dR . \quad (100)$$

If there is no numerical error in the computation, the following equation should be satisfied:

$$\text{FRATE}(9) = - [\text{FRATE}(7) + \text{FRATE}(8)] , \quad (101)$$

and FRATE(6) should be equal to zero. Equation (98) simply states that the negative rate of water going out from the region through the entire boundary and due to a source/sink is equal to the rate of water accumulated in the region.

Subroutine Q8TH

This subroutine is used to compute the contribution of the increasing rate of the water content from an element e

$$QTHP = \int_{R_e} \frac{\partial \theta}{\partial h} \frac{\partial h}{\partial t} dR . \quad (102)$$

The computation of the above integration is straightforward.

5. USER'S MANUAL

The following describes what one should do about 3DFEMWATER code for each site-specific application and how data input should be prepared.

5.1 Specifications of Array Dimensions

The subscripted variable arrays have to be dimensioned for each site-specific problem in the MAIN program (see example problems). Seventy-eight (78) array variables contained between lines MAIN 130 and MAIN 305 in the source code (Appendix A) should be dimensioned according to the indicated subscripts (a total of 35). The listing and definitions of these parameters and their associated subscripts (maximum-control numbers) are given below:

Arrays for Node Coordinates and Element Connectivity

X(MAXNP), Y(MAXNP), Z(MAXNP), IE(MAXEL,9);

MAXEL - maximum number of elements,

MAXNP - maximum number of nodes;

X(NP) - x-coordinate of NP-th nodal point,

Y(NP) - y-coordinate of NP-th nodal point,

Z(NP) - z-coordinate of NP-th nodal point,

IE(M,I) - global node number of the I-th node of the M-th element if I is between 1 and 8, integer to indicate the material type of the M-th element if I is equal to 9.

Arrays to Store the Global Matrix, Global Stencil, and Load Vector

CMATRIX(MAXNP,JBAND), GNOJCN(JBAND,MAXNP), RLD(MAXNP), RI(MAXNP), RL(MAXNP);

JBAND - maximum number of nonzero elements in any row of the matrix;

CMATRIX(NP,I) - an array to store the assembled global matrix,

GNOJCN(I, NP) - global node number of I-th node connected to node NP,
 RLD(NP) - an array to store the assembled global load vector,
 RI(NP) - pressure head iterate in subroutine BLKPTR,
 RL(NP) - a working array to contain final solution for the
 pressure head in subroutine BLKPTR.

Arrays for Subregions (These arrays are not needed for Code PTI)

NTNPLR(MXREGN), LMAXDF(MXREGN), NNPLR(MXREGN),
 GNLR(LTMXNP, MXREGN), LNOJCN(JBAND, LMXNP, MXREGN),
 CMTRXL(LMXNP, LMXBW), RLDL(LMXNP);

MXREGN - maximum number of subregions,

LTMXNP - maximum number of total nodal points in any subregion,
 including interior nodes, global boundary nodes, and
 intraboundary nodes,

LMXBW - maximum number of the bandwidth in any subregion;

NTNPLR(K) - total number of nodes for K-th subregion including
 interior and global boundary and intra-boundary nodes,
 LMAXDF(K) - maximum difference between any two nodes of any
 element in K-th subregion,

NNPLR(K) - number of interior nodes for K-th subregion, including
 global boundary nodes,

GNLR(I, K) - global nodal number of I-th local nodal number for
 K-th subregion,

LNOJCN(J, I, K) - local node number of J-th connecting node surrounding
 I-th local node for K-th subregion,

CMTRXL(NP, I) - assembled matrix for a subregion,

RLDL(NP) - assembled load vector for a subregion.

Arrays for Hydrological Variables and Nonconvergent Nodes

H(MAXNP), HP(MAXNP), HW(MAXNP), HT(MAXNP),
 VX(MAXNP), VY(MAXNP), VZ(MAXNP),
 TH(8, MAXEL), DTH(8, MAXEL), AKR(8, MAXEL)
 NPCNV(MAXNP);

H(NP) - pressure head at NP-th node,

HP(NP) - pressure head of NP-th node at previous time,

HW(NP) - nonlinear pressure head iterate of NP-th node,

HT(NP) - total head of NP-th node,

VX(NP) - x-component velocity at NP-th node,

VY(NP) - y-component velocity at NP-th node,

VZ(NP) - z-component velocity at NP-th node,

TH(I, M) - water content at I-th gaussian point of M-th element,
 DTH(I, M) - dTH/dH - water capacity of I-th gaussian point of
 M-th element,

AKR(I, M) - relative hydraulic conductivity at I-th gaussian
 point of M-th element,

NPCNV(NP) - nodal point of NP-th nonconvergent node.

Arrays for Boundary Surfaces

DCOSB(3,MAXBES), ISB(6,MAXBES), NPBB(MAXBNP),
BFLX(MAXBNP), BFLXP(MAXBNP);

MAXBES - maximum number of boundary-element surfaces,

MAXBNP - maximum number of boundary nodal points;

DCOSB(1,I) - x-directional cosine of I-th boundary element surface,

DCOSB(2,I) - y-directional cosine of I-th boundary element surface,

DCOSB(3,I) - z-directional cosine of I-th boundary element surface,

ISB(1,I) - boundary node number of the first node of I-th
boundary element surface,

ISB(2,I) - boundary node number of the second node of I-th
boundary element surface,

ISB(3,I) - boundary node number of the third node of I-th
boundary element surface,

ISB(4,I) - boundary node number of the fourth node of I-th
boundary element surface,

ISB(5,I) - element side index of I-th boundary element surface,
1 - left side, 2 - front side, 3 - right side,
4 - back side, 5 - bottom side, 6 - top side,

ISB(6,I) - element number to which the I-th boundary
element-surface belongs,

NPBB(I) - global node number of I-th boundary node,

BFLX(I) - boundary flux at I-th boundary node,

BFLXP(I) - boundary flux at previous time of I-th boundary node.

Arrays for Element (Distributed) and Well (Point) Sources/Sinks

SOS(MXSPR), SOSF(MXSDP,MXSPR), TSOSF(MXSDP,MXSPR),

ISTYP(MXSEL), MSEL(MXSEL),

WSS(MXWPR), WSSF(MXWDP,MXWPR), TWSSF(MXWDP,MXWPR),

IWTYP(MXWNP), NPW(MXWNP);

MXSEL - maximum number of source elements,

MXSPR - maximum number of source profiles,

MXSDP - maximum number of data points on each well source/sink
profile,

MXWNP - maximum number of well nodal points,

MXWPR - maximum number of well source/sink profiles,

MXWDP - maximum number of data points on each well source/sink
profile;

SOS(I) - value of I-th element source/sink profile,

SOSF(I,J) - source/sink strength of I-th data point in J-th
element source/sink strength vs time profile,

TSOSF(I,J) - time of I-th data point in J-th element
source/sink strength vs time profile,

MSEL(M) - element number of M-th source/sink element,

ISTYP(M) - source/sink type assigned to M-th source/sink element,

WSS(I) - value of I-th well source/sink profile at present time,

WSSF(I,J) - source/sink strength of I-th data point in J-th

well source/sink strength vs time profile,
 TWSSF(I,J) - time of I-th data point in J-th well
 source/sink strength vs time profile,
 NPW(N) - global node number of N-th source/sink well,
 IWTF(N) - source/sink type assigned to N-th source/sink well.

Arrays for Cauchy Boundary Conditions

QCB(MXCPR), QCBF(MXCDP,MXCPR), TQCBF(MXCDP,MXCPR),
 ICTYP(MXGES), ISC(5,MXGES), NPCB(MXCNP);

MXCNP - maximum number of Cauchy nodal points,
 MXGES - maximum number of Cauchy element surfaces,
 MXCPR - maximum number of Cauchy-flux profiles,
 MXCDP - maximum number of data points on each
 Cauchy-flux profile;

QCB(I) - value of I-th Cauchy flux profile at the present time,
 QCBF(I,J) - flux of I-th data point in J-th Cauchy flux vs time
 profile,
 TQCBF(I,J) - time of I-th data point in J-th Cauchy flux vs time
 profile,
 ICTYP(MP) - type of Cauchy flux vs time profile assigned to MP-th
 Cauchy boundary surface,
 NPCB(NP) - global node number of NP-th Cauchy node for inputting,
 then is changed to contain boundary node number,
 ISC(1,MP) - global node number of the first node of MP-th Cauchy
 boundary surface,
 ISC(2,MP) - global node number of the second node of MP-th Cauchy
 boundary surface,
 ISC(3,MP) - global node number of the third node of MP-th Cauchy
 boundary surface,
 ISC(4,MP) - global node number of the fourth node of MP-th Cauchy
 boundary surface,
 ISC(5,MP) - boundary side number of MP-th Cauchy boundary surface,

Arrays for Neumann Boundary Conditions

QNB(MXNPR), QNBF(MXNDP,MXNPR), TQNB(MXNDP,MXNPR),
 INTYP(MXNES), ISN(5,MXNES), NPNB(MXNNP);

MXNNP - maximum number of Neumann nodal points,
 MXNES - maximum number of Neumann element surfaces,
 MXNPR - maximum number of Neumann-flux profiles,
 MYNDP - maximum number of data points on each
 Neumann-flux profile;

QNB(I) - value of I-th Neumann flux profile at present time,
 QNBF(I,J) - flux of I-th data point in J-th Neumann flux vs time
 profile,
 TQNB(I,J) - time of I-th data point in J-th Neumann flux vs time
 profile,

- INTYP(MP) - type of Neumann flux vs time profile assigned to MP-th Neumann boundary surface,
 NPNB(NP) - global node number of NP-th Neumann node for inputting, then is changed to contain boundary node number,
 ISN(1,MP) - global node number of the first node of MP-th Neumann boundary surface,
 ISN(2,MP) - global node number of the second node of MP-th Neumann boundary surface,
 ISN(3,MP) - global node number of the third node of MP-th Neumann boundary surface,
 ISN(4,MP) - global node number of the fourth node of MP-th Neumann boundary surface,
 ISN(5,MP) - boundary side number of MP-th Neumann boundary surface.

Arrays for Variable Boundary Conditions

- RFALL(MXRPR), RF(MXRDP,MXRPR), TRF(MXRDP,MXRPR),
 IRTYP(MXVES), ISV(5,MXVES), NPVB(MXVNP),
 DCYFLX(MXVNP), FLX(MXVNP), HCON(MXVNP), HMIN(MXVNP),
 NPFLX(MXVNP), NPCON(MXVNP), NPMIN(MXVNP);
- MXVES - maximum number of variable element surfaces,
 MXVNP - maximum number of variable nodal points,
 MXRPR - maximum number of rainfall profiles,
 MXRDP - maximum number of data point on each rainfall profile;
- RFALL(I) - value of I-th rainfall via time profile at present time,
 TRF(I,J) - time of I-th data point on J-th rainfall vs time profile
 RF(I,J) - rainfall value of I-th data point on J-th rainfall vs time profile,
- IRTYP(MP) - type of rainfall profile assigned to MP-th variable boundary surface,
 ISV(1,MP) - global node number of the first node of the MP-th variable element surface for inputting, then is changed to contain compressed variable boundary node number,
 ISV(2,MP) - global node number of the second node of the MP-th variable element surface for inputting, then is changed to contain compressed variable boundary node number,
 ISV(3,MP) - global node number of the third node of the MP-th variable element surface for inputting, then is changed to contain compressed variable boundary node number,
 ISV(4,MP) - global node number of the fourth node of the MP-th variable element surface for inputting, then is changed to contain compressed variable boundary node number,
 ISV(5,MP) - boundary side number of the MP-th variable element surface,

- NPVB(NP) - global node number of the NP-th variable boundary node for inputting, then is changed to contain boundary node number,
- DCYFLX(NP) - Darcy flux through the NP-th variable boundary node,
 FLX(NP) - rainfall rate through the NP-th variable boundary node,
 HCON(NP) - ponding depth allowed for the NP-th variable boundary node,
 HMIN(NP) - minimum pressure head allowed for the NP-th variable boundary node,
 NPFLX(NP) - Cauchy boundary condition indicator for the NP-th variable node,
 NPCON(NP) - ponding depth Dirichlet boundary condition indicator for the NP-th variable node,
 NPMIN(NP) - minimum pressure head Dirichlet boundary condition indicator for the NP-th variable boundary node.

Arrays for Dirichlet Boundary Conditions

- HDB(MXDPR), HDBF(MXDDP,MXDPR), THDBF(MXDDP,MXDPR),
 IDTYP(MXDNP), NPDB(MXDNP);
- MXDNP - maximum number of Dirichlet nodal points,
 MXDPR - maximum number of Dirichlet total head profiles,
 MXDDP - maximum number of data points on each Dirichlet profile;
- HDB(I) - value of total head at the present time of I-th total head vs time profile for Dirichlet boundary,
 HDBF(I,J) - total head of I-th data point in J-th Dirichlet total head vs time profile,
 THDBF(I,J) - time of I-th data point in J-th Dirichlet total head vs time profile,
 IDTYP(NP) - type of Dirichlet total head vs time profile assigned to NP-th Dirichlet node,
 NPDB(NP) - global node number of NP-th Dirichlet node for inputting, then is changed to contain boundary node number.

Arrays for Material Property Array and Material Characteristics

- PROP(MXMPPM,MAXMAT), THPROP(MXSPPM,MAXMAT), AKPROP(MXSPPM,MAXMAT);
- MAXMAT - maximum number of material types (medium formations),
 MXSPPM - maximum number of soil parameters per material to describe soil characteristic curves,
 MXMPPM - maximum number of material properties per material;
- PROP(J,I) - J-th material property of I-th materials,
 J = 1 - saturated x-hydraulic conductivity or permeability,
 J = 2 - saturated y-hydraulic conductivity or permeability,
 J = 3 - saturated z-hydraulic conductivity or permeability,

J - 4 - saturated xy-hydraulic conductivity or permeability,
 J - 5 - saturated xz-hydraulic conductivity or permeability,
 J - 6 - saturated yz-hydraulic conductivity or permeability,
 THPROP(J,I) - J-th parameter to describe the moisture content as
 function of pressure head for I-th material,
 AKPROP(J,I) - J-th parameter to describe the relative hydraulic
 conductivity as a function of pressure head
 for I-th material.

Arrays for Output Control and Time Step Size Change

KPR(MAXNTI), KDSK(MAXNTI), TDTCH(MXNDTC);
 MAXNTI - maximum number of time steps,
 MXNDTC - maximum number of DELT changes;
 KPR(I) - line print control for I-th time step,
 KDSK(I) - disk storage control for I-th time step,
 TDTCH(I) - time of I-th time to reset time step size - DELTO.

The central process unit (CPU) memory requirements in words for all arrays can be computed as

$$\begin{aligned}
 \text{Real Storage} = & [(13 + \text{JBAND}) * \text{MAXNP}] + (24 * \text{MAXEL}) \\
 & + (3 * \text{MAXBES} + 2 * \text{MAXBNP}) + [(1 + \text{LMXBW}) * \text{LMXNP}] \\
 & + [(1 + 2 * \text{MXSDP}) * \text{MXSPR}] + [(1 + 2 * \text{MXWDP}) * \text{MXWPR}] \\
 & + [(1 + 2 * \text{MXCDP}) * \text{MXCPR}] + [(1 + 2 * \text{MXNDP}) * \text{MXNPR}] \\
 & + [(1 + 2 * \text{MXRDP}) * \text{MXRPR} + 4 * \text{MXVNP}] + [(1 + 2 * \text{MXDDP}) * \text{MXDPR}] \\
 & + [(\text{MXMPPM} + 2 * \text{MXSPPM}) * \text{MAXMAT}] , \qquad (103)
 \end{aligned}$$

$$\begin{aligned}
 \text{Integer Storage} = & [(1 + \text{JBAND}) * \text{MAXNP}] + (9 * \text{MAXEL}) + (6 * \text{MAXBES} + \text{MAXBNP}) \\
 & + [(\text{JBAND} * \text{LMXNP} + \text{LTMXNP}) + 3] * \text{MXREGN} \\
 & + [(2 * \text{MXSEL}) + (2 * \text{MXWNP})] + (6 * \text{MXCES} + \text{MXCNP}) \\
 & + (6 * \text{MXNES} + \text{MXNNP}) + (6 * \text{MXVES} + 4 * \text{MXVNP}) \\
 & + (2 * \text{MXDNP}) + (2 * \text{MAXNTI} + \text{MXNDTC}) . \qquad (104)
 \end{aligned}$$

The subscripts (maximum-control numbers) of the above 78 arrays should be specified in the BLOCK DATA in the source program. One should always assign correct numbers to these subscripts so that the program can function properly. If the program fails to function, it is most likely because either the arrays mentioned above are not properly dimensioned or the numbers assigned in the BLOCK DATA to these specification numbers of the arrays are not correct. In the following, we demonstrate how to dimension the above 78 arrays in the MAIN and how to specify the maximum-control numbers in the BLOCK DATA with an example.

Let us assume that a region of interest is discretized by 30 x 20 x 10 nodes and 29 x 19 x 9 elements. In other words, we are discretizing the region with 30 nodes along the longitudinal or x-direction, 20 nodes along the lateral or y-direction, and 10 nodes along the vertical or z-direction. Since we have a total of $30 \times 20 \times 10 = 60,00$ nodes, the maximum number of nodes is MAXNP = 6000. The total number of elements is $29 \times 19 \times 9 = 4,959$, i.e., MAXEL = 4959. For this simple discretization problem, the maximum connecting number to any of the 6,000 nodes in the region of interest is 27, i.e., JBAND = 27. There will be $29 \times 19 = 551$ element surfaces each on the bottom and top faces of the region, $29 \times 9 = 261$ element-surfaces each on the front and back faces of the region, and $19 \times 9 = 171$ element-surfaces each on the left and right faces of the region. Thus, there will be a total of 1966 element-surfaces, i.e., MAXBES = 1966. Similarly, we can compute the surface-boundary nodes to be 1968, i.e., MAXBNP = 1968. With these maximum-control numbers specified,

the arrays related to the global region, global boundary, and hydrologic variables can be dimensioned as

```

DIMENSION X(6000),Y(6000),Z(6000),IE(4959,9)
DIMENSION CMATRX(6000,27),GNOJCN(27,60000),RLD(6000),
DIMENSION RI(6000),RL(6000)
DIMENSION H(6000),HP(6000),HW(6000),HT(6000),
DIMENSION VX(6000),VY(6000),VZ(6000)
DIMENSION TH(8,4959),DTH(8,4959),AKR(8,4959),NPCNV(6000)
DIMENSION DCOSB(3,1966),ISB(6,1966),NPBB(1968),
DIMENSION BFLX(1968),BFLXP(1968)

```

In order to dimension the pointer arrays and the subregion data, we have to know how the region of interest is subdivided into subregions. Let us assume we have subdivided the region of interest into 20 subregions, each subregion has 30 x 10 nodes. It is seen, in fact, we are taking a vertical slice as a subregion. For this subregionalization, we have MXREGN = 20. Each subregion has 30 x 10 = 300 nodes, resulting LMXNP = 300. It is also seen that there will be 600 intraboundary nodes, 300 nodes each on the two neighboring slices of a subregion. Thus, we have LTMXNP = 900. For each subregion, the maximum bandwidth can be computed as LMXBW = 23 if the nodes are labelled along the z-directions consecutively. From these discussions, we can dimension the following arrays as

```

DIMENSION NTNPLR(20),NNPLR(20),LMAXDF(20)
DIMENSION GNLR(900,20),LNOJCN(27,300,20)
DIMENSION CMTRXL(300,23),RLDL(300)

```

We will assume that there will be a maximum of 11 elements that have

the distributed sources/sinks (i.e., MXSEL = 11) and a maximum of 10 nodal points that can be considered as well sources/sinks (i.e., MXWNP = 10). We will also assume that there will be three different distributed source/sink profiles and five distinct point source/sink profiles. Then we will have MXSPR = 3 and MXWPR = 5. Let us further assume that four data points are needed to describe the distributed source/sink profiles as a function of time and that 8 data points are required to describe point source/sink profiles (i.e., MXSDP = 4 and MXWDP = 8). With these assumptions, we can now dimension the arrays related to source/sink conditions

```
DIMENSION SOS(3),SOSF(4,3),TSOSF(4,3),ISTYP(11),MSEL(11)
DIMENSION WSS(5),WSSF(8,5),TWSSF(8,5),IWTYP(10),NPW(10)
```

To specify arrays for boundary conditions, let us assume that the top face is a variable boundary (i.e., on the air-soil interface, either ponding, infiltration, or evapotranspiration may take place). On the left face, fluxes from the adjacent aquifer are known. On the right face, the total head is assumed known. On the bottom face, natural drainage is assumed to occur (i.e., the gradient of the pressure head can be assumed zero).

There are $20 \times 10 = 200$ nodes on the left face and $19 \times 9 = 171$ element surfaces; thus MXCNP = 200 and MXCES = 171. It is further assumed that there two different fluxes going into the region through the left face and that each flux can be described by four data points as a function of time (i.e., MXCPR = 2, and MXCDP = 4). The Cauchy boundary condition

arrays can be dimensioned as

```
DIMENSION QCB(2),QCBF(4,2),TQCBF(4,2)
DIMENSION ICTYP(171),ISC(5,171),NPCB(200)
```

On the bottom surface, there are 30 x 20 = 600 nodes and 29 x 19 = 551 surface elements. Since the gradient of pressure head on the bottom surface is zero, there is only one Neumann flux profile, and two data points, one at zero time and the other at infinite time, are sufficient to describe the constant value of zero. Hence, we have MXNNP = 600, MXNES = 551, MXNPR = 1, and MXNDP = 2; and the Neumann boundary condition arrays can be dimensioned as

```
DIMENSION QNB(1),QNB(2,1),TQNB(2,1)
DIMENSION INTYP(551),ISN(5,551),NPNB(600)
```

On the top face, there will be 30 x 20 = 600 nodes and 29 x 19 = 551 surface elements. Let us assume that there are three different rainfall intensities that might be fall on the air-soil interface, and that each rainfall intensity is a function of time and can be described by 24 data points. With these descriptions, we have MXVNP = 600, MXVES = 551, MXRPR = 3, and MXRDP = 24; and the variable boundary condition arrays can be specified as

```
DIMENSION RFALL(3),RF(24,3),TRF(24,3)
DIMENSION IRTYP(551),ISV(5,551),NPVB(600)
DIMENSION DCYFLX(600),FLX(600),HCON(600),HMIN(600)
DIMENSION NPFLX(600),NPCON(600),NPMIN(600)
```

On the right face, there are 20 x 10 = 200 nodes. Let us assume that

there are twenty different values of the total head, one each on a vertical line of the right face. We further assume that each of these twenty total head can be described by 8 data points as function of time. We then have MXDNP = 200, MXDPR = 20, and MXDDP = 8; and the Dirichlet boundary condition arrays can be dimensioned as

```
DIMENSION HDB(20),HDBF(8,20),THDBF(8,20),IDTYP(200),NPDB(200)
```

In this report, we have six material properties (six saturated hydraulic conductivity components) per material. We will assume that the whole region of interest is composed of three different kinds of materials. The characteristic curves of each material are assumed to be described by four parameters. We then have MAXMAT = 3, MXMPM = 6, and MXSPPM = 4; and the material property arrays can be dimensioned as

```
DIMENSION PROP(6,3)
DIMENSION THPROP(4,3),AKPROP(4,3)
```

If we assume that we will make a 500 time step simulation and we will reinitiate the change on the time step size for 20 times during our simulation, then we have MAXNTI = 500 and MXNDTC = 20. With this assumption, arrays related to time can be dimensioned as

```
DIMENSION KPR(500),KDSK(500),TDTCH(20)
```

Corresponding to the above dimension specifications, the following data statements must be made in BLOCK DATA to specify the maximum-control integers:

```

DATA MAXEL,MAXNP,MAXBES,MAXBNP,JBAND/4959,6000,1966,1968,27/
DATA MAXNTI,MXNDTC/500,20/
DATA LTMXNP,LMXNP,LMXBW,MXREGN/900,300,23,20/
DATA MXSEL,MXSPR,MXSDP,MXWNP,MXWPR,MXWDP/11,3,4,10,5,8/
DATA MXGNP,MXCES,MXCPR,MXCDP/200,171,2,4/
DATA MXNNP,MXNES,MXNPR,MXNDP/600,551,1,2/
DATA MXVES,MXVNP,MXRPR,MXRDP/551,600,3,24/
DATA MXDNP,MXDPR,MXDDP/200,20,8/
DATA MAXMAT,MXSPPM,MXMPPM/3,4,6/

```

5.2 Soil Function Specifications

Analytical functions are used to describe the functional relationships of water content, water capacity, and relative hydraulic conductivity with pressure head. Therefore, the user must supply three functions to compute the water content, water capacity, and relative hydraulic conductivity based on the current value of pressure head. The parameters needed to specify the functional form are read and stored in THPROP and AKPROP. One example is shown in the subroutine SPROP between lines SPRO 405 and SPRO 535 in Appendix A. In this example, the water content, water capacity, and relative hydraulic conductivity are given by (van Genuchten 1980):

$$\theta = \theta_r + \frac{\theta_s - \theta_r}{[1 + (\alpha h)^n]^m} \quad (105)$$

$$\frac{d\theta}{dh} = \alpha(n-1) [1 - f(\theta)]^m [f(\theta)] (\theta_s - \theta_r) \quad (106)$$

$$K_r = [(\theta - \theta_s)/(\theta_s - \theta_r)]^{1/2} (1 - [1 - f(\theta)]^m)^2 \quad (107)$$

in which

$$f(\theta) = [(\theta - \theta_r)/(\theta_s - \theta_r)]^{1/m} \quad , \quad (108)$$

and

$$m = 1 - n \quad , \quad (109)$$

where α , m , and n are the parameters.

To further demonstrate how we should modify the subroutine SPROP in Appendix A to accommodate the material property functions that are different from those given by Eqs. (105) through (109), let us assume that the following Fermi types of functions are used to represent the unsaturated hydraulic properties (Yeh 1987):

$$\theta = \theta_r + (\theta_s - \theta_r)/(1 + \exp[-\alpha(h - h_\theta)]) \quad , \quad (110)$$

$$d\theta/dh = \alpha(\theta_s - \theta_r)\exp[-\alpha(h - h_\theta)]/(1 + \exp[-\alpha(h - h_\theta)])^2 \quad , \quad (111)$$

and

$$\log_{10}(K_r) = \epsilon/(1 + \exp[-\beta(h - h_k)]) - \epsilon \quad , \quad (112)$$

where θ_s , θ_r , α , and h_θ are the parameters for computing the water content and water capacity; and β , ϵ , and h_k are the parameters for computing the relative hydraulic conductivity. Lines between SPRO 405 and SPRO 535 in the subroutine SPROP in Appendix A may be changed, for this example, to

```

WCR=THPROP(1,MTYP)
WCS=THPROP(2,MTYP)
ALPHA=THPROP(3,MTYP)
HTheta=THPROP(4,MTYP)
EPS=AKPROP(1,MTYP)
BETA=AKPROP(2,MTYP)
HSubK=AKPROP(3,MTYP);

```

```

      DO 800 KG-1,8
C
C ----- SATURATED CONDITION
C
      IF(HNP.GT.0.0) GO TO 700
      TH(KG,M)-WCS
      DTH(KG,M)-0.0DO
      AKR(KG,M)-1.0DO
      GO TO 800
C
C ----- UNSATURATED CASE
C
700  EXPAH=DEXP(-ALPHA*(HNP-HTHETA))
      TH(KG,M)-WCR+(WCS-WCR)/(1.0DO+EXPAH)
      DTH(KG,M)-ALPHA*(WCS-WCR)*EXPAH/(1.0DO+EXPAH)**2
      AKRLOG=EPS/(1.0DO+DEXP(-BETA*(HNP-HSUBK))) - EPS
      AKR(KG,M)-10.0DO**AKRLOG

```

5.3 Data Input Guide

The input format for each data card is specified in the following. The number under the rule is the last column of the field. In general, an integer has a field of 5 and should be right-justified. On the other hand, a real number has a field of 10 and can be placed anywhere within the field if F-specification is used. If E- or D- format is used, then the exponential should be right-justified.

1. TITLE

One card per problem is required.

```
FORMAT(I5,9A8,3I1)
```

NPROB	TITLE	IGEOM	IBUG	ICHNG
5	77	78	79	80

NPROB - Problem number.

TITLE - Array for the title of the problem. It may contain up to 72 characters, from column 6 to column 77.

IGEOM - Integer indicating if (1) the geometry, boundary, and pointer arrays are to be printed; (2) the boundary and pointer arrays are to be computed or read via logical units. If to be computed, they should be written on logical units. If IGEOM is even number, (1) will not be printed. If IGEOM is odd number, (1) will be printed. If IGEOM is less than or equal to 1, boundary arrays will be computed and written on unit 3. If IGEOM is greater than 1, boundary arrays will be read via unit 3. If IGEOM is less than or equal to 3, pointer arrays will be computed and written on unit 4. If IGEOM is greater than 3, pointer arrays will be read via unit 4.

IBUG - Integer indicating if the diagnostic output is desired. 0 - No, 1 - Yes.

ICHNG - Integer control number indicating if the cyclic change of rainfall-seepage nodes is to be printed. 0 - No, 1 - Yes.

2. BASIC INTEGER PARAMETERS

One card per problem is required.

FORMAT(16I5)

NNP	NEL	NMAT	NCM	NTI	KSS	NSPPM	NMPPM
5	10	15	20	25	30	35	40
KSTR	KCP	KGRAV	NITER	NCYL	NDTCHG	NPITER	NREGN
45	50	55	60	65	70	75	80

NNP - Number of nodal points.

NEL - Number of elements.

NMAT - Number of material types.

NCM - Number of elements with material property correction.

NTI - Number of time steps or time increments.

- KSS - Steady state control.
 0 - steady state solution desired,
 1 - transient state or transient solutions.
- NSPPM - Number of parameters to specify analytical soil functions per material.
- NMPPM - Number of material properties per material.
 NMPPM = 6 for the present model.
- KSTR - Auxiliary storage output control;
 0 - no storage,
 1 - output stored in Logical Unit 1.
- KCP - Permeability input control;
 0 - input saturated hydraulic conductivity,
 1 - input saturated permeability.
- KGRAV - Gravity term control;
 0 - no gravity term,
 1 - with gravity term.
- NITER - Number of iterations allowed for solving the nonlinear equation.
- NCYL - Number of cycles permitted for iterating rainfall-seepage boundary conditions per time step.
- NDTCHG - Number of times to reset time step size to initial time step size.
- NPITER - Number of iterations for block or pointwise solution.
- NREGN - Number of subregions.

NOTE: NTI can be computed by $NTI = I1 + 1 + I2 + 1$,
 where $I1$ - largest integer not exceeding $\text{Log}(\text{DELMAX}/\text{DELTA})/\text{Log}(1+\text{CHNG})$,
 $I2$ - largest integer not exceeding $(\text{RTIME}-\text{DELTA} * [(1+\text{CHNG})^{(I1+1)} - 1] / \text{CHNG}) / \text{DELMAX}$,
 RTIME - Real simulation time,
 DELMAX, DELTA, and CHNG are defined in Data Set 3.

3. BASIC REAL PARAMETERS

Two cards per problem. Use of an E-, D-, or another F-type field specification in the input card overrides any of the D10.3 field.

Card 1 - FORMAT(8D10.3).

DELT	CHNG	DELMAX	TMAX	TOLA	TOLB	RHO	GRAV
10	20	30	40	50	60	70	80

DELT - Initial time step size (T)

CHNG - Percentage of change in time step size in each of the subsequent time increment, (dimensionless in decimal point).

DELMAX - Maximum value of DELT (T).

TMAX - Maximum simulation time (T).

TOLA - Steady-state convergence criteria (L).

TOLB - Transient-state convergence criteria (L).

RHO - Density of water (M/L^3).

GRAV - Acceleration of gravity (L/T^2).

Card 2 - FORMAT(8D10.3).

VISC	W	OME	OMI		
10	20	30	40	45	80

VISC - Dynamic viscosity of water [$(M/L)/T$].

W - Time derivative weighting factor;
 0.5 - Crank-Nicolson central and/or mid-difference,
 1.0 - backward difference.

OME - Iteration parameter for solving the nonlinear matrix equation;
 0.0 -- 1.0 - underrelaxation,
 1.0 -- 1.0 - exact relaxation,
 1.0 -- 2.0 - over-relaxation.

OMI - Relaxation parameter for solving the linearized matrix equation pointwise;
 0.0 -- 1.0 = underrelaxation,
 1.0 -- 1.0 = exact relaxation,
 1.0 -- 2.0 = overrelaxation.

4. **PRINTER AND DISK STORE CONTROL AND TIMES FOR STEP SIZE RESETTING**
 The number of cards here depends on the number of time increments NTI and the times of resetting step size NDTCHG. The number of cards is $[(NTI/80+1)*2 + (NDTCHG/8+1)]$. $(NTI/80+1)$ cards are for printer output control, $(NTI/80+1)$ cards for storage control, and $(NDTCHG/8+1)$ cards for time-step-size resetting.

Card 1 to Card $[(NTI/80+1)]$ -- FORMAT(80I1)

KPRO	KPR(1)	KPR(2)	---	KPR(I)	---	KPR(NTI)
1	2	3				80

KPRO - Printer control for steady state and initial conditions;
 0 - print nothing,
 1 - print FLOW, FRATE, and TFLOW,
 2 - print above (1) plus pressure head H,
 3 - print above (2) plus total head,
 4 - print above (3) plus moisture content,
 5 - print above (4) plus Darcy's velocity.

KPR(I) - Printer control for I-th time step similar to KPRO.

Card $[(NTI/80+1)+1]$ to Card $[(NTI/80+1)*2]$ -- FORMAT(80I1)

KDSKO	KDSK(1)	KDSK(2)	---	KDSK(I)	---	KDSK(NTI)
1	2	3				80

KDSKO - Auxiliary storage control for steady state and initial condition;
 0 - no storage,
 1 - store on Logical Unit 1.

KDSK(I) - Auxiliary storage control for I-th time step similar to KDSKO.

Card [(NTI/80+1)*2 + 1] to card [(NTI/80+1)*2 + (NDTCHG/8+1)]
 -- FORMAT(8D10.3).

TDTCH(1)	TDTCH(2)	---	TDTCH(I)	---	TDTCH(NDTCHG)
10	20				80

TDTCH(I) - Time when I-th step size resetting is needed.

5. MATERIAL PROPERTIES

A total of NMAT cards are required for this data set.

FORMAT(8D10.3)

PROP(1,1)	PROP(2,1)	----	PROP(6,1)
10	20		60 80

PROP(1,I)	PROP(2,I)	----	PROP(6,I)
10	20		60 80

PROP(1,NMAT)	PROP(2,NMAT)	----	PROP(6,NMAT)
10	20		60 80

PROP(1,I) - Saturated xx- hydraulic conductivity or permeability of medium I (L/T) or (L²).

PROP(2,I) - Saturated yy- hydraulic conductivity or permeability of medium I (L/T) or (L²).

PROP(3,I) - Saturated zz- hydraulic conductivity or permeability of medium I (L/T) or (L²).

PROP(4,I) - Saturated xy- hydraulic conductivity or permeability of medium I (L/T) or (L²).

PROP(5,I) - Saturated xz- hydraulic conductivity or permeability of medium I (L/T) or (L²).

PROP(6,I) - Saturated γ_z - hydraulic conductivity
or permeability of medium I (L/T) or (L²).

6. ANALYTICAL SOIL PARAMETERS

Two sets of cards per material -- one for moisture-content parameters and the other for conductivity (permeability) parameters. The number of cards per set is determined by the number of parameters used to specify the soil properties per material, NSPPM, and by the number of materials, NMAT:

FORMAT(8D10.3)

THPROP(1,1)	THPROP(2,1)	... THPROP(NSPPM,1)
10	20	80

THPROP(1,NMAT)	THPROP(2,NMAT)	... THPROP(NSPPM,NMAT)
10	20	80

AKPROP(1,1)	AKPROP(2,1)	... AKPROP(NSPPM,1)
10	20	80

AKPROP(1,NMAT)	AKPROP(2,NMAT)	... AKPROP(NSPPM,NMAT)
10	20	80

THPROP(J,I) - Analytical moisture-content parameter J
of material I.

AKPROP(J,I) - Analytical relative conductivity parameter
J of material I.

**** NOTE: THPROP(J,I) is also used to compute dTH/dH , the water capacity. One should derive the dTH/dH function by himself.

7. NODAL POINT COORDINATE

Usually a total of NNP cards are required. However, if a group of subsequent nodes appears in regular pattern, automatic generation can be made.

FORMAT(3I5,5X,6D10.3)

NI	NSEQ	NAD		XNI	YNI	ZNI	XIAD	YIAD	ZIAD
5	10	15	20	30	40	50	60	70	80

NI - Node number of the first node in the sequence.

NSEQ - NSEQ subsequent nodes will be automatically generated.

NAD - Increment of node number for each of the NSEQ subsequent nodes.

XNI - x-coordinate of node NI (L).

YNI - y-coordinate of node NI (L).

ZNI - z-coordinate of node NI (L).

XAD - Increment of x-coordinate for each of the NSEQ subsequent nodes (L).

YAD - Increment of y-coordinate for each of the NSEQ subsequent nodes (L).

ZAD - Increment of z-coordinate for each of the NSEQ subsequent nodes (L).

**** NOTE: A blank card must be used to signal the end of this data set.

8. SUBREGION DATA

- (a) Number of Nodes for each Subregion: Normally NREGN cards are required. However, if regular pattern appears, automatic generation can be made.

FORMAT(16I5)

NK	NSEQ	NKAD	NODES	NODAD	
5	10	15	20	25	80

NK - Subregion number of the first region in a sequence.

NSEQ - NSEQ subsequent subregions will have their number of nodes automatically generated.

NKAD - Increment of NK in each of the NSEQ subsequent subregions.

NODES - Number of nodes for the subregion NK.

NODAD - Increment of NODES in each of the NSEQ subsequent subregions.

**** NOTE: A blank card must be used to end the input of this subdata set.

- (b) Mapping between Global nodes and Subregion Nodes: This subdata set should be repeated NREGN times, one for each subregion.

FORMAT(16I5)

LI	NSEQ	LIAD	NI	NIAD	
5	10	15	20	25	80

LI - Local node number of the first node in a sequence.

NSEQ - NSEQ subsequent local nodes will have their corresponding global node number generated automatically.

LIAD - Increment of LI for each of the NSEQ subsequent nodes.

NI - Global node number of local node LI.

NIAD - Increment of NI for each of the NSEQ subsequent nodes.

**** NOTE: A blank card must be used to signal the end of this subdata set.

9. ELEMENT INCIDENCES

Usually a total of NEL cards are needed. However, if a group of elements appears in regular pattern, automatic generation is made.

FORMAT(16I5)

MI	NSEQ	MIAD	IE(MI,1)	---	IE(MI,8)	IEMAD
5	10	15	50			80

MI - Global element number of the first element in a sequence.

NSEQ - NSEQ subsequent elements will have their connectivity automatically generated.

MIAD - Increment of MI for each of the NSEQ subsequent elements.

IE(MI,1) - Global node number of the first node of element MI.

IE(MI,2) - Global node number of the second node of element MI.

IE(MI,3) - Global node number of the third node of element MI.

IE(MI,4) - Global node number of the fourth node of element MI.

IE(MI,5) - Global node number of the fifth node of element MI.

IE(MI,6) - Global node number of the sixth node of element MI.

IE(MI,7) - Global node number of the seventh node of element MI.

$IE(MI,8)$ - Global node number of the eighth node of element MI .

$IEMAD$ - Increment of $IE(MI,1)$ through $IE(MI,8)$ for each of the NSEQ subsequent elements.

$IE(MI,1)$ through $IE(MI,8)$ are numbered according to the convention shown in Fig. 7. The first four nodes start from the front, lower, left corner and progress around the bottom element surface in a counterclockwise direction. The other four nodes begin from the front, upper, left corner and progress around the top element surface in a counterclockwise direction.

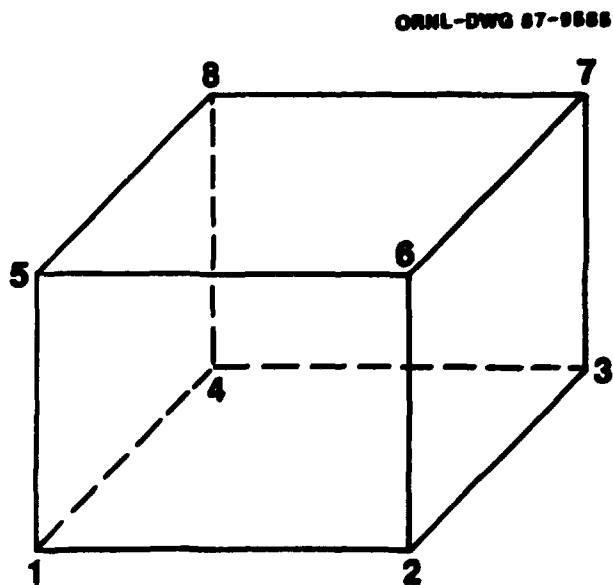


Fig. 7. Numbering of element incidences.

10. MATERIAL TYPE CORRECTION

This data set is required only if $NCM > 0$. Normally, NCM cards are required. However, if a group of elements appears in regular pattern, automatic generation may be made.

FORMAT(4I5)

MI	NSEQ	MAD	MITYP	MTYPAD	
5	10	15	20	25	80

MI - Global element number of the first element in the sequence.

NSEQ - NSEQ subsequent elements will be generated automatically.

MAD - Increment of element number for each of the NSEQ subsequent elements.

MITYP - Type of material correction for element MI.

MTYPAD - Increment of the type of material correction for each of the NSEQ subsequent elements.

**** NOTE: A blank card must be used to signal the end of this data set.

11. CARD INPUT FOR INITIAL OR PRE-INITIAL CCNDITIONS

NNP cards, one card for each node, are needed. However, if a group of nodes appears in regular pattern, auto-generation is made.

FORMAT(3I5,5X,4D10.3)

NI	NSEQ	NAD	HNI	HAD	
5	10	15	20	30	40 80

NI - Global node number of the first node in the sequence.

NSEQ - NSEQ subsequent nodes will be generated automatically.

NAD - Increment of node number for each of the NSEQ nodes.

HNI - Initial or pre-initial pressure head of node NI (L).

HAD - Increment of initial or pre-initial head for each of the NSEQ nodes (L).

****** NOTE:** A blank card must be used to signal the end of this data set.

**** NOTE ON INITIAL CONDITIONS:** The initial condition for a transient calculation may be obtained in two different ways: from card input or steady-state calculation using time-invariant boundary conditions that are different from those for transient computation. In the latter case, a card input of the pre-initial conditions is required as the zeroth order iterate of the steady state solution.

**** NOTE ON AUXILIARY STORAGE UNITS:** Logical Unit 1 is used to store output if KSTR > 0. Proper identification of this logical unit must be made in the job control language (JCL).

**** NOTE ON STEADY STATE INPUT:** Steady state option may be used to provide either the final state of a system under study or the initial conditions for a transient state calculation. In former case, KSS = 0 and NTI = 0, and in the latter case KSS = 0 and NTI > 0. If KSS > 0, there will be no steady state calculation.

12. INTEGER PARAMETERS FOR TRANSIENT SOURCE and BOUNDARY CONDITIONS
Two cards per problem are required.

FORMAT(16I5)

NSEL	NSPR	NSDP	NWNP	NWPR	NWDP	NCES	NCNP
5	10	15	20	25	30	35	40
NCPR	NCDP	NNES	NNNP	NNPR	NNDP	NVES	NVNP
45	50	55	60	65	70	75	80
NVPR	NVDP	NDNP	NDPR	NDDP			
5	10	15	20	25			80

- NSEL** - Number of source/sink elements.
- NSPR** - Number of source/sink profiles, should be .GE. 1.
- NSDP** - Number of data points in each of the NSPR.
source/sink profiles, should be .GE. 2.
- NWNP** - Number of well or point source/sink nodal points.
- NWPR** - Number of well or point source/sink strength
profiles.
- NWDP** - Number of data points in each of the NWPR profiles.
- NCES** - Number of Cauchy boundary element sides.
- NCNP** - Number of Cauchy boundary nodes.
- NCPR** - Number of Cauchy flux profiles.
- NCDP** - Number of data points in each of the NCPR
Cauchy flux profiles.
- NNES** - Number of Neumann boundary element sides.
- NNNP** - Number of Neumann nodal points.
- NNPR** - Number of Neumann flux profiles.
- NNDP** - Number of data points in each of the NNPR
Neumann flux profiles.
- NVES** - Number of variable boundary element sides.
- NVNP** - Number of variable boundary nodes.
- NVPR** - Number of variable boundary profile.
- NVDP** - Number of data points in each of the
NVPR variable boundary profiles.
- NDNP** - Number of Dirichlet nodal points,
should be .GE. 1.
- NDPR** - Number of total Dirichlet-head profiles,
should be .GE. 1.
- NDDP** - Number of data points in each of the NDNP
total Dirichlet-head profiles,
should be .GE. 1.

13. DISTRIBUTED AND POINT SOURCES/SINKS

Two sets of cards are needed: one for the distributed source/sink, and the other for the point source/sink.

- (1) **Distributed Source/sink Data:** This subdata set is needed if and only if $NSEL > 0$. When $NSEL$ is greater than zero, three groups of cards are needed: one for the source profile, one for the source element number, and the other for the source type.

- (a) **Source/sink Profiles:** The number of cards depends on $NSPR$ and $NSDP$. This sub-data set is read in $NSPR$ -wisely. Each card contains four data points.

FORMAT(8D10.3)

1rst profile

TSOSF(1,1)	SOSF(1,1)	TSOSF(2,1)	SOSF(2,1)	---
10	20	30	40	80
.				
.				
---	TSOSF(NSDP,1)	SOSF(NSDP,1)		
80				

Second profile

TSOSF(1,2)	SOSF(1,2)	TSOSF(2,2)	SOSF(2,2)	---
10	20	30	40	80
.				
.				
---	TSOSF(NSDP,2)	SOSF(NSDP,2)		
80				

I-th profile

TSOSF(1,I)	SOSF(1,I)	TSOSF(2,I)	SOSF(2,I)	---
10	20	30	40	80

---	TSOSF(NSDP, I)	SOSF(NSDP, I)	
-----	----------------	---------------	--

80

NSPR-th profile

TSOSF(1,NSPR)	SOSF(1,NSPR)	TSOSF(2,NSPR)	SOSF(2,NSPR)	
---------------	--------------	---------------	--------------	--

10	20	30	40	80
----	----	----	----	----

---	TSOSF(NSDP,NSPR)	SOSF(NSDP,NSPR)	
-----	------------------	-----------------	--

80

TSOSF(J, I) - Time of J-th data point in I-th profile (T).

SOSF(J, I) - Source/sink value of J-th data point in I-th profile $[(L^3/T)/L^3]$.

- (b) Global Element Number of Compressed Distributed Source/Sink Element: The number of cards required in this subdata set depends on NSEL. Each card contains 16 nodes.

FORMAT(16I5).

MSEL(1)	MSEL(2)	MSEL(3)	--- MSEL(I)	--- MSEL(NSEL)
---------	---------	---------	-------------	----------------

5	10	15		80
---	----	----	--	----

MSEL(I) - Global element number of I-th compressed distributed source/sink element.

- (c) Source Type in Each Element: Usually one card per element is required; however, automatic generation can be made.

FORMAT(5I5)

MI	NSEQ	MAD	MITYP	MTYPAD	
----	------	-----	-------	--------	--

5	10	15	20	25	80
---	----	----	----	----	----

MI - Global element number of the first element in the sequence.

NSEQ - NSEQ elements will contain the source

types that will be automatically generated.

MAD - Increment of element number for each of the NSEQ elements.

MITYP - Source type in element MI.

MTYPAD - Increment of the source type for each of the NSEQ subsequent elements.

****** NOTE:** A blank card must be used to signal the end of this data set.

- (2) **Point Source/Sink Data:** This subdata set is needed if and only if $NWNP > 0$. When $NWNP$ is greater than zero, this subdata set is read in similarly to subdata set 12 (1).
- (a) **Well or Point Source/Sink Profiles:** The number of cards depends on $NWPR$ and $NWDP$. This sub-data set is read in similarly to sub data set 12(1)(a).

FORMAT(8D10.3)

First Profile

TWSSF(1,1)	WSSF(1,1)	TWSSF(2,1)	WSSF(2,1)	---	
10	20	30	40		80
.					
.					
.					
--- TWSSF(NWDP,1) WSSF(NWDP,1)					80

Second Profile

TWSSF(1,2)	WSSF(1,2)	TWSSF(2,2)	WSSF(2,2)	---	
10	20	30	40		80
.					
.					
.					
--- TWSSF(NWDP,2) WSSF(NWDP,2)					80

I-th Profile

TWSSF(1,I)	WSSF(1,I)	TWSSF(2,I)	WSSF(2,I)	---
10	20	30	40	80

TWSSF(NWDP,I)		WSSF(NWDP,I)		
				80

NWPR-th Profile

TWSSF(1,NWPR)	WSSF(1,NWPR)	TWSSF(2,NWPR)	WSSF(2,NWPR)	---
10	20	30	40	80

TWSSF(NWDP,NWPR)		WSSF(NWDP,NWPR)		
				80

TWSSF(J,I) - Time of J-th data point in I-th well or point source/sink profile (T).

WSSF(J,I) - Strength of point source/sink of J-th data point in I-th profile (L^3/T).

- (b) **Global Nodal Number of Compressed Well Source/Sink Nodes:**
 The number of cards required in this subdata set depends on NWNP. Each card contains 16 nodes.

FORMAT(1615)

NPW(1)	NPW(2)	NPW(3)	---	NPW(I)	---	NPW(NWNP)
5	10	15				80

NPW(I) - Global node number of I-th compressed well source/sink node.

- (c) **Types of Well Source/Sink Nodes:** Normally, one card per well node is needed (i.e. a total of NVNP cards). However, if the well nodes appear in regular pattern, automatic generation may be made.

FORMAT(515)

NI	NSEQ	NIAD	NITYP	NITYPA	
5	10	15	20	25	80

NI - Compressed well node number of the first node in a sequence.

NSEQ - NSEQ subsequent well nodes will be generated automatically.

NIAD - Increment of compressed well node number for each of the NSEQ subsequent nodes.

NITYP - Type of well/sink source profile assigned to node NI.

NITYPA - Increment of NITYP for each of the NSEQ subsequent nodes.

*** NOTE: A blank card must be used to signal the end of this subdata set.

14. RAINFALL/EVAPORATION-SEEPAGE (VARIABLE) BOUNDARY CONDITIONS

Six groups of cards are required for this data set if and only if NVES > 0. The first group is used to specify the rainfall/evaporation profile, the second group is used to assign the type of rainfall/evaporation profile to each of the NVES rainfall/evaporation-seepage sides, the third group is used to read four global nodal numbers of all NVES rainfall/evaporation-seepage sides, the fourth group is used to read the global nodal number of all the NVNP nodes, the fifth group is used to read in the allowed ponding depth for each of the NVNP nodes, and the sixth group is used to the allowed minimum pressure for each of the NVNP nodes.

- (a) **Rainfall/Potential Evaporation Profiles:** This subdata set is read in similarly to that of subdata set 12(a).

FORMAT(8D10.3)

First profile

TRF(1,1)	RF(1,1)	TRF(2,1)	RF(2,1)	...
10	20	30	40	80
.				
.				
...	TRF(NVDP,1)	RF(NVDP,1)		
80				

Second profile

TRF(1,2)	RF(1,2)	TRF(2,2)	RF(2,2)	...
10	20	30	40	80
.				
.				
...	TRF(NVDP,2)	RF(NVDP,2)		
80				

I-th profile

TRF(1,I)	RF(1,I)	TRF(2,I)	RF(2,I)	...
10	20	30	40	80
.				
.				
...	TRF(NVDP,I)	RF(NVDP,I)		
80				

NVPR-th profile

TRF(1,NVPR)	RF(1,NVPR)	TRF(2,NVPR)	RF(2,NVPR)	...
10	20	30	40	80

... TRF(NVDP,NVPR) RF(NVDP,NVPR)

80

TRF(J,I) - Time of the J-th data point on I-th rainfall/evaporation-vs-time profile (T).

RF(J,I) - Rainfall/evaporation rate of the J-th data point on I-th profile (L/T). For rainfall, input positive value, for potential evaporation, input negative value.

- (b) Rainfall/Evaporation Type Assigned to Each of All NVES Surfaces: This subdata set is read in similarly to that in subdata set 12(1)(c).

FORMAT(5I5)

NI	NSEQ	NIAD	NITYP	NTYPAD	
5	10	15	20	25	80

NI - Compressed variable boundary (rainfall/seepage) element side of the first side in a sequence.

NSEQ - NSEQ subsequent sides will be generated automatically.

NIAD - Increment of the compressed NI for each of the NSEQ subsequent sides.

NITYP - Type of rainfall/evaporation profile assigned to side NI.

NTYPAD - Increment of the type of rainfall/evaporation profile for each of the NSEQ subsequent sides.

*** NOTE: A blank card must be used to signal the end of this subdata set.

- (c) Specification of Rainfall/evaporation-seepage (RES) Sides: Normally, NVES cards are required, one each for a RES boundary element side. However, if a group of RES element sides appears in a regular pattern, automatic generation may be made.

FORMAT(16I5)

MI	NSEQ	MIAD	I1	I2	I3	I4	I1AD	I2AD	I3AD	I4AD
5	10	25	20	25	30	35	40	45	50	55 80

MI - Compressed RES element side number of the first element side in a sequence.

NSEQ - NSEQ subsequent RES element sides will be generated automatically.

MIAD - Increment of MI for each of the NSEQ subsequent RES element sides.

I1 - Global node number of the first node of element side MI.

I2 - Global node number of the second node of element side MI.

I3 - Global node number of the third node of element side MI.

I4 - Global node number of the fourth node of element side MI.

I1AD - Increment of I1 for each of the NSEQ subsequent element sides.

I2AD - Increment of I2 for each of the NSEQ subsequent element sides.

I3AD - Increment of I3 for each of the NSEQ subsequent element sides.

I4AD - Increment of I4 for each of the NSEQ subsequent element sides.

**** NOTE: A blank card must be used to signal the end of this subdata set.

- (d) Global Nodal Number of All Rainfall/Evaporation-Seepage (RES) Nodes: This subdata set is read in similarly to that in subdata set 12(1)(c).

FORMAT(5I5)

NI	NSEQ	NIAD	NODE	NODEAD	
5	10	15	20	25	80

NI - Compressed variable boundary node number of the first node in a sequence.

NSEQ - NSEQ subsequent nodes will be generated automatically.

NIAD - Increment for NI for each of the NSEQ nodes.

NODE - Global nodal number of the node NI.

NODEAD - Increment of the global nodal number for each of the NSEQ subsequent nodes.

**** NOTE: A blank card must used to signal the end of this subdata set.

- (e) Ponding depth: Normally, NVNP cards are needed, one for each of the NVNP variable boundary (VB) nodes. However, if a group of VB nodes has a regular pattern of ponding depth, automatic generation is made.

FORMAT(3I5,5X,2D10.3)

NI	NSEQ	NIAD	HCONNI	HCONAD		
5	10	15	20	30	40	80

NI - Compressed VB nodal number of the first node in a sequence.

NSEQ - NSEQ subsequent nodes will be generated automatically.

NIAD - Increment of the compressed VB nodal number for each of the NSEQ subsequent nodes.

HCONNI - Ponding depth of node NI (L).

HCONAD - Increment of ponding depth for each of the NSEQ subsequent nodes (L).

**** NOTE: A blank card must be used to signal the end of this subdata set.

(f) **Minimum Pressure Head Allowed in Each VB Nodes:** This subdata set is read in similarly to the above subdata set.

NI	NSEQ	NIAD	HMINNI	HMINAD		
5	10	15	20	30	40	80

NI - Compressed VB node number of the first node in a sequence.

NSEQ - NSEQ subsequent VB nodes will be generated automatically.

NIAD - Increment of the compressed VB node number for each of the NSEQ subsequent nodes.

HMINNI - Minimum pressure head of node NI (L).

HMINAD - Increment of minimum pressure head for each of the NSEQ subsequent nodes (L).

**** NOTE: A blank card must be used to signal the end of this subdata set.

15. DIRICHLET BOUNDARY CONDITIONS

This data set is required if NDNP > 0.

(a) **Dirichlet-Head Profiles:** This subdata set is read in similarly to that in subdata set 12(1)(a).

FORMAT(8D10.3)

First profile

THDBF(1,1)	HDBF(1,1)	HDBF(2,1)	HDBF(2,1)	---
10	20	30	40	80
---	THDBF(NDDP,1)	HDBF(NDDP,1)		

Second profile

THDBF(1,2)	HDBF(1,2)	THDBF(2,2)	HDBF(2,2)	---
10	20	30	40	80
---				80
THDBF(NDDP,2)		HDBF(NDDP,2)		

I-th profile

THDBF(1,I)	HDBF(1,I)	THDBF(2,I)	HDBF(2,I)	---
10	20	30	40	80
---				80
THDBF(NDDP,I)		HDBF(NDDP,I)		

NDPR-th profile

THDBF(1,NDPR)	HDBF(1,NDPR)	THDBF(2,NDPR)	HDBF(2,NDPR)	...
10	20	30	40	80
...				80
THDBF(NDDP,NDPR)		HDBF(NDDP,NDPR)		

THDBF(J,I) - Time of J-th data point fr. I-th Dirichlet head profile (T).

HDBF(J,I) - Total head of J-th data point in I-th Dirichlet head profile (L).

- (b) **Dirichlet Nodes:** The number of cards in this subdata set depends on NDNP. Each card contains 16 nodes.

FORMAT(16I5)

NPDB(1) NPDB(2) ... NPDB(I) ... NPDB(NDNP)				
5	10			80

NPDB(I) - Global node number of I-th Dirichlet node.

- (c) **Type of Dirichlet Node:** Normally, one card per Dirichlet node is required (i. e. a total of NDNP cards). However, if the Dirichlet nodes appear in regular pattern, automatic generation may be made.

FORMAT(5I5)

NI	NSEQ	NAD	NITYP	NTYPAD	
5	10	15	20	25	80

NI - Compressed Dirichlet node number of the first node in the sequence.

NSEQ - NSEQ subsequent Dirichlet nodes will be generated automatically.

NAD - Increment of compressed Dirichlet node number for each of the NSEQ nodes.

NITYP - Type of Dirichlet-head profile for node NI and the NSEQ subsequent nodes.

NTYPAD - Increment of NITYP for each of the NSEQ subsequent nodes.

*** NOTE: A blank card must be used to signal the end of this subdata set.

16. CAUCHY BOUNDARY CONDITIONS

This data set is required if and only if NCES > 0. Four groups of cards are required. One group is used to read Cauchy flux profiles, the second group is used to read the type of Cauchy flux profile assigned to each of the NCES Cauchy sides, the third

group is to read Cauchy boundary element sides, and the fourth group is to read the Cauchy boundary nodal points.

- (a) Prescribed Cauchy flux Profiles: This subdata set is read in similarly to that in subdata set 12(a).

FORMAT(8D10.3)

First profile

TQCBF(1,1)	QCBF(1,1)	TQCBF(2,1)	QCBF(2,1)	...
10	20	30	40	80
...	TQCBF(NCDF,1)	QCBF(NCDF,1)		
				80

Second profile

TQCBF(1,2)	QCBF(1,2)	TQCBF(2,2)	QCBF(2,2)	...
10	20	30	40	80
...	TQCBF(NCDF,2)	QCBF(NCDF,2)		
				80

I-th profile

TQCBF(1,I)	QCBF(1,I)	TQCBF(2,I)	QCBF(2,I)	...
10	20	30	40	80
	TQCBF(NCDF,I)	QCBF(NCDF,I)		
				80

NCPR-th profile

TQCBF(1,NCPR)	QCBF(1,NCPR)	TQCBF(2,NCPR)	QCBF(2,NCPR)	...
10	20	30	40	80
... TQCBF(NCDP,NCPR) QCBF(NCDP,NCPR)				
				80

TQCBF(J,I) - Time of the J-th data point on I-th Cauchy-flux profile (T).

QCBF(J,I) - Normal Cauchy flux of the J-th data point on I-th profile $[(L^3/T)/L^2]$.
 QCBF is positive if directed out from the region, it is negative if directed into the region.

- (b) Type of Cauchy Flux Profile Assigned to Cauchy Sides:
 Normally, one card per Cauchy node (i. e. a total of NCES cards) is required. However, if a group of cards appears in regular pattern, automatic generation may be made.

NI	NSEQ	NAD	NITYP	NTYPAD	
5	10	15	20	25	80

NI - Compressed Cauchy side number of the first side in a sequence.

NSEQ - NSEQ subsequent Cauchy sides will be generated automatically.

NAD - Increment of NI for each of the NSEQ subsequent sides.

NITYP - Type of Cauchy flux profile assigned to side NI.

NTYPAD - Increment of NITYP for each of the NSEQ subsequent sides.

*** NOTE: A blank card is used to signal the end of this data set.

- (c) **Cauchy Boundary Element Sides:** Normally, one card per Cauchy boundary-element side (i.e., a total of NCEs cards) is required. However, if a group of Cauchy boundary element sides appears in regular pattern, automatic generation may be made.

FORMAT(16I5)

MI	NSEQ	MIAD	I1	I2	I3	I4	IIAD	I2AD	I3AD	I4AD
5	10	15	20	25	30	35	40	45	50	55

MI - Compressed Cauchy element side number of the first element side in a sequence.

NSEQ - NSEQ subsequent Cauchy element sides will be generated automatically.

MIAD - Increment of MI for each of the NSEQ subsequent element sides.

I1 - Global nodal number of the first node on the MI-th Cauchy side.

I2 - Global nodal number of the third node on the MI-th Cauchy side.

I3 - Global nodal number of the fourth node on the MI-th Cauchy side.

I4 - Global nodal number of the fourth node on the MI-th Cauchy side.

IIAD - Increment of I1 for each of the NSEQ subsequent element sides.

I2AD - Increment of I2 for each of the NSEQ subsequent element sides.

I3AD - Increment of I3 for each of the NSEQ subsequent element sides.

I4AD - Increment of I4 for each of the NSEQ subsequent element sides.

*** NOTE: A blank card is used to end this data set input.

- (d) Cauchy Node' point: The number of cards required is (NCNP/16+1). Each card contain 16 points.

FORMAT(16I5)

NPCB(1) NPCB(2) ... NPCB(I) ... NPCB(NCNP)

5 10 80

NPCB(I) - Global nodal number of I-th compressed Cauchy node.

17. NEUMANN BOUNDARY CONDITIONS

This data set is required if and only if NNEs > 0. Four groups of cards are required. One group is used to read Neumann flux profiles, the second group is used to read the type of Neumann flux profile assigned to each of the NNEs Neumann sides, the third group is to read Neumann boundary element sides, and the fourth group is to read Neumann boundary nodal points.

- (a) Prescribed Neumann Flux Profiles: This subdata set is read in similarly to that in subdata set 15(a).

FORMAT(8D10.3)

First profile

TQBF(1,1)	QBF(1,1)	TQBF(2,1)	QBF(2,1)	---
10	20	30	40	80
:				
---	TQBF(NNDP,1)	QBF(NNDP,1)		

80

Second profile

QBF(1,2)	QBF(1,2)	TQBF(2,2)	QBF(2,2)	---
10	20	30	40	80
:				
---	TQBF(NNDP,2)	QBF(NNDP,2)		

80

I-th profile

TQBNF(1,I)	QBNF(1,I)	TQBNF(2,I)	QBNF(2,I)	---
				80
---	TQBNF(NNDP,I)	QBNF(NNDP,I)		
				80

NNPR-th profile

TQBNF(1,NNPR)	QBNF(1,NNPR)	TQBNF(2,NNPR)	QBNF(2,NNPR)	...
10	20	30	40	80
...	TQBNF(NNDP,NNPR)	QBNF(NNDP,NNPR)		
				80

TQBNF(J,I) - Time of J-th data point in I-th
Neumann flux profile (T).

QBNF(J,I) - Value of Neumann flux of J-th data point
in I-th Neumann flux profile $[(L^3/T)/L^2]$.

- (b) Type of Neumann Flux Profile Assigned to Neumann Sides:
This group of cards is read in similarly to subdata
set 15(b).

FORMAT(16I5)

NI	NSEQ	NAD	NITYP	NTYPAD
5	10	15	20	25
				80

NI - Compressed Neumann side number of
the first side in the sequence.

NSEQ - NSEQ subsequent Neumann sides will be
assigned a Neumann flux of type NITYP.

NAD - Increment of compressed Neumann side number in each of the NSEQ nodes.

NITYP - Type of Neumann flux profile for side NI and its NSEQ subsequent sides.

NTYPAD - Increment of NITYP for each of the NSEQ subsequent sides.

***** NOTE:** A blank card must be used to signal the end of this subdata set.

(c) **Neumann Boundary Element Sides:** This group of data is read in similarly to subdata set 15(c).

FORMAT(1615)

MI	NSEQ	MIAD	I1	I2	I3	I4	I1AD	I2AD	I3AD	I4AD	
5	10	15	20	25	30	35	40	45	50	55	80

MI - Compressed element side number of the first element side in the sequence.

NSEQ - NSEQ subsequent element-sides will be generated automatically.

MIAD - Increment of MI for each of the NSEQ subsequent element sides.

IS1 - Global nodal number of the first node on the MI-th Neumann side.

IS2 - Global nodal number of the second node on the MI-th Neumann side.

IS3 - Global nodal number of the third node on the MI-th Neumann side.

IS4 - Global nodal number of the fourth node on the MI-th Neumann side.

I1AD - Increment of I1 for each of the NSEQ subsequent Neumann sides.

I2AD - Increment of I2 for each of the NSEQ subsequent Neumann sides.

I3AD - Increment of I3 for each of the NSEQ subsequent Neumann sides.

I4AD = Increment of I4 for each of the NSEQ subsequent Neumann sides.

*** NOTE: A blank card must be used to signal the end of this subdata set.

(d) Neumann Nodes: The number of cards needed in this subdata set depend on NNNP. Each card contains 16 nodes.

FORMAT(16I5)

NPNB(1) NPNB(2) ... NPNB(I) ... NPNB(NNNP)		
5	10	80

NPNB(I) = global nodal point number of I-th Neumann node.

18. END OF JOB

If another problem is to be run, then input begins again with input data set 1. If termination of the job is desired, a blank card must be inserted at the end of the data set.

5.4 Input and Output Devices

Five logical units are needed to execute 3DFEMWATER. Units 5 and 6 are standard card input and line printer devices, respectively. Unit 1 must be specified to store the simulation results, which can be used for input to 3DFEMWASTE or for plotting purposes. Unit 3 is used to store the boundary arrays for later uses, if these arrays are computed for the present job. Unit 4 is used to store pointer arrays for later uses, if these arrays are generated for the present job. For large problems, our

experience has indicated that it would take too much time to process the boundary arrays and to generate pointer arrays. Hence, it is advisable that for multijob executions, these boundary and pointer arrays should be computed only once and written on units 3 and 4, respectively. Once they are stored on units 3 and 4, the JCL should be properly identified for the new job so they can be read via units 3 and 4, respectively.

6. SAMPLE PROBLEMS

To verify 3DFEMWATER, three illustrative examples reported elsewhere (Huyakorn 1986) are presented. These represent the one-, two-, and three-dimensional problems, respectively.

6.1 One-Dimensional Column Problem

This example is selected to represent the simulation of a one-dimensional problem with 3DFEMWATER. The column is 200 cm long and 50 by 50 cm in crosssection (Fig. 8). The column is assumed to contain the soil with a saturated hydraulic conductivity of 10 cm/d, a porosity of 0.45 and a field capacity of 0.1. The unsaturated characteristic hydraulic properties of the soil in the column are given as

$$\theta = \theta_s - (\theta_s - \theta_r) \left(\frac{1}{h_b - h_a} \right), \quad (113)$$

and

$$K_r = \frac{\theta - \theta_r}{\theta_s - \theta_r}, \quad (114)$$

where h_b and h_a are the parameters used to compute the water content and the relative hydraulic conductivity, respectively.

The initial conditions assumed are a pressure head of -90 cm imposed on the top surface of the column, 0 cm on the bottom surface of the column, and -97 cm elsewhere. The boundary conditions are given as: no

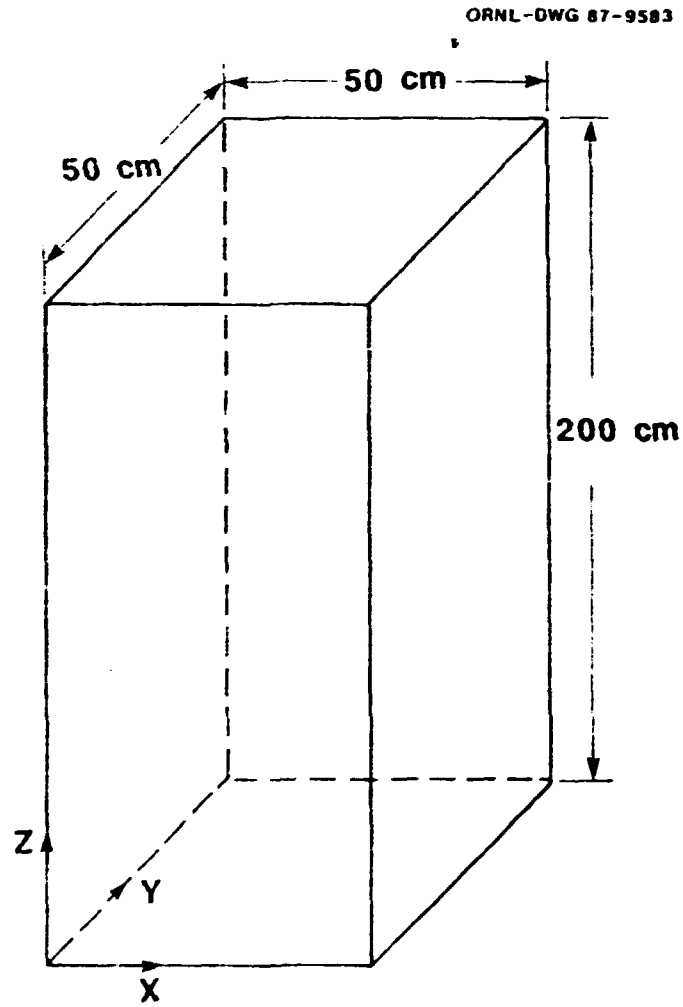


Fig. 8. Problem definition for the one-dimensional transient flow in a soil column

flux is imposed on the left, front, right, and back surfaces of the column; pressure head is held at 0 cm on the bottom surface; and variable condition is used on the top surface of the column with a ponding depth of zero, minimum pressure of -90 cm, and a rainfall of 5 cm/d for the first ten days and a potential evaporation of 5 cm/d for the second 10 days.

The region of interest, that is, the whole column, will be discretized with $1 \times 1 \times 40 = 40$ elements with element size $= 50 \times 50 \times 5$ cm, resulting in $2 \times 2 \times 41 = 164$ node points. For 3DFEMWATER simulation, each of the four vertical lines will be considered a subregion. Thus, a total of four subregions, each with 41 node points, is used for the subregional block iteration simulation.

A variable time step size is used. The initial time step size is 0.05 days, and each subsequent time step size is increased by 0.2 times with a maximum time step size not greater than 1.0 d. Because there is an abrupt change in the flux value from 5 cm/d (infiltration) to -5 cm/d (evaporation) imposed on the top surface at day 10, the time step size is automatically reset to 0.05 d on the tenth day. A 20-day simulation will be made with 3DFEMWATER. With the time step size described above, 44 time steps are needed.

The pressure head tolerance is $2 \cdot 10^{-2}$ cm for nonlinear iteration and is $1 \cdot 10^{-2}$ cm for block iteration. The relaxation factors for both the nonlinear iteration and block iteration are set equal to 0.5.

With the above descriptions, the input data can be prepared according to the instructions given in Sect. 5.3. The input data are given in Table 1.

To execute the problem, the arrays in the main program should be dimensioned as

```
DIMENSION X(164),Y(164),Z(164),IE(40,9)
DIMENSION CMATRX(164,27),GNOJCN(27,164),RLD(164),Ri(164),RL(164)
DIMENSION NTNPLR(4),NNPLR(4),LMAXDF(4)
DIMENSION GNLR(164,4),LNOJCN(27,41,4)
DIMENSION CMTRXL(41,3),RLD(41)
DIMENSION H(164),HP(164),HW(164),HT(164),VX(164),VY(164),VZ(164)
DIMENSION TH(8,40),DTH(8,40),AKR(8,40),NPCNV(164)
DIMENSION DCOSB(3,162),ISB(6,162),NPBB(164),BFLX(164),BFLXP(164)
DIMENSION SOS(1),SOSF(1,1),TSOSF(1,1),ISTYP(1),MSEL(1)
DIMENSION WSS(1),WSSF(1,1),TWSSF(1,1),IWTYP(1),NPW(1)
DIMENSION QCB(1),QCBF(1,1),TQCBF(1,1)
DIMENSION ICTYP(1),ISC(5,1),NPCB(1)
DIMENSION QNB(1),QNB(1,1),TQNB(1,1)
DIMENSION INTYP(1),ISN(5,1),NPNB(1)
DIMENSION RFALL(1),RF(4,1),TRF(4,1)
DIMENSION IRTYP(1),ISV(5,1),NPVB(4)
DIMENSION DCYFLX(4),FLX(4),HCON(4),HMIN(4)
DIMENSION NPFLX(4),NPCON(4),NPMIN(4)
DIMENSION HDB(1),HDBF(2,1),THDBF(2,1),IDTYP(4),NPDB(4)
DIMENSION PROP(6,1)
DIMENSION THPROP(4,1),AKPROP(4,1)
DIMENSION KPR(44),KDSK(44),TDTCH(3)
```

Table 1. Input data for the one-dimensional column problem

```

1 SIMULATION OF ONE-D COLUMN INFILTRATION-EVAPORATION; L-CM, T-DAY, M-C 111
164 40 1 0 44 1 4 6 1 0 1 50 20 3 100 4
0.05D0 0.2D0 1.0D0 20.0D0 2.0D-2 2.0D-2 1.0D0 7.316D12
1.1232D2 1.0D0 0.5D0 0.5D0
55515151115111511151111555151511151115111511115
111010100010001001000011101010001000100100001
1.0D01 2.0000D1 1.0D38
0.0D0 0.0D0 10.0D0 0.0D0 0.0D0 0.0D0
0.150D0 0.450D0 0.00D0 -1.0D2
0.000D0 0.000D0 0.00D0 0.0D0
1 40 1 0.0D0 50.0D0 0.0D0 0.0D0 0.0D0 5.0D0
42 40 1 0.0D0 0.0D0 0.0D0 0.0D0 0.0D0 5.0D0
83 40 1 50.0D0 0.0D0 0.0D0 0.0D0 0.0D0 5.0D0
124 40 1 50.0D0 50.0D0 0.0D0 0.0D0 0.0D0 5.0D0

1 3 1 41 0
END OF NNPLR(K)
1 40 1 1 1
END OF GNLR(I,1)
1 40 1 42 1
END OF GNLR(I,2)
1 40 1 83 1
END OF GNLR(I,3)
1 40 1 124 1
END OF GNLR(I,4)
1 39 1 42 83 124 1 43 84 125 2 1
END OF IE
1 3 41 0.0D0 0.0D0
2 38 1 -9.70D1 0.0D0
43 38 1 -9.70D1 0.0D0
84 38 1 -9.70D1 0.0D0
125 38 1 -9.70D1 0.0D0
41 3 41 -9.00D1 0.0D0
END OF IC

```


To reflect the soil property function given by Eqs. (113) and (114), we have to modify the subroutine SPROP given in Appendix A. Lines between SPRO 405 and SPRO 535 in the subroutine SPROP must be modified as follows:

```

WCR=THPROP(1,MTYP)
WCS=THPROP(2,MTYP)
HAA=THPROP(3,MTYP)
HAB=THPROP(4,MTYP)
DO 800 KG=1,8
HNP=HKG(KG)
HNP--HNP
C
C ----- SATURATED CONDITION
C
      IF(HNP.GT.0) GO TO 700
      TH(KG,H)=WCS
      AKR(KG,M)=1.000
      DTH(KG,M)=0.000
      GO TO 800
C
C ----- UNSATURATED CASE
C
700 THMKG=WCS-(WCS-WCR)*(-HNP-HAA)/(HAB-HAA)
      TH(KG,M)=THMKG
      AKR(KG,M)=(THMKG-WCR)/(WCS-WCR)
      DTH(KG,M)--(WCS-WCR)/(HAB-HAA)
C

```

The pressure head simulated with 3DFEMWATER is plotted in Fig. 9. As expected, during the rainfall period the pressure head is gradually built up, starting from the top surface of the column. In the subsequent evaporation period, the pressure head is gradually reduced. The minimum allowable pressure head of -90 cm was first reached at the top surface of the column and eventually propagated into the soil column. These numerical results are almost identical to those given by Huyakorn (1986).

Thus, the consistency of the computer code is partially verified.

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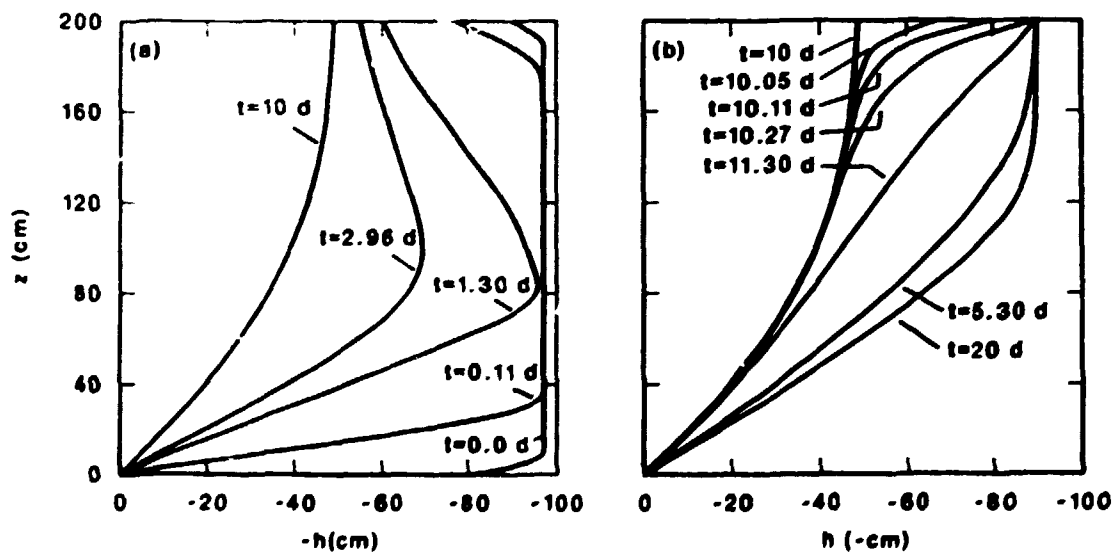


Fig. 9. Simulated pressure head profiles at various times during (a) infiltration and (b) evaporation for the one-dimensional column problem.

6.2 Two-dimensional Drainage Problem

This example is selected to represent the simulation of a two-dimensional problem with 3DFEMWATER. The region of interest is bounded on the left and right by parallel drains fully penetrating the medium, on the bottom by an impervious aquifuge, and on the top by an air-soil interface (Fig. 10). The distance between the two drains is 20 m apart (Fig. 10). The medium is assumed to have a saturated hydraulic conductivity of 0.01 m/d, a porosity of 0.25, and a field capacity of 0.05. The unsaturated characteristic hydraulic properties of the medium are given as

$$\theta = \theta_s + (\theta_s - \theta_r) \frac{A}{A + |h - h_a|^B} \quad , \quad (115)$$

and

$$K_r = \left(\frac{\theta - \theta_r}{\theta_s - \theta_r} \right)^n \quad , \quad (116)$$

where h_a , A , and B are the parameters used to compute the water content and n is the parameter to compute the relative hydraulic conductivity.

Because of the symmetry, the region for numerical simulation will be taken as $0 < x < 10$ m and $0 < z < 10$ m, and 10 m wide along the y -direction will be assumed. The boundary conditions are given as: no flux is imposed on the left ($x = 0$), front ($y = 0$), back ($y = 10$), and bottom ($z = 0$) sides of the region; pressure head is assumed to vary from zero at the water surface ($z = 2$) to 2 m at the bottom ($z = 0$) on the right side ($x = 10$); and variable conditions are used elsewhere. Ponding depth is

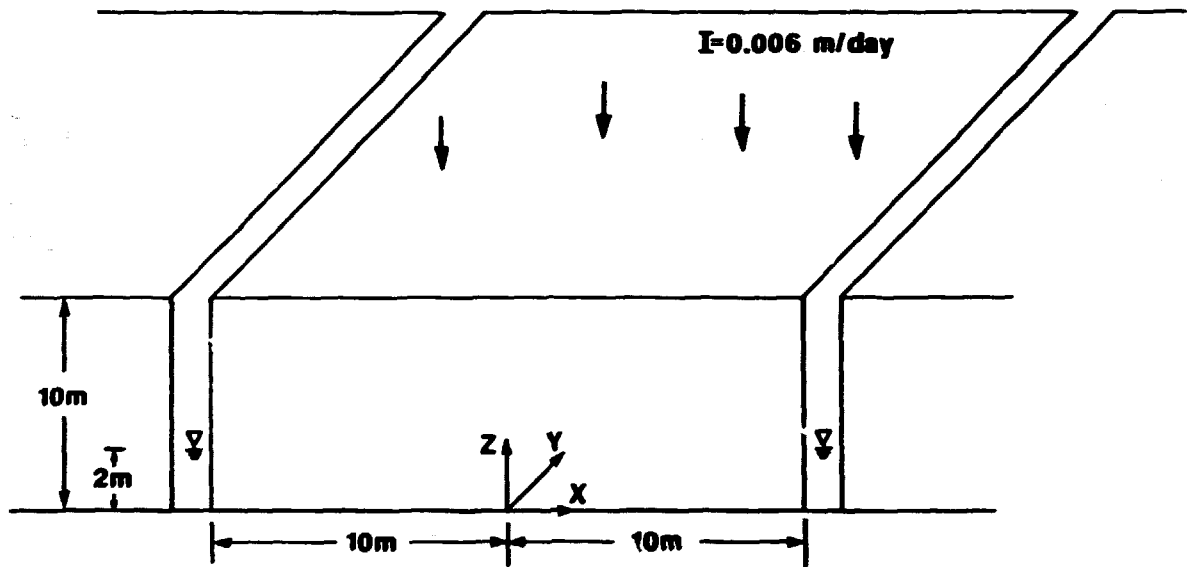


Fig. 10. Problem definition for two-dimensional steady state flow to parallel drains.

assumed to be zero meter on the whole variable boundary. Fluxes on the top side of the variable boundary are assumed equal to 0.006 m/d and on the right side above the water surface are equal to zero. A steady state solution will be sought. A pre-initial condition is set as $h = 10 - z$.

The region of interest is discretized with $10 \times 1 \times 10 = 100$ elements with element size = $1 \times 10 \times 1$ cm, resulting in $11 \times 2 \times 11 = 242$ node points. For 3DFEMWATER simulation, each of the two vertical planes will be considered a subregion. Thus, the total of two subregions, each with 121 node points, is used for the subregional block iteration simulation.

The pressure head tolerance is $2 \cdot 10^{-3}$ m for nonlinear iteration and is 10^{-3} m for block iteration. The relaxation factors for both the nonlinear iteration and block iteration are set equal to 0.5.

With the above descriptions, the input data can be prepared according to the instructions given in Sect. 5.3. The input data are given in Table 2.

To execute the problem, the arrays in the main program should be dimensioned as

```
DIMENSION X(242),Y(242),Z(242),IE(100,9)
DIMENSION CMATRX(242,27),GNOJCN(27,242),RLD(242),RI(242),RL(242)
DIMENSION NTNPLR(2),NNPLR(2),LMAXDF(2)
```

Table 2. Input data for two-dimensional drainage problem

2 SIMULATION OF TWO-D STEADY DRAINAGE; L-M, T-DAY, M-KG											111				
242	100	1	0	0	0	5	6	1	0	1	50	20	1	100	2
0.05D0	0.2D0	1.0D0	20.0D0	2.0D-3	2.0D-3	1.0D0	7.316D10								
1.1232D4	1.0D0	0.5D0	0.5D0												
55															
11															
1.0D38															
0.01D0	0.0D0	0.01D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0								
0.050D0	0.250D0	0.00D0	10.0D0	4.0D0											
4.000D0	0.000D0	0.00D0	0.0D0												
1	10	11	0.0D0	0.0D0	0.0D0	1.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0
2	10	11	0.0D0	0.0D0	1.0D0	1.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0
3	10	11	0.0D0	0.0D0	2.0D0	1.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0
4	10	11	0.0D0	0.0D0	3.0D0	1.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0
5	10	11	0.0D0	0.0D0	4.0D0	1.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0
6	10	11	0.0D0	0.0D0	5.0D0	1.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0
7	10	11	0.0D0	0.0D0	6.0D0	1.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0
8	10	11	0.0D0	0.0D0	7.0D0	1.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0
9	10	11	0.0D0	0.0D0	8.0D0	1.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0
10	10	11	0.0D0	0.0D0	9.0D0	1.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0
11	10	11	0.0D0	0.0D0	10.0D0	1.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0
122	10	11	0.0D0	10.0D0	0.0D0	1.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0
123	10	11	0.0D0	10.0D0	1.0D0	1.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0
124	10	11	0.0D0	10.0D0	2.0D0	1.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0
125	10	11	0.0D0	10.0D0	3.0D0	1.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0
126	10	11	0.0D0	10.0D0	4.0D0	1.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0
127	10	11	0.0D0	10.0D0	5.0D0	1.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0
128	10	11	0.0D0	10.0D0	6.0D0	1.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0
129	10	11	0.0D0	10.0D0	7.0D0	1.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0
130	10	11	0.0D0	10.0D0	8.0D0	1.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0
131	10	11	0.0D0	10.0D0	9.0D0	1.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0
132	10	11	0.0D0	10.0D0	10.0D0	1.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0	0.0D0
1	1	1	121	0											
1	120	1	1	1											
1	120	1	122	1											
1	9	1	1	12	133	122	2	13	134	123	1				
11	9	1	12	23	144	133	13	24	145	134	1				
21	9	1	23	34	155	144	24	35	156	145	1				
31	9	1	34	45	166	155	35	46	167	156	1				
41	9	1	45	56	177	166	46	57	178	167	1				
51	9	1	56	67	188	177	57	68	189	178	1				

END OF NNPLR(K)

END OF GNLR(I,1)

END OF GNLR(I,2)

Table 2 (Continued)

61	9	1	67	78	199	188	68	79	200	189	1		
71	9	1	78	89	210	199	79	90	211	200	1		
81	9	1	89	100	221	210	90	101	222	211	1		
91	9	1	100	111	232	221	101	112	233	222	1		
END OF IE													
1	10	11			10.000		0.000						
2	10	11			9.000		0.000						
3	10	11			8.000		0.000						
4	10	11			7.000		0.000						
5	10	11			6.000		0.000						
6	10	11			5.000		0.000						
7	10	11			4.000		0.000						
8	10	11			3.000		0.000						
9	10	11			2.000		0.000						
10	10	11			1.000		0.000						
11	10	11			0.000		0.000						
122	10	11			10.000		0.000						
123	10	11			9.000		0.000						
124	10	11			8.000		0.000						
125	10	11			7.000		0.000						
126	10	11			6.000		0.000						
127	10	11			5.000		0.000						
128	10	11			4.000		0.000						
129	10	11			3.000		0.000						
130	10	11			2.000		0.000						
131	10	11			1.000		0.000						
132	10	11			0.000		0.000						
END OF IC													
0	0	0	0	0	0	0	0	0	0	0	0	18	38
2	2	6	1	2									
	0.000	6.000	-3	1.000	38		6.000	-3					
	0.000	0.000	0	1.000	38		0.000	0					
1	9	1	1	0									
11	7	1	2	0									
END OF IRTYP													
1	9	1	11	22	143	132	11	11	11	11			
11	7	1	120	241	242	121	-1	-1	-1	-1			
END OF ISV(J,I) J-1,4													
1	10	1	11	11									
12	7	1	120	-1									
20	10	1	132	11									
31	7	1	241	-1									
END OF NPVB													
1	37	1			0.000		0.000						
END OF HCON													

Corresponding to the above dimension specification, we must make the following data statements in BLOCK DATA to specify the maximum-control integers:

```
DATA MAXEL,MAXNP,MAXBES,MAXBNP,JBAND/100,242,240,242,27/
DATA MAXNTI,MXNDTC/1,1/
DATA LTMXNP,LMXNP,LMXBW,MXREGN/242,121,25,2/
DATA MXSEL,MXSPR,MXSDP,MXWNP,MXWPR,MXWDP/1,1,1,1,1,1/
DATA MXCNP,MXCES,MXCPR,MXCDP/1,1,1,1/
DATA MXNNP,MXNES,MXNPR,MXNDP/1,1,1,1/
DATA MXVES,MXVNP,MXVPR,MXVDP/18,38,2,2/
DATA MXDNP,MXDPR,MXDDP/6,1,2/
DATA MAXMA1,MXSPPM,MXMPPM/1,5,6/
```

To reflect the soil property function given by Eqs. (115) and (116), we have to modify the subroutine SPROP given in Appendix A. Lines between SPRO 405 and SPRO 535 in the subroutine SPROP must be modified according to

```
WCR=THPROP(1,MTYP)
WCS=THPROP(2,MTYP)
HAA=THPROP(3,MTYP)
THAA=THPROP(4,MTYP)
THBB=THPROP(5,MTYP)
POWER=AKPROP(1,MTYP)
DO 800 KG=1,8
HNP=HKG(KG)
HNP--HNP
C
C ----- SATURATED CONDITION
C
IF(HNP.GT.0) GO TO 700
TH(KG,M)=WCS
AKR(KG,M)=1.0D0
```

```

      DTH(KG,M)-0.0D0
      GO TO 800
C
C ----- UNSATURATED CASE
C
700 THMKG=WCS+(WCS-WCR)*THAA/(THAA+(DABS(-HNP-HAA))**THBB)
      TH(KG,M)-THMKG
      AKR(KG,M)-((THMKG-WCR)/(WCS-WCR))**POWER
      DNOM=THAA+(DABS(-HNP-HAA))**THBB
      DTH(KG,M)-(WCS-WCR)*THAA*(DABS(-HNP-THAA))**((THBB-1.0D0)/DNOM)**2
C

```

The pressure head simulated with 3DFEMWATER is plotted in Fig. 11. Numerical predictions of these pressure heads are in agreement with those given by Huyakorn (1986). This verifies the one-step steady state solution algorithm provided in 3DFEMWATER. The slight difference between 3DFEMWATER and that of Huyakorn results from the implementation of the variable boundary conditions. While 3DFEMWATER allows the whole amount of flux to infiltrate if the media are capable to do so; the model given by Huyakorn only allows a fraction of flux to infiltrate as long as the ponding depth condition is not violated.

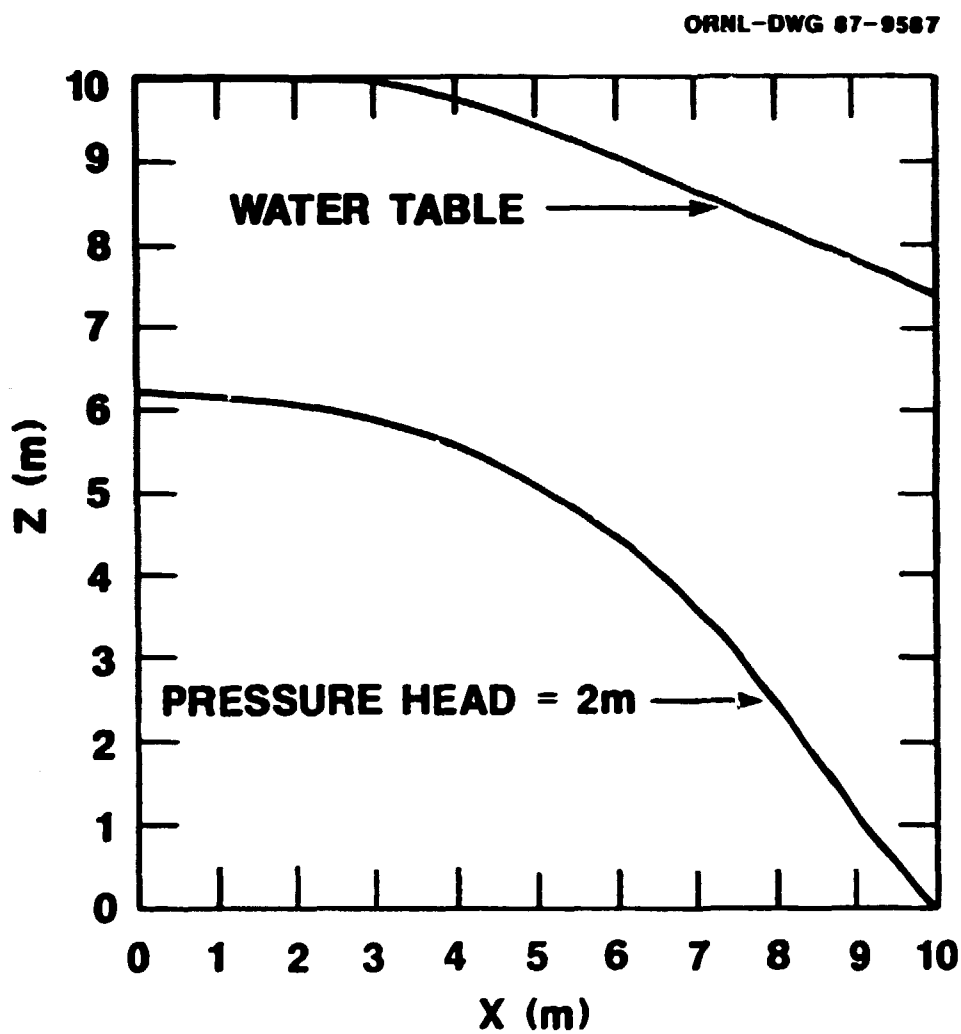


Fig. 11. Simulated steady state profiles of water table and base pressure head for the two-dimensional drainage problem.

6.3 Three-Dimensional Pumping Problem

This example is selected to represent the simulation of a three-dimensional problem with 3DFEMWATER. The problem involves the steady state flow to a pumping well. The region of interest is bounded on the left and right by hydraulically connected rivers; on the front, back, and bottom by impervious aquifuges; and on the top by an air-soil interface (Fig. 12). A pumping well is located at $(x,y) = (540,400)$ (Fig. 12). Initially, the water table is assumed to be horizontal and is 60 m above the bottom of the aquifer. The water level at the well is then lowered to a height of 30 m. This height is held until a steady state condition is reached. The medium in the region is assumed to be anisotropic and have saturated hydraulic conductivity components $K_{xx} = 5$ m/d, $K_{yy} = 0.5$ m/d, and $K_{zz} = 2$ m/d. The porosity of the medium is 0.25 and the field capacity is 0.0125. The unsaturated characteristic hydraulic properties of the medium are given as

$$\theta = \theta_s + (\theta_s - \theta_r) \frac{1}{1 + (\alpha |h - h_a|)^\beta} \quad (117)$$

and

$$K_r = \left(\frac{\theta - \theta_r}{\theta_s - \theta_r} \right)^2 \quad (118)$$

where h_a , α , and β are the parameters used to compute the water content and the relative hydraulic conductivity.

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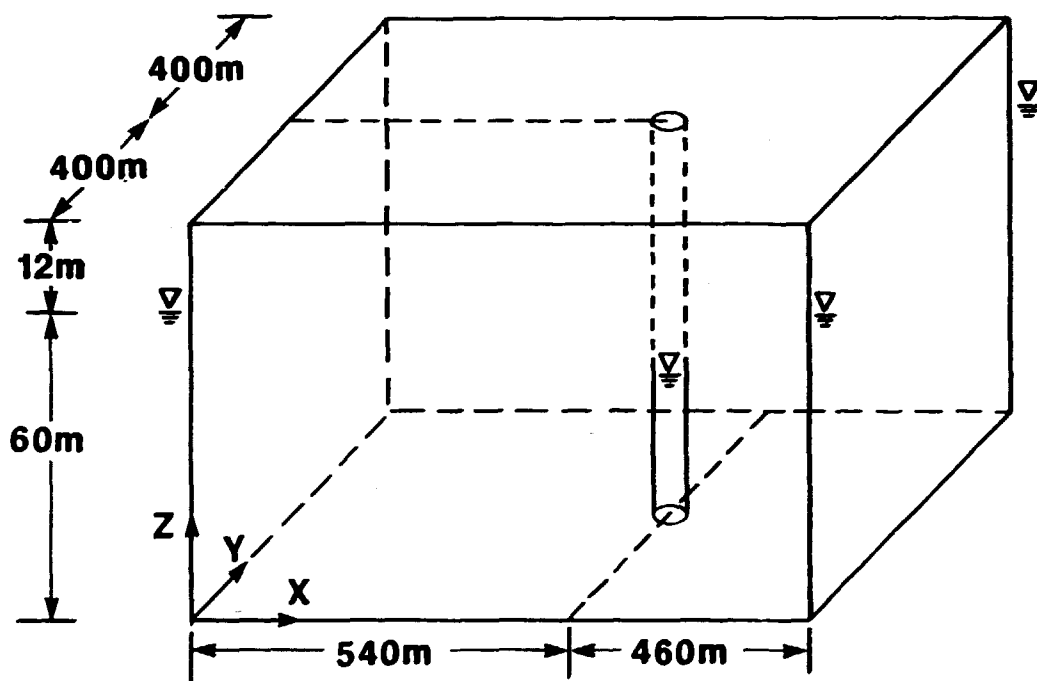


Fig. 12. Problem definition for the three-dimensional steady state flow from pumping.

Because of the symmetry, the region for numerical simulation will be taken as $0 < x < 1000$ m, $0 < y < 400$ m, and $0 < z < 72$ m. The boundary conditions are given as: pressure head is assumed hydrostatic on two vertical planes located at $x = 0$ and $0 < z < 60$, and $x = 1000$ and $0 < z < 60$, respectively; no flux is imposed on all other boundaries of the flow regime. A steady state solution will be sought. A pre-initial condition is set as $h = 60 - z$.

The region of interest is discretized with $20 \times 8 \times 10 = 1600$ elements resulting in $21 \times 9 \times 11 = 2079$ node points. The nodes are located at $x = 0, 70, 120, 160, 200, 275, 350, 400, 450, 500, 540, 570, 600, 650, 750, 800, 850, 900, 950,$ and 1000 in the x -direction, and at $z = 0, 15, 30, 35, 40, 45, 50, 55, 60, 66,$ and 72 m in the z -direction as reported by Huyakorn et al (1986). In the y -direction, nodes are spaced evenly at $\Delta z = 50$ m. For 3DFEMWATER simulation, each of the nine vertical planes perpendicular to the y -axis will be considered a subregion. Thus, a total of 9 subregions, each with 231 node points, is used for the subregional block iteration simulation.

The pressure head tolerance is 10^{-2} m for nonlinear iteration and is $5 \cdot 10^{-3}$ m for block iteration. The relaxation factors for nonlinear iteration and block iteration are set equal to 1.0 and 1.5, respectively.

With the above descriptions, the input data can be prepared according

to the instructions given in Sect. 5.3. The input data are given in Table 3.

To execute the problem, the arrays in the main program should be dimensioned as

```
DIMENSION X(2079),Y(2079),Z(2079),IE(1600,9)
DIMENSION CMATRIX(2079,27),GNOJCN(27,2079),RLD(2079),RI(2079),RL(2079)
DIMENSION NTNPLR(9),NNPLR(9),LMAXDF(9)
DIMENSION GNLR(693,9),LNOJCN(27,231,9)
DIMENSION CMTRXL(231,25),RLD(231)
DIMENSION H(2079),HP(2079),HW(2079),HT(2079),VX(2079),VY(2079),VZ(2079)
DIMENSION TH(8,1600),DTH(8,1600),AKR(8,1600),NPCNV(2079)
DIMENSION DCOSB(3,880),ISB(6,880),NPBB(882),BFLX(882),BFLXP(882)
DIMENSION SOS(1),SOSF(1,1),TSOSF(1,1),ISTYP(1),MSEL(1)
DIMENSION WSS(1),WSSF(1,1),TWSSF(1,1),IWTYP(1),NPW(1)
DIMENSION QCB(1),QCBF(1,1),TQCBF(1,1)
DIMENSION ICTYP(1),ISC(5,1),NPCB(1)
DIMENSION QNB(1),QNB(1,1),TQNB(1,1)
DIMENSION INTYP(1),ISN(5,1),NPNB(1)
DIMENSION RFALL(1),RF(1,1),TRF(1,1)
DIMENSION IRTYP(1),ISV(5,1),NPVB(1)
DIMENSION DCYFLX(1),FLX(1),HCON(1),HMIN(1)
DIMENSION NPFLX(1),NPCON(1),NPMIN(1)
DIMENSION HDB(2),HDBF(2,2),THDBF(2,2),IDTYP(165),NPDB(165)
DIMENSION PROP(6,1)
DIMENSION THPROP(5,1),AKPROP(5,1)
DIMENSION KPR(1),KDSK(1),TDTCH(1)
```

Corresponding to the above dimension specification, we must make the

Table 3 (Continued)

38	8	231	0.16D+03	0.00D+00	0.40D+02	0.00D+00	0.50D+02	0.00D+00
39	8	231	0.16D+03	0.00D+00	0.45D+02	0.00D+00	0.50D+02	0.00D+00
40	8	231	0.16D+03	0.00D+00	0.50D+02	0.00D+00	0.50D+02	0.00D+00
41	8	231	0.16D+03	0.00D+00	0.55D+02	0.00D+00	0.50D+02	0.00D+00
42	8	231	0.16D+03	0.00D+00	0.60D+02	0.00D+00	0.50D+02	0.00D+00
43	8	231	0.16D+03	0.00D+00	0.66D+02	0.00D+00	0.50D+02	0.00D+00
44	8	231	0.16D+03	0.00D+00	0.72D+02	0.00D+00	0.50D+02	0.00D+00
45	8	231	0.20D+03	0.00D+00	0.00D+00	0.00D+00	0.50D+02	0.00D+00
46	8	231	0.20D+03	0.00D+00	0.15D+02	0.00D+00	0.50D+02	0.00D+00
47	8	231	0.20D+03	0.00D+00	0.30D+02	0.00D+00	0.50D+02	0.00D+00
48	8	231	0.20D+03	0.00D+00	0.35D+02	0.00D+00	0.50D+02	0.00D+00
49	8	231	0.20D+03	0.00D+00	0.40D+02	0.00D+00	0.50D+02	0.00D+00
50	8	231	0.20D+03	0.00D+00	0.45D+02	0.00D+00	0.50D+02	0.00D+00
51	8	231	0.20D+03	0.00D+00	0.50D+02	0.00D+00	0.50D+02	0.00D+00
52	8	231	0.20D+03	0.00D+00	0.55D+02	0.00D+00	0.50D+02	0.00D+00
53	8	231	0.20D+03	0.00D+00	0.60D+02	0.00D+00	0.50D+02	0.00D+00
54	8	231	0.20D+03	0.00D+00	0.66D+02	0.00D+00	0.50D+02	0.00D+00
55	8	231	0.20D+03	0.00D+00	0.72D+02	0.00D+00	0.50D+02	0.00D+00
56	8	231	0.28D+03	0.00D+00	0.00D+00	0.00D+00	0.50D+02	0.00D+00
57	8	231	0.28D+03	0.00D+00	0.15D+02	0.00D+00	0.50D+02	0.00D+00
58	8	231	0.28D+03	0.00D+00	0.30D+02	0.00D+00	0.50D+02	0.00D+00
59	8	231	0.28D+03	0.00D+00	0.35D+02	0.00D+00	0.50D+02	0.00D+00
60	8	231	0.28D+03	0.00D+00	0.40D+02	0.00D+00	0.50D+02	0.00D+00
61	8	231	0.28D+03	0.00D+00	0.45D+02	0.00D+00	0.50D+02	0.00D+00
62	8	231	0.28D+03	0.00D+00	0.50D+02	0.00D+00	0.50D+02	0.00D+00
63	8	231	0.28D+03	0.00D+00	0.55D+02	0.00D+00	0.50D+02	0.00D+00
64	8	231	0.28D+03	0.00D+00	0.60D+02	0.00D+00	0.50D+02	0.00D+00
65	8	231	0.28D+03	0.00D+00	0.66D+02	0.00D+00	0.50D+02	0.00D+00
66	8	231	0.28D+03	0.00D+00	0.72D+02	0.00D+00	0.50D+02	0.00D+00
67	8	231	0.35D+03	0.00D+00	0.00D+00	0.00D+00	0.50D+02	0.00D+00
68	8	231	0.35D+03	0.00D+00	0.15D+02	0.00D+00	0.50D+02	0.00D+00
69	8	231	0.35D+03	0.00D+00	0.30D+02	0.00D+00	0.50D+02	0.00D+00
70	8	231	0.35D+03	0.00D+00	0.35D+02	0.00D+00	0.50D+02	0.00D+00
71	8	231	0.35D+03	0.00D+00	0.40D+02	0.00D+00	0.50D+02	0.00D+00
72	8	231	0.35D+03	0.00D+00	0.45D+02	0.00D+00	0.50D+02	0.00D+00
73	8	231	0.35D+03	0.00D+00	0.50D+02	0.00D+00	0.50D+02	0.00D+00
74	8	231	0.35D+03	0.00D+00	0.55D+02	0.00D+00	0.50D+02	0.00D+00
75	8	231	0.35D+03	0.00D+00	0.60D+02	0.00D+00	0.50D+02	0.00D+00
76	8	231	0.35D+03	0.00D+00	0.66D+02	0.00D+00	0.50D+02	0.00D+00
77	8	231	0.35D+03	0.00D+00	0.72D+02	0.00D+00	0.50D+02	0.00D+00
78	8	231	0.40D+03	0.00D+00	0.00D+00	0.00D+00	0.50D+02	0.00D+00
79	8	231	0.40D+03	0.00D+00	0.15D+02	0.00D+00	0.50D+02	0.00D+00
80	8	231	0.40D+03	0.00D+00	0.30D+02	0.00D+00	0.50D+02	0.00D+00
81	8	231	0.40D+03	0.00D+00	0.35D+02	0.00D+00	0.50D+02	0.00D+00
82	8	231	0.40D+03	0.00D+00	0.40D+02	0.00D+00	0.50D+02	0.00D+00

Table 3 (Continued)

83	8	231	0.40D+03	0.00D+00	0.45D+02	0.00D+00	0.50D+02	0.00D+00
84	8	231	0.40D+03	0.00D+00	0.50D+02	0.00D+00	0.50D+02	0.00D+00
85	8	231	0.40D+03	0.00D+00	0.55D+02	0.00D+00	0.50D+02	0.00D+00
86	8	231	0.40D+03	0.00D+00	0.60D+02	0.00D+00	0.50D+02	0.00D+00
87	8	231	0.40D+03	0.00D+00	0.66D+02	0.00D+00	0.50D+02	0.00D+00
88	8	231	0.40D+03	0.00D+00	0.72D+02	0.00D+00	0.50D+02	0.00D+00
89	8	231	0.45D+03	0.00D+00	0.00D+00	0.00D+00	0.50D+02	0.00D+00
90	8	231	0.45D+03	0.00D+00	0.15D+02	0.00D+00	0.50D+02	0.00D+00
91	8	231	0.45D+03	0.00D+00	0.30D+02	0.00D+00	0.50D+02	0.00D+00
92	8	231	0.45D+03	0.00D+00	0.35D+02	0.00D+00	0.50D+02	0.00D+00
93	8	231	0.45D+03	0.00D+00	0.40D+02	0.00D+00	0.50D+02	0.00D+00
94	8	231	0.45D+03	0.00D+00	0.45D+02	0.00D+00	0.50D+02	0.00D+00
95	8	231	0.45D+03	0.00D+00	0.50D+02	0.00D+00	0.50D+02	0.00D+00
96	8	231	0.45D+03	0.00D+00	0.55D+02	0.00D+00	0.50D+02	0.00D+00
97	8	231	0.45D+03	0.00D+00	0.60D+02	0.00D+00	0.50D+02	0.00D+00
98	8	231	0.45D+03	0.00D+00	0.66D+02	0.00D+00	0.50D+02	0.00D+00
99	8	231	0.45D+03	0.00D+00	0.72D+02	0.00D+00	0.50D+02	0.00D+00
100	8	231	0.50D+03	0.00D+00	0.00D+00	0.00D+00	0.50D+02	0.00D+00
101	8	231	0.50D+03	0.00D+00	0.15D+02	0.00D+00	0.50D+02	0.00D+00
102	8	231	0.50D+03	0.00D+00	0.30D+02	0.00D+00	0.50D+02	0.00D+00
103	8	231	0.50D+03	0.00D+00	0.35D+02	0.00D+00	0.50D+02	0.00D+00
104	8	231	0.50D+03	0.00D+00	0.40D+02	0.00D+00	0.50D+02	0.00D+00
105	8	231	0.50D+03	0.00D+00	0.45D+02	0.00D+00	0.50D+02	0.00D+00
106	8	231	0.50D+03	0.00D+00	0.50D+02	0.00D+00	0.50D+02	0.00D+00
107	8	231	0.50D+03	0.00D+00	0.55D+02	0.00D+00	0.50D+02	0.00D+00
108	8	231	0.50D+03	0.00D+00	0.60D+02	0.00D+00	0.50D+02	0.00D+00
109	8	231	0.50D+03	0.00D+00	0.66D+02	0.00D+00	0.50D+02	0.00D+00
110	8	231	0.50D+03	0.00D+00	0.72D+02	0.00D+00	0.50D+02	0.00D+00
111	8	231	0.54D+03	0.00D+00	0.00D+00	0.00D+00	0.50D+02	0.00D+00
112	8	231	0.54D+03	0.00D+00	0.15D+02	0.00D+00	0.50D+02	0.00D+00
113	8	231	0.54D+03	0.00D+00	0.30D+02	0.00D+00	0.50D+02	0.00D+00
114	8	231	0.54D+03	0.00D+00	0.35D+02	0.00D+00	0.50D+02	0.00D+00
115	8	231	0.54D+03	0.00D+00	0.40D+02	0.00D+00	0.50D+02	0.00D+00
116	8	231	0.54D+03	0.00D+00	0.45D+02	0.00D+00	0.50D+02	0.00D+00
117	8	231	0.54D+03	0.00D+00	0.50D+02	0.00D+00	0.50D+02	0.00D+00
118	8	231	0.54D+03	0.00D+00	0.55D+02	0.00D+00	0.50D+02	0.00D+00
119	8	231	0.54D+03	0.00D+00	0.60D+02	0.00D+00	0.50D+02	0.00D+00
120	8	231	0.54D+03	0.00D+00	0.66D+02	0.00D+00	0.50D+02	0.00D+00
121	8	231	0.54D+03	0.00D+00	0.72D+02	0.00D+00	0.50D+02	0.00D+00
122	8	231	0.57D+03	0.00D+00	0.00D+00	0.00D+00	0.50D+02	0.00D+00
123	8	231	0.57D+03	0.00D+00	0.15D+02	0.00D+00	0.50D+02	0.00D+00
124	8	231	0.57D+03	0.00D+00	0.30D+02	0.00D+00	0.50D+02	0.00D+00
125	8	231	0.57D+03	0.00D+00	0.35D+02	0.00D+00	0.50D+02	0.00D+00
126	8	231	0.57D+03	0.00D+00	0.40D+02	0.00D+00	0.50D+02	0.00D+00
127	8	231	0.57D+03	0.00D+00	0.45D+02	0.00D+00	0.50D+02	0.00D+00

Table 3 (Continued)

128	8	231	0.57D+03	0.00D+00	0.50D+02	0.00D+00	0.50D+02	0.00D+00
129	8	231	0.57D+03	0.00D+00	0.55D+02	0.00D+00	0.50D+02	0.00D+00
130	8	231	0.57D+03	0.00D+00	0.60D+02	0.00D+00	0.50D+02	0.00D+00
131	8	231	0.57D+03	0.00D+00	0.66D+02	0.00D+00	0.50D+02	0.00D+00
132	8	231	0.57D+03	0.00D+00	0.72D+02	0.00D+00	0.50D+02	0.00D+00
133	8	231	0.60D+03	0.00D+00	0.00D+00	0.00D+00	0.50D+02	0.00D+00
134	8	231	0.60D+03	0.00D+00	0.15D+02	0.00D+00	0.50D+02	0.00D+00
135	8	231	0.60D+03	0.00D+00	0.30D+02	0.00D+00	0.50D+02	0.00D+00
136	8	231	0.60D+03	0.00D+00	0.35D+02	0.00D+00	0.50D+02	0.00D+00
137	8	231	0.60D+03	0.00D+00	0.40D+02	0.00D+00	0.50D+02	0.00D+00
138	8	231	0.60D+03	0.00D+00	0.45D+02	0.00D+00	0.50D+02	0.00D+00
139	8	231	0.60D+03	0.00D+00	0.50D+02	0.00D+00	0.50D+02	0.00D+00
140	8	231	0.60D+03	0.00D+00	0.55D+02	0.00D+00	0.50D+02	0.00D+00
141	8	231	0.60D+03	0.00D+00	0.60D+02	0.00D+00	0.50D+02	0.00D+00
142	8	231	0.60D+03	0.00D+00	0.66D+02	0.00D+00	0.50D+02	0.00D+00
143	8	231	0.60D+03	0.00D+00	0.72D+02	0.00D+00	0.50D+02	0.00D+00
144	8	231	0.65D+03	0.00D+00	0.00D+00	0.00D+00	0.50D+02	0.00D+00
145	8	231	0.65D+03	0.00D+00	0.15D+02	0.00D+00	0.50D+02	0.00D+00
146	8	231	0.65D+03	0.00D+00	0.30D+02	0.00D+00	0.50D+02	0.00D+00
147	8	231	0.65D+03	0.00D+00	0.35D+02	0.00D+00	0.50D+02	0.00D+00
148	8	231	0.65D+03	0.00D+00	0.40D+02	0.00D+00	0.50D+02	0.00D+00
149	8	231	0.65D+03	0.00D+00	0.45D+02	0.00D+00	0.50D+02	0.00D+00
150	8	231	0.65D+03	0.00D+00	0.50D+02	0.00D+00	0.50D+02	0.00D+00
151	8	231	0.65D+03	0.00D+00	0.55D+02	0.00D+00	0.50D+02	0.00D+00
152	8	231	0.65D+03	0.00D+00	0.60D+02	0.00D+00	0.50D+02	0.00D+00
153	8	231	0.65D+03	0.00D+00	0.66D+02	0.00D+00	0.50D+02	0.00D+00
154	8	231	0.65D+03	0.00D+00	0.72D+02	0.00D+00	0.50D+02	0.00D+00
155	8	231	0.70D+03	0.00D+00	0.00D+00	0.00D+00	0.50D+02	0.00D+00
156	8	231	0.70D+03	0.00D+00	0.15D+02	0.00D+00	0.50D+02	0.00D+00
157	8	231	0.70D+03	0.00D+00	0.30D+02	0.00D+00	0.50D+02	0.00D+00
158	8	231	0.70D+03	0.00D+00	0.35D+02	0.00D+00	0.50D+02	0.00D+00
159	8	231	0.70D+03	0.00D+00	0.40D+02	0.00D+00	0.50D+02	0.00D+00
160	8	231	0.70D+03	0.00D+00	0.45D+02	0.00D+00	0.50D+02	0.00D+00
161	8	231	0.70D+03	0.00D+00	0.50D+02	0.00D+00	0.50D+02	0.00D+00
162	8	231	0.70D+03	0.00D+00	0.55D+02	0.00D+00	0.50D+02	0.00D+00
163	8	231	0.70D+03	0.00D+00	0.60D+02	0.00D+00	0.50D+02	0.00D+00
164	8	231	0.70D+03	0.00D+00	0.66D+02	0.00D+00	0.50D+02	0.00D+00
165	8	231	0.70D+03	0.00D+00	0.72D+02	0.00D+00	0.50D+02	0.00D+00
166	8	231	0.75D+03	0.00D+00	0.00D+00	0.00D+00	0.50D+02	0.00D+00
167	8	231	0.75D+03	0.00D+00	0.15D+02	0.00D+00	0.50D+02	0.00D+00
168	8	231	0.75D+03	0.00D+00	0.30D+02	0.00D+00	0.50D+02	0.00D+00
169	8	231	0.75D+03	0.00D+00	0.35D+02	0.00D+00	0.50D+02	0.00D+00
170	8	231	0.75D+03	0.00D+00	0.40D+02	0.00D+00	0.50D+02	0.00D+00
171	8	231	0.75D+03	0.00D+00	0.45D+02	0.00D+00	0.50D+02	0.00D+00
172	8	231	0.75D+03	0.00D+00	0.50D+02	0.00D+00	0.50D+02	0.00D+00

Table 3 (Continued)

173	8	231	0.75D+03	0.00D+00	0.55D+02	0.00D+00	0.50D+02	0.00D+00
174	8	231	0.75D+03	0.00D+00	0.60D+02	0.00D+00	0.50D+02	0.00D+00
175	8	231	0.75D+03	0.00D+00	0.66D+02	0.00D+00	0.50D+02	0.00D+00
176	8	231	0.75D+03	0.00D+00	0.72D+02	0.00D+00	0.50D+02	0.00D+00
177	8	231	0.80D+03	0.00D+00	0.00D+00	0.00D+00	0.50D+02	0.00D+00
178	8	231	0.80D+03	0.00D+00	0.15D+02	0.00D+00	0.50D+02	0.00D+00
179	8	231	0.80D+03	0.00D+00	0.30D+02	0.00D+00	0.50D+02	0.00D+00
180	8	231	0.80D+03	0.00D+00	0.35D+02	0.00D+00	0.50D+02	0.00D+00
181	8	231	0.80D+03	0.00D+00	0.40D+02	0.00D+00	0.50D+02	0.00D+00
182	8	231	0.80D+03	0.00D+00	0.45D+02	0.00D+00	0.50D+02	0.00D+00
183	8	231	0.80D+03	0.00D+00	0.50D+02	0.00D+00	0.50D+02	0.00D+00
184	8	231	0.80D+03	0.00D+00	0.55D+02	0.00D+00	0.50D+02	0.00D+00
185	8	231	0.80D+03	0.00D+00	0.60D+02	0.00D+00	0.50D+02	0.00D+00
186	8	231	0.80D+03	0.00D+00	0.66D+02	0.00D+00	0.50D+02	0.00D+00
187	8	231	0.80D+03	0.00D+00	0.72D+02	0.00D+00	0.50D+02	0.00D+00
188	8	231	0.85D+03	0.00D+00	0.00D+00	0.00D+00	0.50D+02	0.00D+00
189	8	231	0.85D+03	0.00D+00	0.15D+02	0.00D+00	0.50D+02	0.00D+00
190	8	231	0.85D+03	0.00D+00	0.30D+02	0.00D+00	0.50D+02	0.00D+00
191	8	231	0.85D+03	0.00D+00	0.35D+02	0.00D+00	0.50D+02	0.00D+00
192	8	231	0.85D+03	0.00D+00	0.40D+02	0.00D+00	0.50D+02	0.00D+00
193	8	231	0.85D+03	0.00D+00	0.45D+02	0.00D+00	0.50D+02	0.00D+00
194	8	231	0.85D+03	0.00D+00	0.50D+02	0.00D+00	0.50D+02	0.00D+00
195	8	231	0.85D+03	0.00D+00	0.55D+02	0.00D+00	0.50D+02	0.00D+00
196	8	231	0.85D+03	0.00D+00	0.60D+02	0.00D+00	0.50D+02	0.00D+00
197	8	231	0.85D+03	0.00D+00	0.66D+02	0.00D+00	0.50D+02	0.00D+00
198	8	231	0.85D+03	0.00D+00	0.72D+02	0.00D+00	0.50D+02	0.00D+00
199	8	231	0.90D+03	0.00D+00	0.00D+00	0.00D+00	0.50D+02	0.00D+00
200	8	231	0.90D+03	0.00D+00	0.15D+02	0.00D+00	0.50D+02	0.00D+00
201	8	231	0.90D+03	0.00D+00	0.30D+02	0.00D+00	0.50D+02	0.00D+00
202	8	231	0.90D+03	0.00D+00	0.35D+02	0.00D+00	0.50D+02	0.00D+00
203	8	231	0.90D+03	0.00D+00	0.40D+02	0.00D+00	0.50D+02	0.00D+00
204	8	231	0.90D+03	0.00D+00	0.45D+02	0.00D+00	0.50D+02	0.00D+00
205	8	231	0.90D+03	0.00D+00	0.50D+02	0.00D+00	0.50D+02	0.00D+00
206	8	231	0.90D+03	0.00D+00	0.55D+02	0.00D+00	0.50D+02	0.00D+00
207	8	231	0.90D+03	0.00D+00	0.60D+02	0.00D+00	0.50D+02	0.00D+00
208	8	231	0.90D+03	0.00D+00	0.66D+02	0.00D+00	0.50D+02	0.00D+00
209	8	231	0.90D+03	0.00D+00	0.72D+02	0.00D+00	0.50D+02	0.00D+00
210	8	231	0.95D+03	0.00D+00	0.00D+00	0.00D+00	0.50D+02	0.00D+00
211	8	231	0.95D+03	0.00D+00	0.15D+02	0.00D+00	0.50D+02	0.00D+00
212	8	231	0.95D+03	0.00D+00	0.30D+02	0.00D+00	0.50D+02	0.00D+00
213	8	231	0.95D+03	0.00D+00	0.35D+02	0.00D+00	0.50D+02	0.00D+00
214	8	231	0.95D+03	0.00D+00	0.40D+02	0.00D+00	0.50D+02	0.00D+00
215	8	231	0.95D+03	0.00D+00	0.45D+02	0.00D+00	0.50D+02	0.00D+00
216	8	231	0.95D+03	0.00D+00	0.50D+02	0.00D+00	0.50D+02	0.00D+00
217	8	231	0.95D+03	0.00D+00	0.55D+02	0.00D+00	0.50D+02	0.00D+00

Table 3 (Continued)

218	8	231	0.95D+03	0.00D+00	0.60D+02	0.00D+00	0.50D+02	0.00D+00
219	8	231	0.95D+03	0.00D+00	0.66D+02	0.00D+00	0.50D+02	0.00D+00
220	8	231	0.95D+03	0.00D+00	0.72D+02	0.00D+00	0.50D+02	0.00D+00
221	8	231	0.10D+04	0.00D+00	0.00D+00	0.00D+00	0.50D+02	0.00D+00
222	8	231	0.10D+04	0.00D+00	0.15D+02	0.00D+00	0.50D+02	0.00D+00
223	8	231	0.10D+04	0.00D+00	0.30D+02	0.00D+00	0.50D+02	0.00D+00
224	8	231	0.10D+04	0.00D+00	0.35D+02	0.00D+00	0.50D+02	0.00D+00
225	8	231	0.10D+04	0.00D+00	0.40D+02	0.00D+00	0.50D+02	0.00D+00
226	8	231	0.10D+04	0.00D+00	0.45D+02	0.00D+00	0.50D+02	0.00D+00
227	8	231	0.10D+04	0.00D+00	0.50D+02	0.00D+00	0.50D+02	0.00D+00
228	8	231	0.10D+04	0.00D+00	0.55D+02	0.00D+00	0.50D+02	0.00D+00
229	8	231	0.10D+04	0.00D+00	0.60D+02	0.00D+00	0.50D+02	0.00D+00
230	8	231	0.10D+04	0.00D+00	0.66D+02	0.00D+00	0.50D+02	0.00D+00
231	8	231	0.10D+04	0.00D+00	0.72D+02	0.00D+00	0.50D+02	0.00D+00

END OF COORDINATE

1 8 1 231 0

END OF NNPLR(9)

1 230 1 1 1

END OF GNLR(I,1)

1 230 1 232 1

END OF GNLR(I,2)

1 230 1 463 1

END OF GNLR(I,3)

1 230 1 694 1

END OF GNLR(I,4)

1 230 1 925 1

END OF GNLR(I,5)

1 230 1 1156 1

END OF GNLR(I,6)

1 230 1 1387 1

END OF GNLR(I,7)

1 230 1 1618 1

END OF GNLR(I,8)

1 230 1 1849 1

END OF GNLR(I,9)

1	9	1	1	12	13	2	232	243	244	233	1
11	9	1	12	23	24	13	243	254	255	244	1
21	9	1	23	34	35	24	254	265	266	255	1
31	9	1	34	45	46	35	265	276	277	266	1
41	9	1	45	56	57	46	276	287	288	277	1
51	9	1	56	67	68	57	287	298	299	288	1
61	9	1	67	78	79	68	298	309	310	299	1
71	9	1	78	89	90	79	309	320	321	310	1
81	9	1	89	100	101	90	320	331	332	321	1
91	9	1	100	111	112	101	331	342	343	332	1

Table 3 (Continued)

101	9	1	111	122	123	112	342	353	354	343	1
111	9	1	122	133	134	123	353	364	365	354	1
121	9	1	133	144	145	134	364	375	376	365	1
131	9	1	144	155	156	145	375	386	387	376	1
141	9	1	155	166	167	156	386	397	398	387	1
151	9	1	166	177	178	167	397	408	409	398	1
161	9	1	177	188	189	178	408	419	420	409	1
171	9	1	188	199	200	189	419	430	431	420	1
181	9	1	199	210	211	200	430	441	442	431	1
191	9	1	210	221	222	211	441	452	453	442	1
201	9	1	232	243	244	233	463	474	475	464	1
211	9	1	243	254	255	244	474	485	486	475	1
221	9	1	254	265	266	255	485	496	497	486	1
231	9	1	265	276	277	266	496	507	508	497	1
241	9	1	276	287	288	277	507	518	519	508	1
251	9	1	287	298	299	288	518	529	530	519	1
261	9	1	298	309	310	299	529	540	541	530	1
271	9	1	309	320	321	310	540	551	552	541	1
281	9	1	320	331	332	321	551	562	563	552	1
291	9	1	331	342	343	332	562	573	574	563	1
301	9	1	342	353	354	343	573	584	585	574	1
311	9	1	353	364	365	354	584	595	596	585	1
321	9	1	364	375	376	365	595	606	607	596	1
331	9	1	375	386	387	376	606	617	618	607	1
341	9	1	386	397	398	387	617	628	629	618	1
351	9	1	397	408	409	398	628	639	640	629	1
361	9	1	408	419	420	409	639	650	651	640	1
371	9	1	419	430	431	420	650	661	662	651	1
381	9	1	430	441	442	431	661	672	673	662	1
391	9	1	441	452	453	442	672	683	684	673	1
401	9	1	463	474	475	464	694	705	706	695	1
411	9	1	474	485	486	475	705	716	717	706	1
421	9	1	485	496	497	486	716	727	728	717	1
431	9	1	496	507	508	497	727	738	739	728	1
441	9	1	507	518	519	508	738	749	750	739	1
451	9	1	518	529	530	519	749	760	761	750	1
461	9	1	529	540	541	530	760	771	772	761	1
471	9	1	540	551	552	541	771	782	783	772	1
481	9	1	551	562	563	552	782	793	794	783	1
491	9	1	562	573	574	563	793	804	805	794	1
501	9	1	573	584	585	574	804	815	816	805	1
511	9	1	584	595	596	585	815	826	827	816	1
521	9	1	595	606	607	596	826	837	838	827	1
531	9	1	606	617	618	607	837	848	849	838	1
541	9	1	617	628	629	618	848	859	860	849	1

Table 3 (Continued)

551	9	1	628	639	640	629	859	870	871	860	1
561	9	1	639	650	651	640	870	881	882	871	1
571	9	1	650	661	662	651	881	892	893	882	1
581	9	1	661	672	673	662	892	903	904	893	1
591	9	1	672	683	684	673	903	914	915	904	1
601	9	1	694	705	706	695	925	936	937	926	1
611	9	1	705	716	717	706	936	947	948	937	1
621	9	1	716	727	728	717	947	958	959	948	1
631	9	1	727	738	739	728	958	969	970	959	1
641	9	1	738	749	750	739	969	980	981	970	1
651	9	1	749	760	761	750	980	991	992	981	1
661	9	1	760	771	772	761	991	1002	1003	992	1
671	9	1	771	782	783	772	1002	1013	1014	1003	1
681	9	1	782	793	794	783	1013	1024	1025	1014	1
691	9	1	793	804	805	794	1024	1035	1036	1025	1
701	9	1	804	815	816	805	1035	1046	1047	1036	1
711	9	1	815	826	827	816	1046	1057	1058	1047	1
721	9	1	826	837	838	827	1057	1068	1069	1058	1
731	9	1	837	848	849	838	1068	1079	1080	1069	1
741	9	1	848	859	860	849	1079	1090	1091	1080	1
751	9	1	859	870	871	860	1090	1101	1102	1091	1
761	9	1	870	881	882	871	1101	1112	1113	1102	1
771	9	1	881	892	893	882	1112	1123	1124	1113	1
781	9	1	892	903	904	893	1123	1134	1135	1124	1
791	9	1	903	914	915	904	1134	1145	1146	1135	1
801	9	1	925	936	937	926	1156	1167	1168	1157	1
811	9	1	936	947	948	937	1167	1178	1179	1168	1
821	9	1	947	958	959	948	1178	1189	1190	1179	1
831	9	1	958	969	970	959	1189	1200	1201	1190	1
841	9	1	969	980	981	970	1200	1211	1212	1201	1
851	9	1	980	991	992	981	1211	1222	1223	1212	1
861	9	1	991	1002	1003	992	1222	1233	1234	1223	1
871	9	1	1002	1013	1014	1003	1233	1244	1245	1234	1
881	9	1	1013	1024	1025	1014	1244	1255	1256	1245	1
891	9	1	1024	1035	1036	1025	1255	1266	1267	1256	1
901	9	1	1035	1046	1047	1036	1266	1277	1278	1267	1
911	9	1	1046	1057	1058	1047	1277	1288	1289	1278	1
921	9	1	1057	1068	1069	1058	1288	1299	1300	1289	1
931	9	1	1068	1079	1080	1069	1299	1310	1311	1300	1
941	9	1	1079	1090	1091	1080	1310	1321	1322	1311	1
951	9	1	1090	1101	1102	1091	1321	1332	1333	1322	1
961	9	1	1101	1112	1113	1102	1332	1343	1344	1333	1
971	9	1	1112	1123	1124	1113	1343	1354	1355	1344	1
981	9	1	1123	1134	1135	1124	1354	1365	1366	1355	1
991	9	1	1134	1145	1146	1135	1365	1376	1377	1366	1

Table 3 (Continued)

1001	9	1	1156	1167	1168	1157	1387	1398	1399	1388	1
1011	9	1	1167	1178	1179	1168	1398	1409	1410	1399	1
1021	9	1	1178	1189	1190	1179	1409	1420	1421	1410	1
1031	9	1	1189	1200	1201	1190	1420	1431	1432	1421	1
1041	9	1	1200	1211	1212	1201	1431	1442	1443	1432	1
1051	9	1	1211	1222	1223	1212	1442	1453	1454	1443	1
1061	9	1	1222	1233	1234	1223	1453	1464	1465	1454	1
1071	9	1	1233	1244	1245	1234	1464	1475	1476	1465	1
1081	9	1	1244	1255	1256	1245	1475	1486	1487	1476	1
1091	9	1	1255	1266	1267	1256	1486	1497	1498	1487	1
1101	9	1	1266	1277	1278	1267	1497	1508	1509	1498	1
1111	9	1	1277	1288	1289	1278	1508	1519	1520	1509	1
1121	9	1	1288	1299	1300	1289	1519	1530	1531	1520	1
1131	9	1	1299	1310	1311	1300	1530	1541	1542	1531	1
1141	9	1	1310	1321	1322	1311	1541	1552	1553	1542	1
1151	9	1	1321	1332	1333	1322	1552	1563	1564	1553	1
1161	9	1	1332	1343	1344	1333	1563	1574	1575	1564	1
1171	9	1	1343	1354	1355	1344	1574	1585	1586	1575	1
1181	9	1	1354	1365	1366	1355	1585	1596	1597	1586	1
1191	9	1	1365	1376	1377	1366	1596	1607	1608	1597	1
1201	9	1	1387	1398	1399	1388	1618	1629	1630	1619	1
1211	9	1	1398	1409	1410	1399	1629	1640	1641	1630	1
1221	9	1	1409	1420	1421	1410	1640	1651	1652	1641	1
1231	9	1	1420	1431	1432	1421	1651	1662	1663	1652	1
1241	9	1	1431	1442	1443	1432	1662	1673	1674	1663	1
1251	9	1	1442	1453	1454	1443	1673	1684	1685	1674	1
1261	9	1	1453	1464	1465	1454	1684	1695	1696	1685	1
1271	9	1	1464	1475	1476	1465	1695	1706	1707	1696	1
1281	9	1	1475	1486	1487	1476	1706	1717	1718	1707	1
1291	9	1	1486	1497	1498	1487	1717	1728	1729	1718	1
1301	9	1	1497	1508	1509	1498	1728	1739	1740	1729	1
1311	9	1	1508	1519	1520	1509	1739	1750	1751	1740	1
1321	9	1	1519	1530	1531	1520	1750	1761	1762	1751	1
1331	9	1	1530	1541	1542	1531	1761	1772	1773	1762	1
1341	9	1	1541	1552	1553	1542	1772	1783	1784	1773	1
1351	9	1	1552	1563	1564	1553	1783	1794	1795	1784	1
1361	9	1	1563	1574	1575	1564	1794	1805	1806	1795	1
1371	9	1	1574	1585	1586	1575	1805	1816	1817	1806	1
1381	9	1	1585	1596	1597	1586	1816	1827	1828	1817	1
1391	9	1	1596	1607	1608	1597	1827	1838	1839	1828	1
1401	9	1	1618	1629	1630	1619	1849	1860	1861	1850	1
1411	9	1	1629	1640	1641	1630	1860	1871	1872	1861	1
1421	9	1	1640	1651	1652	1641	1871	1882	1883	1872	1
1431	9	1	1651	1662	1663	1652	1882	1893	1894	1883	1
1441	9	1	1662	1673	1674	1663	1893	1904	1905	1894	1

Table 3 (Continued)

1451	9	1	1673	1684	1685	1674	1904	1915	1916	1905	1
1461	9	1	1684	1695	1696	1685	1915	1926	1927	1916	1
1471	9	1	1695	1706	1707	1696	1926	1937	1938	1927	1
1481	9	1	1706	1717	1718	1707	1937	1948	1949	1938	1
1491	9	1	1717	1728	1729	1718	1948	1959	1960	1949	1
1501	9	1	1728	1739	1740	1729	1959	1970	1971	1960	1
1511	9	1	1739	1750	1751	1740	1970	1981	1982	1971	1
1521	9	1	1750	1761	1762	1751	1981	1992	1993	1982	1
1531	9	1	1761	1772	1773	1762	1992	2003	2004	1993	1
1541	9	1	1772	1783	1784	1773	2003	2014	2015	2004	1
1551	9	1	1783	1794	1795	1784	2014	2025	2026	2015	1
1561	9	1	1794	1805	1806	1795	2025	2036	2037	2025	1
1571	9	1	1805	1816	1817	1806	2036	2047	2048	2037	1
1581	9	1	1816	1827	1828	1817	2047	2058	2059	2048	1
1591	9	1	1827	1838	1839	1828	2058	2069	2070	2059	1

END OF IE

1	8	231	0.60D+02	0.00D+00
2	8	231	0.45D+02	0.00D+00
3	8	231	0.30D+02	0.00D+00
4	8	231	0.25D+02	0.00D+00
5	8	231	0.20D+02	0.00D+00
6	8	231	0.15D+02	0.00D+00
7	8	231	0.10D+02	0.00D+00
8	8	231	0.50D+01	0.00D+00
9	8	231	0.00D+00	0.00D+00
10	8	231	-0.60D+01	0.00D+00
11	8	231	-0.12D+02	0.00D+00
12	8	231	0.60D+02	0.00D+00
13	8	231	0.45D+02	0.00D+00
14	8	231	0.30D+02	0.00D+00
15	8	231	0.25D+02	0.00D+00
16	8	231	0.20D+02	0.00D+00
17	8	231	0.15D+02	0.00D+00
18	8	231	0.10D+02	0.00D+00
19	8	231	0.50D+01	0.00D+00
20	8	231	0.00D+00	0.00D+00
21	8	231	-0.60D+01	0.00D+00
22	8	231	-0.12D+02	0.00D+00
23	8	231	0.60D+02	0.00D+00
24	8	231	0.45D+02	0.00D+00
25	8	231	0.30D+02	0.00D+00
26	8	231	0.25D+02	0.00D+00
27	8	231	0.20D+02	0.00D+00
28	8	231	0.15D+02	0.00D+00
29	8	231	0.10D+02	0.00D+00

Table 3 (Continued)

30	8	231	0.50D+01	0.00D+00
31	8	231	0.00D+00	0.00D+00
32	8	231	-0.60D+01	0.00D+00
33	8	231	-0.12D+02	0.00D+00
34	8	231	0.60D+02	0.00D+00
35	8	231	0.45D+02	0.00D+00
36	8	231	0.30D+02	0.00D+00
37	8	231	0.25D+02	0.00D+00
38	8	231	0.20D+02	0.00D+00
39	8	231	0.15D+02	0.00D+00
40	8	231	0.10D+02	0.00D+00
41	8	231	0.50D+01	0.00D+00
42	8	231	0.00D+00	0.00D+00
43	8	231	-0.60D+01	0.00D+00
44	8	231	-0.12D+02	0.00D+00
45	8	231	0.60D+02	0.00D+00
46	8	231	0.45D+02	0.00D+00
47	8	231	0.30D+02	0.00D+00
48	8	231	0.25D+02	0.00D+00
49	8	231	0.20D+02	0.00D+00
50	8	231	0.15D+02	0.00D+00
51	8	231	0.10D+02	0.00D+00
52	8	231	0.50D+01	0.00D+00
53	8	231	0.00D+00	0.00D+00
54	8	231	-0.60D+01	0.00D+00
55	8	231	-0.12D+02	0.00D+00
56	8	231	0.60D+02	0.00D+00
57	8	231	0.45D+02	0.00D+00
58	8	231	0.30D+02	0.00D+00
59	8	231	0.25D+02	0.00D+00
60	8	231	0.20D+02	0.00D+00
61	8	231	0.15D+02	0.00D+00
62	8	231	0.10D+02	0.00D+00
63	8	231	0.50D+01	0.00D+00
64	8	231	0.00D+00	0.00D+00
65	8	231	-0.60D+01	0.00D+00
66	8	231	-0.12D+02	0.00D+00
67	8	231	0.60D+02	0.00D+00
68	8	231	0.45D+02	0.00D+00
69	8	231	0.30D+02	0.00D+00
70	8	231	0.25D+02	0.00D+00
71	8	231	0.20D+02	0.00D+00
72	8	231	0.15D+02	0.00D+00
73	8	231	0.10D+02	0.00D+00
74	8	231	0.50D+01	0.00D+00

Table 3 (Continued)

75	8	231	0.00D+00	0.00D+00
76	8	231	-0.60D+01	0.00D+00
77	8	231	-0.12D+02	0.00D+00
78	8	231	0.60D+02	0.00D+00
79	8	231	0.45D+02	0.00D+00
80	8	231	0.30D+02	0.00D+00
81	8	231	0.25D+02	0.00D+00
82	8	231	0.20D+02	0.00D+00
83	8	231	0.15D+02	0.00D+00
84	8	231	0.10D+02	0.00D+00
85	8	231	0.50D+01	0.00D+00
86	8	231	0.00D+00	0.00D+00
87	8	231	-0.60D+01	0.00D+00
88	8	231	-0.12D+02	0.00D+00
89	8	231	0.60D+02	0.00D+00
90	8	231	0.45D+02	0.00D+00
91	8	231	0.30D+02	0.00D+00
92	8	231	0.25D+02	0.00D+00
93	8	231	0.20D+02	0.00D+00
94	8	231	0.15D+02	0.00D+00
95	8	231	0.10D+02	0.00D+00
96	8	231	0.50D+01	0.00D+00
97	8	231	0.00D+00	0.00D+00
98	8	231	-0.60D+01	0.00D+00
99	8	231	-0.12D+02	0.00D+00
100	8	231	0.60D+02	0.00D+00
101	8	231	0.45D+02	0.00D+00
102	8	231	0.30D+02	0.00D+00
103	8	231	0.25D+02	0.00D+00
104	8	231	0.20D+02	0.00D+00
105	8	231	0.15D+02	0.00D+00
106	8	231	0.10D+02	0.00D+00
107	8	231	0.50D+01	0.00D+00
108	8	231	0.00D+00	0.00D+00
109	8	231	-0.60D+01	0.00D+00
110	8	231	-0.12D+02	0.00D+00
111	8	231	0.60D+02	0.00D+00
112	8	231	0.45D+02	0.00D+00
113	8	231	0.30D+02	0.00D+00
114	8	231	0.25D+02	0.00D+00
115	8	231	0.20D+02	0.00D+00
116	8	231	0.15D+02	0.00D+00
117	8	231	0.10D+02	0.00D+00
118	8	231	0.50D+01	0.00D+00
119	8	231	0.00D+00	0.00D+00

Table 3 (Continued)

120	8	231	-0.60D+01	0.00D+00
121	8	231	-0.12D+02	0.00D+00
122	8	231	0.60D+02	0.00D+00
123	8	231	0.45D+02	0.00D+00
124	8	231	0.30D+02	0.00D+00
125	8	231	0.25D+02	0.00D+00
126	8	231	0.20D+02	0.00D+00
127	8	231	0.15D+02	0.00D+00
128	8	231	0.10D+02	0.00D+00
129	8	231	0.50D+01	0.00D+00
130	8	231	0.00D+00	0.00D+00
131	8	231	-0.60D+01	0.00D+00
132	8	231	-0.12D+02	0.00D+00
133	8	231	0.60D+02	0.00D+00
134	8	231	0.45D+02	0.00D+00
135	8	231	0.30D+02	0.00D+00
136	8	231	0.25D+02	0.00D+00
137	8	231	0.20D+02	0.00D+00
138	8	231	0.15D+02	0.00D+00
139	8	231	0.10D+02	0.00D+00
140	8	231	0.50D+01	0.00D+00
141	8	231	0.00D+00	0.00D+00
142	8	231	-0.60D+01	0.00D+00
143	8	231	-0.12D+02	0.00D+00
144	8	231	0.60D+02	0.00D+00
145	8	231	0.45D+02	0.00D+00
146	8	231	0.30D+02	0.00D+00
147	8	231	0.25D+02	0.00D+00
148	8	231	0.20D+02	0.00D+00
149	8	231	0.15D+02	0.00D+00
150	8	231	0.10D+02	0.00D+00
151	8	231	0.50D+01	0.00D+00
152	8	231	0.00D+00	0.00D+00
153	8	231	0.60D+01	0.00D+00
154	8	231	-0.12D+02	0.00D+00
155	8	231	0.60D+02	0.00D+00
156	8	231	0.45D+02	0.00D+00
157	8	231	0.30D+02	0.00D+00
158	8	231	0.25D+02	0.00D+00
159	8	231	0.20D+02	0.00D+00
160	8	231	0.15D+02	0.00D+00
161	8	231	0.10D+02	0.00D+00
162	8	231	0.50D+01	0.00D+00
163	8	231	0.00D+00	0.00D+00
164	8	231	0.60D+01	0.00D+00

Table 3 (Continued)

165	8	231	-0.12D+02	0.00D+00
166	8	231	0.60D+02	0.00D+00
167	8	231	0.45D+02	0.00D+00
168	8	231	0.30D+02	0.00D+00
169	8	231	0.25D+02	0.00D+00
170	8	231	0.20D+02	0.00D+00
171	8	231	0.15D+02	0.00D+00
172	8	231	0.10D+02	0.00D+00
173	8	231	0.50D+01	0.00D+00
174	8	231	0.00D+00	0.00D+00
175	8	231	-0.60D+01	0.00D+00
176	8	231	-0.12D+02	0.00D+00
177	8	231	0.60D+02	0.00D+00
178	8	231	0.45D+02	0.00D+00
179	8	231	0.30D+02	0.00D+00
180	8	231	0.25D+02	0.00D+00
181	8	231	0.20D+02	0.00D+00
182	8	231	0.15D+02	0.00D+00
183	8	231	0.10D+02	0.00D+00
184	8	231	0.50D+01	0.00D+00
185	8	231	0.00D+00	0.00D+00
186	8	231	-0.60D+01	0.00D+00
187	8	231	-0.12D+02	0.00D+00
188	8	231	0.60D+02	0.00D+00
189	8	231	0.45D+02	0.00D+00
190	8	231	0.30D+02	0.00D+00
191	8	231	0.25D+02	0.00D+00
192	8	231	0.20D+02	0.00D+00
193	8	231	0.15D+02	0.00D+00
194	8	231	0.10D+02	0.00D+00
195	8	231	0.50D+01	0.00D+00
196	8	231	0.00D+00	0.00D+00
197	8	231	-0.60D+01	0.00D+00
198	8	231	-0.12D+02	0.00D+00
199	8	231	0.60D+02	0.00D+00
200	8	231	0.45D+02	0.00D+00
201	8	231	0.30D+02	0.00D+00
202	8	231	0.25D+02	0.00D+00
203	8	231	0.20D+02	0.00D+00
204	8	231	0.15D+02	0.00D+00
205	8	231	0.10D+02	0.00D+00
206	8	231	0.50D+01	0.00D+00
207	8	231	0.00D+00	0.00D+00
208	8	231	-0.60D+01	0.00D+00
209	8	231	-0.12D+02	0.00D+00

Table 3 (Continued)

210	8	231	0.60D+02	0.00D+00											
211	8	231	0.45D+02	0.00D+00											
212	8	231	0.30D+02	0.00D+00											
213	8	231	0.25D+02	0.00D+00											
214	8	231	0.20D+02	0.00D+00											
215	8	231	0.15D+02	0.00D+00											
216	8	231	0.10D+02	0.00D+00											
217	8	231	0.50D+01	0.00D+00											
218	8	231	0.00D+00	0.00D+00											
219	8	231	-0.60D+01	0.00D+00											
220	8	231	-0.12D+02	0.00D+00											
221	8	231	0.60D+02	0.00D+00											
222	8	231	0.45D+02	0.00D+00											
223	8	231	0.30D+02	0.00D+00											
224	8	231	0.25D+02	0.00D+00											
225	8	231	0.20D+02	0.00D+00											
226	8	231	0.15D+02	0.00D+00											
227	8	231	0.10D+02	0.00D+00											
228	8	231	0.50D+01	0.00D+00											
229	8	231	0.00D+00	0.00D+00											
230	8	231	-0.60D+01	0.00D+00											
231	8	231	-0.12D+02	0.00D+00											
										END OF IC					
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
0	0	164	2	2											
0.000	60.000		1.0038		60.000										
0.000	30.000		1.0038		30.000										
1	2	3	4	5	6	7	8	9	232	233	234	235	236	237	238
239	240	463	464	465	466	467	468	469	470	471	694	695	696	697	698
699	700	701	702	925	926	927	928	929	930	931	932	933	1156	1157	1158
1159	1160	1161	1162	1163	1164	1387	1388	1389	1390	1391	1392	1393	1394	1395	1618
1619	1620	1621	1622	1623	1624	1625	1626	1849	1850	1851	1852	1853	1854	1855	1856
1857	221	222	223	224	225	226	227	228	229	452	453	454	455	456	457
458	459	460	683	684	685	686	687	688	689	690	691	914	915	916	917
918	919	920	921	922	1145	1146	1147	1148	1149	1150	1151	1152	1153	1376	1377
1378	1379	1380	1381	1382	1383	1384	1607	1608	1609	1610	1611	1612	1613	1614	1615
1838	1839	1840	1841	1842	1843	1844	1845	1846	2069	2070	2071	2072	2073	2074	2075
2076	2077	111	112												
1	161	1	1	0											
163	1	1	2	0											
										END OF IDTYP					
END OF JOB															

the following statements in BLOCK DATA to specify the maximum-control integers:

```
DATA MAXEL,MAXNP,MAXBES,MAXBNP,JBAND/1600,2079,880,882,27/
DATA MAXNTI,MXNDTC/1,1/
DATA LTMXNP,LMXNP,LMXBW,MXREGN/693,231,25,9/
DATA MXSEL,MXSPR,MXSDP,MXWNP,MXWPR,MXWDP/1,1,1,1,1,1/
DATA MXCNP,MXCES,MXCPR,MXCDP/1,1,1,1/
DATA MXNNP,MXNES,MXNPR,MXNDP/1,1,1,1/
DATA MXVES,MXVNP,MXVPR,MXVDP/1,1,1,1/
DATA MXDNP,MXDPR,MXDDP/165,2,2/
DATA MAXMAT,MXSPPM,MXMPPM/1,5,6/
```

To reflect the soil property function given by Eqs. (117) and (118), we have to modify the subroutine SPROP given in Appendix A. Lines between SPRO 405 and SPRO 535 in the subroutine SPROP must be modified according to

```
WCR=THPROP(1,MTYP)
WCS=THPROP(2,MTYP)
HAA=THPROP(3,MTYP)
ALPHA=THPROP(4,MTYP)
BETA=THPROP(5,MTYP)
DO 800 KG=1,8
HNP=HKG(KG)
HNP=-HNP
C
C ----- SATURATED CONDITION
C
IF(HNP.GT.0) GO TO 700
TH(KG,M)=WCS
AKR(KG,M)=1.000
DTH(KG,M)=0.000
GO TO 800
C
C ----- UNSATURATED CASE
C
```

```

700 THMKG=WCS+(WCS-WCR)/(1.0D0+(ALPHA*DABS(-HNP-HAA))**BETA)
   TH(KG,M)=THMKG
   AKR(KG,M)-((THMKG-WCR)/(WCS-WCR))**2
   DNOM=1.0D0+(ALPHA*DABS(-HNP-HAA))**BETA
   DTH(KG,M)=(WCS-WCR)*(ALPHA*DABS(-HNP-THAA))**(BETA-1.0D0)/DNOM**2

```

The pressure head simulated with 3DFEMWATER is plotted in Figs. 13(a) and 13(b), respectively, for longitudinal and transverse sections through the pumping well. Numerical predictions of these pressure heads are in good agreement with those given by Huyakorn (1986). This verifies the three-dimensional algorithm of 3DFEMWATER. There are some differences between the two model predictions around the pumping well, which are probably due to different boundary conditions imposed on the pumping well. Because it is not clear what boundary conditions were imposed on the pumping well by Huyakorn, we have imposed a constant total head on the three nodes in the pumping well.

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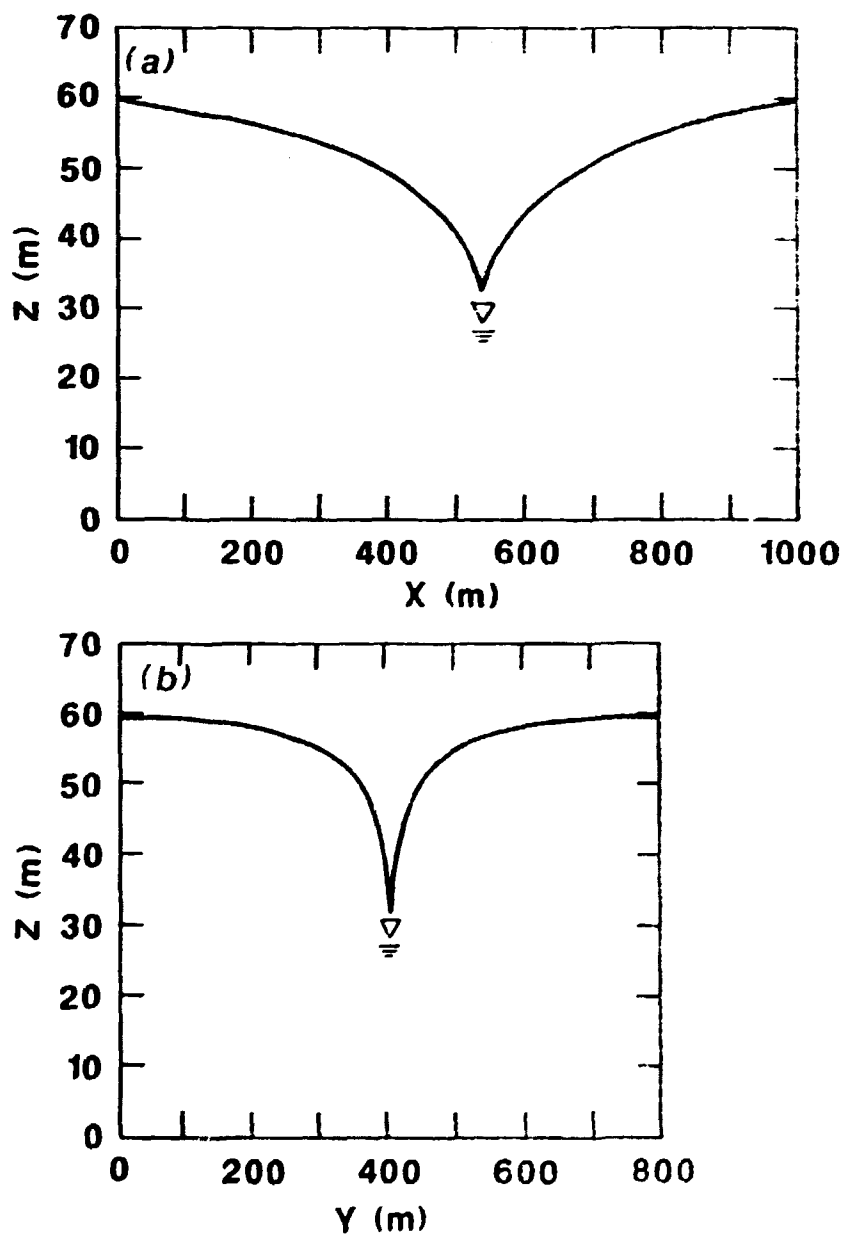


Fig. 13. Simulated steady state profiles of water table over (a) longitudinal and (b) transverse cross-sections through the well for the three-dimensional pumping problem.

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APPENDIX A

**Listing of FORTRAN Source Program of 3DFEMWATER
Code BLI (Block Iteration Version)**

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C *                                     * COM 005
C * *****                          * COM 010
C * *                                  * * COM 015
C * *                                  * * COM 020
C * *          3DFEMWATER              * * COM 025
C * *          WITH BLOCK ITERATION METHOD * * COM 030
C * *                                  * * COM 035
C * *****                          * COM 040
C *                                     * COM 045
C *                                     * COM 050
C * THIS COMPUTER CODE IS CONTAINED IN THE FOLLOWING REPORT: * COM 055
C * YEH, G. T., 1987. "3DFEMWATER: A THREE-DIMENSIONAL FINITE ELEMENT * COM 060
C * MODEL OF WATER FLOW THROUGH SATURATED-UNSATURATED MEDIA" * COM 065
C * ORNL-6386, OAK RIDGE NATIONAL LABORATORY, OAK RIDGE, TN 37831 * COM 070
C *                                     * COM 075
C * FOR ANY QUESTION, PLEASE CONTACT G. T. YEH AT (615) 574-7285 * COM 080
C *                                     * COM 085
C *                                     * COM 090
C *****                          * COM 095
C * *                                  * COM 100
C * DEFINITION OF VARIABLES *          * COM 105
C * *                                  * COM 110
C *****                          * COM 115
C *                                     * COM 120
C * MAXEL - MAXIMUM NO. OF ELEMENTS      * COM 125
C * MAXNP - MAXIMUM NO. OF NODES         * COM 130
C * MAXBES - MAXIMUM NO. OF BOUNDARY ELEMENT-SIDES * COM 135
C * MAXBNP - MAXIMUM NO. OF BOUNDARY NODAL POINTS * COM 140
C * JBAND - MAXIMUM NO. OF NON-ZERO ELEMENTS IN ANY ROW OF THE MATRIX * COM 145
C * MAXNTI - MAXIMUM NO. OF TIME STEPS   * COM 150
C * MXNDTC - MAXIMUM NO. OF DELT CHANGES * COM 155
C *                                     * COM 160
C *                                     * COM 165
C * NNP - NO. OF NODAL POINTS           * COM 170
C * NEL - NO. OF ELEMENTS               * COM 175
C * NBNP - NO. OF BOUNDARY NODE POINTS   * COM 180
C * NBES - NO. OF BOUNDARY ELEMENT-SIDES * COM 185
C * KGRAV - GRAVITY TERM CONTROL, 0 - NOT INCLUDED, 1 - INCLUDED * COM 190
C * NTI - NO. OF TIME INCREMENTS        * COM 195
C * NDTCHG - NO. OF DELT CHANGES       * COM 200
C *                                     * COM 205
C * NCYL - NO. OF CYCLES FOR ITERATING RAINFALL-SEEPAGE * COM 210
C * NITER - NO. OF ITERATIONS ALLOWED FOR SOLVING NONLINEAR EQATIONS * COM 215
C * KSTR - STORE CONTROL INTEGER        * COM 220
C * KPRO - LINE-PRINTING CONTROL FOR INITIAL TIME * COM 225
C * KDSKO - DISK STORE CONTROL INTEGER   * COM 230

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C * KSS	- STEADY STATE SOLUTION CONTROL	* COM 235
C *	0 - STEADY STATE SOLUTION IS WANTED EITHER AS FINAL	* COM 240
C *	SOLUTION OR AS INITIAL CONDIITION OF TRANSIENT STATE	* COM 245
C *	SOLUTION	* COM 250
C *	1 - ONLY TRANSIENT SOLUTION IS NEEDED	* COM 255
C * KCP	- SOIL PERMEABILITY INPUT CONTROL	* COM 260
C *	0 - INPUT SATURATED HYDRAULIC CONDUCTIVITY TO ARRAY PROP	* COM 265
C *	1 - INPUT SATURATED PERMEABILITY TO ARRAY PROP	* COM 270
C *		* COM 275
C * DELT	- TIME STEP SIZE	* COM 280
C * CHNG	- PERCENTAGE CHANGE OF TIME STEP SIZE	* COM 285
C * DELMAX	- MAXIMUM TIME STEP SIZE ALLOWED	* COM 290
C * TMAX	- MAXIMUM SIMULATION TIME ALLOWED	* COM 295
C * DELTO	- INITIAL TIME STEP SIZE	* COM 300
C * TOLA	- TOTLERANCE FOR ITERATING STEADY STATE SOLUTION	* COM 305
C * TOLB	- TOLERANCE FOR ITERATING TRANSIENT SOLUTION OF PRESSURE	* COM 310
C * W	- TIME INTEGRATION PARAMETERS	* COM 315
C *	0.5 - CRANK-NICOLSON CENTRAL DIFFERENCE	* COM 320
C *	1.0 - BACKWARD DIFFERENCE (COMPLETE IMPLICIT SCHEME)	* COM 325
C * OME	- ITERATION PARAMETER FOR SOLVING NONLINEAR EQUATION	* COM 330
C * OMI	- ITERATION PARAMETER FOR SOLVING THE LINEARIZED MATRIX	* COM 335
C *	0.0 TO 1.0 - UNDER RELAXATION	* COM 340
C *	1.0 TO 2.0 - OVER-RELAXATION	* COM 345
C * TIME	- TIME SINCE THE BEGINNING	* COM 350
C *		* COM 355
C *		* COM 360
C * MXSEL	- MAXIMUM NO. OF SOURCE ELEMENTS	* COM 365
C * NSEL	- NO. OF SOURCE ELEMENTS	* COM 370
C * MXSPR	- MAXIMUM NO. OF SOURCE PROFILES	* COM 375
C * MXSDP	- MAXIMUM NO. OF DATA POINTS ON EACH SOURCE PROFILE	* COM 380
C * NSPR	- NO. OF SOURCE PROFILE	* COM 385
C * NSDP	- NO. OF DATA POINTS ON EACH OF THE SOURCE PROFILES	* COM 390
C * MXWNP	- MAXIMUM NO. OF WELL NODAL POINTS	* COM 395
C * NWNP	- NO. OF WELL NODAL POINTS	* COM 400
C * MXWPR	- MAXIMUM NO. OF WELL SOURCE PROFILES	* COM 405
C * MXWDP	- MAXIMUM NO. OF DATA POINT IN EACH WELL SOURCE PROFILE	* COM 410
C * NWPR	- NO. OF WELL SOURCE/SINK PROFILES	* COM 415
C * NWDP	- NO. OF DATA POINTS IN EACH OF ALL SOURCE/SINK PROFILES	* COM 420
C *		* COM 425
C * MXCNP	- MAXIMUM NO. OF CAUCHY NODAL POINTS	* COM 430
C * MXCES	- MAXIMUM NO. OF CAUCHY ELEMENT SIDES	* COM 435
C * MXCPR	- MAXIMUM NO. OF CAUCHY FLUX PROFILES	* COM 440
C * MXCDP	- MAXIMUM NO. OF CAUCHY DATA POINTS ON EACH PROFILE	* COM 445
C * NCNP	- NO. OF CAUCHY NODAL POINTS	* COM 450
C * NCES	- NO. OF CAUCHY ELEMENT SIDES	* COM 455
C * NCPR	- NO. OF CAUCY FLUX PROFILES	* COM 460
C * NCDP	- NO. OF CAUCY FLUX DATA POINTS ON EACH PROFILE	* COM 465
C *		* COM 470

C *	MXNNP	- MAXIMUM NO. OF NEUMANN NODAL POINTS	* COM	475
C *	MXNES	- MAXIMUM NO. OF NEUMANN ELEMENT SIDES	* COM	480
C *	MXNPR	- MAXIMUM NO. OF NEUMANN-FLUX PROFILES	* COM	485
C *	MXNDP	- MAXIMUM NO. OF NEUMANN-FLUX DATA POINTS ON EACH PROFILE	* COM	490
C *	NNNP	- NO. OF NEUMANN NODAL POINTS	* COM	495
C *	NNES	- NO. OF NEUMANN ELEMENT SIDES	* COM	500
C *	NNPR	- NO. OF NEUMANN-FLUX PROFILES	* COM	505
C *	NNDP	- NO. OF NEUMANN-FLUX DATA POINTS ON EACH PROFILE	* COM	510
C *			* COM	515
C *			* COM	520
C *	MXVES	- MAXIMUM NO. OF VARIABLE ELEMENT SIDES	* COM	525
C *	MXVNP	- MAXIMUM NO. OF VARIABLE NODAL POINTS	* COM	530
C *	MXRPR	- MAXIMUM NO. OF RAINFALL PROFILES	* COM	535
C *	MXRDP	- MAXIMUM NO. OF DATA POINT ON EACH RAINFALL PROFILE	* COM	540
C *	NVES	- NO. OF VARIABLE ELEMENT SIDES	* COM	545
C *	NVNP	- NO. OF VARIABLE NODAL POINTS	* COM	550
C *	NRPR	- NO. OF RAINFALL PROFILES	* COM	555
C *	NRDP	- NO. OF DATA POINTS ON EACH RAINFALL PROFILE	* COM	560
C *			* COM	565
C *	MXDNP	- MAXIMUM NO. OF DIRICHLET NODAL POINTS	* COM	570
C *	MXDPR	- MAXIMUM NO. OF DIRICHLET TOTAL HEAD PROFILES	* COM	575
C *	MXDDP	- MAXIMUM NO. OF DATA POINTS ON EACH DIRICHLET PROFILE	* COM	580
C *	NDNP	- NO. OF DIRICHLET NODAL POINTS	* COM	585
C *	NDPR	- NO. OF DIRICHLET TOTAL HEAD PROFILES	* COM	590
C *	NDDP	- NO. OF DIRICHLET DATA POINTS ON EACH DIRICHLET PROFILE	* COM	595
C *			* COM	600
C *	MAXMAT	- MAXIMUM NO. OF MATERIAL TYPES (MEDIUM FORMATIONS)	* COM	605
C *	MXSPPM	- MAXIMUM NO. OF SOIL PARAMETERS PER MATERIAL TO DESCRIBE	* COM	610
C *		SOIL CHARACTERISTIC CURVES.	* COM	615
C *	MXMPPM	- MAXIMUM NO. OF MATERIAL PROPERTIES PER MATERIAL	* COM	620
C *			* COM	625
C *	NMAT	- NO. OF MATERIAL TYPES THAT FORM THE REGION OF INTEREST	* COM	630
C *	NSPPM	- NO. OF SOIL PARAMETERS PER MATERIAL	* COM	635
C *	FRATE(I)	- FLOW RATE THROUGH I-TH TYPE BOUNDARY SEGMENT	* COM	640
C *		I - 1 - DIRICHLET BOUNDARY	* COM	645
C *		I - 2 - NEUMANN BOUNDARY	* COM	650
C *		I - 3 - CAUCHY BOUNDARY	* COM	655
C *		I - 4 - SEEPAGE BOUNDARY	* COM	660
C *		I - 5 - INFILTRATION BOUNDARY	* COM	665
C *		I - 6 - NUMERICAL LOSSES	* COM	670
C *		I - 7 - ENTIRE BOUNDARY	* COM	675
C *		I - 8 - ARTIFICIAL SOURCE INTO THE REGION	* COM	680
C *		I - 9 - INCREASE IN THE WHOLE REGION OF INTEREST	* COM	685
C *	FLOW(I)	- AMOUNT OF FLOW THROUGH I-TH TYPE BOUNDARY IN THE STEP	* COM	690
C *	TFLOW(I)	- ACCUMULATED AMOUNT OF FLOW THROUGH I-TH TYPE BOUNDARY	* COM	695
C *		NOTE: POSITIVE VALUES MEAN OUT FROM THE REGION, NEGATIVE VALUES	* COM	700
C *		MEAN INTO THE REGION.	* COM	705
C *			* COM	710


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C * X(N) - X-COORDINATE OF N-TH NODAL POINT, (L): X(MAXNP) * COM 715
C * Y(N) - Y-COORDINATE OF N-TH NODAL POINT, (L): Y(MAXNP) * COM 720
C * Z(N) - Z-COORDINATE OF N-TH NODAL POINT, (L): X(MAXNP) * COM 725
C * IE(M,I) - GLOBAL NODE NUMBER OF THE I-TH NODE OF M-TH ELEMENT IF * COM 730
C * I IS BETWEEN 1 AND 8 * COM 735
C * IE(M,9) - INTEGER TO INDICATE THE MATERIAL TYPE OF M-TH ELEMENT * COM 740
C * NOTE: IE IS DIMENSIONED IE(MAXEL,9) * COM 745
C * * COM 750
C * CMATRIX(N,I) - AN ARRAY TO STORE THE ASSEMBLED GLOBLE MATRIX * COM 755
C * SHOULD BE DIMENSIONED AS C(MAXNP,JBAND) * COM 760
C * GNOJCN(I,N) - GLOBAL NODE NUMBER OF THE I-TH CONNECTING NODE * COM 765
C * SURROUNDING THE N-TH GLOBAL NODE. THIS ARRAY IS * COM 770
C * GENERATED BASED ON THE INPUT ARRAY IE. * COM 775
C * RLD(N) - AN ARRAY TO STORE THE ASSEMBLED LOAD VECTOR * COM 780
C * SHOULD BE DIMENSIONED AS RLD(MAXNP) * COM 785
C * RI(N) - PRESSURE HEAD ITERATE IN SUBROUTINE BLKTR * COM 790
C * RL(N) - A WORKING ARRAY TO CONTAIN FINAL SOLUTION FOR THE PRES- * COM 795
C * SURE HEAD IN SUBROUTINE BLKTR * COM 800
C * NTNPLR(K) - TOTAL NUMBER OF NODES FOR K-TH SUBREGION INCLUDING * COM 805
C * INTERIOR & GLOBAL BOUNDARY AND INTRA-BOUNDARY NODES * COM 810
C * THIS ARRAY IS GENERATED BASED ON THE INPUT ARRAYS IE * COM 815
C * AND GNLR(I,K) FOR I=1,2,...,NNPLR(K). * COM 820
C * NNPLR(K) - NUMBER OF INTERIOR NODES FOR K-TH SUBREGION, INCLUDING * COM 825
C * GLOBAL BOUNDARY NODES. INPUT. * COM 830
C * GNLR(I,K) - GLOBAL NODAL NUMBER OF I-TH LOCAL NODAL NUMBER FOR * COM 835
C * K-TH SUBREGION. THIS ARRAY IS AN INPUT FOR I=1,2,..., * COM 840
C * NNPLR(K). BUT IT IS GENERATED BASED ON IE(NEL,8) AND * COM 845
C * GNLR(I,K) WITH I=1,2,...,NNPLR(K) FOR I=NNPLR(K)+1 TO * COM 850
C * NTNPLR(K). * COM 855
C * LNOJCN(J,I,K) - LOCAL NODE NUMBER OF J-TH CONNECTING NODE SUR- * COM 860
C * ROUNDING I-TH LOCAL NODE FOR K-TH SUBREGION. * COM 865
C * THIS ARRAY IS GENERATED BASED ON IE AND GNLR. * COM 870
C * LMAXDF(K) - MAXIMUM DIFFERENCE BETWEEN ANY TWO NODES OF AN * COM 875
C * ELEMENT IN K-TH SUBREGION. THIS ARRAY IS GENERATED * COM 880
C * FROM LNOJCN * COM 885
C * CMTRXL(N,I) - ASSEMBLED MATRIX FOR A SUBREGION * COM 890
C * RLDL(N) - ASSEMBLED LOAD VECTOR FOR A SUBREGION * COM 895
C * * COM 900
C * H(N) - PRESSURE HEAD AT N-TH NODE, (L): H(MAXNP) * COM 905
C * HP(N) - PRESSURE HEAD OF N-TH NODE AT PREVIOUS TIME * COM 910
C * HW(N) - NONLINEAR PRESSURE HEAD ITERATE OF N-TH NODE * COM 915
C * HT(N) - TOTAL HEAD OF N-TH NODE * COM 920
C * VX(N) - X-COMPONENT VELOCITY AT N-TH NODE * COM 925
C * VY(N) - Y-COMPONENT VELOCITY AT N-TH NODE * COM 930
C * VZ(N) - Z-COMPONENT VELOCITY AT N-TH NODE * COM 935
C * NPCNV(N) - NODAL POINT OF N-TH NONCONVERGENT NODE * COM 940
C * TH(I,M) - MOISTURE CONTENT AT I-TH GAUSSIAN POINT OF M-TH * COM 945
C * ELEMENT * COM 950

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C * DTH(I,M) - DTH/DH - WATER CAPACITY OF I-TH GAUSSIAN POINT OF M- * COM 955
 C * TH ELEMENT * COM 960
 C * AKR(I,M) - RELATIVE HYDRAULIC CONDUCTIVITY AT I-TH GAUSSIAN * COM 965
 C * POINT OF M-TH ELEMENT * COM 970
 C * DCOSB(1,I) - X-DIRECTIONAL COSINE OF I-TH BOUNDARY ELEMENT SIDE * COM 975
 C * DCOSB(2,I) - Y-DIRECTIONAL COSINE OF I-TH BOUNDARY ELEMENT SIDE * COM 980
 C * DCOSB(3,I) - Z-DIRECTIONAL COSINE OF I-TH BOUNDARY ELEMENT SIDE * COM 985
 C * NOTE: DCOSB SHOULD BE DIMENSIONED AS DCOSB(3,MAXBES). * COM 990
 C * ISB(1,I) - BOUNDARY NODE NUMBER OF THE FIRST NODE OF I-TH * COM 995
 C * BOUNDARY ELEMENT SIDE * COM 1000
 C * ISB(2,I) - BOUNDARY NODE NUMBER OF THE SECOND NODE OF I-TH * COM 1005
 C * BOUNDARY ELEMENT SIDE * COM 1010
 C * ISB(3,I) - BOUNDARY NODE NUMBER OF THE THIRD NODE OF I-TH * COM 1015
 C * BOUNDARY ELEMENT SIDE * COM 1020
 C * ISB(4,I) - BOUNDARY NODE NUMBER OF THE FOURTH NODE OF I-TH * COM 1025
 C * BOUNDARY ELEMENT SIDE * COM 1030
 C * ISB(5,I) - ELEMENT SIDE INDEX OF I-TH BOUNDARY ELEMENT SIDE * COM 1035
 C * -1 - LEFT SIDE, -2 - FRONT SIDE, -3 -RIGHT SIDE * COM 1040
 C * -4 - BACK SIDE, -5 - BOTTOM SIDE, -6 - TOP SIDE * COM 1045
 C * ISB(6,I) - ELEMENT NUMBER TO WHICH THE I-TH BOUNDARY ELEMENT-SIDE * COM 1050
 C * BELONG * COM 1055
 C * NPBB(I) - GLOBAL NODE NUMBER OF I-TH BOUNDARY NODE * COM 1060
 C * BFLX(I) - BOUNDARY FLUX AT I-TH BOUNDARY NODE, (L**3/T) * COM 1065
 C * SHOULD BE DIMENSIONED AS BFLX(MAXBNP) * COM 1070
 C * BFLXP(I) - BOUNDARY FLUX AT PREVIOUS TIME OF I-TH BOUNDARY NODE * COM 1075
 C * SOULD BE DIMENSIONED AS BFLXP(MAXBNP) * COM 1080
 C * * COM 1085
 C * * COM 1090
 C * * COM 1095
 C * SOS(I) - SOURCE STRENGTH OF I-TH SOURCE PROFILE, * COM 1100
 C * ((L**3/T)/L**3): SOS(MXSPR). * COM 1105
 C * SOSF(I,J) - SOURCE STRENGTH OF I-TH DATA POINT IN J-TH ELEMENT * COM 1110
 C * SOURCE VS TIME PROFILE, ((L**3/T)/L**) * COM 1115
 C * TSOSF(I,J) - TIME OF I-TH DATA POINT IN J-TH SOURCE VS TIME * COM 1120
 C * PROFILE, (T) * COM 1125
 C * MS2L(I) - ELEMENT NUMBER OF I-TH SOURCE/SINK ELEMENT * COM 1130
 C * ISTYP(I) - SOURCE TYPE ASSIGNED TO I-TH SOURCE/SINK ELEMENT * COM 1135
 C * WSS(I) - VALUE OF I-TH WELL SOURCE/SINK AT PRESENT TIME, (L**3/T) * COM 1140
 C * WSSF(I,J) - WELL SOURCE/SINK FUNCTION OF I-TH DATA POINT OF J-TH * COM 1145
 C * PROFILE, (L**3/T) * COM 1150
 C * TWSSF(I,J) - TIME OF I-TH DATA POINT OF J-TH PROFILE * COM 1155
 C * NPW(I) - GLOBAL NODE NUMBER OF I-TH WELL SOURCE/SINK POINT * COM 1160
 C * IWTP(I) - TYPE OF WELL SOURCE/SINK ASSIGNED TO I-TH SOURCE/SINK * COM 1165
 C * POINT * COM 1170
 C * * COM 1175
 C * * COM 1180

C * QCB(I) - VALUE OF CAUCHY FLUX AT THE PRESENT TIME OF I-TH CAUCHY * COM 1185
 C * FLUX VS TIME PROFILE, (L**3/T/L**2) * COM 1190
 C * QCBF(I,J) - FLUX OF I-TH DATA POINT IN J-TH CAUCHY FLUX VS TIME * COM 1195
 C * TIEM PROFILE, (L**3/T/L**2) * COM 1200
 C * TQCBF(I,J) - TIME OF I-TH DATA POINT IN J-TH CAUCHY FLUX VS TIME * COM 1205
 C * PROFILE * COM 1210
 C * ICTYP(MP) - TYPE OF CAUCHY FLUX VS TIME PROFILE ASSIGNED TO MP-TH * COM 1215
 C * CAUCHY SIDE * COM 1220
 C * NPCB(NP) - GLOBAL NODE NUMBER OF NP-TH CAUCHY NODE FOR INPUTTING, * COM 1225
 C * THEN IS CHANGED TO CONTAIN BOUNDARY NODE NUMBER * COM 1230
 C * ISC(1,I) - GLOBAL NODE NUMBER OF THE FIRST NODE OF I-TH CAUCHY * COM 1235
 C * SIDE * COM 1240
 C * ISC(2,I) - GLOBAL NODE NUMBER OF THE SECOND NODE OF I-TH CAUCHY * COM 1245
 C * SIDE. * COM 1250
 C * ISC(3,I) - GLOBAL NODE NUMBER OF THE THIRD NODE OF I-TH CAUCHY * COM 1255
 C * SIDE * COM 1260
 C * ISC(4,I) - GLOBAL NODE NUMBER OF THE FOURTH NODE OF I-TH CAUCHY * COM 1265
 C * SIDE * COM 1270
 C * ISC(5,I) - BOUNDARY SIDE NUMBER OF I-TH CAUCHY SIDE * COM 1275
 C * * COM 1280
 C * * COM 1285
 C * QNB(I) - VALUE OF FLUX AT THE PRESENT TIME OF I-TH NEUMANN FLUX VS * COM 1290
 C * TIME PROFILE FOR NEUMANN BOUNDARY, ((L**3/T)/L**2) * COM 1295
 C * QNB(MXNPR) * COM 1300
 C * QNBF(I,J) - FLUX OF I-TH DATA POINT IN J-TH NEUMANN FLUX VS TIME * COM 1305
 C * PROFILE, ((L**3/T)/L**2) * COM 1310
 C * TQnbf(1,J) - TIME OF I-TH DATA POINT IN J-TH NEUMANN FLUX VS TIME * COM 1315
 C * PROFILE FOR NEUMANN BOUNDARY, (T) * COM 1320
 C * INTYP(MP) - TYPE OF NEUMANN FLUX VS TIME PROFILE TO BE ASSIGNED TO * COM 1325
 C * MP-TH NEUMANN SIDE: INTYP(MXNPR) * COM 1330
 C * NPNB(NP) - GLOBAL NODE NUMBER OF NP-TH NEUMANN NODE FOR INPUTTING * COM 1335
 C * THEN IS CHANGED TO CONTAIN BOUNDARY NODE NUMBER * COM 1340
 C * ISN(1,I) - GLOBAL NODE NUMBER OF THE FIRST NODE OF I-TH NEUMANN * COM 1345
 C * SIDE * COM 1350
 C * ISN(2,I) - GLOBAL NODE NUMBER OF THE SECOND NODE OF I-TH NEUMANN * COM 1355
 C * SIDE * COM 1360
 C * ISN(3,I) - GLOBAL NODE NUMBER OF THE THIRD NODE OF I-TH NEUMANN * COM 1365
 C * SIDE * COM 1370
 C * ISN(4,I) - GLOBAL NODE NUMBER OF THE FOURTH NODE OF I-TH NEUMANN * COM 1375
 C * SIDE * COM 1380
 C * ISN(5,I) - BOUNDARY SIDE NUMBER OF I-TH NEUMANN SIDE * COM 1385
 C * * COM 1390
 C * RFALL(I) - VALUE OF RAINFALL AT THE PRESENT TIME OF I-TH RAIN- * COM 1395
 C * FALL VIS TIME PROFILE, (L/T) * COM 1400
 C * TRF(I,J) - TIME OF I-TH DATA POINT ON J-TH RAINFALL VS TIME * COM 1405
 C * PROFILE * COM 1410
 C * RF(I,J) - RAINFALL VALUE OF I-TH DATA POINT ON J-TH RAINFALL VS * COM 1415
 C * TIME PROFILE, (L/T) * COM 1420
 C * IRTYP(MP) - TYPE OF RAINFALL PROFILE ASSEIGNED TO MP-TH VARIABLE * COM 1425
 C * BOUNDARY SIDE * COM 1430

C * ISV(1,I) - GLOBAL NODE NUMBER OF THE FIRST NODE OF I-TH VB SIDE * COM 1435
 C * FOR INPUTTING, THEN IS CHANGED TO CONTAIN COMPRESSED * COM 1440
 C * VB NODE NUMBER. * COM 1445
 C * ISV(2,I) - GLOBAL NODE NUMBER OF THE SECOND NODE OF I-TH VB SIDE * COM 1450
 C * FOR INPUTTING, THEN IS CHANGED TO CONTAIN COMPRESSED * COM 1455
 C * VB NODE NUMBER. * COM 1460
 C * ISV(3,I) - GLOBAL NODE NUMBER OF THE THIRD NODE OF I-TH VB SIDE * COM 1465
 C * FOR INPUTTING, THEN IS CHANGED TO CONTAIN COMPRESSED * COM 1470
 C * VB NODE NUMBER. * COM 1475
 C * ISV(4,I) - GLOBAL NODE NUMBER OF THE FOURTH NODE OF I-TH VB SIDE * COM 1480
 C * FOR INPUTTING, THEN IS CHANGED TO CONTAIN COMPRESSED * COM 1485
 C * VB NODE NUMBER. * COM 1490
 C * ISV(5,I) - BOUNDARY SIDE NUMBER OF I-TH RS SIDE, BETWEEN 1 & NBES * COM 1495
 C * NOTE: "ISV" SHOULD BE DIMENSIONED AS ISV(5,MXVES) * COM 1500
 C * * COM 1505
 C * NPVB(NP) - GLOBAL NODE NUMBER OF NP-TH VB NODE FOR INPUTTING, * COM 1510
 C * THEN IS CHANGED TO CONTAIN BOUNDARY NODE NUMBER. * COM 1515
 C * * COM 1520
 C * DCYFLX(NP) - DARCY FLUX THROUGH NP-TH RAINFALL-SEEPAGE NODE * COM 1525
 C * (L**3/T) * COM 1530
 C * FLX(NP) - RAINFALL RATE THROUGH NP-TH RAINFALL-SEEPAGE NODE * COM 1535
 C * (L**3/T) * COM 1540
 C * HCON(NP) - PONDING DEPTH ALLOWED FOR THE NP-TH NODE OF RAINFALL/ * COM 1545
 C * EVAPORATION SEEPAGE NODES, (L): HCON(MXRSNP) * COM 1550
 C * HMIN(NP) - MINIMUM PRESSURE HEAD ALLOWED FOR THE NP-TH RAINFALL/ * COM 1555
 C * EVAPORATION SEEPAGE NODES, (L): HMIN(MXVNP) * COM 1560
 C * NPFLX(NP) - CAUCHY BOUNDARY CONDITION INDICATOR FOR THE NP-TH * COM 1565
 C * NODE OF RAINFALL(+)/EVAPORATION(-)-SEEPAGE NODE, 0 - * COM 1570
 C * THIS NP-TH RS NODE IS NOT A CAUCHY NODE FOR THE * COM 1575
 C * TIME STEP, GLOBAL NODE NUMBER OF NP-TH RS NODE - THIS * COM 1580
 C * NP-TH RS NODE IS A CAUCHY NODE * COM 1585
 C * * COM 1590
 C * NPCON(NP) - PONDING DEPTH DIRICHLET BOUNDARY CONDITION INDICATOR * COM 1595
 C * FOR THE NP-TH RS NODE, 0 - THIS NP-TH NODE IS NOT A * COM 1600
 C * PONDING DEPTH DIRICHLET NODE, GLOBAL NODE NUMBER OF * COM 1605
 C * NP-TH RS NODE - THIS NP-TH RS NODE IS A PONDING DEPTH * COM 1610
 C * DIRICHLET NODE * COM 1615
 C * * COM 1620
 C * NPMIN(NP) - MINIMUM PRESSURE HEAD DIRICHLET BOUNDARY CONDITION * COM 1625
 C * INDICATOR FOR THE NP-TH RS NODE, 0 - NP-TH RS NODE IS * COM 1630
 C * NOT A MINIMUM PRESSURE HEAD DIRICHLET NODE, GLOBAL * COM 1635
 C * NODE NUMBER OF NP-TH RS NODE - THIS NP-TH RS NODE IS * COM 1640
 C * PRESCRIBED MINIMUM PRESSURE HEAD DIRICHLET NODE * COM 1645
 C * * COM 1650
 C * * COM 1655

C		MAIN 005
C	----- MAIN PROGRAM OF 3DFEMWATER - BLOCK ITERATION METHOD.	MAIN 010
C		MAIN 015
	IMPLICIT REAL*8(A-H,O-Z)	MAIN 020
	INTEGER*4 GNLR,GNOJCN	MAIN 025
C		MAIN 030
	COMMON /SGEOM/ MAXEL,MAXNP,MAXBES,MAXBNP,JBAND,MAXNTI,MXNDTC	MAIN 035
	COMMON /CGEOM/ NNP,NEL,NBNP,NBES,KGRAV,NTI,NDTCHG	MAIN 040
	COMMON /LGEOM/ LTMXNP,LMXNP,LMXBW,MXREGN,NREGN	MAIN 045
	COMMON /CINTE/ NCYL,NITER,KSTR,KPRO,KDSKO,KSS,NPITER,IGEOM	MAIN 050
	COMMON /CREAL/ DELT,CHNG,DELMAX,TMAX,DELTO,TOLA,TOLB,W,OME,OMI	MAIN 055
C		MAIN 060
	COMMON /CS/ MXSEL,MXSPR,MXSDP,NSEL,NSPR,NSDP	MAIN 065
	COMMON /CW/ MXWNP,MXWPR,MXWDP,NWNP,NWPR,NWDP	MAIN 070
C		MAIN 075
	COMMON /CCBC/ MXCNP,MXCES,MXCPR,MXCDP,NCNP,NCES,NCPR,NCDP	MAIN 080
	COMMON /CNBC/ MXNNP,MXNES,MXNPR,MXNDP,NNNP,NNES,NNPR,NNDP	MAIN 085
	COMMON /CVBC/ MXVES,MXVNP,MXRPR,MXRDV,NVES,NVNP,NRPR,NRDP	MAIN 090
	COMMON /CDBC/ MXDNP,MXDPR,MXDDP,NDNP,NDPR,NDDP	MAIN 095
C		MAIN 100
	COMMON /SMTL/ MAXMAT,MXSPPM,MXMPPM	MAIN 105
	COMMON /CMTL/ NMAT,NMPPM,NSPPM	MAIN 110
C		MAIN 115
	COMMON /CFLOW/ FRATE(10),FLOW(10),TFLOW(10)	MAIN 120
C		MAIN 125
	DIMENSION X(6000),Y(6000),Z(6000),IE(4959,9)	MAIN 130
	DIMENSION CMATRX(6000,27),GNOJCN(27,6000),RLD(6000)	MAIN 135
	DIMENSION RI(6000),RL(6000)	MAIN 140
	DIMENSION NTNPLR(20),NNPLR(20),LMAXDF(20)	MAIN 145
	DIMENSION GNLR(900,20),LNOJCN(27,300,20)	MAIN 150
	DIMENSION CMTRXL(300,23),RLDL(300)	MAIN 155
	DIMENSION H(6000),HP(6000),HW(6000),HT(6000)	MAIN 160
	DIMENSION VX(6000),VY(6000),VZ(6000)	MAIN 165
	DIMENSION TH(8,4959),DTH(8,4959),AKR(8,4959),NPCNV(6000)	MAIN 170
C		MAIN 175
	DIMENSION DCOSB(3,1966),ISB(6,1966),NPBB(1968)	MAIN 180
	DIMENSION BFLX(1968),BFLXP(1968)	MAIN 185
C		MAIN 190
	DIMENSION SOS(3),SOSF(4,3),TSOSF(4,3)	MAIN 195
	DIMENSION ISTYP(11),MSEL(11)	MAIN 200
	DIMENSION WSS(5),WSSF(8,5),TWSSF(8,5)	MAIN 205
	DIMENSION IWTYP(10),NPW(10)	MAIN 210
C		MAIN 215
	DIMENSION QCB(2),QCBF(4,2),TQCBF(4,2)	MAIN 220
	DIMENSION ICTYP(171),ISC(5,171),NPCB(200)	MAIN 225
C		MAIN 230
	DIMENSION QNB(1),QNB(2,1),TQNB(2,1)	MAIN 235
	DIMENSION INTYP(551),ISN(5,551),NPNB(600)	MAIN 240
C		MAIN 245

	DIMENSION RFALL(3),RF(24,3),TRF(24,3)	MAIN 250
	DIMENSION IRTYP(551),ISV(5,551),NPVB(600)	MAIN 255
	DIMENSION DCYFLX(600),FLX(600),HCON(600),HMIN(600)	MAIN 260
	DIMENSION NPFLX(600),NPCON(600),NPMIN(600)	MAIN 265
C		MAIN 270
	DIMENSION HDB(20),HDBF(8,20),THDBF(8,20)	MAIN 275
	DIMENSION IDTYP(200),NPDB(200)	MAIN 280
C		MAIN 285
	DIMENSION PROP(6,3)	MAIN 290
	DIMENSION THPROP(4,3),AKPROP(4,3)	MAIN 295
C		MAIN 300
	DIMENSION KPR(500),KDSK(500),TDTCH(20)	MAIN 305
C		MAIN 310
C	----- PASS THE PROGRAM TO GW3D	MAIN 315
C		MAIN 320
	CALL GW3D(X,Y,Z,IE,CMATRX,GNOJCN,RLD,RI,RL,H,HP,HW,HT,	MAIN 325
	1 VX,VY,VZ,TH,DTH,AKR,NPCNV,DCOSB,ISB,NPBB,BFLX,BFLXP,	MAIN 330
	2 SOS,SOSF,TSOSF,ISTYP,MSEL,WSS,WSSF,TWSSF,IWTYP,NPW,	MAIN 335
	3 QCB,QCBF,TQCBF,ICTYP,ISC,NPCB,QNB,QNBF,TQNB,INTYP,ISN,NPNB,	MAIN 340
	4 RFALL,RF,TRF,IRTY,ISV,NPVB,DCYFLX,FLX,HCON,HMIN,	MAIN 345
	5 NPFLX,NPCON,NPMIN,HDB,HDBF,THDBF,IDTYP,NPDB,	MAIN 350
	6 PROP,THPROP,AKPROP,KPR,KDSK,TDTCH,	MAIN 355
	7 NTNPLR,NNPLR,LMAXDF,GNLR,LNOJCN,CMTRXL,RLDL)	MAIN 360
C		MAIN 365
	STOP	MAIN 370
	END	MAIN 375

	BLOCK DATA	BLOC 005
C		BLOC 010
	IMPLICIT REAL*8(A-H,O-Z)	BLOC 015
C		BLOC 020
	COMMON /SGEOM/ MAXEL,MAXNP,MAXBES,MAXBNP,JBAND,MAXNTI,MXNDTC	BLOC 025
	COMMON /LGEOM/ LTMXNP,LMXNP,LMXBW,MXREGN,NREGN	BLOC 030
	COMMON /CS/ MXSEL,MXSPR,MXSDP,NSEL,NSPR,NSDP	BLOC 035
	COMMON /CW/ MXWNP,MXWPR,MXWDP,NWNP,NWPR,NWDP	BLOC 040
	COMMON /CCBC/ MXCNP,MXCES,MXCPR,MXCDP,NCNP,NCES,NCPR,NCDP	BLOC 045
	COMMON /CNBC/ MXNNP,MXNES,MXNPR,MXNDP,NNNP,NNES,NNPR,NNDP	BLOC 050
	COMMON /CVBC/ MXVES,MXVNP,MXVPR,MXVDP,NVES,NVNP,NRPR,NRDP	BLOC 055
	COMMON /CDBC/ MXDNP,MXDPR,MXDDP,NDNP,NDPR,NDDP	BLOC 060
	COMMON /SMTL/ MAXMAT,MXSPPM,MXMPPM	BLOC 065
C		BLOC 070
	DATA MAXEL,MAXNP,MAXBES,MAXBNP,JBAND/4959,6000,1966,1968,27/	BLOC 075
	DATA MAXNTI,MXNDTC/500,20/	BLOC 080
	DATA LTMXNP,LMXNP,LMXBW,MXREGN/900,300,23,20/	BLOC 085

	DATA MXSEL, MXSPR, MXSDP, MXWNP, MXWPR, MXWDP/11, 3, 4, 10, 5, 8/	BLOC 090
	DATA MXCNP, MXCES, MXCPR, MXCDP/200, 171, 2, 4/	BLOC 095
	DATA MXNNP, MXNES, MXNPR, MXNDP/600, 551, 1, 2/	BLOC 100
	DATA MXVES, MXVNP, MXRPR, MXRDP/551, 600, 3, 24/	BLOC 105
	DATA MXDNP, MXDPR, MXDDP/200, 20, 8/	BLOC 110
	DATA MAXMAT, MXSPPM, MXMPPM/3, 4, 6/	BLOC 115
C		BLOC 120
	END	BLOC 125
	SUBROUTINE GW3D(X, Y, Z, IE, CMATRX, GNOJCN, RLD, RI, RL, H, HP, HW, HT,	GW3D 005
	1 VX, VY, VZ, TH, DTH, AKR, NPCNV, DCOSB, ISB, NPBB, BFLX, BFLXP,	GW3D 010
	2 SOS, SOSF, TSOSF, ISTYP, MSEL, WSS, WSSF, TWSSF, IWYP, NPW,	GW3D 015
	3 QCB, QCBF, TQCBF, ICTYP, ISC, NPCB, QNB, QNBF, TQNB, INTYP, ISN, NPNB,	GW3D 020
	4 RFALL, RF, TRF, IRTYP, ISV, NPVB, DCYFLX, FLX, JCON, HMIN,	GW3D 025
	5 NPFLX, NPCON, NPMIN, HDB, HDBF, THDBF, IDTYP, NPDB,	GW3D 030
	6 PROP, THPROP, AKPROP, KPR, KDSK, TDTCH,	GW3D 035
	7 NTNPLR, NNPLR, LMAXDF, GNLR, LNOJCN, CMTRXL, RLDL)	GW3D 040
C		GW3D 045
	IMPLICIT REAL*8(A-H, O-Z)	GW3D 050
	REAL*4 SUBHD	GW3D 055
	INTEGER*4 GNLR, GNOJCN	GW3D 060
C		GW3D 065
	COMMON /SGEOM/ MAXEL, MAXNP, MAXBES, MAXBNP, JBAND, MAXNTI, MXNDTC	GW3D 070
	COMMON /CGEOM/ NNP, NEL, NBNP, NBES, KGRAV, NTI, NDTCHG	GW3D 075
	COMMON /LGEOM/ LTMXNP, LMXNP, LMXBW, MXREGN, NREGN	GW3D 080
	COMMON /CINTE/ NCYL, NITER, KSTR, KPRO, KDSKO, KSS, NPITER, IGEOM	GW3D 085
	COMMON /CREAL/ DELT, CHNG, DELMAX, TMAX, DELTO, TOLA, TOLB, W, OME, OMI	GW3D 090
C		GW3D 095
	COMMON /CS/ MXSEL, MXSPR, MXSDP, NSEL, NSPR, NSDP	GW3D 100
	COMMON /CW/ MXWNP, MXWPR, MXWDP, NWNP, NWPR, NWDP	GW3D 105
C		GW3D 110
	COMMON /CCBC/ MXCNP, MXCES, MXCPR, MXCDP, NCNP, NCES, NCPR, NCDP	GW3D 115
	COMMON /CNBC/ MXNNP, MXNES, MXNPR, MXNDP, NNNP, NNES, NNPR, NNDP	GW3D 120
	COMMON /CVBC/ MXVES, MXVNP, MXRPR, MXRDP, NVES, NVNP, NRPR, NRDP	GW3D 125
	COMMON /CDBC/ MXDNP, MXDPR, MXDDP, NDNP, NDPR, NDDP	GW3D 130
C		GW3D 135
	COMMON /SMTL/ MAXMAT, MXSPPM, MXMPPM	GW3D 140
	COMMON /CMTL/ NMAT, NMPPM, NSPPM	GW3D 145
C		GW3D 150
	COMMON /CFLOW/ FRATE(10), FLOW(10), TFLOW(10)	GW3D 155
C		GW3D 160
	DIMENSION X(MAXNP), Y(MAXNP), Z(MAXNP), IE(MAXEL, 9)	GW3D 165
	DIMENSION CMATRX(MAXNP, JBAND), GNOJCN(JBAND, MAXNP), RLD(MAXNP)	GW3D 170
	DIMENSION RI(MAXNP), RL(MAXNP)	GW3D 175
	DIMENSION NTNPLR(MXREGN), NNPLR(MXREGN), LMAXDF(MXREGN)	GW3D 180
	DIMENSION GNLR(LTMXNP, MXREGN), LNOJCN(JBAND, LMXNP, MXREGN)	GW3D 185
	DIMENSION CMTRXL(LMAXNP, LMXBW), RLDL(LMXNP)	GW3D 190
	DIMENSION H(MAXNP), HP(MAXNP), HW(MAXNP), HT(MAXNP)	GW3D 195

	DIMENSION VX(MAXNP), VY(MAXNP), VZ(MAXNP)	GW3D 200
	DIMENSION TH(8,MAXEL), DTH(8,MAXEL), AKR(8,MAXEL), NPCNV(MAXNP)	GW3D 205
C		GW3D 210
	DIMENSION DCOSB(3,MAXBES), ISB(6,MAXBES), NPBB(MAXBNP)	GW3D 215
	DIMENSION BFLX(MAXBNP), BFLXP(MAXBNP)	GW3D 220
C		GW3D 225
	DIMENSION SOS(MXSPR), SOSF(MXSDP, MXSPR), TSOSF(MXSDP, MXSPR)	GW3D 230
	DIMENSION ISTYP(MXSEL), MSEL(MXSEL)	GW3D 235
	DIMENSION WSS(MXWPR), WSSF(MXWDP, MXWPR), TWSSF(MXWDP, MXWPR)	GW3D 240
	DIMENSION IWTYP(MXWNP), NPW(MXWNP)	GW3D 245
C		GW3D 250
	DIMENSION QCB(MXCPR), QCBF(MXCDP, MXCPR), TQCBF(MXCDP, MXCPR)	GW3D 255
	DIMENSION ICTYP(MXCES), ISC(5, MXCES), NPCB(MXCNP)	GW3D 260
C		GW3D 265
	DIMENSION QNB(MXNPR), QNBF(MXNDP, MXNPR), TQNBF(MXNDP, MXNPR)	GW3D 270
	DIMENSION INTYP(MXNES), ISN(5, MXNES), NPNB(MXNNP)	GW3D 275
C		GW3D 280
	DIMENSION RFALL(MXRPR), RF(MXRDP, MXRPR), TRF(MXRDP, MXRPR)	GW3D 285
	DIMENSION IRTYP(MXVES), ISV(5, MXVES), NPVB(MXVNP)	GW3D 290
	DIMENSION DCYFLX(MXVNP), FLX(MXVNP), HCON(MXVNP), HMIN(MXVNP)	GW3D 295
	DIMENSION NPFLX(MXVNP), NPCON(MXVNP), NPMIN(MXVNP)	GW3D 300
C		GW3D 305
	DIMENSION HDB(MXDPR), HDBF(MXDDP, MXDPR), THDBF(MXDDP, MXDPR)	GW3D 310
	DIMENSION IDTYP(MXDNP), NPDB(MXDNP)	GW3D 315
C		GW3D 320
	DIMENSION PROP(MXMPPM, MAXMAT)	GW3D 325
	DIMENSION THPROP(MXSPPM, MAXMAT), AKPROP(MXSPPM, MAXMAT)	GW3D 330
C		GW3D 335
	DIMENSION KPR(MAXNTI), KDSK(MAXNTI), TDTCH(MXNDTC)	GW3D 340
C		GW3D 345
	DIMENSION TITLE(9)	GW3D 350
	DIMENSION SUBHD(8,3)	GW3D 355
C		GW3D 360
	DATA SUBHD/4HINPU,4HT IN,4HITIA,4HL CO,4HNDIT,4HIONS,2*4H	GW3D 365
	> 4HSTEA,4HDY-S,4HTATE,4H INI,4HTIAL,4H CON,4HDITI,4HONS , 8*	GW3D 370
	> 4H /	GW3D 375
C		GW3D 380
C	***** DATA SET 1: PROBLEM IDENTIFICATION AND DESCRIPTION	GW3D 385
C		GW3D 390
	100 READ 10, NPROB,(TITLE(I),I-1,9),IGEOM,IBUG,ICHNG	GW3D 395
C		GW3D 400
	IF (NPROB.LE.0) GO TO 990	GW3D 405
C		GW3D 410
	PRINT 1000, NPROB,(TITLE(I),I-1,9),IGEOM,IBUG,ICHNG	GW3D 415
C		GW3D 420
C	----- READ AND PRINT INPUT DATA BY CALLING DATAIN	GW3D 425
C		GW3D 430
	KOUT=0	GW3D 435
	TIME=0.0	GW3D 440

C		GW3D 445
C	***** DATA SETS 2 THROUGH 17 WILL BE READ IN DATAIN	GW3D 450
C		GW3D 455
	CALL DATAIN(TITLE,NPROB, KPR,KDSK,TDICH,	GW3D 460
	1 PROP,THPROP,A*PROP, X,Y,Z,IE,H, DCOSE,ISB,NPBB,	GW3D 465
	2 SOSF,TSOSF,ISTYP,MSEL, WSSF,TWSSF,IWTYP,NPW,	GW3D 470
	3 QCBF,TQCBF,ICTYP,ISC,NPCB, QNBF,TQNB,INTYP,ISN,NPNB,	GW3D 475
	4 RF,TRF,IRTY,ISV,NPVB, HCON,HMIN, HDBF,THDBF,IDTY, NPDB,	GW3D 480
	5 ISTOP, NNPLR,GNLR)	GW3D 485
C		GW3D 490
	IF(IGEOM.LE.3) CALL PAGEN(GNOJCN,LNOJCN,LMAXDF,NTNPLR,GNLR,	GW3D 495
	1 IE,NNPLR)	GW3D 500
	REWIND 4	GW3D 505
	IF(IGEOM.LE.3) WRITE(4) ((GNOJCN(J,I),J-1,JBAND),I-1,NNP),	GW3D 510
	1 (NTNPLR(K),K-1,MXREGN),(LMAXDF(K),K-1,MXREGN),	GW3D 515
	2 (((LNOJCN(J,I,K),J-1,JBAND),I-1,LMXNP),K-1,MXREGN),	GW3D 520
	3 ((GNLR(I,K),I-1,LTMXNP),K-1,MXREGN),(NNPLR(K),K-1,MXREGN)	GW3D 525
	IF(IGEOM.GT.3) READ(4) ((GNOJCN(J,I),J-1,JBAND),I-1,NNP),	GW3D 530
	1 (NTNPLR(K),K-1,MXREGN),(LMAXDF(K),K-1,MXREGN),	GW3D 535
	2 (((LNOJCN(J,I,K),J-1,JBAND),I-1,LMXNP),K-1,MXREGN),	GW3D 540
	3 ((GNLR(I,K),I-1,LTMXNP),K-1,MXREGN),(NNPLR(K),K-1,MXREGN)	GW3D 545
C		GW3D 550
	KDIG=0	GW3D 555
	IF (ISTOP.GT.0) GO TO 990	GW3D 560
C		GW3D 565
C	----- PREPARE INITIAL OR PRE-INITIAL VARIABLES	GW3D 570
C		GW3D 575
	IF(NSEL.NE.0) CALL INTERP(SOS,TSOSF,SOSF,TIME,	GW3D 580
	1 MXSPR,MXSDP,NSPR,NSDP)	GW3D 585
	IF(NWNP.NE.0) CALL INTERP(WSS,TWSSF,WSSF,TIME,	GW3D 590
	1 MXWPR,MXWDP,NWPR,NWDP)	GW3D 595
C		GW3D 600
	IF(NCES.NE.0) CALL INTERP(QCB,TQCBF,QCBF,TIME,	GW3D 605
	1 MXCPR,MXCDP,NCPR,NCDP)	GW3D 610
	IF(NNES.NE.0) CALL INTERP(QNB,TQNB, QNB,TIME,	GW3D 615
	1 MXNPR,MXNDP,NNPR,NNDP)	GW3D 620
	IF(NVES.NE.0) CALL INTERP(RFALL,TRF,RF,TIME,	GW3D 625
	1 MXRPR,MXRDP,NRPR,NRDP)	GW3D 630
	IF(NDNP.NE.0) CALL INTERP(HDB,THDBF,HDBF,TIME,	GW3D 635
	1 MXDPR,MXDDP,NDPR,NDDP)	GW3D 640
C		GW3D 645
C	----- PUT DIRICHLET BOUNDARY VALUES TO INITIAL CONDITIONS	GW3D 650
C		GW3D 655
	DO 130 I=1,NDNP	GW3D 660
	NI=NPDB(I)	GW3D 665
	NP=NPBB(NI)	GW3D 670
	ITYP=IDTY(I)	GW3D 675
	H(NP)=HDB(ITYP)-Z(NP)*DFLOAT(KGRAV)	GW3D 680
	130 CONTINUE	GW3D 685

C		GW3D 690
	CALL SPROP(TH,DTH,AKR, IE,H,THPROP,AKPROP)	GW3D 695
C		GW3D 700
	CALL VELT(VX,VY,VZ,CMATRX,X,Y,Z,IE,H,HT,AKR,PROP)	GW3D 705
	KFLOW--1	GW3D 710
C		GW3D 715
	CALL SFLOW(X,Y,Z,IE, H,HP,VX,VY,VZ,TH,DTH,	GW3D 720
	1 BFLX,BFLXP,DCOSB,ISB,NPBB, MSEL,SOS,ISTYP, NPW,WSS,IWTYP,	GW3D 725
	2 NPVB,NPDB,NPCB,NPNB, DELT, KFLOW)	GW3D 730
C		GW3D 735
	DO 140 I=1,9	GW3D 740
	IF(I.EQ.9) GO TO 140	GW3D 745
	FLOW(I)=.0	GW3D 750
	TFLOW(I)=0.0	GW3D 755
	140 CONTINUE	GW3D 760
	FLOW(9)=0.0	GW3D 765
C		GW3D 770
C	----- PRINT INITIAL OR PRE-INITIAL VARIABLES	GW3D 775
C		GW3D 780
	KDIAG=0	GW3D 785
C		GW3D 790
	CALL PRINTT(VX,VY,VZ,H,HT,TH, NPBB,BFLX, NPVB,DCYFLX,NPCON,	GW3D 795
	INPFLX,NPMIN, SUBHD(1,1), TIME,DELT,KPRO,KOUT,KDIAG, -1)	GW3D 800
C		GW3D 805
	IF(KSTR.EQ.1 .AND. KSS.EQ.1 .AND. KDSK0.EQ.1)	GW3D 810
	> CALL STORE(X,Y,Z,IE, H,HT,TH,VX,VY,VZ,DCOSB,ISB,NPBB,	GW3D 815
	1 NNPLR,GNLR, TITLE, TIME, NPROB)	GW3D 820
C		GW3D 825
	IF (KSS.NE.0) GO TO 500	GW3D 830
C		GW3D 835
C	\$\$\$\$\$\$\$	GW3D 840
C	\$\$\$\$\$\$\$ PERFORM STEADY-STATE CALCULATION	GW3D 845
C	\$\$\$\$\$\$\$	GW3D 850
C		GW3D 855
	IF (NVES.EQ.0) GO TO 170	GW3D 860
C		GW3D 865
	DO 150 NPP=1,NVNP	GW3D 870
	NI=NPVB(NPP)	GW3D 875
	NPCON(NPP)=NPBB(NI)	GW3D 880
	NPMIN(NPP)=0	GW3D 885
	150 NPFLX(NPP)=0	GW3D 890
C		GW3D 895
	NCHG--1	GW3D 900
	CALL BCPREP(IE,X,Y,Z,H,VX,VY,VZ,DCOSB,ISB,NPVB,ISV,DCYFLX,FLX,	GW3D 905
	> HCON,HMIN,NPFLX,NPCON,NPMIN, IRTYP,RFALL, NCHG)	GW3D 910
C		GW3D 915
	170 DO 180 NP=1,NNP	GW3D 920
	180 HP(NP)=H(NP)	GW3D 925

C		GW3D 930
	KDIG-KDIG+1	GW3D 935
	IF(IBUG.NE.0) PRINT 10400,KDIG,TIME,DELT	GW3D 940
C		GW3D 945
C	----- ITERATION LOOP ON SEEPAGE-RAINFALL BOUNDARY CONDITIONS BEGINS	GW3D 950
C		GW3D 955
	EPS=0.5DO*TOLA	GW3D 960
C		GW3D 965
	DO 390 ICY-1,NCYL	GW3D 970
C		GW3D 975
	DO 210 NP-1,NNP	GW3D 980
	HW(NP)-OME*H(NP)+(1.0DO-OME)*HP(NP)	GW3D 985
	RI(NP)-HW(NP)	GW3D 990
	210 CONTINUE	GW3D 995
C		GW3D1000
C	----- ITERATION LOOP ON THE NON-LINEAR EQUATION BEGINS	GW3D1005
C		GW3D1010
	IF(IBUG.NE.0) PRINT 10401, ICY	GW3D1015
C		GW3D1020
C	----- PUT DIRICHLET BOUNDARY VALUES OF THE VARIABLE BOUNDARY	GW3D1025
C	----- INTO H, RI, HW, AND RL	GW3D1030
C		GW3D1035
	IF(NVES.EQ.0) GO TO 250	GW3D1040
	DO 230 NPP-1,NVNP	GW3D1045
	NI-NPMIN(NPP)	GW3D1050
	IF(NI.EQ.0) GO TO 220	GW3D1055
	H(NI)-HMIN(NPP)	GW3D1060
	RI(NI)-HMIN(NPP)	GW3D1065
	HW(NI)-HMIN(NPP)	GW3D1070
	RL(NI)-HMIN(NPP)	GW3D1075
	GO TO 230	GW3D1080
	220 NI-NPCON(NPP)	GW3D1085
	IF(NI.EQ.0) GO TO 230	GW3D1090
	H(NI)-HCON(NPP)	GW3D1095
	RI(NI)-HCON(NPP)	GW3D1100
	HW(NI)-HCON(NPP)	GW3D1105
	RL(NI)-HCON(NPP)	GW3D1110
	230 CONTINUE	GW3D1115
	250 CONTINUE	GW3D1120
C		GW3D1125
	DO 350 IT-1,NITER	GW3D1130
C		GW3D1135
C	----- EVALUATE SOIL PROPERTIES FOR PREVIOUS ITERATE	GW3D1140
C		GW3D1145
	CALL SPROP(TH,DTH,AKR, IE,HW,THPROP,AKPROP)	GW3D1150

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C
C ----- ASSEMBLE STEAD-STATE ELEMENT MATRICES QA AND QB INTO THE
C ----- GLOBAL MATRIX C AND CONSTRUCT GLOBAL LOAD VECTOR R FROM
C ----- ELEMENT LOAD VECTOR RQ.
C
      CALL ASEMBL(X,Y,Z,IE,CMATRX,RLD,GNOJCN,HW,HP,DTH,AKR,PROP,
      > SOS,MSEL,ISTYP,WSS,NPW,IWTYP,KSS,W,DELT)
C
C ----- APPLY STEADY-STATE BOUNDARY CONDITIONS
C
      CALL BC(CMATRX,RLD,GNOJCN,IE,X,Y,Z,AKR,PROP,DCOSB,ISB,NPBB,
      1 QCB,ISC,ICTYP,QNB,ISN,INTYP,FLX,HCON,HMIN,NPFLX,NPCON,NPMIN,
      2 HDB,IDTYP,NPDB,KSS)
C
C ----- SOLVE THE MATRIX EQUATION BY BLOCK ITERATION
C
      CALL BLKITR(RL,RI,CMTRXL,RLDL,CMATRX,RLD,GNLR,LNOJCN,NNPLR,
      1 LMAXDF,EPS,NPITER,IBUG,KPRO,OMI)
C
C ----- OBTAIN MAXIMUM RELATIVE DEVIATION FROM PREVIOUS ITERATE
C
      NPP=0
      RD=-1.0D0
      RES=-1.0D0
      DO 320 NP=1,NNP
      RESNP=DABS(RL(NP)-H(NP))
      RES=DMAX1(RES,RESNP)
      IF(H(NP).NE.0.0D0) RD=DMAX1(RD,DABS(RESNP/H(NP)))
      IF(RESNP.LE.TOLA) GO TO 320
      NPP=NPP+1
      NPCNV(NPP)=NP
320 CONTINUE
C
      NNCVN=NPP
C
C ----- UPDATE PRESSURE WITH CURRENT ITERATE
C
      DO 330 NP=1,NNP
      H(NP)=OME*RL(NP)+(1.0D0-OME)*H(NP)
      RI(NP)=H(NP)
      HW(NP)=H(NP)
330 CONTINUE
C
C ----- ESCAPE FROM ITERATION LOOP IF THE MAXIMUM RESIDUAL IS
C ----- SUFFICIENTLY SMALL
C
      IF(IBUG.NE.0) PRINT 10200,IT,RES,RD,NNCVN
      IF(IT.EQ.1) GO TO 350
      IF(RES.LT.TOLA) GO TO 360

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GW3D1155
GW3D1160
GW3D1165
GW3D1170
GW3D1175
GW3D1180
GW3D1185
GW3D1190
GW3D1195
GW3D1200
GW3D1205
GW3D1210
GW3D1215
GW3D1220
GW3D1225
GW3D1230
GW3D1235
GW3D1240
GW3D1245
GW3D1250
GW3D1255
GW3D1260
GW3D1265
GW3D1270
GW3D1275
GW3D1280
GW3D1285
GW3D1290
GW3D1295
GW3D1300
GW3D1305
GW3D1310
GW3D1315
GW3D1320
GW3D1325
GW3D1330
GW3D1335
GW3D1340
GW3D1345
GW3D1350
GW3D1355
GW3D1360
GW3D1365
GW3D1370
GW3D1375
GW3D1380
GW3D1385
GW3D1390
GW3D1395

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C		GW3D1400
	350 CONTINUE	GW3D1405
C		GW3D1410
C	----- END OF ITERATION LOOP ON THE NON-LINEAR EQUATION	GW3D1415
C		GW3D1420
	PRINT 10210, ICY, IT, NITER, RES, RD, NNCVN	GW3D1425
C		GW3D1430
C	----- PRINT NONCONVERGENING NODES	GW3D1435
C		GW3D1440
	IF(IBUG.EQ.0) GO TO 360	GW3D1445
	PRINT 10500	GW3D1450
	PRINT 10600, (NPCNV(NPP), NPP-1, NNCVN)	GW3D1455
C		GW3D1460
	360 IF(ICHNG.EQ.0) GO TO 380	GW3D1465
	IF(NVES.EQ.0) GO TO 380	GW3D1470
C		GW3D1475
C	----- PRINT RAINFALL-SEEPAGE B. C. CHANGE INFORMATION	GW3D1480
C		GW3D1485
	PRINT 10402, ICY	GW3D1490
	DO 370 I=1, NVNP	GW3D1495
	NI=N*VB(I)	GW3D1500
	NP=NPBB(NI)	GW3D1505
	PRINT 10403, I, NP, NPCON(I), HCON(I), NPMIN(I), HMIN(I), NPFLX(I),	GW3D1510
	1 FLX(I), DCYFLX(I)	GW3D1515
	370 CONTINUE	GW3D1520
C		GW3D1525
C	----- CALCULATE DARCY'S VELOCITY	GW3D1530
C		GW3D1535
	380 CALL SPROP(TH, DTH, AKR, IE, H, THPROP, AKPROP)	GW3D1540
C		GW3D1545
	CALL VELT(VX, VY, VZ, CMATRIX, X, Y, Z, IE, H, HT, AKR, PROP)	GW3D1550
C		GW3D1555
	IF(NVES .EQ. 0) GO TO 440	GW3D1560
C		GW3D1565
C	----- PREPARE BOUNDARY CONDITIONS ON THE VARIABLE-TYPE BOUNDARY FOR	GW3D1570
C	----- NEXT CYCLE COMPUTATIONS.	GW3D1575
C		GW3D1580
	CALL BCPREP(IE, X, Y, Z, H, VX, VY, VZ, DCOSB, ISB, NPVB, ISV, DCYFLX, FLX,	GW3D1585
	> HCON, HMIN, NPFLX, NPCON, NPMIN, IRTYP, RFALL, NCHG)	GW3D1590
C		GW3D1595
	IF(NCHG.EQ.0) GO TO 440	GW3D1600
	390 CONTINUE	GW3D1605
C		GW3D1610
C	----- END OF ITERATION LOOP ON SEEPAGE-RAINFALL BOUNDARY CONDITIONS	GW3D1615
C		GW3D1620
	PRINT 10610, ICY, IT, NCVL, NITER, RES, RD, NNCVN	GW3D1625
C		GW3D1630
	440 IF(NNCVN.EQ.0) GO TO 445	GW3D1635
	PRINT 10610, ICY, IT, NCVL, NITER, RES, RD, NNCVN	GW3D1640

C		GW3D1645
C	----- COMPUTE FLUXES THROUGH ALL TYPES OF BOUNDARIES.	GW3D1650
C		GW3D1655
	445 KFLOW=0	GW3D1660
	CALL SFLOW(X,Y,Z,IE, H,HP,VX,VY,VZ,TH,DTH,	GW3D1665
	1 BFLX,BFLXP,DCOSB,ISB,NPBB, MSEL,SOS,ISTYP,NPW,WSS,IWTYP,	GW3D1670
	2 NPVB,NPDB,NPCB,NPNB, DELT, KFLOW)	GW3D1675
C		GW3D1680
	DO 450 I=1,9	GW3D1685
	IF(I.EQ.9) GO TO 450	GW3D1690
	FLOW(I)=0.0	GW3D1695
	TFLOW(I)=0.0	GW3D1700
	450 CONTINUE	GW3D1705
	FLOW(9)=0.0	GW3D1710
C		GW3D1715
C	----- PRINT STEADY-STATE VARIABLES	GW3D1720
C		GW3D1725
	CALL PRINTT(VX,VY,VZ,H,HT,TH, NPBB,BFLX, NPVB,DCYFLX,NPCON,	GW3D1730
	1 NPFLX,NPMIN, SUBHD(1,2), TIME,DELT, KPRO,KOUT,KDIAG,0)	GW3D1735
C		GW3D1740
	IF(KSTR.EQ.1 .AND. KDSKO.EQ.1) CALL STORE(X,Y,Z,IE,	GW3D1745
	> H,HT,TH,VX,VY,VZ,DCOSB,ISB,NPBB, NNPLR,GNLR, TITLE,TIME,NPROB)	GW3D1750
C		GW3D1755
	IF (NTI.EQ.0) GO TO 160	GW3D1760
C		GW3D1765
	KSS=1	GW3D1770
C		GW3D1775
C	\$\$\$\$\$\$\$	GW3D1780
C	\$\$\$\$\$\$\$ PERFORM TRANSIENT-STATE CALCULATION	GW3D1785
C	\$\$\$\$\$\$\$	GW3D1790
C		GW3D1795
	500 IF (NVES.EQ.0) GO TO 550	GW3D1800
C		GW3D1805
	DO 510 NPP=1,NVNP	GW3D1810
	NI=NPVB(NPP)	GW3D1815
	NPCON(NPP)=NPBB(NI)	GW3D1820
	NPMIN(NPP)=0	GW3D1825
	510 NPFLX(NPP)=0	GW3D1830
C		GW3D1835
	NCHG=-1	GW3D1840
C		GW3D1845
	550 TIME=TIME+DELT	GW3D1850
	W1=W	GW3D1855
	W2=1.000 W	GW3D1860
	KFLOW=1	GW3D1865
	TFLOW(9)=0.0	GW3D1870

C		GW3D1875
C	----- BEGIN THE TIME-MARCHING LOOP	GW3D1880
C	EPS=0.5D0*TOLB	GW3D1885
	IDELT=0	GW3D1890
	DO 890 ITM=1,NTI	GW3D1895
	ITMITM=ITM	GW3D1900
C		GW3D1905
C	----- PREPARE TRANSIENT BOUNDARY CONDITIONS AND SOURCE FOR THE STEP	GW3D1910
C		GW3D1915
	IF(NSEL.NE.0) CALL INTERP(SOS,TSOSF,SOSF,TIME,MXSPR,MXSDP,	GW3D1920
	1 NSPR,NSDP)	GW3D1925
	IF(NWNP.NE.0) CALL INTERP(WSS,TWSSF,WSSF,TIME,MXWPR,MXWDP,	GW3D1930
	1 NWPR,NWDP)	GW3D1935
C		GW3D1940
	IF(NCES.NE.0) CALL INTERP(QCB,TQCBF,QCBF,TIME,	GW3D1945
	1 MXCPR,MXCDP,NCPR,NCDP)	GW3D1950
	IF(NNES.NE.0) CALL INTERP(QNB,TQBNF,QBNF,TIME,	GW3D1955
	1 MXNPR,MXNDP,NNPR,NNDP)	GW3D1960
	IF(NVES.NE.0) CALL INTERP(RFALL,TRF,RF,TIME,	GW3D1965
	1 MXRPR,MXRDP,NRPR,NRDP)	GW3D1970
	IF(NDNP.NE.0) CALL INTERP(HDB,THDSF,HDBF,TIME,	GW3D1975
	1 MXDPR,MXDDP,NDPR,NDDP)	GW3D1980
C		GW3D1985
	IF(NVES.EQ.0) GO TO 560	GW3D1990
	NCHG=-1	GW3D1995
	CALL BCPREP(IE,X,Y,Z, H,VX,VY,VZ, DCOSB,ISB, NPVB,ISV,DCYFLX,FLX,	GW3D2000
	1 HCON,HMIN,NPFLX,NPCON,NPMIN, IRTYP,RFALL, NCHG)	GW3D2005
C		GW3D2010
	560 DO 570 NP=1,NNP	GW3D2015
	RL(NP)=H(NP)	GW3D2020
	HP(NP)=H(NP)	GW3D2025
	570 CONTINUE	GW3D2030
C		GW3D2035
	KDIG=KDIG+1	GW3D2040
	IF(IBUG.NE.0 .AND. KPR(ITM).NE.0) PRINT 10400, KDIG,TIME,DELT	GW3D2045
C		GW3D2050
C	----- BEGIN ITERATION LOOP ON SEEPAGE-RAINFALL BOUNDARY CONDITIONS	GW3D2055
C		GW3D2060
	DO 690 ICY=1,NCYL	GW3D2065
	IF(IBUG.NE.0 .AND. KPR(ITM).NE.0) PRINT 10401, ICY	GW3D2070
C		GW3D2075
	DO 580 NP=1,NNP	GW3D2080
	H(NP)=OME*RI(NP)+(1.0D0-OME)*H(NP)	GW3D2085
	RI(NP)=H(NP)	GW3D2090
	HW(NP)=W1*(OME*H(NP)+(1.0D0-OME)*HP(NP))+W2*HP(NP)	GW3D2095
	580 CONTINUE	GW3D2100
		GW3D2105

C		GW3D2110
C	----- BEGIN ITERATION LOOP ON THE NON-LINEAR EQUATION	GW3D2115
C		GW3D2120
C	----- PUT DIRICHLET BOUNDARY VALUES OF THE VARIABLE BOUNDARY	GW3D2125
C	----- INTO H, RI, HW, AND RL	GW3D2130
C		GW3D2135
	IF(NVES.EQ.0) GO TO 595	GW3D2140
	DO 590 NPP-1,NVNP	GW3D2145
	NI-NPMIN(NPP)	GW3D2150
	IF(NI.EQ.0) GO TO 585	GW3D2155
	H(NI)-HMIN(NPP)	GW3D2160
	RI(NI)-HMIN(NPP)	GW3D2165
	HW(NI)-HMIN(NPP)	GW3D2170
	RL(NI)-HMIN(NPP)	GW3D2175
	GO TO 590	GW3D2180
	585 NI-NPCON(NPP)	GW3D2185
	IF(NI.EQ.0) GO TO 590	GW3D2190
	H(NI)-HCON(NPP)	GW3D2195
	RI(NI)-HCON(NPP)	GW3D2200
	HW(NI)-HCON(NPP)	GW3D2205
	RL(NI)-HCON(NPP)	GW3D2210
	590 CONTINUE	GW3D2215
	595 CONTINUE	GW3D2220
C		GW3D2225
	DO 650 IT-1,NITER	GW3D2230
C		GW3D2235
C	----- EVALUATE SOIL PROPERTIES FOR PREVIOUS ITERATE	GW3D2240
C		GW3D2245
	CALL SPROP(TH,DTH,AKR, IE,HW,THPROP,AKPROP)	GW3D2250
C		GW3D2255
C	----- ASSEMBLE ELEMENT MATRICES QA AND QB INTO THE GLOBAL MATRIX C	GW3D2260
C	----- AND CONSTRUCT THE GLOBAL LOAD VECTOR R FROM ELEMENT LOAD	GW3D2265
C	----- VECTOR RQ.	GW3D2270
C		GW3D2275
	CALL ASEMBL(X,Y,Z,IE, CMATRX,RLD,GNOJCN,HW,HP,DTH, AKR,PROP,	GW3D2280
	> SOS,MSEL,ISTYP,WSS,NPW,IWTYP, KSS,W,DELTA)	GW3D2285
C		GW3D2290
C	----- APPLY BOUNDARY CONDITIONS TO MODIFY THE GLOBAL MATRIX C AND	GW3D2295
C	----- THE LOAD VECTOR R.	GW3D2300
C		GW3D2305
	CALL BC(CMATRX,RLD,GNOJCN, IE,X,Y,Z, AKR,PROP, DCOSB,ISB,NPBB,	GW3D2310
	1 QCB,ISC,ICTYP, QNB,ISN,INTYP, FLX,HCON,HMIN,NPFLX,NPCON,NPMIN,	GW3D2315
	2 HDB,IDTYP,NPDB, KSS)	GW3D2320
C		GW3D2325
C	----- SOLVE THE MATRIX EQUATION BY BLOCK ITERATION	GW3D2330
C		GW3D2335
	CALL BLKTR(RL,RI,CMTRXL,RLDL, CMATRX,RLD, CNLR,LNOJCN,NNPLR,	GW3D2340
	1 LMAXDF, EPS,NPITER,IBUG,KPR(ITM),OMI)	GW3D2345

C		GW3D2350
C	----- OBTAIN MAXIMUM RELATIVE DEVIATION FROM PREVIOUS ITERATE	GW3D2355
C		GW3D2360
	NPP=0	GW3D2365
	RD=-1.0D0	GW3D2370
	RES=-1.0D0	GW3D2375
	DO 620 NP=1,NNP	GW3D2380
	RESNP=DABS(RL(NP)-H(NP))	GW3D2385
	RES=DMAX1(RES,RESNP)	GW3D2390
	IF(H(NP) .NE. 0.0D0) RD=DMAX1(RD,DABS(RESNP/H(NP)))	GW3D2395
	IF(RESNP .LE. TOLB) GO TO 620	GW3D2400
	NPP=NPP+1	GW3D2405
	NPCNV(NPP)=NP	GW3D2410
	620 CONTINUE	GW3D2415
C		GW3D2420
	NPCNV=NPP	GW3D2425
C		GW3D2430
C	----- UPDATE PRESSURE WITH CURRENT ITERATE	GW3D2435
C		GW3D2440
	DO 630 NP=1,NNP	GW3D2445
	H(NP)=OME*RL(NP)+(1.0D0-OME)*H(NP)	GW3D2450
	RI(NP)=H(NP)	GW3D2455
	HW(NP)=W1*H(NP)+W2*HP(NP)	GW3D2460
	630 CONTINUE	GW3D2465
C		GW3D2470
C	----- ESCAPE FROM ITERATION LOOP IF THE MAXIMUM RESIDUAL IS	GW3D2475
C	----- SUFFICIENTLY SMALL.	GW3D2480
C		GW3D2485
	IF(IBUG.NE.0 .AND. KPR(ITM).NE.0) PRINT 10200, IT,RES,RD,NPCNV	GW3D2490
	IF(IT.EQ.1 .AND. ITM.EQ.1) GO TO 650	GW3D2495
	IF(RES.LT.TOLB) GO TO 660	GW3D2500
C		GW3D2505
	650 CONTINUE	GW3D2510
C		GW3D2515
C	----- END THE ITERATION LOOP ON THE NON-LINEAR EQUATION	GW3D2520
C		GW3D2525
	PRINT 10710, ITM,ICY,IT,NITER,RES,RD,NPCNV	GW3D2530
C		GW3D2535
	IF(IBUG.EQ.0 .OR. KPR(ITM).EQ.0) GO TO 660	GW3D2540
C		GW3D2545
C	----- PRINT NONCONVERGING NODES	GW3D2550
C		GW3D2555
	PRINT 10500	GW3D2560
	PRINT 10600, (NPCNV(NPP),NPP-1,NPCNV)	GW3D2565
C		GW3D2570
	660 IF(ICHNG.EQ.0 .OR. KPR(ITM).EQ.0) GO TO 680	GW3D2575
	IF(NVES.EQ.0) GO TO 680	GW3D2580

C		GW3D2585
C	----- PRINT RAINFALL-SEEPAGE BOUNDARY CONDITION CHANGE INFORMATION	GW3D2590
C		GW3D2595
	PRINT 10402, ICY	GW3D2600
	DO 670 I=1,NVNP	GW3D2605
	NI-NPVB(I)	GW3D2610
	NP-NPBB(NI)	GW3D2615
	PRINT 10403, I,NP,NPCON(I),HCON(I),NPMIN(I),HMIN(I),NPFLX(I),	GW3D2620
	1 FLX(I),DCYFLX(I)	GW3D2625
	670 CONTINUE	GW3D2630
C		GW3D2635
C	----- CALCULATE DARCY'S VELOCITY	GW3D2640
C		GW3D2645
	680 CALL SPROP(TH,DTH,AKR, IE,H,THPROP,AKPROP)	GW3D2650
C		GW3D2655
	CALL VELT(VX,VY,VZ,CMATRX,X,Y,Z,IE,H,HT,AKR,PROP)	GW3D2660
C		GW3D2665
	IF(NVES.EQ.0) GO TO 710	GW3D2670
C		GW3D2675
	CALL BCPREP(IE,X,Z,H,VX,VY,VZ,DCOSB,ISB,NPVB,ISV,DCYFLX,FLX,	GW3D2680
	> HCON,HMIN,NPFLX,NPCON,NPMIN,IRTP,RFALL,NCHG)	GW3D2685
C		GW3D2690
	IF(NCHG.EQ.0) GO TO 710	GW3D2695
C		GW3D2700
	690 CONTINUE	GW3D2705
C		GW3D2710
C	----- END ITERATION LOOP ON SEEPAGE-RAINFALL BOUNDARY CONDITIONS	GW3D2715
C		GW3D2720
	PRINT 10810, ITM,ICY,IT,NCYL,NITER,RES,RD,NNCVN	GW3D2725
	710 IF(NNCVN.EQ.0) GO TO 740	GW3D2730
	PRINT 10810, ITM,ICY,IT,NCYL,NITER,RES,RD,NNCVN	GW3D2735
C		GW3D2740
C	----- COMPUTE FLUXES THROUGH ALL TYPES OF BOUNDARIES	GW3D2745
C		GW3D2750
	740 CALL SFLOW(X,Y,Z,IE, H,HP,VX,VY,VZ,TH,DTH,	GW3D2755
	1 BFLX,BFLXP,DCOSB,ISB,NPBB, MSEL,SOS,ISTYP,NPW,WSS,IWTYP,	GW3D2760
	2 NPVB,NPDB,NPCB,NPNB, DELT, KFLOW)	GW3D2765
C		GW3D2770
C	----- PRINT VARIABLES AT EACH TIME STEP	GW3D2775
C		GW3D2780
	CALL PRINTT(VX,VY,VZ,H,HT,TH, NPBB,BFLX, NPVB,DCYFLX,NPCON,	GW3D2785
	1 NPFLX,NPMIN.SUBHD(1,3), TIME,DELT, KPR(ITM),KOUT,KDIAG,ITMITM)	GW3D2790
C		GW3D2795
	IF(KSTR.EQ.1 .AND.KDSK(ITM).EQ.1) CALL STORE(X,Y,Z,IE,	GW3D2800
	> H,HT,TH,VX,VY,VZ,DCOSB,ISB,NPBB, NNPLR,GNLR, TITLE, TIME,NPROB)	GW3D2805
C		GW3D2810
C	----- PREPARE FOR NEXT TIME STEP	GW3D2815
C		GW3D2820
	IF(TIME.GT.TMAX) GO TO 100	GW3D2825
	DELT=DELT*(1.000+CHNG)	GW3D2830

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DELT-DMIN1(DELT,DELMAX)
IF(IDELT.EQ.0) GO TO 880
IF(TIME.EQ.TDTCH(IDELT)) DELT-DELTO
880 TIME-TIME+DELT
IF(TIME.LT.TDTCH(IDELT+1)) GO TO 890
IDELT-IDELT+1
TIME-TIME-DELT
DELT-TDTCH(IDELT)-TIME
IF(DELT.LE.0.0) DELT-DELTO
TIME-TIME+DELT
890 CONTINUE
C
C ----- END OF TIME-MARCHING LOOP
C
C GO TO 100
C
990 RETURN
C
10 FORMAT(I5,9A8,3I1)
1000 FORMAT('1 PROBLEM',I5,'... ',9A8,1X,3I1/)
10200 FORMAT(5X,I10,3X,E12.4,3X,E12.4,15X,I10)
10400 FORMAT('1', '*****', GW3D2940
1 '*****', GW3D2945
2 '*****'///' DIAGNOSTIC TABLE',I4,'... AT TIME =',1PD12.4, GW3D2950
3 ' ',(DELT =',1PD12.4,')', GW3D2955
10401 FORMAT(///' TABLE OF ITERATIVE PARAMETERS FOR',I3,'-TH CYCLE'//6X, GW3D2960
1 'ITERATION',7X,'RESIDUAL',6X,'DEVIATION',6X, GW3D2965
2 'NO. NON-CONV. NODES') GW3D2970
10402 FORMAT(///' TABLE OF RAINFALL/EVAPORATION-SEEPAGE B. C. USED FOR', GW3D2975
1 I3,'-TH CYCLE'//7X,' I NPVB NPCON HCON NPMIN HMIN', GW3D2980
2 ' NPFLX FLX DCYFLX FROM PREVIOUS CYCLE'/7X, GW3D2985
3 ' -----' GW3D2990
4 ' -----' GW3D2995
10403 FORMAT(1H ,I8,I6,I7,D12.4,I7,D12.4,I7,D12.4,12X,D12.4) GW3D3000
10500 FORMAT(///' TABLE OF NON-CONVERGING NODES') GW3D3005
10600 FORMAT(/(5X,20I5)) GW3D3010
10210 FORMAT(1H0,'WARNING: NON-CONVERGENCE OCCUR DURING STEADY STATE SOLUGW3D3015
TION AT',I3,'-TH CYCLE'/1H ,IT =',I3,' .GT. MAXIT =',I3, GW3D3020
2 ' , RES =',D12.5,', RD =',D12.4,', NNCVN =',I4) GW3D3025
10610 FORMAT(1H0,'ABSOLUTELY WARNING: STEADY STATE SOLUTION IS NG'/1H , GW3D3030
> 'ICY =',I3,' IT =',I3,' MAXCY =',I3,' MAXIT =',I3, GW3D3035
> ' , RES =',D12.4,', RD =',D12.4,', NNCVN =',I4) GW3D3040
10710 FORMAT(1H0,'WARNING: NON-CONVERGENCE OCCUR AT',I5,'-TH TIME STEP'GW3D3045
>,I3,'-TH CYCLE'/1H ,IT =',I3,' .GT. MAXIT =',I3,2D12.4,I5) GW3D3050
10810 FORMAT(1H0,'ABSOLUTELY WARNING: TRANSIENT SOLUTION IS NG AT',I5, GW3D3055
> ' -TH TIME STEP'/1H ,ICY =',I3,' IT =',I3,' MAXCY =',I3, GW3D3060
> ' MAXIT =',I3,', RES =',D12.4,', RD =',D12.4,', NNCVN =',I4)GW3D3065
C
C END GW3D3070
GW3D3075

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SUBROUTINE DATAIN(TITLE,NPROB, KPR,KDSK, TDTCH, DATA 005
1 PROP, THPROP, AKPROP, X, Y, Z, IE, H, DCOSB, ISB, NPBB, DATA 010
2 SOSF, TSOSF, ISTYP, MSEL, WSSF, TWSSF, IWTYP, NPW, DATA 015
3 QCBF, TQCBF, ICTYP, ISC, NPCB, QNBF, TQNBF, INTYP, ISN, NPNB, DATA 020
4 RF, TRF, IRTYP, ISV, NPVB, HCON, HMIN, HDDBF, THDBF, IDTYP, NPDB, DATA 025
5 ISTOP, NNPLR, GNLR) DATA 030
C DATA 035
C*****1*****2*****3*****4*****5*****6*****7**DATA 040
C ----- TO READ AND PRINT SYSTEM PARAMETERS, GEOMETRY, BOUNDARY AND DATA 045
C ----- INITIAL CONDITIONS, AND PROPERTIES OF THE MEDIA. DATA 050
C*****1*****2*****3*****4*****5*****6*****7**DATA 055
C DATA 060
IMPLICIT REAL*8(A-H,O-Z) DATA 065
REAL*4 PMAT, THPAR, AKPAR DATA 070
INTEGER*4 GNLR DATA 075
C DATA 080
COMMON /SGEOM/ MAXEL, MAXNP, MAXBES, MAXBNP, JBAND, MAXNTI, MXNDTC DATA 085
COMMON /CGEOM/ NNP, NEL, NBNP, NBES, KGRAV, NTI, NDTCHG DATA 090
COMMON /LGEOM/ LTMXNP, LMXNP, LMXBW, MXREGN, NREGN DATA 095
COMMON /CINTE/ NCYL, NITER, KSTR, KPRO, KDSKO, KSS, NPITER, IGEOM DATA 100
COMMON /CREAL/ DELT, CHNG, DELMAX, TMAX, DELT0, TOLA, TOLB, W, OME, OMI DATA 105
C DATA 110
COMMON /CS/ MXSEL, MXSPR, MXSDP, NSEL, NSPR, NSDP DATA 115
COMMON /CW/ MXWNP, MXWPR, MXWDP, NWNP, NWPR, NWDP DATA 120
C DATA 125
COMMON /CCBC/ MXCNP, MXCES, MXCPR, MXCDP, NCNP, NCES, NCPR, NCDP DATA 130
COMMON /CNBC/ MXNNP, MXNES, MXNPR, MXNDP, NNNP, NNES, NNPR, NNDP DATA 135
COMMON /CVBC/ MXVES, MXVNP, MXRPR, MXRDP, NVES, NVNP, NRPR, NRDP DATA 140
COMMON /CDBC/ MXDNP, MXDPR, MXDDP, NDNP, NDPR, NDDP DATA 145
C DATA 150
COMMON /SMTL/ MAXMAT, MXSPPM, MXMPPM DATA 155
COMMON /CMTL/ NMAT, NMPPM, NSPPM DATA 160
C DATA 165
DIMENSION TITLE(9) DATA 170
C DATA 175
DIMENSION KPR(MAXNTI), KDSK(MAXNTI), TDTCH(MXNDTC) DATA 180
C DATA 185
DIMENSION PROP(MXMPPM, MAXMAT) DATA 190
DIMENSION THPROP(MXSPPM, MAXMAT), AKPROP(MXSPPM, MAXMAT) DATA 195
C DATA 200
DIMENSION X(MAXNP), Y(MAXNP), Z(MAXNP), IE(MAXEL, 9), H(MAXNP) DATA 205
DIMENSION DCOSB(3, MAXBES), ISB(6, MAXBES), NPBB(MAXBNP) DATA 210
C DATA 215
DIMENSION MSEL(MXSEL), ISTYP(MXSEL) DATA 220
DIMENSION SOSF(MXSDP, MXSPR), TSOSF(MXSDP, MXSPR) DATA 225
DIMENSION NPW(MXWNP), IWTYP(MXWNP) DATA 230
DIMENSION WSSF(MXWDP, MXWPR), TWSSF(MXWDP, MXWPR) DATA 235
C DATA 240
DIMENSION QCBF(MXCDP, MXCPR), TQCBF(MXCDP, MXCPR), ICTYP(MXCES) DATA 245
DIMENSION ISC(5, MXCES), NPCB(MXCNP) DATA 250

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DIMENSION QNBF(MXNDP,MXNPR),TQNBF(MXNDP,MXNPR),INTYP(MXNES)      DATA 255
DIMENSION ISN(5,MXNES),NPNB(MXNNP)                                DATA 260
DIMENSION RF(MXRDP,MXRPR),TRF(MXRDP,MXRPR),IRTP(MXVES)          DATA 265
DIMENSION ISV(5,MXVES),NPVB(MXVNP)                                DATA 270
DIMENSION HCON(MXVNP),HMIN(MXVNP)                                  DATA 275
DIMENSION HDBF(MXDDP,MXDPR),THDBF(MXDDP,MXDPR),IDTYP(MXDN?)    DATA 280
DIMENSION NPDB(MXDNP)                                             DATA 285
DIMENSION NNPLR(MXREGN),GNLR(LTMXNP,MXREGN)                       DATA 290
C                                                                    DATA 295
DIMENSION NIMI(4),NJMJ(4),IEM(8)                                  DATA 300
DIMENSION PMAT(3,6),AKPAR(3,8),THPAR(3,8)                         DATA 305
C                                                                    DATA 310
DATA PMAT/4H S,4HAT K,4HXX ,4H S,4HAT K,4HYY ,4H S,              DATA 315
> 4HAT K,4HZZ ,4H S,4HAT K,4HXY ,4H S,4HAT K,4HXZ ,4H S,      DATA 320
>4HAT K,4HYZ /                                                    DATA 325
C                                                                    DATA 330
DATA THPAR/4H ,4H TH1,4H ,4H ,4H TH2,4H ,4H ,                    DATA 335
> 4H TH3,4H ,4H ,4H TH4,4H ,4H ,4H TH5,4H ,4H ,                DATA 340
> 4H TH6,4H ,4H ,4H TH7,4H ,4H ,4H TH8,4H /                     DATA 345
C                                                                    DATA 350
DATA AKPAR/4H ,4H K1,4H ,4H ,4H K2,4H ,4H ,                      DATA 355
> 4H K3,4H ,4H ,4H K4,4H ,4H ,4H K5,4H ,                        DATA 360
> 4H ,4H K6,4H ,4H ,4H K7,4H ,4H ,4H K8,4H /                   DATA 365
C                                                                    DATA 370
ISTOP=0                                                            DATA 375
C                                                                    DATA 380
C ***** DATA SET 2: BASIC INTEGER PARAMETERS                   DATA 385
C                                                                    DATA 390
READ 10, NNP,NEL,NMAT,NCM,NTI,KSS,NSPPM,NMPPM,KSTR,              DATA 395
1 KCP,KGRAV,NITER,NCYL,NDTCHG,NPITER,NREGN                      DATA 400
IF(NDTCHG.LE.0) NDTCHG=1                                         DATA 405
PRINT 1000, NNP,NEL,NMAT,NCM,NTI,KSS,NSPPM,NMPPM,KSTP,         DATA 410
1 KCP,KGRAV,NITER,NCYL,NDTCHG,NPITER,NREGN                      DATA 415
C                                                                    DATA 420
C ***** DATA SET 3: BASIC REAL PARAMETERS                     DATA 425
C                                                                    DATA 430
READ 20, DELT,CHNG,DELMAX,TMAX,TOLA,TOLB,RHO,GRAV,VISC,W,      DATA 435
1 OME,OMI                                                         DATA 440
C                                                                    DATA 445
DELTO=DELT                                                         DATA 450
IF(TMAX.LE.0.0) TMAX=1.0D38                                       DATA 455
C                                                                    DATA 460
PRINT 1100, DELT,CHNG,DELMAX,TMAX,TOLA,TOLB,RHO,GRAV,VISC,W,  DATA 465
1 OME,OMI                                                         DATA 470
C                                                                    DATA 475
C ***** DATA SET 4: LINE PRINT CONTROL AND DISK STORE CONTROL DATA 480
C                                                                    DATA 485
READ 30, KPRO,(KPR(ITM),ITM=1,NTI)                                DATA 490
READ 30, KDSK,(KDSK(ITM),ITM=1,NTI)                              DATA 495
READ 20, (TDTCH(I),I=1,NDTCHG)                                    DATA 500

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C		DATA 505
	PRINT 1200	DATA 510
	PRINT 1210, KPRO, (KPR(ITM), ITM-1, NTI)	DATA 515
	PRINT 1300	DATA 520
	PRINT 1210, KDSK0, (KDSK(ITM), ITM-1, NTI)	DATA 525
	PRINT 1350, (TDTCH(I), I-1, NDTCHG)	DATA 530
C		DATA 535
C	***** DATA SET 5: MATERIAL PROPERTIES	DATA 540
C		DATA 545
	PRINT 1400, ((PMAT(I,J), I-1, 3), J-1, NMPPM)	DATA 550
	DO 100 I-1, NMAT	DATA 555
	READ 20, (PROP(J, I), J-1, NMPPM)	DATA 560
	100 PRINT 1410, I, (PROP(J, I), J-1, NMPPM)	DATA 565
C		DATA 570
C	***** DATA SET 6: SOIL PROPERTIES	DATA 575
C		DATA 580
C		DATA 585
C	----- READ AND PRINT PARAMETERS REQUIRE TO COMPUTE	DATA 590
C	----- MOISTURE CONTENT GIVEN THE PRESSURE HEAD	DATA 595
C		DATA 600
	IF (NSPPM.EQ.0) GO TO 200	DATA 605
	PRINT 1500, ((THPAR(I,J), I-1, 3), J-1, 8)	DATA 610
	DO 105 I-1, NMAT	DATA 615
	READ 20, (THPROP(J, I), J-1, NSPPM)	DATA 620
	PRINT 1510, I, (THPROP(J, I), J-1, NSPPM)	DATA 625
	105 CONTINUE	DATA 630
C		DATA 635
C	----- READ AND PRINT PARAMETERS REQUIRED TO COMPUTE RELATIVE	DATA 640
C	----- HYDRAULIC CONDUCTIVITY	DATA 645
C		DATA 650
	PRINT 1600, ((AKPAR(I,J), I-1, 3), J-1, 8)	DATA 655
	DO 110 I-1, NMAT	DATA 660
	READ 20, (AKPROP(J, I), J-1, NSPPM)	DATA 665
	PRINT 1510, I, (AKPROP(J, I), J-1, NSPPM)	DATA 670
	110 CONTINUE	DATA 675
	IF (KCP.EQ.0) GO TO 200	DATA 680
C		DATA 685
C	----- CONVERT FROM SATURATED PERMEABILITY TO SATURATED CONDUCTIVITY	DATA 690
C		DATA 695
	DO 190 I-1, NMAT	DATA 700
	PKCF=RHO*GRAV/VISC	DATA 705
	DO 190 J-1, 6	DATA 710
	PROP(J, I)=PROP(J, I)*PKCF	DATA 715
	190 CONTINUE	DATA 720
C		DATA 725
C	***** DATA SET 7: NODE COORDINATES	DATA 730
C		DATA 735
C	----- READ NODAL POINT COORDINATES	DATA 740
C		DATA 745
	200 NPI=0	DATA 750

210 READ 40, NI,NSEQ,NIAD,XI,YI,ZI,XIAD,YIAD,ZIAD	DATA 755
IF(NI.EQ.0) GO TO 240	DATA 760
NJ=NI+NSEQ	DATA 765
DO 220 NP=NI,NJ	DATA 770
I=NI+NIAD*(NP-NI)	DATA 775
X(I)=XI+XIAD*DFLOAT(NP-NI)	DATA 780
Y(I)=YI+YIAD*DFLOAT(NP-NI)	DATA 785
Z(I)=ZI+ZIAD*DFLOAT(NP-NI)	DATA 790
NPI=NPI+1	DATA 795
220 CONTINUE	DATA 800
GO TO 210	DATA 805
240 IF(NPI.EQ.NNP) GO TO 250	DATA 810
PRINT 2000	DATA 815
STOP	DATA 820
250 CONTINUE	DATA 825
C	DATA 830
C ----- PRINT NODAL POINT COORDINATES	DATA 835
C	DATA 840
IF(MOD(IGEOM,2).EQ.0) GO TO 270	DATA 845
LINE=0	DATA 850
DO 265 NP=1,NNP,3	DATA 855
NJMN=NP	DATA 860
NJMX=MIN0(NP+2,NNP)	DATA 865
LINE=LINE+1	DATA 870
IF(MOD(LINE-1,50).EQ.0) PRINT 2100	DATA 875
PRINT 2110, (NJ,X(NJ),Y(NJ),Z(NJ),NJ-NJMN,NJMX)	DATA 880
265 CONTINUE	DATA 885
270 CONTINUE	DATA 890
C	DATA 895
C ***** DATA SET 8: SUBREGION DATA	DATA 900
C	DATA 905
CALL READN(NNPLR,MXREGN,NREGN)	DATA 910
IF(MOD(IGEOM,2).NE.0) PRINT 2200	DATA 915
DO 280 K=1,NREGN	DATA 920
LNNP=NNPLR(K)	DATA 925
CALL READN(GNLR(1,K),LTMXNP,LNNP)	DATA 930
IF(MOD(IGEOM,2).NE.0) PRINT 2210, K,(GNLR(I,K),I=1,LNNP)	DATA 935
280 CONTINUE	DATA 940
C	DATA 945
C ***** DATA SET 9: ELEMENT DATA	DATA 950
C	DATA 955
C ----- READ ELEMENT INDICES AND COMPUTE MAXIMUM NODAL DIFFERENCE FOR	DATA 960
C ----- EACH ELEMENT	DATA 955
C	DATA 970
MMP=0	DATA 975
300 READ 10, MI,NSEQ,MIAD,(IEM(I),I=1,8),IEMAD	DATA 980
IF(MI.EQ.0) GO TO 330	DATA 985
C	DATA 990
MJ=MI+NSEQ	DATA 995
DO 320 MP=MI,MJ	DATA1000

K=MI+(MP-MI)*MIAD	DATA1005
DO 310 IQ=1,8	DATA1010
NI=IEM(IQ)+(MP-MI)*IEMAD	DATA1015
310 IE(M,IQ)=NI	DATA1020
MMP=MMP+1	DATA1025
320 CONTINUE	DATA1030
GO TO 300	DATA1035
C	DATA1040
330 IF(MMP.EQ.NEL) GO TO 350	DATA1045
PRINT 3000, MMP,NEL	DATA1050
STOP	DATA1055
C	DATA1060
350 DO 360 M=1,NEL	DATA1065
360 IE(M,9)=1	DATA1070
C	DATA1075
C ***** DATA SET 10: MATERIAL CORRECTIONS	DATA1080
C	DATA1085
IF (NCM.LE.0) GO TO 405	DATA1090
CALL READN(IE(1,9),MAXEL,NCM)	DATA1095
C	DATA1100
C ----- PRINT ELEMENT INCIDENCE AND MATERIAL TYPES FOR EACH ELEMENT	DATA1105
C	DATA1110
405 CONTINUE	DATA1115
IF(MOD(IGEOM,2).EQ.0) GO TO 415	DATA1120
LINE=0	DATA1125
DO 410 NI=1,NEL,2	DATA1130
NJMN=NI	DATA1135
NJMX=MINO(NI+1,NEL)	DATA1140
LINE=LINE+1	DATA1145
IF(MOD(LINE-1,50).EQ.0) PRINT 2700	DATA1150
PRINT 3100, (NJ,(IE(NJ,K),K=1,9),NJ-NJMN,NJMX)	DATA1155
410 CONTINUE	DATA1160
415 CONTINUE	DATA1165
C	DATA1170
C ----- CHECK IF MATERIAL TYPE FOR EACH ELEMENT IS CORRECT	DATA1175
C	DATA1180
DO 420 M=1,NEL	DATA1185
MTYP=IE(M,9)	DATA1190
IF(MTYP.GT.0 .AND. MTYP.LE.NMAT) GO TO 420	DATA1195
PRINT 4200, M	DATA1200
ISTOP=ISTOP+1	DATA1205
420 CONTINUE	DATA1210
C	DATA1215
IF(ISTOP.EQ.0) GO TO 430	DATA1220
PRINT 4300, ISTOP	DATA1225
STOP	DATA1230
C	DATA1235
C ----- IDENTIFY BOUNDARY ELEMENTS AND COMPUTE DIRECTIONAL COSINES	DATA1240
C	DATA1245
430 CONTINUE	DATA1250

IF(IGEOM.LE.1) CALL SURF(X,Y,Z,IE, DCOSB,ISB,NPBB)	DATA1255
REWIND 3	DATA1260
IF(IGEOM.LE.1) WRITE(3) NBES,NBNP,((DCOSB(J,I),J-1,3),I-1,NBES).	DATA1265
1 ((ISB(J,I),J-1,6),I-1,NBES), (NPBB(I),I-1,NBNP)	DATA1270
IF(IGEOM.GT.1) READ(3) NBES,NBNP,((DCOSB(J,I),J-1,3),I-1,NBES),	DATA1275
1 ((ISB(J,I),J-1,6),I-1,NBES), (NPBB(I),I-1,NBNP)	DATA1280
C	DATA1285
C ***** DATA SET 11: INITIAL CONDITIONS	DATA1290
C	DATA1295
C	DATA1300
C ----- READ INITIAL OR PRE-INITIAL CONDITIONS VIA CARDS	DATA1305
C	DATA1310
CALL READR(H,MAXNP,NNP)	DATA1315
C	DATA1320
C ***** DATA SET 12: INTEGERS CONTROLLING SOURCES AND B.C.	DATA1325
C	DATA1330
READ 10, NSEL,NSPR,NSDP, NWNP,NWPR,NWDP, NCES,NCNP,NCPR,NCDP,	DATA1335
1 NNES,NNNP,KNPR,NNDP, NVES,NVNP,NRPR,NRDP, NDNP,NDPR,NDDP	DATA1340
C	DATA1345
PRINT 5100, NSEL,NSPR,NSDP, NWNP,NWPR,NWDP	DATA1350
PRINT 5150, NCES,NCNP,NCPR,NCDP,NNES,NNNP,NNPR,NNDP,	DATA1355
1 NVES,NVNP,NRPR,NRDP, NDNP,NDPR,NDDP	DATA1360
C	DATA1365
C ***** DATA SET 13: SOURCE DATA	DATA1370
C	DATA1375
IF(NSEL.EQ.0) GO TO 560	DATA1380
PRINT 5300	DATA1385
DO 510 I=1,NSPR	DATA1390
READ 20, (TSOSF(J,I),SOSF(J,I),J-1,NSDP)	DATA1395
PRINT 5500, I	DATA1400
PRINT 5510, (TSOSF(J,I),SOSF(J,I),J-1,NSDP)	DATA1405
510 CONTINUE	DATA1410
C	DATA1415
C ----- READ SOURCE TYPE ASSIGNED TO EACH ELEMENT	DATA1420
C	DATA1425
READ 10, (MSEL(M),M-1,NSEL)	DATA1430
CALL READN(ISTYP,MXSEL,NSEL)	DATA1435
C	DATA1440
C ----- PRINT ELEMENT SOURCE/SINK PROFILES AND TYPE	DATA1445
C	DATA1450
LINE=0	DATA1455
DO 520 I=1,NSEL,5	DATA1460
LINE=LINE+1	DATA1465
IF(MOD(LINE-1,50).EQ.0) PRINT 5600	DATA1470
NJMN=I	DATA1475
NJMX=MINO(I+4,NSEL)	DATA1480
PRINT 5650, (J,MSEL(J),ISTYP(J),J-NJMN,NJMX)	DATA1485
520 CONTINUE	DATA1490

C		DATA1495
C	----- READ AND WRITE WELL SOURCE/SINK PROFILES	DATA1500
C		DATA1505
	560 IF(NWNP.EQ.0) GO TO 600	DATA1510
	PRINT 5700	DATA1515
	DO 570 I-1,NWPR	DATA1520
	READ 20, (TWSSF(J,I),WSSF(J,I),J-1,NWDP)	DATA1525
	PRINT 5710, I	DATA1530
	PRINT 5510, (TWSSF(J,I),WSSF(J,I),J-1,NWDP)	DATA1535
	570 CONTINUE	DATA1540
C		DATA1545
C	----- READ WELL SOURCE/SINK NODES AND TYPE OF PROFILES ASSIGNED TO	DATA1550
C	----- EACH OF NWNP NODES.	DATA1555
C		DATA1560
	READ 10, (NPW(I),I-1,NWNP)	DATA1565
	CALL READN(IWTYP,MXWNP,NWNP)	DATA1570
C		DATA1575
C	----- PRINT GLOBAL WELL NODE NUMBERS AND PROFILE TYPE OF WELL NODE	DATA1580
C		DATA1585
	LINE=0	DATA1590
	DO 590 I-1,NWNP,5	DATA1595
	LINE=LINE+1	DATA1600
	IF(MOD(LINE-1,50).EQ.0) PRINT 5800	DATA1605
	NJMN=I	DATA1610
	NJMX=MINO(I+4,NWNP)	DATA1615
	PRINT 5850, (J,NPW(J),IWTYP(J),J-NJMN,NJMX)	DATA1620
	590 CONTINUE	DATA1625
C		DATA1630
C	***** DATA SET 14: RAINFALL/EVAPORATION-SEEPAGE BOUNDARY CONDITIONS	DATA1635
C		DATA1640
	600 IF(NVES.EQ.0) GO TO 700	DATA1645
C		DATA1650
	PRINT 6000	DATA1655
C		DATA1660
C	----- READ AND WRITE RAINFALL (+)/EVAPORATION (-) PROFILES	DATA1665
C		DATA1670
	PRINT 6100	DATA1675
	DO 610 I-1,NRPR	DATA1680
	READ 20, (TRF(J,I),RF(J,I),J-1,NRDP)	DATA1685
	PRINT 6150, I	DATA1690
	PRINT 5510, (TRF(J,I),RF(J,I),J-1,NRDP)	DATA1695
	610 CONTINUE	DATA1700
C		DATA1705
C	----- READ RAINFALL/EVAPORATION TYPE ASSIGNED TO EACH RS SIDE	DATA1710
C		DATA1715
	CALL READN(IRTYP,MXVES,NVES)	DATA1720
C		DATA1725
C	----- READ FOUR GLOBAL NODE NUMBER FOR EACH OF ALL VARIABLE	DATA1730
C	----- BOUNDARY ELEMENT SIDES.	DATA1735
C		DATA1740

MPI=0	DATA1745
620 READ 10, MI, NSEQ, MIAD, I1, I2, I3, I4, I1AD, I2AD, I3AD, I4AD	DATA1750
IF(MI.EQ.0) GO TO 630	DATA1755
MJ=MI+NSEQ	DATA1760
DO 625 MP=MI, MJ	DATA1765
I=MI+(MP-MI)*MIAD	DATA1770
ISV(1, I)=I1+(MP-MI)*I1AD	DATA1775
ISV(2, I)=I2+(MP-MI)*I2AD	DATA1780
ISV(3, I)=I3+(MP-MI)*I3AD	DATA1785
ISV(4, I)=I4+(MP-MI)*I4AD	DATA1790
MPI=MPI+1	DATA1795
625 CONTINUE	DATA1800
GO TO 620	DATA1805
630 IF(MPI.EQ.NVES) GO TO 635	DATA1810
PRINT 6300	DATA1815
STOP	DATA1820
C	DATA1825
C ----- PRINT INPUTTED GLOBAL NODAL NUMBER AND RAINFALL TYPES OF ALL	DATA1830
C ----- VARIABLE BOUNDARY ELEMENT SIDES.	DATA1835
C	DATA1840
635 LINE=0	DATA1845
DO 640 MP=1, NVES, 3	DATA1850
LINE=LINE+1	DATA1855
IF(MOD(LINE-1, 50).EQ.0) PRINT 6400	DATA1860
NJMN=MP	DATA1865
NJMX=MINO(MP+2, NVES)	DATA1870
PRINT 6450, (J, (ISV(I, J), I=1, 4), IRTYP(J), J-NJMN, NJMX)	DATA1875
640 CONTINUE	DATA1880
C	DATA1885
C ----- READ GLOBAL NODAL NUMBER FOR EACH OF ALL VARIABLE NODES.	DATA1890
C	DATA1895
CALL READN(NPVB, MXVNP, NVNP)	DATA1900
C	DATA1905
C ----- READ PONDING DEPTH AND MINIMUM HEAD FOR EACH OF ALL RS NODES	DATA1910
C	DATA1915
CALL READR(HCON, MXVNP, NVNP)	DATA1920
CALL READR(HMIN, MXVNP, NVNP)	DATA1925
C	DATA1930
C ----- PRINT GLOBAL NODAL NUMBER, PONDING DEPTH AND MINIMUM PRESURE	DATA1935
C ----- RESSURE HEAD FOR ALL VARIABLE BOUNDARY NODES	DATA1940
C	DATA1945
LINE=0	DATA1950
DO 645 I=1, NVNP, 3	DATA1955
LINE=LINE+1	DATA1960
IF(MOD(LINE-1, 50).EQ.0) PRINT 6500	DATA1965
NJMN=I	DATA1970
NJMX=MING(I+2, NVNP)	DATA1975
PRINT 6550, (J, NPVB(J), HCON(J), HMIN(J), J-NJMN, NJMX)	DATA1980
645 CONTINUE	DATA1985

C		DATA1990
C	----- COMPUTE BOUNDARY SIDE NUMBER FOR EACH OF ALL VARIABLE	DATA1995
C	----- BOUNDARY SIDES.	DATA2000
C		DATA2005
	DO 659 MI-1,NVES	DATA2010
	DO 651 IQ-1,4	DATA2015
	651 NIMI(IQ)-ISV(IQ,MI)	DATA2020
C		DATA2025
	DO 657 MJ-1,NBES	DATA2030
	DO 652 JQ-1,4	DATA2035
	IJ-ISB(JQ,MJ)	DATA2040
	652 NVMJ(JQ)-NPBB(IJ)	DATA2045
	IEQ-0	DATA2050
	DO 656 IQ-1,4	DATA2055
	NI-NIMI(IQ)	DATA2060
	DO 653 JQ-1,4	DATA2065
	NJ-NVMJ(JQ)	DATA2070
	IF(NJ.EQ.NI) GO TO 655	DATA2075
	653 CONTINUE	DATA2080
	GO TO 657	DATA2085
	655 IEQ-IEQ+1	DATA2090
	656 CONTINUE	DATA2095
	IF(IEQ.EQ.4) GO TO 658	DATA2100
	657 CONTINUE	DATA2105
C		DATA2110
	PRINT 6570, MI	DATA2115
	STOP	DATA2120
	658 ISV(5,MI)-MJ	DATA2125
C		DATA2130
	659 CONTINUE	DATA2135
C		DATA2140
C	----- CHANGE NPVB FROM CONTAINING GLOBAL NODAL NUMBER TO	DATA2145
C	----- CONTAINING BOUNDARY NODAL NUMBER.	DATA2150
C		DATA2155
	DO 669 NP-1,NVNP	DATA2160
	NI-NPVB(NP)	DATA2165
C		DATA2170
	DO 665 I-1,NBNP	DATA2175
	NJ-NPBB(I)	DATA2180
	IF(NJ.NE.NI) GO TO 665	DATA2185
	NII-I	DATA2190
	GO TO 667	DATA2195
	665 CONTINUE	DATA2200
C		DATA2205
	PRINT 6670, NP	DATA2210
	STOP	DATA2215
	667 NPVB(NP)-NII	DATA2220
C		DATA2225
	669 CONTINUE	DATA2230

C		DATA2235
C	----- PRINT COMPUTED BOUNDARY NODAL NUMBER FOR ALL VB NODES	DATA2240
C		DATA2245
	LINE=0	DATA2250
	DO 670 I=1,NVNP,10	DATA2255
	LINE=LINE+1	DATA2260
	IF(MOD(LINE-1,50).EQ.0) PRINT 6700	DATA2265
	NJMN=I	DATA2270
	NJMX=MINO(I+9,NVNP)	DATA2275
	PRINT 6750, (J,NPVB(J),J-NJMN,NJMX)	DATA2280
	670 CONTINUE	DATA2285
C		DATA2290
C	----- CHANGE ISV(I,MP) I=1,4 FROM CONTAINING GLOBAL NODAL	DATA2295
C	----- NUMBER TO CONTAINING BOUNDARY NODAL NUMBER.	DATA2300
C		DATA2305
	DO 690 MP=1,NVES	DATA2310
	MPB=ISV(5,MP)	DATA2315
	DO 685 IQ=1,4	DATA2320
	NB=ISB(IQ,MPB)	DATA2325
	DO 675 I=1,NVNP	DATA2330
	NI=NPVB(I)	DATA2335
	IF(NI.NE.NB) GO TO 675	DATA2340
	NII=I	DATA2345
	GO TO 680	DATA2350
	675 CONTINUE	DATA2355
	PRINT 6751, IQ,MP	DATA2360
	STOP	DATA2365
	680 ISV(IQ,MP)=NII	DATA2370
	685 CONTINUE	DATA2375
	690 CONTINUE	DATA2380
C		DATA2385
C	----- PRINT COMPUTED BOUNDARY NODAL NUMBER & SIDE NUMBER AND	DATA2390
C	----- RAINFALL TYPES FOR ALL VB SIDES	DATA2395
C		DATA2400
	LINE=0	DATA2405
	DO 695 MP=1,NVES,3	DATA2410
	LINE=LINE+1	DATA2415
	IF(MOD(LINE-1,50).EQ.0) PRINT 6900	DATA2420
	NJMN=MP	DATA2425
	NJMX=MINO(MP+2,NVES)	DATA2430
	PRINT 6950, (J,(ISV(I,J),I=1,5),IRTYPE(I),J-NJMN,NJMX)	DATA2435
	695 CONTINUE	DATA2440
C		DATA2445
C	***** DATA SET 15: DIRICHLET BOUNDARY CONDITIONS	DATA2450
C		DATA2455
C	----- READ AND PRINT TOTAL DIRICHLET HEAD PROFILES	DATA2460
C		DATA2465
	700 IF(NDNP.EQ.0) GO TO 800	DATA2470
	PRINT 7000	DATA2475
	DO 710 I=1,NDPR	DATA2480

READ 20, (THDBF(J,I),HDBF(J,I),J-1,NDDP)	DATA2485
PRINT 7100, I	DATA2490
PRINT 5510, (THDBF(J,I),HDBF(J,I),J-1,NDDP)	DATA2495
710 CONTINUE	DATA2500
C	DATA2505
C ----- READ GLOBAL NODAL NUMBER OF ALL DIRICHLET NODES AND	DATA2510
C ----- THE TYPE OF TOTAL HEAD ASSIGNED TO EACH OF THEM.	DATA2515
C	DATA2520
READ 10, (NPDB(I),I-1,NDNP)	DATA2525
CALL READN(IDTYP,MXDNP,NDNP)	DATA2530
C	DATA2535
C ----- PRINT GLOBAL NODAL NUMBER AND PROFILE OF DIRICHLET NODES	DATA2540
C	DATA2545
LINE=0	DATA2550
DO 720 I=1,NDNP,5	DATA2555
LINE=LINE+1	DATA2560
IF(MOD(LINE-1,50).EQ.0) PRINT 7200	DATA2565
NJMN=I	DATA2570
NJMX=MINO(I+4,NDNP)	DATA2575
PRINT 7250, (J,NPDB(J),IDTYP(J),J-NJMN,NJMX)	DATA2580
720 CONTINUE	DATA2585
C	DATA2590
C ----- CHANGE NPDB FROM CONTAINING GLOBAL NODAL NUMBER TO	DATA2595
C ----- CONTAINING BOUNDARY NODAL NUMBER.	DATA2600
C	DATA2605
DO 769 NP=1,NDNP	DATA2610
NI=NPDB(NP)	DATA2615
C	DATA2620
DO 765 I=1,NBNP	DATA2625
NJ=NPBB(I)	DATA2630
IF(NJ.NE.NI) GO TO 765	DATA2635
NII=I	DATA2640
GO TO 767	DATA2645
765 CONTINUE	DATA2650
C	DATA2655
PRINT 7670, NF	DATA2660
STOP	DATA2665
767 NPDB(NP)=NII	DATA2670
C	DATA2675
769 CONTINUE	DATA2680
C	DATA2685
C ----- PRINT COMPUTED BOUNDARY NODAL NUMBER AND TYPE OF PROFILES	DATA2690
C ----- FOR DIRICHLET BOUNDARY NODES	DATA2695
C	DATA2700
LINE=0	DATA2705
DO 770 I=1,NDNP,5	DATA2710
LINE=LINE+1	DATA2715
IF(MOD(LINE-1,50).EQ.0) PRINT 7700	DATA2720
NJMN=I	DATA2725
NJMX=MINO(I+4,NDNP)	DATA2730

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PRINT 7750, (J,NPLB(J),IDTYP(J),J-NJMN,NJMX)
770 CONTINUE
C
C ***** DATA SET 16: CAUCHY BOUNDARY CONDITIONS
C
C ----- READ AND PRINT CAUCHY FLUX PROFILES
C
C 800 IF(NCES.EQ.0) GO TO 900
PRINT 8000
DO 810 I=1,NCPR
READ 20, (TQCBF(J,I),QCBF(J,I),J-1,NCDP)
PRINT 8100, I
PRINT 5510, (TQCBF(J,I),QCBF(J,I),J-1,NCDP)
810 CONTINUE
C
C ----- READ CAUCHY FLUX TYPE ASSIGNED TO EACH CAUCHY SIDE
C
CALL READN(ICTYP,MXCES,NCES)
C
C ----- READ FOUR GLOBAL NODE NUMBER FOR EACH OF ALL CAUCHY SIDES
C
MPI=0
820 READ 10, MI,NSEQ,MIAD,11,12,13,14,I1AD,I2AD,I3AD,I4AD
IF(MI.EQ.0) GO TO 830
MJ=MI+NSEQ
DO 825 MP=MI,MJ
I=MI+(MP-MI)*MIAD
ISC(1,I)=I1+(MP-MI)*I1AD
ISC(2,I)=I2+(MP-MI)*I2AD
ISC(3,I)=I3+(MP-MI)*I3AD
ISC(4,I)=I4+(MP-MI)*I4AD
MPI=MPI+1
825 CONTINUE
GO TO 820
830 IF(MPI.EQ.NCES) GO TO 835
PRINT 8300
STOP
C
C ----- PRINT INPUTTED GLOBAL NODAL NUMBER AND CAUCHY FLUX TYPES
C ----- FOR ALL CAUCHY BOUNDARY ELEMENT SIDES.
C
835 LINE=0
DO 840 MP=1,NCES,3
LINE=LINE+1
IF(MOD(LINE-1,50).EQ.0) PRINT 8400
NJMN=MP
NJMX=MINO(MP+2,NCES)
PRINT 8450, (J,(ISC(I,J),I=1,4),ICTYP(J),J-NJMN,NJMX)
840 CONTINUE

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DATA2735
DATA2740
DATA2745
DATA2750
DATA2755
DATA2760
DATA2765
DATA2770
DATA2775
DATA2780
DATA2785
DATA2790
DATA2795
DATA2800
DATA2805
DATA2810
DATA2815
DATA2820
DATA2825
DATA2830
DATA2835
DATA2840
DATA2845
DATA2850
DATA2855
DATA2860
DATA2865
DATA2870
DATA2875
DATA2880
DATA2885
DATA2890
DATA2895
DATA2900
DATA2905
DATA2910
DATA2915
DATA2920
DATA2925
DATA2930
DATA2935
DATA2940
DATA2945
DATA2950
DATA2955
DATA2960
DATA2965
DATA2970
DATA2975

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C		DATA2980
C	----- READ GLOBAL NODAL NUMBER FOR EACH OF ALL CAUCHY NODES.	DATA2985
C		DATA2990
	READ 10, (NPCB(I),I-1,NCNP)	DATA2995
C		DATA3000
C	----- PRINT GLOBAL NODAL NUMBER FOR ALL CAUCHY NODES	DATA3005
C		DATA3010
	LINE=0	DATA3015
	DO 845 I=1,NCNP,10	DATA3020
	LINE=LINE+1	DATA3025
	IF(MOD(LINE-1,50).EQ.0) PRINT 8500	DATA3030
	NJMN=I	DATA3035
	NJMX=MINO(I+9,NCNP)	DATA3040
	PRINT 8550, (J,NPCB(J),J-NJMN,NJMX)	DATA3045
	845 CONTINUE	DATA3050
C		DATA3055
C	----- COMPUTE BOUNDARY SIDE NUMBER FOR ALL CAUSHY SIDES	DATA3060
C		DATA3065
	DO 859 MI=1,NCES	DATA3070
	DO 851 IQ=1,4	DATA3075
	851 NIMI(IQ)=ISC(IQ,MI)	DATA3080
C		DATA3085
	DO 857 MJ=1,NBES	DATA3090
	DO 852 JQ=1,4	DATA3095
	IJ=ISB(JQ,MJ)	DATA3100
	852 NJMJ(JQ)=NPBB(IJ)	DATA3105
	IEQ=0	DATA3110
	DO 856 IQ=1,4	DATA3115
	NI=NIMI(IQ)	DATA3120
	DO 853 JQ=1,4	DATA3125
	NJ=NJMJ(JQ)	DATA3130
	IF(NJ.EQ.NI) GO TO 855	DATA3135
	853 CONTINUE	DATA3140
	GO TO 857	DATA3145
	855 IEQ=IEQ+1	DATA3150
	856 CONTINUE	DATA3155
	IF(IEQ.EQ.4) GO TO 858	DATA3160
	857 CONTINUE	DATA3165
C		DATA3170
	PRINT 8570, MI	DATA3175
	STOP	DATA3180
	858 ISC(5,MI)=MJ	DATA3185
C		DATA3190
	859 CONTINUE	DATA3195
C		DATA3200
C	----- CHANGE NPCB FROM CONTAINING GLOBAL NODAL NUMBER TO	DATA3205
C	----- CONTAINING BOUNDARY NODAL NUMBER.	DATA3210
C		DATA3215
	DO 869 NP=1,NCNP	DATA3220
	NI=NPCB(NP)	DATA3225

C	DO 865 I=1,NBNP	DATA3230
	NJ=NPBB(I)	DATA3235
	IF(NJ.NE.NI) GO TO 865	DATA3240
	NII=I	DATA3245
	GO TO 867	DATA3250
	865 CONTINUE	DATA3255
C	PRINT 8670, NP	DATA3260
	STOP	DATA3265
	867 NPCB(NP)=NII	DATA3270
C	869 CONTINUE	DATA3275
C	----- PRINT COMPUTED BOUNDARY NODAL NUMBER FOR ALL CAUCHY NODES	DATA3280
C	LINE=0	DATA3285
	DO 870 I=1,NCNF 10	DATA3290
	LINE=LINE+1	DATA3295
	IF(MOD(LINE-1,50).EQ.0) PRINT 8700	DATA3300
	NJMN=I	DATA3305
	NJMX=MINO(I+9,NCNP)	DATA3310
	PRINT 8750, (J,NPCB(J),J-NJMN,NJMX)	DATA3315
	870 CONTINUE	DATA3320
C	***** DATA SET 17: NEUMANN BOUNDARY CONDITIONS	DATA3325
C	----- READ AND PRINT NEUMANN FLUX PROFILES	DATA3330
C	900 IF(NNES.EQ.0) GO TO 999	DATA3335
	PRINT 9000	DATA3340
	DO 910 I=1,NNPR	DATA3345
	READ 20, (TQNB(F(J,I),QNB(F(J,I),J=1,NNDP)	DATA3350
	PRINT 9100, I	DATA3355
	PRINT 5510, (TQNB(F(J,I),QNB(F(J,I),J=1,NNDP)	DATA3360
	910 CONTINUE	DATA3365
C	----- READ NEUMANN FLUX TYPE ASSIGNED TO EACH NEUMANN SIDE	DATA3370
C	CALL READN(INTYP,MXNES,NNES)	DATA3375
C	----- READ FOUR GLOBAL NODE NUMBER FOR EACH OF ALL NEUMANN SIDES	DATA3380
C	MPI=0	DATA3385
	920 READ 10, MI,NSEQ,MIAD,I1,I2,I3,I4,I1AD,I2AD,I3AD,I4AD	DATA3390
	IF(MI.EQ.0) GO TO 930	DATA3395
	MJ=MI+NSEQ	DATA3400
	DO 925 MP=MI,MJ	DATA3405
	I=MI+(MP-MI)*MIAD	DATA3410
	ISN(I,I)=I1+(MP-MI)*I1AD	DATA3415
		DATA3420
		DATA3425
		DATA3430
		DATA3435
		DATA3440
		DATA3445
		DATA3450
		DATA3455
		DATA3460
		DATA3465
		DATA3470
		DATA3475

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      ISN(2,1)=I2+(MP-MI)*I2AD
      ISN(3,1)=I3+(MP-MI)*I3AD
      ISN(4,1)=I4+(MP-MI)*I4AD
      MPI=MPI+1
925 CONTINUE
      GO TO 920
930 IF(MPI.EQ.NNES) GO TO 935
      PRINT 9300
      STOP
C
C ----- PRINT INPUTTED GLOBAL NODAL NUMBER AND NEUMANN FLUX TYPES
C ----- FOR ALL NEUMANN BOUNDARY ELEMENT SIDES.
C
935 LINE=0
      DO 940 MP=1,NNES,3
      LINE=LINE+1
      IF(MOD(LINE-1,50).EQ.0) PRINT 9400
      NJMN=MP
      NJMX=MINO(MP+2,NNES)
      PRINT 9450, (J,(ISN(I,J),I=1,4),INTYP(J),J-NJMN,NJMX)
940 CONTINUE
C
C ----- READ GLOBAL NODAL NUMBER FOR EACH OF ALL NEUMANN NODES.
C
      READ 10, (NPNB(I),I=1,NNNP)
C
C ----- PRINT GLOBAL NODAL NUMBER FOR ALL NEUMANN NODES
C
      LINE=0
      DO 945 I=1,NNNP,10
      LINE=LINE+1
      IF(MOD(LINE-1,50).EQ.0) PRINT 9500
      NJMN=I
      NJMX=MINO(I+9,NNNP)
      PRINT 9550, (J,NPNB(J),J-NJMN,NJMX)
945 CONTINUE
C
C ----- COMPUTE BOUNDARY SIDE NUMBER FOR EACH OF NEUMANN
C ----- BOUNDARY SIDES.
C
      DO 959 MI=1,NNES
      DO 951 IQ=1,4
951 NIMI(IQ)=ISN(IQ,MI)
C
      DO 957 MJ=1,NBES
      DO 952 JQ=1,4
      IJ=ISB(JQ,MJ)
952 NJMJ(JQ)=NPBB(IJ)
      IEQ=0
      DO 956 IQ=1,4

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DATA3480
 DATA3485
 DATA3490
 DATA3495
 DATA3500
 DATA3505
 DATA3510
 DATA3515
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 DATA3685
 DATA3690
 DATA3695
 DATA3700
 DATA3705
 DATA3710
 DATA3715
 DATA3720
 DATA3725

NI=NIMI(IQ)	DATA3730
DO 953 JQ-1,4	DATA3735
NJ=NJM(JQ)	DATA3740
IF(NJ.EQ.NI) GO TO 955	DATA3745
953 CONTINUE	DATA3750
GO TO 957	DATA3755
955 IEQ-IEQ+1	DATA3760
956 CONTINUE	DATA3765
IF(IEQ.EQ.4) GO TO 958	DATA3770
957 CONTINUE	DATA3775
C	DATA3780
PRINT 9570, MI	DATA3785
STOP	DATA3790
958 ISN(5,MI)-MJ	DATA3795
C	DATA3800
959 CONTINUE	DATA3805
C	DATA3810
C ----- CHANGE NPNB FROM CONTAINING GLOBAL NODAL NUMBER TO	DATA3815
C ----- CONTAINING BOUNDARY NODAL NUMBER.	DATA3820
C	DATA3825
DO 969 NP-1,NNNP	DATA3830
NI-NPNB(NP)	DATA3835
C	DATA3840
DO 965 I-1,NBNP	DATA3845
NJ-NPBB(I)	DATA3850
IF(NJ.NE.NI) GO TO 965	DATA3855
NII-I	DATA3860
GO TO 967	DATA3865
965 CONTINUE	DATA3870
C	DATA3875
PRINT 9670, NP	DATA3880
STOP	DATA3885
967 NPNB(NP)-NII	DATA3890
C	DATA3895
969 CONTINUE	DATA3900
C	DATA3905
C ----- PRINT COMPUTED BOUNDARY NODAL NUMBER FOR ALL NEUMANN NODES	DATA3910
C	DATA3915
LINE=0	DATA3920
DO 970 I-1,NNNP,10	DATA3925
LINE=LINE+1	DATA3930
IF(MOD(LINE-1,50).EQ.0) PRINT 9700	DATA3935
NJMN-I	DATA3940
NJMX-MINO(I+9,NNNP)	DATA3945
PRINT 9750, (J,NPNB(J),J-NJMN,NJMX)	DATA3950
970 CONTINUE	DATA3955
C	DATA3960
999 CONTINUE	DATA3965
C	DATA3970
RETURN	DATA3975

C	10	FORMAT(16I5)	DATA3980
	20	FORMAT(8D10.3)	DATA3985
	30	FORMAT(80I1)	DATA3990
	40	FORMAT(3I5,5X,6D10.3)	DATA3995
C	1000	FORMAT(40H0 **** BAISC INTEGEK PARAMETERS ****//5X,	DATA4000
	1	40H NUMBEF. OF NODAL POINTS.,I5/ 5X,	DATA4005
	2	40H NUMBER OF ELEMENTS.,I5/ 5X,	DATA4010
	3	40H NUMBER OF DIFFERENT MATERIALS,I5/ 5X,	DATA4015
	4	40H NUMBER OF CORRECTION MATERIALS.,I5/ 5X,	DATA4020
	5	40H NUMBER OF TIME INCREMENTS,I5//5X,	DATA4025
	6	40H STEADY-STATE I.C. CONTROL,I5/ 5X,	DATA4030
	8	40H NUMBER OF SOIL PARAMETERS,I5/ 5X,	DATA4035
	9	40H NUMBER OF MATERIAL PROPERTIES,I5//5X,	DATA4040
	A	40H AUXILIARY STORAGE CONTROL,I5/ 5X,	DATA4045
	B	40H CONDUCTIVITY-PERMEABILITY CONTROL,I5/ 5X,	DATA4050
	C	40H GRAVITY CONTROL,I5/ 5X,	DATA4055
	E	40H NO. OF ITERATIONS PER CYCLE,I5/ 5X,	DATA4060
	F	40H NO. OF CYCLES PER TIME STEP,I5/ 5X,	DATA4065
	G	40H NO. OF TIMES TO RESET TIME STEP SIZE .,I5/ 5X,	DATA4070
	H	40H NO. OF BLOCKWISE ITERATIONS ALLOWED . ,I5/ 5X,	DATA4075
	I	40H NO. OF SUBREGIONS,I5/)	DATA4080
	1100	FORMAT(5X,40H TIME INCREMENT.,E15.6/ 5X,	DATA4085
	1	40H MULTIPLIER FOR INCREASING DELT.,E15.6/ 5X,	DATA4090
	2	40H MAXIMUM VALUE OF DELT,E15.6/ 5X,	DATA4095
	3	40H MAXIMUM VALUE OF TIME,E15.6//5X,	DATA4100
	5	40H STEADY-STATE TOLERANCE.,E15.6/ 5X,	DATA4105
	6	40H TRANSIENT-STATE TOLERANCE,E15.6//5X,	DATA4110
	7	40H DENSITY OF WATER.,E15.6/ 5X,	DATA4115
	8	40H ACCELERATION OF GRAVITY,E15.6/ 5X,	DATA4120
	9	40H VISCOSITY OF WATER.,E15.6//5X,	DATA4125
	A	40H TIME-INTEGRATION PARAMETER.,E15.6/ 5X,	DATA4130
	B	40H ITERATION PARAMETER FOR NONLINEAR EQ. ,E15.6/ 5X,	DATA4135
	C	40H RELAXATION PARAMETER FOR POINTWISE SOL.,E15.6//)	DATA4140
	1200	FORMAT(//6X,14HOUTPUT CONTROL)	DATA4145
	1210	FORMAT(10X,50I2)	DATA4150
	1300	FORMAT(//6X,19HDISK OUTPUT CONTROL)	DATA4155
	1350	FORMAT(1H0,6X,'TIME OF CHANGING DELT'/(10X,8D12.4))	DATA4160
	1400	FORMAT(36H1 **** MATERIAL PROPERTIES **** // 9H MAT. NO., 9(> 3A4))	DATA4165
	1410	FORMAT(18,9D12.4)	DATA4170
	1500	FORMAT(44H1INPUT TABLE 3. MOISTURE-CONTENT PARAMETERS// > 9H MAT. NO.,8(3A4))	DATA4175
	1510	FORMAT(18,9D12.4/(8X,9D12.4))	DATA4180
	1600	FORMAT(40H1 **** CONDUCTIVITY PARAMETERS **** // 9H MAT. NO., > 8(3A4))	DATA4185
	2000	FORMAT(1H0/5X,'*** ERROR IN READING COORDINATE STOP ***'/)	DATA4190
			DATA4195
			DATA4200
			DATA4205
			DATA4210
			DATA4215

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2100 FORMAT(38H1      **** NODAL COORDINATE DATA **** //1X,          DATA4220
      > 3(1X,5H NODE,11H   X   ,11H   Y   ,11H   Z   ,1X)/1X,DATA4225
      > 3(1X,5H ****,33H ***** ***** ***** ,1X))          DATA4230
2110 FORMAT(1H ,3(1X,15,3D11.3,1X))          DATA4235
2200 FORMAT(1H1/5X,25H *** OUTPUT GNL(R,I,K) ***          DATA4240
2210 FORMAT(1H0,5X,26H ---- SUBREGION NUMBER K -,14/(6X,10I5))          DATA4245
2700 FORMAT(62H1      **** ELEMENT DATA: GLOBAL INDICES OF ELEMENT NODES DATA4250
      1 **** //2(5X,5H ELM,5H NOD1,5H NOD2,5H NOD3,5H NOD4,5H NOD5,          DATA4255
      2 5H NOD6,5H NOD7,5H NOD8,5H MTYP)/2(5X,5H ---,5H ----,5H ----,          DATA4260
      3 5H ----,5H ----,5H ----,5H ----,5H ----,5H ----,5H ----))          DATA4265
3000 FORMAT(////'ERROR IN READING IE, MMP -,15,' NEL -,15,' STOP')          DATA4270
3100 FORMAT(2(5X,10I5))          DATA4275
4200 FORMAT(////40H ERROR IN MATERIAL TYPE CODE FOR ELEMENT,15////)          DATA4280
4300 FC3MAT(////28H EXECUTION HALTED BECAUSE OF,15,13H FATAL ERRORS////)DATA4285
5100 FORMAT('1      **** TRANSIENT INTEGERS **** '// 5X,          DATA4290
      1 ' NO. OF SOURCE ELEMENTS . . . . .',15/ 5X,          DATA4295
      2 ' NO. OF SOURCE PROFILES . . . . .',15/ 5X,          DATA4300
      3 ' NO. OF DATA POINTS FOR EACH SOURCE PROF',15/ 5X,          DATA4305
      4 ' NO. OF WELL SOURCES/SINKS NODES . . . . .',15/ 5X,          DATA4310
      5 ' NO. OF WELL SOURCE PROFILES . . . . .',15/ 5X,          DATA4315
      6 ' NO. OF DATA POINTS IN EACH WELL PROF. .',15/)          DATA4320
5150 FORMAT(1H /5X,          DATA4325
      1 40H NO. OF CAUCHY SIDES . . . . .,15/ 5X,          DATA4330
      2 40H NO. OF CAUCHY NODES . . . . .,15/ 5X,          DATA4335
      3 40H NO. OF CAUCHY FLUX PROFILES . . . . .,15/ 5X,          DATA4340
      4 40H NO. OF DATA POINTS IN EACH CAUCHY PROF.,15/ 5X,          DATA4345
      5 40H NO. OF NEUMANN SIDES . . . . .,15/ 5X,          DATA4350
      6 40H NO. OF NEUMANN NODES . . . . .,15/ 5X,          DATA4355
      7 40H NO. OF NEUMANN FLUXES . . . . .,15/ 5X,          DATA4360
      8 40H NO. OF DATA POINTS IN NEUMANN PROF. . .,15/ 5X,          DATA4365
      9 40H NO. OF VARIABLE BOUNDARY SIDES. . . . .,15/ 5X,          DATA4370
      A 40H NO. OF VARIABLE BOUNDARY NODES. . . . .,15/ 5X,          DATA4375
      B 40H NO. OF RAINFALL PROFILES . . . . .,15/ 5X,          DATA4380
      C 40H NO. OF DATA POINTS IN RAINFALL PROF. .,15/ 5X,          DATA4385
      D 40H NO. OF DIRICHLET NODES . . . . .,15/ 5X,          DATA4390
      E 40H NO. OF DIRICHLET TOTAL HEAD PROF. . . .,15/ 5X,          DATA4395
      F 40H NO. OF DATA POINTS IN DIRICHLET PROF. .,15/)          DATA4400
5300 FORMAT(1H1/5X,27H *** SOURCE INFORMATION ***          DATA4405
5500 FORMAT(1H0/5X,12H PROFILE NO.,12,/ 5(4X,4HTIME,6X,6HSOURCE,2X)/          DATA4410
      > 5(4X,4H----,6X,6H-----,2X))          DATA4415
5510 FORMAT(1H .5(2D11.3))          DATA4420
5600 FORMAT(1H0//10X,65H ELEMENT NUMBER AND PROFILE TYPES OF ELEMENT          DATA4425
      1 //5X,5(5H I,5H MSEL,5H STYP,5X))          DATA4430
5650 FORMAT(1H ,4X,5(3I5,5X))          DATA4435
5700 FORMAT(1H0//5X,37H *** WELL SOURCE/SINK INFORMATION ***          DATA4440
5710 FORMAT(1H0/5X,12H PROFILE NO.,12/ 4(4X,4HTIME,6X,6HSOURCE,2X)/          DATA4445
      1 4(4X,4H----,6X,6H-----,2X))          DATA4450
5800 FORMAT(1H0//10X,65H GLOBAL NODAL NUMBER AND PROFILE TYPE OF WELLS          DATA4455
      1OUCE/SINK NODES //5X,5(5H I,5H NPW,5H WTYP,5X))          DATA4460

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5850 FORMAT(1H ,4X,5(3I5,5X)) DATA4465
6000 FORMAT(1H1/5X,46H **** RAINFALL-SEEPAGE BOUNDARY CONDITIONS ***) DATA4470
6100 FORMAT(1H0///10X,25H --- RAINFALL PROFILE ---) DATA4475
6150 FORMAT(1H0/5X,12H PROFILE NO. ,I2,///5(4X,4H TIME,6X,6H RAINS,2X)/ DATA4480
  > 5(4X,4H----,6X,6H-----,2X)) DATA4485
6300 FORMAT(1H0,10X,61H *** ERROR IN READING RAINFALL-SEEPAGE ELEMENT DATA4490
  1SIDE STOP ***) DATA4495
6400 FORMAT(1H0/10X,36H --- INPUTTED VARIABLE SIDE DATA ---//5X, DATA4500
  2 3(5H MP,5H GN1,5H GN2,5H GN3,5H GN4,5H RTYP,5X)/5X, DATA4505
  3 3(30H -- --- --- --- --- ---,5X)) DATA4510
6450 FORMAT(1H ,4X,3(6I5,5X)) DATA4515
6500 FORMAT(1H0/10X,36H --- INPUTTED VARIABLE NODE DATA ---//1X, DATA4520
  1 3(1X,5H I,5H NPVB,12H HCON ,12H HMIN ,1X)/1X, DATA4525
  2 3(1X,5H --,5H ----,12H ---- ,12F ---- ,1X)) DATA4530
6550 FORMAT(1H ,3(1X,2I5,2D12.4,1X)) DATA4535
6570 FORMAT(1H1/5X,44H CANNOT FIND A BOUNDARY SIDE COINCIDING WITH, DATA4540
  1 I3,36H-TH VARIABLE BOUNDARY SIDE: STOP ***) DATA4545
6670 FORMAT(1H1/5X,44H *** CANNOT FIND A BOUNDARY NODAL NUMBER FOR, DATA4550
  1 I3,31H-TH VARIABLE BOUNDARY NODE STOP) DATA4555
6700 FORMAT(1H0//10X,47H COMPUTED BOUNDARY NODAL NUMBER OF ALL VB NODES DATA4560
  1 //5X,10(5H I,5H NPVB,2X)/5X,10(5H --,5H ----,2X)) DATA4565
6750 FORMAT(1H ,4X,10(2I5,2X)) DATA4570
6751 FORMAT(1H0,5X,42H *** CAN NOT FIND A COMPRESSED RS NODE FOR, DATA4575
  1 I2,12H-TH POINT OF, I4,20H-TH RS SIDE STOP ***) DATA4580
6900 FORMAT(1H0/10X,30H --- COMPUTED VB SIDE DATA ---,//1X, DATA4585
  1 3(5H MP,5H CNP1,5H CNP2,5H CNP3,5H CNP4,5H MPB,5H RTYP,1X)/1X, DATA4590
  2 3(5H --,5H ----,5H ----,5H ----,5H ----,5H ----,5H ----,1X)) DATA4595
6950 FORMAT(1H ,3(7I5,1X)) DATA4600
7000 FORMAT(1H1/5X,40H **** DIRICHLET BOUNDARY CONDITIONS ****) DATA4605
7100 FORMAT(1H0/5X,12H PROFILE NO. ,I2,/ 4(4X,4H TIME,6X,6H HEAD ,2X)/ DATA4610
  > 4(4X,4H----,6X,6H ---- ,2X)) DATA4615
7200 FORMAT(1H0//10X,65H GLOBAL NODAL NUMBER AND PROFILE TYPE OF DIRICH DATA4620
  1LET BOUNDARY NODES//5X,5(5H I,5H NPDB,5H TYPE,5X)/ DATA4625
  1 5X,5(5H --,5H ----,5H ----,5X)) DATA4630
7250 FORMAT(1H ,4X,5(3I5,5X)) DATA4635
7670 FORMAT(1H1/5X,44H *** CANNOT FIND A BOUNDARY NODAL NUMBER FOR, DATA4640
  1 I3,32H-TH DIRICHLET BOUNDARY NODE STOP) DATA4645
7700 FORMAT(1H0//10X,66H COMPUTED BOUNDARY NODAL NUMBER & TYPE OF DIRIC DATA4650
  1HLET BOUNDARY NODES//5X,5(5H I,5H NPDB,5H TYPE,5X)/ DATA4655
  1 5X,5(5H --,5H ----,5H ----,5X)) DATA4660
7750 FORMAT(1H ,4X,5(3I5,5X)) DATA4665
8000 FORMAT(1H1/5X,38H **** CAUCHY BOUNDARY CONDITIONS ****) DATA4670
8100 FORMAT(1H0/5X,12H PROFILE NO. ,I2/ 4(4X,4H TIME,6X,6H FLUX ,2X)/ DATA4675
  > 4(4X,4H----,6X,6H ---- ,2X)) DATA4680
8300 FORMAT(1H0,10X,61H *** ERROR IN READING CAUCHY BOUNDARY ELEMEN DATA4685
  1T SIDE STOP *) DATA4690
8400 FORMAT(1H0/10X,34H --- INPUTTED CAUCHY SIDE DATA ---//5X, DATA4695
  1 3(5H MP,5H GN1,5H GN2,5H GN3,5H GN4,5H CTYP,5X)/5X, DATA4700
  3 3(30H -- --- --- --- --- ---,5X)) DATA4705
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8450	FORMAT(1H ,4X,3(6I5,5X))	DATA4710
8500	FORMAT(1H0/10X,34H --- INPUTTED CAUCHY NODE DATA ---//5X, 1 10(5H I,5H NPCB,2X)/5X,10(5H -.5H ----,2X))	DATA4715
8550	FORMAT(1H ,4X,10(2I5,2X))	DATA4720
8570	FORMAT(1H1/5X,44H CANNOT FIND A BOUNDARY SIDE COINCIDING WITH, 1 I3,36H-TH CAUCY BOUNDARY SIDE: STOP ***)	DATA4725
8670	FORMAT(1H1/5X,44H *** CANNOT FIND A BOUNDARY NODAL NUMBER FOR, 1 I3,31H-TH CAUCHY BOUNDARY NODE: STOP)	DATA4730
8700	FORMAT(1H0/10X,34H --- COMPUTED CAUCHY NODE DATA ---//5X, 1 10(5H I,5H NPCB,2X)/5X,10(5H -.5H ----,2X))	DATA4735
8750	FORMAT(1H ,4X,10(2I5,2X))	DATA4740
9000	FORMAT(1H1/5X,38H **** NEUMANN BOUNDARY CONDITIONS ****)	DATA4745
9100	FORMAT(1H0/5X,12H PROFILE NO.,I2/ 4(4X,4HTIME,6X,6H FLUX ,2X)/ > 4(4X,4H----,6X,6H ---- ,2X))	DATA4750
9300	FORMAT(1H0,10X,61H *** ERROR IF READING NEUMANN BOUNDARY ELEMEN >T SIDE STOP *)	DATA4755
9400	FORMAT(1H0/10X,35H --- INPUTTED NEUMANN SIDE DATA ---//5X, 1 3(5H MP,5H GN1,5H GN2,5H GN3,5H GN4,5H NTYP,5X)/5X, 2 3(30H -- --- --- --- --- ---,5X))	DATA4760
9450	FORMAT(1H ,4X,3(6I5,5X))	DATA4765
9500	FORMAT(1H0/10X,35H --- INPUTTED NEUMANN NODE DATA ---//5X, 1 10(5H I,5H NPNB,2X)/5X,10(5H -.5H ----,2X))	DATA4770
9550	FORMAT(1H ,4X,10(2I5,2X))	DATA4775
9570	FORMAT(1H1/5X,44H CANNOT FIND A BOUNDARY SIDE COINCIDING WITH, 1 I3,37H-TH NEUMANN BOUNDARY SIDE: STOP ***)	DATA4780
9670	FORMAT(1H1/5X,44H *** CANNOT FIND A BOUNDARY NODAL NUMBER FOR, 1 I3,31H-TH NEUMANN BOUNDARY NODE: STOP)	DATA4785
9700	FORMAT(1H0/10X,35H --- COMPUTED NEUMANN NODE DATA ---//5X, 1 10(5H I,5H NPNB,2X)/5X,10(5H -.5H ----,2X))	DATA4790
9750	FORMAT(1H ,4X,10(2I5,2X))	DATA4795
C		DATA4800
	END	DATA4805
		DATA4810
		DATA4815
		DATA4820
		DATA4825
		DATA4830
		DATA4835
		DATA4840
		DATA4845
		DATA4850
		DATA4855
		DATA4860
		DATA4865

	SUBROUTINE SURF(X,Y,Z,IE,DCOSB,ISB,NPBB)	SURF 005
C		SURF 010
C	*****1*****2*****3*****4*****5*****6*****7**	SURF 015
C		SURF 020
C	----- TO GENERATE BOUNDARY GEOMETRY.	SURF 025
C		SURF 030
C	*****1*****2*****3*****4*****5*****6*****7**	SURF 035
C		SURF 040
C	----- INPUT: X(NNP), Y(NNP), Z(NNP), IE(NEL,9).	SURF 045
C		SURF 050
C	----- OUTPUT: DCOSB(3,NBES), ISB(6,NBES), NPBB(NBNP), NBES, NBNP.	SURF 055
C		SURF 060
C	*****1*****2*****3*****4*****5*****6*****7**	SURF 065
C		SURF 070

	IMPLICIT REAL*8(A-H,O-Z)	SURF 075
C		SURF 080
	COMMON /SGEOM/ MAXEL,MAXNP,MAXBES,MAXBNP,JBAND,MAXNTI,MAXTCH	SURF 085
	COMMON /CGEOM/ NNP,NEL,NBNP,NBES,KCRAV,NTI,NDTCHG	SURF 090
	COMMON /CINTE/ NCYL,NITER,KSTR,KPRO,KDSKO,KSS,NPITER,IGEOM	SURF 095
C		SURF 100
	DIMENSION X(MAXNP),Y(MAXNP),Z(MAXNP),IE(MAXEL,9)	SURF 105
	DIMENSION DCOSB(3,MAXBES),ISB(6,MAXBES),NPBB(MAXBNP)	SURF 110
C		SURF 115
	DIMENSION IEMI(4),IEMJ(4)	SURF 120
C		SURF 125
	DIMENSION KGB(4,6)	SURF 130
C		SURF 135
	DATA KGB/1,4,8,5, 1,2,6,5, 2,3,7,6, 4,3,7,8, 1,2,3,4, 5,6,7,8/	SURF 140
C		SURF 145
	NBES=0	SURF 150
	NBNP=0	SURF 155
	DO 390 MI=1,NEL	SURF 160
	DO 380 LS=1,6	SURF 165
C		SURF 170
C	----- STORE FOUR GLOBAL NODAL NUMBERS OF LS-TH SIDE OF MI-TH	SURF 175
C	----- ELEMENT IN ARRAY IEMI(4) FOR LATER USE.	SURF 180
C		SURF 185
	DO 120 IQ=1,4	SURF 190
	K=KGB(IQ,LS)	SURF 195
	IEMI(IQ)=IE(MI,K)	SURF 200
	120 CONTINUE	SURF 205
C		SURF 210
C	----- CHECK IF THE LS-TH SIDE OF ELEMENT MI IS A BOUNDARY	SURF 215
C	----- SIDE BY LOOPING OVER EACH OF THE SIX SIDES OF ALL ELEMENTS	SURF 220
C	----- OTHER THAN THE ELEMENT MI.	SURF 225
C		SURF 230
	DO 290 MJ=1,NEL	SURF 235
	IF(MJ.EQ.MI) GO TO 290	SURF 240
C		SURF 245
	DO 280 J=1,6	SURF 250
C		SURF 255
C	----- STORE THE FOUR GLOBAL NODAL NUMBERS OF J-TH SIDE OF ELEMENT	SURF 260
C	----- MJ IN ARRAY IEMJ(4).	SURF 265
C		SURF 270
	DO 140 JQ=1,4	SURF 275
	K=KGB(JQ,J)	SURF 280
	IEMJ(JQ)=IE(MJ,K)	SURF 285
	140 CONTINUE	SURF 290
C		SURF 295
C	----- CHECK IF IEMI(4) CONTAINS THE SAME FOUR GLOBAL NODES AS	SURF 300
C	----- IEMJ(4).	SURF 305
C		SURF 310
	IEQ=0	SURF 315

DO 180 IQ-1,4	SURF 320
NI-IEMI(IQ)	SURF 325
DO 160 JQ-1,4	SURF 330
NJ-IEMJ(JQ)	SURF 335
IF(NJ.EQ.NI) GO TO 170	SURF 340
160 CONTINUE	SURF 345
GO TO 180	SURF 350
170 IEQ-IEQ+1	SURF 355
180 CONTINUE	SURF 360
C	SURF 365
C ----- IF IEQ.EQ.4, THEN IEMJ(4) CONTAINS THE SAME FOUR GLOBAL	SURF 370
C ----- NODES AS IEMI(4). THUS THE LS-TH SIDE OF ELEMENT MI IS NOT	SURF 375
C ----- A BOUNDARY SIDE. HENCE GO TO 380 TO START A NEW SIDE.	SURF 380
C	SURF 385
IF(IEQ.EQ.4) GO TO 380	SURF 390
C	SURF 395
280 CONTINUE	SURF 400
290 CONTINUE	SURF 405
C	SURF 410
C ----- AFTER LOOPING OVER J FROM 1 TO 6 AND MJ FROM 1 TO NEL, WE	SURF 415
C ----- STILL CANNOT FIND A SIDE CONTAINING THE SAME FOUR GLOBAL	SURF 420
C ----- NODES AS THE LS-TH SIDE OF ELEMENT MI. THUS THE LS-TH SIDE	SURF 425
C ----- OF ELEMENT MI IS A BOUNDARY SIDE.	SURF 430
C	SURF 435
NBES-NBES+1	SURF 440
ISB(5,NBES)-LS	SURF 445
ISB(6,NBES)-MI	SURF 450
C	SURF 455
C ----- COMPUTE DIRECTIONAL COSINES FOR THE NBES-TH SIDE.	SURF 460
C	SURF 465
K-KGB(1,LS)	SURF 470
NI-IE(MI,K)	SURF 475
K-KGB(2,LS)	SURF 480
NJ-IE(MI,K)	SURF 485
A1-X(NJ)-X(NI)	SURF 490
A2-Y(NJ)-Y(NI)	SURF 495
A3-Z(NJ)-Z(NI)	SURF 500
K-KGB(3,LS)	SURF 505
NJ-IE(MI,K)	SURF 510
B1-X(NJ)-X(NI)	SURF 515
B2-Y(NJ)-Y(NI)	SURF 520
B3-Z(NJ)-Z(NI)	SURF 525
AB23=A2*B3-A3*B2	SURF 530
AB31=A3*B1-A1*B3	SURF 535
AB12=A1*B2-A2*B1	SURF 540
AREA=DSQRT(AB23*AB23+AB31*AB31+AB12*AB12)	SURF 545
DCOSB(1,NBES)=AB23/AREA	SURF 550
DCOSB(2,NBES)=AB31/AREA	SURF 555
DCOSB(3,NBES)=AB12/AREA	SURF 560

	IF(LS.EQ.2 .OR. LS.EQ.3 .OR. LS.EQ.6) GO TO 305	SURF 565
	DCOSB(1,NBES)--DCOSB(1,NBES)	SURF 570
	DCOSB(2,NBES)--DCOSB(2,NBES)	SURF 575
	DCOSB(3,NBES)--DCOSB(3,NBES)	SURF 580
C		SURF 585
305	IF(NBES.GT.1) GO TO 320	SURF 590
	DO 310 IQ=1,4	SURF 595
	K-KGB(IQ,LS)	SURF 600
	NI-IE(MI,K)	SURF 605
	NBNP-NBNP+1	SURF 610
	NPBB(NBNP)-NI	SURF 615
310	CONTINUE	SURF 620
320	DO 340 IQ=1,4	SURF 625
	K-KGB(IQ,LS)	SURF 630
	NI-IE(MI,K)	SURF 635
	DO 330 IJ=1,NBNP	SURF 640
	NJ-NPBB(IJ)	SURF 645
	IF(NJ.EQ.NI) GO TO 340	SURF 650
330	CONTINUE	SURF 655
	NBNP-NBNP+1	SURF 660
	NPBB(NBNP)-NI	SURF 665
340	CONTINUE	SURF 670
C		SURF 675
380	CONTINUE	SURF 680
390	CONTINUE	SURF 685
C		SURF 690
C	----- PRINT BOUNDARY NODE INFORMATION	SURF 695
C		SURF 700
	IF(MOD(ICEOM,2).EQ.0) GO TO 396	SURF 705
	LINE=0	SURF 710
	DO 395 I=1,NBNP,10	SURF 715
	LINE=LINE+1	SURF 720
	IF(MOD(LINE-1,50).EQ.0) PRINT 3900	SURF 725
	NJMN=I	SURF 730
	NJMX=MINO(I+9,NBNP)	SURF 735
	PRINT 3950, (J,NPBB(J),J-NJMN,NJMX)	SURF 740
395	CONTINUE	SURF 745
396	CONTINUE	SURF 750
C		SURF 755
C	----- COMPUTE THE COMPRESSED BOUNDARY NODE NUMBER FOR EACH OF THE	SURF 760
C	----- FOUR NODES OF A BOUNDARY SIDE	SURF 765
C		SURF 770
	DO 490 MP=1,NBES	SURF 775
	LS=ISB(5,MP)	SURF 780
	M=ISB(6,MP)	SURF 785
	DO 460 IQ=1,4	SURF 790
	I-KGB(IQ,LS)	SURF 795
	NI-IE(M,I)	SURF 800

DO 420 NB-1, NBNP	SURF 805
NP-NPBB(NB)	SURF 810
IF(NP.NE.NI) GO TO 420	SURF 815
NII-NB	SURF 820
GO TO 440	SURF 825
420 CONTINUE	SURF 830
PRINT 4000, IQ,MP	SURF 835
4000 FORMAT(1H0,10X,' CAN NOT FIND A COMPRESSED BOUNDARY NODE FOR',	SURF 840
1 I2,'-TH POINT OF',I4,'-TH BOUNDARY SIDE STOP')	SURF 845
STOP	SURF 850
440 ISB(IQ,MP)-NII	SURF 855
460 CONTINUE	SURF 860
490 CONTINUE	SURF 865
C	SURF 870
C ----- PRINT BOUNDARY SIDE INFORMATION	SURF 875
C	SURF 880
IF(MOD(IGEOM,2).EQ.0) GO TO 696	SURF 885
LINE-0	SURF 890
DO 695 MP-1, NBES	SURF 895
LINE-LINE+1	SURF 900
IF(MOD(LINE-1,50).EQ.0) PRINT 6900	SURF 905
PRINT 6950, MP, (DCOSB(I,MP),I-i,3),(ISB(I,MP),I-1,6)	SURF 910
695 CONTINUE	SURF 915
696 CONTINUE	SURF 920
C	SURF 925
3900 FORMAT(1H1//10X,' **** COMPUTED BOUNDARY NODE DATA ****'//5X,	SURF 930
1 I C(' I NPBB',2X)/5X,10(' - ----',2X))	SURF 935
3950 FORMAT(1H ,4X,10(2I5,2X))	SURF 940
6900 FORMAT(1H1//10X,' *** COMPUTED BOUNDARY ELEMENT SIDE INFORMATION',	SURF 945
1 '***'//5X,' MP DCOSXB DCOSYB DCOSZB',	SURF 950
2 ' BP1 BP2 BP3 BP4 LS M'/5X,	SURF 955
3 ' -- ----- ,	SURF 960
4 ' --- ---- - - - -')	SURF 965
6950 FORMAT(1H ,4X,I5,3D15.6,6I5)	SURF 970
C	SURF 975
RETURN	SURF 980
END	SURF 985

C		PAGE 245
	220 DO 290 IQ=1,8	PAGE 250
	NI-IE(M,IQ)	PAGE 255
C		PAGE 260
C	----- COMPRESS THE NODES TO 1 TO JBAND	PAGE 265
C		PAGE 270
	NLNOD-NLNOD+1	PAGE 275
	IF(NLNOD.GT.1) GO TO 230	PAGE 280
C		PAGE 285
C	----- THE FIRST NODE IS ENCOUNTERED	PAGE 290
C		PAGE 295
	KOUNT-KOUNT+1	PAGE 300
	GNOJCN(KOUNT, NP)-NI	PAGE 305
	GO TO 290	PAGE 310
C		PAGE 315
C	----- IF NLNOD IS GREATER THAN 1, WE HAVE TO CHECK IF NI IS THE	PAGE 320
C	----- NODE ALREADY COMPRESSED? IF YES, SKIP. IF NOT INCREASE THE	PAGE 325
C	----- KOUNT.	PAGE 330
C		PAGE 335
	230 DO 240 J=1,KOUNT	PAGE 340
	NJ-GNOJCN(J, NP)	PAGE 345
	IF(NI.EQ.NJ) GO TO 290	PAGE 350
	240 CONTINUE	PAGE 355
C		PAGE 360
C	----- THE NODE NI HAS NOT BEEN COMPRESSED YET. HENCE COMPRESS IT.	PAGE 365
C		PAGE 370
	KOUNT-KOUNT+1	PAGE 375
	GNOJCN(KOUNT, NP)-NI	PAGE 380
C		PAGE 385
	290 CONTINUE	PAGE 390
C		PAGE 395
	390 CONTINUE	PAGE 400
C		PAGE 405
	IF(KOUNT.LE.JBAND) GO TO 490	PAGE 410
	KONT-KOUNT-1	PAGE 415
	JBND-JBAND-1	PAGE 420
	WRITE(6,1000) NP,KONT,JBND	PAGE 425
	STOP	PAGE 430
C		PAGE 435
	490 CONTINUE	PAGE 440
C		PAGE 445
C	***** PRINT GENERATED ARRAY GNOJCN	PAGE 450
C		PAGE 455
	IF(MOD(IGEOM,2).EQ.0) GO TO 595	PAGE 460
	LINE=0	PAGE 465
	DO 590 NP=1,NNP	PAGE 470
	LINE=LINE+1	PAGE 475
	IF(MOD(LINE-1,50).EQ.0) PRINT 5000	PAGE 480
	PRINT 5100, NP,(GNOJCN(I, NP), I=1, JBAND)	PAGE 485
	590 CONTINUE	PAGE 490

595 CONTINUE	PAGE 495
C	PAGE 500
C ***** 1. FILL-UP GNP(I,MXKR) FROM I-MXNR+1 TO I-MXTNR BASED ON	PAGE 505
C ***** IE(MAXEL,8) AND ON GNP(I,MXKR) FROM I-1 TO I-MXNR,	PAGE 510
C ***** 2. GENERATE NTNR(MXKR) ALSO BASED ON IE(MAXEL,8) AND ON	PAGE 515
C ***** GNP(I,MXKR) FROM I-1 TO I-MXNR.	PAGE 520
C	PAGE 525
DO 690 K-1,NREGN	PAGE 530
LNNP-NNR(K)	PAGE 535
LTNNP-LNNP	PAGE 540
DO 680 M-1,NEL	PAGE 545
C	PAGE 550
DO 630 IQ-1,8	PAGE 555
NI-IE(M,IQ)	PAGE 560
DO 620 J-1,LNNP	PAGE 565
NJ-GNP(J,K)	PAGE 570
IF(NI.NE.NJ) GO TO 620	PAGE 575
GO TO 650	PAGE 580
620 CONTINUE	PAGE 585
630 CONTINUE	PAGE 590
C	PAGE 595
C ----- NONE OF THE EIGHT NODES IS ONE OF THE INTERIOR NODES	PAGE 600
C ----- HENCE SKIP THIS ELEMENT AND GO TO 680.	PAGE 605
C	PAGE 610
GO TO 680	PAGE 615
C	PAGE 620
C ----- ONE OF THE EIGHT NODES IS ONE OF THE INTERIOR NODES,	PAGE 625
C ----- HENCE EACH OF THE EIGHT NODES IS EITHER AN INTERIOR NODE	PAGE 630
C ----- OR AN INTRA-BOUNDARY NODE.	PAGE 635
C	PAGE 640
650 DO 670 IQ-1,8	PAGE 645
NI-IE(M,IQ)	PAGE 650
C	PAGE 655
C ----- CHECK IF NI IS ONE OF THE POINTS IN GNP(I,K) FOR I-1,LTNNP	PAGE 660
C	PAGE 665
DO 660 J-1,LTNNP	PAGE 670
NJ-GNP(J,K)	PAGE 675
C	PAGE 680
C ----- NJ.EQ.NI MEANS NI IS ALREADY ONE OF THE GNP(I,K) POINTS,	PAGE 685
C ----- HENCE SKIP AND GO TO 670	PAGE 690
C	PAGE 695
IF(NJ.EQ.NI) GO TO 670	PAGE 700
660 CONTINUE	PAGE 705
C	PAGE 710
C ----- THE IQ-TH NODE, I.E. NI, IS NOT ONE OF THE GNP(I,K) POINTS,	PAGE 715
C ----- HENCE FACTOR THIS NODE INTO THE ARRAY GNP(I,K) BY FILLING-UP.	PAGE 720
C	PAGE 725
LTNNP-LTNNP+1	PAGE 730
GNP(LTNNP,K)-NI	PAGE 735
670 CONTINUE	PAGE 740

C		PAGE 745
C	680 CONTINUE	PAGE 750
C		PAGE 755
	NTNR(K)-LTNNP	PAGE 760
C		PAGE 765
C	690 CONTINUE	PAGE 770
C		PAGE 775
C	***** GENERATE LNOJCN(JBAND, MXNR, MXKR) BASED ON GNP(MXTNR, MXKR)	PAGE 780
C	***** AND GNOJCN(JBAND, MAXNP) AND PRODUCE LMAXDF(MXKR) BASED ON	PAGE 785
C	***** LNOJCN(JBAND, MXNR, MXKR) FOR ALL SUBREGIONS.	PAGE 790
C		PAGE 795
	DO 790 K=1, NREGN	PAGE 800
	LNNP=NNR(K)	PAGE 805
	LTNNP=NTNR(K)	PAGE 810
C		PAGE 815
	DO 710 J=1, JBAND	PAGE 820
	DO 710 LI=1, LNNP	PAGE 825
	LNOJCN(J, LI, K)=0	PAGE 830
	710 CONTINUE	PAGE 835
C		PAGE 840
C	----- GENERATE LNOJCN(JBAND, MXNR, MXKR)	PAGE 845
C		PAGE 850
	DO 770 LI=1, LNNP	PAGE 855
	NI=GNP(LI, K)	PAGE 860
C		PAGE 865
	DO 750 J=1, JBAND	PAGE 870
	NJ=GNOJCN(J, NI)	PAGE 875
C		PAGE 880
	IF(NJ.EQ.0) GO TO 740	PAGE 885
C		PAGE 890
	DO 720 LJ=1, LTNNP	PAGE 895
	NLJ=GNP(LJ, K)	PAGE 900
	IF(NLJ.EQ.NJ) GO TO 730	PAGE 905
	720 CONTINUE	PAGE 910
C		PAGE 915
	WRITE (6, 7000) K, J, NJ, NI, LI	PAGE 920
	STOP	PAGE 925
C		PAGE 930
	730 LNOJCN(J, LI, K)=LJ	PAGE 935
	GO TO 750	PAGE 940
C		PAGE 945
	740 LNOJCN(J, LI, K)=0	PAGE 950
C		PAGE 955
	750 CONTINUE	PAGE 960
	770 CONTINUE	PAGE 965
C		PAGE 970
C	----- GENERATE LMAXDF(MXKR)	PAGE 975
C		PAGE 980

MAXDF=0	PAGE 985
DO 780 LI=1,LNNP	PAGE 990
DO 780 J=1,JBAND	PAGE 995
LJ=LNOJCN(J,LI,K)	PAGE1000
IF(LJ.GT.LNNP .OR. LJ.EQ.0) GO TO 780	PAGE1005
IDIF=LI-LJ	PAGE1010
IF(IDIF.LT.0) IDIF=LJ-LI	PAGE1015
IF(MAXDF.LT.IDIF) MAXDF=IDIF	PAGE1020
780 CONTINUE	PAGE1025
C	PAGE1030
LMAXDF(K)=MAXDF	PAGE1035
C	PAGE1040
790 CONTINUE	PAGE1045
C	PAGE1050
C ***** PRINT GENERATED ARRAYS LNOJCN(J,AND,MXNR,MXKR) AND	PAGE1055
C ***** GNP(MXTNR,MXKR).	PAGE1060
C	PAGE1065
IF(MOD(IGEOM,2).EQ.0) GO TO 895	PAGE1070
DO 890 K=1,NREGN	PAGE1075
PRINT 8000, K	PAGE1080
C	PAGE1085
LNNP=NNR(K)	PAGE1090
LNNP1=LNNP+1	PAGE1095
LTNNP=NTNR(K)	PAGE1100
C	PAGE1105
DO 820 I=1,LNNP	PAGE1110
PRINT 8200, I,GNP(I,K),(LNOJCN(J,I,K),J-1,JBAND)	PAGE1115
820 CONTINUE	PAGE1120
C	PAGE1125
DO 830 I=LNNP1,LTNNP	PAGE1130
PRINT 8200, I,GNP(I,K)	PAGE1135
830 CONTINUE	PAGE1140
C	PAGE1145
890 CONTINUE	PAGE1150
895 CONTINUE	PAGE1155
C	PAGE1160
WRITE(6,9000) (LMAXDF(K),K-1,NREGN)	PAGE1165
C	PAGE1170
1000 FORMAT(1H0//5X,' ***',14,'-TH NODE HAS',14,' NODES SURROUNDING',	PAGE1175
1 ' IT, WHICH IS MORE THAN JBAND - 1 -',15,' STOP ***')	PAGE1180
5000 FORMAT(1H1/5X,' ** GENERATED SURROUNDING NODES OF ALL NODES *',//	PAGE1185
1 5X,' NP 1 2 3 4 5 6 7 8',	PAGE1190
2 ' 9 10 11 12 13 14 15 16 17',	PAGE1195
3 ' 18 19 20 21 22 23 24 25 26 27',	PAGE1200
4 /5X,28(' --'))	PAGE1205
5100 FORMAT(1H ,4X,28I4)	PAGE1210

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7000 FORMAT(1H0//5X, ' WE CANNOT FIND A LOCAL NODE IN REGION', I3,      PAGE1215
1 ' CORRESPONDING TO', I3, '-TH COMPRESSED GLOBAL NODE', I4,      PAGE1220
2 ' CONNECTING TO GLOBAL NODE', I4, ' OR CONNECTING TO THE LOCAL ', PAGE1225
3 ' NODE ', I3)                                                    PAGE1230
8000 FORMAT(1H1, 10X, ' *** ARRAY GMLR AND LNOJCN ***'//5X,      PAGE1235
1 ' -- SUBREGION K =', I3, ' --'//5X,                                PAGE1240
2 ' LNODE GNODE SURROUNDING AND INCLUDING LOCAL NODES'/5X,      PAGE1245
3 ' -----' )                                                    PAGE1250
8200 FORMAT(1H , 4X, 2I6, 27I4)                                       PAGE1255
9000 FORMAT(1H0//5X, ' LIST OF HALF BAND WIDTH FOR ALL SUBREGIONS'/5X, PAGE1260
1 (30I4))                                                            PAGE1265
C                                                                    PAGE1270
RETURN                                                                PAGE 275
END                                                                    PAGE1280

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SUBROUTINE VELT(VX,VY,VZ, CMATRX, X,Y,Z, IE,H,HT,AKR, PROP)          VELT 005
C                                                                    VELT 010
C*****1*****2*****3*****4*****5*****6*****7**VELT 015
C                                                                    VELT 020
C ----- TO COMPUTE DARCY'S VELOCITY.                             VELT 025
C                                                                    VELT 030
C*****1*****2*****3*****4*****5*****6*****7**VELT 035
C                                                                    VELT 040
C ----- INPUT: X(NNP), Y(NNP), Z(NNP), IE(NEL,9), H(NNP), HT(NNP), VELT 045
C ----- AKR(8,NEL), PROP(NMPPM,NMAT)                             VELT 050
C                                                                    VELT 055
C ----- OUTPUT: VX(NNP), VY(NNP), VZ(NNP).                       VELT 060
C                                                                    VELT 065
C*****1*****2*****3*****4*****5*****6*****7**VELT 070
C                                                                    VELT 075
C IMPLICIT REAL*8(A-H,O-Z)                                          VELT 080
C                                                                    VELT 085
COMMON /SGEOM/ MAXEL,MAXNP,MAXBES,MAXBNP,JBAND,MAXNTI,MXNDTC        VELT 090
COMMON /CGEOM/ NNP,NEL,NBNP,NBES,KGRAV,NTI,NDTCHG                  VELT 095
COMMON /SMTL/ MAXMAT,MXSPPM,MXMPPM                                 VELT 100
C                                                                    VELT 105
DIMENSION VX(MAXNP),VY(MAXNP),VZ(MAXNP)                            VELT 110
DIMENSION CMATRX(MAXNP,JBAND)                                       VELT 115
DIMENSION X(MAXNP),Y(MAXNP),Z(MAXNP),IE(MAXEL,9)                   VELT 120
DIMENSION H(MAXNP),HT(MAXNP),AKR(8,MAXEL),PROP(MXMPPM,MAXMAT)     VELT 125
C                                                                    VELT 130
DIMENSION QB(8,8),QRX(8),QRY(8),QRZ(8),XQ(8),YQ(8),ZQ(8),HTQ(8)  VELT 135
DIMENSION AKXG(8),AKYG(8),AKZG(8),AKXYG(8),AKXZG(9),AKYZG(8)     VELT 140

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C		VELT 145
	AGRAV-DFLOAT(KGRAV)	VELT 150
C		VELT 155
C	----- INITIATE THE DARCY VELOCITY COMPONENTS	VELT 160
C		VELT 165
	DO 100 NP-1,NNP	VELT 170
	VX(NP)-0.0	VELT 175
	VY(NP)-0.0	VELT 180
	100 VZ(NP)-0.0	VELT 185
C		VELT 190
C	----- CALCULATE THE TOTAL HEAD HT(NP)	VELT 195
C		VELT 200
	DO 105 NP-1,NNP	VELT 205
	105 HT(NP)=H(NP) +AGRAV*Z(NP)	VELT 210
C		VELT 215
C	----- COMPUTE DARCY VELOCITIES BY APPLYING FINITE ELEMENT METHOD TO	VELT 220
C	----- DARCY LAW.	VELT 225
C		VELT 230
C		VELT 235
C	----- INITIATE MATRIX CMATRIX(NP,IB)	VELT 240
C		VELT 245
	DO 160 NP-1,NNP	VELT 250
	160 CMATRIX(NP,1)-0.0	VELT 255
C		VELT 260
C	----- COMPUTE ELEMENT MATRICES QB(IQ,JQ), QRX(IQ),QRY(IQ), & QRZ(IQ)	VELT 265
C		VELT 270
	DO 290 M-1,NEL	VELT 275
	MTYP=IE(M,9)	VELT 280
C		VELT 285
	DO 210 IQ-1,8	VELT 290
	NP=IE(M,IQ)	VELT 295
	XQ(IQ)=X(NP)	VELT 300
	YQ(IQ)=Y(NP)	VELT 305
	ZQ(IQ)=Z(NP)	VELT 310
	210 HTQ(IQ)=HT(NP)	VELT 315
C		VELT 320
	DO 215 KG-1,8	VELT 325
	AKXG(KG)=AKR(KG,M)*PROP(1,MTYP)	VELT 330
	AKYG(KG)=AKR(KG,M)*PROP(2,MTYP)	VELT 335
	AKZG(KG)=AKR(KG,M)*PROP(3,MTYP)	VELT 340
	AKXYG(KG)=AKR(KG,M)*PROP(4,MTYP)	VELT 345
	AKXZG(KG)=AKR(KG,M)*PROP(5,MTYP)	VELT 350
	215 AKYZG(KG)=AKR(KG,M)*PROP(6,MTYP)	VELT 355
C		VELT 360
	CALL Q8DV(QB,QRX,QRY,QRZ, XQ,YQ,ZQ,HTQ,AKXG,AKYG,AKZG,	VELT 365
	1 AKXYG,AKXZG,AKYZG)	VELT 370

```

C
C ----- ASSEMBLE QB(IQ,JQ) INTO THE GLOBAL MATRIX CMATRX(NP,IB) AND
C ----- FORM THE LOAD VECTOR VX(NP), VY(NP), AND VZ(NP).
C
      DO 280 IQ=1,8
      NI=IE(M,IQ)
      DO 240 JQ=1,8
      CMATRX(NI,1)-CMATRX(NI,1)+QB(IQ,JQ)
240 CONTINUE
C
      VX(NI)=VX(NI)+QRX(IQ)
      VY(NI)=VY(NI)+QRY(IQ)
      VZ(NI)=VZ(NI)+QRZ(IQ)
280 CONTINUE
C
290 CONTINUE
C
C ----- SOLVE THE MATRIX EQUATION CX=B
C
      DO 370 NP=1,NNP
      VX(NP)=VX(NP)/CMATRX(NP,1)
      VY(NP)=VY(NP)/CMATRX(NP,1)
370 VZ(NP)=VZ(NP)/CMATRX(NP,1)
C
      RETURN
      END

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VELT 375
VELT 380
VELT 385
VELT 390
VELT 395
VELT 400
VELT 405
VELT 410
VELT 415
VELT 420
VELT 425
VELT 430
VELT 435
VELT 440
VELT 445
VELT 450
VELT 455
VELT 460
VELT 465
VELT 470
VELT 475
VELT 480
VELT 485
VELT 490
VELT 495
VELT 500

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      SUBROUTINE Q8DV(QB,QRX,QRZ, XQ,YQ,ZQ,HTQ,AKXG,AKYG,AKZG,
1 AKXYG,AKXZG,AKYZG)
C
C*****1*****2*****3*****4*****5*****6*****7**Q8DV 005
C
C ----- TO COMPUTE THE INTEGRATION OF N(I)*N(J) AND -N(I)*K.GRAD(HT)
C
C*****1*****2*****3*****4*****5*****6*****7**Q8DV 010
C
C ----- INPUT: XQ(8), YQ(8), ZQ(8), HTQ(8), AKXG(8), AKYG(8), AKZG(8),
C ----- AKXYG(8), AKXZG(8), AKYZG(8).
C
C ----- OUTPUT: QB(8,8), QRX(8), QRY(8), QRZ(8).
C
C*****1*****2*****3*****4*****5*****6*****7**Q8DV 020
C
      IMPLICIT REAL*8 (A-H,O-Z)
      REAL*8 N(8)

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Q8DV 015
Q8DV 025
Q8DV 030
Q8DV 035
Q8DV 040
Q8DV 045
Q8DV 050
Q8DV 055
Q8DV 060
Q8DV 065
Q8DV 070
Q8DV 075
Q8DV 080
Q8DV 085
Q8DV 090

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C	DIMENSION QB(8,8),QRX(8),QRY(8),QRZ(8),XQ(8),YQ(8),ZQ(8),HTQ(8)	Q8DV 095
	DIMENSION AKXG(8),AKYG(8),AKZG(8),AKXYG(8),AKXZG(8),AKYZG(8)	Q8DV 100
	DIMENSION S(8),T(8),U(8),DNX(8),DNY(8),DNZ(8)	Q8DV 105
C		Q8DV 110
	DATA P /0.577350269189626D0/	Q8DV 115
	DATA S /-1.0D0,1.0D0,1.0D0,-1.0D0,-1.0D0,1.0D0,1.0D0,-1.0D0/	Q8DV 120
	DATA T /-1.0D0,-1.0D0,1.0D0,1.0D0,-1.0D0,-1.0D0,1.0D0,1.0D0/	Q8DV 125
	DATA U /-1.0D0,-1.0D0,-1.0D0,-1.0D0,1.0D0,1.0D0,1.0D0,1.0D0/	Q8DV 130
C		Q8DV 135
C	----- INITIATE MATRICES QB(IQ,JQ), QRX(IQ),QRY(IQ) & QRZ(IQ)	Q8DV 140
C		Q8DV 145
	DO 100 IQ=1,8	Q8DV 150
	QRX(IQ)=0.0	Q8DV 155
	QRY(IQ)=0.0	Q8DV 160
	QRZ(IQ)=0.0	Q8DV 165
	DO 100 JQ=1,8	Q8DV 170
	100 QB(IQ,JQ)=0.0	Q8DV 175
C		Q8DV 180
C	----- SUMMATION OF THE INTEGRAND OVER THE GAUSSIAN POINTS	Q8DV 185
C		Q8DV 190
	DO 490 KG=1,8	Q8DV 195
C		Q8DV 200
C	----- DETERMINE LOCAL COORDINATE OF GAUSSIAN POINT KG	Q8DV 205
C		Q8DV 210
	SS=P*S(KG)	Q8DV 215
	TT=P*T(KG)	Q8DV 220
	UU=P*U(KG)	Q8DV 225
C		Q8DV 230
C	----- CALCULATE VALUES OF BASIS FUNCTIONS N(IQ) AND THEIR	Q8DV 235
C	----- DERIVATIVES DNX(IQ), DNY(IQ), AND DNZ(IQ), W.R.T. TO	Q8DV 240
C	----- X, Y, AND Z, RESPECTIVELY, AT THE GAUSSIAN POINT KG.	Q8DV 245
C		Q8DV 250
	CALL BASE(N, DNX, DNY, DNZ, DJAC, XQ, YQ, ZQ, SS, TT, UU)	Q8DV 255
C		Q8DV 260
	AKXK=AKXG(KG)	Q8DV 265
	AKYK=AKYG(KG)	Q8DV 270
	AKZK=AKZG(KG)	Q8DV 275
	AKXYK=AKXYG(KG)	Q8DV 280
	AKXZK=AKXZG(KG)	Q8DV 285
	AKYZK=AKYZG(KG)	Q8DV 290
C		Q8DV 295
C	----- ACCUMULATE THE SUMS TO OBTAIN THE MATRIX INTEGRALS QB(IQ,JQ)	Q8DV 300
C	----- AND QRX(IQ), QRY(IQ), AND QRZ(IQ)	Q8DV 305
C		Q8DV 310
	DO 390 IQ=1,8	Q8DV 315
	DO 390 JQ=1,8	Q8DV 320
	QB(IQ,JQ)=QB(IQ,JQ)+ N(IQ)*N(JQ)*DJAC	Q8DV 325
		Q8DV 330

QRX(IQ)-QRX(IQ)-N(IQ)*HTQ(JQ)*(AKXK*DNX(JQ)+AKXYK*DNY(JQ)+	Q8DV 335
1 AKXZK*DNZ(JQ))*DJAC	Q8DV 340
QRY(IQ)-QRY(IQ)-N(IQ)*HTQ(JQ)*(AKXYK*DNX(JQ)+AKYK*DNY(JQ)+	Q8DV 345
1 AKYZK*DNZ(JQ))*DJAC	Q8DV 350
QRZ(IQ)-QRZ(IQ)-N(IQ)*HTQ(JQ)*(AKXZK*DNX(JQ)+AKYZK*DNY(JQ)+	Q8DV 355
1 AKZK*DNZ(JQ))*DJAC	Q8DV 360
390 CONTINUE	Q8DV 365
C	Q8DV 370
490 CONTINUE	Q8DV 375
C	Q8DV 380
RETURN	Q8DV 385
END	Q8DV 390

SUBROUTINE SPROP(TH,DTH,AKR, IE,H,THPROP,AKPROP)	SPRO 005
C	SPRO 010
C*****1*****2*****3*****4*****5*****6*****7**	SPRO 015
C	SPRO 020
C ----- TO COMPUTE RELATIVE HYDRAULIC CONDUCTIVITY OR PERMEABILITY,	SPRO 025
C ----- MOISTURE CONTENT, AND WATER CAPACITY GIVEN THE PRESSURE	SPRO 030
C ----- HEAD.	SPRO 035
C	SPRO 040
C*****1*****2*****3*****4*****5*****6*****7**	SPRO 045
C	SPRO 050
C ----- INPUT: IE(NEL,9), H(NNP), THPROP(NSPPM,NMAT),	SPRO 055
C ----- AKPROP(NSPPM,NMAT).	SPRO 060
C	SPRO 065
C ----- OUTPUT: AKR(8,NEL), TH(8,NEL), DTH(8,NEL).	SPRO 070
C	SPRO 075
C*****1*****2*****3*****4*****5*****6*****7**	SPRO 080
C	SPRO 085
IMPLICIT REAL*8(A-H,O-Z)	SPRO 090
REAL*8 N(8)	SPRO 095
C	SPRO 100
COMMON /SGEOM/ MAXEL,MAXNP,MAXBES,MAXBNP,JBAND,MAXNTI,MXNDTC	SPRO 105
COMMON /CGEOM/ NNP,NEL,NBNP,NBES,KGRAV,NTI,NDTCHG	SPRO 110
COMMON /SMTL/ MAXMAT,MXSPPM,MXMPPM	SPRO 115
C	SPRO 120
DIMENSION TH(8,MAXEL),DTH(8,MAXEL),AKR(8,MAXEL)	SPRO 125
DIMENSION IE(MAXEL,9),H(MAXNP)	SPRO 130
DIMENSION THPROP(MXSPPM,MAXMAT),AKPROP(MXSPPM,MAXMAT)	SPRO 135
C	SPRO 140
DIMENSION HQ(8),S(8),T(8),U(8),HKG(8)	SPRO 145

C	DATA P/O.577350269189626/	SPRO 150
	DATA S/-1.0DO,1.0DO,1.0DO,-1.0DO, -1.0DO,1.0DO,1.0DO,-1.0DO/	SPRO 155
	DATA T/-1.0DO,-1.0DO,1.0DO,1.0DO, -1.0DO,-1.0DO,1.0DO,1.0DO/	SPRO 160
	DATA U/-1.0DO,-1.0DO,-1.0DO,-1.0DO, 1.0DO,1.0DO,1.0DO,1.0DO/	SPRO 165
C	DO 900 M-1,NEL	SPRO 170
C	DO 110 IQ-1,8	SPRO 175
	NP-IE(M,IQ)	SPRO 180
	110 HQ(IQ)-H(NP)	SPRO 185
C		SPRO 190
C	----- EVALUATE PRESSURE AT EIGHT GAUSSIAN POINTS.	SPRO 195
C		SPRO 200
	DO 150 KG-1,8	SPRO 205
	SS-P*S(KG)	SPRO 210
	TT-P*T(KG)	SPRO 215
	UU-P*U(KG)	SPRO 220
	SM-1.0DO-SS	SPRO 225
	SP-1.0DO+SS	SPRO 230
	TM-1.0DO-TT	SPRO 235
	TP-1.0DO+TT	SPRO 240
	UM-1.0DO-UU	SPRO 245
	UP-1.0DO+UU	SPRO 250
C		SPRO 255
	N(1)-0.125DO*SM*TM*UM	SPRO 260
	N(2)-0.125DO*SP*TM*UM	SPRO 265
	N(3)-0.125DO*SP*TP*UM	SPRO 270
	N(4)-0.125DO*SM*TP*UM	SPRO 275
	N(5)-0.125DO*SM*TM*UP	SPRO 280
	N(6)-0.125DO*SP*TM*UP	SPRO 285
	N(7)-0.125DO*SP*TP*UP	SPRO 290
	N(8)-0.125DO*SM*TP*UP	SPRO 295
C		SPRO 300
	HKG(KG)-0.0	SPRO 305
	DO 120 IQ-1,8	SPRO 310
	120 HKG(KG)-HKG(KG)+HQ(IQ)*N(IQ)	SPRO 315
	150 CONTINUE	SPRO 320
C		SPRO 325
	MTYP-IE(M,9)	SPRO 330
C		SPRO 335
C		SPRO 340
C		SPRO 345
C	----- TH, DTH/DH, AND AKR ARE OBTAINED WITH ANALYTICAL FUNCTIONS.	SPRO 350
C	----- THE READER MUST SUPPLY THE FUNCTIONAL FORM OF FKR AND FTH	SPRO 355
		SPRO 360
		SPRO 365

C		SPRO 370
C	----- THE FOLLOWING IS JUST AN EXAMPLE.	SPRO 375
C	----- WCR- THPROP(1,MTYP)-0.065, 0.050 FOR TWO SAMPLE MATERIALS	SPRO 380
C	----- WCS-THPROP(2,MTYP)-0.364, 0.341 FOR TWO SAMPLE MATERIALS	SPRO 385
C	----- RN-THPROP(3,MTYP)-1.092217, 1.546937 FOR TWO SAMPLE MATERIALS	SPRO 390
C	----- ALPH-THPROP(4,MTYP)-0.109, 0.002166 FOR TWO SAMPLE MATERIALS	SPRO 395
C		SPRO 400
	WCR-THPROP(1,MTYP)	SPRO 405
	WCS-THPROP(2,MTYP)	SPRO 410
	RN-PROP(3,MTYP)	SPRO 415
	ALPH-PROP(4,MTYP)	SPRO 420
	RM-1.000-1.000/RN	SPRO 425
	DO 800 KG-1,8	SPRO 430
	HNP-HKG(KG)	SPRO 435
	HNP--HNP	SPRO 440
C		SPRO 445
C	----- SATURATED CONDITION	SPRO 450
C		SPRO 455
	IF(HNP.GT.0.0) GO TO 700	SPRO 460
	TH(KG,M)-WCS	SPRO 465
	DTH(KG,M)-0.000	SPRO 470
	AKR(KG,M)-1.000	SPRO 475
	GO TO 800	SPRO 480
C		SPRO 485
C	----- UNSATURATED CASE	SPRO 490
C		SPRO 495
	700 THMKG=WCR+(WCS-WCR)/(1.000+(ALPH*HNP)**RN)**RM	SPRO 500
	TH(KG,M)-THMKG	SPRO 505
	RWC=(THMKG-WCR)/(WCS-WCR)	SPRO 510
	TERM=(1.000-RWC**(1.000/RM))**RM	SPRO 515
	RK=DSQRT(RWC)*(1.000-TERM)*(1.000-TERM)	SPRO 520
	AKR(KG,M)-RK	SPRO 525
	DTH(KG,M)=ALPH*(RN-1.000)*TERM*RWC**(1.000/RM)*(WCS-WCR)	SPRO 530
C		SPRO 535
	800 CONTINUE	SPRO 540
	900 CONTINUE	SPRO 545
	RETURN	SPRO 550
	END	SPRO 555


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SUBROUTINE BCPREP(IE,X,Y,Z, H,VX,VY,VZ, DCOSB,ISB, NPVB,ISV,      BCPR 005
> DCYFLX,FLX,HCON,HMIN,NPFLX,NPCON,NPMIN, IRTYP,RFALL, NCHG)    BCPR 010
C                                                                    BCPR 015
C*****1*****2*****3*****4*****5*****6*****7**BCPR 020
C                                                                    BCPR 025
C ----- TO DETERMINE WHETHER THE DIRICHLET B. C. WITH PONDING DEPTH, BCPR 030
C ----- OR THE DIRICHLET B. C. WITH MINIMUM PRESSURE HEAD, OR THE FLUXBCPR 035
C ----- B. C. WITH PRESCRIBED FLUX TO BE APPLIED ON THE VARIABLE BCPR 040
C ----- BOUNDARIES, NORMALLY THE AIR-MEDIA INTERFACE. BCPR 045
C                                                                    BCPR 050
C*****1*****2*****3*****4*****5*****6*****7**BCPR 055
C                                                                    BCPR 060
C ----- INPUT: IE(NEL,9), X(NNP), Y(NNP), Z(NNP), H(NNP), VX(NNP), BCPR 065
C ----- VY(NNP), VZ(NNP), DCOSB(3,NBES), ISB(6,NBES), BCPR 070
C ----- NPNV(NVNP), ISV(5,NVES), IRTYP(NVES), RFALL(NRPR), BCPR 075
C ----- HCON(NVNP), HMIN(NVNP), NCHG. BCPR 080
C                                                                    BCPR 085
C ----- OUTPUT: NPCON(NVNP), NPFLX(NVNP), NPMIN(NVNP), FLX(NVNP), BCPR 090
C ----- DCYFLX(NVNP), NCHG. BCPR 095
C                                                                    BCPR 100
C*****1*****2*****3*****4*****5*****6*****7**BCPR 105
C                                                                    BCPR 110
C      IMPLICIT REAL*8 (A-H,O-Z) BCPR 115
C                                                                    BCPR 120
C      COMMON /SGEOM/ MAXEL,MAXNP,MAXBES,MAXBNP,JBAND,MAXNTI BCPR 125
C      COMMON /CGEOM/ NNP,NEL,NBNP,NBES,KGRAV,NTI BCPR 130
C      COMMON /CVBC/ MXVES,MXVNP,MXRPR,MXRDP,NVES,NVNP,NRPR,NRDP BCPR 135
C                                                                    BCPR 140
C      DIMENSION IE(MAXEL,9),X(MAXNP),Y(MAXNP),Z(MAXNP) BCPR 145
C      DIMENSION H(MAXNP),VX(MAXNP),VY(MAXNP),VZ(MAXNP) BCPR 150
C                                                                    BCPR 155
C      DIMENSION DCOSB(3,MAXBES),ISB(6,MAXBES),ISV(5,MXVES),NPVB(MXVNP) BCPR 160
C      DIMENSION DCYFLX(MXVNP),FLX(MXVNP),HCON(MXVNP),HMIN(MXVNP) BCPR 165
C      DIMENSION NPFLX(MXVNP),NPCON(MXVNP),NPMIN(MXVNP) BCPR 170
C      DIMENSION RFALL(MXRPR),IRTP(MXVES) BCPR 175
C                                                                    BCPR 180
C      DIMENSION R1Q(4),R2Q(4),XQ(4),YQ(4),ZQ(4),F1Q(4),F2Q(4) BCPR 185
C                                                                    BCPR 190
C      DIMENSION KGB(4,6) BCPR 195
C                                                                    BCPR 200
C      DATA KGB/1,4,8,5, 1,2,6,5, 2,3,7,6, 4,3,7,8, 1,2,3,4, 5,6,7,8/ BCPR 205
C                                                                    BCPR 210
C ----- DETERMINE NORMAL RAINFALLS FLX(I) AND DARCY FLUXES DCYFLX(I) BCPR 215
C ----- FOR EACH NODAL POINT ON THE VARIABLE ELEMENT-SIDE. BCPR 220
C                                                                    BCPR 225
C      DO 210 NP=1,NVNP BCPR 230
C          FLX(NP)=0. BCPR 235
210 DCYFLX(NP)=0. BCPR 240

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C	DO 290 MP=1,NVES	BCPR 245
	ITYP=IRTP(MP)	BCPR 250
	RFMP=RFALL(ITYP)	BCPR 255
C	MPB=ISV(5,MP)	BCPR 260
	LS=ISB(5,MPB)	BCPR 265
	M=ISB(6,MPB)	BCPR 270
C	PROJ=DCOSB(3,MPB)	BCPR 275
	RFMPN=RFMP*PROJ	BCPR 280
C	DO 230 IQ=1,4	BCPR 285
	I=KGB(IQ,LS)	BCPR 290
	NI=IE(M,I)	BCPR 295
	XQ(IQ)=X(NI)	BCPR 300
	YQ(IQ)=Y(NI)	BCPR 305
	ZQ(IQ)=Z(NI)	BCPR 310
	F1Q(IQ)=RFMPN	BCPR 315
	F2Q(IQ)=VX(NI)*DCOSB(1,MPB)+DCOSB(2,MPB)*VY(NI)+DCOSB(3,MPB)*	BCPR 320
	1 VZ(NI)	BCPR 325
	230 CONTINUE	BCPR 330
C	----- COMPUTE SURFACE INTEGRAL OF N(IQ).F	BCPR 335
C	CALL Q4S(R1Q,R2Q,XQ,YQ,ZQ,F1Q,F2Q)	BCPR 340
C	DO 270 IQ=1,4	BCPR 345
	I=ISV(IQ,MP)	BCPR 350
	FLX(I)=FLX(I)+R1Q(IQ)	BCPR 355
	DCYFLX(I)=DCYFLX(I)+R2Q(IQ)	BCPR 360
	270 CONTINUE	BCPR 365
C	290 CONTINUE	BCPR 370
C	----- CHANGE TO FLUX OR HEAD CONDITIONS, AS NECESSARY, AND SO	BCPR 375
C	----- INDICATE IN THE ARRAYS NPFLX(NPP) AND NPCON(NPP).	BCPR 380
C	IF (NCHG.NE.(-1)) GO TO 300	BCPR 385
	NCHG=0	BCPR 390
	RETURN	BCPR 395
C	300 NCHG=0	BCPR 400
C	DO 390 NPP=1,NVNP	BCPR 405
C	DCYNNP=DCYFLX(NPP)	BCPR 410
	FLXNNP=FLX(NPP)	BCPR 415
	HCONNP=HCON(NPP)	BCPR 420
	HMINNP=HMIN(NPP)	BCPR 425
		BCPR 430
		BCPR 435
		BCPR 440
		BCPR 445
		BCPR 450
		BCPR 455
		BCPR 460
		BCPR 465
		BCPR 470
		BCPR 475
		BCPR 480
		BCPR 485
		BCPR 490

C		BCPR 495
	IF (FLXNNP.GT.0.0) GO TO 350	BCPR 500
C		BCPR 505
C	**** RAINFALL(INFILTRATION)-SEEPAGE CONDITIONS PREVAIL DURING RAINFALL	BCPR 510
C		BCPR 515
C		BCPR 520
C	----- CHECK IF THE CHANGE FROM RAINFALL-FLUX (NEUMANN) CONDITION TO	BCPR 525
C	----- PONDING (DIRICHLET) CONDITION IS NECESSARY?	BCPR 530
C		BCPR 535
	NP-NPFLX(NPP)	BCPR 540
	IF (NP.EQ.0) GO TO 310	BCPR 545
	IF(HCONNP.GE.H(NP)) GO TO 390	BCPR 550
	NPCON(NPP)-NPFLX(NPP)	BCPR 555
	NPFLX(NPP)-0	BCPR 560
	NCHG-NCHG+1	BCPR 565
	GO TO 390	BCPR 570
C		BCPR 575
C	----- CHECK IF THE CHANGE FROM PONDING (DIRICHLET) CONDITION TO	BCPR 580
C	----- RAINFALL-FLUX (NEUMANN) CONDITION IS NECESSARY?	BCPR 585
C		BCPR 590
	310 NP-NPCON(NPP)	BCPR 595
	IF(NP.EQ.0) GO TO 320	BCPR 600
	IF(FLXNNP.LE.DCYNNP) GO TO 390	BCPR 605
	NPFLX(NPP)-NPCON(NPP)	BCPR 610
	NPCON(NPP)-0	BCPR 615
	NCHG-NCHG+1	BCPR 620
	GO TO 390	BCPR 625
C		BCPR 630
C	----- CHANGE MINIMUM PRESSURE CONDITION TO RAINFALL-FLUX CONDITION	BCPR 635
C	----- SINCE A MINIMUM PRESSURE CONDITION IS NOT LIKELY TO BE	BCPR 640
C	----- DURING RAINFALL PERIOD	BCPR 645
C		BCPR 650
	320 NP-NPMIN(NPP)	BCPR 655
	IF(NP.EQ.0) GO TO 390	BCPR 660
	NPFLX(NPP)-NPMIN(NPP)	BCPR 665
	NPMIN(NPP)-0	BCPR 670
	NCHG-NCHG+1	BCPR 675
	GO TO 390	BCPR 680
C		BCPR 685
C	**** EVAPORATION-SEEPAGE CONDITIONS PREVAIL DURING NON-RAINFALL PERIOD	BCPR 690
C		BCPR 695
C		BCPR 700
C	----- CHECK IF THE CHANGE FROM EVAPORATION-FLUX CONDITION TO	BCPR 705
C	----- MINIMUM PRESSURE HEAD CONDITION IS NECESSARY?	BCPR 710
C		BCPR 715
	350 NP-NPFLX(NPP)	BCPR 720
	IF(NP.EQ.0) GO TO 360	BCPR 725
	IF(HMINNP.LE.H(NP)) GO TO 390	BCPR 730
	NPMIN(NPP)-NPFLX(NPP)	BCPR 735

NPFLX(NPP)-0	BCPR 740
NCHG-NCHG+1	BCPR 745
GO TO 390	BCPR 750
C	BCPR 755
C ----- CHECK IF THE CHANGE FROM PONDING CONDITION TO EVAPORATION-FLUX	BCPR 760
C ----- CONDITION IS NECESSARY?	BCPR 765
C	BCPR 770
360 NP-NPCON(NPP)	BCPR 775
IF(NP.EQ.0) GO TO 370	BCPR 780
IF(DCYNNP.GE.0.0) GO TO 390	BCPR 785
NPFLX(NPP)-NPCON(NPP)	BCPR 790
NPCON(NPP)-0	BCPR 795
NCHG-NCHG+1	BCPR 800
GO TO 390	BCPR 805
C	BCPR 810
C ----- CHECK IF THE CHANGE FROM MINIMUM PRESSURE HEAD CONDITION TO	BCPR 815
C ----- EVAPORATION-FLUX CONDITION IS NECESSARY?	BCPR 820
C	BCPR 825
370 NP-NPMIN(NPP)	BCPR 830
IF(NP.EQ.0) GO TO 390	BCPR 835
C IF(DCYNNP.LT.0.0) GO TO 380	BCPR 840
IF(DCYNNP.LT.FLXNNP) GO TO 390	BCPR 845
NPFLX(NPP)-NPMIN(NPP)	BCPR 850
NPMIN(NPP)-0	BCPR 855
NCHG-NCHG+1	BCPR 860
GO TO 390	BCPR 865
C	BCPR 870
C 380 PRINT 1000, NPP	BCPR 875
C STOP	BCPR 880
C	BCPR 885
390 CONTINUE	BCPR 890
C	BCPR 895
C1000 FORMAT(1H1,'*** WARNING DURING NON-RAINFALL PERIOD',I3,	BCPR 900
C 1 '-TH VB NODE USING MINIMUM HEAD CONDITION RESULTS IN ',	BCPR 905
C 2 'DARCY FLUX INTO THE REGION'/1X,'THIS SHOULD NOT HAPPEN. ',	BCPR 910
C 3 'HENCE EITHER MINIMUM HEAD IS NOT SMALL ENOUGH OR THE INTERIOR ',	BCPR 915
C 4 'NODE PRESSURE IS TOO SMALL: STOP')	BCPR 920
C	BCPR 925
RETURN	BCPR 930
END	BCPR 935

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SUBROUTINE ASEMBL(X,Y,Z,IE, CMATRX,RLD,LRN, HW,HP,DTH,AKR,PROP, ASEM 005
> SOS,MSEL,ISTYP,WSS,NPW,IWTYP, KSS,W, DELT) ASEM 010
C ASEM 015
C*****1*****2*****3*****4*****5*****6*****7**ASEM 020
C ASEM 025
C ----- TO ASSEMBLE THE GLOBAL COEFFICIENT MATRIX AND GLOBAL LOAD ASEM 030
C ----- VECTOR IN COMPRESSED FORM. ASEM 035
C ASEM 040
C*****1*****2*****3*****4*****5*****6*****7**ASEM 045
C ASEM 050
C ----- INPUT: X(NNP), Y(NNP), Z(NNP), IE(NEL,9), LRN(JBAND,NNP), ASEM 055
C ----- HW(NNP), HP(NNP), DTH(8,NEL), AKR(8,NEL), ASEM 060
C ----- PROP(NMPPM,NMAT), SOS(NSPR), MSEL(NSEL), ISTYP(NSEL), ASEM 065
C ----- WSS(NWPR), NPW(NWNP), IWTYP(NWNP), KSS, W, DELT. ASEM 070
C ASEM 075
C ----- OUTPUT: CMATRX(NNP,JBAND), RLD(NNP). ASEM 080
C ASEM 085
C*****1*****2*****3*****4*****5*****6*****7**ASEM 090
C ASEM 095
C IMPLICIT REAL*8(A-H,O-Z) ASEM 100
C ASEM 105
COMMON /SGEOM/ MAXEL,MAXNP,MAXBES,MAXBNP,JBAND,MAXNTI,MXNDTC ASEM 110
COMMON /CGEOM/ NNP,NEL,NBN,NBEL,KGRAV,NIT,NDTCHG ASEM 115
COMMON /CS/ MXSPR,MXSDP,MXSEL,NSPR,NSDP,NSEL ASEM 120
COMMON /CW/ MXWPR,MXWDP,MXWNP,NWPR,NWDP,NWNP ASEM 125
C ASEM 130
COMMON /SMTL/ MAXMAT,MXSPPM,MXMPPM ASEM 135
C ASEM 140
DIMENSION X(MAXNP),Y(MAXNP),Z(MAXNP),IE(MAXEL,9) ASEM 145
DIMENSION CMATRX(MAXNP,JBAND),RLD(MAXNP),LRN(JBAND,MAXNP) ASEM 150
DIMENSION HW(MAXNP),HP(MAXNP),DTH(8,MAXEL),AKR(8,MAXEL) ASEM 155
DIMENSION PROP(MXMPPM,MAXMAT) ASEM 160
DIMENSION SOS(MXSPR),MSEL(MXSEL),ISTYP(MXSEL) ASEM 165
DIMENSION WSS(MXWPR),NPW(MXWNP),IWTYP(MXWNP) ASEM 170
C ASEM 175
DIMENSION QA(8,8),QB(8,8),RQ(8) ASEM 180
DIMENSION DTHG(8),AKXG(8),AKYG(8),AKZG(8),AKXYG(9),AKXZG(8), ASEM 185
1 AKYZG(8),XQ(8),YQ(8),ZQ(8),IEM(8) ASEM 190
C ASEM 195
C ASEM 200
C AGRAV-DFLOAT(KGRAV) ASEM 205
C ASEM 210
DELTI=1./DELT ASEM 215
W1=W ASEM 220
W2=1.-W ASEM 225
IF (KSS.GT.0) GO TO 100 ASEM 230
DELTI=0. ASEM 235
W1=1. ASEM 240
W2=0. ASEM 245

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C		ASEM 250
C	----- INITIATE MATRICES C(NP,IB) AND R(NP)	ASEM 255
C		ASEM 260
	100 DO 150 NP-1,NNP	ASEM 265
	RLD(NP)=0.0	ASEM 270
	DO 150 I=1,JBAND	ASEM 275
	CMATRX(NP,I)=0.0	ASEM 280
	150 CONTINUE	ASEM 285
C		ASEM 290
C	----- START TO ASSEMBLE OVER ALL ELEMENTS	ASEM 295
C		ASEM 300
	DO 490 M=1,NEL	ASEM 305
C		ASEM 310
C	----- COMPUTE MATRICES QA(IQ,JQ), QB(IQ,JQ), AND RQ(IQ) FOR EACH M	ASEM 315
C		ASEM 320
	MTYP=IE(M,9)	ASEM 325
	SAKX=PROP(1,MTYP)	ASEM 330
	SAKY=PROP(2,MTYP)	ASEM 335
	SAKZ=PROP(3,MTYP)	ASEM 340
	SAKXY=PROP(4,MTYP)	ASEM 345
	SAKXZ=PROP(5,MTYP)	ASEM 350
	SAKYZ=PROP(6,MTYP)	ASEM 355
C		ASEM 360
	DO 210 IQ=1,8	ASEM 365
	NP=IE(M,IQ)	ASEM 370
	IEM(IQ)=NP	ASEM 375
	XQ(IQ)=X(NP)	ASEM 380
	YQ(IQ)=Y(NP)	ASEM 385
	ZQ(IQ)=Z(NP)	ASEM 390
	210 CONTINUE	ASEM 395
C		ASEM 400
	DO 220 KG=1,8	ASEM 405
	DTHG(KG)=DTH(KG,M)	ASEM 410
	AKXG(KG)=SAKX*AKR(KG,M)	ASEM 415
	AKYG(KG)=SAKY*AKR(KG,M)	ASEM 420
	AKZG(KG)=SAKZ*AKR(KG,M)	ASEM 425
	AKXYG(KG)=SAKXY*AKR(KG,M)	ASEM 430
	AKXZG(KG)=SAKXZ*AKR(KG,M)	ASEM 435
	AKYZG(KG)=SAKYZ*AKR(KG,M)	ASEM 440
	220 CONTINUE	ASEM 445
C		ASEM 450
	SOSM=0.0	ASEM 455
	IF(NSEL.EQ.0) GO TO 260	ASEM 460
	DO 240 I=1,NSEL	ASEM 465
	MP=MSEL(I)	ASEM 470
	IF(MP.NE.M) GO TO 240	ASEM 475
	ITYP=ISTYP(I)	ASEM 480
	SOSM=SOS(ITYP)	ASEM 485

GO TO 260	ASEM 490
240 CONTINUE	ASEM 495
260 CONTINUE	ASEM 500
C	ASEM 505
CALL Q8(QA,QB,RQ, DTHG,AKXG,AKYG,AKZG,AKXYG,AKXZG,AKYZG, > XQ,YQ,ZQ, SOSM,AGRAV)	ASEM 510 ASEM 515
C	ASEM 520
C ----- ASSEMBLE QA(IQ,JQ) AND QB(IQ,JQ) INTO THE GLOBAL MATRIX	ASEM 525
C ----- C(NP,IB) = B + A/DELT AND FORM THE GLOBAL LOAD VECTOR R(NP).	ASEM 530
C	ASEM 535
DO 390 IQ=1,8	ASEM 540
NI=IEM(IQ)	ASEM 545
RLD(NI)=RLD(NI)-RQ(IQ)	ASEM 550
DO 340 JQ=1,8	ASEM 555
NJ=IEM(JQ)	ASEM 560
QA(IQ,JQ)=QA(IQ,JQ)*DELT	ASEM 565
RLD(NI)=RLD(NI)+(QA(IQ,JQ)-W2*QB(IQ,JQ))*HP(NJ)	ASEM 570
DO 325 I=1,JBAND	ASEM 575
LNODE=LRN(I,NI)	ASEM 580
IF(NJ.EQ.LNODE) GO TO 330	ASEM 585
325 CONTINUE	ASEM 590
C	ASEM 595
WRITE(6,1000) NI,M,JQ	ASEM 600
STOP	ASEM 605
C	ASEM 610
330 CMATRX(NI,I)=CMATRX(NI,I)+QA(IQ,JQ)+W1*QB(IQ,JQ)	ASEM 615
C	ASEM 620
340 CONTINUE	ASEM 625
390 CONTINUE	ASEM 630
490 CONTINUE	ASEM 635
C	ASEM 640
C ----- INCORPORATE WELL SOURCE/SINK	ASEM 645
C	ASEM 650
700 IF(NWNP.EQ.0) GO TO 910	ASEM 655
DO 790 I=1,NWNP	ASEM 660
NI=NPW(I)	ASEM 665
ITYP=IWTYP(I)	ASEM 670
RLD(NI)=RLD(NI)+WSS(ITYP)	ASEM 675
790 CONTINUE	ASEM 680
C	ASEM 685
910 CONTINUE	ASEM 690
C	ASEM 695
1000 FORMAT(1H1/5X,'*** WARNING: NONE OF THE LOWER-LEFT NODE IN EQUATIOA 1N',I3,/5X,'*** IS CORRESPONDING TO ',I5,'-TH ELEMENT-S',I2, 2'-TH NODE; STOP ****')	ASEM 700 ASEM 705 ASEM 710
C	ASEM 715
RETURN	ASEM 720
END	ASEM 725

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SUBROUTINE Q8(QA,QB,RQ, DTHG,AKXG,AKYG,AKZG,AKXYG,AKXZG,AKYZG, Q8 005
> XQ,YQ,ZQ,SOSM,AGRAV) Q8 010
C Q8 015
C*****1*****2*****3*****4*****5*****6*****7**Q8 020
C Q8 025
C ----- TO COMPUTE ELEMENT MATRICES AND ELEMENT LOAD VECTORS. Q8 030
C Q8 035
C*****1*****2*****3*****4*****5*****6*****7**Q8 040
C Q8 045
C ----- INPUT: XQ(8), YQ(8), ZQ(8), DTHG(8), AKXG(8), AKYG(8), Q8 050
C ----- AKZG(8), AKXYG(8), AKXZG(8), AKYZG(8), SOSM, AGRAV. Q8 055
C Q8 060
C ----- OUTPUT: QA(8,8), QB(8,8), RQ(8). Q8 065
C Q8 070
C*****1*****2*****3*****4*****5*****6*****7**Q8 075
C Q8 080
C IMPLICIT REAL*8 (A-H,O-Z) Q8 085
C REAL*8 N(8) Q8 090
C Q8 095
C DIMENSION QA(8,8),QB(8,8),RQ(8),DTHG(8) Q8 100
C DIMENSION AKXG(8),AKYG(8),AKZG(8),AKXYG(8),AKXZG(8),AKYZG(8) Q8 105
C DIMENSION XQ(8),YQ(8),ZQ(8) Q8 110
C Q8 115
C DIMENSION DNX(8),DNY(8),DNZ(8) Q8 120
C DIMENSION S(8),T(8),U(8) Q8 125
C Q8 130
C DATA P / 0.577350269189626D0/ Q8 135
C DATA S/-1.0D0,1.0D0,1.0D0,-1.0D0, -1.0D0,1.0D0,1.0D0,-1.0D0/ Q8 140
C DATA T/-1.0D0,-1.0D0,1.0D0,1.0D0, -1.0D0,-1.0D0,1.0D0,1.0D0/ Q8 145
C DATA U/-1.0D0,-1.0D0,-1.0D0,-1.0D0, 1.0D0,1.0D0,1.0D0,1.0D0/ Q8 150
C Q8 155
C ----- INITIATE MATRICES QA, QB, AND RQ Q8 160
C Q8 165
C DO 110 IQ=1,8 Q8 170
C RQ(IQ)=0.0 Q8 175
C DO 110 JQ=1,8 Q8 180
C QA(IQ,JQ)=0.0 Q8 185
C QB(IQ,JQ)=0.0 Q8 190
C 110 CONTINUE Q8 195
C Q8 200
C DO 490 KG=1,8 Q8 205
C Q8 210
C ----- DETERMINE LOCAL COORDINATE OF GAUSSIAN POINT KG Q8 215
C Q8 220
C SS=P*S(KG) Q8 225
C TT=P*T(KG) Q8 230
C UU=P*U(KG) Q8 235

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C		Q8	240
C	----- CALCULATE VALUES OF BASIS FUNCTIONS N(IQ) AND THEIR	Q8	245
C	----- DERIVATIVES DNX(IQ), DNY(IQ), & DNZ(IQ) W.R.T. X, Y, & Z,	Q8	250
C	----- RESPECTIVELY AND THE DETERMINANT OF THE JACOBIAN.	Q8	255
C		Q8	260
	CALL BASE(N, DNX, DNY, DNZ, DJAC, XQ, YQ, ZQ, SS, TT, UU)	Q8	265
C		Q8	270
	AKXQP=AKXG(KG)*DJAC	Q8	275
	AKYQP=AKYG(KG)*DJAC	Q8	280
	AKZQP=AKZG(KG)*DJAC	Q8	285
	AKXYQP=AKXYG(KG)*DJAC	Q8	290
	AKXZQP=AKXZG(KG)*DJAC	Q8	295
	AKYZQP=AKYZG(KG)*DJAC	Q8	300
	DTHQP=DTHG(KG)*DJAC	Q8	305
	SOSMQP=SOSM*DJAC	Q8	310
C		Q8	315
C	----- ACCUMULATE THE SUMS TO OBTAIN THE MATRIX INTEGRALS QA(IQ, JQ),	Q8	320
C	----- QB(IQ, JQ), AND RQ(IQ).	Q8	325
C		Q8	330
	DO 390 IQ=1,8	Q8	335
	RQ(IQ)=RQ(IQ)+AGRAV*(DNX(IQ)*AKXZQP+AKYZQP*DNY(IQ)+AKZQP*DNZ(IQ))+Q8	340	
	1 N(IQ)*SOSMQP	Q8	345
	DO 390 JQ=1,8	Q8	350
	QA(IQ, JQ)=QA(IQ, JQ) + DTHQP*N(IQ)*N(JQ)	Q8	355
	QB(IQ, JQ)=QB(IQ, JQ) + DNX(IQ)*(AKXQP*DNX(JQ)+AKXYQP*DNY(JQ)+	Q8	360
	1 AKXZQP*DNZ(JQ)) + DNY(IQ)*(AKXYQP*DNX(JQ)+AKYQP*DNY(JQ)+AKYZQP*	Q8	365
	2 DNZ(JQ)) + DNZ(IQ)*(AKXZQP*DNX(JQ)+AKYZQP*DNY(JQ)+AKZQP*DNZ(JQ))	Q8	370
	390 CONTINUE	Q8	375
C		Q8	380
	490 CONTINUE	Q8	385
	690 CONTINUE	Q8	390
C		Q8	395
	RETURN	Q8	400
	END	Q8	405

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SUBROUTINE BASE(N, DNX, DNY, DNZ, DJAC, XQ, YQ, ZQ, SS, TT, UU)
C
C *****1*****2*****3*****4*****5*****6*****7**
C ----- TO COMPUTE THE BASIS AND WEIGHTING FUNCTIONS, THEIR
C ----- DERIVATIVES WITH RESPECT TO X, Y, Z, AND THE JACOBIAN
C ----- AT A GAUSSIAN POINT.
C
C *****1*****2*****3*****4*****5*****6*****7**
C ----- INPUT: XQ(8), YQ(8), ZQ(8), SS, TT, UU.
C
C ----- OUTPUT: N(8), DNX(8), DNY(8), DNZ(8), DJAC.
C
C ----- LOCALLY DEFINED WORKING ARRAYS: DNSS(8), DNNT(8), DNUU(8).
C
C *****1*****2*****3*****4*****5*****6*****7**
C
C      IMPLICIT REAL*8 (A-H,O-Z)
C      REAL*8 N(8)
C
C      DIMENSION DNX(8), DNY(8), DNZ(8), XQ(8), YQ(8), ZQ(8)
C      DIMENSION DNSS(8), DNNT(8), DNUU(8)
C
C      SM=1.0D0-SS
C      SP=1.0D0+SS
C      TM=1.0D0-TT
C      TP=1.0D0+TT
C      UM=1.0D0-UU
C      UP=1.0D0+UU
C
C      N(1)=.125D0*SM*TM*UM
C      N(2)=.125D0*SP*TM*UM
C      N(3)=.125D0*SP*TP*UM
C      N(4)=.125D0*SM*TP*UM
C      N(5)=.125D0*SM*TM*UP
C      N(6)=.125D0*SP*TM*UP
C      N(7)=.125D0*SP*TP*UP
C      N(8)=.125D0*SM*TP*UP
C
C      DNSS(1)=.125D0*TM*UM
C      DNSS(2)=.125D0*TM*UM
C      DNSS(3)=.125D0*TP*UM
C      DNSS(4)=.125D0*TP*UM
C      DNSS(5)=.125D0*TM*UP
C      DNSS(6)=.125D0*TM*UP
C      DNSS(7)=.125D0*TP*UP
C      DNSS(8)=.125D0*TP*UP

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C	DNTT(1)--.125D0*SM*UM	BASE 245
	DNTT(2)--.125D0*SP*UM	BASE 250
	DNTT(3)--.125D0*SP*UM	BASE 255
	DNTT(4)--.125D0*SM*UM	BASE 260
	DNTT(5)--.125D0*SM*UP	BASE 265
	DNTT(6)--.125D0*SP*UP	BASE 270
	DNTT(7)--.125D0*SP*UP	BASE 275
	DNTT(8)--.125D0*SM*UP	BASE 280
		BASE 285
		BASE 290
C	DNUU(1)--.125D0*SM*TM	BASE 295
	DNUU(2)--.125D0*SP*TM	BASE 300
	DNUU(3)--.125D0*SP*TP	BASE 305
	DNUU(4)--.125D0*SM*TP	BASE 310
	DNUU(5)--.125D0*SM*TM	BASE 315
	DNUU(6)--.125D0*SP*TM	BASE 320
	DNUU(7)--.125D0*SP*TP	BASE 325
	DNUU(8)--.125D0*SM*TP	BASE 330
		BASE 335
		BASE 340
C	SUM1=0.0	BASE 345
	SUM2=0.0	BASE 350
	SUM3=0.0	BASE 355
	SUM4=0.0	BASE 360
	SUM5=0.0	BASE 365
	SUM6=0.0	BASE 370
	SUM7=0.0	BASE 375
	SUM8=0.0	BASE 380
	SUM9=0.0	BASE 385
		BASE 390
	DO 290 I=1,8	BASE 395
	SUM1-SUM1+XQ(I)*DNSS(I)	BASE 400
	SUM2-SUM2+YQ(I)*DNSS(I)	BASE 405
	SUM3-SUM3+ZQ(I)*DNSS(I)	BASE 410
	SUM4-SUM4+XQ(I)*DNTT(I)	BASE 415
	SUM5-SUM5+YQ(I)*DNTT(I)	BASE 420
	SUM6-SUM6+ZQ(I)*DNTT(I)	BASE 425
	SUM7-SUM7+XQ(I)*DNUU(I)	BASE 430
	SUM8-SUM8+YQ(I)*DNUU(I)	BASE 435
	SUM9-SUM9+ZQ(I)*DNUU(I)	BASE 440
	290 CONTINUE	BASE 445
		BASE 450
C	DJAC-SUM1*(SUM5*SUM9-SUM6*SUM8) + SUM2*(SUM6*SUM7-SUM4*SUM9) +	BASE 455
	1 SUM3*(SUM4*SUM8-SUM5*SUM7)	BASE 460
		BASE 465
C	DJACI=1.0D0/DJAC	

C		BASE 470
	SUMI1-DJACI*(SUM5*SUM9-SUM6*SUM8)	BASE 475
	SUMI2-DJACI*(SUM3*SUM8-SUM2*SUM9)	BASE 480
	SUMI3-DJACI*(SUM2*SUM6-SUM3*SUM5)	BASE 485
	SUMI4-DJACI*(SUM6*SUM7-SUM4*SUM9)	BASE 490
	SUMI5-DJACI*(SUM1*SUM9-SUM3*SUM7)	BASE 495
	SUMI6-DJACI*(SUM3*SUM4-SUM1*SUM6)	BASE 500
	SUMI7-DJACI*(SUM4*SUM3-SUM5*SUM7)	BASE 505
	SUMI8-DJACI*(SUM2*SUM7-SUM1*SUM8)	BASE 510
	SUMI9-DJACI*(SUM1*SUM5-SUM2*SUM4)	BASE 515
C		BASE 520
	DO 390 I=1,8	BASE 525
	DNX(I)-SUMI1*DNSS(I) + SUMI2*DNTT(I) + SUMI3*DNUU(I)	BASE 530
	DNY(I)-SUMI4*DNSS(I) + SUMI5*DNTT(I) + SUMI6*DNUU(I)	BASE 535
	DNZ(I)-SUMI7*DNSS(I) + SUMI8*DNTT(I) + SUMI9*DNUU(I)	BASE 540
	390 CONTINUE	BASE 545
C		BASE 550
	RETURN	BASE 555
	END	BASE 560

	SUBROUTINE BC(CMATRX,RLD,LRN, IE,X,Y,Z, AKR,PROP, DCOSB,ISB,NPBB, BC	005
	1 QCB,ISC,ICTYP, QNB,ISN,INTYP, FLX,HCON,HMIN,NPFLX,NPCON,NPMIN, BC	010
	2 HDB, IDTYP,NPDB, KSS) BC	015
C		BC 020
C	C*****1*****2*****3*****4*****5*****6*****7**BC	025
C		BC 030
C	----- TO APPLY CAUCHY, NEUMANN, VARIABLE, AND DIRICHLET BOUNDARY BC	035
C	----- CONDITIONS. BC	040
C		BC 045
C	C*****1*****2*****3*****4*****5*****6*****7**BC	050
C		BC 055
C	----- INPUT: X(NNP), Y(NNP), Z(NNP), IE(NEL,9), LRN(JBAND,NNP), BC	060
C	----- AKR(8,NEL), PROP(NMPPM,NMAT), DCOSB(3,NBES), BC	065
C	----- ISB(6,NBES), NPBB(NBNP), QCB(NCPR), ISC(5,NCES), BC	070
C	----- ICTYP(NCES), QNB(NNPR), ISN(5,NNES), INTYP(NNES), BC	075
C	----- FLX(NVNP), HCON(NVNP), HMIN(NVNP), NPFLX(NVNP), BC	080
C	----- NPCON(NVNP), NPMIN(NVNP), HDB(NDPR), IDTYP(NDNP), BC	085
C	----- NPDB(NDNP), KSS. BC	090
C		BC 095
C	----- OUTPUT: MODIFIED CMATRX(NNP,JBAND), RLD(NNP). BC	100
C		BC 105
C	C*****1*****2*****3*****4*****5*****6*****7**BC	110
C		BC 115
C	IMPLICIT REAL*8(A-H,O-Z)	BC 120

C		BC	125
	COMMON /SCEOM/ MAXEL,MAXNP,MAXBES,MAXBNP,JBAND,MAXNTI	BC	130
	COMMON /CGEOM/ NNP,NEL,NBNP,NBES,KGRAV,NTI,NTCHG	BC	135
C		BC	140
	COMMON /CCBC/ MXCNP,MXCES,MXCPR,MXCDP,NCNP,NCES,NCPR,NCDP	BC	145
	COMMON /CNBC/ MXNNP,MXNES,MXNPR,MXNDP,NNNP,NNES,NNPR,NNDP	BC	150
	COMMON /CVBC/ MXVES,MXVNP,MXRPR,MXRDP,NVES,NVNP,NRPR,NRDP	BC	155
	COMMON /CDBC/ MXDNP,MXDPR,MXDDP,NDNP,NDPR,NDDP	BC	160
C		BC	165
	COMMON /SMTL/ MAXMAT,MSPPM,MMPPM	BC	170
CC		BC	175
	DIMENSION CMATRX(MAXNP,JBAND),RLD(MAXNP),LRN(JBAND,MAXNP)	BC	180
	DIMENSION X(MAXNP),Y(MAXNP),Z(MAXNP),IE(MAXEL,9)	BC	185
	DIMENSION AKR(8,MAXEL),PROP(MXMPPM,MAXMAT)	BC	190
	DIMENSION DCOSB(3,MAXBES),ISB(6,MAXBES),NPBB(MAXBNP)	BC	195
C		BC	200
	DIMENSION FLX(MXVNP),HCON(MXVNP),NPCON(MXVNP),NPFLX(MXVNP)	BC	205
	DIMENSION HMIN(MXVNP),NPMIN(MXVNP)	BC	210
C		BC	215
	DIMENSION HDB(MXDPR),IDTYP(MXDNP),NPDB(MXDNP)	BC	220
	DIMENSION QCB(MXCPR),ICTYP(MXCES),ISC(5,MXCES)	BC	225
C		BC	230
	DIMENSION QNB(MXNPR),INTYP(MXNES),ISN(5,MXNES)	BC	235
C		BC	240
	DIMENSION RIQ(4),R2Q(4),XQ(4),YQ(4),ZQ(4),F1Q(4),F2Q(4)	BC	245
C		BC	250
	DIMENSION KGB(4,6)	BC	255
C		BC	260
	DATA KGB/1,4,8,5, 1,2,6,5, 2,3,7,6, 4,3,7,8, 1,2,3,4, 5,6,7,8/	BC	265
C		BC	270
	AGRAV=DFLOAT(KGRAV)	BC	275
C		BC	280
C	***** APPLY CAUCHY BOUNDARY CONDITIONS	BC	285
C		BC	290
	IF(NCES.LE.0) GO TO 300	BC	295
	DO 260 MP=1,NCES	BC	300
	ITYP=ICTYP(MP)	BC	305
	QCBMP=QCB(MP)	BC	310
C		BC	315
	MPB=ISC(5,MP)	BC	320
	LS=ISB(5,MPB)	BC	325
	M=ISB(6,MPB)	BC	330
C		BC	335
	DO 210 IQ=1,4	BC	340
	I=KGB(IQ,LS)	BC	345
	NI=IE(M,I)	BC	350
	XQ(IQ)=X(NI)	BC	355
	YQ(IQ)=Y(NI)	BC	360
	ZQ(IQ)=Z(NI)	BC	365

	F1Q(IQ)-QCBMP	BC	370
	F2Q(IQ)-0.0	BC	375
	210 CONTINUE	BC	380
C		BC	385
	CALL Q4S(R1Q,R2Q,XQ,YQ,ZQ,F1Q,F2Q)	BC	390
C		BC	395
	DO 230 IQ=1,4	BC	400
	I-KGB(IQ,LS)	BC	405
	NI-IE(M,I)	BC	410
	RLD(NI)-RLD(NI)-R1Q(IQ)	BC	415
	230 CONTINUE	BC	420
	260 CONTINUE	BC	425
C		BC	430
C	***** APPLY NEUMANN BOUNDARY CONDITIONS	BC	435
C		BC	440
	300 IF(NNES.EQ.0) GO TO 500	BC	445
	DO 390 MP=1,NNES	BC	450
	ITYP=INTYP(MP)	BC	455
	QNBMP=QNB(MP)	BC	460
C		BC	465
	MPB=ISN(5,MP)	BC	470
	LS=ISB(5,MPB)	BC	475
	M=ISB(6,MPB)	BC	480
C		BC	485
	MTYP=IE(M,9)	BC	490
	AKZX=PROP(5,MTYP)	BC	495
	AKZY=PROP(6,MTYP)	BC	500
	AKZZ=PROP(3,MTYP)	BC	505
C		BC	510
	DO 310 IQ=1,4	BC	515
	I-KGB(IQ,LS)	BC	520
	NI-IE(M,I)	BC	525
	XQ(IQ)-X(NI)	BC	530
	YQ(IQ)-Y(NI)	BC	535
	ZQ(IQ)-Z(NI)	BC	540
	F1Q(IQ)-QNBMP	BC	545
	F2Q(IQ)-AKR(IQ,M)*(DCOSB(1,MPB)*AKZX+DCOSB(2,MPB)*AKZY+	BC	550
	1 DCOSB(3,MPB)*AKZZ)	BC	555
	310 CONTINUE	BC	560
C		BC	565
	CALL Q4S(R1Q,R2Q,XQ,YQ,ZQ,F1Q,F2Q)	BC	570
C		BC	575
C	----- MODIFY LOAD VECTOR DUE TO NEUMANN FLUX AND GRAVITY TERM.	BC	580
C		BC	585
	DO 360 IQ=1,4	BC	590
	I-KGB(IQ,LS)	BC	595
	NI-IE(M,I)	BC	600
	RLD(NI)-RLD(NI)-R1Q(IQ)+R2Q(IQ)	BC	605
	360 CONTINUE	BC	610

C		BC	615
	390 CONTINUE	BC	620
C		BC	625
C	***** APPLY VARIABLE (RAINFALL-SEEPAGE) BOUNDARY CONDITIONS	BC	630
C		BC	635
	500 IF(NVES.EQ.0) GO TO 600	BC	640
C		BC	645
C	----- CAUCHY PART OF VARIABLE BOUNDARY CONDITIONS	BC	650
C		BC	655
	DO 410 NPP-1,NVNP	BC	660
	NP-NPFLX(NPP)	BC	665
	IF (NP.EQ.0) GO TO 410	BC	670
	RLD(NP)-RLD(NP)-FLX(NPP)	BC	675
	410 CONTINUE	BC	680
C		BC	685
C	----- DIRICHLET PART OF VARIABLE BOUNDARY CONDITIONS	BC	690
C		BC	695
	DO 490 NPP-1,NVNP	BC	700
	NI-NPCON(NPP)	BC	705
	IF(NI.NE.0) GO TO 450	BC	710
	NI-NPMIN(NPP)	BC	715
	IF(NI.NE.0) GO TO 460	BC	720
	GO TO 490	BC	725
	450 BB-HCON(NPP)	BC	730
	GO TO 470	BC	735
	460 BB-HMIN(NPP)	BC	740
C		BC	745
	470 RLD(NI)-BB	BC	750
	DO 480 I-1,JBAND	BC	755
	CMATRX(NI,I)-0.0	BC	760
	IB-LRN(I,NI)	BC	765
	IF(IB.EQ.NI) CMATRX(NI,I)-1.0DO	BC	770
	480 CONTINUE	BC	775
	490 CONTINUE	BC	780
C		BC	785
C	***** APPLY DIRICHLET BOUNDARY CONDITIONS	BC	790
C		BC	795
	600 IF(NDNP.EQ.0) GO TO 900	BC	800
	DO 740 NPP-1,NDNP	BC	805
	NP-NPDB(NPP)	BC	810
	NI-NPBB(NP)	BC	815
	ITYP-IDTYP(NPP)	BC	820
	BB-HDB(ITYP)-Z(NI)*AGRAV	BC	825
	RLD(NI)-BB	BC	830
	DO 710 I-1,JBAND	BC	835
	CMATRX(NI,I)-0.0	BC	840
	IB-LRN(I,NI)	BC	845
	IF(IB.EQ.NI) CMATRX(NI,I)-1.0DO	BC	850
	710 CONTINUE	BC	855
	740 CONTINUE	BC	860

C		BC	865
	900 CONTINUE	BC	870
C		BC	875
	RETURN	BC	880
	END	BC	885
	SUBROUTINE Q4S(R1Q,R2Q,XQ,YQ,ZQ,F1Q,F2Q)	Q4S	005
C		Q4S	010
	C*****1*****2*****3*****4*****5*****6*****7**	Q4S	015
C		Q4S	020
	C ----- TO COMPUTE BOUNDARY SURFACE LOAD VECTOR OVER A BOUNDARY	Q4S	025
C		Q4S	030
	C ----- SURFACE.	Q4S	035
C		Q4S	040
	C*****1*****2*****3*****4*****5*****6*****7**	Q4S	045
C		Q4S	050
	C ----- INPUT: XQ(4), YQ(4), ZQ(4), F1Q(4), F2Q(4).	Q4S	055
C		Q4S	060
	C ----- OUTPUT: R1Q(4), R2Q(4).	Q4S	065
C		Q4S	070
	C*****1*****2*****3*****4*****5*****6*****7**	Q4S	075
C		Q4S	080
	IMPLICIT REAL*8 (A-H,O-Z)	Q4S	085
	REAL*8 N(4)	Q4S	090
C		Q4S	095
	DIMENSION R1Q(4),R2Q(4),XQ(4),YQ(4),ZQ(4),F1Q(4),F2Q(4)	Q4S	100
	DIMENSION S(4),T(4),DNSS(4),DNST(4)	Q4S	105
C		Q4S	110
	DATA P/ 0.577350269189626D0/, S/-1.0D+00, 1.0D+00, 1.0D+00,	Q4S	115
	>- 1.0D+00/, T/-1.0D+00,-1.0D+00, 1.0D+00, 1.0D+00/	Q4S	120
C		Q4S	125
	C ----- INITIATE MATRICES RQ(IQ)	Q4S	130
C		Q4S	135
	DO 100 IQ=1,4	Q4S	140
	R1Q(IQ)=0.0	Q4S	145
	100 R2Q(IQ)=0.0	Q4S	150
C		Q4S	155
	C ----- SUMMATION OF THE INTEGRAND OVER THE GAUSSIAN POINTS	Q4S	160
C		Q4S	165
	DO 490 KG=1,4	Q4S	170
C		Q4S	175
	C ----- DETERMINE LOCAL COORDINATE OF GAUSSIAN POINT KG	Q4S	180
C		Q4S	185
	SS=P*S(KG)	Q4S	190
	TT=P*T(KG)	Q4S	195
	SM=1.0D0-SS	Q4S	200
	SP=1.0D0+SS	Q4S	200

	TM-1.0D0-TT	Q4S 205
	TP-1.0D0+TT	Q4S 210
C		Q4S 215
	N(1)-0.25D0*SM*TM	Q4S 220
	N(2)-0.25D0*SP*TM	Q4S 225
	N(3)-0.25D0*SP*TP	Q4S 230
	N(4)-0.25D0*SM*TP	Q4S 235
	DNSS(1)--0.25D0*TM	Q4S 240
	DNSS(2)- 0.25D0*TM	Q4S 245
	DNSS(3)- 0.25D0*TP	Q4S 250
	DNSS(4)--0.25D0*TP	Q4S 255
	DNTT(1)--0.25D0*SM	Q4S 260
	DNTT(2)--0.25D0*SP	Q4S 265
	DNTT(3)- 0.25D0*SP	Q4S 270
	DNTT(4)- 0.25D0*SM	Q4S 275
C		Q4S 280
	DXDSS-0.0D0	Q4S 285
	DYDSS-0.0D0	Q4S 290
	DZDSS-0.0D0	Q4S 295
	DXDTT-0.0D0	Q4S 300
	DYDTT-0.0D0	Q4S 305
	DZDTT-0.0D0	Q4S 310
	DO 290 IQ-1,4	Q4S 315
	DXDSS-DXDSS+XQ(IQ)*DNSS(IQ)	Q4S 320
	DYDSS-DYDSS+YQ(IQ)*DNSS(IQ)	Q4S 325
	DZDSS-DZDSS+ZQ(IQ)*DNSS(IQ)	Q4S 330
	DXDTT-DXDTT+XQ(IQ)*DNTT(IQ)	Q4S 335
	DYDTT-DYDTT+YQ(IQ)*DNTT(IQ)	Q4S 340
	DZDTT-DZDTT+ZQ(IQ)*DNTT(IQ)	Q4S 345
	290 CONTINUE	Q4S 350
C		Q4S 355
	DETZ-DXDSS*DYDTT-DYDSS*DXDTT	Q4S 360
	DETY--DXDSS*DZDTT+DZDSS*DXDTT	Q4S 365
	DETX-DYDSS*DZDTT-DZDSS*DYDTT	Q4S 370
	DET-DSQRT (DETX*DETX+DETY*DETY+DETZ*DETZ)	Q4S 375
C		Q4S 380
C	----- ACCUMULATE THE SUMS TO OBTAIN THE MATRIX INTEGRALS RQ(IQ)	Q4S 385
C		Q4S 390
	F1K-0.0D0	Q4S 395
	F2K-0.0	Q4S 400
	DO 350 IQ-1,4	Q4S 405
	F1K-F1K+F1Q(IQ)*N(IQ)	Q4S 410
	F2K-F2K+F2Q(IQ)*N(IQ)	Q4S 415
	350 CONTINUE	Q4S 420
C		Q4S 425
	DO 390 IQ-1,4	Q4S 430
	R1Q(IQ)=R1Q(IQ)+N(IQ)*F1K*DET	Q4S 435
	R2Q(IQ)=R2Q(IQ)+N(IQ)*F2K*DET	Q4S 440
	390 CONTINUE	Q4S 445

C		Q4S	450
	490 CONTINUE	Q4S	455
C		Q4S	460
	RETURN	Q4S	465
	END	Q4S	470

SUBROUTINE BLKTR(C,CW, CMTRXL,RLDL, CMTRXG,RLDG, GNLR,LNOJCN,
1 NNPLR,LMAXDF, TOLB,NITER,IBUG,KPR,OME) BLKI 005

C BLKI 010
C *****1*****2*****3*****4*****5*****6*****7** BLKI 020

C BLKI 025

C ----- TO SOLVE THE MATRIX EQUATION WITH BLOCK ITERATION. FIRST, BLKI 030

C ----- THE BLOCK MATRIX EQUATION IS ASSEMBLED OUT OF THE GLOBAL BLKI 035

C ----- MATRIX EQUATION. THEN THE INTRA-BOUNDARY CONDITIONS ARE BLKI 040

C ----- IMPLEMENTED. FINALLY, THE BLOCK MATRIX EQUATION IS SOLVED BLKI 045

C ----- WITH DIRECT BAND MATRIX SOLVER. BLKI 050

C BLKI 055

C *****1*****2*****3*****4*****5*****6*****7** BLKI 060

C BLKI 065

C ----- INPUT: CW(NNP), CMTRXG(NNP,JBAND), RLDG(NNP), BLKI 070

C ----- GNLR(NTNNP,NREGN), LNOJCN(JBAND,NNPLR(K),NREGN), BLKI 075

C ----- NNPLR(NREGN), LMAXDF(NREGN), TOLB, NITER, IBUG, KPR, BLKI 080

C ----- OME. BLKI 085

C BLKI 090

C ----- OUTPUT: C(NNP), CW(NNP). BLKI 095

C BLKI 100

C ----- INPUTING WORKING ARRAYS: CMTRXL(LMXNP,LMXBW), RLDL(LMXNP). BLKI 105

C BLKI 110

C *****1*****2*****3*****4*****5*****6*****7** BLKI 115

C BLKI 120

IMPLICIT REAL*8(A-H,O-Z) BLKI 125

INTEGER*4 GNLR BLKI 130

C BLKI 135

COMMON /SGEOM/ MAXEL,MAXNP,MAXBES,MAXBNP,JBAND,MAXNTI,MXNDTC BLKI 140

COMMON /CGEOM/ NNP,NEL,NBNP,NBES,KGRAV,NTI,NDTCHG BLKI 145

COMMON /LGEOM/ LTMXNP,LMXNP,LMXBW,MXREGN,NREGN BLKI 150

C BLKI 155

DIMENSION C(MAXNP),CW(MAXNP) BLKI 160

DIMENSION CMTRXL(LMXNP,LMXBW),RLDL(LMXNP) BLKI 165

DIMENSION CMTRXG(MAXNP,JBAND),RLDG(MAXNP) BLKI 170

DIMENSION GNLR(LTMXNP,MXREGN),LNOJCN(JBAND,LMXNP,MXREGN) BLKI 175

DIMENSION NNPLR(MXREGN),LMAXDF(MXREGN) BLKI 180

C		BLKI 185
C	----- PUT ZERO-TH ITERATE INTO ARRAY C	BLKI 190
C		BLKI 195
	DO 110 NP-1,NNP	BLKI 200
	110 C(NP)-CW(NP)	BLKI 205
C		BLKI 210
C	***** START INTERATION LOOP	BLKI 215
C		BLKI 220
	IF(IBUG.NE.0 .AND. KPR.NE.0) PRINT 1000	BLKI 225
C		BLKI 230
	DO 690 IT-1,NITER	BLKI 235
C		BLKI 240
C	----- FOR EACH ITERATION, SOLVE FOR NREGN REGIONS	BLKI 245
C		BLKI 250
	DO 590 K-1,NREGN	BLKI 255
C		BLKI 260
	LHALFB=LMAXDF(K)	BLKI 265
	LIHBP=LHALFB+1	BLKI 270
	IBAND=2*LHALFB+1	BLKI 275
	LNNP=NNPLR(K)	BLKI 280
C		BLKI 285
C	----- PUT GLOBAL LOAD VECTOR INTO CORRESPONDING LOCAL LOAD VECTOR	BLKI 290
C	----- AND INITIATE THE LOCAL MATRIX CMTRXL(LNNP,IBAND) WHERE	BLKI 295
C		BLKI 300
	DO 210 LI-1,LNNP	BLKI 305
	NP=GNLR(LI,K)	BLKI 310
	RLDL(LI)=RLDG(NP)	BLKI 315
	DO 210 J-1,IBAND	BLKI 320
	CMTRXL(LI,J)=0.0	BLKI 325
	210 CONTINUE	BLKI 330
C		BLKI 335
C	----- ASSEMBLE LOCAL COEFFICIENT MATRIX CMTRXL(LMXNP,LMXBW) FROM THE	BLKI 340
C	----- GLOBAL COEFFICIENT MATRIX CMTRXG(MAXNP,JBAND) AND INCORPORATE	BLKI 345
C	----- INTERFACIAL DIRICHLET BOUNDARY CONDITIONS INTO RLDL(LMXNP).	BLKI 350
C		BLKI 355
	DO 490 LI-1,LNNP	BLKI 360
	NI=GNLR(LI,K)	BLKI 365
C		BLKI 370
	DO 390 J-1,JBAND	BLKI 375
	LJ=LNOJCN(J,LI,K)	BLKI 380
	NJ=GNLR(LJ,K)	BLKI 385
C		BLKI 390
	IF(LJ.LE.0) GO TO 390	BLKI 395
C		BLKI 400
	IF(LJ.GT.LNNP) GO TO 380	BLKI 405
	LJB=LJ-LI+LIHBP	BLKI 410
	CMTRXL(LI,LJB)=CMTRXG(NI,J)	BLKI 415
	GO TO 390	BLKI 420

C		BLKI 425
	380 RLDL(LI)-RLDL(LI)-CMTRXG(NI,J)*C(NJ)	BLKI 430
C		BLKI 435
	390 CONTINUE	BLKI 440
C		BLKI 445
	490 CONTINUE	BLKI 450
C		BLKI 455
C	----- SOLVE THE BLOCK EQUATIONS	BLKI 460
C		BLKI 465
	CALL SOLVE(1,CMTRXL,RLDL,LNNP,LHALFB,LMXNP,LMXBW)	BLKI 470
	CALL SOLVE(2,CMTRXL,RLDL,LNNP,LHALFB,LMXNP,LMXBW)	BLKI 475
C		BLKI 480
C	----- PUT THE NEWLY OBTAINED BLOCK SOLUTION INTO THE GLOBAL SOLUTION.	BLKI 485
C		BLKI 490
	DO 560 LI=1,LNNP	BLKI 495
	NP=GNLR(LI,K)	BLKI 500
	560 C(NP)-RLDL(LI)*OME + (1.000-OME)*C(NP)	BLKI 505
C		BLKI 510
	590 CONTINUE	BLKI 515
C		BLKI 520
C	----- CHECK IF THE CONVERGENT SOLUTION IS OBTAINED?	BLKI 525
C		BLKI 530
	DIFMAX=0.0	BLKI 535
	NOCCUR=1	BLKI 540
	DO 660 NP=1,NNP	BLKI 545
	DIF=C(NP)-CW(NP)	BLKI 550
	DIF=DABS(DIF)	BLKI 555
	IF(DIF.LE.DIFMAX) GO TO 660	BLKI 560
	DIFMAX=DIF	BLKI 565
	NOCCUR=NP	BLKI 570
	660 CONTINUE	BLKI 575
C		BLKI 580
C	----- UP DATA THE ITERATE	BLKI 585
C		BLKI 590
	DO 680 NP=1,NNP	BLKI 595
	680 CW(NP)=C(NP)	BLKI 600
C		BLKI 605
C	----- PRINT ITERATION INFORMATION	BLKI 610
C		BLKI 615
	IF(IBUG.NE.0 .AND. KPR.NE.0) PRINT 1100, IT,DIFMAX,TOLB,NOCCUR	BLKI 620
C		BLKI 625
	IF(IT.EQ.1) GO TO 690	BLKI 630
C		BLKI 635
	IF(DIFMAX.LT.TOLB) GO TO 990	BLKI 640
C		BLKI 645
	690 CONTINUE	BLKI 650

C		BLKI 655
	PRINT 2000, IT,NITER,DIFMAX,TOLB,NOCCUR	BLKI 660
C		BLKI 665
C		BLKI 670
	990 CONTINUE	BLKI 675
C		BLKI 680
	1000 FORMAT(1H0//75X,' IT DIFMAX TOLB NOCCUR'/75X,	BLKI 685
	1 ' -- -----')	BLKI 690
	1100 FORMAT(1H ,75X,15,2D12.4,110)	BLKI 695
	2000 FORMAT(1H0/60X,' *** WARNING: NO CONVERGENCE IN BLKI AFTER ',I4,	BLKI 700
	1 ' ITERATIONS'/60X,' NITER -',I4,' DIFMAX -',D11.4,	BLKI 705
	2 ' TOLB -',D11.4,' NOCCUR -',I4)	BLKI 710
C		BLKI 715
	RETURN	BLKI 720
	END	BLKI 725

	SUBROUTINE SOLVE(KKK,C,R,NNP,IHALFB,MAXNP,MAXBW)	SOLV 005
C		SOLV 010
	C*****1*****2*****3*****4*****5*****6*****7**	SOLV 015
C		SOLV 020
	C ----- TO SOVE A MATRIX EQUATION WITH BAND MATRIX SOLVER.	SOLV 025
C		SOLV 030
	C*****1*****2*****3*****4*****5*****5*****7**	SOLV 035
C		SOLV 040
	C ----- INPUT: C(NEQ,NBAND), R(NEQ), NNP, IHALFB, KKK,	SOLV 045
C	WHERE NNP=NEQ AND IHALFB=(NBAND-1)/2	SOLV 050
C		SOLV 055
	C ----- OUTPUT: C(NEQ).	SOLV 060
C		SOLV 065
	C*****1*****2*****3*****4*****5*****6*****7**	SOLV 070
C		SOLV 075
	IMPLICIT REAL*8(A-H,O-Z)	SOLV 080
C		SOLV 085
	DIMENSION C(MAXNP,MAXBW),R(MAXNP)	SOLV 090
C		SOLV 095
	IHBP=IHALFB+1	SOLV 100
C		SOLV 105
	C IF KKK = 1, THEN TRIANGULARIZE THE BAND MATRIX C(NP,IB), BUT	SOLV 110
C	IF KKK = 2, THEN SIMPLY SOLVE WITH THE RIGHT-HAND SIDE R(NP)	SOLV 115
C		SOLV 120
	IF (KKK.EQ.2) GO TO 50	SOLV 125

C		SOLV 130
C	TRIANGULARIZE MATRIX C(NP, IB)	SOLV 135
C		SOLV 140
	NU=NNP-IHALFB	SOLV 145
	DO 20 NI-1, NU	SOLV 150
	PIVOTI=1.0DO/C(NI, IHBP)	SOLV 155
	NJ=NI+1	SOLV 160
	IB=IHBP	SOLV 165
	NK=NI+IHALFB	SOLV 170
	DO 10 NL=NJ, NK	SOLV 175
	IB=IB-1	SOLV 180
	A=-C(NL, IB)*PIVOTI	SOLV 185
	C(NL, IB)=A	SOLV 190
	JB=IB+1	SOLV 195
	KB=IB+IHALFB	SOLV 200
	LB=IHBP-IB	SOLV 205
	DO 10 MB=JB, KB	SOLV 210
	NB=LB+MB	SOLV 215
10	C(NL, MB)=C(NL, MB)+A*C(NI, NB)	SOLV 220
20	CONTINUE	SOLV 225
	NR=NU+1	SOLV 230
	NU=NNP-1	SOLV 235
	NK=NNP	SOLV 240
	IF(NR.GT.NU) RETURN	SOLV 245
	DO 40 NI=NR, NU	SOLV 250
	PIVOTI=1.0DO/C(NI, IHBP)	SOLV 255
	NJ=NI+1	SOLV 260
	IB=IHBP	SOLV 265
	DO 30 NL=NJ, NK	SOLV 270
	IB=IB-1	SOLV 275
	A=-C(NL, IB)*PIVOTI	SOLV 280
	C(NL, IB)=A	SOLV 285
	JB=IB+1	SOLV 290
	KB=IB+IHALFB	SOLV 295
	LB=IHBP-IB	SOLV 300
	DO 30 MB=JB, KB	SOLV 305
	NB=LB+MB	SOLV 310
30	C(NL, MB)=C(NL, MB)+A*C(NI, NB)	SOLV 315
40	CONTINUE	SOLV 320
	RETURN	SOLV 325
C		SOLV 330
C	MODIFY LOAD VECTOR R(NP)	SOLV 335
C		SOLV 340
	50 NU=NNP+1	SOLV 345
	IBAND=2*IHALFB+1	SOLV 350
	DO 70 NI=2, IHBP	SOLV 355
	IB=IHBP-NI+1	SOLV 360
	NJ=1	SOLV 365
	SUM=0.0	SOLV 370

	DO 60 JB=IB, IHALFB	SOLV 375
	SUM=SUM+C(NI, JB)*R(NJ)	SOLV 380
60	NJ=NJ+1	SOLV 385
70	R(NI)=R(NI)+SUM	SOLV 390
	IB=1	SOLV 395
	NL=IHBP+1	SOLV 400
	DO 90 NI=NL, NNP	SOLV 405
	NJ=NI-IHBP+1	SOLV 410
	SUM=0.0	SOLV 415
	DO 80 JB=IB, IHALFB	SOLV 420
	SUM=SUM+C(NI, JB)*R(NJ)	SOLV 425
80	NJ=NJ+1	SOLV 430
90	R(NI)=R(NI)+SUM	SOLV 435
C		SOLV 440
C	BACK SOLVE	SOLV 445
C		SOLV 450
	R(NNP)=R(NNP)/C(NNP, IHBP)	SOLV 455
	DO 110 IB=2, IHBP	SOLV 460
	NI=NU-IB	SOLV 465
	NJ=NI	SOLV 470
	MB=IHALFB+IB	SOLV 475
	SUM=0.0	SOLV 480
	DO 100 JB=NL, MB	SOLV 485
	NJ=NJ+1	SOLV 490
100	SUM=SUM+C(NI, JB)*R(NJ)	SOLV 495
110	R(NI)=(R(NI)-SUM)/C(NI, IHBP)	SOLV 500
	MB=IBAND	SOLV 505
	DO 130 IB=NL, NNP	SOLV 510
	NI=NU-IB	SOLV 515
	NJ=NI	SOLV 520
	SUM=0.0	SOLV 525
	DO 120 JB=NL, MB	SOLV 530
	NJ=NJ+1	SOLV 535
120	SUM=SUM+C(NI, JB)*R(NJ)	SOLV 540
130	R(NI)=(R(NI)-SUM)/C(NI, IHBP)	SOLV 545
	RETURN	SOLV 550
	END	SOLV 555

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SUBROUTINE SFLOW(X,Y,Z,IE,H,HP,VX,VY,VZ,TH,DTH,
1 BFLX,BFLXP,DCOSB,ISB,NPBB,MSEL,SOS,ISTYP,NPW,WSS,IWTYP,
2 NPVB,NPDB,NPCB,NPNB,DELT,KFLOW)
C
C*****1*****2*****3*****4*****5*****6*****7**
C
C ----- TO COMPUTE WATER FLUXES, INCREMENTAL FLOW, AND ACCUMULATED
C ----- FLOW THROUGH ALL TYPES OF BOUNDARIES AND CHANGE OF WATER
C ----- STORED IN THE REGION OF INTEREST.
C
C*****1*****2*****3*****4*****5*****6*****7**
C
C ----- INPUT: X(NNP), Y(NNP), Z(NNP), IE(NEL,9), H(NNP), HP(NNP),
C ----- VX(NNP), VY(NNP), VZ(NNP), TH(8,NEL), DTH(8,NEL),
C ----- DCOSB(3,NBES), ISB(6,NBES), NPBB(NBNP), MSEL(NSEL),
C ----- SOS(NSPR), ISTYP(NSEL), NPW(NWNP), WSS(NWPR),
C ----- IWTYP(NWNP), NPVB(NVNP), NPDB(NDNP), NPCB(NCNP),
C ----- NPNB(NNNP), DELT, KFLOW.
C
C ----- OUTPUT: FRATE(10), FLOW(10), TFLOW(10).
C
C ----- WORKING ARRAYS: BFLX(NBNP), BFLXP(NBNP).
C
C*****1*****2*****3*****4*****5*****6*****7**
C
C      IMPLICIT REAL*8(A-H,O-Z)
C
C      COMMON /SGEOM/ MAXEL,MAXNP,MAXBES,MAXBNP,JBAND,MAXNTI
C      COMMON /CGEOM/ NNP,NEL,NBNP,NBES,GRAV,NTI
C
C      COMMON /CS/ MXSEL,MXSPR,MXSDP,NSEL,NSPR,NSDP
C      COMMON /CW/ MXWNP,MXWPR,MXWDP,NWNP,NWPR,NWDP
C
C      COMMON /CVBC/ MXVES,MXVNP,MXRPR,MXRDV,NVES,NVNP,NRPR,NRDP
C      COMMON /CDBC/ MXDNP,MXDPR,MXDDP,NDNP,NDPR,NDDP
C      COMMON /CCBC/ MXCNP,MXCES,MXCPR,MXCDP,NCNP,NCES,NCPR,NCDP
C      COMMON /CNBC/ MXNNP,MXNES,MXNPR,MXNDP,NNNP,NNES,NNPR,NNDP
C
C      COMMON /CFLOW/ FRATE(10),FLOW(10),TFLOW(10)
C
C      DIMENSION X(MAXNP),Y(MAXNP),Z(MAXNP),IE(MAXEL,9)
C
C      DIMENSION H(MAXNP),HP(MAXNP),VX(MAXNP),VY(MAXNP),VZ(MAXNP)
C      DIMENSION TH(8,MAXEL),DTH(8,MAXEL)
C
C      DIMENSION BFLX(MAXBNP),BFLXP(MAXBNP)
C      DIMENSION DCOSB(3,MAXBES),ISB(6,MAXBES),NPBB(MAXBNP)
C
C      DIMENSION SOS(MXSPR),MSEL(MXSEL),ISTYP(MAXEL)
C      DIMENSION WSS(MXWPR),NPW(MXWNP),IWTYP(MXWNP)

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SFLO 005

SFLO 010

SFLO 015

SFLO 020

SFLO 025

SFLO 030

SFLO 035

SFLO 040

SFLO 045

SFLO 050

SFLO 055

SFLO 060

SFLO 065

SFLO 070

SFLO 075

SFLO 080

SFLO 085

SFLO 090

SFLO 095

SFLO 100

SFLO 105

SFLO 110

SFLO 115

SFLO 120

SFLO 125

SFLO 130

SFLO 135

SFLO 140

SFLO 145

SFLO 150

SFLO 155

SFLO 160

SFLO 165

SFLO 170

SFLO 175

SFLO 180

SFLO 185

SFLO 190

SFLO 195

SFLO 200

SFLO 205

SFLO 210

SFLO 215

SFLO 220

SFLO 225

SFLO 230

SFLO 235

SFLO 240

SFLO 245

SFLO 250

C		SFLO 255
	DIMENSION NPVB(MXVNP), NPDB(MXDNP), NPCB(MXCNP), NPNB(MXNNP)	SFLC 260
C		SFLO 265
	DIMENSION XQ(8), YQ(8), ZQ(8), DHQ(8), THG(8)	SFLO 270
	DIMENSION R1Q(4), R2Q(4), XXQ(4), YYQ(4), ZZQ(4), F1Q(4), F2Q(4)	SFLO 275
C		SFLO 280
	DIMENSION KGB(4,6)	SFLO 285
C		SFLO 290
	DATA KGB/1,4,8,5, 1,2,6,5, 2,3,7,6, 4,3,7,8, 1,2,3,4, 5,6,7,8/	SFLO 295
	DATA QSOS/0.0DO/	SFLO 300
C		SFLO 305
	DO 110 NP-1, NBNP	SFLO 310
	BFLXP(NP)-BFLX(NP)	SFLO 315
	110 BFLX(NP)-0.0	SFLO 320
C		SFLO 325
C	***** CALCULATE VOLUMETRIC FLOW RATE THROUGH ALL BOUNDARY NODES.	SFLO 330
C		SFLO 335
	DO 170 MP-1, NBES	SFLO 340
C		SFLO 345
	LS=ISB(5,MP)	SFLO 350
	M=ISB(6,MP)	SFLO 355
C		SFLO 360
	DO 120 IQ-1,4	SFLO 365
	I=KGB(IQ,LS)	SFLO 370
	NI=IE(M,I)	SFLO 375
	XXQ(IQ)-X(NI)	SFLO 380
	YYQ(IQ)-Y(NI)	SFLO 385
	ZZQ(IQ)-Z(NI)	SFLO 390
	F1Q(IQ)=DCOSB(1,MP)*VX(NI)+DCOSB(2,MP)*VY(NI)+DCOSB(3,MP)*VZ(NI)	SFLO 395
	F2Q(IQ)=0.0	SFLO 400
	120 CONTINUE	SFLO 405
C		SFLO 410
	CALL Q4S(R1Q,R2Q,XXQ,YYQ,ZZQ,F1Q,F2Q)	SFLO 415
C		SFLO 420
	DO 140 IQ-1,4	SFLO 425
	NII=ISB(IQ,MP)	SFLO 430
	BFLX(NII)-BFLX(NII)+R1Q(IQ)	SFLO 435
	140 CONTINUE	SFLO 440
	170 CONTINUE	SFLO 445
C		SFLO 450
	IF (KFLOW.GT.0) GO TO 200	SFLO 455
	DO 180 NP-1, NBNP	SFLO 460
	180 BFLXP(NP)-BFLX(NP)	SFLO 465
C		SFLO 470
	DO 190 I-1,9	SFLO 475
	190 TFLOW(I)=0.0	SFLO 480

C		SFLO 485
C	***** DETERMINE TOTAL FLOWS AND TOTAL FLOW RATES THROUGH VARIOUS	SFLO 490
C	***** TYPES OF BOUNDARIES, STARTING WITH THE NET FLOWS THROUGH THE	SFLO 495
C	***** ENTIRE BOUNDARY.	SFLO 500
C		SFLO 505
	200 SUM=0.	SFLO 510
	SUMP=0.	SFLO 515
	DO 210 NP=1,NBNP	SFLO 520
	SUM=SUM+BFLX(NP)	SFLO 525
	210 SUMP=SUMP+BFLXP(NP)	SFLO 530
C		SFLO 535
	FRATE(7)=SUM	SFLO 540
	FLOW(7)=0.5DO*(SUM+SUMP)*DELT	SFLO 545
C		SFLO 550
C	***** THE DIRICHLET BOUNDARY	SFLO 555
C		SFLO 560
	FRATE(1)=0.	SFLO 565
	FLOW(1)=0.	SFLO 570
	IF(NDNP.LE.0) GO TO 400	SFLO 575
	SUM=0.	SFLO 580
	SUMP=0.	SFLO 585
	DO 330 NPP=1,NDNP	SFLO 590
	NII=NPDB(NPP)	SFLO 595
	SUM=SUM+BFLX(NII)	SFLO 600
	SUMP=SUMP+BFLXP(NII)	SFLO 605
	330 CONTINUE	SFLO 610
	FRATE(1)=SUM	SFLO 615
	FLOW(1)=0.5DO*(SUM+SUMP)*DELT	SFLO 620
C		SFLO 625
C		SFLO 630
C	***** THE CAUCHY BOUNDARY	SFLO 635
C		SFLO 640
	400 FRATE(2)=0.0	SFLO 645
	FLOW(2)=0.0	SFLO 650
	IF(NCNP.LE.0) GO TO 500	SFLO 655
	SUM=0.0	SFLO 660
	SUMP=0.0	SFLO 665
	DO 430 NPP=1,NCNP	SFLO 670
	NII=NPCB(NPP)	SFLO 675
	SUM=SUM+BFLX(NII)	SFLO 680
	SUMP=SUMP+BFLXP(NII)	SFLO 685
	430 CONTINUE	SFLO 690
	FRATE(2)=SUM	SFLO 695
	FLOW(2)=0.5DO*(SUM+SUMP)*DELT	SFLO 700

C		SFLO 705
C		SFLO 710
C	***** THE NEUMANN BOUNDARY	SFLO 715
C		SFLO 720
	500 FRATE(3)-0.	SFLO 725
	FLOW(3)-0.	SFLO 730
	IF(NNNP.LE.0) GO TO 600	SFLO 735
	SUM-0.	SFLO 740
	SUMP-0.	SFLO 745
	DO 530 NPP-1,NNNP	SFLO 750
	NII-NPNB(NPP)	SFLO 755
	SUM-SUM+BFLX(NII)	SFLO 760
	SUMP-SUMP+BFLXP(NII)	SFLO 765
	530 CONTINUE	SFLO 770
	FRATE(3)-SUM	SFLO 775
	FLOW(3)-0.5D0*(SUM+SUMP)*DELT	SFLO 780
C		SFLO 785
C	***** THE RAINFALL-SEEPAGE BOUNDARY	SFLO 790
C		SFLO 795
	600 FRATE(4)-0.	SFLO 800
	FLOW(4)-0.	SFLO 805
	FRATE(5)-0.	SFLO 810
	FLOW(5)-0.	SFLO 815
	IF(NVNP.LE.0) GO TO 700	SFLO 820
	SUMS-0.	SFLO 825
	SUMSP-0.	SFLO 830
	SUMR-0.	SFLO 835
	SUMRP-0.	SFLO 840
	DO 640 NPP-1,NVNP	SFLO 845
	NII-NPVB(NPP)	SFLO 850
	BFLXA-BFLX(NII)	SFLO 855
	IF (BFLXA.LT.0.D0) GO TO 630	SFLO 860
	SUMS-SUMS+BFLX(NII)	SFLO 865
	SUMSP-SUMSP+BFLXP(NII)	SFLO 870
	GO TO 640	SFLO 875
	630 SUMR-SUMR+BFLX(NII)	SFLO 880
	SUMRP-SUMRP+BFLXP(NII)	SFLO 885
	640 CONTINUE	SFLO 890
	FRATE(4)-SUMS	SFLO 895
	FLOW(4)-0.5D0*(SUMS+SUMSP)*DELT	SFLO 900
	FRATE(5)-SUMR	SFLO 905
	FLOW(5)-0.5D0*(SUMR+SUMRP)*DELT	SFLO 910

C		SFLO 915
C	***** THE UNSPECIFIED BOUNDARY, I. E. BOUNDARY WITH ZERO TOTAL FLUX	SFLO 920
C		SFLO 925
	700 SUM=0.	SFLO 930
	SUMP=0.	SFLO 935
	DO 710 I=1,5	SFLO 940
	SUM=SUM+FRATE(I)	SFLO 945
	710 SUMP=SUMP+FLOW(I)	SFLO 950
	FRATE(6)=FRATE(7)-SUM	SFLO 955
	FLOW(6)=FLOW(7)-SUMP	SFLO 960
C		SFLO 965
C	***** CALCULATE THE INCREASE IN THE WATER CONTENT AND THE SOURCE	SFLO 970
C		SFLO 975
	QSOSP=QSOS	SFLO 980
	QSOS=0.0	SFLO 985
	QTH=0.	SFLO 990
	DO 850 M=1,NEL	SFLO 995
C		SFLO1000
	SOURCE=0.0	SFLO1005
	IF(NSEL.EQ.0) GO TO 830	SFLO1010
	DO 810 MP=1,NSEL	SFLO1015
	MS=MSEL(MP)	SFLO1020
	IF(MS.NE.M) GO TO 810	SFLO1025
	ITYP=ISTYP(MP)	SFLO1030
	SOURCE=SOS(ITYP)	SFLO1035
	GO TO 830	SFLO1040
	810 CONTINUE	SFLO1045
C		SFLO1050
	830 DO 840 IQ=1,8	SFLO1055
	NP=IE(M,IQ)	SFLO1060
	XQ(IQ)=X(NP)	SFLO1065
	YQ(IQ)=Y(NP)	SFLO1070
	ZQ(IQ)=Z(NP)	SFLO1075
	DHQ(IQ)=H(NP)-HP(NP)	SFLO1080
	IF(KFLOW.LE.0) DHQ(IQ)=1.0D0	SFLO1085
	THG(IQ)=TH(IQ,M)	SFLO1090
	IF(KFLOW.GT.0) THG(IQ)=DTH(IQ,M)	SFLO1095
	840 CONTINUE	SFLO1100
C		SFLO1105
	CALL Q8TH(QTHM,QSOSM,DHQ,THG,XQ,YQ,ZQ,SOURCE)	SFLO1110
C		SFLO1115
	QSOS=QSOS-QSOSM	SFLO1120
	QTH=QTH+QTHM	SFLO1125
	850 CONTINUE	SFLO1130
C		SFLO1135
	IF(NWNP.EQ.0) GO TO 870	SFLO1140
	DO 860 I=1,NWNP	SFLO1145
	ITYP=IWTYP(I)	SFLO1150
	860 QSOS=QSOS-WSS(ITYP)	SFLO1155
	870 CONTINUE	SFLO1160

C	IF(KFLOW.GT.0) GO TO 880	SFL01165
	QSOSP-QSOS	SFL01170
C		SFL01175
	880 FRATE(8)-QSOS	SFL01180
	FLOW(8)-0.5D0*(QSOS+QSOSP)*DELT	SFL01185
	FLOW(9)-QTH	SFL01190
	FRATE(9)-FLOW(9)/DELT	SFL01195
	IF(KFLOW.LE.0) FRATE(9)--(FRATE(7)+FRATE(8))	SFL01200
C		SFL01205
	DO 910 I=1,9	SFL01210
	910 TFLOW(I)-TFLOW(I)+FLOW(I)	SFL01215
C		SFL01220
	RETURN	SFL01225
	END	SFL01230
		SFL01235

	SUBROUTINE Q8TH(QTHM, QSOSM, DHQ, THG, XQ, YQ, ZQ, SOURCE)	Q8TH 005
C		Q8TH 010
	C*****1*****2*****3*****4*****5*****6*****7**	Q8TH 015
C		Q8TH 020
C	----- TO COMPUTE WATER CONTENT INTEGRATION AND ELEMENT SOURCE	Q8TH 025
C	----- INTEGRATION OVER AN ELEMENT.	Q8TH 030
C		Q8TH 035
	C*****1*****2*****3*****4*****5*****6*****7**	Q8TH 040
C		Q8TH 045
C	----- INPUT: DHQ(8), THG(8), XQ(8), YQ(8), ZQ(8), SOURCE.	Q8TH 050
C		Q8TH 055
C	----- OUTPUT: QTHM, QSOSM.	Q8TH 060
C		Q8TH 065
	C*****1*****2*****3*****4*****5*****6*****7**	Q8TH 070
C		Q8TH 075
	IMPLICIT REAL*8 (A-H,O-Z)	Q8TH 080
	REAL*8 N(8)	Q8TH 085
C		Q8TH 090
	DIMENSION DHQ(8), THG(8), XQ(8), YQ(8), ZQ(8)	Q8TH 095
	DIMENSION PJAB(3,3), DNSS(8), DNIT(8), DNUU(8)	Q8TH 100
	DIMENSION S(8), T(8), U(8)	Q8TH 105
C		Q8TH 110
	DATA P / 0.577350269189626D0/	Q8TH 115
	DATA S / -1.0D0, 1.0D0, 1.0D0, -1.0D0, -1.0D0, 1.0D0, 1.0D0, -1.0D0/	Q8TH 120
	DATA T / -1.0D0, -1.0D0, 1.0D0, 1.0D0, -1.0D0, -1.0D0, 1.0D0, 1.0D0/	Q8TH 125
	DATA U / -1.0D0, -1.0D0, -1.0D0, -1.0D0, 1.0D0, 1.0D0, 1.0D0, 1.0D0/	Q8TH 130

C	QSOSM-0.0	Q8TH 135
	QTHM-0.	Q8TH 140
	DO 490 KG-1,8	Q8TH 145
C		Q8TH 150
C	----- DETERMINE LOCAL COORDINATE OF GAUSSIAN POINT KG	Q8TH 155
C		Q8TH 160
	SS-P*S(KG)	Q8TH 165
	TT-P*T(KG)	Q8TH 170
	UU-P*U(KG)	Q8TH 175
C		Q8TH 180
	SM-1.0DO-SS	Q8TH 185
	SP-1.0DO+SS	Q8TH 190
	TM-1.0DO-TT	Q8TH 195
	TP-1.0DO+TT	Q8TH 200
	UM-1.0DO-UU	Q8TH 205
	UP-1.0DO+UU	Q8TH 210
C		Q8TH 215
C	----- CALCULATE VALUES OF BASIS FUNCTIONS N(IQ).	Q8TH 220
C		Q8TH 225
	N(1)-0.125DO*SM*TM*UM	Q8TH 230
	N(2)-0.125DO*SP*TM*UM	Q8TH 235
	N(3)-0.125DO*SP*TP*UM	Q8TH 240
	N(4)-0.125DO*SM*TP*UM	Q8TH 245
	N(5)-0.125DO*SM*TM*UP	Q8TH 250
	N(6)-0.125DO*SP*TM*UP	Q8TH 255
	N(7)-0.125DO*SP*TP*UP	Q8TH 260
	N(8)-0.125DO*SM*TP*UP	Q8TH 265
C		Q8TH 270
	DNSS(1)--0.125DO*TM*UM	Q8TH 275
	DNSS(2)- 0.125DO*TM*UM	Q8TH 280
	DNSS(3)- 0.125DO*TP*UM	Q8TH 285
	DNSS(4)--0.125DO*TP*UM	Q8TH 290
	DNSS(5)--0.125DO*TM*UP	Q8TH 295
	DNSS(6)- 0.125L0*TM*UP	Q8TH 300
	DNSS(7)- 0.125DO*TP*UP	Q8TH 305
	DNSS(8)--0.125DO*TP*UP	Q8TH 310
C		Q8TH 315
	DNTT(1)--0.125DO*SM*UM	Q8TH 320
	DNTT(2)--0.125DO*SP*UM	Q8TH 325
	DNTT(3)- 0.125DO*SP*UM	Q8TH 330
	DNTT(4)- 0.125DO*SM*UM	Q8TH 335
	DNTT(5)--0.125DO*SM*UP	Q8TH 340
	DNTT(6)--0.125DO*SP*UP	Q8TH 345
	DNTT(7)- 0.125DO*SP*UP	Q8TH 350
	DNTT(8)- 0.125DO*SM*UP	Q8TH 355
		Q8TH 360

C	DNUU(1)--0.125DO*SM*TM	Q8TH 365
	DNUU(2)--0.125DO*SP*TM	Q8TH 370
	DNUU(3)--0.125DO*SP*TP	Q8TH 375
	DNUU(4)--0.125DO*SM*TP	Q8TH 380
	DNUU(5)- 0.125DO*SM*TM	Q8TH 385
	DNUU(6)- 0.125DO*SP*TM	Q8TH 390
	DNUU(7)- 0.125DO*SP*TP	Q8TH 395
	DNUU(8)- 0.125DO*SM*TP	Q8TH 400
C	DO 210 J-1,3	Q8TH 405
	DO 210 I-1,3	Q8TH 410
210	PJAB(I,J)-0.0	Q8TH 415
C	DO 220 I-1,8	Q8TH 420
	PJAB(1,1)-PJAB(1,1)+XQ(I)*DNSS(I)	Q8TH 425
	PJAB(1,2)-PJAB(1,2)+YQ(I)*DNSS(I)	Q8TH 430
	PJAB(1,3)-PJAB(1,3)+ZQ(I)*DNSS(I)	Q8TH 435
	PJAB(2,1)-PJAB(2,1)+XQ(I)*DNSS(I)	Q8TH 440
	PJAB(2,2)-PJAB(2,2)+YQ(I)*DNSS(I)	Q8TH 445
	PJAB(2,3)-PJAB(2,3)+ZQ(I)*DNSS(I)	Q8TH 450
	PJAB(3,1)-PJAB(3,1)+XQ(I)*DNSS(I)	Q8TH 455
	PJAB(3,2)-PJAB(3,2)+YQ(I)*DNSS(I)	Q8TH 460
	PJAB(3,3)-PJAB(3,3)+ZQ(I)*DNSS(I)	Q8TH 465
220	CONTINUE	Q8TH 470
C	DJAC-PJAB(1,1)*(PJAB(2,2)*PJAB(3,3)-PJAB(2,3)*PJAB(3,2)) -	Q8TH 475
1	PJAB(1,2)*(PJAB(2,1)*PJAB(3,3)-PJAB(2,3)*PJAB(3,1)) +	Q8TH 480
2	PJAB(1,3)*(PJAB(2,1)*PJAB(3,2)-PJAB(2,2)*PJAB(3,1))	Q8TH 485
C	----- INTERPOLATE TO OBTAIN WATER CONTENT AT THE GAUSSIAN POINT KG	Q8TH 490
C	DHQP=0.0	Q8TH 495
	DO 390 IQ-1,8	Q8TH 500
	DHQP=DHQP+DHQ(IQ)*N(IQ)	Q8TH 505
390	CONTINUE	Q8TH 510
C	THQP=DHQP*THG(KG)	Q8TH 515
C	----- ACCUMULATE THE SUM TO EVALUATE THE INTEGRAL	Q8TH 520
C	QSOSM-QSOSM+SOURCE*DJAC	Q8TH 525
	QTHM-QTHM+THQP*DJAC	Q8TH 530
490	CONTINUE	Q8TH 535
C	RETURN	Q8TH 540
	END	Q8TH 545
		Q8TH 550
		Q8TH 555
		Q8TH 560
		Q8TH 565
		Q8TH 570
		Q8TH 575
		Q8TH 580
		Q8TH 585
		Q8TH 590
		Q8TH 595

```

SUBROUTINE PRINTT(VX,VY,VZ,H,HT,TH, NPBB,BFLX, NPVB,DCYFLX,NPCON, PRIN 005
1 NPFLX,NPMIN, SUBHD, TIME,DELT, KPR,KOUT,KDIAG,ITIM) PRIN 010
C PRIN 015
C*****1*****2*****3*****4*****5*****6*****7**PRIN 020
C PRIN 025
C ----- TO OUTPUT FLOWS, PRESSURE HEAD, TOTAL HEAD, WATER CONTENT, PRIN 030
C ----- AND DARCY'S VELOCITY AS SPECIFIED BY THE PARAMETER KPR. PRIN 035
C PRIN 040
C*****1*****2*****3*****4*****5*****6*****7**PRIN 045
C PRIN 050
C ----- INPUT: VX(NNP), VY(NNP), VZ(NNP), H(NNP), HT(NNP), TH(8,NEL), PRIN 055
C ----- NPBB(NBNP), DCYFLX(NVNP), NPCON(NVNP), NPFLX(NVNP), PRIN 060
C ----- NPMIN(NVNP), SUBHD(8), TIME, DELT, KPR, KOUT, KDIAG, PRIN 065
C ----- ITIM. PRIN 070
C PRIN 075
C ----- OUTPUT: LINE PRINT ALL INPUTS IF NEEDED EXCEPT FOR KPR. PRIN 080
C PRIN 085
C*****1*****2*****3*****4*****5*****6*****7**PRIN 090
C PRIN 095
      IMPLICIT REAL*8(A-H,O-Z) PRIN 100
      REAL*4 SUBHD PRIN 105
C PRIN 110
      COMMON /SGEOM/ MAXEL,MAXNP,MAXBES,MAXBNP,JBAND,MAXNTI PRIN 115
      COMMON /CGEOM/ NNP,NEL,NBNP,NBES,KGRAV,NTI PRIN 120
      COMMON /CVBC/ MXVES,MXVNP,MXRPR,MXRDP,NVES,NVNP,NRPR,NRDP PRIN 125
C PRIN 130
      COMMON /CFLOW/ FRATE(10),FLOW(10),TFLOW(10) PRIN 135
C PRIN 140
      DIMENSION VX(MAXNP),VY(MAXNP),VZ(MAXNP),H(MAXNP),HT(MAXNP) PRIN 145
      DIMENSION TH(8,MAXEL) PRIN 150
      DIMENSION NPBB(MAXBNP),BFLX(MAXBNP) PRIN 155
      DIMENSION NPVB(MXVNP),NPCON(MXVNP),NPFLX(MXVNP),NPMIN(MXVNP) PRIN 160
      DIMENSION DCYFLX(MXVNP) PRIN 165
C PRIN 170
      DIMENSION SUBHD(8) PRIN 175
C PRIN 180
      IF(KPR.EQ.0) RETURN PRIN 185
C PRIN 190
C -----PRINT DIAGNOSTIC FLOW INFORMATION PRIN 195
C PRIN 200
      KDIAG=KDIAG+1 PRIN 205
      KDIA=KDIAG-1 PRIN 210
      PRINT 1000, KDIA,TIME,DELT,ITIM,(FRATE(I),FLOW(I),TFLOW(I),I-1,9) PRIN 215
      IF (NVNP.EQ.0) GO TO 130 PRIN 220
      DO 120 NPP-1,NVNP PRIN 225
      NKK=NPVB(NPP) PRIN 230
120 DCYFLX(NPP)=BFLX(NKK) PRIN 235
      PRINT 1100 PRIN 240
      PRINT 1110, (DCYFLX(NPP),NPP-1,NVNP) PRIN 245
      PRINT 1120, (NPCON(NPP),NPP-1,NVNP) PRIN 250

```


PRINT 1125, (NPMIN(NPP),NPP-1,NVNP)	PRIN 255
PRINT 1130, (NPFLX(NPP),NPP-1,NVNP)	PRIN 260
130 IF (KPR.EQ.1) RETURN	PRIN 265
C	PRIN 270
C ----- PRINT PRESSURE HEADS	PRIN 275
C	PRIN 280
KOUT=KOUT+1	PRIN 285
KLINE--1	PRIN 290
PRINT 2000, KOUT,TIME,DELT,JBAND,ITIM,(SUBHD(I),I-1,8)	PRIN 295
DO 210 NI-1,NNP,8	PRIN 300
NJMN=NI	PRIN 305
NJMX=MINO(NI+7,NNP)	PRIN 310
KLINE=KLINE+1	PRIN 315
IF(MOD(KLINE,50).EQ.0 .AND. KLINE.GE.1) PRINT 2000, KOUT,TIME,	PRIN 320
> DELT,JBAND,ITIM,(SUBHD(I),I-1,8)	PRIN 325
310 PRINT 2100, NI,(H(NJ),NJ-NJMN,NJMX)	PRIN 330
IF (KPR.EQ.2) RETURN	PRIN 335
C	PRIN 340
C ----- PRINT TOTAL HEADS	PRIN 345
C	PRIN 350
KOUT=KOUT+1	PRIN 355
KLINE--1	PRIN 360
PRINT 3000, KOUT,TIME,DELT,JBAND,ITIM,(SUBHD(I),I-1,8)	PRIN 365
DO 310 NI-1,NNP,8	PRIN 370
NJMN=NI	PRIN 375
NJMX=MINO(NI+7,NNP)	PRIN 380
KLINE=KLINE+1	PRIN 385
IF(MOD(KLINE,50).EQ.0 .AND. KLINE.GE.1) PRINT 3000, KOUT,TIME,	PRIN 390
> DELT,JBAND,ITIM,(SUBHD(I),I-1,8)	PRIN 395
310 PRINT 2100, NI,(HT(NJ),NJ-NJMN,NJMX)	PRIN 400
IF(KPR.EQ.3) RETURN	PRIN 405
C	PRIN 410
C ----- PRINT WATER CONTENTS	PRIN 415
C	PRIN 420
KOUT=KOUT+1	PRIN 425
KLINE--1	PRIN 430
PRINT 4000, KOUT,TIME,DELT,JBAND,ITIM,(SUBHD(I),I-1,8)	PRIN 435
DO 410 M-1,NEL	PRIN 440
KLINE=KLINE+1	PRIN 445
IF(MOD(KLINE,50).EQ.0 .AND. KLINE.GE.1) PRINT 4000, KOUT,TIME,	PRIN 450
> DELT,JBAND,ITIM,(SUBHD(I),I-1,8)	PRIN 455
410 PRINT 4100, M,(TH(IQ,M),IQ-1,8)	PRIN 460
IF (KPR.EQ.4) RETURN	PRIN 465

```

C
C ----- PRINT DARCY VELOCITIES
C
      KOUT=KOUT+1
      KLINE--1
      PRINT 5000, KOUT, TIME, DELT, JBAND, ITIM, (SUBHD(I), I-1, 8)
      DO 510 NP=1, NNP, 3
      KLINE=KLINE+1
      IF(MOD(KLINE, 50).EQ.0 .AND. KLINE.GE.1) PRINT 5000, KOUT, TIME,
>      DELT, JBAND, ITIM, (SUBHD(I), I-1, 8)
      NJMN=NP
      NJMX=MINO(NP+2, NNP)
510 PRINT 5100, (NJ, VX(NJ), VY(NJ), VZ(NJ), NJ-NJMN, NJMX)
C
      RETURN
C
1000 FORMAT(1H1, ' TABLE OF SYSTEM-FLOW PARAMETERS', 2X, 'TABLE: ', I4,
> ' .. AT TIME =', 1PD12.4, ' ', (DELT =', 1PD12.4, ')', ' ITIM=', 14//5X,
> ' TYPE OF FLOW', 35X, 'RATE(L**3/T )', 3X, 'INC. FLOW(L**3 )', 4X,
> 'TOTAL FLOW(L**3 )'/5X,
1 ' 1. FLOW THROUGH DIRICHLET NODES . . . . .', 3(E12.4, 10X)/5X,
2 ' 2. FLOW THROUGH CAUCHY NODES . . . . .', 3(E12.4, 10X)/5X,
3 ' 3. FLOW THROUGH NEUMANN NODES . . . . .', 3(E12.4, 10X)/5X,
4 ' 4. FLOW THROUGH SEEPAGE NODES . . . . .', 3(E12.4, 10X)/5X,
5 ' 5. FLOW THROUGH INFILTRATION NODES . . . . .', 3(E12.4, 10X)/5X,
6 ' 6. FLOW THROUGH UNSPECIFIED NODES . . . . .', 3(E12.4, 10X)/5X,
7 ' 7. NET FLOW THROUGH ENTIRE BOUNDARY . . . . .', 3(E12.4, 10X)/5X,
8 ' 8. ARTIFICIAL SOURCES/SINKS . . . . .', 3(E12.4, 10X)/5X,
9 ' 9. INCREASE IN WATER CONTENT . . . . .', 3(E12.4, 10X)/5X,
A ' *** NOTE: (+) - OUT FROM, (-) - INTO THE REGION. '//)
1100 FORMAT('/' RAINFALL-SEEPAGE NODAL FLOWS (L**3/T)')
1110 FORMAT(8D15.4)
1120 FORMAT(1H0, ' VALUES OF NPCON'/(8I15))
1125 FORMAT(1H0, ' VALUES OF NPMIN'/(8I15))
1130 FORMAT(1H0, ' VALUES OF NPFLX'/(6I15))
2000 FORMAT('1 OUTPUT TABLE', I4, ' .. PRESSURE HEADS(L) AT TIME =',
1 1PD12.4, ' ', (DELT =', 1PD12.4, '), (BAND WIDTH =', I4, ')', ' IT =',
2 I5//1X, 8A4/1X, ' NODE I', 5X, 'PRESSURE HEAD (L) OF NODES I, I+1, ..',
3 ', I+7 '//)
2100 FORMAT(I7, 8(1PD15.4))
3000 FORMAT('1 OUTPUT TABLE', I4, ' .. TOTAL HEADS(L) AT TIME =', 1PD12.4,
1 ' ', (DELT =', 1PD12.4, '), (BAND WIDTH =', I4, ')', ' IT =', I5//1X, 8A4,
2 /1X, ' NODE I', 5X, 'TOTAL HEAD (L) OF NODES I, I+1, . . . , I+7 '//)
4000 FORMAT('1 OUTPUT TABLE', I4, ' .. WATER CONTENT(L**3/L**3) AT TIME =',
1 1PD12.4, ' ', (DELT =', 1PD12.4, '), (BAND WIDTH =', I4, ')', ' IT =',
3 I5//1X, 8A4//51X, ' GAUSSIAN POINTS'/17X, '1', 14X, '2', 14X, '3', 14X,
4 '4', 14X, '5', 14X, '6', 14X, '7', 14X, '8'/1X, 'ELEMENT', 2X, '* .*****',
5 '*****',
6 '*****')

```

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PRIN 470
PRIN 475
PRIN 480
PRIN 485
PRIN 490
PRIN 495
PRIN 500
PRIN 505
PRIN 510
PRIN 515
PRIN 520
PRIN 525
PRIN 530
PRIN 535
PRIN 540
PRIN 545
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PRIN 600
PRIN 605
PRIN 610
PRIN 615
PRIN 620
PRIN 625
PRIN 630
PRIN 635
PRIN 640
PRIN 645
PRIN 650
PRIN 655
PRIN 660
PRIN 665
PRIN 670
PRIN 675
PRIN 680
PRIN 685
PRIN 690
PRIN 695
PRIN 700
PRIN 705
PRIN 710

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```

4100 FORMAT(1H ,I7,2X,8D15.7) PRIN 715
5000 FORMAT('1 OUTPUT TABLE',I4,'... DARCY VELOCITIES (L/T) AT TIME -', PRIN 720
      1 1PD12.4,' ,(DELT -',1PD12.4,')',(BAND WIDTH -',I4,')', ' IT -', PRIN 725
      2 15//1X,8A4//1X,3(' NODE VX VY VZ', PRIN 730
      3 ' ')/1X,3('*****'/)) PRIN 735
5100 FORMAT(1H ,3(I5,3D11.3)) PRIN 740
      END PRIN 745
  
```

```

      SUBROUTINE STORE(X,Y,Z,IE,H,HT,TH,VX,VY,VZ,DCOSB,ISB,NPBB, STOR 005
      1 NNPLR,GNLR, TITLE, TIME, NPROB) STOR 010
C STOR 015
C*****1*****2*****3*****4*****5*****6*****7**STOR 020
C STOR 025
C ----- TO STORE PERTINENT QUANTITIES ON AUXILIARY DEVICES FOR FUTURE STOR 030
C ----- USES, E. G., FOR PLOTTING. WHAT DEVICE IS TO BE USED MUST BE STOR 035
C ----- SPECIFIED IN THE JCL. STOR 040
C STOR 045
C*****1*****2*****3*****4*****5*****6*****7**STOR 050
C STOR 055
C ----- INPUT: X(NNP), Y(NNP), Z(NNP), IE(NEL,9), H(NNP), HT(NNP), STOR 060
C ----- TH(8,NEL), VX(NNP), VY(NNP), VZ(NNP), DCOSB(3,NBES), STOR 065
C ----- ISB(6,NBES),NPBB(NBNP), NNPLR(MXREGN), STOR 070
C ----- GNLR(LTMXNP,MXREGN), TITLE,TIME,NPROB. STOR 075
C STOR 080
C ----- OUTPUT: STORE ALL INPUTS IN LOGICAL UNIT 1. STOR 085
C STOR 090
C*****1*****2*****3*****4*****5*****6*****7**STOR 095
C STOR 100
      IMPLICIT REAL*8(A-H,O-Z) STOR 105
      INTEGER*4 GNLR STOR 110
C STOR 115
      COMMON /SGEOM/ MAXEL,MAXNP,MAXBES,MAXBNP,JBAND,MAXNTI STOR 120
      COMMON /CGEOM/ NNP,NEL,NBNP,NBES,KGRAV,NTI STOR 125
      COMMON /LGEOM/ LTMXNP,LMXNP,LMXBW,MXREGN,NREGN STOR 130
C STOR 135
      DIMENSION TITLE(9) STOR 140
      DIMENSION X(MAXNP),Y(MAXNP),Z(MAXNP),IE(MAXEL,9) STOR 145
      DIMENSION H(MAXNP),HT(MAXNP),VX(MAXNP),VY(MAXNP),VZ(MAXNP) STOR 150
      DIMENSION TH(8,MAXEL) STOR 155
      DIMENSION DCOSB(3,MAXBES),ISB(6,MAXBES),NPBB(MAXBNP) STOR 160
      DIMENSION NNPLR(MXREGN),GNLR(LTMXNP,MXREGN) STOR 165
C STOR 170
      DATA NPPROB/-1/ STOR 175
  
```

```

C
IF (NPPROB.EQ.(-1)) REWIND 1
IF (NPPROB.EQ.NFROB) GO TO 110
WRITE(1) (TITLE(I), I-1, 9), NPROB, NNP, NEL, NBNP, NBES, NTI
WRITE(1) (X(N), N-1, NNP), (Y(N), N-1, NNP), (Z(N), N-1, NNP),
1 ((IE(M, I), M-1, NEL), I-1, 9), ((DCOSB(I, M), I-1, 3), M-1, NBES),
2 ((ISB(I, M), I-1, 6), M-1, NBES), (NPBB(N), N-1, NBNP), (NNPLR(N), N-1,
3 NREGN), ((GNLR(N, I), N-1, LTMXNP), I-1, NREGN)
NPPROB=NPROB
C
110 WRITE(1) TIME, (H(N), N-1, NNP), (HT(N), N-1, NNP), ((TH(I, M), I-1, 8), M-1,
1 NEL), (VX(N), N-1, NNP), (VY(N), N-1, NNP), (VZ(N), N-1, NNP)
RETURN
END

```

```

STOR 180
STOR 185
STOR 190
STOR 195
STOR 200
STOR 205
STOR 210
STOR 215
STOR 220
STOR 225
STOR 230
STOR 235
STOR 240
STOR 245

```

```

SUBROUTINE INTERP(FALL, TRF, RF, TIME, MXPR, MXDP, NPR, NDP)
C
C*****1*****2*****3*****4*****5*****6*****7**
C
C ----- TO INTERPOLATE FOR THE VALUE FROM THE TABLE INPUT. IF THE
C ----- NUMBER IS OUT OF RANGE, THE FUNCTIONAL VALUE IS SET TO ZERO.
C
C*****1*****2*****3*****4*****5*****6*****7**
C
C ----- INPUT: TRF(NPD,NPR), RF(NPD,NPR), TIME, NPR, AND NPD.
C
C ----- OUTPUT: FALL(NPR).
C
C*****1*****1*****3*****4*****5*****6*****7**
C
C IMPLICIT REAL*8(A-H,O-Z)
C
C DIMENSION FALL(MXPR), TRF(MXDP, MXPR), RF(MXDP, MXPR)
C
DO 160 I=1, NPR
DO 140 J=2, NDP
IF (TRF(J-1, I) .LE. TIME .AND. TIME .LE. TRF(J, I)) GO TO 120
GO TO 140
120 RFJM1=RF(J-1, I)
TRFJM1=TRF(J-1, I)
RFJ=RF(J, I)
RFJ=TRF(J, I)
'BC=RFJ-RFJM1
ABCD=TRFJ-TRFJM1
FALL(I)=RFJM1+(TIME-TRFJM1)*ABC/ABCD

```

```

INTE 005
INTE 010
INTE 015
INTE 020
INTE 025
INTE 030
INTE 035
INTE 040
INTE 045
INTE 050
INTE 055
INTE 060
INTE 065
INTE 070
INTE 075
INTE 080
INTE 085
INTE 090
INTE 095
INTE 100
INTE 105
INTE 110
INTE 115
INTE 120
INTE 125
INTE 130
INTE 135
INTE 140
INTE 145
INTE 150

```

GO TO 160	INTE 155
140 CONTINUE	INTE 160
FALL(I)-0.0	INTE 165
160 CONTINUE	INTE 170
C	INTE 175
RETURN	INTE 180
END	INTE 185

SUBROUTINE READR(F,MAXNOD,NNP)	REDR 005
C	REDR 010
C*****1*****2*****3*****4*****5*****6*****7**	REDR 015
C	REDR 020
C ----- TO AUTOMATICALLY GENERATE REAL NUMBER INPUT.	REDR 025
C	REDR 030
C*****1*****2*****3*****4*****5*****6*****7**	REDR 035
C	REDR 040
IMPLICIT REAL*8(A-H,O-Z)	REDR 045
C	REDR 050
DIMENSION F(MAXNOD)	REDR 055
C	REDR 060
NODES=0	REDR 065
150 READ 40, NI,NSEQ,NAD,FNI,FAD,FRD	REDR 070
IF(NI.EQ.0) GO TO 170	REDR 075
NJ=NI+NSEQ	REDR 080
DO 160 N=NI,NJ	REDR 085
NODES=NODES+1	REDR 090
I=NI+(N-NI)*NAD	REDR 095
IF(FRD.NE.0.0) GO TO 155	REDR 100
F(I)=FNI+FAD*DFLOAT(N-NI)	REDR 105
GO TO 160	REDR 110
155 I1=I-NAD	REDR 115
IF(N.EQ.NI) F(I)=FNI	REDR 120
IF(N.EQ.NI) DINC=1.0D0	REDR 125
IF(N.GT.NI) DINC=DINC*(1.0D0+FRD)	REDR 130
IF(N.GT.NI) F(I)=F(I1)+FAD*DINC	REDR 135
160 CONTINUE	REDR 140
GO TO 150	REDR 145
170 IF(NODES.EQ.NNP) GO TO 180	REDR 150
PRINT 1100	REDR 155
STOP	REDR 160
180 IF(NNP.LE.MAXNOD) GO TO 190	REDR 165
PRINT 1200	REDR 170
STOP	REDR 175
190 CONTINUE	REDR 180

```

C
40 FORMAT(3I5,5X,4D10.3)
1100 FORMAT(1H1/1H ,64H *** ERROR IN EXECUTING READR SINCE NODES .NE.
> NNP: STOP ***)
1200 FORMAT(1H1/1H ,46H *** NNP .GT. MAXNOD IN EXECUTING READR: STOP)
C
RETURN
END

```

REDR 185
REDR 190
REDR 195
REDR 200
REDR 205
REDR 210
REDR 215
REDR 220

```

SUBROUTINE READN(INDTYP,MXTYP,NTYPE)
C
C*****1*****2*****3*****4*****5*****6*****7**
C
C ----- TO AUTOMATICALLY GENERATE INTEGER INPUT.
C
C*****1*****2*****3*****4*****5*****6*****7**
C
IMPLICIT REAL*8(A-H,O-Z)
C
DIMENSION INDTYP(MXTYP)
C
NTYPES=0
110 READ 30,NI,NSEQ,NAD,NITYP,NTYPAD
IF(NI.EQ.0) GO TO 130
NJ=NI+NSEQ
DO 120 N=NI,NJ
I=NI+(N-NI)*NAD
INDTYP(I)=NITYP + (N-NI)*NTYPAD
NTYPES=NTYPES+1
120 CONTINUE
GO TO 110
130 IF(NTYPES.EQ.NTYPE) GO TO 140
PRINT 1100
STOP
140 IF(NTYPE.LE.MXTYP) GO TO 150
PRINT 1200
STOP
150 CONTINUE
C
30 FORMAT(5I5)
1100 FORMAT(1H1/1H ,64H *** ERROR IN EXECUTING READN SINCE NTYPES .NE.
> NTYPE: STOP ***)
1200 FORMAT(1H1/1H ,46H *** NTYPE .GT. MXTYP IN EXECUTING READN: STOP)
C
RETURN
END

```

REDN 005
REDN 010
REDN 015
REDN 020
REDN 025
REDN 030
REDN 035
REDN 040
REDN 045
REDN 050
REDN 055
REDN 060
REDN 065
REDN 070
REDN 075
REDN 080
REDN 085
REDN 090
REDN 095
REDN 100
REDN 105
REDN 110
REDN 115
REDN 120
REDN 125
REDN 130
REDN 135
REDN 140
REDN 145
REDN 150
REDN 155
REDN 160
REDN 165
REDN 170
REDN 175
REDN 180
REDN 185

APPENDIX B

**Listing of FORTRAN Source Program of 3DFEMWATER
Code PTI (Point Iteration Version)**

```

SUBROUTINE GW3D(X,Y,Z,IE,CMATRX,GNOJCN,RLD,RI,RL,H,HP,HW,HT,      GW3D 005
1 VX,VY,VZ,TH,DTH,AKR,NPCNV,DCOSB,ISB,NPBB,BFLX,BFLXP,        GW3D 010
2 SOS,SOSF,TSOSF,ISTYP,MSEL,WSS,WSSF,TWSSF,IWTYP,NPW,          GW3D 015
3 QCB,QCBF,TQCBF,ICTYP,ISC,NPCB,QNB,QNBF,TQNBF,INTYP,ISN,NPNB, GW3D 020
4 RFALL,RF,TRF,IRTY,ISV,NPVB,DCYFLX,FLX,HCON,HMIN,            GW3D 025
5 NPFLX,NPCON,NPMIN,HDB,HDBF,THDBF,IDTYP,NPDB,                GW3D 030
6 PROP,THPROP,AKPROP,KPR,KDSK,TDTC)                            GW3D 035

C                                                                GW3D 040
  IMPLICIT REAL*8(A-H,O-Z)                                     GW3D 045
  REAL*4 SUBHD                                                GW3D 050
  INTEGER*4 GNOJCN                                           GW3D 055

C                                                                GW3D 060
  COMMON /SGEOM/ MAXEL,MAXNP,MAXBES,MAXBNP,JBAND,MAXNTI,MXNDTC  GW3D 065
  COMMON /CGEOM/ NNP,NEL,NBNP,NPES,KGRAV,NTI,NDTCHG           GW3D 070
  COMMON /CINTE/ NCYL,NITER,KSTI,KPRO,KDSKO,KSS,NPITER,IGEOM  GW3D 075
  COMMON /CREAL/ DELT,CHNG,DELMAX,TMAX,DELTO,TOLA,TOLB,W,OME,OMI GW3D 080

C                                                                GW3D 085
  COMMON /CS/ MXSEL,MXSPR,MXSDP,NSEL,NSPR,NSDP                GW3D 090
  COMMON /CW/ MXWNP,MXWPR,MXWDP,NWNP,NWPR,NWDP                GW3D 095

C                                                                GW3D 100
  COMMON /CCBC/ MXCNP,MXCES,MXCPR,MXCDP,NCNP,NCES,NCPR,NCDP   GW3D 105
  COMMON /CNBC/ MXNNP,MXNES,MXNPR,MXNDP,NNNP,NNES,NNPR,NNDP   GW3D 110
  COMMON /CVBC/ MXVES,MXVNP,MXRPR,MXRDV,MVES,MVNP,NRPR,NRDP   GW3D 115
  COMMON /CDBC/ MXDNP,MXDPR,MXDDP,NDNP,NDPR,NDDP              GW3D 120

C                                                                GW3D 125
  COMMON /SMTL/ MAXMAT,MXSPPM,MXMPPM                           GW3D 130
  COMMON /CMTL/ NMAT,NMPPM,NSPPM                              GW3D 135

C                                                                GW3D 140
  COMMON /CFLOW/ FRATE(10),FLOW(10),TFLOW(10)                 GW3D 145

C                                                                GW3D 150
  DIMENSION X(MAXNP),Y(MAXNP),Z(MAXNP),IE(MAXEL,9)           GW3D 155
  DIMENSION CMATRX(MAXNP,JBAND),GNOJCN(JBAND,MAXNP),RLD(MAXNP) GW3D 160
  DIMENSION RI(MAXNP),RL(MAXNP)                                GW3D 165
  DIMENSION H(MAXNP),HP(MAXNP),HW(MAXNP),HT(MAXNP)           GW3D 170
  DIMENSION VX(MAXNP),VY(MAXNP),VZ(MAXNP)                     GW3D 175
  DIMENSION TH(8,MAXEL),DTH(8,MAXEL),AKR(8,MAXEL),NPCNV(MAXNP) GW3D 180

C                                                                GW3D 185
  DIMENSION DCOSB(3,MAXBES),ISB(6,MAXBES),NPBB(MAXBNP)       GW3D 190
  DIMENSION BFLX(MAXBNP),BFLXP(MAXBNP)                         GW3D 195

C                                                                GW3D 200
  DIMENSION SOS(MXSPR),SOSF(MXSDP,MXSPR),TSOSF(MXSDP,MXSPR)  GW3D 205
  DIMENSION ISTYP(MXSEL),MSEL(MXSEL)                           GW3D 210
  DIMENSION WSS(MXWPR),WSSF(MXWDP,MXWPR),TWSSF(MXWDP,MXWPR)  GW3D 215
  DIMENSION IWTYP(MXWNP),NPW(MXWNP)                             GW3D 220

C                                                                GW3D 225
  DIMENSION QCB(MXCPR),QCBF(MXCDP,MXCPR),TQCBF(MXCDP,MXCPR)  GW3D 230
  DIMENSION ICTYP(MXCES),ISC(5,MXCES),NPCB(MXCNP)             GW3D 235

C                                                                GW3D 240
  DIMENSION QNB(MXNPR),QNBf(MXNDP,MXNPR),TQNBf(MXNDP,MXNPR)  GW3D 245
  DIMENSION INTYP(MXNES),ISN(5,MXNES),NPNB(MXNNP)             GW3D 250

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C		GW3D 255
	DIMENSION RFALL(MXRPR), RF(MXRDP, MXRPR), TRF(MXRDP, MXRPR)	GW3D 260
	DIMENSION IRTYP(MXVES), ISV(5, MXVES), NPVB(MXVNP)	GW3D 265
	DIMENSION DCYFLX(MXVNP), FLX(MXVNP), HCON(MXVNP), HMIN(MXVNP)	GW3D 270
	DIMENSION NPFLX(MXVNP), NPCON(MXVNP), NPMIN(MXVNP)	GW3D 275
C		GW3D 280
	DIMENSION HDB(MXDPR), HDBF(MXDDP, MXDPR), THDBF(MXDDP, MXDPR)	GW3D 285
	DIMENSION IDTYP(MXDNP), NPDB(MXDNP)	GW3D 290
C		GW3D 295
	DIMENSION PROP(MXMPPM, MAXMAT)	GW3D 300
	DIMENSION THPROP(MXSPPM, MAXMAT), AKPROP(MXSPPM, MAXMAT)	GW3D 305
C		GW3D 310
	DIMENSION KPR(MAXNTI), KDSK(MAXNTI), TDTCH(MXNDTC)	GW3D 315
C		GW3D 320
	DIMENSION TITLE(9)	GW3D 325
	DIMENSION SUBHD(8, 3)	GW3D 330
C		GW3D 335
	DATA SUBHD/4HINPU, 4HT IN, 4HITIA, 4HL CO, 4HNDIT, 4HIONS, 2*4H	GW3D 340
	> 4HSTEA, 4HDY-S, 4HTATE, 4H INI, 4HTIAL, 4H CON, 4HDITI, 4HONS , 8*	GW3D 345
	> 4H /	GW3D 350
C		GW3D 355
C	***** DATA SET 1: PROBLEM IDENTIFICATION AND DESCRIPTION	GW3D 360
C		GW3D 365
	100 READ 10, NPROB, (TITLE(I), I-1, 9), IGEOM, IBUG, ICHNG	GW3D 370
C		GW3D 375
	IF (NPROB.LE.0) GO TO 990	GW3D 380
C		GW3D 385
	PRINT 1000, NPROB, (TITLE(I), I-1, 9), IGEOM, IBUG, ICHNG	GW3D 390
C		GW3D 395
C	----- READ AND PRINT INPUT DATA BY CALLING DATAIN	GW3D 400
C		GW3D 405
	KOUT=0	GW3D 410
	TIME=0.0	GW3D 415
C		GW3D 420
C	***** DATA SETS 2 THROUGH 16 WILL BE READ IN DATAIN	GW3D 425
C		GW3D 430
	CALL DATAIN(TITLE, NPROB, KPR, KDSK, TDTCH,	GW3D 435
	1 PROP, THPROP, AKPROP, X, Y, Z, IE, H, DCOSB, ISB, NPBB,	GW3D 440
	2 SOSF, TSOSF, ISTYP, MSEL, WSSF, TWSSF, IWTF, NPW,	GW3D 445
	3 QCBF, TQCBF, ICTYP, ISC, NPCB, QNBF, TQNBF, INTYP, ISN, NPNB,	GW3D 450
	4 RF, TRF, IRTYP, ISV, NPVB, HCON, HMIN, HDBF, THDBF, IDTYP, NPDB,	GW3D 455
	5 ISTOP)	GW3D 460
C		GW3D 465
	IF(IGEOM.LE.3) CALL PAGEN(GNOJCN, IE)	GW3D 470
	REWIND 4	GW3D 475
	IF(IGEOM.LE.3) WRITE(4) ((GNOJCN(J, I), J-1, JBAND), I-1, NNP)	GW3D 480
	IF(IGEOM.GT.3) READ(4) ((GNOJCN(J, I), J-1, JBAND), I-1, NNP)	GW3D 485
C		GW3D 490
	KDIG=0	GW3D 495
	IF (ISTOP.GT.0) GO TO 990	GW3D 500

C		GW3D 505
C	----- PREPARE INITIAL OR PRE-INITIAL VARIABLES	GW3D 510
C		GW3D 515
	IF(NSEL.NE.0) CALL INTERP(SOS,TSOSF,SOSF,TIME,	GW3D 520
1	MXSPR,MXSDP,NSPR,NSDP)	GW3D 525
	IF(NWNP.NE.0) CALL INTERP(WSS,TWSSF,WSSF,TIME,	GW3D 530
1	MXWPR,MXWDP,NWPR,NWD)	GW3D 535
C		GW3D 540
	IF(NCES.NE.0) CALL INTERP(QCB,TQCBF,QCBF,TIME,	GW3D 545
1	MXCPR,MXCDP,NCPR,NCDP)	GW3D 550
	IF(NNES.NE.0) CALL INTERP(QNB,TQBNF,QBNF,TIME,	GW3D 555
1	MXNPR,MXNDP,NRPR,NNDP)	GW3D 560
	IF(NVES.NE.0) CALL INTERP(RFALL,TRF,RF,TIME,	GW3D 565
1	MXRPR,MXRDPR,NRPR,NRDP)	GW3D 570
	IF(NDNP.NE.0) CALL INTERP(HDB,THDBF,HDBF,TIME,	GW3D 575
1	MXDPR,MXDDP,NDPR,NDDP)	GW3D 580
C		GW3D 585
C	----- PUT DIRICHLET BOUNDARY VALUES TO INITIAL CONDITIONS	GW3D 590
C		GW3D 595
	DO 130 I=1,NDNP	GW3D 600
	NI-NPDB(I)	GW3D 605
	NP-NPBB(NI)	GW3D 610
	ITYP-IDTYP(I)	GW3D 615
	H(NP)-HDB(ITYP)-Z(NP)*DFLOAT(KGRAV)	GW3D 620
130	CONTINUE	GW3D 625
C		GW3D 630
	CALL SPROP(TH,DTH,AKR, IE,H,THPROP,AKPROP)	GW3D 635
C		GW3D 640
	CALL VELT(VX,VY,VZ,CMATRX,X,Y,Z,IE,H,HT,AKR,PROP)	GW3D 645
	KFLOW--1	GW3D 650
C		GW3D 655
	CALL SFLOW(X,Y,Z,IE, H,HP,VX,VY,VZ,TH,DTH,	GW3D 660
1	BFLX,BFLXP,DCOSB,ISB,NPBB, MSEL,SOS,ISTYP, NPW,WSS,IWTYP,	GW3D 665
2	NPVB,NPDB,NPCB,NPNB, DELT, KFLOW)	GW3D 670
C		GW3D 675
	DO 140 I=1,9	GW3D 680
	IF(I.EQ.9) GO TO 140	GW3D 685
	FLOW(I)=0.0	GW3D 690
	TFLOW(I)=0.0	GW3D 695
140	CONTINUE	GW3D 700
	FLOW(9)=0.0	GW3D 705
C		GW3D 710
C	----- PRINT INITIAL OR PRE-INITIAL VARIABLES	GW3D 715
C		GW3D 720
	KDIAG=0	GW3D 725
C		GW3D 730
	CALL PRINTT(VX,VY,VZ,H,HT,TH, NPBB,BFLX, NPVB,DCYFLX,NPCON,	GW3D 735
	INPFLX,NPMIN, SUBHD(1,1), TIME,DELT,KPRO,KOUT,KDIAG,-1)	GW3D 740

C		GW3D 745
	IF(KSTR.EQ.1 .AND. KSS.EQ.1 .AND. KDSKO.EQ.1)	GW3D 750
	> CALL STORE(X,Y,Z,IE, H,HT,TH,VX,VY,VZ,DCOSB,ISB,NPBB,	GW3D 755
	1 TITLE, TIME, NPROB)	GW3D 760
C		GW3D 765
	IF (KSS.NE.0) GO TO 500	GW3D 770
C		GW3D 775
C	\$\$\$\$\$\$	GW3D 780
C	\$\$\$\$\$\$ PERFORM STEADY-STATE CALCULATION	GW3D 785
C	\$\$\$\$\$\$	GW3D 790
C		GW3D 795
	IF (NVES.EQ.0) GO TO 170	GW3D 800
C		GW3D 805
	DO 150 NPP-1,NVNP	GW3D 810
	NI-NPVB(NPP)	GW3D 815
	NPCON(NPP)-NPBB(NI)	GW3D 820
	NPMIN(NPP)-0	GW3D 825
	150 NPFLX(NPP)-0	GW3D 830
C		GW3D 835
	NCHG--1	GW3D 840
	CALL BCPREP(IE,X,Y,Z,H,VX,VY,VZ,DCOSB,ISB,NPVB,ISV,DCYFLX,FLX,	GW3D 845
	> HCON,HMIN,NPFLX,NPCON,NPMIN, IRTYP,RFALL, NCHG)	GW3D 850
C		GW3D 855
	170 DO 180 NP-1,NNP	GW3D 860
	180 HP(NP)-H(NP)	GW3D 865
C		GW3D 870
	KDIG-KDIG+1	GW3D 875
	IF(IBUG.NE.0) PRINT 10400,KDIG,TIME,DELT	GW3D 880
C		GW3D 885
C	----- ITERATION LOOP ON SEEPAGE-RAINFALL BOUNDARY CONDITIONS BEGINS	GW3D 890
C		GW3D 895
	EPS=0.5D0*TOLA	GW3D 900
C		GW3D 905
	DO 390 ICY-1,NCYL	GW3D 910
C		GW3D 915
	DO 210 NP-1,NNP	GW3D 920
	HW(NP)-OME*H(NP)+(1.0D0-OME)*HP(NP)	GW3D 925
	RI(NP)-HW(NP)	GW3D 930
	210 CONTINUE	GW3D 935
C		GW3D 940
C	----- ITERATION LOOP ON THE NON-LINEAR EQUATION BEGINS	GW3D 945
C		GW3D 950
	IF(IBUG.NE.0) PRINT 10401, ICY	GW3D 955
C		GW3D 960
C	----- PUT DIRICHLET BOUNDARY VALUES OF THE VARIABLE BOUNDARY	GW3D 965
C	----- INTO H, RI, HW, AND RL	GW3D 970
C		GW3D 975
	IF(NVES.EQ.0) GO TO 250	GW3D 980
	DO 230 NPP-1,NVNP	GW3D 985
	NI-NPMIN(NPP)	GW3D 990

IF(NI.EQ.0) GO TO 220	GW3D 995
H(NI)-HMIN(NPP)	GW3D1000
RI(NI)-HMIN(NPP)	GW3D1005
HW(NI)-HMIN(NPP)	GW3D1010
RL(NI)-HMIN(NPP)	GW3D1015
GO TO 230	GW3D1020
220 NI-NPCON(NPP)	GW3D1025
IF(NI.EQ.0) GO TO 230	GW3D1030
H(NI)-HCON(NPP)	GW3D1035
RI(NI)-HCON(NPP)	GW3D1040
HW(NI)-HCON(NPP)	GW3D1045
RL(NI)-HCON(NPP)	GW3D1050
230 CONTINUE	GW3D1055
250 CONTINUE	GW3D1060
C	GW3D1065
DO 350 IT-1,NITER	GW3D1070
C	GW3D1075
C ----- EVALUATE SOIL PROPERTIES FOR PREVIOUS ITERATE	GW3D1080
C	GW3D1085
CALL SPROP(TH,DTH,AKR, IE,HW,THPROP,AKPROP)	GW3D1090
C	GW3D1095
C ----- ASSEMBLE STEAD-STATE ELEMENT MATRICES QA AND QB INTO THE	GW3D1100
C ----- GLOBAL MATRIX C AND CONSTRUCT GLOBAL LOAD VECTOR R FROM	GW3D1105
C ----- ELEMENT LOAD VECTOR RQ.	GW3D1110
C	GW3D1115
CALL ASEMBL(X,Y,Z,IE, CMATRX,RLD,GNOJCN,HW,HP,DTH,AKR,PROP,	GW3D1120
> SOS,MSEL,ISTYP,WSS,NPW,IWTYP, KSS,W,DELT)	GW3D1125
C	GW3D1130
C ----- APPLY STEADY-STATE BOUNDARY CONDITIONS	GW3D1135
C	GW3D1140
CALL BC(CMATRX,RLD,GNOJCN, IE,X,Y,Z, AKR,PROP, DCOSE,ISB,NPBB,	GW3D1145
1 QCB,ISC,ICTYP, QNB,ISN,INTYP, FLX,HCON,HMIN,NPFLX,NPCON,NPMIN,	GW3D1150
2 HDB,IDTYP,NPDB, KSS)	GW3D1155
C	GW3D1160
C ----- SOLVE THE MATRIX EQUATION BY POINTWISE ITERATION	GW3D1165
C	GW3D1170
CALL PISS(RL,RI,RLD,CMATRX,GNOJCN,OMI, EPS,NNP,NPITER,MAXNP,JBAND,	GW3D1175
1 IBUG,KPRO)	GW3D1180
C	GW3D1185
C ----- OBTAIN MAXIMUM RELATIVE DEVIATION FROM PREVIOUS ITERATE	GW3D1190
C	GW3D1195
NPP=0	GW3D1200
RD=-1.0D0	GW3D1205
RES=-1.0D0	GW3D1210
DO 320 NP=1,NNP	GW3D1215
RESNP=DABS(RL(NP)-H(NP))	GW3D1220
RES=DMAX1(RES,RESNP)	GW3D1225
IF(H(NP).NE.0.0D0) RD=DMAX1(RD,DABS(RESNP/H(NP)))	GW3D1230
IF(RESNP .LE. TOLA) GO TO 320	GW3D1235
NPP=NPP+1	GW3D1240

	NPCNV(NPP)-NP	GW3D1245
	320 CONTINUE	GW3D1250
C		GW3D1255
	NNCVN-NPP	GW3D1260
C		GW3D1265
C	----- UPDATE PRESSURE WITH CURRENT ITERATE	GW3D1270
C		GW3D1275
	DO 330 NP-1,NNP	GW3D1280
	H(NP)-OME*RL(NP)+(1.ODO-OME)*H(NP)	GW3D1285
	RI(NP)-H(NP)	GW3D1290
	HW(NP)-H(NP)	GW3D1295
	330 CONTINUE	GW3D1300
C		GW3D1305
C	----- ESCAPE FROM ITERATION LOOP IF THE MAXIMUM RESIDUAL IS	GW3D1310
C	----- SUFFICIENTLY SMALL	GW3D1315
C		GW3D1320
	IF(IBUG.NE.0) PRINT 10200, IT,RES,RD,NNCVN	GW3D1325
	IF(IT.EQ.1) GO TO 350	GW3D1330
	IF(RES.LT.TOLA) GO TO 360	GW3D1335
C		GW3D1340
	350 CONTINUE	GW3D1345
C		GW3D1350
C	----- END OF ITERATION LOOP ON THE NON-LINEAR EQUATION	GW3D1355
C		GW3D1360
	PRINT 10210, ICY,IT,NITER,RES,RD,NNCVN	GW3D1365
C		GW3D1370
C	----- PRINT NONCONVERGENING NODES	GW3D1375
C		GW3D1380
	IF(IBUG.EQ.0) GO TO 360	GW3D1385
	PRINT 10500	GW3D1390
	PRINT 10600, (NPCNV(NPP),NPP-1,NNCVN)	GW3D1395
C		GW3D1400
	360 IF(ICHNG.EQ.0) GO TO 380	GW3D1405
	IF(NVES.EQ.0) GO TO 380	GW3D1410
C		GW3D1415
C	----- PRINT RAINFALL-SEEPAGE B. C. CHANGE INFORMATION	GW3D1420
C		GW3D1425
	PRINT 10402, ICY	GW3D1430
	DO 370 I-1,NVNP	GW3D1435
	NI-NPVB(I)	GW3D1440
	NP-NPBB(NI)	GW3D1445
	PRINT 10403, I,NP,NPCON(I),HCON(I),NPMIN(I),HMIN(I),NPFLX(I),	GW3D1450
	1 FLX(I),DCYFLX(I)	GW3D1455
	370 CONTINUE	GW3D1460
C		GW3D1465
C	----- CALCULATE DARCY'S VELOCITY	GW3D1470
C		GW3D1475
	380 CALL SPROP(TH,DTH,AKR, IE,H,THPROP,AKPROP)	GW3D1480
C		GW3D1485
	CALL VELT(VX,VY,VZ,CMATRX,X,Y,Z,IE,H,HT,AKR,PROP)	GW3D1490

C		GW3D1495
	IF(NVES .EQ. 0) GO TO 440	GW3D1500
C		GW3D1505
C	----- PREPARE BOUNDARY CONDITIONS ON THE VARIABLE-TYPE BOUNDARY FOR	GW3D1510
C	----- NEXT CYCLE COMPUTATIONS.	GW3D1515
C		GW3D1520
	CALL BCPREP(IE,X,Y,Z, H,VX,VY,VZ, DCOSB, ISB, NPVB, ISV, DCYFLX, FLX,	GW3D1525
	> HCON, HMIN, NPFLX, NPCON, NPMIN, IRTYP, RFALL, NCHG)	GW3D1530
C		GW3D1535
	IF(NCHG.EQ.0) GO TO 440	GW3D1540
	390 CONTINUE	GW3D1545
C		GW3D1550
C	----- END OF ITERATION LOOP ON SEEPAGE-RAINFALL BOUNDARY CONDITIONS	GW3D1555
C		GW3D1560
	PRINT 10610, ICY, IT, NCYL, NITER, RES, RD, NNCVN	GW3D1565
C		GW3D1570
	440 IF(NNCVN.EQ.0) GO TO 445	GW3D1575
	PRINT 10610, ICY, IT, NCYL, NITER, RES, RD, NNCVN	GW3D1580
C		GW3D1585
C	----- COMPUTE FLUXES THROUGH ALL TYPES OF BOUNDARIES.	GW3D1590
C		GW3D1595
	445 KFLOW=0	GW3D1600
	CALL SFLOW(X,Y,Z, IE, H,HP,VX,VY,VZ TH,DTH,	GW3D1605
	1 BFLX,BFLXP,DCOSB, ISB,NPBB, MSEL,SOS,ISTYP,NPW,WSS,IWTYP,	GW3D1610
	2 NPVB,NPDB,NPCB,NPNB, DELT, KFLOW)	GW3D1615
C		GW3D1620
	DO 450 I=1,9	GW3D1625
	IF(I.EQ.9) GO TO 450	GW3D1630
	FLOW(I)=0.0	GW3D1635
	TFLOW(I)=0.0	GW3D1640
	450 CONTINUE	GW3D1645
	FLOW(9)=0.0	GW3D1650
C		GW3D1655
C	----- PRINT STEADY-STATE VARIABLES	GW3D1660
C		GW3D1665
	CALL PRINTT(VX,VY,VZ,H,HT,TH, NPBB,BFLX, NPVB,DCYFLX,NPCON,	GW3D1670
	1 NPFLX,NPMIN, SUBHD(1,2), TIME,DELT, KPRO,KOUT,KDIAG,0)	GW3D1675
C		GW3D1680
	IF(KSTR.EQ.1 .AND. KDSKO.EQ.1) CALL STORE(X,Y,Z,IE,	GW3D1685
	> H,HT,TH,VX,VY,VZ,DCOSB, ISB,NPBB, TITLE,TIME,NPROB)	GW3D1690
C		GW3D1695
	IF (NTI.EQ.0) GO TO 100	GW3D1700
C		GW3D1705
	KSS=1	GW3D1710
C		GW3D1715
C	\$\$\$\$\$\$	GW3D1720
C	\$\$\$\$\$\$ PERFORM TRANSIENT-STATE CALCULATION	GW3D1725
C	\$\$\$\$\$\$	GW3D1730
C		GW3D1735
	500 IF (NVES.EQ.0) GO TO 550	GW3D1740

C		GW3D1745
	DO 510 NPP-1,NVNP	GW3D1750
	NI-NPVB(NPP)	GW3D1755
	NPCON(NPP)-NPBB(NI)	GW3D1760
	NPMIN(NPP)-0	GW3D1765
	510 NPFLX(NPP)-0	GW3D1770
C		GW3D1775
	NCHG--1	GW3D1780
C		GW3D1785
	550 TIME=TIME+DELT	GW3D1790
	W1-W	GW3D1795
	W2-1.0D0-W	GW3D1800
	KFLOW-1	GW3D1805
	TFLOW(9)-0.0	GW3D1810
C		GW3D1815
C	----- BEGIN THE TIME-MARCHING LOOP	GW3D1820
C		GW3D1825
	EPS=0.5D0*TOLB	GW3D1830
	IDELT=0	GW3D1835
	DO 890 ITM-1,NTI	GW3D1840
	ITMITM-ITM	GW3D1845
C		GW3D1850
C	----- PREPARE TRANSIENT BOUNDARY CONDITIONS AND SOURCE FOR THE STEP	GW3D1855
C		GW3D1860
	IF(NSEL.NE.0) CALL INTERP(SOS,TSOSF,SOSF,TIME,MXSPR,MXSDP,	GW3D1865
	1 NSPR,NSDP)	GW3D1870
	IF(NWNP.NE.0) CALL INTERP(WSS,TWSSF,WSSF,TIME,MKWPR,MKWDP,	GW3D1875
	1 NWPR,NWDP)	GW3D1880
C		GW3D1885
	IF(NCES.NE.0) CALL INTERP(QCB,TQCBF,QCBF,TIME,	GW3D1890
	1 MXCPR,MXCDP,NCPR,NCDP)	GW3D1895
	IF(NNES.NE.0) CALL INTERP(QNB,TQBNF,QBNF,TIME,	GW3D1900
	1 MXNPR,MXNDP,NNPR,NNDP)	GW3D1905
	IF(NVES.NE.0) CALL INTERP(RFALL,TRF,RF,TIME,	GW3D1910
	1 MXRPR,MXRDP,NRPR,NRDP)	GW3D1915
	IF(NDNP.NE.0) CALL INTERP(HDB,THDBF,HDBF,TIME,	GW3D1920
	1 MXDPR,MXDPP,NDPR,NDDP)	GW3D1925
C		GW3D1930
	IF(NVES.EQ.0) GO TO 560	GW3D1935
	NCHG--1	GW3D1940
	CALL BCPREP(IE,X,Y,Z, H,VX,VY,VZ, DCOSB,ISB, NPVB,ISV,DCYFLX,FLX,	GW3D1945
	1 HCON,HMIN,NPFLX,NPCON,NPMIN, IRTYP,RFALL, NCHG)	GW3D1950
C		GW3D1955
	560 DO 570 NP=1,MNP	GW3D1960
	RL(NP)-H(NP)	GW3D1965
	HP(NP)-H(NP)	GW3D1970
	570 CONTINUE	GW3D1975
C		GW3D1980
	KDIG=KDIG+1	GW3D1985
	IF(IBUG.NE.0 .AND. KPR(ITM).NE.0) PRINT 10400, KDIG,TIME,DELT	GW3D1990

C		GW3D1995
C	----- BEGIN ITERATION LOOP ON SEEPAGE-RAINFALL BOUNDARY CONDITIONS	GW3D2000
C		GW3D2005
	DO 690 ICY=i,NCYL	GW3D2010
	IF(IBUG.NE.0 .AND. KPR(ITM).NE.0) PRINT 10401, ICY	GW3D2015
C		GW3D2020
	DO 580 NP=1,NNP	GW3D2025
	H(NP)-OME*RL(NP)+(1.ODO-OME)*H(NP)	GW3D2030
	RI(NP)-H(NP)	GW3D2035
	HW(NP)-W1*(OME*H(NP)+(1.ODO-OME)*HP(NP))+W2*HP(NP)	GW3D2040
	580 CONTINUE	GW3D2045
C		GW3D2050
C	----- BEGIN ITERATION LOOP ON THE NON-LINEAR EQUATION	GW3D2055
C		GW3D2060
C	----- PUT DIRICHLET BOUNDARY VALUES OF THE VARIABLE BOUNDARY	GW3D2065
C	----- INTO H, RI, HW, AND RL	GW3D2070
C		GW3D2075
	IF(NVES.EQ.0) GO TO 595	GW3D2080
	DO 590 NPP=1,NVNP	GW3D2085
	NI-NPMIN(NPP)	GW3D2090
	IF(NI.EQ.0) GO TO 585	GW3D2095
	H(NI)-HMIN(NPP)	GW3D2100
	RI(NI)-HMIN(NPP)	GW3D2105
	HW(NI)-HMIN(NPP)	GW3D2110
	RL(NI)-HMIN(NPP)	GW3D2115
	GO TO 590	GW3D2120
	585 NI-NPCON(NPP)	GW3D2125
	IF(NI.EQ.0) GO TO 590	GW3D2130
	H(NI)-HCON(NPP)	GW3D2135
	RI(NI)-HCON(NPP)	GW3D2140
	HW(NI)-HCON(NPP)	GW3D2145
	RL(NI)-HCON(NPP)	GW3D2150
	590 CONTINUE	GW3D2155
	595 CONTINUE	GW3D2160
C		GW3D2165
	DO 650 IT=1,NITER	GW3D2170
C		GW3D2175
C	----- EVALUATE SOIL PROPERTIES FOR PREVIOUS ITERATE	GW3D2180
C		GW3D2185
	CALL SPROP(TH,DTH,AKR, IE,HW,THPROP,AKPROP)	GW3D2190
C		GW3D2195
C	----- ASSEMBLE ELEMENT MATRICES QA AND QB INTO THE GLOBAL MATRIX C	GW3D2200
C	----- AND CONSTRUCT THE GLOBAL LOAD VECTOR R FROM ELEMENT LOAD	GW3D2205
C	----- VECTOR RQ.	GW3D2210
C		GW3D2215
	CALL ASEMBL(X,Y,Z,IE, CMATRX,RLD,GNOJCN,HW,HP,DTH, AKR,PROP,	GW3D2220
	> SOS,MS2L,ISTYP,WSS,NPW,IWTYP, KSS,W,DELT)	GW3D2225

C		GW3D2230
C	----- APPLY BOUNDARY CONDITIONS TO MODIFY THE GLOBAL MATRIX C AND	GW3D2235
C	----- THE LOAD VECTOR R.	GW3D2240
C		GW3D2245
	CALL BC(CMATRX,RLD,GNOJCN, IE,X,Y,Z, AKR,PROP, DCOSB,ISB,NPBB,	GW3D2250
	1 QCB,ISC,ICTYP, QNB,ISN,INTYP, FLX,HCON,HMIN,NPFLX,NPCON,NPMIN,	GW3D2255
	2 HDB,IDTYP,NPDB, KSS)	GW3D2260
C		GW3D2265
C	----- SOLVE THE MATRIX EQUATION BY POINTWISE ITERATION	GW3D2270
C		GW3D2275
	CALL PISS(RL,RI,RLD,CMATRX,GNOJCN,OMI, EPS,NNP,NPITER,MAXNP,JBAND,	GW3D2280
	1 IBUG,KPR(ITM))	GW3D2285
C		GW3D2290
C	----- OBTAIN MAXIMUM RELATIVE DEVIATION FROM PREVIOUS ITERATE	GW3D2295
C		GW3D2300
	NPP=0	GW3D2305
	RD=-1.0D0	GW3D2310
	RES=-1.0D0	GW3D2315
	DO 620 NP=1,NNP	GW3D2320
	RESNP=DABS(RL(NP)-H(NP))	GW3D2325
	RES=DMAX1(RES,RESNP)	GW3D2330
	IF(H(NP) .NE. 0.0D0) RD=DMAX1(RD,DABS(RESNP/H(NP)))	GW3D2335
	IF(RESNP .LE. TOLB) GO TO 620	GW3D2340
	NPP=NPP+1	GW3D2345
	NPCNV(NPP)-NP	GW3D2350
	620 CONTINUE	GW3D2355
C		GW3D2360
	NNCVN=NPP	GW3D2365
C		GW3D2370
C	----- UPDATE PRESSURE WITH CURRENT ITERATE	GW3D2375
C		GW3D2380
	DO 630 NP=1,NNP	GW3D2385
	H(NP)=OME*RL(NP)+(1.0D0-OME)*H(NP)	GW3D2390
	RI(NP)=H(NP)	GW3D2395
	HW(NP)=W1*H(NP)+W2*HP(NP)	GW3D2400
	630 CONTINUE	GW3D2405
C		GW3D2410
C	----- ESCAPE FROM ITERATION LOOP IF THE MAXIMUM RESIDUAL IS	GW3D2415
C	----- SUFFICIENTLY SMALL.	GW3D2420
C		GW3D2425
	IF(IBUG.NE.0 .AND. KPR(ITM).NE.0) PRINT 10200, IT,RES,RD,NNCVN	GW3D2430
	IF(IT.EQ.1 .AND. ITM.EQ.1) GO TO 650	GW3D2435
	IF(RES.LT.TOLB) GO TO 660	GW3D2440
C		GW3D2445
	650 CONTINUE	GW3D2450
C		GW3D2455
C	----- END THE ITERATION LOOP ON THE NON-LINEAR EQUATION	GW3D2460
C		GW3D2465
	PRINT 10710, ITM,ICY,IT,NITER,RES,RD,NNCVN	GW3D2470

C		GW3D2475
	IF(IBUG.EQ.0 .OR. KPR(ITM).EQ.0) GO TO 66C	GW3D2480
C		GW3D2485
C	----- PRINT NONCONVERGING NODES	GW3D2490
C		GW3D2495
	PRINT 10500	GW3D2500
	PRINT 10600, (NPCNV(NPP),NPP-1,NNCVN)	GW3D2505
C		GW3D2510
	660 IF(ICHNG.EQ.0 .OR. KPR(ITM).EQ.0) GO TO 680	GW3D2515
	IF(NVES.EQ.0) GO TO 680	GW3D2520
C		GW3D2525
C	----- PRINT RAINFALL-SEEPAGE BOUNDARY CONDITION CHANGE INFORMATION	GW3D2530
C		GW3D2535
	PRINT 10402, ICY	GW3D2540
	DO 670 I-1,NVNP	GW3D2545
	NI-NPVB(I)	GW3D2550
	NP-NPBB(NI)	GW3D2555
	PRINT 10403, I,NP,NPCON(I),HCON(I),NPMIN(I),HMIN(I),NPFLX(I),	GW3D2560
	1 FLX(I),DCYFLX(I)	GW3D2565
	670 CONTINUE	GW3D2570
C		GW3D2575
C	----- CALCULATE DARCY'S VELOCITY	GW3D2580
C		GW3D2585
	680 CALL SPROP(TH,DTH,AKR, IE,H,THPROP,AKPROP)	GW3D2590
C		GW3D2595
	CALL VELT(VX,VY,VZ,CMATRX,X,Y,Z,IE,H,HT,AKR,PROP)	GW3D2600
C		GW3D2605
	IF(NVES.EQ.0) GO TO 710	GW3D2610
C		GW3D2615
	CALL BCPREP(IE,X,Y,Z,H,VX,VY,VZ, DCOSB,ISB, NPVB,ISV,DCYFLX,FLX,	GW3D2620
	> HCON,HMIN,NPFLX,NPCON,NPMIN,IRTYP,RFALL, NCHG)	GW3D2625
C		GW3D2630
	IF(NCHG.EQ.0) GO TO 710	GW3D2635
C		GW3D2640
	690 CONTINUE	GW3D2645
C		GW3D2650
C	----- END ITERATION LOOP ON SEEPAGE-RAINFALL BOUNDARY CONDITIONS	GW3D2655
C		GW3D2660
	PRINT 10810, ITM,ICY,IT,NCYL,NITER,RES,RD,NNCVN	GW3D2665
	710 IF(NNCVN.EQ.0) GO TO 740	GW3D2670
	PRINT 10810, ITM,ICY,IT,NCYL,NITER,RES,RD,NNCVN	GW3D2675
C		GW3D2680
C	----- COMPUTE FLUXES THROUGH ALL TYPES OF BOUNDARIES	GW3D2685
C		GW3D2690
	740 CALL SFLOW(X,Y,Z,IE, H,HP,VX,VY,VZ,TH,DTH,	GW3D2695
	1 BFLX,BFLXP,DCOSB,ISB,NPBB, MSEL,SOS,ISTYP,NPW,WSS,IWTYP,	GW3D2700
	2 NPVB,NPDB,NPCB,NPNB, DELT, KFLOW)	GW3D2705

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C                                                              GW3D2710
C ----- PRINT VARIABLES AT EACH TIME STEP                    GW3D2715
C                                                              GW3D2720
    CALL PRINT(VX,VY,VZ,H,HT,TH, NPBB,BFLX, NPVB,DCYFLX,NPCON,    GW3D2725
    1 NPFLX,NPMIN,SUBHD(1,3), TIME,DELT, KPR(ITM),KOUT,KDIAG,ITMITH) GW3D2730
C                                                              GW3D2735
    IF(KSTR.EQ.1 .AND.KDSK(ITM).EQ.1) CALL STORE(X,Y,Z,IE,        GW3D2740
    > H,HT,TH,VX,VY,VZ, DCOSB,ISB,NPBB, TITLE, TIME,NPROB)      GW3D2745
C                                                              GW3D2750
C ----- PREPARE FOR NEXT TIME STEP                            GW3D2755
C                                                              GW3D2760
    IF(TIME.GT.TMAX) GO TO 100                                    GW3D2765
    DELT=DELT*(1.0D0+CHNG)                                       GW3D2770
    DELT=DMINI(DELT,DELMAX)                                       GW3D2775
    IF(IDELT.EQ.0) GO TO 880                                       GW3D2780
    IF(TIME.EQ.TDTCH(IDELT)) DELT=DELTO                           GW3D2785
880 TIME=TIME+DELT                                                GW3D2790
    IF(TIME.LT.TDTCH(IDELT+1)) GO TO 890                         GW3D2795
    IDELT=IDELT+1                                                 GW3D2800
    TIME=TIME-DELT                                                GW3D2805
    DELT=TDTCH(IDELT)-TIME                                         GW3D2810
    IF(DELT.LE.0.0) DELT=DELTO                                     GW3D2815
    TIME=TIME+DELT                                                GW3D2820
890 CONTINUE                                                      GW3D2825
C                                                              GW3D2830
C ----- END OF TIME-MARCHING LOOP                             GW3D2835
C                                                              GW3D2840
    GO TO 100                                                      GW3D2845
C                                                              GW3D2850
990 RETURN                                                         GW3D2855
C                                                              GW3D2860
10  FORMAT(I5,9A8,3I1)                                           GW3D2865
1000 FORMAT('1 PROBLEM',I5,'... ',9A8,1X,3I1/)                 GW3D2870
10200 FORMAT(5X,I10,3X,E12.4,3X,E12.4,15X,I10)                 GW3D2875
10400 FORMAT('1', '*****', GW3D2880
1  '*****', GW3D2885
2  '*****'////' DIAGNOSTIC TABLE',I4,'.. AT TIME -',1PD12.4, GW3D2890
3  ' ,(DELT =', 1PD12.4,')' ) GW3D2895
10401 FORMAT(//' TABLE OF ITERATIVE PARAMETERS FOR',I3,'-TH CYCLE'//6X, GW3D2900
1  ' ITERATION',7X,'RESIDUAL',6X,'DEVIATION',6X, GW3D2905
2  'NO. NON-CONV. NODES') GW3D2910
10402 FORMAT(//' TABLE OF RAINFALL/EVAPORATION-SEEPAGE B. C. USED FOR', GW3D2915
1  I3,'-TH CYCLE'//7X,' I  NPVB  NPCON  HCON  NPMIN  HMIN', GW3D2920
2  '      NPFLX      FLX      DCYFLX FROM PREVIOUS CYCLE'/7X, GW3D2925
3  '      - - - - -', GW3D2930
4  '      - - - - -' ) GW3D2935
10403 FORMAT(1H ,I8,I6,I7,D12.4,I7,D12.4,I7,D12.4,12X,D12.4) GW3D2940
10500 FORMAT(//' TABLE OF NON-CONVERGING NODES')             GW3D2945
10600 FORMAT(/(5X,20I5))                                        GW3D2950

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10210 FORMAT(1H0,'WARNING: NON-CONVERGENCE OCCUR DURING STEADY STATE SOLUTION AT',I3,' -TH CYCLE'/1H , 'IT = ',I3,' .GT. MAXIT = ',I3, GW3D2960
2 ', RES =',D12.5,', RD =',D12.4,', NNCVN =',I4) GW3D2965
10610 FORMAT(1H0,'ABSOLUTELY WARNING: STEADY STATE SOLUTION IS NG'/1H , GW3D2970
> 'ICY = ',I3,' IT = ',I3,' MAXCY = ',I3,' MAXIT = ',I3, GW3D2975
> ', RES =',D12.4,', RD =',D12.4,', NNCVN =',I4) GW3D2980
10710 FORMAT(1H0,'WARNING: NON-CONVERGENCE OCCUR AT',I5,' -TH TIME STEP',I5) GW3D2985
>,I3,' -TH CYCLE'/1H , 'IT = ',I3,' .GT. MAXIT = ',I3,2D12.4,I5) GW3D2990
10810 FORMAT(1H0,'ABSOLUTELY WARNING: TRANSIENT SOLUTION IS NG AT ',I5, GW3D2995
> ' -TH TIME STEP'/1H , 'ICY = ',I3,' IT = ',I3,' MAXCY = ',I3, GW3D3000
> ' MAXIT = ',I3,', RES =',D12.4,', RD =',D12.4,', NNCVN =',I4)GW3D3005
END GW3D3010

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SUBROUTINE DATAIN(TITLE,NPROB, KPR,KDSK,TDCH, DATA 005
1 PROP,THPROP,AKPROP, X,Y,Z,IE,H, DCOSB,ISB,NPBB, DATA 010
2 SOSF,TSOSF,ISTYP,MSEL, WSSF,TWSSF,IWTYP,NPW, DATA 015
3 QCBF,TQCBF,ICTYP,ISC,NPCB, QNBF,TQNB,INTYP,ISN,NPNB, DATA 020
4 RF,TRF,IRTY,ISV,NPVB, HCON,HMIN, HDBF,THDBF,IDTYP,NPDB, DATA 025
5 ISTOP) DATA 030
C DATA 035
C*****1*****2*****3*****4*****5*****6*****7**DATA 040
C ----- TO READ AND PRINT SYSTEM PARAMETERS, GEOMETRY, BOUNDARY AND DATA 045
C ----- INITIAL CONDITIONS, AND PROPERTIES OF THE MEDIA. DATA 050
C*****1*****2*****3*****4*****5*****6*****7**DATA 055
C DATA 060
C IMPLICIT REAL*8(A-H,O-Z) DATA 065
REAL*4 PHAT,THPAR,AKPAR DATA 070
C DATA 075
COMMON /SGEOM/ MAXEL,MAXNP,MAXBES,MAXBNP,JBAND,MAXNTI,MXNDTC DATA 080
COMMON /CGEOM/ NNP,NEL,NBNP,NBES,KGRAV,NTI,NDTCHG DATA 085
COMMON /CINTE/ NCYL,NITER,KSTR,KPRO,KDSKO,KSS,NPITER,IGEOM DATA 090
COMMON /CREAL/ DELT,CHNG,DELMAX,TMAX,DELTO,TOLA,TOLB,W,OME,OMI DATA 095
C DATA 100
COMMON /CS/ MXSEL,MXSPR,MXSDP,NSEL,NSPR,NSDP DATA 105
COMMON /CW/ MXWNP,MXWPR,MXWDP,NWNP,NWPR,NWDP DATA 110
C DATA 115
COMMON /CCBC/ MXCNP,MXCES,MXCPR,MXCDP,NCNP,NCES,NCPR,NCDP DATA 120
COMMON /CNBC/ MXNNP,MXNES,MXNPR,MXNDP,NNNP,NNES,NNPR,NNDP DATA 125
COMMON /CVBC/ MXVES,MXVNP,MXRPR,MXRD, NVES,NVNP,NRPR,NRDP DATA 130
COMMON /CDBC/ MXDNP,MXDPR,MXDDP,NDNP,NDPR,NDDP DATA 135
C DATA 140
COMMON /SMTL/ MAXMAT,MXSPPM,MXMPPM DATA 145
COMMON /CMTL/ NMAT,NMPPM,NSPPM DATA 150
C DATA 155
DIMENSION TITLE(9) DATA 160

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C          DIMENSION KPR(MAXNTI),KDSK(MAXNTI),TDTCH(MXNDTC)          DATA 165
C          DIMENSION PROP(MXMPPM,MAXMAT)                               DATA 170
C          DIMENSION THPROP(MXSPPM,MAXMAT),AKPROP(MXSPPM,MAXMAT)     DATA 175
C          DIMENSION X(MAXNP),Y(MAXNP),Z(MAXNP),IE(MAXEL,9),H(MAXNP)  DATA 180
C          DIMENSION DCOSB(3,MAXBES),ISB(6,MAXBES),NPBB(MAXBNP)      DATA 185
C          DIMENSION MSEL(MXSEL),ISTYP(MXSEL)                          DATA 190
C          DIMENSION SOSF(MXSDP,MXSPR),TSOSF(MXSDP,MXSPR)            DATA 195
C          DIMENSION NPW(MXWNP),IWTYP(MXWNP)                           DATA 200
C          DIMENSION WSSF(MXWDP,MXWPR),TWSSF(MXWDP,MXWPR)            DATA 205
C          DIMENSION QCBF(MXCDP,MXCPR),TQCBF(MXCDP,MXCPR),ICTYP(MXCES) DATA 210
C          DIMENSION ISC(5,MXCES),NPCB(MXCNP)                           DATA 215
C          DIMENSION QNBF(MXNDP,MXNPR),TQNBF(MXNDP,MXNPR),INTYP(MXNES) DATA 220
C          DIMENSION ISN(5,MXNES),NPNB(MXNNP)                           DATA 225
C          DIMENSION RF(MXRDP,MXRPR),TRF(MXRDP,MXRPR),IRTP(MXVES)   DATA 230
C          DIMENSION ISV(5,MXVES),NPVB(MXVNP)                          DATA 235
C          DIMENSION HCON(MXVNP),HMIN(MXVNP)                           DATA 240
C          DIMENSION HDBF(MXDDP,MXDPR),THDBF(MXDDP,MXDPR),IDTYP(MXDNP) DATA 245
C          DIMENSION NPDB(MXDNP)                                        DATA 250
C          DIMENSION NIMI(4),NJMJ(4),IEM(8)                             DATA 255
C          DIMENSION PMAT(3,6),AKPAR(3,8),THPAR(3,8)                   DATA 260
C          DATA PMAT/4H S,4HAT K,4HXX 4H S,4HAT K,4HYY 4H S,        DATA 265
C          > 4HAT K,4HZZ 4H S,4HAT K,4HXY 4H S,4HAT K,4HXZ 4H S,    DATA 270
C          >4HAT K,4HYZ /                                             DATA 275
C          DATA THPAR/4H ,4H TH1,4H ,4H ,4H TH2,4H ,4H ,          DATA 280
C          > 4H TH3,4H ,4H ,4H TH4,4H ,4H ,4H TH5,4H ,4H ,        DATA 285
C          > 4H TH6,4H ,4H ,4H TH7,4H ,4H ,4H TH8,4H /            DATA 290
C          DATA AKPAR/4H ,4H K1,4H ,4H ,4H K2,4H ,4H ,          DATA 295
C          > 4H K3,4H ,4H ,4H K4,4H ,4H ,4H K5,4H ,              DATA 300
C          > 4H ,4H K6,4H ,4H ,4H K7,4H ,4H ,4H K8,4H /          DATA 305
C          ISTOP=0                                                    DATA 310
C          DATA 315
C          ***** DATA SET 2: BASIC INTEGER PARAMETERS             DATA 320
C          READ 10, NNP,NEL,NMAT,NCM,NTI,KSS,NSPPM,NMPPM,KSTR,        DATA 325
C          1 KCP,KGRAV,NITER,NCYL,NDTCHG,NPITER,NREGN                 DATA 330
C          IF(NDTCHG.LE.0) NDTCHG=-1                                  DATA 335
C          PRINT 1000, NNP,NEL,NMAT,NCM,NTI,KSS,NSPPM,NMPPM,KSTR,    DATA 340
C          1 KCP,KGRAV,NITER,NCYL,NDTCHG,NPITER,NREGN                DATA 345
C          DATA 350
C          DATA 355
C          DATA 360
C          DATA 365
C          DATA 370
C          DATA 375
C          DATA 380
C          DATA 385
C          DATA 390
C          DATA 395
C          DATA 400
    
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C		DATA 405
C	***** DATA SET 3: BASIC REAL PARAMETERS	DATA 410
C		DATA 415
	READ 20, DELT, CHNG, DELMAX, TMAX, TOLA, TOLB, RHO, GRAV, VISC, W,	DATA 420
	1 OME, OMI	DATA 425
C		DATA 430
	DELTO-DELT	DATA 435
	IF(TMAX.LE.0.0) TMAX-1.0D38	DATA 440
C		DATA 445
	PRINT 1100, DELT, CHNG, DELMAX, TMAX, TOLA, TOLB, RHO, GRAV, VISC, W,	DATA 450
	1 OME, OMI	DATA 455
C		DATA 460
C	***** DATA SET 4: LINE PRINT CONTROL AND DISK STORE CONTROL	DATA 465
C		DATA 470
	READ 30, KPRO, (KPR(ITM), ITM-1, NTI)	DATA 475
	READ 30, KDSKO, (KDSK(ITM), ITM-1, NTI)	DATA 480
	READ 20, (TDTCH(I), I-1, NDTCHG)	DATA 485
C		DATA 490
	PRINT 1200	DATA 495
	PRINT 1210, KPRO, (KPR(ITM), ITM-1, NTI)	DATA 500
	PRINT 1300	DATA 505
	PRINT 1210, KDSKO, (KDSK(ITM), ITM-1, NTI)	DATA 510
	PRINT 1350, (TDTCH(I), I-1, NDTCHG)	DATA 515
C		DATA 520
C	***** DATA SET 5: MATERIAL PROPERTIES	DATA 525
C		DATA 530
	PRINT 1400, ((PMAT(I,J), I-1, 3), J-1, NMPPM)	DATA 535
	DO 100 I-1, NMAT	DATA 540
	READ 20, (PROP(J,I), J-1, NMPPM)	DATA 545
	100 PRINT 1410, I, (PROP(J,I), J-1, NMPPM)	DATA 550
C		DATA 555
C	***** DATA SET 6: SOIL PROPERTIES	DATA 560
C		DATA 565
C		DATA 570
C	----- READ AND PRINT PARAMETERS REQUIRE TO COMPUTE	DATA 575
C	----- MOISTURE CONTENT GIVEN THE PRESSURE HEAD	DATA 580
C		DATA 585
	IF (NSPPM.EQ.0) GO TO 200	DATA 590
	PRINT 1500, ((THPAR(I,J), I-1, 3), J-1, 8)	DATA 595
	DO 105 I-1, NMAT	DATA 600
	READ 20, (THPROP(J,I), J-1, NSPPM)	DATA 605
	PRINT 1510, I, (THPROP(J,I), J-1, NSPPM)	DATA 610
	105 CONTINUE	DATA 615
C		DATA 620
C	----- READ AND PRINT PARAMETERS REQUIRED TO COMPUTE RELATIVE	DATA 625
C	----- HYDRAULIC CONDUCTIVITY	DATA 630
C		DATA 635
	PRINT 1600, ((AKPAR(I,J), I-1, 3), J-1, 8)	DATA 640
	DO 110 I-1, NMAT	DATA 645
	READ 20, (AKPROP(J,I), J-1, NSPPM)	DATA 650

PRINT 1510, I, (AKPROP(J,I),J-1,NSPPM)	DATA 655
110 CONTINUE	DATA 660
IF (KCP.EQ.0) GO TO 200	DATA 665
C	DATA 670
C ----- CONVERT FROM SATURATED PERMEABILITY TO SATURATED CONDUCTIVITY	DATA 675
C	DATA 680
DO 190 I-1,NMAT	DATA 685
PKCF=RHO*GRAV/VISC	DATA 690
DO 190 J-1,6	DATA 695
PROP(J,I)=PROP(J,I)*PKCF	DATA 700
190 CONTINUE	DATA 705
C	DATA 710
C ***** DATA SET 7: NODE COORDINATES	DATA 715
C	DATA 720
C ----- READ NODAL POINT COORDINATES	DATA 725
C	DATA 730
200 NPI=0	DATA 735
210 READ 40, NI,NSEQ,NIAD,XI,YI,ZI,XIAD,YIAD,ZIAD	DATA 740
IF(NI.EQ.0) GO TO 240	DATA 745
NJ=NI+NSEQ	DATA 750
DO 220 NP=NI,NJ	DATA 755
I=NI+NIAD*(NP-NI)	DATA 760
X(I)=XI+XIAD*DFLOAT(NP-NI)	DATA 765
Y(I)=YI+YIAD*DFLOAT(NP-NI)	DATA 770
Z(I)=ZI+ZIAD*DFLOAT(NP-NI)	DATA 775
NPI=NPI+1	DATA 780
220 CONTINUE	DATA 785
GO TO 210	DATA 790
240 IF(NPI.EQ.NNP) GO TO 250	DATA 795
PRINT 2000	DATA 800
STOP	DATA 805
250 CONTINUE	DATA 810
C	DATA 815
C ----- PRINT NODAL POINT COORDINATES	DATA 820
C	DATA 825
IF(MOD(IGEOM,2).EQ.0) GO TO 270	DATA 830
LINE=0	DATA 835
DO 265 NP=1,NNP,3	DATA 840
NJMN=NP	DATA 845
NJMX=MINO(NP+2,NNP)	DATA 850
LINE=LINE+1	DATA 855
IF(MOD(LINE-1,50).EQ.0) PRINT 2100	DATA 860
PRINT 2110, (NJ,X(NJ),Y(NJ),Z(NJ),NJ=NJMN,NJMX)	DATA 865
265 CONTINUE	DATA 870
270 CONTINUE	DATA 875
C	DATA 880
C ***** DATA SET 8: ELEMENT DATA	DATA 885
C	DATA 890
C ----- READ ELEMENT INDICES AND COMPUTE MAXIMUM NODAL DIFFERENCE FOR	DATA 895
C ----- EACH ELEMENT	DATA 900

C		DATA 905
	MMP=0	DATA 910
	300 READ 10, MI,NSEQ,MIAD,(IEM(I),I-1,8),IEMAD	DATA 915
	IF(MI.EQ.0) GO TO 330	DATA 920
C		DATA 925
	MJ=MI+NSEQ	DATA 930
	DO 320 MP=MI,MJ	DATA 935
	M=MI+(MP-MI)*MIAD	DATA 940
	DO 310 IQ=1,8	DATA 945
	NI=IEM(IQ)+(MP-MI)*IEMAD	DATA 950
	310 IE(M,IQ)=NI	DATA 955
	MMP=MMP+1	DATA 960
	320 CONTINUE	DATA 965
	GO TO 300	DATA 970
C		DATA 975
	330 IF(MMP.EQ.NEL) GO TO 350	DATA 980
	PRINT 3000, MMP,NEL	DATA 985
	STOP	DATA 990
C		DATA 995
	350 DO 360 M=1,NEL	DATA1000
	360 IE(M,9)=1	DATA1005
C		DATA1010
C	***** DATA SET 9: MATERIAL CORRECTIONS	DATA1015
C		DATA1020
	IF (NCM.LE.0) GO TO 405	DATA1025
	CALL READN(IE(1,9),MAXEL,NCM)	DATA1030
C		DATA1035
C	----- PRINT ELEMENT INCIDENCE AND MATERIAL TYPES FOR EACH ELEMENT	DATA1040
C		DATA1045
	405 CONTINUE	DATA1050
	IF(MOD(IGEOM,2).EQ.0) GO TO 415	DATA1055
	LINE=0	DATA1060
	DO 410 NI=1,NEL,2	DATA1065
	NJMN=NI	DATA1070
	NJMX=MINO(NI+1,NEL)	DATA1075
	LINE=LINE+1	DATA1080
	IF(MOD(LINE-1,50).EQ.0) PRINT 2700	DATA1085
	PRINT 3100, (NJ,(IE(NJ,K),K=1,9),NJ-NJMN,NJMX)	DATA1090
	410 CONTINUE	DATA1095
	415 CONTINUE	DATA1100
C		DATA1105
C	----- CHECK IF MATERIAL TYPE FOR EACH ELEMENT IS CORRECT	DATA1110
C		DATA1115
	DO 420 M=1,NEL	DATA1120
	MTYP=IE(M,9)	DATA1125
	IF(MTYP.GT.0 .AND. MTYP.LE.NMAT) GO TO 420	DATA1130
	PRINT 4200, M	DATA1135
	ISTOP=ISTOP+1	DATA1140
	420 CONTINUE	DATA1145

C		DATA1150
	IF(ISTOP.EQ.0) GO TO 430	DATA1155
	PRINT 4300, ISTOP	DATA1160
	STOP	DATA1165
C		DATA1170
C	----- IDENTIFY BOUNDARY ELEMENTS AND COMPUTE DIRECTIONAL COSINES	DATA1175
C		DATA1180
	430 CONTINUE	DATA1185
	IF(IGEOM.LE.1) CALL SURF(X,Y,Z,IE,DCOSB,ISB,NPBB)	DATA1190
	REWIND 3	DATA1195
	IF(IGEOM.LE.1) WRITE(3) NBES,NBNP,((DCOSB(J,I),J-1,3),I-1,NBES),	DATA1200
	1 ((ISB(J,I),J-1,6),I-1,NBES),(NPBB(I),I-1,NBNP)	DATA1205
	IF(IGEOM.GT.1) READ(3) NBES,NBNP,((DCOSB(J,I),J-1,3),I-1,NBES),	DATA1210
	1 ((ISB(J,I),J-1,6),I-1,NBES),(NPBB(I),I-1,NBNP)	DATA1215
C		DATA1220
C	***** DATA SET 10: INITIAL CONDITIONS	DATA1225
C		DATA1230
C		DATA1235
C	----- READ INITIAL OR PRE-INITIAL CONDITIONS VIA CARDS	DATA1240
C		DATA1245
	CALL READR(H,MAXNP,NNP)	DATA1250
C		DATA1255
C	***** DATA SET 11: INTEGERS CONTROLLING SOURCES AND B.C.	DATA1260
C		DATA1265
	READ 10, NSEL,NSPR,NSDP, NWNP,NWPR,NWDP, NCES,NCNP,NCPR,NCDP,	DATA1270
	1 NNES,NNNP,NNPR,NNDP, NVES,NVNP,NRPR,NRDP, NDNP,NDPR,NDDP	DATA1275
C		DATA1280
	PRINT 5100, NSEL,NSPR,NSDP, NWNP,NWPR,NWDP	DATA1285
	PRINT 5150, NCES,NCNP,NCPR,NCDP,NNES,NNNP,NRPR,NNDP,	DATA1290
	1 NVES,NVNP,NRPR,NRDP, NDNP,NDPR,NDDP	DATA1295
C		DATA1300
C	***** DATA SET 12: SOURCE DATA	DATA1305
C		DATA1310
	IF(NSEL.EQ.0) GO TO 560	DATA1315
	PRINT 5300	DATA1320
	DO 510 I-1,NSPR	DATA1325
	READ 20, (TSOSF(J,I),SOSF(J,I),J-1,NSDP)	DATA1330
	PRINT 5500, I	DATA1335
	PRINT 5510, (TSOSF(J,I),SOSF(J,I),J-1,NSDP)	DATA1340
	510 CONTINUE	DATA1345
C		DATA1350
C	----- READ SOURCE TYPE ASSIGNED TO EACH ELEMENT	DATA1355
C		DATA1360
	READ 10, (MSEL(M),M-1,NSEL)	DATA1365
	CALL READN(ISTYP,MXSEL,NSEL)	DATA1370
C		DATA1375
C	----- PRINT ELEMENT SOURCE/SINK PROFILES AND TYPE	DATA1380
C		DATA1385
	LINE-0	DATA1390

DO 520 I=1,NSEL,5	DATA1395
LINE=LINE+1	DATA1400
IF(MOD(LINE-1,50).EQ.0) PRINT 5600	DATA1405
NJMN=I	DATA1410
NJMX=MINO(I+4,NSEL)	DATA1415
PRINT 5650, (J,MSEL(J),ISTYP(J),J-NJMN,NJMX)	DATA1420
520 CONTINUE	DATA1425
C	DATA1430
C ----- READ AND WRITE WELL SOURCE/SINK PROFILES	DATA1435
C	DATA1440
560 IF(NWNP.EQ.0) GO TO 600	DATA1445
PRINT 5700	DATA1450
DO 570 I=1,NWPR	DATA1455
READ 20, (TWSSF(J,I),WSSF(J,I),J-1,NWDP)	DATA1460
PRINT 5710, I	DATA1465
PRINT 5510, (TWSSF(J,I),WSSF(J,I),J-1,NWDP)	DATA1470
570 CONTINUE	DATA1475
C	DATA1480
C ----- READ WELL SOURCE/SINK NODES AND TYPE OF PROFILES ASSIGNED TO	DATA1485
C ----- EACH OF NWNP NODES.	DATA1490
C	DATA1495
READ 10, (NPW(I),I-1,NWNP)	DATA1500
CALL READN(IWTYP,MXWNP,NWNP)	DATA1505
C	DATA1510
C ----- PRINT GLOBAL WELL NODE NUMBERS AND PROFILE TYPE OF WELL NODE	DATA1515
C	DATA1520
LINE=0	DATA1525
DO 590 I=1,NWNP,5	DATA1530
LINE=LINE+1	DATA1535
IF(MOD(LINE-1,50).EQ.0) PRINT 5800	DATA1540
NJMN=I	DATA1545
NJMX=MINO(I+4,NWNP)	DATA1550
PRINT 5850, (J,NPW(J),IWTYP(J),J-NJMN,NJMX)	DATA1555
590 CONTINUE	DATA1560
C	DATA1565
C ***** DATA SET 13: RAINFALL/EVAPORATION-SEEPAGE BOUNDARY CONDITIONS	DATA1570
C	DATA1575
600 IF(NVES.EQ.0) GO TO 700	DATA1580
C	DATA1585
PRINT 6000	DATA1590
C	DATA1595
C ----- READ AND WRITE RAINFALL (+)/EVAPORATION (-) PROFILES	DATA1600
C	DATA1605
PRINT 6100	DATA1610
DO 610 I=1,NRPR	DATA1615
READ 20, (TRF(J,I),RF(J,I),J-1,NRDP)	DATA1620
PRINT 6150, I	DATA1625
PRINT 5510, (TRF(J,I),RF(J,I),J-1,NRDP)	DATA1630
610 CONTINUE	DATA1635

C		DATA1640
C	----- READ RAINFALL/EVAPORATION TYPE ASSIGNED TO EACH RS SIDE	DATA1645
C		DATA1650
	CALL READN(IRTYP, MXVES, NVES)	DATA1655
C		DATA1660
C	----- READ FOUR GLOBAL NODE NUMBER FOR EACH OF ALL VARIABLE	DATA1665
C	----- BOUNDARY ELEMENT SIDES.	DATA1670
C		DATA1675
	MPI=0	DATA1680
620	READ 10, MI, NSEQ, MIAD, I1, I2, I3, I4, I1AD, I2AD, I3AD, I4AD	DATA1685
	IF(MI.EQ.0) GO TO 630	DATA1690
	MJ=MI+NSEQ	DATA1695
	DO 625 MP=MI, MJ	DATA1700
	I=MI+(MP-MI)*MIAD	DATA1705
	ISV(1, I)=I1+(MP-MI)*I1AD	DATA1710
	ISV(2, I)=I2+(MP-MI)*I2AD	DATA1715
	ISV(3, I)=I3+(MP-MI)*I3AD	DATA1720
	ISV(4, I)=I4+(MP-MI)*I4AD	DATA1725
	MPI=MPI+1	DATA1730
625	CONTINUE	DATA1735
	GO TO 620	DATA1740
630	IF(MPI.EQ.NVES) GO TO 635	DATA1745
	PRINT 6300	DATA1750
	STOP	DATA1755
C		DATA1760
C	----- PRINT INPUTTED GLOBAL NODAL NUMBER AND RAINFALL TYPES OF ALL	DATA1765
C	----- VARIABLE BOUNDARY ELEMENT SIDES.	DATA1770
C		DATA1775
635	LINE=0	DATA1780
	DO 640 MP=1, NVES, 3	DATA1785
	LINE=LINE+1	DATA1790
	IF(MOD(LINE-1, 50).EQ.0) PRINT 6400	DATA1795
	NJMN=MP	DATA1800
	NJMX=MINO(MP+2, NVES)	DATA1805
	PRINT 6450, (J, (ISV(I, J), I=1, 4), IRTYP(J), J-NJMN, NJMX)	DATA1810
640	CONTINUE	DATA1815
C		DATA1820
C	----- READ GLOBAL NODAL NUMBER FOR EACH OF ALL VARIABLE NODES.	DATA1825
C		DATA1830
	CALL READN(NPVB, MXVNP, NVNP)	DATA1835
C		DATA1840
C	----- READ PONDING DEPTH AND MINIMUM HEAD FOR EACH OF ALL RS NODES	DATA1845
C		DATA1850
	CALL READR(HCON, MXVNP, NVNP)	DATA1855
	CALL READR(HMIN, MXVNP, NVNP)	DATA1860
C		DATA1865
C	----- PRINT GLOBAL NODAL NUMBER, PONDING DEPTH AND MINIMUM PRESURE	DATA1870
C	----- RESSURE HEAD FOR ALL VARIABLE BOUNDARY NODES	DATA1875
C		DATA1880
	LINE=0	DATA1885

DO 645 I=1,NVNP,3	DATA1890
LINE=LINE+1	DATA1895
IF(MOD(LINE-1,50).EQ.0) PRINT 6500	DATA1900
NJMN=I	DATA1905
NJMX=MINO(I+2,NVNP)	DATA1910
PRINT 6550, (J,NPVB(J),HCON(J),HMIN(J),J-NJMN,NJMX)	DATA1915
645 CONTINUE	DATA1920
C	DATA1925
C ----- COMPUTE BOUNDARY SIDE NUMBER FOR EACH OF ALL VARIABLE	DATA1930
C ----- BOUNDARY SIDES.	DATA1935
C	DATA1940
DO 659 MI=1,NVES	DATA1945
DO 651 IQ=1,4	DATA1950
651 NIMI(IQ)=ISV(IQ,MI)	DATA1955
C	DATA1960
DO 657 MJ=1,NBES	DATA1965
DO 652 JQ=1,4	DATA1970
IJ=ISB(JQ,MJ)	DATA1975
652 NJMJ(JQ)=NPBB(IJ)	DATA1980
IEQ=0	DATA1985
DO 656 IQ=1,4	DATA1990
NI=NIMI(IQ)	DATA1995
DO 653 JQ=1,4	DATA2000
NJ=NJMJ(JQ)	DATA2005
IF(NJ.EQ.NI) GO TO 655	DATA2010
653 CONTINUE	DATA2015
GO TO 657	DATA2020
655 IEQ=IEQ+1	DATA2025
656 CONTINUE	DATA2030
IF(IEQ.EQ.4) GO TO 658	DATA2035
657 CONTINUE	DATA2040
C	DATA2045
PRINT 6570, MI	DATA2050
STOP	DATA2055
658 ISV(5,MI)=MJ	DATA2060
C	DATA2065
659 CONTINUE	DATA2070
C	DATA2075
C ----- CHANGE NPVB FROM CONTAINING GLOBAL NODAL NUMBER TO	DATA2080
C ----- CONTAINING BOUNDARY NODAL NUMBER.	DATA2085
C	DATA2090
DO 669 NP=1,NVNP	DATA2095
NI=NPVB(NP)	DATA2100
C	DATA2105
DO 665 I=1,NBNP	DATA2110
NJ=NPBB(I)	DATA2115
IF(NJ.NE.NI) GO TO 665	DATA2120
NII=I	DATA2125
GO TO 667	DATA2130
665 CONTINUE	DATA2135

C	PRINT 6670, NP	DATA2140
	STOP	DATA2145
	667 NPVB(NP)-NII	DATA2150
C	669 CONTINUE	DATA2155
		DATA2160
C	----- PRINT COMPUTED BOUNDARY NODAL NUMBER FOR ALL VB NODES	DATA2165
		DATA2170
C	LINE-0	DATA2175
	DO 670 I-1,NVNP,10	DATA2180
	LINE=LINE+1	DATA2185
	IF(MOD(LINE-1,50).EQ.0) PRINT 6700	DATA2190
	NJMN-I	DATA2195
	NJMX-MINO(I+9,NVNP)	DATA2200
	PRINT 6750, (J,NPVB(J),J-NJMN,NJMX)	DATA2205
	670 CONTINUE	DATA2210
		DATA2215
C	----- CHANGE ISV(I,MP) I-1,4 FROM CONTAINING GLOBAL NODAL	DATA2220
	NUMBER TO CONTAINING BOUNDARY NODAL NUMBER.	DATA2225
C		DATA2230
	DO 690 MP-1,NVES	DATA2235
	MPB-ISV(5,MP)	DATA2240
	DO 685 IQ-1,4	DATA2245
	NB-ISB(IQ,MPB)	DATA2250
	DO 675 I-1,NVNP	DATA2255
	NI-NPVB(I)	DATA2260
	IF(NI.NE.NB) GO TO 675	DATA2265
	NII-I	DATA2270
	GO TO 680	DATA2275
	675 CONTINUE	DATA2280
	PRINT 6751, IQ,MP	DATA2285
	STOP	DATA2290
	680 ISV(IQ,MP)-NII	DATA2295
	685 CONTINUE	DATA2300
	690 CONTINUE	DATA2305
		DATA2310
C	----- PRINT COMPUTED BOUNDARY NODAL NUMBER & SIDE NUMBER AND	DATA2315
	RAINFALL TYPES FOR ALL VS SIDES	DATA2320
C		DATA2325
	LINE-0	DATA2330
	DO 695 MP-1,NVES,3	DATA2335
	LINE=LINE+1	DATA2340
	IF(MOD(LINE-1,50).EQ.0) PRINT 6900	DATA2345
	NJMN-MP	DATA2350
	NJMX-MINO(MP+2,NVES)	DATA2355
	PRINT 6950, (J,(ISV(I,J),I-1,5),IRTP(J),J-NJMN,NJMX)	DATA2360
	695 CONTINUE	DATA2365
		DATA2370
		DATA2375

C		DATA2380
C	***** DATA SET 14: DIRICHLET BOUNDARY CONDITIONS	DATA2385
C		DATA2390
C	----- READ AND PRINT TOTAL DIRICHLET HEAD PROFILES	DATA2395
C		DATA2400
	700 IF(NDNP.EQ.6) GO TO 80	DATA2405
	PRINT 7000	DATA2410
	DO 710 I=1,NDPR	DATA2415
	READ 20, (THDBF(J,I),HDBF(J,I),J-1,NDDP)	DATA2420
	PRINT 7100, I	DATA2425
	PRINT 5510, (THDBF(J,I),HDBF(J,I),J-1,NDDP)	DATA2430
	710 CONTINUE	DATA2435
C		DATA2440
C	----- READ GLOBAL NODAL NUMBER OF ALL DIRICHLET NODES AND	DATA2445
C	----- THE TYPE OF TOTAL HEAD ASSIGNED TO EACH OF THEM.	DATA2450
C		DATA2455
	READ 10, (NPDB(I),I-1,NDNP)	DATA2460
	CALL READN(IDTYP,MXDNP,NDNP)	DATA2465
C		DATA2470
C	----- PRINT GLOBAL NODAL NUMBER AND PROFILE OF DIRICHLET NODES	DATA2475
C		DATA2480
	LINE=0	DATA2485
	DO 720 I=1,NDNP,5	DATA2490
	LINE=LINE+1	DATA2495
	IF(MOD(LINE-1,50).EQ.0) PRINT 7200	DATA2500
	NJMN=I	DATA2505
	NJMX=MINO(I+4,NDNP)	DATA2510
	PRINT 7250, (J,NPDB(J),IDTYP(J),J-NJMN,NJMX)	DATA2515
	720 CONTINUE	DATA2520
C		DATA2525
C	----- CHANGE NPDB FROM CONTAINING GLOBAL NODAL NUMBER TO	DATA2530
C	----- CONTAINING BOUNDARY NODAL NUMBER.	DATA2535
C		DATA2540
	DO 769 NP=1,NDNP	DATA2545
	NI=NPDB(NP)	DATA2550
C		DATA2555
	DO 765 I=1,NBNP	DATA2560
	NJ=NPBB(I)	DATA2565
	IF(NJ.NE.NI) GO TO 765	DATA2570
	NII=I	DATA2575
	GO TO 767	DATA2580
	765 CONTINUE	DATA2585
C		DATA2590
	PRINT 7670, NP	DATA2595
	STOP	DATA2600
	767 NPDB(NP)=NII	DATA2605
C		DATA2610
	769 CONTINUE	DATA2615

C		DATA2620
C	----- PRINT COMPUTED BOUNDARY NODAL NUMBER AND TYPE OF PROFILES	DATA2625
C	----- FOR DIRICHLET BOUNDARY NODES	DATA2630
C		DATA2635
	LINE=0	DATA2640
	DO 770 I=1,NDNP,5	DATA2645
	LINE=LINE+1	DATA2650
	IF(MOD(LINE-1,50).EQ.0) PRINT 7700	DATA2655
	NJMN=I	DATA2660
	KJMX=MINO(I+4,NDNP)	DATA2665
	PRINT 7750, (J,NPDB(J),IDTYP(J),J-NJMN,NJMX)	DATA2670
	770 CONTINUE	DATA2675
C		DATA2680
C	***** DATA SET 15: CAUCHY BOUNDARY CONDITIONS	DATA2685
C		DATA2690
C	----- READ AND PRINT CAUCHY FLUX PROFILES	DATA2695
C		DATA2700
	800 IF(NCES.EQ.0) GO TO 900	DATA2705
	PRINT 8000	DATA2710
	DO 810 I=1,NCPR	DATA2715
	READ 20, (TQCBF(J,I),QCBF(J,I),J=1,NCDP)	DATA2720
	PRINT 8100, I	DATA2725
	PRINT 5510, (TQCBF(J,I),QCBF(J,I),J=1,NCDP)	DATA2730
	810 CONTINUE	DATA2735
C		DATA2740
C	----- READ CAUCHY FLUX TYPE ASSIGNED TO EACH CAUCHY SIDE	DATA2745
C		DATA2750
	CALL READN(ICTYP,MXCES,NCES)	DATA2755
C		DATA2760
C	----- READ FOUR GLOBAL NODE NUMBER FOR EACH OF ALL CAUCHY SIDES	DATA2765
C		DATA2770
	MPI=0	DATA2775
	820 READ 10, MI,NSEQ,MIAD,I1,I2,I3,I4,I1AD,I2AD,I3AD,I4AD	DATA2780
	IF(MI.EQ.0) GO TO 830	DATA2785
	MJ=MI+NSEQ	DATA2790
	DO 825 MP=MI,MJ	DATA2795
	I=MI+(MP-MI)*MIAD	DATA2800
	ISC(1,I)=I1+(MP-MI)*I1AD	DATA2805
	ISC(2,I)=I2+(MP-MI)*I2AD	DATA2810
	ISC(3,I)=I3+(MP-MI)*I3AD	DATA2815
	ISC(4,I)=I4+(MP-MI)*I4AD	DATA2820
	MPI=MPI+1	DATA2825
	825 CONTINUE	DATA2830
	GO TO 820	DATA2835
	830 IF(MPI.EQ.NCES) GO TO 835	DATA2840
	PRINT 8300	DATA2845
	STOP	DATA2850

C		DATA2855
C	----- PRINT INPUTTED GLOBAL NODAL NUMBER AND CAUCHY FLUX TYPES	DATA2860
C	----- FOR ALL CAUCHY BOUNDARY ELEMENT SIDES.	DATA2865
C		DATA2870
	835 LINE=0	DATA2875
	DO 840 MP=1,NCES,3	DATA2880
	LINE=LINE+1	DATA2885
	IF(MOD(LINE-1,50).EQ.0) PRINT 8400	DATA2890
	NJMN=MP	DATA2895
	NJMX=MINO(MP+2,NCES)	DATA2900
	PRINT 8450, (J,(ISC(I,J),I-1,4),ICTYP(J),J-NJMN,NJMX)	DATA2905
	840 CONTINUE	DATA2910
C		DATA2915
C	----- READ GLOBAL NODAL NUMBER FOR EACH OF ALL CAUCHY NODES.	DATA2920
C		DATA2925
	READ 10, (NPCB(I),I-1,NCNP)	DATA2930
C		DATA2935
C	----- PRINT GLOBAL NODAL NUMBER FOR ALL CAUCHY NODES	DATA2940
C		DATA2945
	LINE=0	DATA2950
	DO 845 I=1,NCNP,10	DATA2955
	LINE=LINE+1	DATA2960
	IF(MOD(LINE-1,50).EQ.0) PRINT 8500	DATA2965
	NJMN=I	DATA2970
	NJMX=MINO(I+9,NCNP)	DATA2975
	PRINT 8550, (J,NPCB(J),J-NJMN,NJMX)	DATA2980
	845 CONTINUE	DATA2985
C		DATA2990
C	----- COMPUTE BOUNDARY SIDE NUMBER FOR ALL CAUSHY SIDES	DATA2995
C		DATA3000
	DO 859 MI=1,NCES	DATA3005
	DO 851 IQ=1,4	DATA3010
	851 NIMI(IQ)=ISC(IQ,MI)	DATA3015
C		DATA3020
	DO 857 MJ=1,NBES	DATA3025
	DO 852 JQ=1,4	DATA3030
	IJ=ISB(JQ,MJ)	DATA3035
	852 NJMJ(JQ)=NPBB(IJ)	DATA3040
	IEQ=0	DATA3045
	DO 856 IQ=1,4	DATA3050
	NI=NIMI(IQ)	DATA3055
	DO 853 JQ=1,4	DATA3060
	NJ=NJMJ(JQ)	DATA3065
	IF(NJ.EQ.NI) GO TO 855	DATA3070
	853 CONTINUE	DATA3075
	GO TO 857	DATA3080
	855 IEQ=IEQ+1	DATA3085
	856 CONTINUE	DATA3090
	IF(IEQ.EQ.4) GO TO 858	DATA3095
	857 CONTINUE	DATA3100

C	PRINT 8570, MI	DATA3105
	STOP	DATA3110
	858 ISC(5,MI)-MJ	DATA3115
C	859 CONTINUE	DATA3120
C	----- CHANGE NPCB FROM CONTAINING GLOBAL NODAL NUMBER TO	DATA3125
C	----- CONTAINING BOUNDARY NODAL NUMBER.	DATA3130
C	DO 869 NP-1,NCNP	DATA3135
	NI-NPCB(NP)	DATA3140
C	DO 865 I-1,NBNP	DATA3145
	NJ-NPBB(I)	DATA3150
	IF(NJ.NE.NI) GO TO 865	DATA3155
	NII-I	DATA3160
	GO TO 867	DATA3165
	865 CONTINUE	DATA3170
C	PRINT 8670, NP	DATA3175
	STOP	DATA3180
	867 NPCB(NP)-NII	DATA3185
C	869 CONTINUE	DATA3190
C	----- PRINT COMPUTED BOUNDARY NODAL NUMBER FOR ALL CAUCHY NODES	DATA3195
C	LINE-0	DATA3200
	DO 870 I-1,NCNP,10	DATA3205
	LINE-LINE+1	DATA3210
	IF(MOD(LINE-1,50).EQ.0) PRINT 8700	DATA3215
	NJMN-I	DATA3220
	NJMX-MINO(I+9,NCNP)	DATA3225
	PRINT 8750, (J,NPCB(J),J-NJMN,NJMX)	DATA3230
	870 CONTINUE	DATA3235
C	***** DATA SET 16: NEUMANN BOUNDARY CONDITIONS	DATA3240
C	----- READ AND PRINT NEUMANN FLUX PROFILES	DATA3245
C	900 IF(NNES.EQ.0) GO TO 999	DATA3250
	PRINT 9000	DATA3255
	DO 910 I-1,NNPR	DATA3260
	READ 20, (TQNB(F,J,I),QNB(F,J,I),J-1,NNDP)	DATA3265
	PRINT 9100, I	DATA3270
	PRINT 5510, (TQNB(F,J,I),QNB(F,J,I),J-1,NNDP)	DATA3275
	910 CONTINUE	DATA3280
		DATA3285
		DATA3290
		DATA3295
		DATA3300
		DATA3305
		DATA3310
		DATA3315
		DATA3320
		DATA3325
		DATA3330
		DATA3335
		DATA3340

C		DATA3345
C	----- READ NEUMANN FLUX TYPE ASSIGNED TO EACH NEUMANN SIDE	DATA3350
C		DATA3355
	CALL READN(INTYP,MXNES,NNES)	DATA3360
C		DATA3365
C	----- READ FOUR GLOBAL NODE NUMBER FOR EACH OF ALL NEUMANN SIDES	DATA3370
C		DATA3375
	MPI=0	DATA3380
	920 READ 10, MI,NSEQ,MIAD,I1,I2,I3,I4,I1AD,I2AD,I3AD,I4AD	DATA3385
	IF(MI.EQ.0) GO TO 930	DATA3390
	MJ=MI+NSEQ	DATA3395
	DO 925 MP=MI,MJ	DATA3400
	I=MI+(MP-MI)*MIAD	DATA3405
	ISN(1,I)=I1+(MP-MI)*I1AD	DATA3410
	ISN(2,I)=I2+(MP-MI)*I2AD	DATA3415
	ISN(3,I)=I3+(MP-MI)*I3AD	DATA3420
	ISN(4,I)=I4+(MP-MI)*I4AD	DATA3425
	MPI=MPI+1	DATA3430
	925 CONTINUE	DATA3435
	GO TO 920	DATA3440
	930 IF(MPI.EQ.NNES) GO TO 935	DATA3445
	PRINT 9300	DATA3450
	STOP	DATA3455
		DATA3460
C	----- PRINT INPUTTED GLOBAL NODAL NUMBER AND NEUMANN FLUX TYPES	DATA3465
C	----- FOR ALL NEUMANN BOUNDARY ELEMENT SIDES.	DATA3470
C		DATA3475
	935 LINE=0	DATA3480
	DO 940 MP=1,NNES,3	DATA3485
	LINE=LINE+1	DATA3490
	IF(MOD(LINE-1,50).EQ.0) PRINT 9400	DATA3495
	NJMN=MP	DATA3500
	NJMX=MINO(MP+2,NNES)	DATA3505
	PRINT 9450, (J,(ISN(I,J),I-1,4),INTYP(J),J-NJMN,NJMX)	DATA3510
	940 CONTINUE	DATA3515
		DATA3520
C	----- READ GLOBAL NODAL NUMBER FOR EACH OF ALL NEUMANN NODES.	DATA3525
C		DATA3530
	READ 10, (NPNB(I),I-1,NNNP)	DATA3535
C		DATA3540
C	----- PRINT GLOBAL NODAL NUMBER FOR ALL NEUMANN NODES	DATA3545
C		DATA3550
	LINE=0	DATA3555
	DO 945 I=1,NNNP,10	DATA3560
	LINE=LINE+1	DATA3565
	IF(MOD(LINE-1,50).EQ.0) PRINT 9500	DATA3570
	NJMN=I	DATA3575
	NJMX=MINO(I+9,NNNP)	DATA3580
	PRINT 9550, (J,NPNB(J),J-NJMN,NJMX)	DATA3585
	945 CONTINUE	DATA3590

C		DATA3595
C	----- COMPUTE BOUNDARY SIDE NUMBER FOR EACH OF NEUMANN	DATA3600
C	----- BOUNDARY SIDES.	DATA3605
C		DATA3610
	DO 959 MI-1,NNES	DATA3615
	DO 951 IQ-1,4	DATA3620
	951 NIMI(IQ)-ISN(IQ,MI)	DATA3625
C		DATA3630
	DO 957 MJ-1,NBES	DATA3635
	DO 952 JQ-1,4	DATA3640
	IJ-ISB(JQ,MJ)	DATA3645
	952 NJMJ(JQ)-NPBB(IJ)	DATA3650
	IEQ-0	DATA3655
	DO 956 IQ-1,4	DATA3660
	NI-NIMI(IQ)	DATA3665
	DO 953 JQ-1,4	DATA3670
	NJ-NJMJ(JQ)	DATA3675
	IF(NJ.EQ.NI) GO TO 955	DATA3680
	953 CONTINUE	DATA3685
	GO TO 957	DATA3690
	955 IEQ-IEQ+1	DATA3695
	956 CONTINUE	DATA3700
	IF(IEQ.EQ.4) GO TO 958	DATA3705
	957 CONTINUE	DATA3710
C		DATA3715
	PRINT 9570, MI	DATA3720
	STOP	DATA3725
	958 ISN(5,MI)-MJ	DATA3730
C		DATA3735
	959 CONTINUE	DATA3740
C		DATA3745
C	----- CHANGE NPNB FROM CONTAINING GLOBAL NODAL NUMBER TO	DATA3750
C	----- CONTAINING BOUNDARY NODAL NUMBER.	DATA3755
C		DATA3760
	DO 969 NP-1,NNNP	DATA3765
	NI-NPNB(NP)	DATA3770
C		DATA3775
	DO 965 I-1,NBNP	DATA3780
	NJ-NPBB(I)	DATA3785
	IF(NJ.NE.NI) GO TO 965	DATA3790
	NII-I	DATA3795
	GO TO 967	DATA3800
	965 CONTINUE	DATA3805
C		DATA3810
	PRINT 9670, NP	DATA3815
	STOP	DATA3820
	967 NPNB(NP)-NII	DATA3825
C		DATA3830
	969 CONTINUE	DATA3835

C		DATA3840
C	----- PRINT COMPUTED BOUNDARY NODAL NUMBER FOR ALL NEUMANN NODES	DATA3845
C		DATA3850
	LINE-0	DATA3855
	DO 970 I-1,NNNP,10	DATA3860
	LINE=LINE+1	DATA3865
	IF(MOD(LINE-1,50).EQ 0) PRINT 9700	DATA3870
	NJMN-I	DATA3875
	NJMX-MINO(I+9,NNNP)	DATA3880
	PRINT 9750, (J,NPNB(J),J-NJMN,NJMX)	DATA3885
	970 CONTINUE	DATA3890
C		DATA3895
	999 CONTINUE	DATA3900
C		DATA3905
	RETURN	DATA3910
C		DATA3915
	10 FORMAT(16I5)	DATA3920
	20 FORMAT(8D10.3)	DATA3925
	30 FORMAT(80I1)	DATA3930
	40 FORMAT(3I5,5X,6D10.3)	DATA3935
C		DATA3940
	1000 FORMAT(40H0 **** BASIC INTEGER PARAMETERS ****//5X,	DATA3945
	1 40H NUMBER OF NODAL POINTS.,I5/ 5X,	DATA3950
	2 40H NUMBER OF ELEMENTS.,I5/ 5X,	DATA3955
	3 40H NUMBER OF DIFFERENT MATERIALS,I5/ 5X,	DATA3960
	4 40H NUMBER OF CORRECTION MATERIALS.,I5/ 5X,	DATA3965
	5 40H NUMBER OF TIME INCREMENTS,I5//5X,	DATA3970
	6 40H STEADY-STATE I.C. CONTROL,I5/ 5X,	DATA3975
	8 40H NUMBER OF SOIL PARAMETERS,I5/ 5X,	DATA3980
	9 40H NUMBER OF MATERIAL PROPERTIES,I5//5X,	DATA3985
	A 40H AUXILIARY STORAGE CONTROL,I5/ 5X,	DATA3990
	B 40H CONDUCTIVITY-PERMEABILITY CONTROL,I5/ 5X,	DATA3995
	C 40H GRAVITY CONTROL,I5/ 5X,	DATA4000
	E 40H NO. OF ITERATIONS PER CYCLE,I5/ 5X,	DATA4005
	F 40H NO. OF CYCLES PER TIME STEP,I5/ 5X,	DATA4010
	G 40H NO. OF TIMES TO RESET TIME STEP SIZE,I5/ 5X,	DATA4015
	H 40H NO. OF BLOCKWISE ITERATIONS ALLOWED,I5/ 5X,	DATA4020
	I 40H NO. OF SUBREGIONS,I5/)	DATA4025
	1100 FORMAT(5X,40H TIME INCREMENT.,E15 6/ 5X,	DATA4030
	1 40H MULTIPLIER FOR INCREASING DELT.,E15.6/ 5X,	DATA4035
	2 40H MAXIMUM VALUE OF DELT,E15.6/ 5X,	DATA4040
	3 40H MAXIMUM VALUE OF TIME,E15.6//5X,	DATA4045
	5 40H STEADY-STATE TOLERANCE.,E15.6/ 5X,	DATA4050
	6 40H TRANSIENT-STATE TOLERANCE,E15.6//5X,	DATA4055
	7 40H DENSITY OF WATER.,E15.6/ 5X,	DATA4060
	8 40H ACCELERATION OF GRAVITY,E15.6/ 5X,	DATA4065
	9 40H VISCOSITY OF WATER.,E15.6//5X,	DATA4070
	A 40H TIME-INTEGRATION PARAMETER.,E15.6/ 5X,	DATA4075
	B 40H ITERATION PARAMETER FOR NONLINEAR EQ.,E15.6/ 5X,	DATA4080
	C 40H RELAXATION PARAMETER FOR POINTWISE SOL.,E15.6//)	DATA4085

1200	FORMAT(//6X,14HOUTPUT CONTROL)	DATA4090
1210	FORMAT(10X,50I2)	DATA4095
1300	FORMAT(//6X,19HDISK OUTPUT CONTROL)	DATA4100
1350	FORMAT(1H0,6X,'TIME OF CHANGING DELT'/(10X,8D12.4))	DATA4105
1400	FORMAT(36H1 **** MATERIAL PROPERTIES **** // 9H MAT. NO., 9(> 3A4))	DATA4110 DATA4115
1410	FORMAT(18,9D12.4)	DATA4120
1500	FORMAT(44H1INPUT TABLE 3. MOISTURE-CONTENT PARAMETERS// > 9H MAT. NO.,8(3A4))	DATA4125 DATA4130
1510	FORMAT(18,9D12.4/(8X,9D12.4))	DATA4135
1600	FORMAT(40H1 **** CONDUCTIVITY PARAMETERS **** // 9H MAT. NO., > 8(3A4))	DATA4140 DATA4145
2000	FORMAT(1H0/5X,'*** ERROR IN READING COORDINATE STOP ***'/)	DATA4150
2100	FORMAT(38H1 **** NODAL COORDINATE DATA **** //1X, > 3(1X,5H NODE,11H X ,11H Y ,11H Z ,1X)/1X,DATA4160 > 3(1X,5H ****,33H ***** :***** ***** ,1X))	DATA4155 DATA4165
2110	FORMAT(1H ,3(1X,15,3D11.3,1X))	DATA4170
2700	FORMAT(62H1 **** ELEMENT DATA: GLOBAL INDICES OF ELEMENT NODES 1 **** //2(5X,5H ELM,5H NOD1,5H NOD2,5H NOD3,5H NOD4,5H NOD5, 2 5H NOD6,5H NOD7,5H NOD8,5H MTYP)/2(5X,5H ----,5H ----,5H ----, 3 5H ----,5H ----,5H ----,5H ----,5H ----,5H ----,5H ----))	DATA4175 DATA4180 DATA4185 DATA4190
3000	FORMAT(////'ERROR IN READING IE, MMP -',15,' NEL -',15,' STOP')	DATA4195
3100	FORMAT(2(5X,10I5))	DATA4200
4200	FORMAT(////40H ERROR IN MATERIAL TYPE CODE FOR ELEMENT,15///)	DATA4205
4300	FORMAT(////28H EXECUTION HALTED BECAUSE OF,15,13H FATAL ERRORS///)	DATA4210
5100	FORMAT('1 **** TRANSIENT INTEGERS **** '// 5X, 1 ' NO. OF SOURCE ELEMENTS',15/ 5X, 2 ' NO. OF SOURCE PROFILES',15/ 5X, 3 ' NO. OF DATA POINTS FOR EACH SOURCE PROF',15/ 5X, 4 ' NO. OF WELL SOURCES/SINKS NODES',15/ 5X, 5 ' NO. OF WELL SOURCE PROFILES',15/ 5X, 6 ' NO. OF DATA POINTS IN EACH WELL PROF. .',15/)	DATA4215 DATA4220 DATA4225 DATA4230 DATA4235 DATA4240 DATA4245
5150	FORMAT(1H /5X, 1 40H NO. OF CAUCHY SIDES,15/ 5X, 2 40H NO. OF CAUCHY NODES,15/ 5X, 3 40H NO. OF CAUCHY FLUX PROFILES,15/ 5X, 4 40H NO. OF DATA POINTS IN EACH CAUCHY PROF.,15/ 5X, 5 40H NO. OF NEUMANN SIDES,15/ 5X, 6 40H NO. OF NEUMANN NODES,15/ 5X, 7 40H NO. OF NEUMANN FLUXES,15/ 5X, 8 40H NO. OF DATA POINTS IN NEUMANN PROF. . .,15/ 5X, 9 40H NO. OF VARIABLE BOUNDARY SIDES.,15/ 5X, A 40H NO. OF VARIABLE BOUNDARY NODES.,15/ 5X, B 40H NO. OF RAINFALL PROFILES,15/ 5X, C 40H NO. OF DATA POINTS IN RAINFALL PROF. .,15/ 5X, D 40H NO. OF DIRICHLET NODES,15/ 5X, E 40H NO. OF DIRICHLET TOTAL HEAD PROF. . .,15/ 5X, F 40H NO. OF DATA POINTS IN DIRICHLET PROF. .,15/)	DATA4250 DATA4255 DATA4260 DATA4265 DATA4270 DATA4275 DATA4280 DATA4285 DATA4290 DATA4295 DATA4300 DATA4305 DATA4310 DATA4315 DATA4320 DATA4325
5300	FORMAT(1H1/5X,27H *** SOURCE INFORMATION ***)	DATA4330

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5500 FORMAT(1H0/5X,12H PROFILE NO. ,I2,/ 5(4X,4HTIME,6X,6HSOURCE,2X)/
  > 5(4X,4H----,6X,6H-----,2X)) DATA4335
5510 FORMAT(1H ,5(2D11.3)) DATA4340
5600 FORMAT(1H0//10X,65H ELEMENT NUMBER AND PROFILE TYPES OF ELEMENT DATA4345
  1 //5X,5(5H I,5H MSEL,5H STYP,5X)) DATA4350
5650 FORMAT(1H ,4X,5(3I5,5X)) DATA4360
5700 FORMAT(1H0///5X,37H *** WELL SOURCE/SINK INFORMATION ***) DATA4365
5710 FORMAT(1H0/5X,12K PROFILE NO. ,I2/ 4(4X,4HTIME,6X,6HSOURCE,2X)/
  1 4(4X,4H----,6X,6H ----,2X)) DATA4370
5800 FORMAT(1H0//10X,65H GLOBAL NODAL NUMBER AND PROFILE TYPE OF WELLS DATA4380
  LOUGE/SINK NODES //5X,5(5H I,5H NPW,5H WTYP,5X)) DATA4385
5850 FORPAT(1H ,4X,5(3I5,5X)) DATA4390
6000 FORMAT(1H1/5X,46H **** RAINFALL-SEEPAGE BOUNDARY CONDITIONS ***) DATA4395
6100 FORMAT(1H0///10X,25H --- RAINFALL PROFILE ---) DATA4400
6150 FORMAT(1H0/5X,12H PROFILE NO. ,I2,//5(4X,4HTIME,6X,6H RAINS,2X)/
  > 5(4X,4H----,6X,6H-----,2X)) DATA4405
6300 FORMAT(1H0,10X,61H *** ERROR IN READING RAINFALL-SEEPAGE ELEMENT DATA4410
  ISIDE STOP ***) DATA4415
6400 FORMAT(1H0/10X,36H --- INPUTTED VARIABLE SIDE DATA ---//5X,
  2 3(5H MP,5H GN1,5H GN2,5H GN3,5H GN4,5H RTYP,5X)/5X,
  3 3(30H -- --- --- --- ---,5X)) DATA4420
6450 FORMAT(1H ,4X,3(6I5,5X)) DATA4425
6500 FORMAT(1H0/10X,36H --- INPUTTED VARIABLE NODE DATA ---//1X,
  1 3(1X,5H I,5H NPVB,12H HCON ,12H HMIN ,1X)/1X,
  2 3(1X,5H -,5H ----,12H ---- ,12H ---- ,1X)) DATA4430
6550 FORMAT(1H ,3(1X,2I5,2D12.4,1X)) DATA4435
6570 FORMAT(1H1/5X,44H CANNOT FIND A BOUNDARY SIDE COINCIDING WITH,
  1 I3,36H-TH VARIABLE BOUNDARY SIDE: STOP ***) DATA4440
6670 FORMAT(1H1/5X,44H *** CANNOT FIND A BOUNDARY NODAL NUMBER FOR,
  1 I3,31H-TH VARIABLE BOUNDARY NODE STOP) DATA4445
6700 FORMAT(1H0//10X,47H COMPUTED BOUNDARY NODAL NUMBER OF ALL VB NODES DATA4450
  1 //5X,10(5H I,5H NPVB,2X)/5X,10(5H -,5H ----,2X)) DATA4455
6750 FORMAT(1H ,4X,10(2I5,2X)) DATA4460
6751 FORMAT(1H0,5X,42H *** CAN NOT FIND A COMPRESSED RS NODE FOR,
  1 I2,12H-TH POINT OF,I4,20H-TH RS SIDE STOP ***) DATA4465
6900 FORMAT(1H0/10X,30H --- COMPUTED VB SIDE DATA ---,//1X,
  1 3(5H MP,5H CNP1,5H CNP2,5H CNP3,5H CNP4,5H MPB,5H RTYP,1X)/1X,
  2 3(5H --,5H ----,5H ----,5H ----,5H ----,5H ----,5H ----,1X)) DATA4470
6950 FORMAT(1H ,3(7I5,1X)) DATA4475
7000 FORMAT(1H1/5X,40H **** DIRICHLET BOUNDARY CONDITIONS ****) DATA4480
7100 FORMAT(1H0/5X,12H PROFILE NO. ,I2,/ 4(4X,4HTIME,6X,6H HEAD ,2X)/
  > 4(4X,4H----,6X,6H ---- ,2X)) DATA4485
7200 FORMAT(1H0//10X,65H GLOBAL NODAL NUMBER AND PROFILE TYPE OF DIRICHDATA4490
  LET BOUNDARY NODES//5X,5(5H I,5H NPDB,5H TYPE,5X)/
  1 5X,5(5H -,5H ----,5H ----,5X)) DATA4495
7250 FORMAT(1H ,4X,5(3I5,5X)) DATA4500
7670 FORMAT(1H1/5X,44H *** CANNOT FIND A BOUNDARY NODAL NUMBER FOR,
  1 I3,32H-TH DIRICHLET BOUNDARY NODE STOP) DATA4505

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7700 FORMAT(1H0//10X,66H COMPUTED BOUNDARY NODAL NUMBER & TYPE OF DIRICDATA4575
1HLET BOUNDARY NODES//5X,5(5H I,5H NPDB,5H TYPE,5X)/ DATA4580
1 5X,5(5H -,5H ----,5H ----,5X)) DATA4585
7750 FORMAT(1H ,4X,5(3I5,5X)) DATA4590
8000 FORMAT(1H1/5X,38H **** CAUCHY BOUNDARY CONDITIONS ****) DATA4595
8100 FORMAT(1H0/5X,12H PROFILE NO.,12/ 4(4X,4HTIME,6X,6H FLUX ,2X)/ DATA4600
> 4(4X,4H----,6X,6H ---- ,2X)) DATA4605
8300 FORMAT(1H0,10X,61H *** ERROR IN READING CAUCHY BOUNDARY ELEMEN DATA4610
1T SIDE STOP *) DATA4615
8400 FORMAT(1H0/10X,34H --- INPUTTED CAUCHY SIDE DATA ---//5X, DATA4620
1 3(5H MP,5H GN1,5H GN2,5H GN3,5H GN4,5H GTYP,5X)/5X, DATA4625
3 3(30H -- ---- ---- ---- ----,5X)) DATA4630
8450 FORMAT(1H ,4X,3(6I5,5X)) DATA4635
8500 FORMAT(1H0/10X,34H --- INPUTTED CAUCHY NODE DATA ---//5X, DATA4640
1 10(5H I,5H NPCB,2X)/5X,10(5H -,5H ----,2X)) DATA4645
8550 FORMAT(1H ,4X,10(2I5,2X)) DATA4650
8570 FORMAT(1H1/5X,44H CANNOT FIND A BOUNDARY SIDE COINCIDING WITH, DATA4655
1 I3,36H-TH CAUCY BOUNDARY SIDE: STOP ***) DATA4660
8670 FORMAT(1H1/5X,44H *** CANNOT FIND A BOUNDARY NODAL NUMBER FOR, DATA4665
1 I3,31H-TH CAUCHY BOUNDARY NODE: STOP) DATA4670
8700 FORMAT(1H0/10X,34H --- COMPUTED CAUCHY NODE DATA ---//5X, DATA4675
1 10(5H I,5H NPCB,2X)/5X,10(5H -,5H ----,2X)) DATA4680
8750 FORMAT(1H ,4X,10(2I5,2X)) DATA4685
9000 FORMAT(1H1/5X,38H **** NEUMANN BOUNDARY CONDITIONS ****) DATA4690
910J FORMAT(1H0/5X,12H PROFILE NO.,12/ 4(4X,4HTIME,6X,6H FLUX ,2X)/ DATA4695
> 4(4X,4H----,6X,6H ---- ,2X)) DATA4700
9300 FORMAT(1H0,10X,61H *** ERROR IN READING NEUMANN BOUNDARY ELEMEN DATA4705
>T SIDE STOP *) DATA4710
9400 FORMAT(1H0/10X,35H --- INPUTTED NEUMANN SIDE DATA ---//5X, DATA4715
1 3(5H MP,5H GN1,5H GN2,5H GN3,5H GN4,5H NTYP,5X)/5X, DATA4720
2 3(30H -- ---- ---- ---- ---- ----,5X)) DATA4725
9450 FORMAT(1H ,4X,3(6I5,5X)) DATA4730
9500 FORMAT(1H0/10X,35H -- INPUTTED NEUMANN NODE DATA ---//5X, DATA4735
1 10(5H I,5H NPNB,2X)/5X,10(5H -,5H ----,2X)) DATA4740
9550 FORMAT(1H ,4X,10(2I5,2X)) DATA4745
9570 FORMAT(1H1/5X,44H CANNOT FIND A BOUNDARY SIDE COINCIDING WITH, DATA4750
1 I3,37H-TH NEUMANN BOUNDARY SIDE: STOP ***) DATA4755
9670 FORMAT(1H1/5X,44H *** CANNOT FIND A BOUNDARY NODAL NUMBER FOR, DATA4760
1 I3,31H-TH NEUMANN BOUNDARY NODE: STOP) DATA4765
9700 FORMAT(1H0/10X,35H --- COMPUTED NEUMANN NODE DATA ---//5X, DATA4770
1 10(5H I,5H NPNB,2X)/5X,10(5H -,5H ----,2X)) DATA4775
9750 FORMAT(1H ,4X,10(2I5,2X)) DATA4780
C DATA4785
END DATA4790

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SUBROUTINE SURF(X,Y,Z,IE, DCOSE,ISB,NPBB)

SURF 005

(Same as those in Appendix A)

	SUBROUTINE PAGEN(GNOJCN, IE)	PAGE 005
C		PAGE 010
C	*****1*****2*****3*****4*****5*****6*****7**	PAGE 015
C		PAGE 020
C	----- TO GENERATE POINTER ARRAYS.	PAGE 025
C		PAGE 030
C	*****1*****2*****3*****4*****5*****6*****7**	PAGE 035
C		PAGE 040
C	----- INPUT: IE(NEL,9)	PAGE 045
C		PAGE 050
C	----- OUTPUT: GNOJCN(JBAND,NNP)	PAGE 055
C		PAGE 060
C	*****1*****2*****3*****4*****5*****6*****7**	PAGE 065
C		PAGE 070
	IMPLICIT REAL*8(A-H,O-Z)	PAGE 075
	INTEGER*4 GNOJCN	PAGE 080
C		PAGE 085
	COMMON /SGEOM/ MAXEL,MAXNP,MAXBES,MAXBNP,JBAND,MAXNTI,MXNDTC	PAGE 090
	COMMON /CGEOM/ NNP,NEL,NBNP,NBES,KGRAV,NTI,NDTCHG	PAGE 095
	COMMON /CINTE/ NCYL,NITER,KSTR,KPRO,KDSK0,KSS,NPITER,IGEOM	PAGE 100
C		PAGE 105
	DIMENSION GNOJCN(JBAND,MAXNP),IE(MAXEL,9)	PAGE 110
	DIMENSION IEM(8)	PAGE 115
C		PAGE 120
C	***** GENERATE GNOJCN(JBAND,MAXNP) BASED ON IE(MAXEL,9)	PAGE 125
C		PAGE 130
	DO 490 NP=1,NNP	PAGE 135
C		PAGE 140
	DO 110 I=1,JBAND	PAGE 145
	110 GNOJCN(I,NP)=0	PAGE 150
C		PAGE 155
	NLNOD=0	PAGE 160
	KOUNT=0	PAGE 165
C		PAGE 170
	DO 390 M=1,NEL	PAGE 175
C		PAGE 180
	DO 160 IQ=1,8	PAGE 185
	160 IEM(IQ)=IE(M,IQ)	PAGE 190
C		PAGE 195
	DO 170 IQ=1,8	PAGE 200
	NI=IEM(IQ)	PAGE 205
	IF(NI.NE.NP) GO TO 170	PAGE 210
	GO TO 220	PAGE 215
	170 CONTINUE	PAGE 220
	GO TO 390	PAGE 225
C		PAGE 230
	220 DO 290 IQ=1,8	PAGE 235
	NI=IE(M,IQ)	PAGE 240

C		PAGE 245
C	----- COMPRESS THE NODES TO 1 TO JBAND	PAGE 250
C		PAGE 255
	NLNOD=NLNOD+1	PAGE 260
	IF(NLNOD.GT.1) GO TO 230	PAGE 265
C		PAGE 270
C	----- THE FIRST NODE IS ENCOUNTERED	PAGE 275
C		PAGE 280
	KOUNT=KOUNT+1	PAGE 285
	GNOJCN(KOUNT,NP)=NI	PAGE 290
	GO TO 290	PAGE 295
C		PAGE 300
C	----- IF NLNOD IS GREATER THAN 1, WE HAVE TO CHECK IF NI IS THE	PAGE 305
C	----- NODE ALREADY COMPRESSED? IF YES, SKIP. IF NOT INCREASE THE	PAGE 310
C	----- KOUNT.	PAGE 315
C		PAGE 320
	230 DO 240 J=1,KOUNT	PAGE 325
	NJ=GNOJCN(J,NP)	PAGE 330
	IF(NI.EQ.NJ) GO TO 290	PAGE 335
	240 CONTINUE	PAGE 340
C		PAGE 345
C	----- THE NODE NI HAS NOT BEEN COMPRESSED YET. HENCE COMPRESS IT.	PAGE 350
C		PAGE 355
	KOUNT=KOUNT+1	PAGE 360
	GNOJCN(KOUNT,NP)=NI	PAGE 365
C		PAGE 370
	290 CONTINUE	PAGE 375
C		PAGE 380
	390 CONTINUE	PAGE 385
C		PAGE 390
	IF(KOUNT.LE.JBAND) GO TO 490	PAGE 395
	KONT=KOUNT-1	PAGE 400
	JBND=JBAND-1	PAGE 405
	WRITE(6,1000) NP,KONT,JBND	PAGE 410
	STOP	PAGE 415
C		PAGE 420
	490 CONTINUE	PAGE 425
C		PAGE 430
C	***** PRINT GENERATED ARRAY GNOJCN	PAGE 435
C		PAGE 440
	IF(MOD(IGEOM,2).EQ.0) GO TO 595	PAGE 445
	LINE=0	PAGE 450
	DO 590 NP=1,NNP	PAGE 455
	LINE=LINE+1	PAGE 460
	IF(MOD(LINE-1,50).EQ.0) PRINT 5000	PAGE 465
	PRINT 5100, NP,(GNOJCN(I,NP),I=1,JBAND)	PAGE 470
	590 CONTINUE	PAGE 475
	595 CONTINUE	PAGE 480

C		PAGE 485
1000	FORMAT(1H0//5X,' ***',I4,'-TH NODE HAS ',I4,' NODES SURROUNDING',	PAGE 490
1	' IT, WHICH IS MORE THAN JBAND - 1 -',I5,' STOP ***')	PAGE 495
5000	FORMAT(1H1/5X,' ** GENERATED SURROUNDING NODES OF ALL NODES *'//	PAGE 500
1	5X,' NP 1 2 3 4 5 6 7 8',	PAGE 505
2	' 9 10 11 12 13 14 15 16 17',	PAGE 510
3	' 18 19 20 21 22 23 24 25 26 27',	PAGE 515
4	/5X,28(' --'))	PAGE 520
5100	FORMAT(1H ,4X,28I4)	PAGE 525
C		PAGE 530
	RETURN	PAGE 535
	END	PAGE 540

SUBROUTINE VELT(VX,VY,VZ, CMATKX, X,Y,Z, IE,H,HT,AKR, PROP) VELT 005

(Same as those in Appendix A)

SUBROUTINE Q8DV(QB,QRX,QRY,QRZ, XQ,YQ,ZQ,HTQ,AKXG,AKYG,AKZG,
1 AKXYG,AKXZG,AKYZG) Q8DV 005
Q8DV 010

(Same as those in Appendix A)

SUBROUTINE SPROP(TH,DTH,AKR, IE,H,THPROP,AKPROP) SPRO 005

(Same as those in Appendix A)

SUBROUTINE BCPREP(IE,X,Y,Z, H,VX,VI,VZ, DCOSB,ISB, NPVB,ISV,
> DCYFLX,FLX,HCON,HMIN,NPFLX,NPCCN,NPMIN, IRTYP,RFALL, NCHG) BCPR 005
BCPR 010

(Same as those in Appendix A)

SUBROUTINE ASEMBL(X,Y,Z,IE,CMATRX,RLD,LRN,HW,HP,DTH,AKR,PROP, ASEM 005
 > SOS,MSEL,ISTYP,WSS,NPW,IWTYP,KSS,W,DELT) ASEM 010

(Same as those in Appendix A)

SUBROUTINE Q8(QA,QB,RQ,DTHG,AKXG,AKYG,AKZG,AKXYG,AKXZG,AKYZG, Q8 005
 > XQ,YQ,ZQ,SOSM,AGRAV) Q8 010

(Same as those in Appendix A)

SUBROUTINE BASE(N,DNX,DNY,DNZ,DJAC,XQ,YQ,ZQ,SS,TT,UU) BASE 005

(Same as those in Appendix A)

SUBROUTINE BC(CMATRX,RLD,LRN,IE,X,Y,Z,AKR,PROP,DCOSB,ISB,NPBB, BC 005
 1 QCB,ISC,ICTYP,QNB,ISN,INTYP,FLX,HCON,HMIN,NPFLX,NPCON,NPMIN, BC 010
 2 HDB,IDTYP,NPDB,KSS) BC 015

(Same as those in Appendix A)

SUBROUTINE Q4S(R1Q,R2Q,XQ,YQ,ZQ,F1Q,F2Q) Q4S 005

(Same as those in Appendix A)

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SUBROUTINE PISS(R,RI,RL,C,LRN,OMI,EPS,NNP,NITER,MAXNP,JBAND,IBUG, PISS 005
1 KTIM) PISS 010
C PISS 015
C*****1*****2*****3*****4*****5*****6*****7**PISS 020
C PISS 025
C ----- TO SOLVE A MATRIX EQUATION WITH POINTWISE ITERATION SOLUTION PISS 030
C ----- STRATEGIES. PISS 035
C PISS 040
C*****1*****2*****3*****4*****5*****6*****7**PISS 045
C PISS 050
C ----- INPUT: RI(NNP), RL(NNP), C(NNP,JBAND), LRN(JBAND,NNP), PISS 055
C ----- OMI, EPS, NNP, NITER, MAXNP, JBAND, IBUG, AND KTIM. PISS 060
C PISS 065
C ----- OUTPUT: R(NNP) - FINAL SOLUTION; AND RI(NNP)-ITERATE. PISS 070
C PISS 075
C*****1*****2*****3*****4*****5*****6*****7**PISS 080
C PISS 085
C IMPLICIT REAL*8(A-H,O-Z) PISS 090
C PISS 095
C DIMENSION R(MAXNP),RI(MAXNP) PISS 100
C DIMENSION RL(MAXNP),C(MAXNP,JBAND),LRN(JBAND,MAXNP) PISS 105
C PISS 110
C ----- PRINT ITERATION INFORMATION IF DESIRED. PISS 115
C PISS 120
C IF(IBUG.NE.0 .AND. KTIM.NE.0) PRINT 1000 PISS 125
C PISS 130
C DO 290 IT=1,NITER PISS 135
C PISS 140
C ----- FOR EACH ITERATION, PUT THE LOAD VECTOR INTO R(MAXNP). PISS 145
C PISS 150
C DO 210 NP=1,NNP PISS 155
C 210 R(NP)=RL(NP) PISS 160
C PISS 165
C ----- THE MATRIX C = L + I + U, WHERE L IS THE LOWER TRIANGULAR PISS 170
C ----- MATRIX AND U IS THE UPPER TRIANGULAR MATRIX AND I IS THE PISS 175
C ----- DIAGONAL MATRIX. PISS 180
C ----- NOW ADD U*RI TO THE RIGHT HAND SIDE, WHERE RI IS THE PREVIOUS PISS 185
C ----- ITERATE. PISS 190
C PISS 195
C DO 230 NP=1,NNP PISS 200
C DO 220 I=1,JBAND PISS 205
C LNODE=LRN(I, NP) PISS 210
C IF(LNODE.EQ.0) GO TO 220 PISS 215
C IF(LNODE.LE.NP) GO TO 220 PISS 220
C R(NP)=R(NP)-C(NP,I)*RI(LNODE) PISS 225
220 CONTINUE PISS 230
230 CONTINUE PISS 235

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C		PISS 240
C	----- START TO COMPUTE NEW ITERATE WITH POINTWISE ITERATIONS.	PISS 245
C		PISS 250
	DO 250 NP-1,NNP	PISS 255
	DO 240 I-1,JBAND	PISS 260
	LNODE=LRN(I,NP)	PISS 265
	IF(LNODE.EQ.0) GO TO 240	PISS 270
	IF(LNODE.GE.NP) GO TO 240	PISS 275
	R(NP)=R(NP)-C(NP,I)*R(LNODE)	PISS 280
	240 CONTINUE	PISS 285
	DO 245 I-1,JBAND	PISS 290
	LNODE=LRN(I,NP)	PISS 295
	IF(LNODE.NE.NP) GO TO 245	PISS 300
	R(NP)=OMI*(R(NP)/C(NP,I)) + (1.0D0-OMI)*RI(NP)	PISS 305
	245 CONTINUE	PISS 310
	250 CONTINUE	PISS 315
C		PISS 320
C	----- CHECK IF A CONVERGENT SOLUTION IS OBTAINED?	PISS 325
C		PISS 330
	NNCVN=0	PISS 335
	RELERR=-1.0D0	PISS 340
	ABSERR=-1.0D0	PISS 345
	DO 260 NP-1,NNP	PISS 350
	ABSDIF=DABS(R(NP)-RI(NP))	PISS 355
	ABSERR=DMAX1(ABSERR,ABSDIF)	PISS 360
	IF(RI(NP).NE.0.0D0) RELERR=DMAX1(RELERR,DABS(ABSDIF/RI(NP)))	PISS 365
	IF(ABSERR.LE.EPS) GO TO 260	PISS 370
	NNCVN=NNCVN+1	PISS 375
	260 CONTINUE	PISS 380
C		PISS 385
C	----- UPDATE THE ITERATE.	PISS 390
C		PISS 395
	DO 280 NP-1,NNP	PISS 400
	280 RI(NP)=R(NP)	PISS 405
C		PISS 410
C	----- PRINT ITERATION INFORMATION IF DESIRED.	PISS 415
C		PISS 420
	IF(IBUG.NE.0 .AND. KTIM.NE.0) PRINT 1100, IT,ABSERR,RELERR,NNCVN	PISS 425
C		PISS 430
	IF(IT.EQ.1) GO TO 290	PISS 435
	IF(ABSERR.LE.EPS) GO TO 990	PISS 440
C		PISS 445
	290 CONTINUE	PISS 450
C		PISS 455
	PRINT 2000, IT,NITER,ABSERR,RELERR,NNCVN	PISS 460
C		PISS 465
	990 CONTINUE	PISS 470

C		PISS 475
	1000 FORMAT(1H0/75X,5H IT,12H ABS ERR ,12H REL ERR ,	PISS 480
	1 13H NO. OF NODES/75X,5H ---,12H --- --- ,12H --- --- ,	PISS 485
	2 13H --- -- -----)	PISS 490
	1100 FORMAT(75X,I5,2D12.4,5X,I5)	PISS 495
	2000 FORMAT(1H0/70X,43H ::: WARNING: NO CONVERGENCE IN PISS AFTER ,	PISS 500
	1 I4,11H ITERATIONS/75X,9H NPITER -,14,11H ABSERR -,D12.4/75X,	PISS 505
	2 11H RELERR -,D12.4,11H NNCVN -,I4)	PISS 510
C		PISS 515
	RETURN	PISS 520
	END	PISS 525

SUBROUTINE SFLOW(X,Y,Z,IE, H,HP,VX,VY,VZ,TH,DTH,	SFLO 005
1 BFLX,BFLXP, DCOSB,ISB,NPBB, MSEL,SOS,ISTYP,NPW,WSS,IWTYP,	SFLO 010
2 NPVB,NPDB,NPCB,NPNB, DELT, KFLOW)	SFLO 015

(Same as those in Appendix A)

SUBROUTINE Q8TH(QTHM,QSOSM,DHQ,THG,XQ,YQ,ZQ,SOURCE)	Q8TH 005
---	----------

(Same as those in Appendix A)

SUBROUTINE PRINTT(VX,VY,VZ,H,HT,TH, NPBB,BFLX, NPVB,DCYFLX,NPCON,	PRIN 005
1 NPFLX,NPMIN, SUBHD, TIME,DELT, KPR,KOUT,KDIAG,ITIM)	PRIN 010

(Same as those in Appendix A)

SUBROUTINE INTERP(FALL,TRF,RF,TIME,MXPR,MXDP,NPR,NDP)

INTE 005

(Same as those in Appendix A)

SUBROUTINE READR(F,MAXNOD,NNP)

REDR 005

(Same as those in Appendix A)

SUBROUTINE READN(INDTYP,MXTYP,NTYPE)

REDN 005

(Same as those in Appendix A)

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