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# 5G Synchronization, Positioning, and Mapping from Diffuse Multipath

Fuxi Wen, *Senior Member, IEEE* and Henk Wymeersch, *Senior Member, IEEE*

**Abstract**—5G mmWave communication systems have the potential to jointly estimate the positions of user equipment (UE) and mapping their propagation environments using a single base station. But such potential depends on the characteristics of the reflecting surfaces, such as a deterministic specular nature, a stochastic diffuse/scattering nature, or a combination of both. In this letter, we proposed a 5G positioning and mapping algorithm with unknown orientation and clock bias for single-bounce diffuse multipath channel models. The method is able to accurately localize, calibrate and synchronize the UE, even in the absence of line-of-sight and specular components. This enables robust positioning and mapping using only diffuse multipath.

**Index Terms**—5G mmWave, positioning and mapping, diffuse components, tensor decomposition, orientation and clock bias calibration

## I. INTRODUCTION

5G mmWave communication systems provides new opportunities for improving the quality and robustness of communications, as well as for accurate user equipment (UE) positioning from a single base station (BS) [1]. Large bandwidth and multiple antennas, at both the BS and UE sides, allows for high resolution, with recent theoretical studies showing the potential of simultaneous positioning the UE and mapping the propagation environments utilizing the resolvable angle-of-departures (AODs), angle-of-arrivals (AOAs), and time-of-arrivals (TOAs) [2], [3]. However, this potential depends on the characteristics of the objects in the environment, whereby propagation paths may be of a deterministic specular nature, or of a stochastic diffuse/scattering nature, or a combination of both. In general, as the frequency increases, surfaces appear rougher and lead to more diffuse scatterings [4], there is higher path loss, and higher sensitivity to line-of-sight (LOS) blockage. For non-LOS (NLOS) mmWave propagation, especially for vehicle-to-everything communications in urban scenarios [5], specular components together with single-bounce diffuse components form a majority of the overall channel gain [4]. Diffuse multipath is often treated as a disturbance, though geometry-based diffuse scattering channel models can also be considered, where each surface contributes with a cluster of paths, all with similar angles and delays [6], [7]. Such a model was exploited in the positioning and mapping problem [7]. However, [7] did not consider the impact of the UE's clock bias and orientation, both of which are important practical parameters. Joint localization and synchronization has been treated in several studies [8]–[12]: an analysis based on Fisher information theory in [8] showed that, under LOS, joint localization, synchronization and orientation estimation

are possible and that NLOS paths do not negatively impact the performance. [13] showed that NLOS paths from ideal reflections can be harness to improve performance, while [9] showed that the UE location and clock bias can be estimated with a sufficient number of NLOS paths, even when the LOS is blocked. In [10] a message passing method was proposed, which requires a priori knowledge of the position and clock bias. Furthermore, cooperative network synchronization [11] and single-anchor localization and synchronization of full-duplex agents [12] have also been proposed. Common among all these works is that only specular multipath is considered, while diffuse multipath is ignored.

In this letter, we extend [7] by using estimated diffuse and specular multipath parameters to recover the UE position, orientation, clock bias and the map of the propagation environment, for single-bounce channels. Our specific contributions are as follows:

- We propose a low-complexity processing chain (requiring only a 2D search) for estimating the UE position, orientation, clock bias, and the map of the propagation environment based on a single downlink transmission;
- We demonstrate that joint synchronization, positioning, and mapping is possible *even when both LOS and specular multipath are absent*.

*Notation:* Scalars are denoted in italic, e.g.,  $x$ . Lower case boldface indicates a column vector, e.g.,  $\mathbf{x}$ . Upper case boldface denotes a matrix, e.g.,  $\mathbf{X}$  with  $\mathbf{I}_N$  representing an  $N \times N$  identity matrix, while upper case boldface calligraphic denotes a tensor, e.g.,  $\mathcal{X}$ . Matrix transpose, conjugate transpose, and inverse are indicated by superscript  $\top$ ,  $\text{H}$  and  $^{-1}$ , respectively. The Euclidean norm is denoted by  $\|\cdot\|$ , while the tensor Frobenius norm is indicated by  $\|\cdot\|_F$ . The expectation operator is denoted by  $\mathbb{E}\{\cdot\}$  and the set of all complex numbers is denoted by  $\mathbb{C}$ .

## II. SYSTEM MODEL AND PROBLEM FORMULATION

We consider a 3D scenario with a single transmitting BS with known location  $\mathbf{p}_T = [x_T, y_T, z_T]^\top$  and a receiving UE with unknown location  $\mathbf{p}_R = [x_R, y_R, z_R]^\top$ , as well as an unknown clock bias expressed in meters  $\beta c$  ( $c$  is the speed of light) and an unknown orientation  $\alpha \in [0, 2\pi)$  with respect to the vertical axis. There are  $R$  reflectors and each reflector gives rise to  $N_r \geq 1$  rays [14], with the  $l$ -th ray corresponding to an unknown and random incidence point (a scattering point (SP)) on the  $r$ th reflecting surface in the environment, denoted by  $\mathbf{p}_{rl} = [x_{rl}, y_{rl}, z_{rl}]^\top$ , whose distribution on the surface depends on the electromagnetic properties [15]. The LOS path, if it exists, has index  $r = 0$ , with  $N_0 = 1$ .

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The BS and UE both employ uniform rectangular arrays (URAs) consist of sensors in a grid of size  $M_T = M_1 \times M_2$  and  $M_R = M_3 \times M_4$ , and transmit MIMO-OFDM signals (other signals may be used provided they are compatible with the signal model (3), to be defined later) with  $M_5$  sub-carriers and sub-carrier spacing  $\Delta_f$ . The channel parameters associated with incidence point  $\mathbf{p}_{rl}$  are the 6-tuple of (i) AOD in azimuth and elevation angles  $(\phi_{rl}, \psi_{rl})$  at the BS; (ii) AOA in azimuth and elevation angles  $(\theta_{rl}, \varphi_{rl})$  at UE; (iii) the TOA  $\tau_{rl}$ ; and (v) the complex channel gain  $\gamma_{rl}$ . The models for the channel gains follows the standard path loss model for the LOS path and specular components, while for diffuse components, each gain has identical magnitude and uniform phase [7].

The downlink frequency-domain channel response for sub-carrier  $f_i$  is represented as  $\mathbf{H}_i \in \mathbb{C}^{M_R \times M_T}$  is expressed as

$$\mathbf{H}_i = \sum_{r=0}^R \sum_{l=1}^{N_r} \gamma_{rl} e^{-j2\pi f_i \tau_{rl}} \mathbf{a}_R(\theta_{rl}, \varphi_{rl}) \mathbf{a}_T^H(\phi_{rl}, \psi_{rl}), \quad (1)$$

where  $\mathbf{a}_R(\theta_{rl}, \varphi_{rl})$  and  $\mathbf{a}_T(\phi_{rl}, \psi_{rl})$  are the antenna array response vectors at the UE and BS, respectively [6], [16]. For subcarrier  $i$ ,  $\mathbf{H}_i$  can be converted in a 4D tensor of suitable dimension,  $\mathcal{H}_i \in \mathbb{C}^{M_1 \times M_2 \times M_3 \times M_4}$  [17]. The received signal on subcarrier  $i$  is of the form  $\mathbf{Y}_i = \mathbf{H}_i \mathbf{S}_i + \mathbf{N}_i$ , where  $\mathbf{S}_i$  is a known pilot signal with orthogonality property ( $\mathbf{S}_i \mathbf{S}_i^H = \rho \mathbf{I}_{M_T}$ ) and  $\mathbf{N}_i$  is i.i.d. Gaussian noise. Then we have  $\mathbf{X}_i = \frac{1}{\rho} \mathbf{Y}_i \mathbf{S}_i^H = \mathbf{H}_i + \frac{1}{\rho} \mathbf{N}_i \mathbf{S}_i^H = \mathbf{H}_i + \mathbf{W}_i$ , where  $\mathbf{W}_i$  is also i.i.d. Gaussian noise with a scaled covariance matrix.

Our objective is, given measurements  $\mathbf{X}_i$  of the mmWave channel, to determine  $\mathbf{p}_{UE}, B, \alpha$  and a parametrization of the  $K$  surfaces. This involves three steps: (i) estimation and association of parameters of specular and diffuse multipath, (ii) localization, synchronization, and orientation estimation; (iii) mapping.

### III. PROPOSED METHOD

#### A. Estimation and Association of Specular and Diffuse Multipath Parameters

**Remark 1.** While there are many mmWave channel estimation methods, our application has two specific requirements. First of all, for each estimated path, the AOA, AOD, and TOA should be correctly matched. In other words, the channel estimator should return 5D tuples, not unordered sets of angles and delays. Secondly, the estimator should provide such tuples not only for the specular paths, but also for diffuse components. This is in contrast to the conventional approach, which treats diffuse multipath as a random process without exploiting its relation to the environment geometry. To the best of our knowledge, tensor-ESPRIT (estimation of signal parameters via rotational invariance techniques) [18] is unique in meeting these two requirements and explained briefly here.

We exploit the  $R$ -D grid structure inherent in the data, as well as the Vandermonde structure in angle and delay domain to map from geometric channel parameters to spatial frequencies. For subcarrier  $i$ ,  $\mathbf{X}_i$  and  $\mathbf{W}_i$  are  $M_3 M_4 \times M_1 M_2$  matrices. We convert these  $M_5$  matrices (one per subcarrier) in a 5D tensor of suitable dimension,  $\mathcal{X}$ ,  $\mathcal{H}$  and  $\mathcal{W} \in \mathbb{C}^{M_1 \times M_2 \times M_3 \times M_4 \times M_5}$ . For the  $p$ th path ( $p = 1, 2, \dots, P$  where  $P = \sum_{k=1}^R N_k$ , where we have renumbered the paths

compared to (1)) and  $d$ -th dimension ( $d \in \{1, 2, \dots, 5\}$ ), we now introduce  $\mathbf{a}(\omega_p^{(d)}) \in \mathbb{C}^{M_d \times 1}$ , which is equivalent to the uniform linear array steering vector composed of  $M_d$  sensors, and  $\omega_p^{(d)}$  is the spatial frequency, with [17]

$$\omega_p^{(1)} = \pi \sin(\phi_p) \cos(\psi_p), \quad \omega_p^{(2)} = \pi \sin(\psi_p), \quad (2a)$$

$$\omega_p^{(3)} = \pi \sin(\theta_p) \cos(\varphi_p), \quad \omega_p^{(4)} = \pi \sin(\varphi_p), \quad (2b)$$

$$\omega_p^{(5)} = 2\pi \Delta_f \tau_p. \quad (2c)$$

For the  $p$ th path, the equivalent 5D array steering tensor can be written as  $\mathcal{A}_p = \mathbf{a}(\omega_p^{(1)}) \circ \mathbf{a}(\omega_p^{(2)}) \circ \dots \circ \mathbf{a}(\omega_p^{(5)})$ , where  $\circ$  represents the outer product. This allows us to express the observation as

$$\mathcal{X} = \sum_{p=1}^P \gamma_p \mathcal{A}_p + \mathcal{W} \in \mathbb{C}^{M_1 \times M_2 \times \dots \times M_5}. \quad (3)$$

This formulation directly allows us to apply tensor-ESPRIT [18] for channel estimation with high resolution and limited computational complexity. The basic idea of tensor-ESPRIT is exploiting the multidimensional shift invariant structure of  $\mathcal{A}_p$ . Here, the spatial frequency estimates are obtained without nonlinear optimization and without computing or searching of any spatial spectrum. The number of signal components is a prerequisite for subspace based methods, such as tensor-ESPRIT. In the the CP decomposition model [19], tensor  $\mathcal{X}$  is decomposed into a sum of rank-one tensors, each component corresponds to one path. Model order selection techniques [20] can be used to detect the number of paths  $\hat{P}$ . In general, the estimated  $\hat{P} \ll P$  for rough surfaces with hundreds of closely located diffuse paths. The reason the number of paths is underestimated is due to the finite resolution of the receiver. The diffuse multipath is generated from a very large number of scatter points on the surface of each object, densely spaced to approximate the underlying continuous distribution. The receiver can only resolve paths to the extent allowed by its bandwidth (delay resolution) and array size (angular resolution). Finally, the estimated spatial frequencies  $\{\hat{\omega}_k^{(d)}\}$  for  $d \in \{1, 2, \dots, 5\}$  and  $k \in \{1, 2, \dots, \hat{P}\}$  are converted to AOA, AOD and TOA, via (2). Additional details can be found in [7]. Each of the  $\hat{P}$  estimated paths can be associated with a 3D point on one of the  $R$  surfaces. We denote these points as *artificial* SPs, since they will be different from the  $P$  *physical* SPs  $\mathbf{p}_{rl}$  corresponding to the rays. Both the physical SPs and the artificial SPs are random. However, the proposed method does not require knowledge of their distributions.

#### B. Positioning, Synchronization, and Orientation Estimation

We make use of the following essential geometric relations. For the LOS path, we introduce  $\mathbf{p}_{01}$  as any point on the line strictly between  $\mathbf{p}_T$  and  $\mathbf{p}_R$ , but not equal to either point. Then the following relations hold for any path, i.e.,  $\forall r, l$ :

$$\tau_{rl} = \|\mathbf{p}_{rl} - \mathbf{p}_T\|/c + \|\mathbf{p}_{rl} - \mathbf{p}_R\|/c + \beta \quad (4a)$$

$$\theta_{rl} = \pi + \text{atan2}(y_{rl} - y_R, x_{rl} - x_R) - \alpha \quad (4b)$$

$$\varphi_{rl} = \text{asin}(z_{rl} - z_R) / \|\mathbf{p}_{rl} - \mathbf{p}_R\| \quad (4c)$$

$$\psi_{rl} = \text{asin}(z_{rl} - z_T) / \|\mathbf{p}_{rl} - \mathbf{p}_T\| \quad (4d)$$

$$\phi_{rl} = \text{atan2}(y_{rl} - y_T, x_{rl} - x_T). \quad (4e)$$

Due to the presence of  $\alpha$  and  $\beta$ , solving for the UE location is not trivial. We propose a two-step approach. We first determine an estimate of the UE location, assuming known orientation and clock bias. This estimate is denoted by  $\hat{\mathbf{p}}_R(\alpha, \beta)$ . Then we optimize over all pairs  $(\alpha, \beta)$  of orientations and clock biases.

1) *Estimation of  $\hat{\mathbf{p}}_R(\alpha, \beta)$* : The estimation problem is challenging, due to the lack of knowledge on whether the LOS path is present. We tackle the problem based on the methods from [21], [22]. We first define

$$\mathbf{f}_{T,k} = \begin{bmatrix} \cos(\hat{\phi}_k) \cos(\hat{\theta}_k) \\ \cos(\hat{\phi}_k) \sin(\hat{\theta}_k) \\ \sin(\hat{\phi}_k) \end{bmatrix}, \quad (5)$$

which points along the AOD of path  $k \in \{1, \dots, \hat{P}\}$ ; and  $\mathbf{f}_{R,k}$  is defined equivalently for the AOA, pointing from the UE towards the  $k$ -th artificial SP:

$$\mathbf{f}_{R,k} = \begin{bmatrix} \cos(\hat{\phi}_k) \cos(\hat{\theta}_k + \alpha - \pi) \\ \cos(\hat{\phi}_k) \sin(\hat{\theta}_k + \alpha - \pi) \\ \sin(-\hat{\phi}_k) \end{bmatrix}, \quad (6)$$

where we recall that  $\alpha$  is assumed known in this first step.

For each path  $k$ , we can establish the following relation:

$$\mathbf{p}_R = \mathbf{p}_T + c\tilde{\tau}_k \xi_k \mathbf{f}_{T,k} + c\tilde{\tau}_k (1 - \xi_k) (-\mathbf{f}_{R,k}), \quad (7)$$

where  $\tilde{\tau}_k = \hat{\tau}_k - \beta$ , where  $\xi_k \in [0, 1]$  is unknown and represents the fraction of the delay  $\tilde{\tau}_k$  that is attributed to the line from BS to a scatter point. Note that the value of  $\xi_k$  is arbitrary for the LOS path (if it is present). Rearranging the terms in (7) results in

$$\mathbf{p}_R = \boldsymbol{\delta}_k + \xi_k \mathbf{u}_k, \quad k \in \{1, \dots, \hat{P}\}, \quad (8)$$

with  $\boldsymbol{\delta}_k = \mathbf{p}_T - c\tilde{\tau}_k \mathbf{f}_{R,k}$  and  $\mathbf{u}_k = c\tilde{\tau}_k (\mathbf{f}_{T,k} + \mathbf{f}_{R,k})$ . From (8), we see that  $\xi_k \|\mathbf{u}_k\|^2 = \mathbf{u}_k^\top (\mathbf{p}_R - \boldsymbol{\delta}_k)$ . Solving for  $\xi_k$  and substituting back into (8) provides us with the following cost function

$$\mathcal{C}(\mathbf{p}_R) = \sum_{k=1}^{\hat{P}} \zeta_k \|\mathbf{p}_R - (\boldsymbol{\delta}_k + \bar{\mathbf{u}}_k^\top (\mathbf{p}_R - \boldsymbol{\delta}_k) \bar{\mathbf{u}}_k)\|^2, \quad (9)$$

where  $\bar{\mathbf{u}}_k = \mathbf{u}_k / \|\mathbf{u}_k\|$  and  $\zeta_k \geq 0$  is the weight of the  $k$ -th path, which can depend on the channel gain (amplitude) of the path. Minimizing  $\mathcal{C}(\mathbf{p}_R)$  yields a closed-form solution

$$\hat{\mathbf{p}}_R(\alpha, \beta) = \left( \sum_{k=1}^{\hat{P}} \zeta_k (\mathbf{I} - \bar{\mathbf{u}}_k \bar{\mathbf{u}}_k^\top) \right)^{-1} \sum_{k=1}^{\hat{P}} \zeta_k (\mathbf{I} - \bar{\mathbf{u}}_k \bar{\mathbf{u}}_k^\top) \boldsymbol{\delta}_k. \quad (10)$$

Note that the method does not require separation of specular and diffuse paths, nor does it rely on knowledge of which path is the LOS (or even presence of the LOS). The cost function in (9) can be applied with all  $\hat{P}$  estimated paths, or only a selected subset of paths (e.g., the strongest ones).

2) *Estimation of  $(\alpha, \beta)$* : Substituting  $\hat{\mathbf{p}}_R(\alpha, \beta)$  back into (9) yields a cost function over  $(\alpha, \beta)$ , i.e.,  $\mathcal{C}(\alpha, \beta) = \mathcal{C}(\hat{\mathbf{p}}_R(\alpha, \beta))$ , (without depending on the unknown  $\mathbf{p}_R$ ) from which  $(\alpha, \beta)$  can be found by solving

$$\text{minimize } \mathcal{C}(\alpha, \beta) \quad (11a)$$

$$\text{s.t. } \alpha \in [\alpha_{\min}, +\alpha_{\max}], \quad (11b)$$

$$\beta \in [\beta_{\min}, +\beta_{\max}], \quad (11c)$$

with a 2D grid search. Geometric constraints can be introduced to limit the size of the search space [23]. Denoting the solution to (11) by  $(\hat{\alpha}, \hat{\beta})$ , the final estimate of the UE location is  $\hat{\mathbf{p}}_R(\hat{\alpha}, \hat{\beta})$ .

**Remark 2** (Intuition of the method). *The UE state can be estimated by noticing that each estimated artificial SP provides 5 observations (1 delay and 4 angles), while being parameterized by 3 unknowns (the artificial SP position). Hence, the system is over-determined, so that with a sufficient number of estimated paths, all unknowns can be estimated, even if the artificial SP locations are unknown. Note that in contrast to [9], a single sufficiently rough surface is sufficient to provide an unambiguous UE state estimate in the absence of LOS.*

### C. Mapping the Propagation Environment

Finally, we use the estimates of the UE state to determine estimates of the environment. Given  $\hat{\mathbf{p}}_R(\hat{\alpha}, \hat{\beta})$ ,  $\hat{\alpha}$  and  $\hat{\beta}$ , we can recover artificial SPs  $\mathbf{p}_k, k \in \{1, \dots, \hat{P}\}$  as the intersection of the lines  $\mathbf{p}_T + \kappa_T \mathbf{f}_{T,k}, \kappa_T \in \mathbb{R}$  and  $\mathbf{p}_R + \kappa_R \mathbf{f}_{R,k}, \kappa_R \in \mathbb{R}$ . The least-squares solution is readily found to be

$$\hat{\mathbf{p}}_k = (\mathbf{H}_{T,k} + \mathbf{H}_{R,k})^{-1} (\mathbf{H}_{T,k} \mathbf{p}_T + \mathbf{H}_{R,k} \hat{\mathbf{p}}_R(\hat{\alpha}, \hat{\beta})), \quad (12)$$

with  $\mathbf{H}_{T,k} = \mathbf{I} - \mathbf{f}_{T,k} \mathbf{f}_{T,k}^\top$ ,  $\mathbf{H}_{R,k} = \mathbf{I} - \mathbf{f}_{R,k} \mathbf{f}_{R,k}^\top$ . Note that  $\hat{\mathbf{p}}_k$  need not correspond to any physical SP  $\mathbf{p}_{r_i}$ , due to the limited resolution in angle and delay of the 5G mmWave communication system.

In order to attach a meaning to the artificial SPs, a post-processing step is needed. The artificial SPs are first partitioned into clusters, say  $\mathcal{C}_1, \mathcal{C}_2, \dots, \mathcal{C}_{\hat{K}}$  using standard clustering methods. Each cluster  $\mathcal{C}_c$  ideally corresponds to one surface and can then be represented by a mean  $\boldsymbol{\mu}_c$  and a covariance  $\boldsymbol{\Sigma}_c$ , given by

$$\boldsymbol{\mu}_c = \frac{1}{|\mathcal{C}_c|} \sum_{i \in \mathcal{C}_c} \mathbf{p}_i, \quad (13)$$

$$\boldsymbol{\Sigma}_c = \frac{1}{|\mathcal{C}_c| - 1} \sum_{i \in \mathcal{C}_c} (\mathbf{p}_i - \boldsymbol{\mu}_c) (\mathbf{p}_i - \boldsymbol{\mu}_c)^\top \quad (14)$$

where  $|\cdot|$  denotes the number of elements of the set. The proposed algorithm is summarized in Algorithm 1. Note that equations (5), (7)–(10) for positioning and (12) for mapping are the same as in [7].

## IV. NUMERICAL RESULTS

### A. Simulation Setup

We consider a carrier frequency of 28 GHz, corresponding to  $\lambda = 1.07$  cm, a total bandwidth of 20 MHz with 100 subcarriers, of which 10 equally spaced subcarriers are used for pilots. A cyclic prefix of length 7 is used. 64 pilot OFDM symbols are sent, for a total duration of 3.52 ms. We set the pilots as  $\mathbf{S}_i = \mathbf{I}_{M_T}, \forall i$ . The BS and UE are located at  $\mathbf{p}_T = [20, 0, 8]^\top$  and  $\mathbf{p}_R = [0, 0, 2]^\top$  with unknown orientation  $\alpha = \pi/3$  and clock bias  $\beta c = 4$  m, respectively. There two reflecting surfaces: one building facade and a ground surface. The 10 m high and 20 m long building facade's center is at  $[10, 10, 5]^\top$ , with orientation  $[0, 1, 0]^\top$  ( $x$ - $z$  plane).

**Algorithm 1: Summary of the proposed algorithm**
**Input:** Channel tensor measurement  $\mathcal{X}$ 
**Output:**  $\hat{\mathbf{p}}_R, \hat{\alpha}, \hat{\beta}$  and  $\{\boldsymbol{\mu}_c, \boldsymbol{\Sigma}_c\}_{c=1,2,\dots,\hat{K}}$ 

- ```

/* Geometric Channel Estimation */
    • Estimate number of paths  $\hat{P}$  [20]
    • AOA, AOD and delay for path  $k \in [1, \hat{P}]$  [18]
/* UE Positioning and Calibration */
    • Estimate UE orientation  $\hat{\alpha}$  and clock bias  $\hat{\beta}$  (11)
    • Estimate UE position  $\hat{\mathbf{p}}_R$  by plugging  $\hat{\alpha}, \hat{\beta}$  into (10)
/* Mapping and Clustering */
    • Estimate scattering points  $\{\hat{\mathbf{p}}_k\}_{k=1,2,\dots,\hat{P}}$  by (12)
    • Cluster estimated scattering points
    • Evaluate center  $\boldsymbol{\mu}_c$  (13) and spread  $\boldsymbol{\Sigma}_c$  (14)
    
```

The second surface is at  $[10, 0, 0]^\top$  with orientation  $[0, 0, 1]^\top$  (reflected from ground,  $x$ - $y$  plane), surface dimension is  $20\text{ m} \times 20\text{ m}$ . Both surfaces are described as rough surfaces with one specular component each, using  $N_r = 50$  scatter points each. Directivity parameter  $\alpha_R = 10$  and scattering coefficient  $S = 0.6$  are used to describe the roughness of the surface. The BS and UE are equipped with URAs with  $(8 \times 8)$  elements and placed along  $y$ - $z$  plane. The inter-element spacing is  $0.5\lambda$  in both directions. and the origin is the array reference point. The Matlab package Tensorlab [24] is utilized for tensor computation.

### B. Results

We assess the capability of the proposed algorithm to estimate the positioning, clock bias and orientation using the root-mean-square error (RMSE<sup>1</sup>), defined for the position as  $\text{RMSE} = \sqrt{\mathbb{E}\{\|\mathbf{p}_R - \hat{\mathbf{p}}_R(\hat{\alpha}, \hat{\beta})\|^2\}}$ , and similarly for the bias and orientation, for different levels of signal-to-noise ratio (SNR), which is defined as  $\text{SNR} = \|\mathcal{X} - \mathcal{N}\|_F^2 / \|\mathcal{N}\|_F^2$ . We consider four different combinations<sup>2</sup> of utilizing the LOS path, specular components (interpreted as the shortest estimated path for each cluster) and diffuse paths, given by:

- C1. LOS plus the two specular components (so that  $N_0 = 1, N_1 = 1, N_2 = 1$ ).
- C2. LOS plus the diffuse paths for each cluster (so that  $N_0 = 1, N_1 \gg 1, N_2 \gg 1$ , no specular path).
- C3. The specular components plus the diffuse paths (so that  $N_0 = 0, N_1 \gg 1, N_2 \gg 1$ ).
- C4. Only the diffuse paths for each cluster (so that  $N_0 = 0, N_1 \gg 1, N_2 \gg 1$ , no specular path).

Note that the definition of the SNR implies that the effective transmit power in C4 will be larger than C3, which in turn will be larger than C1 and C2.

1) *Positioning*: Fig. 1 shows the positioning performance of the four combination. We also show two benchmarks: B1. without estimating the orientation and clock bias (without

<sup>1</sup>Since the diffuse paths cannot be resolved and the artificial SPs are a side-product of the channel estimation method itself, standard Cramér-Rao bounds considering separated sources cannot be applied.

<sup>2</sup>Note that some combinations will have low signal power  $\|\mathcal{X}\|_F^2$ , so that for a fixed SNR, the noise power  $\|\mathcal{N}\|_F^2$  will also be low.

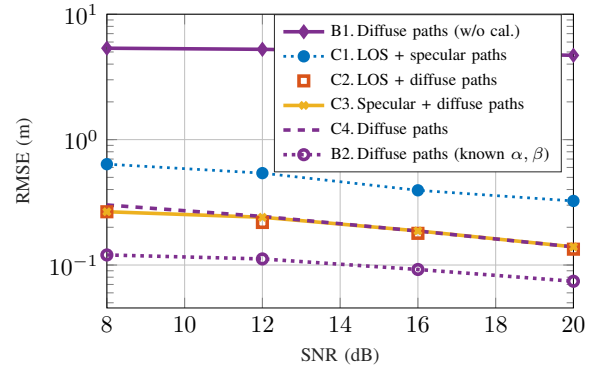


Fig. 1. UE positioning: RMSE versus SNR for different combinations of availability of the LOS path and specular components.

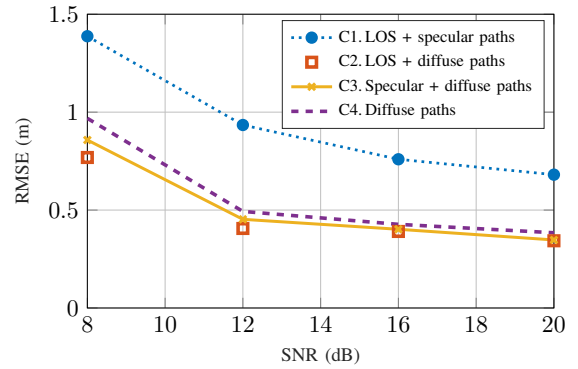


Fig. 2. UE clock bias estimation: RMSE versus SNR for different combinations of availability of the LOS path and specular components.

calibration, meaning that the UE assumes  $(\alpha, \beta) = (0, 0)$  and B2. with known orientation and clock bias  $(\alpha, \beta)$ . All variations use weights  $\zeta_k = 1$ . The largest positioning error occurs for benchmark algorithm B1. That is because the incorrect orientation  $\alpha$  and clock bias  $\beta$  is assumed in (10). Sub-meter accuracy is achievable by using LOS and two specular paths. The smallest positioning error occurs for B2, indicating the importance of knowledge of the clock bias and orientation. Among the four combinations C1–C4, the worst performance is obtained when the diffuse paths are ignored (C1). The combinations C2–C4 all yield similar RMSE, with C2 providing the best performance. Giving a larger weight to LOS and specular paths in (9) can provide additional gains, but was not explored in this letter.

2) *Synchronization and orientation estimation*: Fig. 2 shows the corresponding results for the clock bias (without the benchmarks, which are meaningless here), which largely follows the positioning performance. In terms of orientation estimation, Fig. 3, lower RMSE is achieved by utilizing the resolvable diffuse paths. Slightly improvements are observable by including the LOS and specular paths.

3) *Mapping*: Mapping performance at 20 dB SNR in terms of the projection onto the  $x$ - $y$  and  $x$ - $z$  planes is shown in Fig. 4. We observe relatively good performance for both surfaces. Both the location and shape of the surfaces can be recovered.

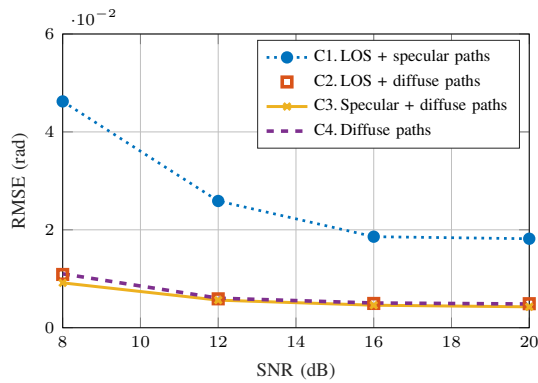


Fig. 3. UE orientation estimation: RMSE versus SNR for different combinations of availability of the LOS path and specular components.

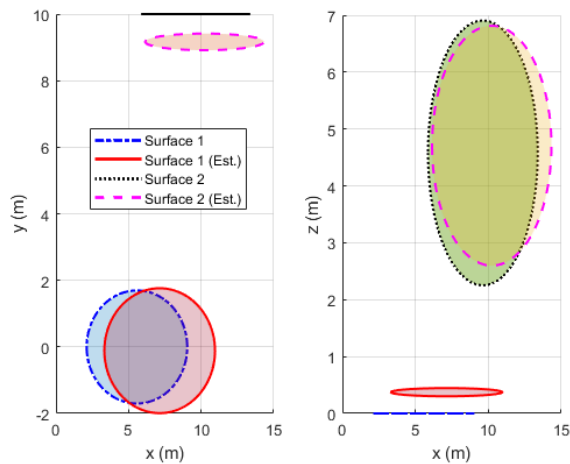


Fig. 4. Mapping results (projection onto the  $x$ - $y$  and  $x$ - $z$  planes), SNR = 20 dB, LOS is present, clock bias  $\beta c = 4\text{m}$  and orientation  $\alpha = \pi/3$  are unknown.

## V. CONCLUSIONS

We studied the problem of geometric parameter estimation in mmWave MIMO communications with diffuse scattering components, combined with UE orientation and clock bias estimation. We proposed a positioning and mapping method based on the estimated geometric channel parameters, and demonstrate that accurate UE positioning and propagation environment mapping is possible, even when the LOS path is blocked and specular components are absent, the reflecting surfaces are only characterized by diffuse scattering. Moreover, the method does not require identifying LOS or specular signal components. Modifications are needed for multi-bounce scenarios.

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