

A 100-Element HBT Grid Amplifier

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Abstract—A 100-element 10-GHz grid amplifier has been developed. The active devices in the grid are chips with heterojunction-bipolar-transistor (HBT) differential-pairs. The metal grid pattern was empirically designed to provide effective coupling between the HBT's and free space. Two independent measurements, one with focusing lenses, the other without, were used to characterize the grid. In each case, the peak gain was 10 dB at 10 GHz with a 3-dB bandwidth of 1 GHz. The input and output return loss were better than 15 dB at 10 GHz. The maximum output power was 450 mW, and the minimum noise figure was 7 dB. By varying the bias, a signal could be amplitude modulated with a modulation index as large as 0.65. Tests show that the grid was quite tolerant of failures—the output power dropped by only 1 dB when 10% of the inputs were detuned. The grid amplifier is a multi-mode device that amplifies beams of different shapes and angles. Beams with incidence angles up to 30° were amplified with less than a 3-dB drop in gain.

I. INTRODUCTION

QUASI-OPTICAL GRIDS offer the possibility of large-scale power combining of solid-state devices without the loss limitations of transmission-line combiners. A variety of grids have been demonstrated, including detectors [1], phase shifters [2], [3], frequency multipliers [4], [5], oscillators [6], [7], amplifiers [8], [9], mixers [10], and switches [11], [12]. The first grid amplifier [8] was a device with 25 pairs of MESFET's that amplifies a beam, with cross-polarized input and output (Fig. 1). This configuration helps to prevent the grid from oscillating, and allows polarizers to tune the input and the output independently. The transistors were wired as differential pairs, with the two sources tied together. The two gates were the inputs, and the two drains were the outputs. The grid showed a gain of 11 dB at 3.3 GHz. It had metal strips on the back for biasing, and resistors and pins to connect to packaged transistors on the front. The strips were

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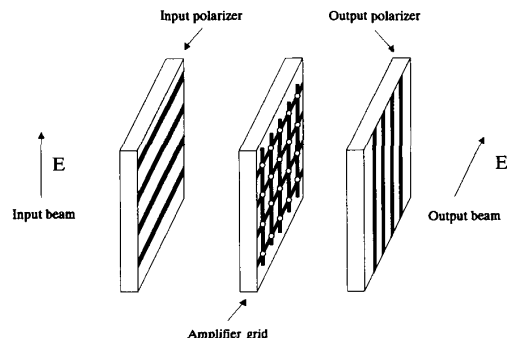


Fig. 1. A perspective view of a grid amplifier. The input beam is vertically polarized and the output beam is horizontally polarized. The metal strips on the grid couple the beam to the active devices, and radiate an amplified beam through the output polarizer. The position of the polarizers determines the input and output matching frequency.

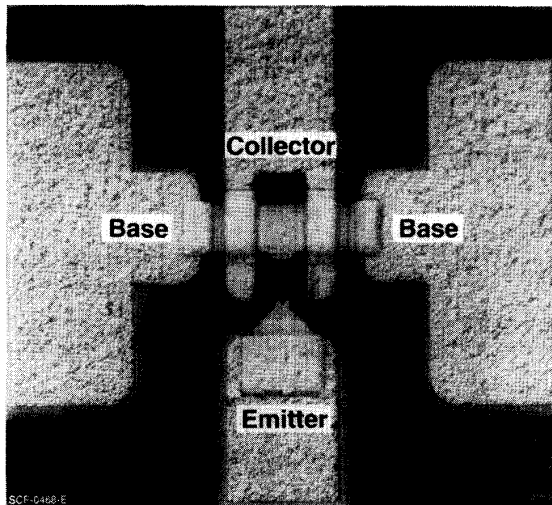
necessary for bias, but they also caused the grid to have a 3-dB bandwidth of only 3%. This configuration was also not a good candidate for future monolithic integration. Furthermore, the transistors were packaged devices. This forces the unit cell to be large, restricting operation to a relatively low frequency. More recently, a 16-element planar grid with custom differential-pair heterojunction-bipolar-transistor (HBT) chips was demonstrated, with a gain of 11 dB at 10 GHz [9]. However, this grid was small, little more than a wavelength across, and this made other measurements difficult. Here we report a much larger 100-element amplifier that is nearly three wavelengths across. We have made measurements of gain, input and output match, saturated power, noise figure, modulation, failure tolerance, and angled beams.

II. CONSTRUCTION

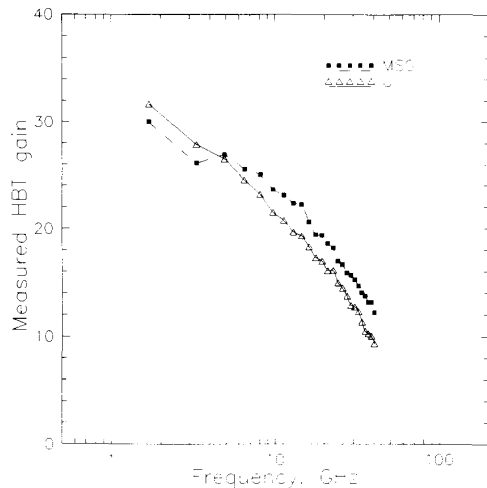
The AlGaAs/GaAs HBT's were fabricated by Rockwell International. The epitaxial layers were grown by MOCVD. Table I gives the details. Carbon and silicon are the p-type and n-type dopants. The transistors were made by a self-aligned dual lift-off process [13]. The emitter area is 40 μm^2 . The base resistance is estimated to be 10 Ω and the base-collector capacitance to be 35 fF. A single HBT (Fig. 2(a)), biased at $I_c = 20$ mA and $V_{ce} = 2.5$ V, had a dc common-emitter current gain, β , of 10. The common-emitter power gain, $|s_{21}|^2$, was measured by Cascade probe, and was 11 dB at

TABLE I
THE LAYERS IN THE $Al_xGa_{1-x}As/GaAs$ HBT'S (THESE WERE GROWN BY MOCVD)

Layer	Thickness, μm	Material	Doping, cm^{-3}	Content, x
Cap	0.15–0.25	n^+	$4-5 \times 10^{18}$	0.0
Emitter	0.07–0.12	n	$3-7 \times 10^{17}$	0.25
Base	0.05–0.10	p^+	$3-6 \times 10^{19}$	0.0
Collector	0.50–0.90	n	$3-8 \times 10^{16}$	0.0
Subcollector	0.60–0.90	n^+	$4-5 \times 10^{18}$	0.0



(a)



(b)

Fig. 2. (a) The layout of the single HBT used in device characterization measurements. There are two $10 \mu m \times 2 \mu m$ emitter fingers. (b) Maximum stable gain (MSG) and unilateral gain (U) versus frequency for this HBT.

10 GHz, with a unilateral gain of 18 dB (Fig. 2(b)). The cutoff frequency, f_t , was 65 GHz, and the maximum frequency of oscillation, f_{max} , was 90 GHz.

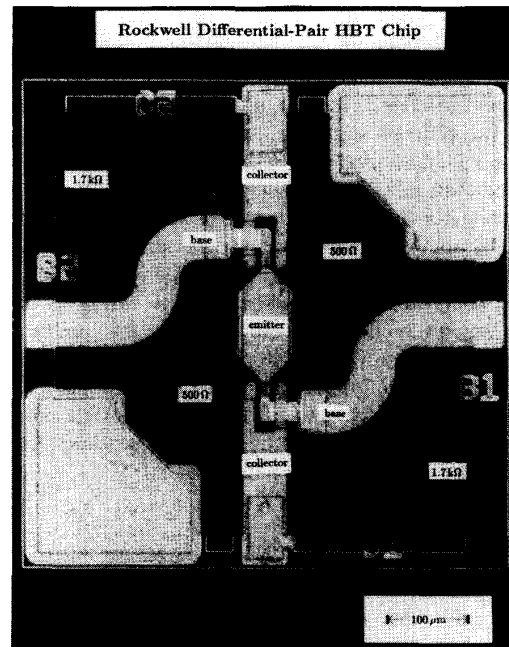


Fig. 3. The differential-pair HBT chip layout.

The differential-pair HBT chip used in the amplifier grid is shown in Fig. 3. The 1.7-k Ω resistors provide bias to the base, so there are only two external bias connections. They also provide negative feedback to help stabilize the grid. In addition, there are a pair of parallel 500- Ω emitter resistors to reduce the common-mode gain to prevent the grid from oscillating. The values of the resistors were chosen to provide a bias of $V_{ce} = 3$ V and $I_e = 11$ mA, assuming a β of 10. During the grid measurements, a bias of 5 V and 860 mA was applied to the entire 100-chip grid. This means that the average emitter current was only 4.3 mA, indicating that the chip β was less than half that of a single HBT. We do not know why the β 's are so different. All the devices came from the same wafer. The chips were passivated with silicon dioxide, but there was a drop in grid gain during the six-month period that the grids were being tested. This could be caused by device degradation or failure of the individual chips. In any event, we would expect the RF gain of the amplifier grid to be smaller than that of the single HBT chips.

The metal structure in the grid has two parts: RF coupling for the input and output, and bias for the HBT chips. Our goal was to put both on the same surface. For input and output coupling, inductive strips are attractive because they are strongly polarized, providing good isolation between the input and the output to prevent unwanted oscillations. Ideally, the bias lines should have a large reactance so as not to disturb the input and output beams. Various metal patterns were tested on smaller 4×4 grids [14]. Best results were obtained from the unit-cell pattern shown in Figure 4(a). This design was then adopted for the 10×10 grid shown in Fig. 4(b). Inductive strips couple the chips to the input and output beams, and 0.1-mm wide meander lines provide bias. A 0.1-mm wide capacitive gap is etched in the input strips to tune out inductance. To evaluate the behavior of the meander lines, two different structures, each containing a narrow metal strip in a 2-mm square TEM waveguide were examined on the Hewlett-Packard High Frequency Structure Simulator (Fig. 5). The meander line had an inductive reactance of 100Ω at 10 GHz, compared with 50Ω for the straight strip. Similar ratios were obtained on different size waveguides [14].

The completed grid amplifier is shown in Fig. 6. Initially there was an oscillation at 10 GHz, but this problem was solved by adding a Duroid substrate with a dielectric constant of 10.5 behind the grid. There is also an additional dielectric slab at the output for tuning. The positions of the polarizers were carefully adjusted to produce the largest amplifier gain at 10 GHz.

III. GAIN AND RETURN LOSS

The grid gain, and input and output return loss, were measured by a quasi-optical network analyzer with focusing lenses [15]. The measurement setup includes an HP8510B network analyzer, two feed horns, and two teflon lenses (Fig. 7). The lenses have a diameter of 30 cm, and focus the beam at a point 46 cm from the lens. At 10 GHz the beam-waist diameter is 10 cm. In order to measure the amplifier gain, the system was first calibrated for transmission loss using an absorber screen with a square hole, 8 cm on a side to match the amplifier grid (Fig. 7(a)). This absorber intercepts about half of the power in the focused beam. After the calibration, the amplifier grid was inserted, and the receiving horn was rotated 90° to match the amplified beam polarization (Fig. 7(b)). The absorber was not required around the amplifier grid because the transmitting horn and the receiving horn were cross-polarized. The results show that the peak gain was 10 dB at 10 GHz with a 3-dB bandwidth of 1 GHz (Fig. 8). The peak could be shifted from 8 GHz to 11 GHz by adjusting the polarizers. With no bias, the gain dropped below -8 dB everywhere.

A similar arrangement with one horn and one lens served as a reflectometer to measure input and output return loss. The calibration standards were an absorber load, a metal short, and a 1-cm offset short. The results in Fig. 9 indicate that both the input and the output return loss were better than 15 dB at 10 GHz. The output match is narrower than the input match.

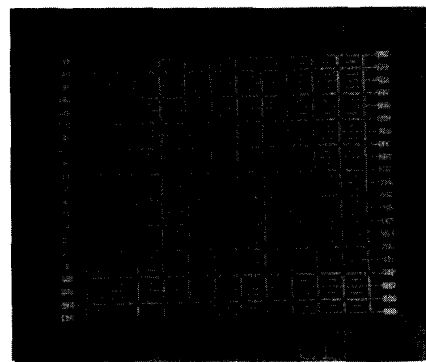
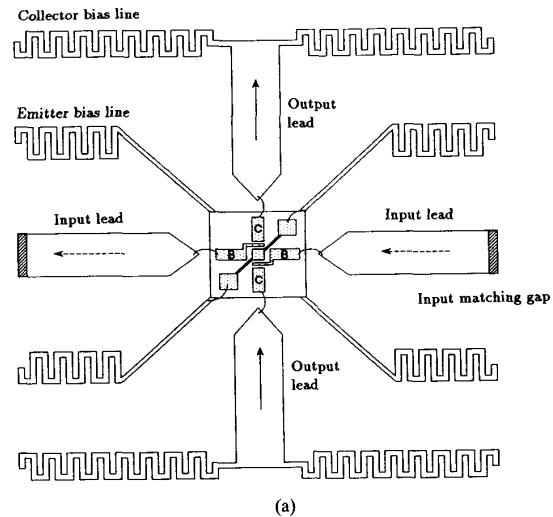


Fig. 4. (a) Grid-amplifier unit-cell design. The arrows indicate the direction of current flow. The unit cell size is 8 mm. The radiating leads are 0.8 mm wide and the meandering bias lines are 0.1 mm wide. The span of the meander lines is 0.6 mm from top to bottom with 0.1-mm gaps. The input matching gap is 0.1 mm wide. (b) Photograph of the 100-element grid amplifier.

Possibly this is because the output beam must pass through the high-dielectric constant Duroid slab under the grid.

One can also measure the amplifier gain in the far field without lenses with the setup in Fig. 10 [8]. The gain G can be expressed in terms of the ratio of the calibration power, P_c , measured in (a), and the power received from the grid amplifier, P_r , measured in (b), as

$$G = \frac{P_r}{P_c} \left(\frac{\lambda r}{2A} \right)^2 \quad (1)$$

where λ is the free-space wavelength and r is the distance between the grid and each of the horns (90 cm). A is the geometric area of the grid, 64 cm^2 . The results were almost identical to the previous measurements using lenses, showing a peak gain of 10 dB at 10 GHz with a 3-dB bandwidth of 1 GHz.

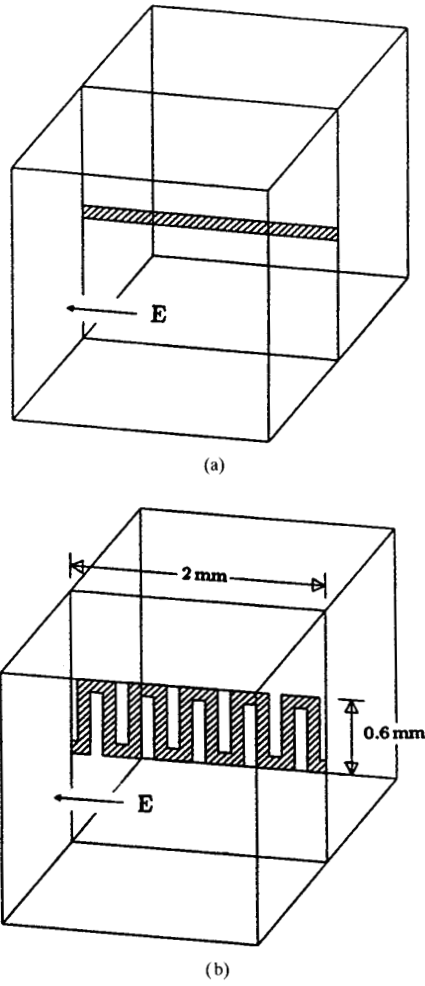


Fig. 5. High-Frequency Structure Simulator bias-line models in 2-mm TEM waveguide. (a) A straight strip. (b) A meander line. The sides of the waveguides are electric walls, and the top and bottom are magnetic walls, where the tangential component of the magnetic field goes to zero. The strips sit on a dielectric with $\epsilon_r = 2.2$. The results show that between 7 GHz and 13 GHz, the inductance of the meander lines is 1.6 nH, compared with only 0.8 nH for the straight strip [14].

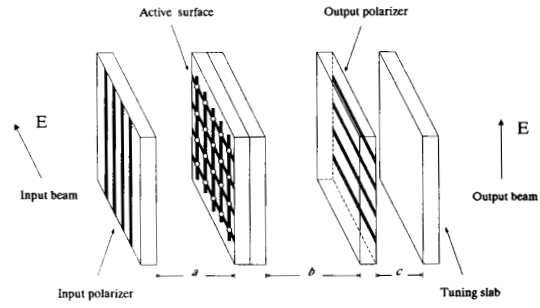
IV. POWER SATURATION

In the far-field setup above, the incident beam has a uniform phase and amplitude, suitable for measuring power saturation. We need to know the gain of the transmitting and receiving horns, G_t and G_r . These gains were assumed to be identical, and the setup in Fig. 10(a) was used to calculate the horn gain as

$$G_t = G_r = \sqrt{\frac{P_c}{P_t}} \left(\frac{4\pi r}{\lambda} \right) \quad (2)$$

where P_t is the transmitted power. We can write the input power to the grid, P_i , as

$$P_i = P_t \left(\frac{G_t A}{4\pi r^2} \right). \quad (3)$$



	dielectric constant	Physical length, mm	Electrical length, 10 GHz
a	1	14	168°
b	1	15	180°
c	1	10	120°
□	10.5	3.81	148°
□	2.2	3.18	57°

Fig. 6. View of the assembled grid amplifier. The table shows the slab thicknesses and optimum spacings for maximum gain at 10 GHz.

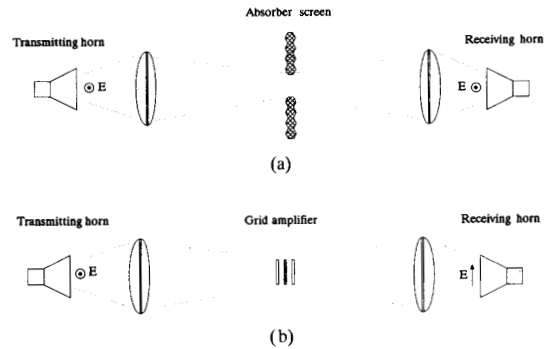


Fig. 7. Quasi-optical gain measurements with focusing lenses. (a) Transmission loss calibration. (b) Amplifier gain measurement.

We can write a related expression for the output power, P_o , as

$$P_o = P_r \left(\frac{4\pi r^2}{G_r A} \right). \quad (4)$$

Fig. 11(a) shows the output power at 10 GHz, with the polarizers and slabs in the same positions as before. At a 5-V bias, the 1-dB compression point was 105 mW and the maximum output power was 450 mW. The maximum power-added-efficiency was 5%, at an output power level of 330 mW. The dc power supplied to the grid was 4.3 W. We estimate that half the power was consumed in the base and emitter resistors, indicating that an active bias network that avoids this loss would help. The maximum output power decreased sharply as the frequency was changed from 10 GHz (Figure 11(b)). The peak in output power comes at the same frequency where the output was matched.

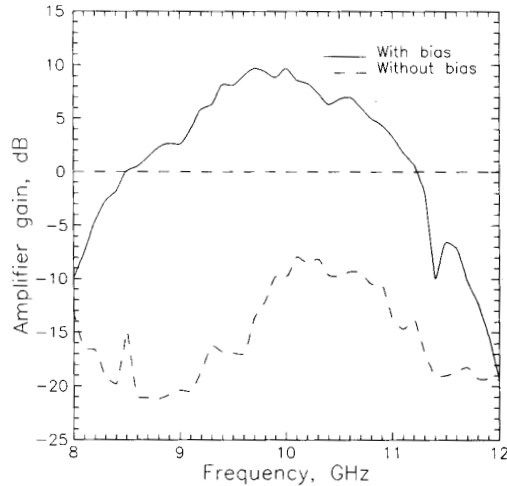


Fig. 8. Grid-amplifier gain versus frequency. The peak is 10 dB at 10 GHz. The 3-dB gain bandwidth is 1 GHz.

V. NOISE-FIGURE

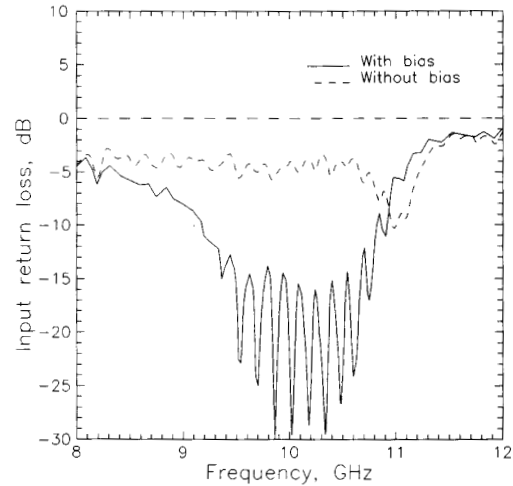
The far-field setup can also be used to measure the grid noise figure if the transmitting signal generator is replaced by a noise source, and the receiving power meter is replaced by a noise-figure meter. A noise diode with a high excess noise ratio (ENR) is required. We used a Noise-Com NC3206 diode, which has an ENR of 36 dB. In the measurements, there is a noise contribution from background radiation, and a calibration measurement is made using the setup in Fig. 10(a) to correct for this. The antenna temperature at the receiving horn, T_c , can be expressed as a contribution from the noise source, with temperature T_t , and the effective background temperature T_b ,

$$T_c = L_c T_t + (1 - L_c) T_b \quad (5)$$

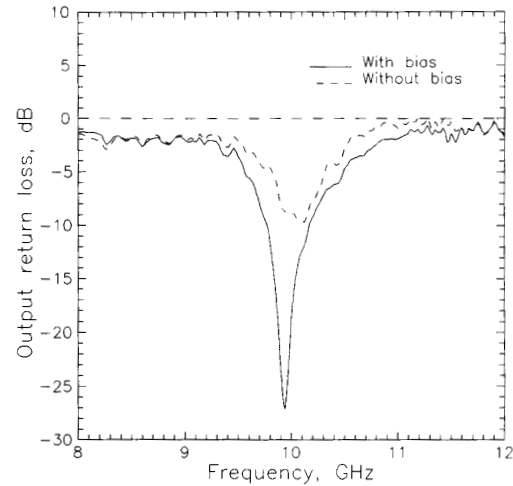
where L_c is the space-loss factor $G_t G_r (\lambda / 4\pi 2r)^2$. The noise contributed by the horns themselves is neglected. From the meter measurements, we can invert this formula to find T_b . The results, shown in Fig. 12(a), indicate that the room background varied between 250 K and 380 K. To measure the noise temperature of the grid, we use the arrangement in Fig. 10(b). The temperature of the receiving horn, T_r , is given in terms of T_t , T_b , and the noise temperature of the grid T as

$$T_r = GLT + GL^2 T_t + (1 - L)(GL + 1) T_b \quad (6)$$

where G is the grid gain, and L is the space-loss factor $G_t A / (4\pi r^2) = G_r A / (4\pi r^2)$. From the measurements, this formula can be inverted to find T . The results, converted to noise figure using a reference temperature $T_0 = 290$ K, are plotted in Fig. 12(b). The best noise figure at 5-V bias was 7 dB. When the bias was lowered to 4 V, the noise figure improved to 6 dB, but the gain also dropped by 1 dB. For comparison, an optimized single HBT transistor circuit gave a noise figure of 4 dB [16]. In our measurements, the grid noise and the background noise were comparable, and we feel this limits the accuracy of the measurements to only ± 1 dB. For future low-noise grids based on HEMT amplifiers, it would



(a)



(b)

Fig. 9. (a) Input and (b) output return loss. The ripple in the input plot indicates that some reflected component was not accurately corrected for.

be better to measure noise figure with a cold background such as the sky.

VI. AMPLITUDE MODULATION

The grid gain varies with bias, and this can be used for amplitude modulation. In Fig. 13(a), we plot the square root of the power gain G —the field transfer coefficient, $|s_{21}|$ —as a function of the bias voltage. Near 2 V, we can write a linear approximation for this curve as

$$|s_{21}| = 1.16(1 + 0.82v) \quad (7)$$

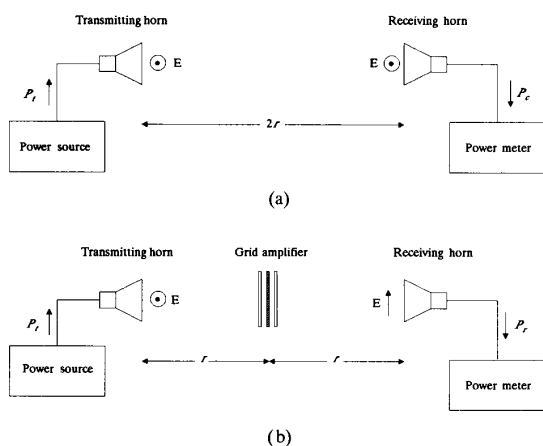


Fig. 10. Quasi-optical gain measurements in the far field. (a) Transmission loss calibration. (b) Amplifier gain measurement.

where v is the voltage offset from 2 V. We can write an amplitude-modulated signal $x(t)$ in the form

$$x(t) = A[1 + m \cos(\omega_m t)] \cos(\omega t) \quad (8)$$

where m is the modulation index and ω_m is the modulation frequency. If we compare these two equations, we can see that the modulation index m should be given by $m = 0.82v$, if we consider v to be the peak amplitude of the modulating signal. Fig. 13(b) compares measurements of m with this prediction. At low modulation indexes, theory and experiment agree, but as m approaches 0.5, the points diverge. Also, additional sidebands begin to appear in the output spectrum [14].

VII. RELIABILITY

A key issue in any system is how it responds to failure. Previously, a failure test was performed on a grid oscillator with 36 transistors by physically removing transistors from the grid [17]. The output power dropped quickly, by 2 dB per transistor. However, it is not clear how these results apply to grid amplifiers. Intuitively, we might expect each device to contribute equally to the radiated field, and the effect of a particular failure rate should show up as a corresponding drop in the radiated field. Thus a 10% failure rate would cause a 10% drop in the output field, and a 1-dB drop in output power.

Bias is another reliability issue. If all the devices are biased in parallel, a short brings down the entire grid. In principle, this can be avoided by fusing individual bias lines. This problem did not occur during the six-month testing period. A number of devices failed open and the only effect was a small drop in gain. As a practical matter, bias failures in an HBT grid can be detected with an infrared viewer. When an HBT chip is properly biased, minority carriers recombine in the base, producing infrared radiation. This allows us to replace chips that are not biased, although it does not guarantee that all the chips are working.

To study failures, we detuned some of the base inputs by closing the input matching gaps with bond wires. These

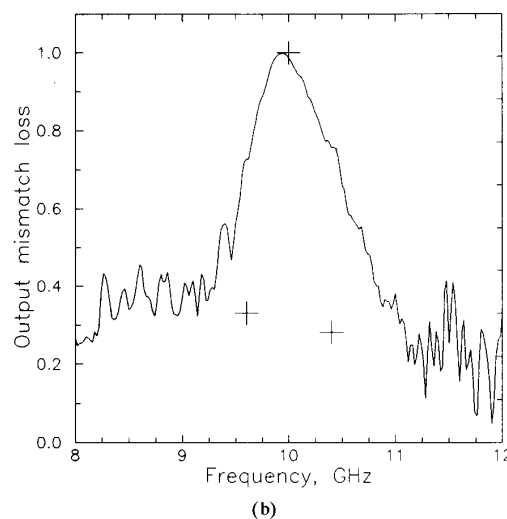
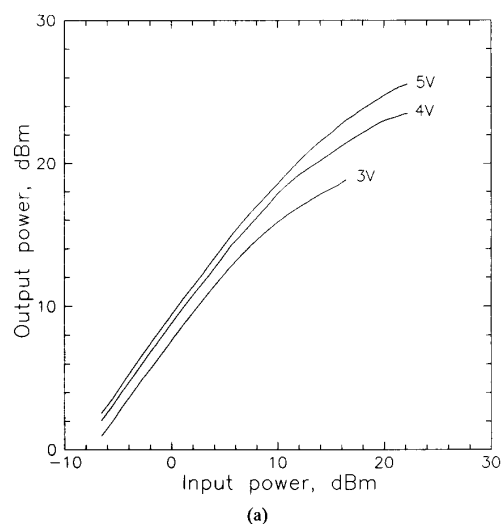
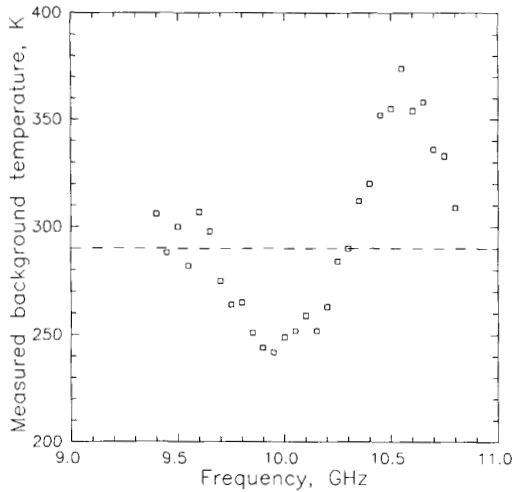
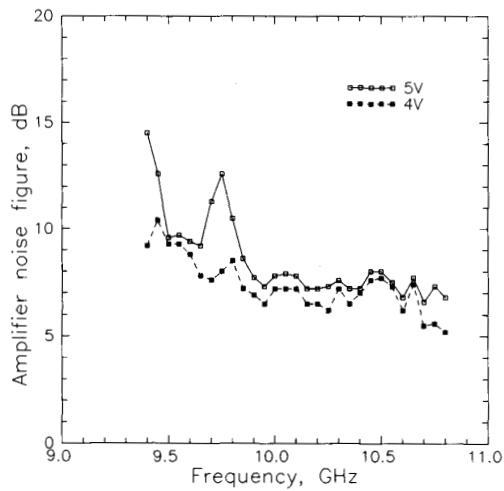


Fig. 11. Power saturation measurements. (a) Output power at 10 GHz plotted against input power, for three different grid bias voltages. (b) Output mismatch loss factor, $1 - |s_{22}|^2$, plotted against frequency. For comparison, the maximum output power, measured at three different frequencies, is also plotted, normalized to the same scale. The grid bias voltage in each case was 5 V.

input matching gaps are 0.1 mm wide, and provide series capacitance for tuning out the inductance of the base lead (see Fig. 4(a)). Each bond wire detunes 2 of the 200 base circuits, so that we can produce a 10% failure rate by adding 10 bond wires. The bond wires were placed uniformly across the grid. The bonds did not result in any spurious oscillations. Fig. 14 shows the effect on the gain. At the normal bias voltage of 5 V, the gain dropped 1 dB with a 10% failure rate. With a 25% failure rate, the drop was 5 dB, and at 50%, the gain fell all the way to the normal zero-bias gain.



(a)



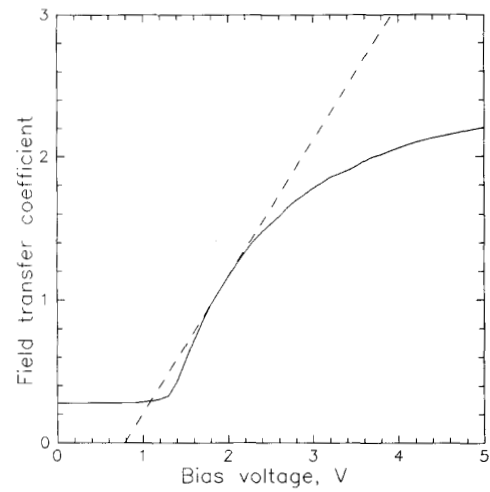
(b)

Fig. 12. (a) Effective background temperature T_b . (b) Grid noise figure at two different bias voltages.

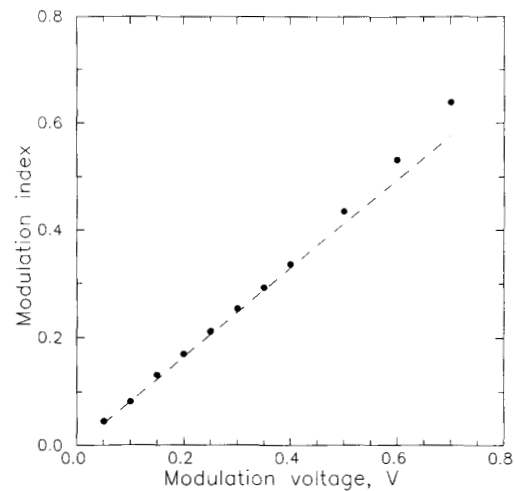
VIII. BEAM PATTERNS

The grid amplifier is nearly three wavelengths across, and we would expect that if the phase and amplitude of the input beam vary across the grid, then the phase and amplitude of the output beam would vary in the same way. Diverging input beams should produce diverging output beams and the angle of a beam should be preserved as it is amplified. Practically, this means that beams can be formed in a transmitter at a low-power level with a particular direction, width and sidelobe level, and then amplified.

To test this idea we used a small 8-transistor HEMT grid oscillator as a source. Its H-plane pattern is shown in Fig. 15(a) as a solid line. The oscillator was then moved back 5 cm (1.6λ) to allow the grid amplifier to be inserted. The pattern of the amplified beam (this is the E-plane pattern because



(a)



(b)

Fig. 13. Amplitude modulation by changing the grid bias. (a) The field transfer coefficient $|s_{21}|$, plotted on a linear scale. The dashed line is a linear approximation of the curve near 2 V, given by $|s_{21}| = 1.16(1 + 0.82v)$. This measurement was made several months after the first measurements, and the gain has dropped. (b) Modulation index m as a function of the peak amplitude v of the modulating signal. The bias was 2 V. The circles are the measured values, and the dashed line is the prediction $m = 0.82v$.

the grid changes the polarization) is shown as a dashed line in Fig. 15(a). Both patterns have relatively wide beams, with the amplified beam being somewhat narrower. The amplifier increased the peak power density by 15 dB. Next the oscillator grid was moved back until the two grids were separated by 34 cm (11.4λ). This amplified beam is the solid line in Fig. 15(b). The beam is narrower, because the input phase and amplitude are now nearly uniform. In this case the beamwidth is diffraction limited by the grid amplifier. This idea is supported by close agreement with a theoretical pattern calculated for a uniform array of 10 elementary dipoles 8 mm apart (the dashed line in Fig. 15(b)).

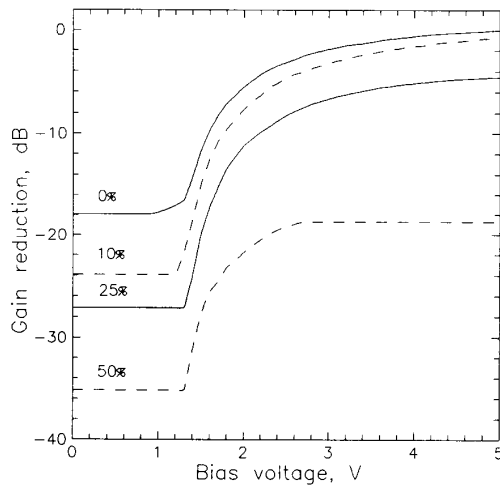
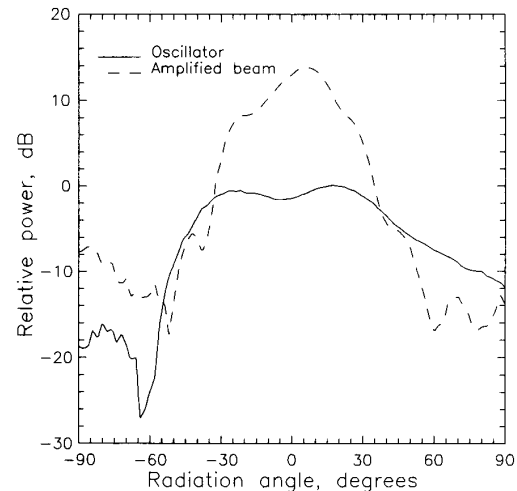


Fig. 14. Closing the input matching gaps with bond wires. The plot shows the measured gain at 10 GHz as a function of the bias voltage, normalized to the gain at 5-V bias. A 10% failure rate results in a gain drop of 1 dB.

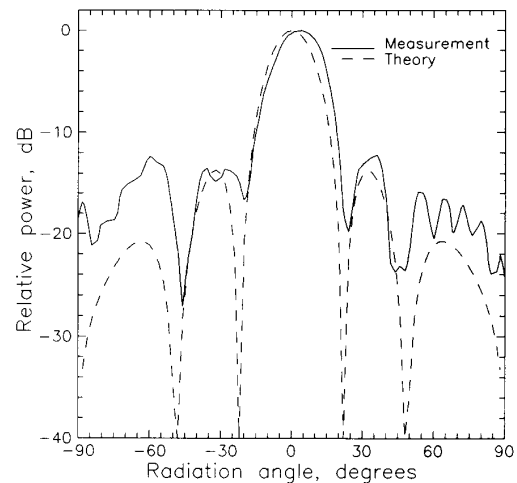
We also tested the amplifier with beams incident at different angles. Fig. 16(a) shows the patterns for incidence at 0° , $+20^\circ$, and -20° . The peaks in the output beams are within 1° of the incident angles. The beams are all of similar width, and the sidelobes are all at about the 13-dB level that we would expect for a uniformly illuminated aperture. In another test, we started with the far-field arrangement in Fig. 10(b), and rotated the grid amplifier. This measures the change in gain for different angles of incidence. The gain drops less than 3 dB for angles of incidence less than 30° . Presumably the primary cause of this drop in gain at extreme angles is changing beam impedance. However, part of the loss is due to the fact that less power is being intercepted by the grid at oblique angles. This obliquity factor shows up in both transmitting and receiving space-loss factors, so we expect a $\cos^2 \theta$ loss (1.2 dB at 30°) in addition to the drop caused by changing impedances. We can avoid this obliquity loss in applications where grid can be made larger than the beam.

IX. CONCLUSION

We have presented a 100-element HBT grid amplifier with a gain of 10 dB at 10 GHz, a 10% 3-dB bandwidth, and an input and output match better than 15 dB. At a 5-V bias, the maximum output power is 450 mW and the minimum noise figure is 7 dB. These results are consistent with the idea that the gain, bandwidth, input and output match, and noise figure are comparable to single-transistor amplifiers, but that power scales with the size of the grid. The grid degrades gracefully—10% failures produce only a 1-dB drop in gain. This means that grid amplifier could be much more reliable than a single high-power solid-state device or vacuum tube. A grid amplifier is a multi-mode device that preserves the propagation angles of beams. It amplifies at incident angles



(a)



(b)

Fig. 15. Amplifying the beam of a small 10-GHz grid oscillator with a grid amplifier. (a) H-plane pattern for the oscillator grid (solid line), and the E-plane pattern for the amplified beam (dashed line). The distance between the two grids was 1.6λ . Notice that both the grid-oscillator beam and the grid-amplifier beam are broad. (b) Spacing increased to 11.4λ . The solid line is the E-plane pattern of the amplified beam, now narrowed because the input phase and amplitude are uniform. The dashed line shows the theoretical pattern of a uniform array of 10 elementary dipoles 8 mm apart.

up to 30° with less than a 3-dB loss in gain. This means that a grid amplifier could amplify a beam for an electronic beam steerer, easing the loss requirements for the steering system. Recently a monolithic grid oscillator has been demonstrated at 35 GHz [18]. This grid-amplifier design is also suitable for monolithic integration at millimeter wavelengths.

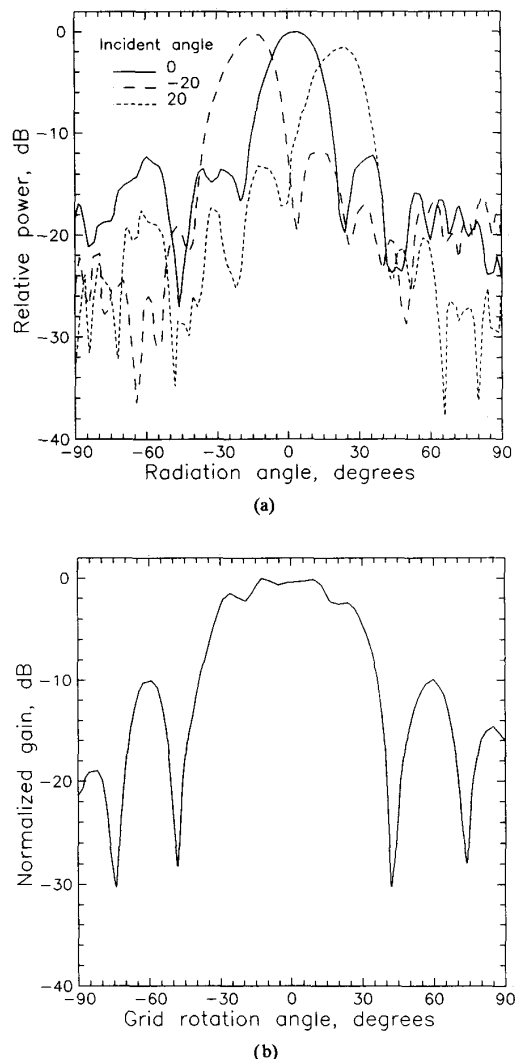
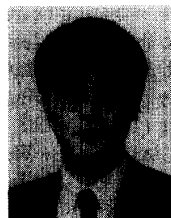


Fig. 16. Amplifying beams at angles. (a) The grid-amplifier radiation patterns for three different incident beams (b) Gain variation with incidence angle.

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David B. Rutledge, (M'75-SM'89-F'93) for a photograph and biography, see this issue, pp. 1662.