



# Article A Cost-Effective Solution for Non-Convex Economic Load Dispatch Problems in Power Systems Using Slime Mould Algorithm

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**Abstract:** Slime Mould Algorithm (SMA) is a newly designed meat-heuristic search that mimics the nature of slime mould during the oscillation phase. This is demonstrated in a unique mathematical formulation that utilizes adjustable weights to influence the sequence of both negative and positive propagation waves to develop a method to link food supply with intensive exploration capacity and exploitation affinity. The study shows the usage of the SM algorithm to solve a non-convex and cost-effective Load Dispatch Problem (ELD) in an electric power system. The effectiveness of SMA is investigated for single area economic load dispatch on large-, medium-, and small-scale power systems, with 3-, 5-, 6-, 10-, 13-, 15-, 20-, 38-, and 40-unit test systems, and the results are substantiated by finding the difference between other well-known meta-heuristic algorithms. The SMA is more efficient than other standard, heuristic, and meta-heuristic search strategies in granting extremely ambitious outputs according to the comparison records.

Keywords: economic load dispatch; non-convex; slime mould algorithm; with and without valve-point effect

### 1. Introduction

In the actual functioning of power systems, Economic Load Dispatch (ELD) is a crucial problem to solve. The role of the power system is to deliver continuous power to the consumers at affordable price which is its main important feature [1,2]. The objective is to reduce energy-generating costs while fulfilling load needs and ensuring equality and inequality constraints. This fact results in a higher degree of pollution awareness in thermal plants, as well as a lower cost of diagnosing the problem. Because they operate in conjunction with a collection of viable alternatives, evolutionary methods are now perfectly suited for discovering answers to optimization problems. All optimization approaches, including evolutionary ones, are known to be influenced by constraints [3], since the traditional procedure of an evolutionary approach by employing operators for individuals in a population may violate the constraints rules. The way evolutionary approaches deal with constraint rules of challenges is a significant aspect that is directly connected to the



Citation: Kamboj, V.K.; Kumari, C.L.; Bath, S.K.; Prashar, D.; Rashid, M.; Alshamrani, S.S.; AlGhamdi, A.S. A Cost-Effective Solution for Non-Convex Economic Load Dispatch Problems in Power Systems Using Slime Mould Algorithm. *Sustainability* 2022, *14*, 2586. https://doi.org/10.3390/su14052586

Academic Editors: Maryam Bahramipanah and Zagros Shahooei

Received: 9 December 2021 Accepted: 16 February 2022 Published: 23 February 2022

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**Copyright:** © 2022 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). quality of solutions created for such problems. By converting the present solution that opposes the constraints into a viable one, a redesigned method eliminates unattainable solutions. In every step of the evolutionary method, the number of better individuals grows as a result.

Wind, solar, thermal, nuclear, renewable, hydro, and other power producing facilities are used in most power generation systems. It is known that nuclear power plants are controlled at stable power outputs. In the case of renewable energy systems, the operational cost will not change as much as the production. In thermal systems, however, the running cost varies with the total power output. As a result, the economic load dispatch issue, which includes the use of thermal systems as generators, is considered a critical optimization issue in electric power systems. Maintaining an economical operation is a difficult challenge for both traditional and smart grid systems. When power systems are exposed to operational and transmission imperatives, the economic load dispatch limit the optimal outcome for an electric power generation to sustain the load demand with minimum generation price. The economic load dispatch problem is usually solved by sophisticated computerized approaches that meet the operational and power system imperatives via minute-to-minute monitoring. A little increase in economic load dispatch demonstrates its long-term reaction to the declining price of total power output. As a result, a variety of optimization methods have been developed to address cost-effective load dispatch issues while producing high-quality results. Traditional optimization approaches were the sole option to address economic load dispatch concerns for many years. Because of the limitations of conventional methods, system operators have a chance to fail to notice the realistic and technological imperatives of the system's units. There are two types of simplifications in this category. First, combined with the accuracy of the generating unit's pricing model, particularly for different types of fuels or taking the valve-point loading impact into account [4], multivalve steam turbines are widely seen in real-world generating units. The valve point of the generating unit is drawn when the steam turbine's intake valve opens abruptly, pushing the energy consumption curve upward. This phenomenon is known as the "valve-point effect". The sine term must be overlaid on the fuel cost function due to the valve-point effects' discontinuity and high-order nonlinearity of input and output characteristics. Therefore, it is necessary to analyze the fuel curve and cost function for power generation with the valve-point effect. The other is related to network topology and is only concerned with reducing transmission system loss [5].

The main contributions of this work are as follows:

- The slime mould algorithm is implemented as it has great global search capability.
- The SM algorithm is used to solve a non-convex and cost-effective load dispatch problem (ELD) in an electric power system.
- The efficiency of the algorithm is tested on standard IEEE test systems.
- The method is evaluated on nine different test systems with and without valve-point loading effects.

The remaining sections of this article are structured as follows: Section 2 consists of the literature survey; mathematical formulation for single area economic load dispatch is provided in Section 3; concepts of the slime mould algorithm and its economic load dispatch flow chart are provided in Sections 4 and 5, respectively. Section 6 contains results and discussions, and the conclusion is given in Section 7.

#### 2. Literature Survey

The economic load dispatch problem is a major concern for the cost-effective operation of electric power systems, as it concentrates on basically assembling the power outputs of the units by establishing time intervals in order to decrease generating costs while still meeting other system requirements. In general, the traditional economic load dispatch problem is reduced in order to solve the convex quadratic programming problem [6], which may now be handled effectively using MOSEK [7]. Furthermore, the system becomes nonsmooth, non-convex, and non-continuous when the valve-point loading effect, transmission loss, and prohibited operating zones are taken into account. The objective function arises as multiples of the local minimum as a result of these features, making global minima exceedingly difficult to attain. Aside from that, the non-smooth nature of the function makes the derivate-based mathematical programming technique challenging to apply directly.

Traditional optimization techniques often look at linear, piecewise linear, and price functions of generators in quadratic functions, with only network loss being considered. These classic techniques include Lambda Iteration [8], Gradient Descent Method [9], Linear Programming [10], Newton's Technique [11], Dynamic Programming [12], Gradient search [13], and the Lagrangian Relaxation Algorithm [14]. Because of the persistence of severe nonlinear characteristics in real-world practical networks, such as the use of more fuel, nonlinearity in power flow, prohibited operating zones, and valve-point loading effects, traditional techniques are being harmed by oscillatory issues which lengthen the solution time for large systems [15]. As a result, while dealing with high-dimensional economic dispatch difficulties, these suffer from disadvantages such as failure to meet imperatives and lengthy time calculations.

This time-consuming calculation in optimization methods prompted researchers to develop meta-heuristic optimization strategies to solve large-scale problems. The meta-heuristics method in [16] takes into consideration non-convex pricing functions and non-smooth operating functions as well as other imperatives. This includes techniques such as Synergic Predator-Prey Optimization (SPPO) [17], Seeker Optimization Algorithm (SOA) [18], Genetic Algorithm (GA) [19,20], Evolutionary Programming (EP) [21], Firefly Algorithm (FA) [22], Particle Swarm Optimization (PSO) [23–25], Artificial Bee Colony (ABC) [26], Colonial Competitive Differential Algorithm (ITS) [29], Ant Colony Optimization (ACO) [30], Group Search Optimizer (GSO) [31], Harmony Search Algorithm (HAS) [32], Biogeography Based Optimization (BBO) [33], and Differential Evolution (DE) [34].

Heuristic techniques, which are known for their adaptability and flexibility, have received a lot of attention in recent years for solving a range of real-time economic load dispatch issues. Such techniques include Orthogonal Learning Competitive Swarm Optimizer(OLCSO) [35], Water Cycle Algorithm (WCA) [36], Moth Flame Optimizer (MFO) [37], Opposition-Based Krill Herd Algorithm (OKHA) [38], Two-Stage Artificial Bee Colony (TSABC) [39], Modified Crow Search Algorithm (MCS) [40], Chaotic Improved Harmony Search Algorithm (CIHSA) [41], Improved Fireworks Algorithm with Chaotic Sequence Operator (IFWA-CSO) [42], Exchange Market Algorithm (EMA) [43], Distance-Based Firefly Algorithm (DFA) [44], Root Tree Optimization Algorithm (RTO) [45], Backtracking Search Algorithm (BSA) [46], Adaptive Charged System Search Algorithm (ACSS), Ant Lion optimizer (ALO) [47], Grey Wolf Optimization (GWO) [48], Improved Differential Evolution (IDE) [49], Improved Bird Swarm Algorithm (IBSA) [50], Chaotic Bat Algorithm (CBA) [51], Particle Swarm Optimization (PSO) [52,53], Island Bat Algorithm (IBA) [54], Dual-Population Adaptive Differential Evolution (DPADE) [55], and Chaotic Teaching-Learning-Based Optimization (CTLBO) [56], which are used to solve economic load dispatch problems. To summarize, the Artificial Cooperative Search Algorithm (ACS) [57] was recently proposed on the basis of a co-evolution method that may find an optimal solution for the problematical economic load dispatch issue with a high degree of probability. Offering economic load dispatch with valve-point loading impact [58] evolves the requisite condition for the local minimum. A Traverse Search Method (TSM) was presented for addressing economic load dispatch with valve-point loading effect by taking into account such an important state. A method called Dimensional Steepest Decline Technique (DSD), which employs the decline rate series of fuel cost, was proposed in [58] to search efficiently for optimum solutions based on prior local minima data. Few articles have focused on combining two or more ways to solve the issue of economic load dispatch in order to improve the strategies' performance.

Furthermore, to meet the greater complexity of economic dispatch problems in practice, two or more techniques have been pooled to produce a hybrid methodology. This technique combines two or more traditional methods with any meta-heuristic optimizer. The newly designed hybrid optimizers include Bee Colony Optimization joined with Sequential Quadratic Programming (BCO-SQP) [59], Interior Point Method (IPM) integrated with Differential Evolution (DE) [60], mixed Differential Evolution with Biogeography-Based Optimization (DE-BBO) [61], Particle Swarm Optimizer-Sequential Quadratic Programming (PSO-SQP) [62], combined Active Power Optimization with Genetic Algorithm (GA-APO) [63], Chaotic Self-adaptive Particle Swarm Optimization [64], and Modified Sub-Gradient integrated with Harmony Search (MSG-HS) [65].

Their stochastic character, on the other hand, leads to a few drawbacks that many heuristics-based approaches suffer from. The choice of parameters, for example, is crucial for these techniques to function, and they need a lot of individual research to get an acceptable result.

The optimization approaches, on the other hand, are difficult to master, and the solutions obtained in each run are similar. As a result, unlike stochastic searching approaches, these strategies must be conducted just once. As a result, these approaches have recently received a lot of attention. Mixed Integer Quadratic Programming (MIQP) was developed to linearize the cost function induced by valve-point effects, according to [66]. Three approaches to find a solution for dynamic economic dispatch (DED) were incorporated in [11] based on this MIQP method: Multistep Method, Warm Start Method, and Range Restriction Format. The complete generating price function was recovered by its linear nearness to solve Dynamic Economic Load Dispatch (DED), and then a combination approach was included with Mixed Integer Linear Programming and Interior Point Technique in [67]. In [68], the economic dispatch problem was rebuilt using the Quadratically Constrained Quadratic Programming (QCQP) form, resulting in the Semi-Definite Programming (SDP) technique. This problem may be addressed iteratively using the Convex Iteration Method and the Branch and Bound approach. To address the economic dispatch issue, which included transmission loss and prohibited operating zones, [69] suggested a method called A Bi-level Branch and Bound approach (BB) in combination with Mixed Integer Quadratically Constrained Quadratic Programming. A fresh Big-M approach based on the MIQP strategy was proposed in the publication [70]. In [71], R.A. Jabr proposed the Semi definite Programming (SDP) technique.

In the paper [72], the authors focused on solving economic dispatch problems with penetration of wind energy sources. Peng et al. in [73] discussed the combined scheduling problem with due consideration of other renewable energy sources. The paper [74] provided a comprehensive review on different optimization methods available to find solutions for a combined economic emission dispatch problem. Liaquat et al. [75] made a comprehensive literature review on several developed optimization techniques and discussed the nature of the objective functions engaged in various dispatch problems. Tapas et al. [76] listed different techniques which were suggested by various authors for combined economic operation and environmental impact. B. Y. Qu et al. [77] in his literature survey covered the topics of typical MOEAs, classical EED problems, Dynamic EED problems which incorporated wind power, EED problems which incorporated electric vehicles, and EED problems within microgrids. Liaquat et al. [78] suggested the firefly method which succeeded fruitfully in solving a highly non-linear and multi-modal dispatch problem by assigning the optimum power sharing for every energy source in different scheduling time limits. Nazari-Heris et al. [79] explained the interconnection of gas, water, and power generation systems initially and then presented the mathematical formulation in a later stage and listed its advantages.

When utilizing these various meta-heuristic approaches, the primary faults at an idle are particularly aware for the initial value of the control parameters. While combining optimizers yields acceptable results, identifying the optimal point of inclusion between two meta-heuristics is challenging. Furthermore, hybrid systems' intrinsic complexity demands a non-eligible rise in the amount of work necessary to appropriately manage the control parameters. To address the issue of economic load dispatch, the following are the primary contributions of this article which are based on a few limitations pointed in this section: firstly, it analyses the objective functions implicated in each problem and considers different types of constraints and goal functions. Secondly, it goes through the nature of the objective function that each dispatch problem involves and highlights the most important decision variables and suggests ways to update the situation. Lastly, it provides suggestions on how to enhance the present forms of common ED issues. Thus, this study proposes a new meta-heuristic method called the Slime Mould Optimization (SMA). Slime mould behavior is replicated using a unique meta-heuristics Slime mould method [80–82]. This approach includes a number of techniques that may be used to effectively balance the exploration and exploitation stages. This method deals with engineering design optimization and real-world issues. In this work, SMA is used to identify solutions to economic load dispatch problems on a variety of test systems. Other new and popular approach outcomes are compared to analyze the results.

#### 3. Mathematical Formulation for Single-Area Economic Load Dispatch

The goal of the economic load dispatch problem is to lower the entire fuel cost of the power system by finding the optimum combination of power outputs from all generating units while congregating load demand and operational constraints.

### 3.1. Single-Area Economic Load Dispatch

The fuel cost for unit generation is represented as a quadratic function, with the assumption that the collective cost curves of the generating units develop as linear functions over time. The math for the single-area economic load dispatch for an hour is as follows in Equation (1):

$$fc(P^g) = \sum_{n=1}^{ng} \left[ a_n \left( P_n^g \right)^2 + b_n P_n^g + c_n \right]$$
(1)

here,  $n \in ng$ 

The dispatching of power generating units for 'Hr' Hours can be represented as:

$$fc(P^g) = \sum_{hr=1}^{Hr} \left( \sum_{n=1}^{ng} \left[ a_n \left( P_n^g \right)^2 + b_n P_n^g + c_n \right] \right)$$
(2)

here  $n \in ng$ ;  $hr \in Hr$ 

The right mathematics for ED is Equation (2). Because load demand changes over time, *'hr'* is changed from a single hour to *'Hr'* hours.

The above objective functions are subjected to the following equality and inequality constraints:

### 3.1.1. Power Balance Constraint

Total power generation is equal to total power demand plus system power loss.

$$\sum_{n=1}^{ng} P_n^g = P^d + P^l$$
(3)

here,  $P^d$  indicates requirement of power

here, the power loss,  $P^l$ , might be written as:

$$P^{I} = \sum_{n=1}^{ng} \sum_{m=1}^{ng} P_{n}^{g} B_{nm} P_{m}^{g}$$
(4)

In presence of loss coefficients  $B_{i0}$  and  $B_{00}$  matrices, the Equation (4) can be written as:

$$P^{l} = P_{n}^{g} B_{nm} P_{m}^{g} + \sum_{n=1}^{ng} P_{n}^{g} \times B_{i0} + B_{00}$$
(5)

The extension of Equation (5) is as follows:

$$P^{l} = \begin{bmatrix} P_{1} & P_{2} \dots & P_{ng} \end{bmatrix} \begin{bmatrix} B_{11} & B_{12} & B_{1n} \\ B_{21} & B_{22} & B_{2n} \\ B_{n1} & B_{n2} & B_{nn} \end{bmatrix} \begin{bmatrix} P_{1} \\ P_{2} \\ P_{ng} \end{bmatrix} + \begin{bmatrix} P_{1} & P_{2} & P_{ng} \end{bmatrix} \begin{bmatrix} B_{01} \\ B_{02} \\ B_{0ng} \end{bmatrix} + B \quad (6)$$

### 3.1.2. Generator Limit Constraint

The true power output of each generator is controlled by the upper and lower operational limits.

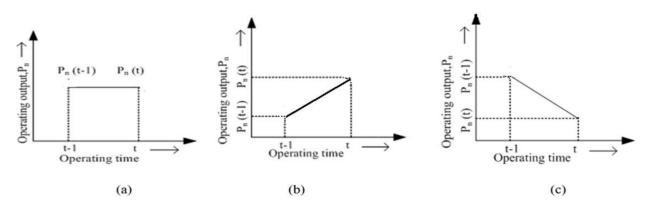
$$P_{n(minimum)}^{g} \le P_{n}^{g} \le P_{n(maximum)}^{g} \quad n = 1, 2, 3, \dots, ng$$

$$\tag{7}$$

where  $P_{n(minimum)}^{g}$  implies the lowest real power allocated at unit *n* and  $P_{n(maximum)}^{g}$  implies the highest real power allotted at unit *n*.

### 3.1.3. Ramp Rate Limits

The output power of the generating unit is boosted between the lower and higher limits of active power generation. Figure 1 depicts ramp rate limits.



**Figure 1.** Ramp rate limits (**a**) Increasing generator power (**b**) Reducing generator power (**c**) Generated power within upper and lower limits.

(a) By increasing generated power,

$$P_n^g - P_0^{g_0} \le ur_n \quad n = 1, 2, 3, \dots, ng$$
 (8)

(b) By reducing the amount of generated power,

$$P_n^{g_0} - P_n^g \le dr_n \quad n = 1, 2, 3, \dots, ng$$
(9)

As a consequence, the generator ramp rate is shown in the following equation.

$$maximum[P_{n(maximum)}^{g}, (ur_{n} - P_{n}^{g})] \le minimum[P_{n(minimum)}^{g}, (P_{n}^{g_{0}} - dr_{n})$$
(10)

where n = 1, 2, 3, ..., ng,  $P_n^{g0}$  is the current active power of the *n*th generation unit,  $P_n^g$  is the previous result of the active power of the *n*th generation unit,  $dr_n$  and  $ur_n$  are the lower and upper range for *n*th generation unit ramp rate limits.

Figure 1 [65] depicts the ramp limitations requirement.

### 3.1.4. Prohibited Operating Zones

Prohibited Operating Zones (POZ) are allocated to the graph for input–output powers in the generating unit, which may discontinue due to functional constraints of the generator produced by a defective mistake in the machine parts or the machine itself. As tracing genuine performance curves becomes increasingly difficult, the competent economy is calculated by disregarding performance curves in these areas. Figure 2 [46] depicts curves of prohibited operating zones. The discontinuous input–output power limitations are as follows in Equation (11):

$$\begin{cases}
P_{n(minimum)} \leq P_n \leq P_{n(minimum),1}^{POZ} \\
P_{n(maximum),m-1}^{POZ} \leq P_n \leq P_{(minimum),m}^{POZ} ; m = 2, 3, \dots n_{poz} \\
P_{n(maximum),m}^{POZ} \leq n_i \leq P_{n(maximum)}; m = n_{poz}
\end{cases}$$
(11)

where *m* denotes overall operating zones of *n*th generator,

 $P_{n(maximum),m-1}^{POZ}$  indicates upper limit of (m - 1)th*poz* of *n*th generator  $P_{(minimum),m}^{POZ}$  shows the lower limit of *m*th*poz* of *n*th generator

 $n_{poz}$  stands for overall operating zones.

Figure 2 [46] shows a sketch of the prohibited operating zones.

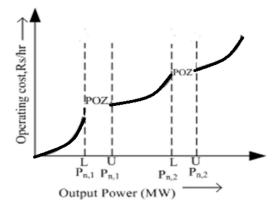


Figure 2. Curves of POZ.

### 4. Slime Mould Algorithm

There are numerous species in nature, each with their own distinctive behavior; however, only a handful of these characteristics draw attention and may be easily adopted and statistically molded to confront non-convex models. Many analysts aspire to emulate the working process for computational and algorithm evolution because of this flexibility. Slime moulds have been approved for the past few years based on this concept. The living style, characteristic behaviour of moulding structure based on the conditions, physical nature adjustments in food by estimating the distance, future plans for safeguarding by shifting to new regions of food sources before foraging based on the available information for moving towards rich food centres, and having the capability of stretching its biomass to various places to reach rich food are the key features to adopt in a SMA technique. Because of tremendous global search capabilities, SMA provides superior results.

It is known that the behavior of the organism can be imitated and molded to tackle the mathematics of unconstrained and non-convex characteristics. Researchers have tried to imitate the guiding principles to develop computations and algorithms. The slime moulds have received considerable attention over the past few years. Scientifically, the slime mould is titled Physarum polycephalum [83]. The slime mould undergoes a few changes in its structure, i.e., it repositions its front position into a fan shape model and its interconnected venous network allows the cytoplasm to flow inside at some level in a relocation series. This stretchable venous network helps in searching for food in multiple places and grabs

the food from food points. The slime mould has the ability to creep up to 900 sq. meters if it finds rich food points in the environment.

If there is no food, the slime mould creeps brilliantly. This natural behavior of slime moulds explains how it searches, travels, and reaches the food point according to environmental changes [84]. When the slime mould is approaching the target, it has the ability to judge its positive and negative wave propagation to discover a faster route to grab the food. This indicates that the slime mould can build a perfect path to reach the food point. It always selects a rich food area [85]. Based on the food availability and environmental changes, it changes speed and reaches a new location from an old location before foraging. The slime mould gathers the information about available food on empirical rules and plans to start the new search. Though the current region is rich in food, it divides its biomass to search for other resources which have high-quality food. According to the availability of the food point, the slime mould adjusts its search patterns. Figure 3 [86] displays slime mould moving towards food source.

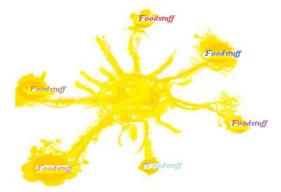


Figure 3. Slime mould creeping towards food.

### 4.1. Mathematical Modeling of SMA

The mathematical modeling of SMA is discussed in three stages, namely approaching food, wrapping food, and food grabble.

### 4.1.1. Technique of Approaching Food

Step1: Slime mould identifies the food based on the smell present in the air. The mathematics to explicate contraction phase and update its position during food search process are presented in the below expression which depends on x and p.

$$\overrightarrow{Y(\tau+1)} = \overrightarrow{Y_b(\tau)} + \overrightarrow{vb} \times (\overrightarrow{W} \times \overrightarrow{Y_A(\tau)} - \overrightarrow{Y_B(\tau)}), x > p$$
(12)

$$\overrightarrow{Y(\tau+1)} = \overrightarrow{vc} \times \overrightarrow{Y(\tau)}, x > p$$
(13)

where  $v\dot{b}$  is the parameter which ranges from [-d, d],  $\vec{vc}$  is the parameter which reaches zero linearly.  $\tau$  is the current iteration,  $\vec{Y_b}$  is the position of every particle in that area where aroma is maximum,  $\vec{Y}$  is the position of slime mould, randomly picked variables are  $\vec{Y_A}$ ,  $\vec{Y_b}$ , and  $\vec{W}$  is the weight.

The maximum limit *p* is as follows:

$$p = tanh|F(t) - bf| \tag{14}$$

where t = 1, 2, ..., n, F(t) is the fitness of slime mould's location, bf is the fitness value from all the steps. Equation (4) describes the range of the parameter vb.

v

$$\vec{b} = [-d,d] \tag{15}$$

$$d = \operatorname{arctanh}\left[-\left(\frac{\tau}{\operatorname{max}_{\tau}}\right) + 1\right] \tag{16}$$

The equation  $\vec{W}$  is expressed as follows:

$$\overrightarrow{W[StenchIndex(\tau)]} = \begin{cases} 1 + xlog\left(\frac{OpF - F(t)}{OpF - lF} + 1\right) \\ 1 - xlog\left(\frac{OpF - F(t)}{OpF - lF} + 1\right) \end{cases}$$
(17)

$$StenchIndex = sort(F) \tag{18}$$

Here, F(t) ranks the first half of the population, random value x lies in the interval [0, 1], optimal fitness value and least fitness value of the present iteration is given by OpF and lF, sorting the fitness value is done by sort(F). Figure 4a,b [86] depicts the outcomes of the Equations (12) and (13) and the possible positions of the slime mould in 2D and 3D view.

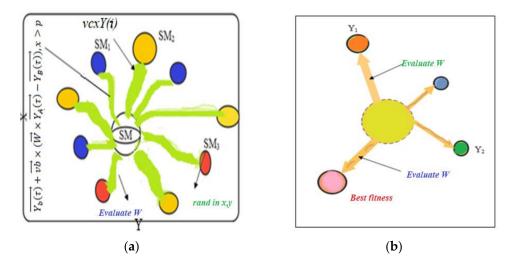


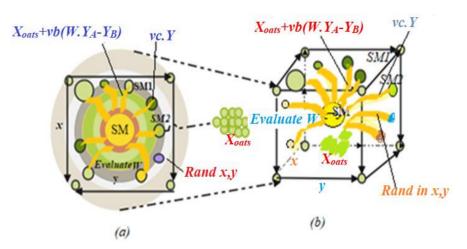
Figure 4. (a): 2D view of possible position; (b) assessment of fitness.

4.1.2. Technique of Wrapping Food

The slime mould's updated location is numerically given as:

$$\vec{Y}^{I} = \begin{cases} rand \times (U_{ub} - U_{lb}) + U_{lb}, rand < z \\ \overrightarrow{Y_{b}(\tau)} + \overrightarrow{vb} \times (\overrightarrow{W} \times \overrightarrow{Y_{A}(\tau)} - \overrightarrow{Y_{B}(\tau)}), x > p \\ \overrightarrow{vc} \times \overrightarrow{Y(\tau)}, x > p \end{cases}$$
(19)

The upper and lower bounds of search ranges are given as  $U_{ub}$ ,  $U_{lb}$ , rand, and x indicates the random value in the interval [0,1]. Figure 5a,b [86] depicts the slime mould's fitness value assessment process.



**Figure 5.** (a) Slime mould fitness assessment in 2D view and (b) Slime mould fitness assessment in 3D view.

4.1.3. Technique of Food Grabble

The slime mould's location gets upgraded in the search process and the value of vb varies within the limits [-d, d], and vc fluctuates between [-1, 1] and falls to zero.

The PSEUDO code for the proposed SM algorithm is exposed in Algorithm 1 and Figure 6 [86] presents the flow chart.

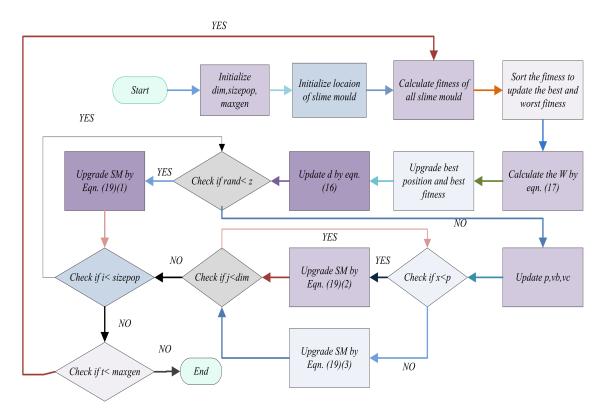


Figure 6. Flow Chart of SMA Algorithm.

#### Algorithm 1 PSEUDO Code for Slime Mould Algorithm.

Initialize the parameter popsize, Max\_iteration; Initialize the positions of slime mould  $Y^{I}$  (I = 1,2,3,...,n) While ( $\tau \leq Max_{iteration}$ ) Calculate the fitness of all slime mould; update bestfitness, OpF Calculate the W by Equation (17); For each search portion Update p,  $\overrightarrow{vc}$ ,  $\overrightarrow{vb}$ ; Update positions by Equation (19); End For  $\tau = \tau + 1$ ; End while Return Bestfitness, OpF;

### 5. Economic Load Dispatch Flow Chart Using Slime Mould Optimizer

Next, load the slime mould algorithm's input factors. The number of generations in which the system optimizes to achieve a lower price by meeting all of the constraints is based on the initial data loaded. Every objective function's fitness value is established by fulfilling the search space's bounds. Using Equation (19), the performance of the economic load dispatch issue is evaluated until the best price is found. SMA chooses the values within boundaries, especially for inequality constraints if the results generated in any iteration go out of range, and it adds a penalty factor for equality constraints, exactly like any other method. This procedure is continued until the last iteration has been finished and the best outcomes have been achieved. The algorithm steps are:

Step 1: Initiate by loading the system parameters and SMA factors; Step 2: Place the preliminary data at random to equal the entire number of generators present; Step 3: Optimize for the random point of every search agent and deliver back when diverging from the search space; Step 4: Verify each main function's fitness value; Step 5: Set t determined fitness in an array; Step 6: Adapt the best and worst fitness values; Step 7: Regulate for slime mould's flexible weight; Step 8: Revise the locations of search agents; Step 9: Evaluate slime mould's weight in the phases of wrapping and grabbling food; Step 10: Search agents find two locations randomly in the phase of food approach; Step 11: Return to exploring fitness; Step 12: Find the optimum cost-effective fuel price; Step 13: Put an end to the program.

Figure 6 [86] depicts the slime mould algorithm flow chart.

The flowchart in Figure 6 describes the functioning of slime mould algorithm in which the position of slime mould is initialized. The fitness is calculated and sorted to update the best and worst fitness. The slime mould is actually based on the propagation wave generated by the biological oscillator to alter the cytoplasm flow in veins in order to reach the better location of food. To show the venous width variations in the slime mould,  $\vec{W}$ ,  $\vec{vb}$ ,  $\vec{vc}$  are used which recognize the variations. The value of  $\vec{W}$  is calculated to upgrade the best position and best-fitness values.  $\vec{vb}$  lies between [-d,d] and reaches zero as the iteration increases.  $\vec{vc}$  remains in the interval [-1,1] and tends to zero.  $\vec{vb}$  plays a key role in deciding to reach a food source. Thus, finally the slime mould reaches the best location of food point by the iterative process.

#### 6. Test System Results and Discussion

In this section of the paper, the IEEE bus systems in small-, medium-, and large-size test systems are considered, and comparisons are done with other methods to see how well the slime mould optimization algorithm performed on the economic load dispatch issue. The goal of implementing this approach was to lower the cost of fuel. The recommended method was implemented in MATALB R2016a on a laptop with an Intel Core i3 CPU,

cover a solution for the economic load

7th generation, and 8GB RAM in order to discover a solution for the economic load dispatch issue. Search agents considered 50 and 500 iterations, and 30 maximum runs while implementing SMA. The effectiveness of the proposed approach was tested on a variety of test systems, including constraints such as with and without valve-point loading effects, which are addressed in Section 6.

To validate the efficacy of the proposed SMA technique, it was implemented on 3-, 5-, 6-, 10-, 13-, 15-, 20-, 38-, and 40- unit systems to find solution for the economic load dispatch issue. Overall, the obtained fuel cost results of SMA were compared with other already existing economic load dispatch solution methods from standard papers. The conditions considered for the analysis to solve economic load dispatch by SMA include: (a) without valve-point effect; (b) with valve-point effect; (c) with transmission losses; and (d) without transmission losses. The following are the test cases discussed.

### 6.1. Test System-I (Small-Scale Power System)

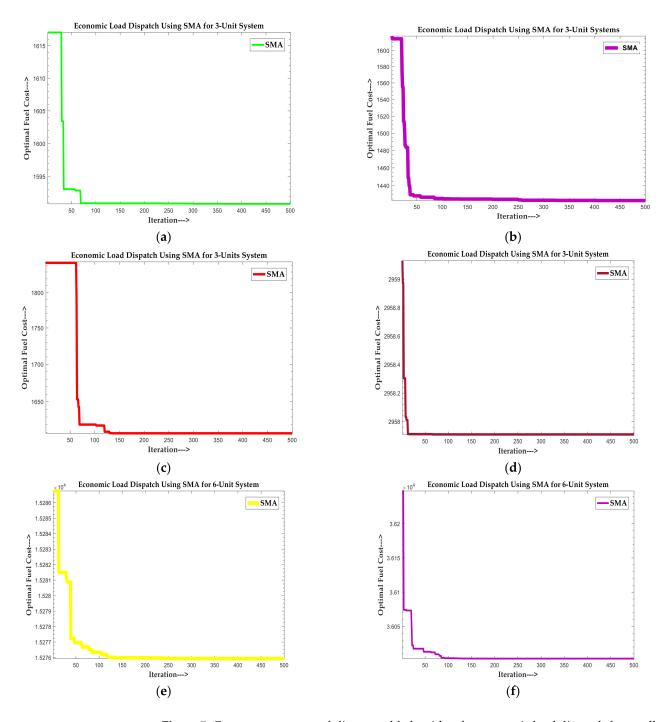
This section covers six different cases without valve-point loading and two different cases with valve-point loading:

### I—Case Study

The input test data, as well as loss coefficient matrices, were obtained from [87]. A three-generator test system with a power requirement of 150 MW was assessed, which is given in Appendix A in Table A1. In this case, the ELD issue was cracked without the valve-point effect. Table 1 indicates that the slime Mould algorithm's fuel price was 1590.627083 Rs./h, which was the lowest of all the algorithms while still satisfying the system constraints. Figure 7a depicts the convergence curve of SMA obtained by simulation which was stable.

**Table 1.** (Case-I) Slime mould algorithm results for economic dispatch of a 3-unit system (without valve-point effect).

|                                  |                       | Transfer of Power Generating Units |         |          |          |  |  |  |  |  |  |
|----------------------------------|-----------------------|------------------------------------|---------|----------|----------|--|--|--|--|--|--|
| Method                           | Fuel Price<br>(Rs./h) | Required Power in<br>Demand (MW)   | G1      | G2       | G3       | Loss in Power,<br>P <sub>Loss</sub> (MW) |  |  |  |  |  |
| Grey Wolf Optimizer [88]         | 1597.4815             | 150                                | 30.4998 | 64.6208  | 54.8994  | 2.3444                                   |  |  |  |  |  |
| Quadratic Programming [89]       | 1596                  | 150                                | 32.8116 | 64.5973  | 54.9329  | 2.3419                                   |  |  |  |  |  |
| Lambda Method [87]               | 1599.98               | 150                                | 33.4701 | 64.0974  | 55.1011  | 2.6686                                   |  |  |  |  |  |
| Particle Swarm Optimization [87] | 1597.48               | 150                                | 32.8101 | 64.595   | 54.9369  | 2.342                                    |  |  |  |  |  |
| Genetic Algorithm [87]           | 1600                  | 150                                | 34.4895 | 64.0299  | 54.1534  | 2.6728                                   |  |  |  |  |  |
| Slime Mould Algorithm            | 1590.627083           | 150                                | 10      | 76.42812 | 64.24508 | 0.336600019                              |  |  |  |  |  |



**Figure 7.** Convergence curve of slime mould algorithm for economic load dispatch for small-scale power systems (3-generating unit systems and 6-generating unit systems) without valve-point loading effect; (a) Case-I (3-unit system) convergence curve, (b) Case-II (3-unit system) convergence curve, (c) Case-III (3-unit system) convergence curve, (d) Case-IV (3-unit system) convergence curve, (e) Case-V (6-unit system) convergence curve, (f) Case-VI (6-unit system) convergence curve.

#### II—Case Study

The input data for this system were drawn from [90] and loss coefficient matrices. A three-generator test system with a power requirement of 125 MW was used which was needed to assess the comparable transmission given in Table A2. In this case, the ELD issue was cracked without the valve-point effect. Table 2 indicates that the slime mould algorithm's fuel price was 1413.990605 Rs./h, which was the best of all algorithms while

still satisfying the system constraints. Figure 7b depicts the convergence curve of SMA obtained by simulation which was stable.

**Table 2.** (Case-II) Slime Mould algorithm results for economic dispatch of a 3-unit system (without valve-point effect).

|                        | Transfer of Power Generating Units |                                  |    |          |          |  |  |  |  |  |  |
|------------------------|------------------------------------|----------------------------------|----|----------|----------|--|--|--|--|--|--|
| Method                 | Fuel Price<br>(Rs./h)              | Required Power<br>in Demand (MW) | G1 | G2       | G3       | Loss in Power,<br>P <sub>Loss</sub> (MW) |  |  |  |  |  |
| Lambda Algorithm [90]  | 1422.159458                        | 125                              | -  | -        | -        | 2.084005739                              |  |  |  |  |  |
| Firefly Algorithm [90] | 1421.561972                        | 125                              | -  | -        | -        | 1.964774407                              |  |  |  |  |  |
| Slime Mould Algorithm  | 1413.990605                        | 125                              | 10 | 70.21971 | 45.41896 | 0.319332527                              |  |  |  |  |  |

### III—Case Study

The input data for this system were drawn from [90] and loss coefficient matrices. A three-generator test system with a power requirement of 150 MW was assessed which is given in Table A3. In this case, the ELD issue was cracked without the valve-point effect. Table 3 indicates that the slime mould algorithm's fuel price was 1608.866334 Rs./h, which was the best of all algorithms while still satisfying the system constraints. Figure 7c depicts the convergence curve of SMA obtained by simulation which was stable.

**Table 3.** (Case-III) Slime mould algorithm results for economic dispatch of a 3-unit system (without valve-point effect).

|                        | Transfer of Power Generating Units |                                  |        |        |          |  |  |  |  |  |  |
|------------------------|------------------------------------|----------------------------------|--------|--------|----------|--|--|--|--|--|--|
| Method                 | Fuel Price<br>(Rs./hr)             | Required Power<br>in Demand (MW) | G1     | G2     | G3       | Loss in Power,<br>P <sub>Loss</sub> (MW) |  |  |  |  |  |
| Lambda Algorithm [90]  | 1625.4586                          | 150                              | -      | -      | -        | 2.813864755                              |  |  |  |  |  |
| Firefly Algorithm [90] | 1616.921725                        | 150                              | 32.729 | 63.843 | 56.151   | 2.721760653                              |  |  |  |  |  |
| Slime Mould Algorithm  | 1608.866334                        | 150                              | 10     | 80     | 60.74528 | 0.372641                                 |  |  |  |  |  |

### IV—Case Study

The input data for a three-unit test system were drawn from [91], with 250 MW power need, as well as loss coefficient matrices which were required to assess comparable transmission and are displayed in Table A4. Table 4 indicates that the slime mould technique yielded a fuel price of 2957.909554 Rs./h, which was the best fuel price among all known algorithms while still satisfying all the constraints. Figure 7d depicts the convergence curve of SMA obtained by simulation which was stable.

**Table 4.** (Case-IV) Slime mould algorithm results for economic dispatch of a 3-unit system (without valve-point effect).

|                                     | Transfer of Power Generating Units |                                  |          |          |          |  |  |  |  |  |  |  |
|-------------------------------------|------------------------------------|----------------------------------|----------|----------|----------|--|--|--|--|--|--|--|
| Method                              | Fuel Price<br>(Rs./h)              | Required Power<br>in Demand (MW) | G1       | G2       | G3       | Loss in Power,<br>P <sub>Loss</sub> (MW) |  |  |  |  |  |  |
| Particle Swarm<br>Optimization [91] | 2959.98                            | 250                              | 151.09   | 42.04    | 56.87    | 0  |  |  |  |  |  |  |
| Slime Mould Algorithm               | 2957.909554                        | 250                              | 165.7781 | 29.85793 | 54.36396 | 0  |  |  |  |  |  |  |

### V—Case Study

With a power demand of 1263 MW, a six-unit test system without valve-point load effect was taken from [92], which is given in Table A5. The loss coefficients matrix was zero.

Table 5 shows that the slime mould algorithm obtained a best fuel price of 15,275.9304 Rs./h, beating already existing algorithms by satisfying all the constraints. The convergence curve of SMA obtained by simulation which was stable is shown in Figure 7e.

**Table 5.** (Case-V) Slime mould algorithm results for economic dispatch of a 6-unit system (without valve-point effect).

|  |                          |  | Tran     | sfer of Pow | er Generatin | g Units     |             |             |   |
|--|--------------------------|--|----------|-------------|--------------|-------------|-------------|-------------|---|
| Method   | Fuel<br>Price<br>(Rs./h) | Required<br>Power in<br>Demand<br>(MW) | G1       | G2          | G3           | G4          | G5          | G6          | Loss in<br>Power,<br>P <sub>Loss</sub> (MW) |
| New Particle Swarm Optimization-local<br>random search [93]          | 15,450                   | 1263                                   | 446.96   | 173.3944    | 262.3436     | 139.5120    | 164.7089    | 89.0162     | 12.9361                                     |
| Differential Evaluation [94]   | 15,445.90                | 1263                                   | 400.00   | 186.55      | 289.00       | 150.00      | 200.00      | 50.00       | 12.52                                       |
| New Particle Swarm Optimization [93]                                 | 15,450                   | 1263                                   | 447.4734 | 173.1012    | 262.6804     | 139.4156    | 165.3002    | 87.9761     | 12.9470                                     |
| Simulated Annealing Algorithm [92]                                   | 15,466.00                | 1263                                   | 447.08   | 173.18      | 263.92       | 139.06      | 165.58      | 86.63       | 12.47                                       |
| Classical Particle Swarm Optimization<br>2(CPSO2) [24]               | 15,446                   | 1263                                   | 434.4295 | 173.3231    | 274.4735     | 128.0598    | 179.4759    | 85.9281     | 12.9582                                     |
| Particle Swarm Optimization [95]                                     | 15,450                   | 1263                                   | 447.50   | 173.32      | 263.47       | 139.06      | 165.48      | 87.13       | 12.958                                      |
| Genetic Algorithm [96]   | 15,459                   | 1263                                   | 474.81   | 178.64      | 262.21       | 134.28      | 151.90      | 74.18       | 13.022                                      |
| New Modified Particle Swarm<br>Optimization [97]                     | 15,447                   | 1263                                   | 446.71   | 173.01      | 265.00       | 139.00      | 165.23      | 86.78       | 12.733                                      |
| Particle Swarm Optimization –local<br>random search [93]             | 15,450                   | 1263                                   | 47.4440  | 173.3430    | 263.3646     | 139.1279    | 165.5076    | 87.1698     | 12.9571                                     |
| Firefly Algorithm [92]   | 15,443                   | 1263                                   | 445.08   | 173.08      | 264.42       | 139.59      | 166.02      | 87.21       | 12.4  |
| Classical Particle Swarm Optimization<br>1(CPSO1) [24]               | 15,447                   | 1263                                   | 434.4236 | 173.4385    | 274.2247     | 128.0183    | 179.7042    | 85.9082     | 12.9583                                     |
| Biogeography-Based Optimization [98]                                 | 15,443.0963              | 1263                                   | 447.3997 | 173.2392    | 263.3163     | 138.0006    | 165.4104    | 87.07979    | 12.464                                      |
| Iteration Particle Swarm Optimization<br>(IPSO) [24]                 | 15,444                   | 1263                                   | 440.5711 | 179.8365    | 261.3798     | 131.9134    | 170.9823    | 90.8241     | 12.548                                      |
| Artificial Bee Colony Optimization [99]                              | 15,445.90                | 1263                                   | 438.65   | 167.90      | 262.82       | 136.77      | 171.76      | 97.67       | 12.52                                       |
| Self-Organizing Hierarchical<br>Particle Swarm<br>Optimization [100] | 15,446.02                | 1263                                   | 438.21   | 172.58      | 257.42       | 141.09      | 179.37      | 86.88       | 12.55                                       |
| Slime Mould Algorithm  | 15,275.9304              | 1263                                   | 446.6889 | 171.254     | 264.1159     | 125.2018495 | 172.1444773 | 83.59471703 | 0   |

### VI—Case Study

This system was comprised of a six-unit test system with a total power requirement of 700 MW, as well as loss coefficient matrices which were needed to assess comparable transmission, and the input data were drawn from [91], which is given in Table A6. Table 6 indicates that the fuel cost using the slime mould algorithm was 36,003.12394 Rs./h, which was the best of all methods satisfying the constraints. Figure 7f depicts the convergence curve of SMA obtained by simulation which was stable.

**Table 6.** (Case-VI) Slime mould algorithm results for economic dispatch of a 6-unit system (without valve-point effect).

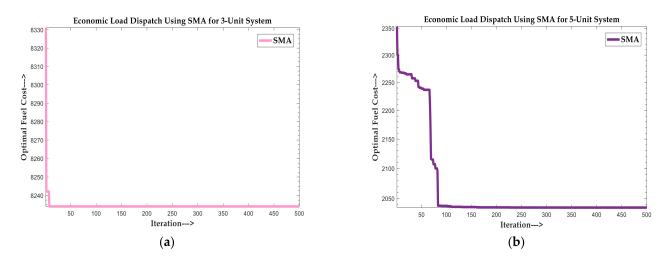
|                                     | Transfer of Power Generating Units |  |         |    |          |                 |                 |                 |  |  |
|-------------------------------------|------------------------------------|--|---------|----|----------|-----------------|-----------------|-----------------|--|--|
| Method                              | Fuel Price<br>(Rs./h)              | Required<br>Power in<br>Demand<br>(MW) | G1      | G2 | G3       | G4              | G5              | G6              | Loss in<br>Power,<br>P <sub>Loss</sub><br>(MW) |  |
| Conventional<br>Method [91]         | 36,914.01                          | 700                                    | 28.33   | 10 | 118.95   | 118.67          | 230.75          | 212.80          | 19.50  |  |
| Particle Swarm<br>Optimization [91] | 36,912.16                          | 700                                    | 28.28   | 10 | 119.02   | 118.79          | 230.78          | 212.56          | 19.43  |  |
| Slime Mould Algorithm               | 36,003.12394                       | 700                                    | 24.9763 | 10 | 102.6661 | 110.6311<br>238 | 232.677<br>8302 | 219.0486<br>296 | 0  |  |

### VII—Case Study

A three-generator test system with valve-point loading effect was utilized with a 850 MW power demand, and the input test information is given in Table A7 which was acquired from [4] with the loss coefficient matrix set to zero. Table 7 indicates that the best fuel price across all algorithms was 8234.07173 Rs./h when utilizing the slime mould algorithm that satisfied all the constraints. Figure 8a depicts the convergence curve of SMA obtained by simulation which was stable.

**Table 7.** (Case-VII) Slime mould algorithm results for economic dispatch of a 3-unit system (with valve-point effect).

|                       |                       | Transfer                         | of Power Ger | erating Uni | its         |  |
|-----------------------|-----------------------|----------------------------------|--------------|-------------|-------------|--|
| Method                | Fuel Price<br>(Rs./h) | Required Power in<br>Demand (MW) | G1           | G2          | G3          | Loss in Power,<br>P <sub>Loss</sub> (MW) |
| CPSO [4]              | 8234.07               | 850                              | 300.267      | 400         | 149.733     | NR                                       |
| GA [101]              | 8575.64               | 850                              | 382.2552     | 340.3202    | 127.4184    | NR                                       |
| EP-SQP [4]            | 8234.07               | 850                              | 300.264      | 400         | 149.733     | NR                                       |
| DE [49]               | 8234.07173            | 850                              | 300.2668999  | 400         | 149.7331001 | NR                                       |
| PSO [4]               | 8234.07               | 850                              | 300.267      | 400         | 149.733     | NR                                       |
| ABC [101]             | 8253.10               | 850                              | 300.266      | 400         | 149.733     | NR                                       |
| PSO-SQP [4]           | 8234.07               | 850                              | 300.268      | 400         | 149.733     | NR                                       |
| EP [4]                | 8234.07               | 850                              | 300.264      | 400         | 149.736     | NR                                       |
| Lambda [101]          | 8575.68               | 850                              | 382.258      | 340.323     | 127.419     | NR                                       |
| CPSO-SQP [4]          | 8234.07               | 850                              | 300.266      | 400         | 149.734     | NR                                       |
| Slime Mould Algorithm | 8234.07173            | 850                              | 300.2668998  | 400         | 149.7331002 | 0  |



**Figure 8.** Convergence curve of slime old algorithm for economic load dispatch for small-scale power systems (3-generating unit system and 5-generating unit system) with valve-point loading effect, (a) Convergence curve for Case-VII (3-unit system), (b)Convergence curve for Case-VIII (5-unit system).

### VIII—Case Study

With a power demand of 730 MW, a five-unit test system with valve-point loading effect was used, and its input test information was taken from [101] with the loss coefficient matrix set to zero, which is given in Table A8. Table 8 shows that the slime mould algorithm obtained a fuel price of 2034.972427 Rs./h, satisfying all the constraints and was the best

fuel price among all algorithms. The convergence curve of SMA obtained by simulation which was stable is shown in Figure 8b.

**Table 8.** (Case-VIII) Slime mould algorithm results for economic dispatch of a 6-unit system (with valve-point effect).

|                                      | Transfer of Power Generating Units |                                  |             |             |             |            |            |  |  |  |  |  |  |
|--------------------------------------|------------------------------------|----------------------------------|-------------|-------------|-------------|------------|------------|--|--|--|--|--|--|
| Method                               | Fuel Price<br>(Rs./h)              | Required Power in<br>Demand (MW) | G1          | G2          | G3          | G4         | G5         | Loss in Power, P <sub>Loss</sub><br>(MW) |  |  |  |  |  |
| Genetic Algorithm [101]              | 2412.538                           | 730                              | 218.0184    | 109.0092    | 147.5229    | 28.37844   | 227.0275   | NR                                       |  |  |  |  |  |
| Particle Swarm<br>Optimization [101] | 2252.572                           | 730                              | 229.5195    | 125         | 175         | 75         | 125.4804   | NR                                       |  |  |  |  |  |
| Lambda [101]                         | 2412.709                           | 730                              | 218.028     | 109.014     | 147.535     | 28.380     | 272.042    | NR                                       |  |  |  |  |  |
| APSO [101]                           | 2140.97                            | 730                              | 225.3845    | 113.020     | 109.4146    | 73.11176   | 209.0692   | NR                                       |  |  |  |  |  |
| Slime Mould Algorithm                | 2034.972427                        | 730                              | 229.5195832 | 102.9830227 | 112.6813882 | 74.9999977 | 209.816008 | 0  |  |  |  |  |  |

### 6.2. Test System-II (Medium-Scale Power System)

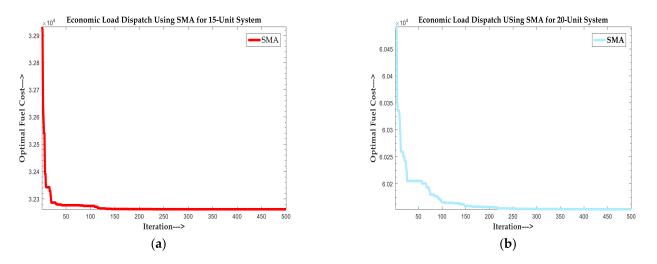
Under medium-size power systems, four distinct test systems were tested. Two of the cases were examined without the effect of valve-point loading, whereas the other two were tested with the influence of valve-point loading.

I—Case Study

For a 15-unit test system with a power demand of 2630 MW, the input test information was obtained from [102], coupled with loss coefficient matrices which were essential to predict comparable transmission and are given in Table A9. In this case, the ELD issue was cracked without valve-point effect. Table 9 indicates that the best fuel price across all algorithms was 32,259.69352 Rs./h when utilizing the slime mould algorithm which satisfied all the constraints. Figure 9a depicts the convergence curve of SMA obtained by simulation which was stable.

**Table 9.** (Case-I) Slime mould algorithm results for economic dispatch of a 15-unit system (without valve-point effect).

| Method                                      | CPSO1<br>[24] | ETQ<br>[102] | PSO<br>[102] | ESO<br>[102] | SOH_PSO<br>[24] | PSO(4)<br>[102] | CPSO2<br>[24] | IPSO<br>[24] | ABC<br>[103] | ES<br>[102] | Hybrid<br>GAPSO<br>[24] | GA<br>[102] | Slime<br>Mould<br>Algorithm |
|---|---------------|--------------|--------------|--------------|-----------------|-----------------|---------------|--------------|--------------|-------------|-------------------------|-------------|-----------------------------|
| Fuel price (Rs. /h)                         | 32,835        | 32,507.5     | 32,858       | 32,506.      | 682,751.39      | 32,508.12       | 32,834        | 32,709       | 32,707.85    | 32,568.54   | 32,724                  | 33,113      | 32,259.69325                |
| Required Power in<br>Demand<br>(MW)         | 2630          | 2630         | 2630         | 2630         | 2630            | 2630            | 2630          | 2630         | 2630         | 2630        | 2630                    | 2630        | 2630                        |
| G1  | 450.05        | 450          | 439.12       | 456          | 455             | 440.499         | 450.02        | 455          | 455          | 455         | 436.8482                | 415.31      | 455                         |
| G2  | 454.04        | 450          | 407.97       | 456          | 380             | 179.5947        | 454.06        | 380          | 380          | 380         | 409.6974                | 359.72      | 454.7336                    |
| G3  | 124.82        | 130          | 119.63       | 130          | 130             | 21.0524         | 124.81        | 129.97       | 130          | 130         | 117.0074                | 104.42      | 130                         |
| G4  | 124.82        | 130          | 129.99       | 130          | 130             | 87.1376         | 124.81        | 130          | 130          | 150         | 128.2705                | 74.98       | 129.9999991                 |
| G5  | 151.03        | 335          | 151.07       | 304.24       | 170             | 360.7675        | 151.06        | 169.93       | 169.9997     | 168.92      | 153.3361                | 380.28      | 288.3104957                 |
| G6  | 460           | 455          | 459.99       | 460          | 459.96          | 395.833         | 460           | 459.88       | 460          | 459.34      | 457.4078                | 426.79      | 459.9767033                 |
| G7  | 434.53        | 465          | 425.56       | 465          | 430             | 432.0085        | 434.57        | 429.25       | 430          | 430         | 424.4400                | 341.32      | 465                         |
| G8  | 148.41        | 60           | 98.56        | 60           | 117.53          | 168.9198        | 148.46        | 60.43        | 71.9698      | 97.42       | 101.1949                | 124.79      | 60.19352401                 |
| G9  | 63.61         | 25           | 113.49       | 25           | 77.90           | 162             | 63.59         | 74.78        | 59.1798      | 30.61       | 116.1186                | 133.14      | 25                          |
| G10   | 101.13        | 20           | 101.11       | 20           | 119.54          | 138.4343        | 101.12        | 158.02       | 159.8004     | 142.56      | 102.2243                | 89.26       | 25.24209                    |
| G11   | 28.656        | 20           | 33.91        | 29.15        | 54.50           | 52.6294         | 28.655        | 80           | 80           | 80          | 35.0317                 | 60.06       | 20.04263                    |
| G12   | 20.912        | 55           | 79.96        | 59.24        | 80              | 66.8875         | 20.914        | 78.57        | 80           | 85          | 78.8482                 | 50          | 61.37133                    |
| G13   | 25.001        | 25           | 25.          | 25           | 25              | 62.7471         | 25.002        | 25           | 25.0024      | 15          | 27.1292                 | 38.77       | 25.00313                    |
| G14   | 54.418        | 15           | 41.41        | 17.28        | 17.86           | 47.5574         | 54.414        | 15           | 15.0056      | 15          | 37.1594                 | 41.94       | 15.09977                    |
| G15   | 20.625        | 15           | 35.61        | 15           | 15              | 27.6065         | 20.624        | 15           | 15.0014      | 15          | 37.0390                 | 22.64       | 15.04694                    |
| Loss in Power,<br>P <sub>Loss</sub><br>(MW) | 32.1302       | 15.8         | 32.42        | 13.79        | 32.28           | 13.6745         | 32.1303       | 30.858       | 13           | 23.85       | 31.75                   | 38.28       | 0.010082332                 |



**Figure 9.** Convergence curve of slime mould algorithm for economic load dispatch for mediumscale power systems (15-generating unit system and 20-generating unit system) without valve-point loading effect, (**a**) Convergence curve for Case-I (15-unit system), (**b**) Convergence curve for Case-II (20-unit system).

### II—Case Study

For a twenty generator test system with a power requirement of 2500 MW, the input test data were obtained from [102], which is shown in Table A10 along with loss coefficient matrices which are essential to predict comparable transmission. In this case, the ELD issue was cracked without valve-point effect. Table 10 indicates that the slime mould algorithm yielded a fuel price of 60,152.72915 Rs./h, which was the lowest of all methods. Figure 9b depicts the convergence curve of SMA obtained by simulation which was stable.

**Table 10.** (Case-II) Slime mould algorithm results for economic dispatch of a 20-unit system (without valve-point effect).

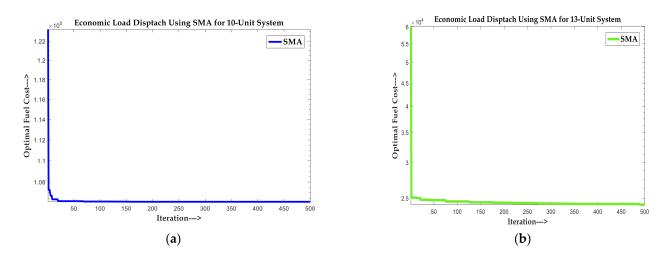
| Method                                | Hopfield Neural Network [104] | Lambda-Iteration Method [102] | Slime Mould Algorithm |
|---------------------------------------|-------------------------------|-------------------------------|-----------------------|
| Fuel Price (Rs./h)                    | 62,456.6341                   | 62,456.6391                   | 60,152.72915          |
| Required Power in Demand<br>(MW)      | 2500                          | 2500                          | 2500                  |
| G1                                    | 512.7804                      | 512.7805                      | 599.9962              |
| G2                                    | 169.1035                      | 169.1033                      | 127.2091              |
| G3                                    | 126.8897                      | 126.8898                      | 50.01089              |
| G4                                    | 102.8656                      | 102.8657                      | 50                    |
| G5                                    | 113.6836                      | 113.6836                      | 92.80191              |
| G6                                    | 73.5709                       | 73.5710                       | 20.00047              |
| G7                                    | 115.2876                      | 115.2878                      | 124.9982              |
| G8                                    | 116.3994                      | 116.3994                      | 50                    |
| G9                                    | 100.4063                      | 100.4062                      | 112.1931              |
| G10                                   | 106.0267                      | 106.0267                      | 43.44606              |
| G11                                   | 150.2395                      | 150.2394                      | 289.1196              |
| G12                                   | 292.7647                      | 292.7648                      | 433.1905              |
| G13                                   | 119.1155                      | 119.1154                      | 122.9385              |
| G14                                   | 30.8342                       | 30.8340                       | 72.39983              |
| G15                                   | 115.8056                      | 115.8057                      | 95.40311              |
| G16                                   | 36.2545                       | 36.2545                       | 36.15509              |
| G17                                   | 66.8590                       | 66.8590                       | 30.01615              |
| G18                                   | 87.9720                       | 87.9720                       | 39.79051              |
| G19                                   | 100.8033                      | 100.8033                      | 80.33078              |
| G20                                   | 54.3050                       | 54.3050                       | 30                    |
| Loss in Power, P <sub>Loss</sub> (MW) | 91.9669                       | 91.9670                       | 0                     |

### III—Case Study

The input test information was obtained from [105] with the loss coefficient matrix set to zero, and a ten generator test system with valve-point loading effect was used with a power demand of 2000 MW, which is shown in Table A11. Table 11 shows that when utilizing the slime mould algorithm, the fuel price was 106170.418 Rs./h, which was the best fuel price among all algorithms. The convergence curve of SMA obtained by simulation which was stable is shown in Figure 10a.

**Table 11.** (Case-III) Slime mould algorithm results for economic dispatch of a 10-unit system (with valve-point effect).

| Method                                      | PDE<br>[106] | FPA<br>[106] | MODE<br>[106] | PSO<br>[105] | NSGAII<br>[106] | GSA<br>[106] | PSO-TVAC<br>[107] | ABC_PSO<br>[106] | EMOCA<br>[106] | MSCO<br>[106] | SPEA-2<br>[106] | Slime Mould<br>Algorithm |
|---|--------------|--------------|---------------|--------------|-----------------|--------------|-------------------|------------------|----------------|---------------|-----------------|--------------------------|
| Fuel Price<br>(Rs./h)                       | 113,510      | 113,370      | 113,484       | 107,620      | 113,539         | 113,490      | 107,620           | 113,420          | 113,445        | 110,870       | 113,520         | 106,170.418              |
| Power in<br>Demand<br>(MW)                  | 2000         | 2000         | 2000          | 2000         | 2000            | 2000         | 2000              | 2000             | 2000           | 2000          | 2000            | 2000                     |
| G1  | 54.9853      | 53.188       | 54.9487       | 53.1000      | 51.9515         | 54.9992      | 53.8              | 55               | 55             | 52.8995       | 52.9761         | 54.99996                 |
| G2  | 79.3803      | 79.975       | 74.5821       | 79.2000      | 67.2584         | 79.9586      | 78.9              | 80               | 80             | 74.9428       | 72.813          | 79.9999                  |
| G3  | 83.9842      | 78.105       | 79.4294       | 112          | 73.6879         | 79.4341      | 109               | 81.14            | 83.5594        | 97.4068       | 78.1128         | 89.30891                 |
| G4  | 86.5942      | 97.119       | 80.6875       | 121          | 91.3554         | 85.0000      | 125               | 84.216           | 84.6031        | 95.9554       | 83.6088         | 79.87863                 |
| G5  | 144.4386     | 152.74       | 136.8551      | 98.8000      | 134.0522        | 142.1063     | 98.8              | 138.3377         | 146.5632       | 131.8702      | 137.2432        | 66.48786                 |
| G6  | 165.7756     | 163.08       | 172.6393      | 100          | 174.9504        | 166.5670     | 90.4              | 167.5086         | 169.2481       | 200.5119      | 172.9188        | 70.00002                 |
| G7  | 283.2122     | 258.61       | 283.8233      | 299          | 289.4350        | 292.8749     | 298               | 296.8338         | 300            | 227.9224      | 287.2033        | 290.7383                 |
| G8  | 312.7709     | 302.22       | 316.3407      | 320          | 314.0556        | 313.2387     | 330               | 311.5824         | 317.3496       | 303.6511      | 326.4023        | 328.5865                 |
| G9  | 440.1135     | 433.21       | 448.5923      | 467          | 455.6978        | 441.1775     | 468               | 420.3363         | 412.9183       | 366.3189      | 448.8814        | 470                      |
| G10   | 432.6783     | 466.07       | 436.4287      | 356          | 431.8054        | 428.6306     | 351               | 449.1598         | 434.3133       | 470.0000      | 423.9025        | 470                      |
| Loss in<br>Power, P <sub>Loss</sub><br>(MW) | 83.9         | 84.3         | 84.33         | NR           | 84.25           | 83.9869      | NR                | 84.1736          | 83.56          | 21.4789       | 84.1            | 0                        |



**Figure 10.** Convergence curve of slime mould algorithm for economic load dispatch for mediumscale power systems (10-generating unit system and 13-generating unit system) with valve-point loading effect, (**a**) Convergence curve for Case-III (10-unit system), (**b**) Convergence curve for Case-IV (13-unit system).

### IV—Case Study

With a power demand of 2520 MW, a thirteen generator test system with valve-point loading effect was used and the input test data were obtained from [62], with the loss coefficient matrix set to zero and shown in Table A12. Table 12 shows that when utilizing the slime mould algorithm, the fuel price was 24,177.23727 Rs./h, which was the best fuel price among all known algorithms. The convergence curve of SMA obtained by simulation which was stable is shown in Figure 10b.

| Method                                 | GWO<br>[108] | JAYA<br>[108] | NGWO<br>[108] | EP-SQP<br>[62] | SA<br>[62] | GA<br>[62] | PSO-SQP<br>[62] | CJAYA<br>[62] | GWOII<br>[108] | GWOI<br>[108] | GA-SA<br>[62] | CPSO<br>[4] | Slime<br>Mould<br>Algorithm |
|--|--------------|---------------|---------------|----------------|------------|------------|-----------------|---------------|----------------|---------------|---------------|-------------|-----------------------------|
| Fuel Price<br>(Rs./h)                  | 24,231.18    | 24,220.752    | 2924,185.45   | 24,266.44      | 24,970.91  | 24,418.99  | 24,261.05       | 24,178.8040   | ) 24,198.47    | 24,244.69     | 24,275.71     | 24,211.5    | 6 24,177.23727              |
| Required<br>Power in<br>Demand<br>(MW) | 2520         | 2520          | 2520          | 2520           | 2520       | 2520       | 2520            | 2520          | 2520           | 2520          | 2520          | 2520        | 2520                        |
| G1                                     | 647.3842     | 628.3185      | 630.9951      | 628.3136       | 668.40     | 627.05     | 628.3205        | 628.3185      | 630.9811       | 645.5569      | 628.23        | 682.32      | 628.3184973                 |
| G2                                     | 306.3995     | 299.2009      | 297.9355      | 299.1715       | 359.78     | 359.40     | 299.0524        | 299.1992      | 300.8038       | 306.9539      | 299.22        | 299.83      | 298.0415722                 |
| G3                                     | 309.6117     | 306.9105      | 299.9253      | 299.0474       | 358.20     | 358.95     | 298.9681        | 299.1993      | 302.7475       | 306.5356      | 299.17        | 299.17      | 298.9244776                 |
| G4                                     | 175.1400     | 159.7339      | 157.9267      | 159.6399       | 104.28     | 158.93     | 159.4680        | 159.7330      | 160.1702       | 169.6878      | 159.12        | 159.70      | 159.7225373                 |
| G5                                     | 66.8791      | 159.7337      | 159.6433      | 159.6560       | 60.36      | 159.73     | 159.1429        | 159.7331      | 161.0252       | 168.4922      | 159.95        | 159.64      | 159.6885214                 |
| G6                                     | 162.7466     | 159.7338      | 159.2335      | 158.4831       | 110.64     | 159.68     | 159.2724        | 159.7331      | 160.9845       | 174.9721      | 158.85        | 159.67      | 159.72331                   |
| G7                                     | 174.3111     | 109.8673      | 159.7630      | 159.6749       | 162.12     | 159.53     | 159.5371        | 159.7330      | 159.1231       | 167.1394      | 157.26        | 159.64      | 159.4163763                 |
| G8                                     | 61.2250      | 159.7342      | 159.6615      | 159.7265       | 163.03     | 158.89     | 158.8522        | 159.7330      | 110.4278       | 116.8800      | 159.93        | 159.65      | 159.6905                    |
| G9                                     | 175.1400     | 159.7340      | 159.4265      | 159.6653       | 161.52     | 110.15     | 159.7845        | 159.7331      | 159.7720       | 116.8800      | 159.86        | 159.78      | 159.7157                    |
| G10                                    | 116.7600     | 114.8012      | 76.8790       | 114.0334       | 117.09     | 77.27      | 110.9618        | 110.0403      | 116.8577       | 116.8800      | 110.78        | 112.46      | 76.2922                     |
| G11                                    | 116.7600     | 114.8001      | 79.5038       | 75             | 75         | 75         | 75              | 114.7994      | 77.0418        | 109.9096      | 75            | 74          | 114.166                     |
| G12                                    | 99.9167      | 92.4018       | 86.8040       | 60             | 60         | 60         | 60              | 55            | 91.4990        | 59.0347       | 60            | 56.50       | 55.00003                    |
| G13                                    | 108.5598     | 55.0027       | 94.1941       | 87.5884        | 119.58     | 55.41      | 91.6401         | 55            | 88.6915        | 66.5129       | 92.62         | 91.64       | 91.30029                    |
| P <sub>Loss</sub><br>(MW)              | NR           | NR            | NR            | NR             | NR         | NR         | NR              | NR            | NR             | NR            | NR            | NR          | 0                           |

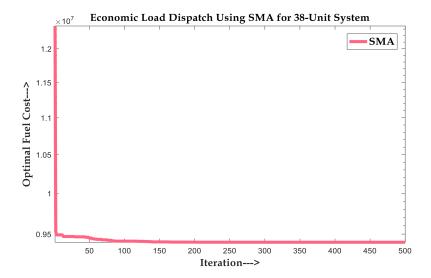
**Table 12.** (Case-IV) Slime mould algorithm results for economic dispatch of a 13-unit system (with valve-point effect).

### 6.3. Test System-III (Large-Scale Power System)

Two test systems were examined in this section, one without valve-point loading and the other with valve-point loading.

### I—Case Study

The input test information was taken from [88] with the loss coefficient matrix set to zero, and a thirty-eight generator test system with a power demand of 6000 MW was evaluated. The input test data are given in Table A13. Table 13 shows that the fuel price using the slime mould algorithm was 9402608.045 Rs./h, which was the best fuel price among all algorithms. The convergence curve of SMA obtained by simulation which was stable is depicted in Figure 11.



**Figure 11.** Convergence curve of slime mould algorithm for economic load dispatch for large-scale power systems (38-generating unit system) without valve-point loading effect.

| Method                                      | Grey Wolf<br>Optimizer<br>(GWO)<br>[88] | Pattern<br>Search<br>(PS) [88] | Biogeography<br>Based Optimization<br>(BBO)<br>[88] | SPSO<br>[109]    | PSO_Crazy<br>[109] | λ-Logic-<br>Based<br>Method [88] | PSO_TVAC<br>[109] | New PSO<br>[109] | Slime<br>Mould<br>Algorithm |
|---|---|--------------------------------|---|------------------|--------------------|----------------------------------|-------------------|------------------|-----------------------------|
| Fuel Price<br>(Rs./h)                       | 9,417,226                               | 9,543,984.8                    | 9,417,633.6   | 9,543,984.777    | 9,520,024.601      | 9,417,235.8                      | 9,500,448.307     | 9,516,448.312    | 9,402,608.045               |
| Required<br>Power in<br>Demand<br>(MW)      | 6000                                    | 6000                           | 6000  | 6000             | 6000               | 6000                             | 6000              | 6000             | 6000                        |
| G1  | 429.7056                                | 258.3397                       | 550   | 519.097          | 366.631            | 426.6061                         | 443.659           | 550.000          | 550                         |
| G2  | 416.2439                                | 258.3397                       | 550   | 437.920          | 550.000            | 426.6061                         | 342.956           | 512.263          | 324.723                     |
| G3  | 408.4052                                | 238.3397                       | 500   | 374.789          | 467.129            | 429.6633                         | 433.117           | 485.733          | 326.8208                    |
| G4  | 412.4527                                | 238.3397                       | 500   | 394.877          | 370.471            | 429.6633                         | 500.000           | 391.083          | 327.2394159                 |
| G5  | 433.6422                                | 238.3397                       | 375.6216  | 356.603          | 425.712            | 429.6633                         | 410.539           | 443.846          | 326.6712585                 |
| G6  | 425.6522                                | 238.3397                       | 200   | 380.358          | 415.226            | 429.6633                         | 482.864           | 358.398          | 326.5721853                 |
| G7  | 435.6207                                | 238.3397                       | 200   | 300.234          | 339.872            | 429.6633                         | 409.483           | 415.729          | 327.0354                    |
| G8  | 437.6536                                | 238.3397                       | 200   | 335.871          | 289.777            | 429.6633                         | 446.079           | 320.816          | 327.5622428                 |
| G9  | 115.2751                                | 196.2345                       | 114   | 238.171          | 195.965            | 114                              | 119.566           | 115.347          | 114                         |
| G10   | 116.883                                 | 196.2345                       | 114.6486  | 218.563          | 170.608            | 114                              | 137.274           | 204.422          | 114                         |
| G11   | 130.7939                                | 196.2345                       | 162.1622  | 196.630          | 138.984            | 119.7681                         | 138.933           | 114.000          | 114                         |
| G12   | 153.2393                                | 196.2345                       | 114   | 234.500          | 262.350            | 127.0729                         | 155.401           | 249.197          | 114                         |
| G13   | 110                                     | 196.2345                       | 129.2432  | 111.529          | 114.008            | 110                              | 121.719           | 118.886          | 110                         |
| G14   | 90.028                                  | 196.2345                       | 90  | 100.731          | 92.393             | 90                               | 90.924            | 102.802          | 90                          |
| G15   | 82.0111                                 | 196.2345                       | 153.2432  | 122.464          | 89.044             | 82                               | 97.941            | 89.039           | 82.00004                    |
| G16   | 120                                     | 196.2345                       | 120   | 125.310          | 130.555            | 120                              | 128.106           | 120.000          | 120.0000328                 |
| G17   | 157.1682                                | 196.2345                       | 204.3243  | 155.981          | 167.850            | 159.5981                         | 189.108           | 156.562          | 147.205372                  |
| G18   | 65                                      | 196.2345                       | 65  | 65.000           | 65.754             | 65                               | 65.000            | 84.265           | 65.00016196                 |
| G19   | 65.0326                                 | 196.2345                       | 65  | 70.071           | 65.000             | 65                               | 65.000            | 65.041           | 65                          |
| G20   | 271.9524                                | 196.2345                       | 120   | 263.950          | 199.594            | 272                              | 267.422           | 151.104          | 272                         |
| G21   | 271.959                                 | 196.2345                       | 182.4324  | 245.065          | 272.000            | 272                              | 221.383           | 226.344          | 272                         |
| G22   | 259.81                                  | 196.2345                       | 110   | 191.702          | 130.379            | 160                              | 130.804           | 209.298          | 260                         |
| G23   | 120.8832                                | 190.2010                       | 187.2973  | 99.123           | 173.544            | 130.6487                         | 124.269           | 85.719           | 96.81893                    |
| G24   | 12.3567                                 | 150                            | 27.027  | 15.058           | 13.263             | 100.0407                         | 11.535            | 10.000           | 10.00006                    |
| G24<br>G25                                  | 107.634                                 | 130                            | 125   | 60.060           | 112.161            | 113.3051                         | 77.103            | 60.000           | 84.92456                    |
| G26   | 92.4117                                 | 110                            | 110   | 91.140           | 105.898            | 88.0669                          | 55.018            | 90.489           | 72.26642                    |
| G20<br>G27                                  | 39.6668                                 | 75                             | 75  | 41.006           | 35.995             | 37.5051                          | 75.000            | 39.670           | 35.00027                    |
| G28   | 20.005                                  | 70                             | 70  | 20.399           | 22.335             | 20                               | 21.682            | 20.000           | 20                          |
| G29   | 20.0014                                 | 70                             | 70  | 34.650           | 30.045             | 20                               | 29.829            | 20.995           | 20.00028                    |
| G29<br>G30                                  | 20.0014                                 | 70                             | 70  | 20.957           | 24.112             | 20                               | 29.329            | 20.995           | 20.00028                    |
| G30<br>G31                                  | 20.0302                                 | 70                             | 70  | 20.937           | 24.112             | 20                               | 20.328            | 22.810           | 20.00006                    |
| G31<br>G32                                  | 20.013                                  | 60                             | 60  | 25.424           | 20.494             | 20                               | 20.000            | 20.000           | 20.00008                    |
| G32<br>G33                                  | 25.0032                                 | 60                             | 60  | 25.424           | 20.011 27.440      | 35                               | 25.620            | 25.000           | 25.00003                    |
| G33<br>G34                                  | 18.008                                  | 60                             | 60  | 18.822           | 18.000             | 18                               | 23.820            | 23.000           | 18                          |
| G34<br>G35                                  | 8.006                                   | 60                             | 60  | 9.173            | 8.024              | 8                                | 9.667             | 9.122            | 8.000021                    |
|   |   |                                |   |                  | 25.000             |                                  |                   |                  |                             |
| G36   | 25.002                                  | 60                             | 60  | 26.507<br>24.344 |                    | 25                               | 25.000            | 25.184           | 25<br>20                    |
| G37<br>G38                                  | 22.4379                                 | 38                             | 38  | 24.344 27.181    | 20.000             | 21                               | 31.642<br>29.935  | 20.000           | 20                          |
| Loss in<br>power, P <sub>Loss</sub><br>(MW) | 20.0048<br>NR                           | NA                             | NR  | NA               | 24.371<br>NA       | NR                               | 29.935<br>NA      | 23.104<br>NA     | 0                           |

**Table 13.** (Case-I) Slime mould algorithm results for economic dispatch of a 38-unit system (without valve-point effect).

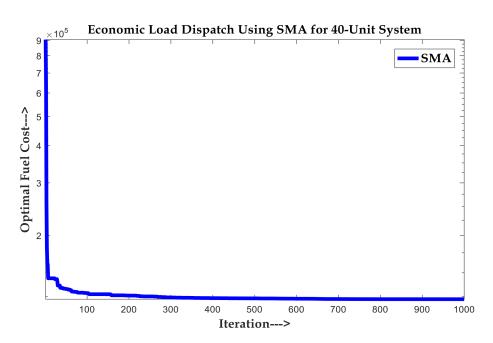
### II—Case Study

With a power demand of 10,500 MW, a forty generator test system with valve-point loading effect was used and the input test information was taken from [108] with the loss coefficient matrix set to zero, which is shown in Table A14. Table 14 shows that when utilizing the slime mould algorithm, the fuel price was 121,658.6656 Rs./h, which was the

best fuel price among other known algorithms. The convergence curve of SMA obtained by simulation which was stable is seen in Figure 12.

**Table 14.** (Case-II) Slime mould algorithm results for economic dispatch of a 40-unit system (with valve-point effect).

| Method                                      | MPSO<br>[108] | GWO<br>[108] | NGWO<br>[108] | PSO-LRS<br>[108] | IGA<br>[108] | NPSO<br>[108] | GWOII<br>[108] | CJAYA<br>[108] | GWOI<br>[108] | Slime<br>Mould<br>Algorithm |
|---|---------------|--------------|---------------|------------------|--------------|---------------|----------------|----------------|---------------|-----------------------------|
| Fuel Price<br>(Rs./h)                       | 122,252.265   | 122,602.37   | 121,881.81    | 122,035.7946     | 121,915.93   | 121,704.7391  | 122,430.74     | 122,581.85     | 122,678.91    | 121,658.6656                |
| Required<br>Power in<br>Demand<br>(MW)      | 10,500        | 10,500       | 10,500        | 10,500           | 10,500       | 10,500        | 10,500         | 10,500         | 10,500        | 10,500                      |
| G1  | 114           | 109.0947     | 111.3177      | 111.9858         | 110.97       | 113.9891      | 107.6544       | 114            | 109.7268      | 112.3525188                 |
| G2  | 114           | 112.0471     | 112.7551      | 110.5273         | 110.88       | 113.6334      | 109.2161       | 111.6651       | 111.7342      | 112.4688984                 |
| G3  | 120           | 115.4584     | 118.6377      | 98.5560          | 98.17        | 97.5500       | 94.7874        | 119.9876       | 119.2197      | 97.49149956                 |
| G4  | 182.222       | 179.8333     | 183.3649      | 182.9622         | 178.85       | 180.0059      | 182.3441       | 188.2606       | 181.6041      | 179.7415579                 |
| G5  | 97            | 46.1649      | 91.8097       | 87.7254          | 87.78        | 97            | 86.9731        | 96.9763        | 89.8836       | 93.71705917                 |
| G6  | 140           | 83.1571      | 104.3697      | 139.9933         | 140          | 140           | 109.1907       | 139.9488       | 125.1816      | 139.99945                   |
| G7  | 300           | 261.6345     | 297.6533      | 259.6628         | 260.37       | 300           | 259.4910       | 264.0949       | 265.0775      | 260.4361978                 |
| G8  | 299.021       | 292.4025     | 289.4349      | 297.7912         | 286.83       | 300           | 284.1803       | 299.9814       | 290.2216      | 289.743                     |
| G9  | 300           | 284.7149     | 298.4044      | 284.8459         | 285.14       | 284.5797      | 285.1526       | 284.9042       | 285.2586      | 296.0535                    |
| G10   | 130           | 132.9049     | 129.35        | 130              | 204.86       | 130.0517      | 129.3500       | 130.0908       | 134.9231      | 130.0189                    |
| G11   | 94            | 101.6726     | 241.9702      | 94.6741          | 165.98       | 243.7131      | 317.4787       | 94.0011        | 167.9983      | 168.7887                    |
| G12   | 94            | 319.8174     | 166.9113      | 94.3734          | 167.75       | 169.0104      | 157.3563       | 94             | 183.6314      | 168.7212                    |
| G13   | 125           | 215.0746     | 214.849       | 214.7369         | 214.31       | 125           | 300.6095       | 125.1028       | 219.5396      | 125.0003                    |
| G14   | 304.485       | 394.9259     | 215.669       | 394.1370         | 305.65       | 393.9662      | 305.0848       | 394.2529       | 394.9259      | 394.2872                    |
| G15   | 394.607       | 398.1829     | 305.69        | 483.1816         | 393.66       | 304.7586      | 395.3099       | 484.1262       | 212.7154      | 304.5919403                 |
| G16   | 305.323       | 304.1546     | 394.6479      | 304.5381         | 394.60       | 304.5120      | 203.9544       | 304.5950       | 484.5572      | 394.3118                    |
| G10<br>G17                                  | 490.272       | 490.0842     | 494.7618      | 489.2139         | 489.22       | 489.6024      | 489.6721       | 490.8265       | 494.3478      | 489.2914608                 |
| G18   | 500           | 493.2515     | 493.1559      | 489.6154         | 489.25       | 489.6087      | 492.3490       | 489.3438       | 491.2367      | 489.881                     |
| G10<br>G19                                  | 511.404       | 511.4229     | 512.7416      | 511.1782         | 511.23       | 511.7903      | 514.3882       | 51.3775        | 514.3755      | 511.2385                    |
| G19<br>G20                                  | 512.174       | 511.9422     | 520.8929      | 511.7336         | 510.69       | 511.2624      | 511.7323       | 512.1395       | 514.3755      | 511.2866                    |
| G20<br>G21                                  | 550           | 532.3762     | 526.1137      | 523.4072         | 524.74       | 523.3274      | 532.2046       | 523.6621       | 514.3733      | 523.3004                    |
| G21<br>G22                                  | 523.655       | 532.2484     | 532.1443      | 523.4599         | 525.52       | 523.2196      | 527.3193       |                |               | 523.2929                    |
|   |               |              |               |                  |              |               |                | 523.3534       | 523.6988      |                             |
| G23   | 534.661       | 530.7732     | 536.8421      | 523.4756         | 522.98       | 523.4707      | 527.3193       | 524.9677       | 523.6988      | 523.3215                    |
| G24   | 550           | 526.1112     | 524.4669      | 523.7032         | 522.22       | 523.0661      | 539.9336       | 524.2850       | 536.1385      | 523.2599                    |
| G25   | 525.057       | 524.4545     | 525.2461      | 523.7854         | 523.26       | 523.3978      | 526.6306       | 522.9279       | 523.5451      | 523.3046                    |
| G26   | 549.155       | 523.4934     | 529.3289      | 523.2757         | 523.32       | 523.2897      | 524.8658       | 523.2298       | 524.0780      | 523.2675                    |
| G27   | 10            | 11.5028      | 9.95          | 10               | 10           | 10.0208       | 9.95           | 10             | 14.8568       | 10.00489                    |
| G28   | 10            | 9.9541       | 9.95          | 10.6251          | 10           | 10.0927       | 9.95           | 10.0047        | 21.0962       | 10                          |
| G29   | 10            | 10.3272      | 9.95          | 10.0727          | 10           | 10.0621       | 9.95           | 10             | 13.1286       | 10.00001                    |
| G30   | 97            | 91.6019      | 88.4106       | 51.3321          | 88.86        | 88.9456       | 90.3385        | 97             | 88.5089       | 92.73674                    |
| G31   | 190           | 188.8475     | 188.9088      | 189.8048         | 162.30       | 189.9951      | 159.6875       | 190            | 188.0180      | 189.9981                    |
| G32   | 190           | 165.2531     | 188.8126      | 189.7386         | 177.94       | 190           | 188.9923       | 189.9503       | 166.2968      | 190                         |
| G33   | 190           | 188.9197     | 186.9624      | 189.9122         | 160.18       | 190           | 173.1974       | 190            | 182.0808      | 190                         |
| G34   | 200           | 189.2968     | 195.0897      | 199.3258         | 166.54       | 165.9825      | 189.6808       | 169.8860       | 164.9636      | 195.8292                    |
| G35   | 200           | 180.4605     | 171.5047      | 199.3065         | 164.80       | 172.4153      | 192.1671       | 199.8549       | 172.6948      | 200                         |
| G36   | 200           | 184.2698     | 176.1085      | 192.8977         | 170.68       | 191.2978      | 157.5027       | 199.9896       | 191.0765      | 200                         |
| G37   | 110           | 89.6748      | 89.5297       | 110              | 108.17       | 109.9893      | 104.4095       | 109.9712       | 108.8942      | 89.89076                    |
| G38   | 110           | 90.1485      | 89.3589       | 109.8628         | 100.68       | 109.9521      | 86.74132       | 109.9977       | 100.8804      | 91.73751                    |
| G39   | 110           | 57.0464      | 109.3222      | 92.8751          | 109.34       | 109.8733      | 100.2970       | 109.9871       | 27.8744       | 109.9905                    |
| G40   | 512.964       | 514.3622     | 512.5412      | 511.6883         | 511.28       | 511.5671      | 512.43873      | 511.2250       | 511.7717      | 511.2371                    |
| Loss in<br>Power, P <sub>Loss</sub><br>(MW) | NR            | NR           | NR            | NR               | NR           | NR            | NR             | NR             | NR            | 0                           |

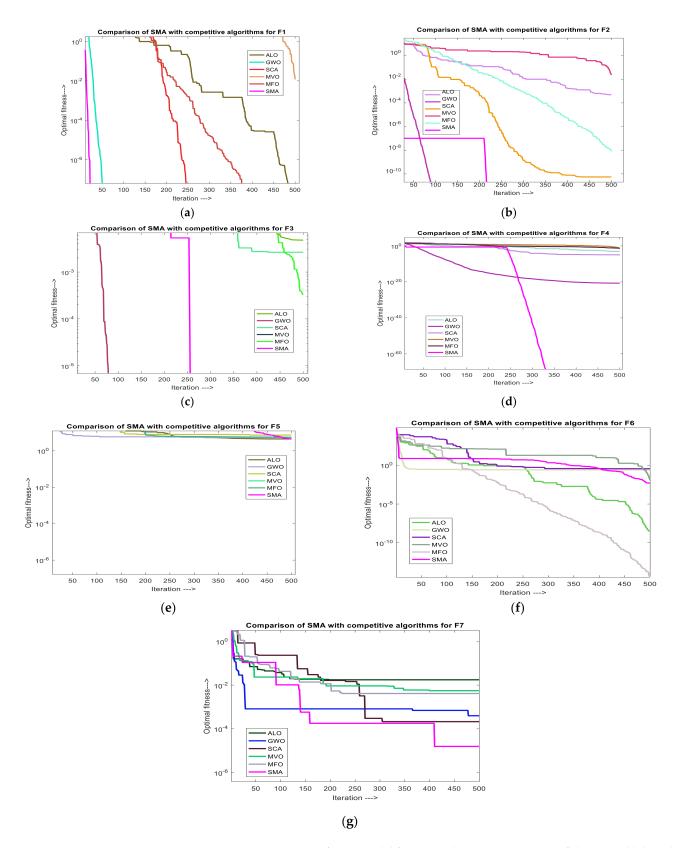


**Figure 12.** Convergence curve of slime mould algorithm for economic load dispatch for large-scale power systems (40-generating unit system) with valve-point loading effect.

It can be observed that the SMA technique reported minimum fuel cost when compared with other methods. Thus, the proposed SMA method presented an excellent performance compared to the competition. As per the condition considered in solving the ED problem, it has been proven that the SMA technique was best suited for all cases and situations in this paper.

In order to intuitively analyze the location and fitness changes of the slime mould during foraging, the qualitative analysis findings of SMA in lowering the fuel cost in economic load dispatch are provided in Figures 7–12. During the iteration phase, the convergence curve reveals the ideal fitness value in the slime mould. The convergence curve shows how the average fitness of the slime mould's ideal fitness value changes over time. We can see the slime mould's convergence rate and the moment when it transitions between exploration and exploration gradation by looking at the decline of the curve.

On an Intel Core i3, 7th Gen, with 8GB RAM, the suggested SMA method was tested. The capacity of the search agents to get closer to the origin determines the search procedure for the best position. During the search process by various agents, there is a chance of being entrapped far or near, which is characterized in terms of exploration and exploitation. The suggested algorithm's stochastic nature was justified and studied by running it for 30 maximum runs and 500 iterations. The approach was tested on typical benchmark functions, and it was shown that it increases the rate of convergence and has a high capacity to escape from local minima. The convergence rate was higher than that of other globally certified systems, and the system outperformed them. A comparison of SMA and other approaches is shown in Figure 13, and it was observed that the convergence curves of unimodal benchmark functions show that the proposed approach reaches the optimal state substantially sooner.



**Figure 13.** Convergence curve for unimodal functions showing comparison of slime mouldalgorithm) with other existing algorithms, (**a**) Convergence curve for F1 function, (**b**) Convergence curve for F2 function, (**c**) Convergence curve for F3 function, (**d**) Convergence curve for F4 function, (**e**) Convergence curve for F5 function, (**f**) Convergence curve for F6 function, (**g**) Convergence curve for F7 function.

### 7. Conclusions

The slime mould optimization technique was utilized in this paper to tackle economic load dispatch problems in electric power networks. The proficiency of this method was studied on standard IEEE bus systems of 3-, 5-, 6-, 10-, 13-, 15-, 20-, 38-, and 40-generating unit systems under small-, medium-, and large-sized power systems. According to the data, the slime mould optimizer is obviously best appropriate to handle economic load dispatch problems due to its lower fuel costs and minimal transmission loss. Its convergence rate was greater than that of other well-known optimizers. The slime mould optimizer achieves maximum avoidance in the local optimum by striking a balance between exploration and exploitation. As a result, this algorithm delivers better solutions for economic load dispatch issues. It has the potential to be utilized in the future to solve economic load dispatch problems in multiple areas and in a variety of sectors.

**Author Contributions:** Conceptualization, V.K.K.; methodology, S.K.B.; validation, D.P. and M.R.; formal analysis, V.K.K.; writing—original draft preparation, C.L.K.; writing—review and editing, M.R.; supervision, S.S.A.; funding acquisition, A.S.A. All authors have read and agreed to the published version of the manuscript.

**Funding:** This study was funded by the Deanship of Scientific Research, Taif University Researchers Supporting Project number (TURSP-2020/311), Taif University, Taif, Saudi Arabia.

Institutional Review Board Statement: Not applicable.

Informed Consent Statement: Not applicable.

**Data Availability Statement:** Data used in this manuscript can be shared by making a request to the corresponding author.

Conflicts of Interest: The authors declare no conflict of interest.

### Abbreviations

 $P^g$  = Generating units' output power;  $P_n^g$  = the active power of the *n*th generator; ng = number of generators in total;  $a_n$ ,  $b_n$ ,  $c_n$  are the fuel coefficients for power producing units;  $fc(P^g)$  = the total cost of fuel for all power plants;  $P^d$ ,  $P^l$  are total power demand and system power loss;  $dr_n$ ,  $ur_n$  are the lower and upper ranges of *n*th generator unit ramp rate limitations;  $B_{i0}$ ,  $B_{00}$  are the loss coefficient matrices;  $P_n^{g_0}$  is the current active power of the *n*th generation unit.

### Appendix A

| Total Units | Fotal Units P <sub>min</sub><br>(MW) |     | c (\$/h) b (\$/MWh) |       | P <sub>max</sub> (MW) |  |
|-------------|--------------------------------------|-----|---------------------|-------|-----------------------|--|
| 1           | 10                                   | 200 | 7.00                | 0.008 | 85                    |  |
| 2           | 10                                   | 180 | 6.3                 | 0.009 | 80                    |  |
| 3           | 10                                   | 140 | 6.8                 | 0.007 | 70                    |  |

Table A1. Data for the 3-unit generator test system.

Matrix of Transmission loss coefficient for three-unit system:

|                  |        |  | 0.0218 | 0.0093 | 0.0028 |  |
|------------------|--------|--|--------|--------|--------|--|
| $B_0 = [0.0003]$ | 0.0031 | 0.0015 ]; $B_{00} = [0.00030523]; B = 10^{-3}$ | 0.0093 | 0.0228 | 0.0017 |  |
| -                |        | -  | 0.0028 | 0.0017 | 0.0179 |  |

| Total Units | P <sub>min</sub><br>(MW) | c<br>(\$/h) | b<br>(\$/MWh) | a<br>(\$/(MW) <sup>2</sup> h) | P <sub>max</sub><br>(MW) |
|-------------|--------------------------|-------------|---------------|-------------------------------|--------------------------|
| 1           | 10                       | 200         | 7.02          | 0.00816                       | 85                       |
| 2           | 10                       | 180         | 6.35          | 0.00900                       | 80                       |
| 3           | 10                       | 140         | 6.97          | 0.00782                       | 70                       |

Table A2. Data for the 3-unit generator test system.

Matrix of Transmission loss coefficient for 3-unit system:

|                  |        | 0.0015 ]; $B_{00} = [0.00030523]; B = 10^{-3}$ | 0.0218 | 0.0093 | 0.0028 ] |
|------------------|--------|--|--------|--------|----------|
| $B_0 = [0.0003]$ | 0.0031 | 0.0015 ]; $B_{00} = [0.00030523]; B = 10^{-3}$ | 0.0093 | 0.0228 | 0.0017   |
| -                |        | -  | 0.0028 | 0.0017 | 0.0179   |

Table A3. Data for the 3-unit generator test system.

| Total Units | P <sub>min</sub><br>(MW) | c<br>(\$/h) | b<br>(\$/MWh) | a<br>(\$/(MW) <sup>2</sup> h) | P <sub>max</sub><br>(MW) |
|-------------|--------------------------|-------------|---------------|-------------------------------|--------------------------|
| 1           | 10                       | 200         | 7.02          | 0.00816                       | 85                       |
| 2           | 10                       | 180         | 6.35          | 0.00900                       | 80                       |
| 3           | 10                       | 140         | 6.97          | 0.00782                       | 70                       |

Matrix of Transmission loss coefficient for 3-unit system:

|  |        |  | 0.0218 | 0.0093 | 0.0028 ] |
|--|--------|--|--------|--------|----------|
| $B_0 = \begin{bmatrix} 0.0003 \end{bmatrix}$ | 0.0031 | $0.0015$ ]; $B_{00} = [0.00030523]; B = 10^{-3}$ | 0.0093 | 0.0228 | 0.0017   |
| -  |        | 0.0015 ]; $B_{00} = [0.00030523]; B = 10^{-3}$   | 0.0028 | 0.0017 | 0.0179   |

Table A4. Data for the 3-unit generator test system.

| Total Units | P <sub>min</sub> (MW) | c<br>(\$/h) | b<br>(\$/MWh) | a<br>(\$/(MW) <sup>2</sup> h) | P <sub>max</sub><br>(MW) |
|-------------|-----------------------|-------------|---------------|-------------------------------|--------------------------|
| 1           | 50                    | 328.13      | 8.663         | 0.00525                       | 250                      |
| 2           | 5                     | 136.91      | 10.04         | 0.00609                       | 150                      |
| 3           | 15                    | 59.16       | 9.76          | 0.00592                       | 100                      |

Matrix of Transmission loss coefficient for 3-unit system:

$$B_0 = \begin{bmatrix} 0 & 0 & 0 \end{bmatrix}; B_{00} = \begin{bmatrix} 0 \end{bmatrix}; B = \begin{bmatrix} 0.000136 & 0.0000175 & 0.000184 \\ 0.000175 & 0.0001540 & 0.000283 \\ 0.000184 & 0.0002830 & 0.001610 \end{bmatrix}$$

| Total Units | P <sub>min</sub><br>(MW) | c<br>(\$/h) | b<br>(\$/MWh) | a<br>(\$/(MW) <sup>2</sup> h) | P <sub>max</sub><br>(MW) |
|-------------|--------------------------|-------------|---------------|-------------------------------|--------------------------|
| 1           | 100                      | 240         | 7.0           | 0.0070                        | 500                      |
| 2           | 50                       | 200         | 10.0          | 0.0095                        | 200                      |
| 3           | 80                       | 220         | 8.5           | 0.0090                        | 300                      |
| 4           | 50                       | 200         | 11.0          | 0.0090                        | 150                      |
| 5           | 50                       | 220         | 10.5          | 0.0080                        | 200                      |
| 6           | 50                       | 190         | 12.0          | 0.0075                        | 120                      |

Table A5. Data for the 6-unit generator test system.

Table A6. Data for the 6-unit generator test system.

| Total Units | P <sub>min</sub><br>(MW) | c<br>(\$/h) | b<br>(\$/MWh) | a<br>(\$/(MW) <sup>2</sup> h) | P <sub>max</sub><br>(MW) |
|-------------|--------------------------|-------------|---------------|-------------------------------|--------------------------|
| 1           | 10                       | 756.79886   | 38.53973      | 0.15240                       | 125                      |
| 2           | 10                       | 451.32513   | 46.15916      | 0.10587                       | 150                      |
| 3           | 35                       | 1049.9977   | 40.39655      | 0.02803                       | 225                      |
| 4           | 35                       | 1243.5311   | 38.30553      | 0.03546                       | 210                      |
| 5           | 130                      | 1658.5596   | 36.32782      | 0.02111                       | 325                      |
| 6           | 125                      | 1356.6592   | 38.27041      | 0.01799                       | 315                      |

Matrix of Transmission loss coefficient for 6-unit system:

$$B_{0} = \begin{bmatrix} 0 & 0 & 0 \end{bmatrix}; B_{00} = [0]; B = \begin{bmatrix} 0.000140 & 0.00017 & 0.00015 & 0.00019 & 0.00026 & 0.00022 \\ 0.000017 & 0.000060 & 0.00013 & 0.00016 & 0.00015 & 0.00020 \\ 0.000015 & 0.000013 & 0.00065 & 0.000017 & 0.00024 & 0.000019 \\ 0.000019 & 0.000016 & 0.000017 & 0.000071 & 0.000030 & 0.000025 \\ 0.000026 & 0.000015 & 0.000024 & 0.000032 & 0.000032 \\ 0.000022 & 0.000020 & 0.000019 & 0.000025 & 0.000032 & 0.000085 \end{bmatrix}$$

Table A7. Data for the 3-unit generator test system.

| Total Units | P <sub>min</sub><br>(MW) | e<br>(1/MW) | d<br>(\$/h) | c<br>(\$/hr) | b<br>(\$/MWh) | a<br>(\$/(MW) <sup>2</sup> h) | P <sub>max</sub><br>(MW) |
|-------------|--------------------------|-------------|-------------|--------------|---------------|-------------------------------|--------------------------|
| 1           | 100                      | 0.0315      | 300         | 561          | 7.92          | 0.001562                      | 600                      |
| 2           | 100                      | 0.042       | 200         | 310          | 7.85          | 0.00194                       | 400                      |
| 3           | 50                       | 0.063       | 150         | 78           | 7.97          | 0.00482                       | 200                      |

**Table A8.** Data for the 5-unit generator test system.

| Total Units | P <sub>min</sub><br>(MW) | e<br>(1/MW) | d<br>(\$/h) | c<br>(\$/hr) | b<br>(\$/MWh) | a<br>(\$/(MW) <sup>2</sup> h) | P <sub>max</sub><br>(MW) |
|-------------|--------------------------|-------------|-------------|--------------|---------------|-------------------------------|--------------------------|
| 1           | 50                       | 0.035       | 200.0       | 40.0         | 1.8           | 0.0015                        | 300                      |
| 2           | 20                       | 0.040       | 140.0       | 60.0         | 1.8           | 0.0035                        | 125                      |
| 3           | 30                       | 0.038       | 160.0       | 100.0        | 2.1           | 0.0012                        | 175                      |
| 4           | 10                       | 0.042       | 100.0       | 25.0         | 2.0           | 0.0080                        | 75                       |
| 5           | 40                       | 0.037       | 180.0       | 120.0        | 2.0           | 0.0010                        | 250                      |

| ]   | 1.4  | 1.2  | 0.7   | -0.1   | -0.3   | -0.1   | -0.1   | -0.1 | -0.3 | -0.5 | -0.3  | -0.2 | 0.4   | 0.3   | -0.1  |
|---|------|------|-------|--------|--------|--------|--------|------|------|------|-------|------|-------|-------|-------|
|   | 1.2  | 1.5  | 1.3   | 0.0    | -0.5   | -0.2   | 0.0    | 0.1  | -0.2 | -0.4 | -0.4  | 0.0  | 0.4   | 1.0   | -0.2  |
|   | 0.7  | 1.3  | 7.6   | -0.1   | -1.3   | -0.9   | -0.1   | 0.0  | -0.8 | -1.2 | -1.7  | 0.0  | -2.6  | 11.1  | -2.8  |
|   | -0.1 | 0.0  | -0.1  | 3.4    | -0.7   | -0.4   | 1.1    | 5.0  | 2.9  | 3.2  | -1.1  | 0.0  | 0.1   | 0.1   | -2.6  |
|   | -0.3 | -0.5 | -1.3  | -0.7   | 9.0    | 1.4    | -0.3   | -1.2 | -1.0 | -1.3 | 0.7   | -0.2 | -0.2  | -2.4  | -0.3  |
|   | -0.1 | -0.2 | -0.9  | -0.4   | 1.4    | 1.6    | 0.0    | -0.6 | -0.5 | -0.8 | 1.1   | -0.1 | -0.2  | -1.7  | 0.3   |
|   | -0.1 | 0.0  | -0.1  | 1.1    | -0.3   | 0.0    | 1.5    | 1.7  | 1.5  | 0.9  | -0.5  | 0.7  | 0.0   | -0.2  | -0.8  |
| $B_{00} = [0.0055]; B = 10^{-3}$                          | -0.1 | 0.1  | 0.0   | 5.0    | -1.2   | -0.6   | 1.7    | 16.8 | 8.2  | 7.9  | -2.3  | -3.6 | 0.0   | 0.5   | -7.8  |
|   | -0.3 | -0.2 | -0.8  | 2.9    | -1.0   | -0.5   | 1.5    | 8.2  | 12.9 | 11.6 | -2.1  | -2.5 | 0.7   | -1.2  | -7.2  |
|   | -0.5 | -0.4 | -1.2  | 3.2    | -1.3   | -0.8   | 0.9    | 7.9  | 11.6 | 20.0 | -2.7  | -3.4 | 0.9   | -1.1  | -8.8  |
|   | -0.3 | -0.4 | -1.7  | -1.1   | 0.1    | 1.1    | -0.5   | -2.3 | -2.1 | -2.7 | 14.0  | 0.1  | 0.4   | -3.8  | 16.8  |
|   | -0.2 | 0.0  | 0.0   | 0.0    | -0.2   | -0.1   | 0.7    | -3.6 | -2.5 | -3.4 | 0.1   | 5.4  | -0.1  | -0.4  | 2.8   |
|   | 0.4  | 0.4  | -2.6  | 0.1    | -0.2   | -0.2   | 0.0    | 0.0  | 0.7  | 0.9  | 0.4   | -0.1 | 10.3  | -10.1 | 2.8   |
|   | 0.3  | 1.0  | 11.1  | 0.1    | -2.4   | -1.7   | -0.2   | 0.5  | -1.2 | -1.1 | -3.8  | -0.4 | -10.1 | 57.8  | -9.4  |
| l   | -0.1 | -0.2 | -2.8  | -2.6   | -0.3   | 0.3    | -0.8   | -7.8 | -7.2 | -8.8 | 16.8  | 2.8  | 2.8   | -9.4  | 128.3 |
| $B_0 = 10^{-3} \begin{bmatrix} -0.1 & -0.2 \end{bmatrix}$ | 2.8  | -0.1 | 0.1 – | -0.3 – | -0.2 – | 0.2 0. | .6 3.9 | -1.7 | 0.0  | -3.2 | 6.7 – | 6.4  |       |       |       |

# Matrix of Transmission loss coefficient for 15-unit system:

 Table A9. Data for the 15-unit generator test system.

| Total Units | P <sub>min</sub><br>(MW) | c<br>(\$/h) | b<br>(\$/MWh) | a<br>(\$/(MW) <sup>2</sup> h) | P <sub>max</sub><br>(MW) |
|-------------|--------------------------|-------------|---------------|-------------------------------|--------------------------|
| 1           | 150                      | 671         | 10.1          | 0.000299                      | 455                      |
| 2           | 150                      | 574         | 10.2          | 0.000183                      | 455                      |
| 3           | 20                       | 374         | 8.8           | 0.001126                      | 130                      |
| 4           | 20                       | 374         | 8.8           | 0.001126                      | 130                      |
| 5           | 150                      | 461         | 10.4          | 0.000205                      | 470                      |
| 6           | 135                      | 630         | 10.1          | 0.000301                      | 460                      |
| 7           | 135                      | 548         | 9.8           | 0.000364                      | 465                      |
| 8           | 60                       | 227         | 11.2          | 0.000338                      | 300                      |
| 9           | 25                       | 173         | 11.2          | 0.000807                      | 162                      |
| 10          | 25                       | 175         | 10.7          | 0.001203                      | 160                      |
| 11          | 20                       | 186         | 10.2          | 0.003586                      | 80                       |
| 12          | 20                       | 230         | 9.9           | 0.005513                      | 80                       |
| 13          | 25                       | 225         | 13.1          | 0.000371                      | 85                       |
| 14          | 15                       | 309         | 12.1          | 0.001929                      | 55                       |
| 15          | 15                       | 323         | 12.4          | 0.004447                      | 55                       |

| ſ             | 8.70  | 0.43  | -4.61 | 0.36  | 0.32  | -0.66 | 0.96  | -1.60 | 0.80  | -0.10 | 3.60  | 0.64  | 0.79  | 2.10  | 1.70  | 0.80  | -3.20 | 0.70  | 0.48  | -0.70 |  |
|---------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--|
|               | 0.43  | 8.30  | -0.97 | 0.22  | 0.75  | -0.28 | 5.04  | 1.70  | 0.54  | 7.20  | -0.28 | 0.98  | -0.46 | 1.30  | 0.80  | -0.20 | 0.52  | -1.70 | 0.80  | 0.20  |  |
|               | -4.61 | -0.97 | 9.00  | -2.00 | 0.63  | 3.00  | 1.70  | -4.30 | 3.10  | -2.00 | 0.70  | -0.77 | 0.93  | 4.60  | -0.30 | 4.20  | 0.38  | 0.70  | -2.00 | 3.60  |  |
|               | 0.36  | 0.22  | -2.00 | 5.30  | 0.47  | 2.62  | -1.96 | 2.10  | 0.67  | 1.80  | -0.45 | 0.92  | 2.40  | 7.60  | -0.20 | 0.70  | -1.00 | 0.86  | 1.60  | 0.87  |  |
|               | 0.32  | 0.75  | 0.63  | 0.47  | 8.60  | -0.80 | 0.37  | 0.72  | -0.90 | 0.69  | 1.80  | 4.30  | -2.80 | -0.70 | 2.30  | 3.60  | 0.80  | 0.20  | -3.00 | 0.50  |  |
|               | -0.66 | -0.28 | 3.00  | 2.62  | -0.80 | 11.8  | -4.90 | 0.30  | 3.00  | -3.00 | 0.40  | 0.78  | 6.40  | 2.60  | -0.20 | 2.10  | -0.40 | 2.30  | 1.60  | -2.10 |  |
|               | 0.96  | 5.04  | 1.70  | -1.96 | 0.37  | -4.90 | 8.24  | -0.90 | 5.90  | -0.60 | 8.50  | -0.83 | 7.20  | 4.80  | -0.90 | -0.10 | 1.30  | 0.76  | 1.90  | 1.30  |  |
|               | -1.60 | 1.70  | -4.30 | 2.10  | 0.72  | 0.30  | -0.90 | 1.20  | -0.96 | 0.56  | 1.60  | 0.80  | -0.40 | 0.23  | 0.75  | -0.56 | 0.80  | -0.30 | 5.30  | 0.80  |  |
|               | 0.80  | 0.54  | 3.10  | 0.67  | -0.90 | 3.00  | 5.90  | -0.96 | 0.93  | -0.30 | 6.50  | 2.30  | 2.60  | 0.58  | -0.10 | 0.23  | -0.30 | 1.50  | 0.74  | 0.70  |  |
| $B = 10^{-3}$ | -0.10 | 7.20  | -2.00 | 1.80  | 0.69  | -3.00 | -0.60 | 0.56  | -0.30 | 0.99  | -6.60 | 3.90  | 2.30  | -0.30 | 2.80  | -0.80 | 0.38  | 1.90  | 0.47  | -0.26 |  |
|               | 3.60  | -0.28 | 0.70  | -0.45 | 1.80  | 0.40  | 8.50  | 1.60  | 6.50  | -6.60 | 10.7  | 5.30  | -0.60 | 0.70  | 1.90  | -2.60 | 0.93  | -0.60 | 3.80  | -1.50 |  |
|               | 0.64  | 0.98  | -0.77 | 0.92  | 4.30  | 0.78  | -0.83 | 0.80  | 2.30  | 3.90  | 5.30  | 8.00  | 0.90  | 2.10  | -0.70 | 5.70  | 5.40  | 1.50  | 0.70  | 0.10  |  |
|               | 0.79  | -0.46 | 0.93  | 2.40  | -2.80 | 6.40  | 7.20  | -0.40 | 2.60  | 2.30  | -0.60 | 0.90  | 11.0  | 0.87  | -1.00 | 3.60  | 0.46  | -0.90 | 0.60  | 1.50  |  |
|               | 2.10  | 1.30  | 4.60  | 7.60  | -0.70 | 2.60  | 4.80  | 0.23  | 0.58  | -0.30 | 0.70  | 2.10  | 0.87  | 3.80  | 0.50  | -0.70 | 1.90  | 2.30  | -0.97 | 0.90  |  |
|               | 1.70  | 0.80  | -0.30 | -0.20 | 2.30  | -0.20 | -0.90 | 0.75  | -0.10 | 2.80  | 1.90  | -0.70 | -1.00 | 0.50  | 11.0  | 1.90  | -0.80 | 2.60  | 2.30  | -0.10 |  |
|               | 0.80  | -0.20 | 4.20  | 0.70  | 3.60  | 2.10  | -0.10 | -0.56 | 0.23  | -0.80 | -2.60 | 5.70  | 3.60  | -0.70 | 1.90  | 10.8  | 2.50  | -1.80 | 0.90  | -2.60 |  |
|               | -3.20 | 0.52  | 0.38  | -1.00 | 0.80  | -0.40 | 1.30  | 0.80  | -0.30 | 0.38  | 0.93  | 5.40  | 0.46  | 1.90  | -0.80 | 2.50  | 8.70  | 4.20  | -0.30 | 0.68  |  |
|               | 0.70  | -1.70 | 0.70  | 0.86  | 0.20  | 2.30  | 0.76  | -0.30 | 1.50  | 1.90  | -0.60 | 1.50  | -0.90 | 2.30  | 2.60  | -1.80 | 4.20  | 2.20  | 0.16  | -0.30 |  |
|               | 0.48  | 0.80  | -2.00 | 1.60  | -3.00 | 1.60  | 1.90  | 5.30  | 0.74  | 0.47  | 3.80  | 0.70  | 0.60  | -0.97 | 2.30  | 0.90  | -0.30 | 0.16  | 7.60  | 0.69  |  |
| l             | -0.70 | 0.20  | 3.60  | 0.87  | 0.50  | -2.10 | 1.30  | 0.80  | 0.70  | -0.26 | -1.50 | 0.10  | 1.50  | 0.90  | -0.10 | -2.60 | 0.68  | -0.30 | 0.69  | 7.00  |  |
|               |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |  |

# Matrix of Transmission loss coefficient for 20-unit system:

Table A10. Data for the 20-unit generator test system.

| Total Units | P <sub>min</sub><br>(MW) | c<br>(\$/h) | b<br>(\$/MWh) | a<br>(\$/(MW) <sup>2</sup> h) | P <sub>max</sub> (MW) |
|-------------|--------------------------|-------------|---------------|-------------------------------|-----------------------|
| 1           | 150                      | 1000        | 18.19         | 0.00068                       | 600                   |
| 2           | 50                       | 970         | 19.26         | 0.00071                       | 200                   |
| 3           | 50                       | 600         | 19.80         | 0.00650                       | 200                   |
| 4           | 50                       | 700         | 19.10         | 0.00500                       | 200                   |
| 5           | 50                       | 420         | 18.10         | 0.00738                       | 160                   |
| 6           | 20                       | 360         | 19.26         | 0.00612                       | 100                   |
| 7           | 25                       | 490         | 17.14         | 0.00790                       | 125                   |
| 8           | 50                       | 660         | 18.92         | 0.00813                       | 150                   |
| 9           | 50                       | 765         | 18.27         | 0.00522                       | 200                   |
| 10          | 30                       | 770         | 18.92         | 0.00573                       | 150                   |
| 11          | 100                      | 800         | 16.69         | 0.00480                       | 300                   |
| 12          | 150                      | 970         | 16.76         | 0.00310                       | 500                   |
| 13          | 40                       | 900         | 17.36         | 0.00850                       | 160                   |
| 14          | 20                       | 700         | 18.70         | 0.00511                       | 130                   |
| 15          | 25                       | 450         | 18.70         | 0.00398                       | 185                   |
| 16          | 20                       | 370         | 14.26         | 0.07120                       | 80                    |
| 17          | 30                       | 480         | 19.14         | 0.00890                       | 85                    |
| 18          | 30                       | 680         | 18.92         | 0.00713                       | 120                   |
| 19          | 40                       | 700         | 18.47         | 0.00622                       | 120                   |
| 20          | 30                       | 850         | 19.79         | 0.00773                       | 100                   |

| Total Units | P <sub>min</sub><br>(MW) | e<br>(1/MW) | d<br>(\$/h) | c<br>(\$/hr) | b<br>(\$/MWh) | a<br>(\$/(MW) <sup>2</sup> h) | P <sub>max</sub><br>(MW) |
|-------------|--------------------------|-------------|-------------|--------------|---------------|-------------------------------|--------------------------|
| 1           | 10                       | 0.0174      | 33          | 1000.403     | 40.5407       | 0.12951                       | 55                       |
| 2           | 20                       | 0.0178      | 25          | 950.606      | 39.5804       | 0.10908                       | 80                       |
| 3           | 47                       | 0.0162      | 32          | 900.705      | 36.5104       | 0.12511                       | 120                      |
| 4           | 20                       | 0.0168      | 30          | 800.705      | 39.5104       | 0.12111                       | 130                      |
| 5           | 50                       | 0.0148      | 30          | 756.799      | 38.539        | 0.15247                       | 160                      |
| 6           | 70                       | 0.0163      | 20          | 451.325      | 46.1592       | 0.10587                       | 240                      |
| 7           | 60                       | 0.0152      | 20          | 1243.531     | 38.3055       | 0.03546                       | 300                      |
| 8           | 70                       | 0.0128      | 30          | 1049.998     | 40.3965       | 0.02803                       | 340                      |
| 9           | 135                      | 0.0136      | 60          | 1658.569     | 36.3278       | 0.02111                       | 470                      |
| 10          | 150                      | 0.0141      | 40          | 1356.659     | 38.2704       | 0.01799                       | 470                      |

 Table A11. Data for the 10-unit generator test system.

 Table A12. Data for the 13-unit generator test system.

| Total Units | P <sub>min</sub><br>(MW) | e<br>(1/MW) | d<br>(\$/h) | c<br>(\$/hr) | b<br>(\$/MWh) | a<br>(\$/(MW) <sup>2</sup> h) | P <sub>max</sub><br>(MW) |
|-------------|--------------------------|-------------|-------------|--------------|---------------|-------------------------------|--------------------------|
| 1           | 0                        | 0.035       | 300         | 550          | 8.10          | 0.00028                       | 680                      |
| 2           | 0                        | 0.042       | 200         | 309          | 8.10          | 0.00056                       | 360                      |
| 3           | 0                        | 0.042       | 200         | 307          | 8.10          | 0.00056                       | 360                      |
| 4           | 60                       | 0.063       | 150         | 240          | 7.74          | 0.00324                       | 180                      |
| 5           | 60                       | 0.063       | 150         | 240          | 7.74          | 0.00324                       | 180                      |
| 6           | 60                       | 0.063       | 150         | 240          | 7.74          | 0.00324                       | 180                      |
| 7           | 60                       | 0.063       | 150         | 240          | 7.74          | 0.00324                       | 180                      |
| 8           | 60                       | 0.063       | 150         | 240          | 7.74          | 0.00324                       | 180                      |
| 9           | 60                       | 0.063       | 150         | 240          | 7.74          | 0.00324                       | 180                      |
| 10          | 40                       | 0.084       | 100         | 126          | 8.6           | 0.00284                       | 120                      |
| 11          | 40                       | 0.084       | 100         | 126          | 8.6           | 0.00284                       | 120                      |
| 12          | 55                       | 0.084       | 100         | 126          | 8.6           | 0.00284                       | 120                      |
| 13          | 55                       | 0.084       | 100         | 126          | 8.6           | 0.00284                       | 120                      |

| Total Units | P <sub>min</sub><br>(MW) | c<br>(\$/h) | b<br>(\$/MWh) | a<br>(\$/(MW) <sup>2</sup> h) | P <sub>max</sub><br>(MW) |
|-------------|--------------------------|-------------|---------------|-------------------------------|--------------------------|
| 1           | 220                      | 64,782      | 796.9         | 0.3133                        | 550                      |
| 2           | 220                      | 64,782      | 796.9         | 0.3133                        | 550                      |
| 3           | 220                      | 64,670      | 795.5         | 0.3127                        | 550                      |
| 4           | 220                      | 64,670      | 795.5         | 0.3127                        | 550                      |
| 5           | 220                      | 64,670      | 795.5         | 0.3127                        | 550                      |
| 6           | 220                      | 64,670      | 795.5         | 0.3127                        | 550                      |
| 7           | 220                      | 64,670      | 795.5         | 0.3127                        | 550                      |
| 8           | 220                      | 64,670      | 795.5         | 0.3127                        | 550                      |
| 9           | 114                      | 172,832     | 915.7         | 0.7075                        | 500                      |
| 10          | 114                      | 172,832     | 915.7         | 0.7075                        | 500                      |
| 11          | 114                      | 176,003     | 884.2         | 0.7515                        | 500                      |
| 12          | 114                      | 173,028     | 884.2         | 0.7083                        | 500                      |
| 13          | 110                      | 91,340      | 1250.1        | 0.4211                        | 500                      |
| 14          | 90                       | 63,440      | 1298.6        | 0.5145                        | 365                      |
| 15          | 82                       | 65,468      | 1298.6        | 0.5691                        | 365                      |
| 16          | 120                      | 77,282      | 1290.8        | 0.5691                        | 325                      |
| 17          | 65                       | 190,928     | 238.1         | 2.5881                        | 315                      |
| 18          | 65                       | 285,372     | 1149.5        | 3.8734                        | 315                      |
| 19          | 65                       | 271,676     | 1269.1        | 3.6842                        | 315                      |
| 20          | 120                      | 39,197      | 696.1         | 0.4921                        | 272                      |
| 21          | 120                      | 45,576      | 660.2         | 0.5728                        | 272                      |
| 22          | 110                      | 28,770      | 803.2         | 0.3572                        | 260                      |
| 23          | 80                       | 36,902      | 818.2         | 0.9415                        | 190                      |
| 24          | 10                       | 105,510     | 33.5          | 52.123                        | 150                      |
| 25          | 60                       | 22,233      | 805.4         | 1.1421                        | 125                      |
| 26          | 55                       | 30,953      | 707.1         | 2.0275                        | 110                      |
| 27          | 35                       | 17,044      | 833.6         | 3.0744                        | 75                       |
| 28          | 20                       | 81,079      | 2188.7        | 16.765                        | 70                       |
| 29          | 20                       | 124,767     | 1024.4        | 26.355                        | 70                       |
| 30          | 20                       | 121,915     | 837.1         | 30.575                        | 70                       |
| 31          | 20                       | 120,780     | 1305.2        | 25.098                        | 70                       |
| 32          | 20                       | 104,441     | 716.6         | 33.722                        | 60                       |
| 33          | 25                       | 83,224      | 1633.9        | 23.915                        | 60                       |
| 34          | 18                       | 111,281     | 969.6         | 32.562                        | 60                       |
| 35          | 8                        | 64,142      | 2625.8        | 18.360                        | 60                       |
| 36          | 25                       | 103,519     | 1633.9        | 23.915                        | 60                       |
| 37          | 20                       | 13,547      | 694.7         | 8.482                         | 38                       |
| 38          | 20                       | 13,518      | 655.9         | 9.693                         | 38                       |

 Table A13. Data for the 38-unit generator test system.

| Total Units | P <sub>min</sub><br>(MW) | e<br>(1/MW) | d<br>(\$/h) | c<br>(\$/hr) | b<br>(\$/MWh) | a<br>(\$/(MW) <sup>2</sup> h) | P <sub>max</sub><br>(MW) |
|-------------|--------------------------|-------------|-------------|--------------|---------------|-------------------------------|--------------------------|
| 1           | 36                       | 0.084       | 100         | 94.705       | 6.73          | 0.00690                       | 114                      |
| 2           | 36                       | 0.084       | 100         | 94.705       | 6.73          | 0.00690                       | 114                      |
| 3           | 60                       | 0.084       | 100         | 309.54       | 7.07          | 0.02028                       | 120                      |
| 4           | 80                       | 0.063       | 150         | 369.03       | 8.18          | 0.00942                       | 190                      |
| 5           | 46                       | 0.077       | 120         | 148.89       | 5.35          | 0.01140                       | 97                       |
| 6           | 68                       | 0.084       | 100         | 222.33       | 8.05          | 0.01142                       | 140                      |
| 7           | 110                      | 0.042       | 200         | 287.71       | 8.03          | 0.00357                       | 300                      |
| 8           | 135                      | 0.042       | 200         | 391.98       | 6.99          | 0.00492                       | 300                      |
| 9           | 135                      | 0.042       | 200         | 455.76       | 6.60          | 0.00573                       | 300                      |
| 10          | 130                      | 0.042       | 200         | 722.82       | 12.9          | 0.00606                       | 300                      |
| 11          | 94                       | 0.042       | 200         | 635.20       | 12.9          | 0.00515                       | 375                      |
| 12          | 94                       | 0.042       | 200         | 654.69       | 12.8          | 0.00569                       | 375                      |
| 13          | 125                      | 0.035       | 300         | 913.40       | 12.5          | 0.00421                       | 500                      |
| 14          | 125                      | 0.035       | 300         | 1760.4       | 8.84          | 0.00752                       | 500                      |
| 15          | 125                      | 0.035       | 300         | 1728.3       | 9.15          | 0.00708                       | 500                      |
| 16          | 125                      | 0.035       | 300         | 1728.3       | 9.15          | 0.00708                       | 500                      |
| 17          | 220                      | 0.035       | 300         | 647.85       | 7.97          | 0.00313                       | 500                      |
| 18          | 220                      | 0.035       | 300         | 649.69       | 7.95          | 0.00313                       | 500                      |
| 19          | 242                      | 0.035       | 300         | 647.83       | 7.97          | 0.00313                       | 550                      |
| 20          | 242                      | 0.035       | 300         | 647.81       | 7.97          | 0.00313                       | 550                      |
| 21          | 254                      | 0.035       | 300         | 785.96       | 6.63          | 0.00298                       | 550                      |
| 22          | 254                      | 0.035       | 300         | 785.96       | 6.63          | 0.00298                       | 550                      |
| 23          | 254                      | 0.035       | 300         | 794.53       | 6.66          | 0.00284                       | 550                      |
| 24          | 254                      | 0.035       | 300         | 794.53       | 6.66          | 0.00284                       | 550                      |
| 25          | 254                      | 0.035       | 300         | 801.32       | 7.10          | 0.00277                       | 550                      |
| 26          | 254                      | 0.035       | 300         | 801.32       | 7.10          | 0.00277                       | 550                      |
| 27          | 10                       | 0.077       | 120         | 1055.1       | 3.33          | 0.52124                       | 150                      |
| 28          | 10                       | 0.077       | 120         | 1055.1       | 3.33          | 0.52124                       | 150                      |
| 29          | 10                       | 0.077       | 120         | 1055.1       | 3.33          | 0.52124                       | 150                      |
| 30          | 47                       | 0.077       | 120         | 148.89       | 5.35          | 0.01140                       | 97                       |
| 31          | 60                       | 0.063       | 150         | 222.92       | 6.43          | 0.00160                       | 190                      |
| 32          | 60                       | 0.063       | 150         | 222.92       | 6.43          | 0.00160                       | 190                      |
| 33          | 60                       | 0.063       | 150         | 222.92       | 6.43          | 0.00160                       | 190                      |
| 34          | 90                       | 0.042       | 200         | 107.87       | 8.95          | 0.0001                        | 200                      |
| 35          | 90                       | 0.042       | 200         | 116.58       | 8.62          | 0.0001                        | 200                      |
| 36          | 90                       | 0.042       | 200         | 116.58       | 8.62          | 0.0001                        | 200                      |
| 37          | 25                       | 0.098       | 80          | 307.45       | 5.88          | 0.0161                        | 110                      |
| 38          | 25                       | 0.098       | 80          | 307.45       | 5.88          | 0.0161                        | 110                      |
| 39          | 25                       | 0.098       | 80          | 307.45       | 5.88          | 0.0161                        | 110                      |
| 40          | 242                      | 0.035       | 300         | 647.83       | 7.97          | 0.00313                       | 550                      |

 Table A14. Data for the 40-unit generator test system.

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