

## A critical assessment of the standard molar Gibbs free energy of formation of NiWO<sub>4</sub>

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**Abstract.** Three independent studies have been reported on the free energy of formation of NiWO<sub>4</sub>. Results of these measurements are analyzed by the “third-law” method, using thermal functions for NiWO<sub>4</sub> derived from both low and high temperature heat capacity measurements. Values for the standard molar enthalpy of formation of NiWO<sub>4</sub> at 298·15 K obtained from “third-law” analysis are compared with direct calorimetric determinations. Only one set of free energy measurements is found to be compatible with calorimetric enthalpies of formation. The selected value for  $\Delta_f H_m^0(\text{NiWO}_4, \text{cr}, 298\cdot15 \text{ K})$  is the average of the three calorimetric measurements, using both high temperature solution and combustion techniques, and the compatible free energy determination. A new set of evaluated data for NiWO<sub>4</sub> is presented.

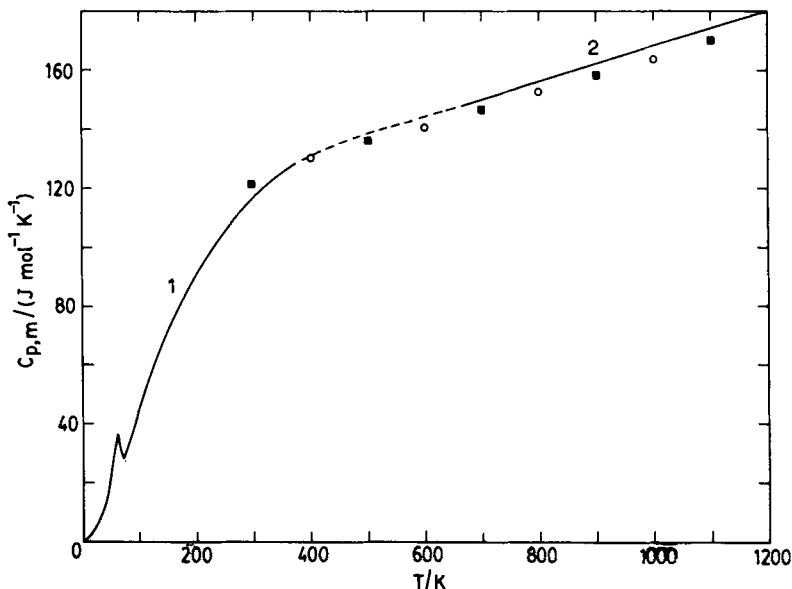
**Keywords.** “Third-law” analysis; Gibbs energy function; e.m.f. measurements; enthalpy of formation; heat capacity; entropy; phase relations.

### 1. Introduction

Tungsten-fibre reinforced composites with nickel or nickel base alloy as a matrix material find application as a structural component under extreme conditions such as those encountered in turbo-jet engines. Studies on the high-temperature stability of nickel-coated composites in atmospheres containing oxygen indicate that the internal oxidation of tungsten result in a mixture of several binary oxides and NiWO<sub>4</sub> (Kvernes and Kofstad 1973). Oxidation behaviour of the composite depends upon the relative stability of phases that appear during its oxidation. Conversely, thermodynamic properties of various phases in the system Ni–W–O also guide the reduction path of NiWO<sub>4</sub>. Studies on the reduction kinetics of complex oxides are essential in developing processes for the synthesis of various composites through powder metallurgy routes.

Recently, Aune *et al* (1994) reported values for the standard Gibbs free energy of formation of NiWO<sub>4</sub> in the temperature range 1167 K to 1317 K using a solid-state galvanic cell incorporating calcia-stabilized zirconia as the electrolyte. Their results, after correcting for obvious errors, differ significantly from earlier measurements of the free energy of formation by Jacob (1977) and Rezhukhina and Kashina (1974). At a temperature of 1200 K the results of Rezhukhina and Kashina (1974) are more negative by  $\sim 41\cdot4 \text{ kJ mol}^{-1}$  than those reported by Aune *et al* (1994).

The heat capacity of NiWO<sub>4</sub> has been measured from 5 K to 350 K by Landee and Westrum (1976) using an adiabatic calorimeter. There is a cooperative transition from antiferromagnetically-ordered state to the paramagnetic state at 59·8 K. The excess entropy associated with this antiferromagnetic anomaly was evaluated as  $R \ln 3$  for NiWO<sub>4</sub>. The standard entropy of NiWO<sub>4</sub> at 298·15 K obtained by integrating the low temperature heat capacities is  $(119\cdot34 \pm 0\cdot42) \text{ J mol}^{-1} \text{ K}^{-1}$ . Enthalpy increments ( $H_m^0(T) - H_m^0(298\cdot15 \text{ K})$ ) have been measured by Rezhukhina and Zharkova (1958) for



**Figure 1.** Temperature dependence of molar heat capacity of  $\text{NiWO}_4$ . (1) Low temperature measurements of Landee and Westrum (1976); (2) high temperature measurements of Zharkova and Rezhukhina (1958); ■, Values suggested in the compilation of Mah and Pankratz (1976); ○, Data given in the compilations of Knacke *et al* (1991).

four temperatures ranging from 715 K to 1107 K. The samples were dropped from high temperatures into a calorimeter maintained at room temperature. From these measurements the high temperature heat capacity can be deduced:

$$C_{p,m}^0 = 102 + 0.0657(T/K) \text{ J/(mol K)}. \quad (1)$$

As shown in figure 1, the heat capacity from low temperature studies joins reasonably well with that from high temperature measurements.

The enthalpy of formation,  $\Delta_f H_m^0(\text{NiWO}_4, \text{cr}, 298.15 \text{ K})$ , has been measured calorimetrically by three groups of investigators. Navrotsky and Kleppa (1969) used high-temperature solution calorimetry, with  $3\text{Na}_2\text{O} \cdot 4\text{MoO}_3$  as the solvent, to obtain a value of  $(-44.1 \pm 1.2) \text{ kJ mol}^{-1}$  for the enthalpy of formation of  $\text{NiWO}_4$  from  $\text{NiO}$  and  $\text{WO}_3$  at 970 K. Amosse and Mathieu (1974) determined the enthalpy of formation of  $\text{NiWO}_4$  from component oxides as  $(-49.8 \pm 1.7) \text{ kJ mol}^{-1}$  at 298.15 K. In separate experiments, they measured the enthalpy changes associated with the solution of  $\text{NiWO}_4$  and an equimolar mixture of  $\text{WO}_3$  and  $\text{NiO}$  at 298.15 K in a metaborate ( $0.5\text{LiBO}_2 - 0.5\text{NaBO}_2$ ) solvent maintained at 940 K. Porshina and Rezhukhina (1960) used a bomb calorimeter to determine the  $\Delta_f H_m^0(\text{NiWO}_4, \text{cr}, 298.15 \text{ K}) = (-1133.86 \pm 3.35) \text{ kJ mol}^{-1}$ . This corresponds to an enthalpy of formation of  $(-51.1 \pm 4) \text{ kJ mol}^{-1}$  from component oxides,  $\text{NiO}$  and  $\text{WO}_3$ . In this deduction, the enthalpies of formations of binary oxides were taken from Pankratz (1982). The three sets of calorimetric measurements on enthalpy of formation of  $\text{NiWO}_4$  are in fair agreement.

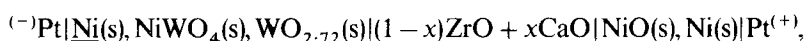
With the data now available it is possible to critically analyze the three independent high-temperature measurements of the  $\Delta_f G_m^0(\text{NiWO}_4, \text{cr})$ . Aune *et al* (1994) did not

compare their results with the calorimetric data. Thermodynamic data of NiWO<sub>4</sub> have been reported in the compilations of Mah and Pankratz (1976) and Knacke *et al* (1991). However, these assessments did not take into account all the information now available in the literature. For example, both compilations use estimated values for the standard entropy of NiWO<sub>4</sub>.

## 2. Analysis and discussion

### 2.1 Free energy data of Aune *et al* (1994) – correction of error

Aune *et al* (1994) measured the standard molar Gibbs free energy of formation of NiWO<sub>4</sub> in the temperature range 1167 K to 1318 K using a solid-state galvanic cell:



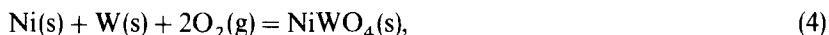
where  $\underline{\text{Ni}}(\text{s})$  denotes the Ni-rich f.c.c alloy containing a small amount ( $X_{\text{W}} < 0.03$ ) of tungsten. The virtual cell reaction was represented as:



From the e.m.f.s measured by Aune *et al* (1994) the standard free energy for the cell reaction can be obtained:

$$\Delta_2 G_{\text{m}}^0 = -14.610 - 0.02046(T/\text{K}) \text{ kJ/mol}. \quad (3)$$

Combining with standard free energies of formation of NiO (Charette and Flengas 1968) and WO<sub>2.72</sub> (Rizzo *et al* 1969) and ignoring the small correction for the activity of Ni in the alloy, the free energy for the formation of NiWO<sub>4</sub> is obtained. For the reaction,



$$\Delta_4 G_{\text{m}}^0 = -1067.890 + 0.3033(T/\text{K}) \text{ kJ/mol}. \quad (5)$$

The auxiliary data for NiO and WO<sub>2.72</sub> used here are identical with those employed by Aune *et al* (1994). They have incorrectly calculated

$$\Delta_4 G_{\text{m}}^0 = -1092.4 + 0.310(T/\text{K}) \text{ kJ/mol}, \quad (6)$$

which is more negative by  $\sim 16.5 \text{ kJ mol}^{-1}$  at 1200 K. This error in their calculation is also reflected in figure 3 of their paper. The correction for the reduced activity of the nickel in the solid solution, estimated assuming Raoult's law for the solvent is  $0.3 \text{ kJ mol}^{-1}$  at 1200 K. However, since the composition of the solid solution has not been experimentally determined, and the value calculated by Aune *et al* (1994) is dependent on their value for Gibbs free energy of formation of NiWO<sub>4</sub>, the justification for this small correction is at best tenuous.

### 2.2 Computation of Gibbs energy function (GEF) for NiWO<sub>4</sub>

From the high temperature heat capacity reported by Rezukhina and Zharkova (1958), ( $H_{\text{m}}^0(T) - H_{\text{m}}^0(298.15 \text{ K})$ ) and ( $S_{\text{m}}^0(T) - S_{\text{m}}^0(298.15 \text{ K})$ ) have been calculated. Using the value of the entropy at 298.15 K, reported by Landee and Westrum (1976) from low temperature heat capacity studies, values of  $S_{\text{m}}^0(T)$  have been derived.

Table 1. Evaluated standard molar thermodynamic properties for NiWO<sub>4</sub>(cr).

| T<br>K | C <sub>p,m</sub> <sup>o</sup>       |                                     | (H <sub>m</sub> <sup>o</sup> (T) - H <sub>m</sub> <sup>o</sup> (T <sub>r</sub> )) |                                     | S <sub>m</sub> <sup>o</sup>         |                                     | GEF                                 |                                     | Δ <sub>r</sub> H <sub>m</sub> <sup>o</sup> |                      | Δ <sub>r</sub> G <sub>m</sub> <sup>o</sup> |                      | log K <sub>r</sub> |
|--------|-------------------------------------|-------------------------------------|---|-------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|--|----------------------|--|----------------------|--------------------|
|        | J mol <sup>-1</sup> K <sup>-1</sup> | J mol <sup>-1</sup> K <sup>-1</sup> | J mol <sup>-1</sup>   | J mol <sup>-1</sup> K <sup>-1</sup> | J mol <sup>-1</sup> K <sup>-1</sup> | J mol <sup>-1</sup> K <sup>-1</sup> | J mol <sup>-1</sup> K <sup>-1</sup> | J mol <sup>-1</sup> K <sup>-1</sup> | kJ mol <sup>-1</sup>                       | kJ mol <sup>-1</sup> | kJ mol <sup>-1</sup>                       | kJ mol <sup>-1</sup> |                    |
| 298.15 | 121.6                               | 121.7                               | 0   | 119.34                              | 119.34                              | 119.34                              | -119.34                             | -1128.98                            | -1023.66                                   | 179.32               |  |                      |                    |
| 300    | 121.7                               | 121.7                               | 225   | 120.09                              | 120.09                              | 120.09                              | -119.34                             | -1128.96                            | -1023.00                                   | 178.10               |  |                      |                    |
| 400    | 128.3                               | 128.3                               | 12730   | 156.01                              | 156.01                              | 156.01                              | -124.19                             | -1127.61                            | -987.88                                    | 128.99               |  |                      |                    |
| 500    | 134.9                               | 134.9                               | 25880   | 185.34                              | 185.34                              | 185.34                              | -133.57                             | -1126.07                            | -953.13                                    | 99.56                |  |                      |                    |
| 600    | 141.4                               | 141.4                               | 39700   | 210.51                              | 210.51                              | 210.51                              | -144.35                             | -1124.43                            | -918.72                                    | 79.97                |  |                      |                    |
| 631    | 143.5                               | 143.5                               | 44140   | 217.75                              | 217.75                              | 217.75                              | -147.81                             | -1123.99                            | -908.12                                    | 75.16                |  |                      |                    |
| 700    | 148.0                               | 148.0                               | 54170   | 232.81                              | 232.81                              | 232.81                              | -155.42                             | -1122.42                            | -884.54                                    | 65.99                |  |                      |                    |
| 800    | 154.6                               | 154.6                               | 69300   | 253.00                              | 253.00                              | 253.00                              | -166.38                             | -1119.70                            | -850.78                                    | 55.54                |  |                      |                    |
| 900    | 161.2                               | 161.2                               | 85090   | 271.59                              | 271.59                              | 271.59                              | -177.05                             | -1116.54                            | -817.35                                    | 47.43                |  |                      |                    |
| 1000   | 167.7                               | 167.7                               | 101530  | 288.91                              | 288.91                              | 288.91                              | -187.36                             | -1112.90                            | -784.28                                    | 40.96                |  |                      |                    |
| 1100   | 174.3                               | 174.3                               | 118630  | 305.21                              | 305.21                              | 305.21                              | -197.36                             | -1108.81                            | -751.54                                    | 35.68                |  |                      |                    |
| 1200   | 180.9                               | 180.9                               | 136400  | 320.66                              | 320.66                              | 320.66                              | -207.00                             | -1104.24                            | -719.29                                    | 31.30                |  |                      |                    |
| 1300   | 187.4                               | 187.4                               | 154810  | 335.39                              | 335.39                              | 335.39                              | -216.31                             | -1099.20                            | -687.41                                    | 27.62                |  |                      |                    |
| 1400   | 194.0                               | 194.0                               | 173890  | 349.52                              | 349.52                              | 349.52                              | -225.32                             | -1093.69                            | -655.89                                    | 24.47                |  |                      |                    |
| 1500   | 200.6                               | 200.6                               | 193610  | 363.13                              | 363.13                              | 363.13                              | -234.06                             | -1083.51                            | -620.67                                    | 21.61                |  |                      |                    |
| 1600   | 207.2                               | 207.2                               | 214000  | 376.29                              | 376.29                              | 376.29                              | -242.54                             | -1073.70                            | -586.65                                    | 19.15                |  |                      |                    |

T<sub>r</sub> = 298.15 K; P<sup>o</sup> = 101.325 kPa.

The Gibbs energy function, defined as,

$$\text{GEF} = -S_m^0 + \frac{H_m^0(T) - H_m^0(298.15 \text{ K})}{T}, \quad (7)$$

and calculated as a function of temperature, is summarized in table 1.

### 2.3 'Third-law' analysis of the high temperature free energy data

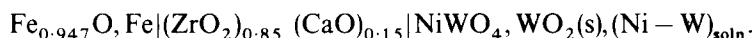
The corrected expression (5) for the energy of formation of NiWO<sub>4</sub> calculated from the e.m.f. measurements of Aune *et al* (1994), is significantly different from that given by Rezukhina and Kashina (1974):

$$\Delta_4 G_m^0 = -1108.51 + 0.302(T/\text{K}) \text{ kJ/mol}, \quad (8)$$

in the temperature range 1150 K to 1350 K, and that given by Jacob (1977):

$$\Delta_4 G_m^0 = -1104.7 + 0.323(T/\text{K}) \text{ kJ/mol}, \quad (9)$$

in the temperature range 1025 K to 1300 K. The galvanic cell employed by Jacob (1977) was identical to that used by Aune *et al* (1994). The e.m.f.s obtained by Aune *et al* (1994) are significantly lower than that registered by Jacob (1977). At a temperature of 1200 K, the difference is 25 mV. Rezukhina and Kashina (1974) did their studies on the cell,

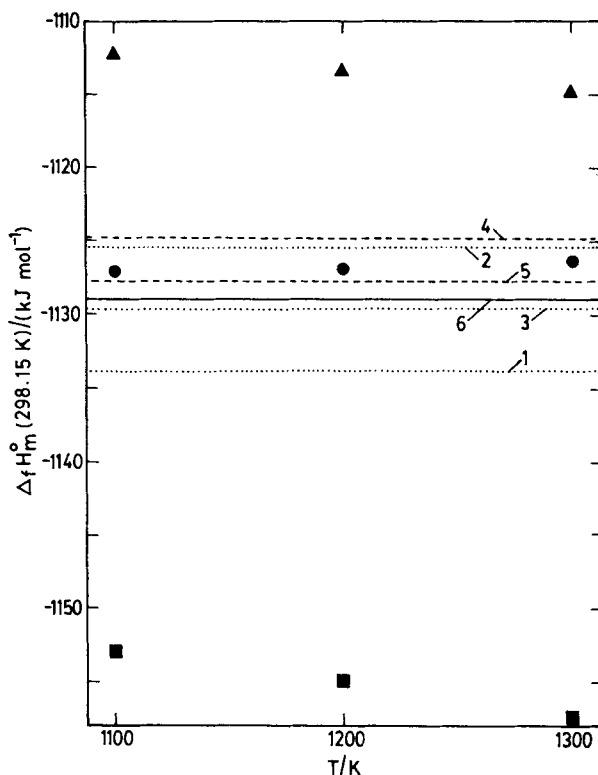


In the temperature range 1170 K to 1243 K, the alloy in equilibrium with NiWO<sub>4</sub> and WO<sub>2</sub> was assumed to have the composition Ni<sub>4</sub>W. From 1243 K to 1346 K, composition in the alloy was considered as Ni<sub>0.83</sub>W<sub>0.17</sub>. There are important differences among the three high temperature studies in the composition of the tungsten oxide phase in equilibrium with NiWO<sub>4</sub> and Ni-rich alloy. Rezukhina and Kashina (1974) identify WO<sub>2</sub> as the oxide phase in equilibrium in the entire range of temperatures covered in their study. Jacob (1977) identified the phase as WO<sub>2.72</sub> by X-ray diffraction. Aune *et al* (1994) suggest WO<sub>2.72</sub> as oxide phase in equilibrium above 1167 K and WO<sub>2.9</sub> at lower temperatures. The inference regarding the change in oxide composition was based on the observed change in the slope of e.m.f. as a function of temperature. They could not get unambiguous X-ray evidence for the change in the composition of the oxide phase. Careful phase diagram studies are required to solve this discrepancy.

Measurements on metastable equilibria can also be used to derive thermodynamic information on one of the phases involved (Jacob and Srikanth 1988). E.m.f. studies of ternary oxides at moderate temperatures can sometime yield the correct values even when they are mixed with other phases not in true thermodynamic equilibrium. Therefore, it is prudent to consider all the e.m.f. studies on NiWO<sub>4</sub> for the 'third-law' analysis.

The validity of the expressions for the free energy of formation of NiWO<sub>4</sub> can be checked by the 'third-law' analysis. The standard enthalpy of formation,  $\Delta_f H_m^0$  (NiWO<sub>4</sub>, cr, 298.15 K) can be calculated from each value of  $\Delta_f G_m^0$  (NiWO<sub>4</sub>, cr) at temperature  $T$  and the Gibbs energy function (GEF), for the reaction (4):

$$\Delta_f H_m^0(298.15 \text{ K}) = -T\Delta(\text{GEF}) + \Delta_f G_m^0(T). \quad (10)$$



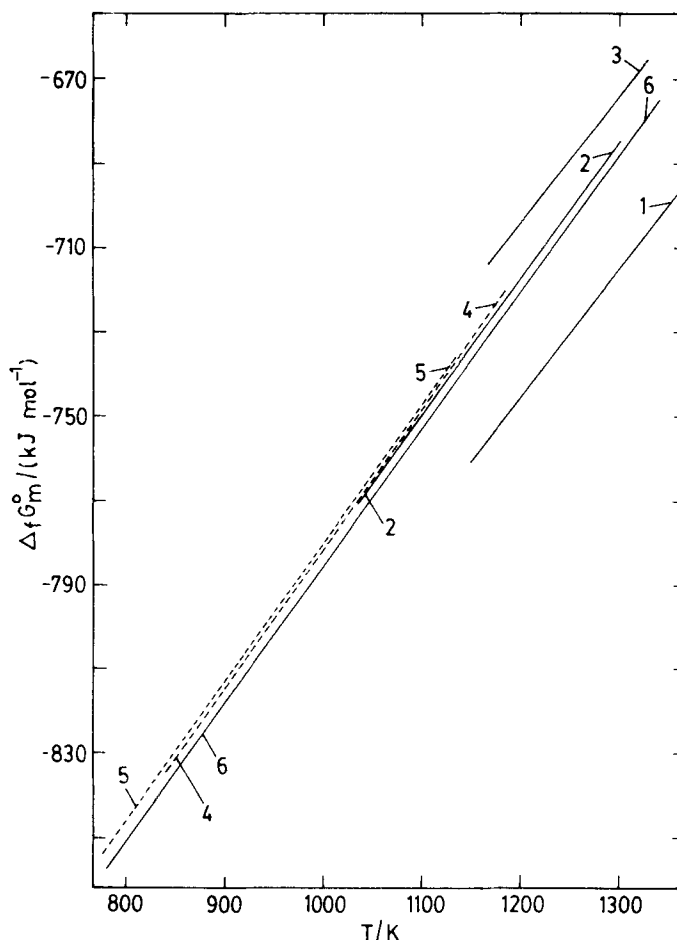
**Figure 2.** Comparison of standard molar enthalpy of formation of  $\text{NiWO}_4$  at 298.15 K. Results of 'third-law' analysis: ■, Rezukhina and Kashina (1974); ●, Jacob (1977); ▲, Aune *et al* (1994). Calorimetric data: (1) Porshina and Rezukhina (1960), (2) Navrotsky and Kleppa (1969), (3) Amosse and Mathieu (1974). Data from compilations: (4) Mah and Pankratz (1976), (5) Knacke *et al* (1991). The value selected in this evaluation is indicated by line 6.

The values of GEF for Ni, W and  $\text{O}_2$  are taken from the compilations by Pankratz (1982) and GEF for  $\text{NiWO}_4$  evaluated in this work is used. The values for  $\Delta_f H_m^0(\text{NiWO}_4, \text{cr}, 298.15 \text{ K})$ , evaluated from the free energy data at 1100, 1200 and 1300 K are compared with the calorimetric data in figure 2.

It can be seen that the values of  $\Delta_f H_m^0(\text{NiWO}_4, \text{cr}, 298.15 \text{ K})$  obtained from the 'third-law' analysis of the free energy data of Jacob (1977) are relatively constant and in fair agreement with calorimetric values reported in the literature. The free energies of formation of  $\text{NiWO}_4$  given by Aune *et al* (1994) and Rezukhina and Kashina (1974) are not consistent with the calorimetric data. Moreover, the analysis of these results show a small but significant systematic drift in the enthalpy of formation. This may be indicative of small temperature dependent errors in their measurements.

#### 2.4 Evaluation of enthalpy and free energy of formation of $\text{NiWO}_4$

Since the calorimetric data and free energy measurements of Jacob (1977) are reasonably concordant, an average value for the  $\Delta_f H_m^0(\text{NiWO}_4, \text{cr}, 298.15 \text{ K}) = (-1126.97 \pm 4) \text{ kJ mol}^{-1}$  may be selected. The free energy of formation can be calculated



**Figure 3.** Temperature dependence of the standard molar Gibbs free energy of formation of NiWO<sub>4</sub>. Data from measurements: (1) Rezhikhina and Kashina (1974), (2) Jacob (1977), (3) Aune *et al* (1994). Data from compilations: (4) Knacke *et al* (1991), (5) Mah and Pankratz (1976). The results of this evaluation are shown by line 6.

at regular intervals of temperature based on the  $\Delta_f G_m^0(\text{NiWO}_4, \text{cr}, 298.15 \text{ K})$  and other thermal functions based on calorimetric data. The computed values for  $\Delta_f G_m^0(\text{NiWO}_4, \text{cr})$  are also given in table 1.

The standard free energy of formation from different studies and compilations are compared with the data selected in this study, in figure 3. The selected data set is in reasonable accord with the values suggested by Jacob (1977) based on the e.m.f. measurements and earlier compilations of Mah and Pankratz (1976) and Knacke *et al* (1991). The uncertainty in the free energy of formation evaluated in this study is  $(\pm 4) \text{ kJ mol}^{-1}$ . The free energy data of Rezhikhina and Kashina (1974) are significantly more negative. The values of free energy of formation of NiWO<sub>4</sub> suggested recently by Aune *et al* (1994) are on the average more positive than the selected data by  $\sim 20 \text{ kJ mol}^{-1}$ .

Aune *et al* (1994) calculated the phase diagram for the system (Ni–W–O) based on their data on the free energy of formation of NiWO<sub>4</sub>. The topology of the computed

diagram depends critically on the input thermodynamic data. It is clear from the above discussion that the diagram suggested by Aune *et al* (1994) is not based on the best available information on the free energy of formation of NiWO<sub>4</sub>. More specifically, their computed phase relations involving the phase NiWO<sub>4</sub> would be seriously affected.

### 3. Summary

The selected values of  $\Delta_f G_m^0(\text{NiWO}_4, \text{cr})$  at various temperatures are based on the three calorimetric measurements (Porshina and Rezhukhina 1960; Navrotsky and Kleppa 1969; Amosse and Mathieu 1974) of the heat of formation of NiWO<sub>4</sub> and one set of free energy data (Jacob 1977) which are in reasonable agreement. Two (Rezhukhina and Kashina 1974; Aune *et al* 1994) of the three sets of the reported free energy data are found to be inconsistent with the calorimetric information. In computation of reliable phase diagrams it is important to use the best available thermodynamic information.

### List of symbols

|                  |  |
|------------------|--|
| $C_{p,m}^0$      | Standard molar heat capacity.                                |
| $T$              | Thermodynamic temperature in kelvin.                         |
| $\Delta_f G_m^0$ | Standard molar Gibbs free energy of formation from elements. |
| $\Delta_i G_m^0$ | Standard molar Gibbs free energy change for reaction i.      |
| $\Delta_f H_m^0$ | Standard molar enthalpy of formation from elements.          |
| cr               | crystal  |
| GEF              | Gibbs energy function.                                       |

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