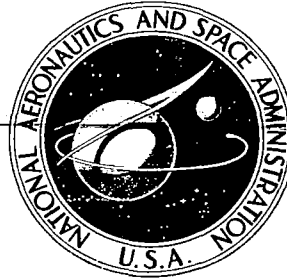


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A FURTHER STUDY OF JIMSPHERE WIND PROFILES AS RELATED TO SPACE VEHICLE DESIGN AND OPERATIONS

*by S. I. Adelfang, A. Court,
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FOREWORD

This report was prepared by the Lockheed-California Company, Burbank, California for the National Aeronautics and Space Administration, George C. Marshall Space Flight Center, Huntsville, Alabama under Contract NAS 8-30165. The contract title is "Further Study of Jimsphere Wind Profiles Related to Space Vehicle Design and Operations".

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The principal sections of this report were contributed by the following Lockheed-California Company (Calac) personnel and consultants: Dr. Stanley I. Adelfang (Calac), Sections 2 and 4; Dr. Arnold Court (Consultant) with Mr. Craig A. Melvin (Calac), Section 3; and Mr. Mohsen Pazirandeh (Consultant), Section 5.

ABSTRACT

Statistical characteristics of steady state winds, gusts and wind shears observed over Cape Kennedy, Florida and Point Mugu, California with Jimsphere balloon sensors are described. Gusts in Jimsphere wind profiles as viewed in the time coordinates of a Saturn vehicle were isolated from the original profiles with a 33 weight digital high pass filter with negligible transmission of wind fluctuations at frequencies less than 0.15 cps. The distribution of gust variance computed for three ten second intervals of Saturn flight time for Cape Kennedy profiles was found to be log-normal. Maximum absolute gusts increased with altitude for altitudes from 4 to 15 km. The distribution of spectrum densities of gusts computed at frequencies from 0.3 to 3 cps for 900 Cape Kennedy profiles decreases with increasing frequency at a rate proportional to the -2.9 power of frequency for frequencies from 0.6 to 2.1 cps; at frequencies greater than 2.1 cps a power law relation is not supported by the results. When spectrum densities were grouped with respect to deciles of wind speed and various wind shears they showed a tendency to be larger at the high deciles.

A preliminary study of a method for mathematical representation of observed gust functions suggests that the method can be applied to Jimsphere wind profiles that are closely spaced in time.

Steady state winds for 794 Cape Kennedy profiles that were complete between 4 and 15 km, computed by subtraction of the gust component from the total wind, were in good agreement with the annual wind speeds of the Atlantic Missile Range Reference Atmosphere for the 50 percent cumulative frequency but were significantly smaller for the 90, 95, 97.7 and 99 percent cumulative frequencies.

A study of the climatological means and standard deviations of the magnitude of the vector shear at altitudes between 8 and 15 km indicates that they can

be described by power law functions of layer thickness that are nearly alike for Cape Kennedy and Point Mugu but are significantly different from those derived from a few summer profiles by other workers.

A method for profile sampling is developed which provides profile sample sets that represent five critical characteristics of the parent population. A test of the method consisting of a comparison of the distributions of spectrum densities between 0.3 and 3.0 cps of five sample sets, each composed of 25 profiles, to the corresponding distributions of the entire population indicated that the spectrum distributions of any of the five sample sets offer a fair approximation to that of the whole 900 profile parent population.

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Section 1

INTRODUCTION

The characteristics of wind fluctuations that are important in space vehicle design and operation must be known with sufficient accuracy to assure a minimum risk of critical elastic and control mode responses. The development and use of roughened super-pressure (Jimsphere) balloons with minimal self induced motions that are tracked with advanced radar systems represents a significant advance towards increasing the accuracy of routine measurements of the horizontal vector wind as a fluctuation of altitude. The 119⁴ Jimsphere profiles taken over Cape Kennedy, Florida between Nov. 1964 and May 1967, were the subject of a detailed study by Adelfang, Ashburn, and Court (Ref. 1). Two aspects of that study which are further developed in this report are the analysis of gust profiles computed from Jimsphere wind profiles expressed as a function of Saturn vehicle time coordinates (Section 2) and the study of the magnitude of the vector wind shear over various layer thicknesses (Section 4); the later study includes a set of 83 Jimsphere profiles taken over Point Mugu, California. The principal aim of these studies has been to derive, from the entire set of available profiles, statistical characteristics that are useful for space vehicle design and operation. However, in addition, it is often desirable to have the capability of selecting a relatively small sample of profiles which represent the critical characteristics of the large parent sample; in Section 3, a set of critical and test characteristics are suggested and a methodology is described and tested for selecting profile sub-sets.

In Section 5 a preliminary study is presented of a method for representing gust functions observed in Jimsphere wind profiles. The theory and original application of the method by Dutton (Ref. 2) and its application to groups of Jimsphere profiles closely spaced in time are discussed.

Section 2

ANALYSIS OF GUSTS DERIVED FROM JIMSPHERE WIND PROFILES TRANSFORMED TO VEHICLE TIME COORDINATES

2.1 INTRODUCTION

Past analyses of Jimsphere profiles have resulted in the derivation of statistics which are valid for wind fluctuations described in altitude coordinates; for example Endlich et al, (Ref. 3) who studied three profile sequences, each composed of 4-6 profiles, found that there are no consistent or well-defined spectrum peaks that indicate natural separations between scales of motion and that the power spectrum density decreases with increasing frequency at a rate proportional to the -2.5 to -3 power. Although these and other similar results are interesting from a meteorological point of view they are not strictly applicable in describing the wind fluctuations that are seen by an accelerating space vehicle. For this study, 900 Cape Kennedy Jimsphere wind profiles were used as basic data for an analysis of wind fluctuations as viewed by a Saturn vehicle.

2.2 GUST PROFILE DEFINITION

The frequency response of space vehicles to wind fluctuations is a function of control and structural mode characteristics which are nearly uniform for a particular class of vehicles. These vehicle response characteristics are usually defined in terms of temporal frequency, f (cps), rather than spatial frequency, K (cycles per meter, cpm). As a vehicle ascends with vertical velocity, $v(t)$, through the atmosphere, wind fluctuations at spatial frequency, K , are seen by the vehicle at frequency, f , given by

$$f = K v(t) \quad (2.1)$$

Thus, for example, the fluctuations in the wind profile at $K = 2.74 \cdot 10^{-3}$ (cpm) as seen by a Saturn vehicle increase from $f = 0.534$ cps at 4 km ($v = 195$ m/sec) to $f = 1.00$ cps at 12 km ($v = 365$ m/sec). Since the first bending mode frequency of a Saturn 5 vehicle is approximately 1 cps the fluctuations at $K = 2.74 \cdot 10^{-3}$ (cpm) are more important at 12 km than at 4 km. It is obvious that innumerable spatial frequencies exist for a particular critical value of temporal vehicle response frequency. Therefore it is necessary to transform the spatial fluctuations of wind profiles to temporal fluctuations as seen by the vehicle.

The general procedure suggested by Adelfang, Ashburn, and Court (Ref. 1) for deriving gust profiles is used for this study of Jimsphere wind profiles. The principal steps in the derivation are the transformation of Jimsphere profiles to a vehicle time coordinate system, definition of the wind fluctuations of interest, and digital high pass filtering.

Jimsphere wind profiles were transformed to vehicle time coordinates by evaluating them at altitudes, Z , (km.) corresponding to the time, t (sec), from launch at intervals of time, Δt (sec), according to the least squares quadratic fit to the Saturn AS-504 trajectory given by Jacobs (Ref. 4).

$$Z = 2.98416 - 0.14889 t + 0.00330 t^2 \quad (2.2)$$

Z calculated from Equation 2.1 deviates less than 1.7% from the AS-504 trajectory for the time interval from 50 to 95 seconds ($Z = 3.855$ to 18.530 km). The time interval Δt was chosen small enough to include all Jimsphere data up to 17.2 km. Assuming that a Jimsphere profile contains independent estimates of wind over 75m altitude intervals, the time interval, Δt (sec), between independent wind estimates as seen by a vehicle is $75/v(t)$; at 17.2 km, for Saturn AS-504, $v(t) = 450$ m/sec and thus $\Delta t = 1/6$ second.

The transformed wind profile is an approximation of the profile "seen" by the vehicle; the accuracy of the approximation for space vehicle studies is

not yet known and may only be determined when the statistics of vehicle responses derived from simulated flights through Jimsphere wind profiles are compared to the same statistics derived from wind profile data obtained from sensors which traverse the atmosphere in space-time coordinates that are similar to those of space vehicles.

The fluctuations of interest which will be referred to as gusts are characterized by their influence on space vehicle control and structural excitation frequency modes. For a Saturn vehicle significant response to wind fluctuations occur at the control frequency (~ 0.2 cps) and at the first and second bending mode frequencies ($\sim 1,2$ cps). Wind profiles which have fluctuations at frequencies ≥ 0.2 cps are defined as gust profiles. Gust profiles were calculated by application of a 33 weight digital high pass filter which has a transfer function of the form

$$H(f) = 1 - e^{-\left[f/f_s(.0255)\right]^2} \quad (2.3)$$

where f = frequency (cps)

Since f_s , the data sampling frequency is 6 sec^{-1} Equation (2.3) reduces to

$$H(f) = 1 - e^{-(6.535 f)^2} \quad (2.4)$$

The 33 point weighting function (listed in Table 2.1) for the high pass filter was calculated by subtracting the weighting function of the low pass filter described by Alfriend (Ref. 5) from the weighting function of an all pass filter (an all pass filter has weights equal to zero except for the middle weight which is unity). The transfer function of the Alfriend low pass filter for $f_s = 6 \text{ sec}^{-1}$ is

$$H(f) = e^{-(6.535 f)^2} \quad (2.5)$$

The transfer functions of the high and low pass filters described by Equations 2.4 and 2.5 are illustrated in Figure 2.1.

TABLE 2.1
 33 WEIGHT DIGITAL HIGH PASS FILTER
 WITH TRANSFER FUNCTION GIVEN BY
 EQUATION 2.4; $\Delta t = 1/6$ SEC.

TIME	NUMERICAL WEIGHTS
t	0.951844
$-\Delta t, + \Delta t$	-0.047848
$-Z\Delta t, + Z\Delta t$	-0.046936
•	-0.045453
•	-0.043457
•	-0.041013
•	-0.038222
•	-0.035162
•	-0.031935
•	-0.028634
•	-0.025346
•	-0.022151
$-n\Delta t, + n\Delta t$	-0.019110
•	-0.016288
•	-0.013689
•	-0.011364
$-16\Delta t, + 16\Delta t$	-0.009314

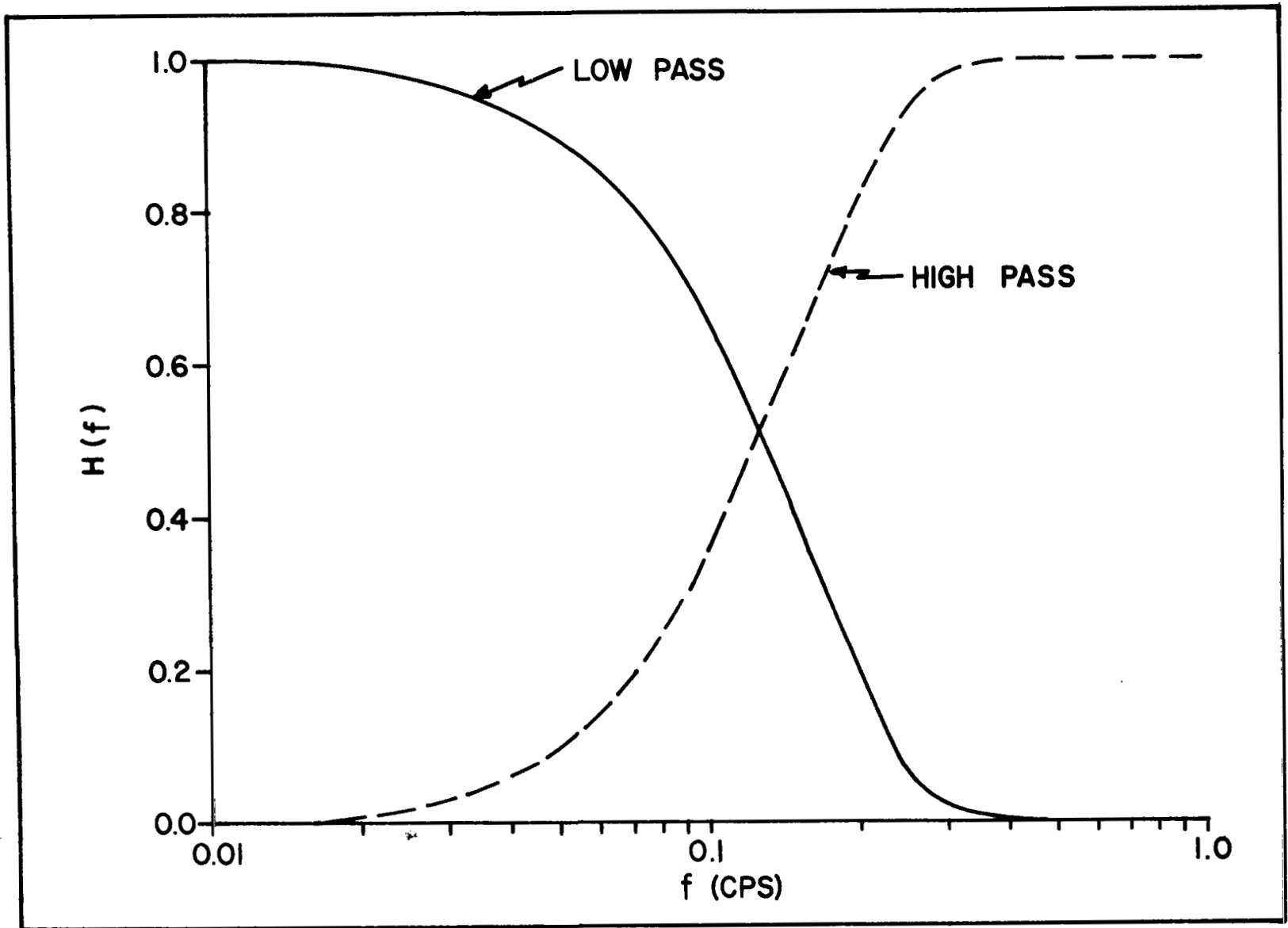


Figure 2.1 Transfer Function of Alfriend Exponential Low and High Pass Filters for a Sampling Frequency of 6/sec.

The relation between the low and high pass filtered profile and the total profile is illustrated in Figure 2.2 for Cape Kennedy Jimsphere profile # 477; the total profile transformed to Saturn AS-504 time coordinates is represented by the solid line; the low frequency or low pass filtered profile which has been termed the steady state wind profile with respect to the Saturn AS-504 in Reference 1 is illustrated by the dashed line; the gust or high pass filtered profile which is the total profile minus the low pass filtered profile is illustrated across the top of the figure.

2.3 STATISTICAL ANALYSIS

2.3.1 Introduction

The Cape Kennedy Jimsphere wind speed profiles, each decomposed into a low frequency steady state component and a high frequency gust component according to the method described in the previous section, were analyzed to determine the distribution of, gusts and steady state winds as a function of altitude, gust variance as a function of Saturn AS-504 flight time interval, and the power spectrum densities (PSD) of gusts. The distribution of PSD's of gusts were computed for 900 profiles that were complete between 1 and 14 km. The distribution of PSD's were also computed for sub-sets of 90 profiles associated with the deciles of maximum wind speed and maximum 100, 400, 1,000 and 3,000 m vector shears (for winds increasing with height) computed for each of the 900 profile parent population. Additional PSD calculations used to verify the technique for selecting representative profile sub-sets are presented in Section 3.

2.3.2 Distribution of Steady State Wind Speeds, Gusts, and Gust Variance

The percentile distributions of steady state wind speeds and gusts as a function of altitude are illustrated in Figures 2.3 and 2.4. The percentiles were computed for the 794 profiles which had steady state and gust data between 4 and 15 km. The percentiles are plotted at altitude intervals of

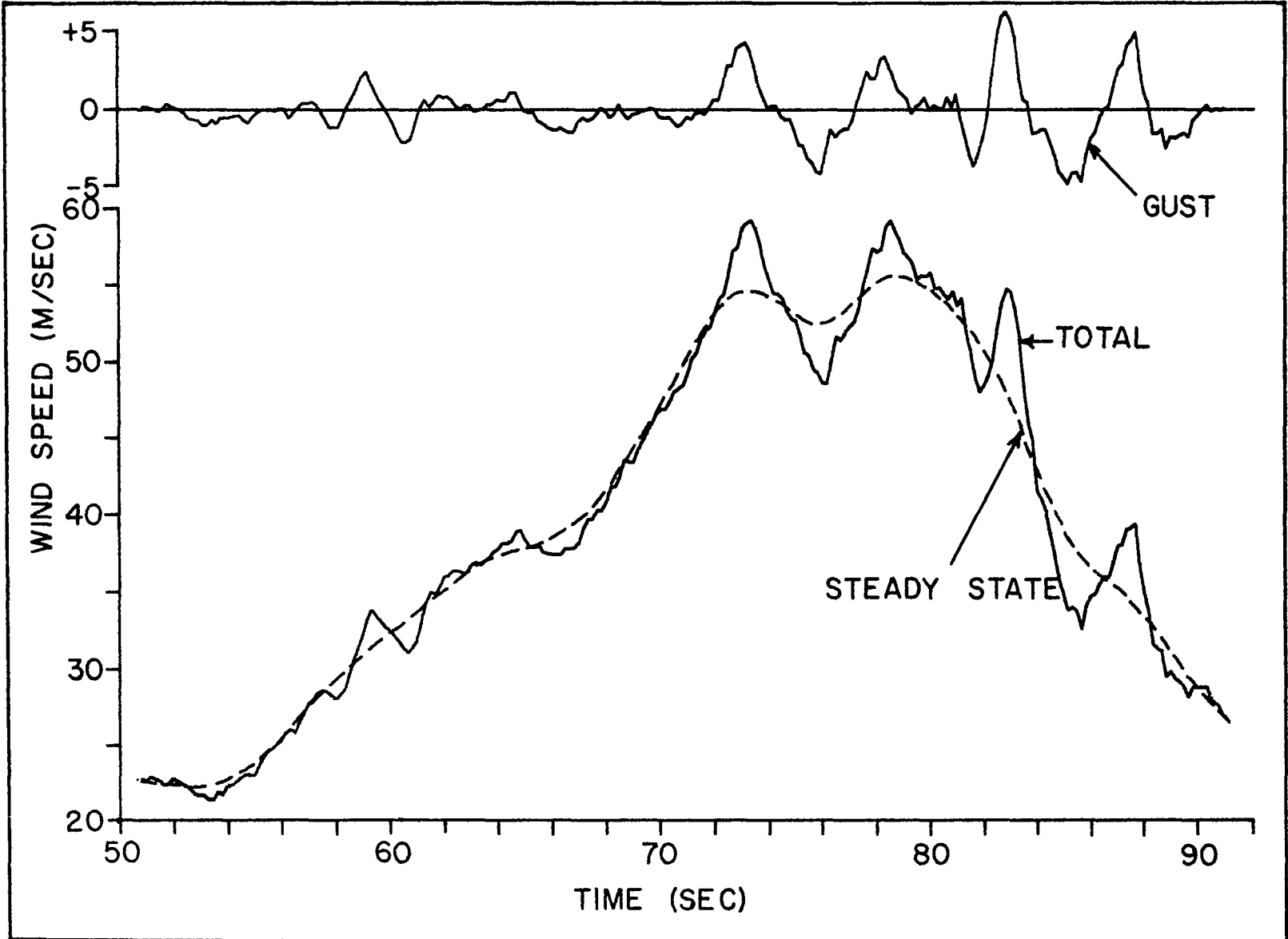


Figure 2.2 Jimsphere Wind Profile No. 477, Transformed to Saturn AS-504 Time Coordinates (Solid Line), Steady State (Dashed Line) and Gust as Labeled.

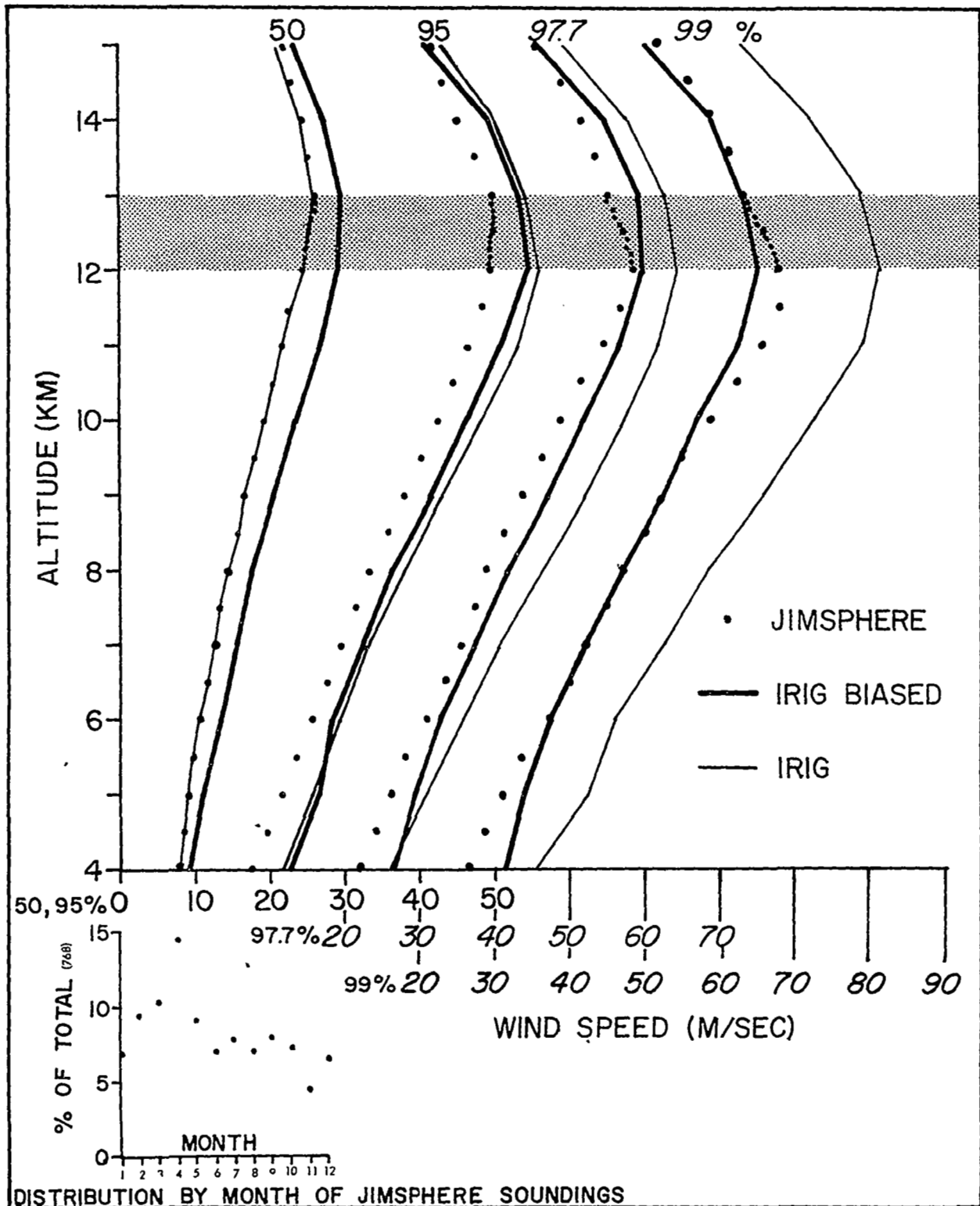


Figure 2.3 Distribution of Steady State Winds as a Function of Altitude Computed from 794 Cape Kennedy Jimsphere Profiles; at Lower Left Distribution by Month of the 794 Profiles Used; Also Illustrated are the Annual and Biased Annual IRIG Wind Speeds for Cape Kennedy (Ref. 5).

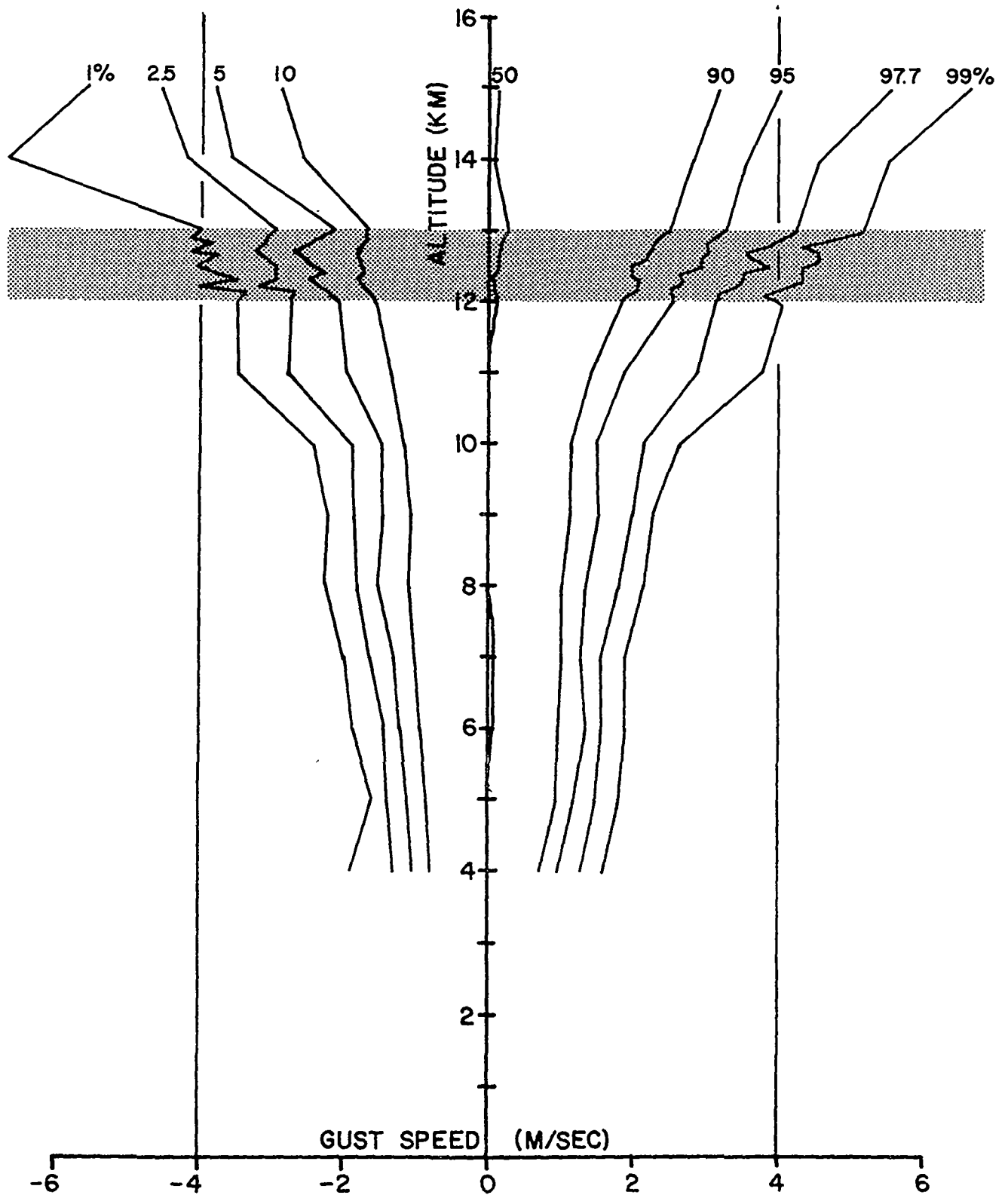


Figure 2.4 Distribution of Gusts as a Function of Altitude Computed from 794 Cape Kennedy Jimsphere Profiles; the Distribution by Month of the 794 Profiles is Illustrated in Figure 2.3

1 km between 4 and 15 km, and 100 m between 11 and 12 km. Also illustrated in Figure 2.3, for comparison, are the 50, 95, 99.7 and 99% annual scalar wind speeds of the IRIG reference atmosphere (Ref. 6) which were derived from 4,384 Rawinsonde profiles over Cape Kennedy. As illustrated the steady state winds derived from Jimsphere profiles increase with increasing altitude above 4 km attaining a maximum at an altitude of 12.9 km for 50%, 12.0 km for 95%, 12.1 km for 97.7% and < 12 km for 99%. The 95, 97.7 and 99 percentile steady state winds computed from Jimsphere wind profiles are systematically smaller than the wind speeds of the IRIG standard atmosphere. As illustrated in Figure 2.3, the distribution of the 794 Jimsphere profiles by month is non-uniform with a large peak for April thus introducing a bias in the annual distribution. However, when biased annual IRIG wind speed percentiles, computed by taking an average of the monthly values weighted according to the number of Jimsphere soundings for a particular month, are compared to the Jimsphere distribution the same qualitative conclusions stated above for the comparison to the unbiased IRIG atmosphere are valid for the 95 and 97.7 percentiles; however at altitudes between 10 and 15 km the biased IRIG 99% wind speeds are as much as 5% less than the Jimsphere steady state winds. At the 50 percentile there is good agreement between Jimsphere and IRIG annual whereas the IRIG biased annual is substantially larger than the Jimsphere steady state winds. Thus by biasing the IRIG distribution the correspondance between IRIG and Jimsphere was generally improved at the extreme percentiles and degraded at the median.

As illustrated in Figure 2.4 the gust magnitudes at the extreme percentiles ($\geq 90\%$, $\leq 10\%$) generally increase with altitude; the variability of gust magnitudes for small scale variations of altitude is illustrated by the data given at 100 m intervals between 12 and 13 km. The maximum observed absolute gust speed (G_{\max} , m/sec) as a function of altitude (km) is illustrated in Figure 2.5; the solid line in the figure is the least squares quadratic function fitted to the data

$$G_{\max} = 2.90 - 0.30Z + 0.05Z^2 \quad (2.6)$$

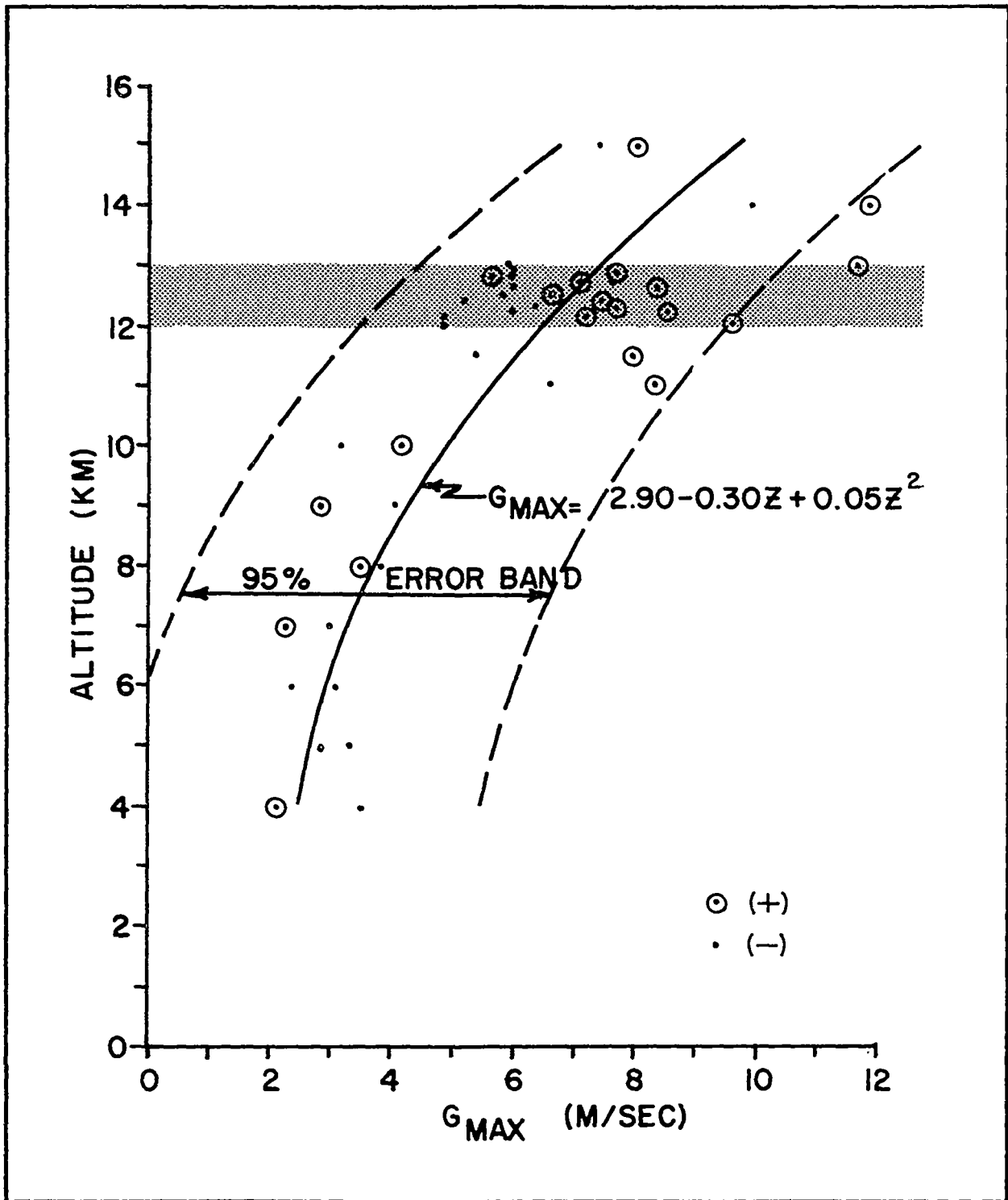


Figure 2.5 Maximum Observed Absolute Gust Speed as a Function of Altitude in 794 Cape Kennedy Jimsphere Profiles

Figure 2.6 illustrates the cumulative percentile distribution of gust variance (m^2/sec^2) for three Saturn vehicle flight time intervals of 60-70, 70-80 and 80-90 seconds; these time intervals correspond to Saturn altitude intervals of 5.93 to 8.73, 9.73 to 12.19, and 12.19 to 16.31 km respectively. The cumulative distribution is approximately log-normal as indicated by the straight lines fitted to the plotted points.

2.3.3 Power Spectrum Densities of Gusts

Power spectrum densities (PSD's) of 900 Jimsphere gust profiles defined in the time domain of a Saturn vehicle were computed according to the method described by Blackman and Tukey (Ref. 7). The 900 profiles were selected on the basis of completeness between 4 and 14 km. A Saturn vehicle in an AS-504 trajectory requires 36 seconds to traverse the 4 to 14 km altitude interval; thus a gust profile evaluated at 1/6 second intervals according to Equation 1 would contain 216 data points. PSD's, computed using 10 lags, are given at intervals of 0.3 cps from 0.3 to 3.0 cps. The cumulative percentile distribution of the PSD's $\left[\frac{(M/sec)^2}{cycle/sec} \right]$ at each frequency is given in Table 2.2.

In Figure 2.7 the PSD's at the median and the 95 and 99 percentiles are compared with recent updated MSFC design criteria spectra (Ref. 8) derived in the altitude domain from a similar set of Cape Kennedy Jimsphere wind profiles. The direct comparison is valid only if the MSFC PSD's, $\Phi(K) \left[\frac{(M/sec)^2}{(cycle/4,000 m)} \right]$, originally expressed as a function of spatial frequency, K (cycles/4,000 m) can be transformed to PSD's in the time domain of vehicle flight, $\Phi(f) \left[\frac{(M/sec)^2}{(cycle/sec)} \right]$ according to the simple relation, implied by Ryan et al, (Ref. 9),

$$\Phi(f) = \frac{4 \times 10^3 \Phi(K)}{v} \quad (2.7)$$

where v is a vehicle vertical velocity arbitrarily chosen at the altitude

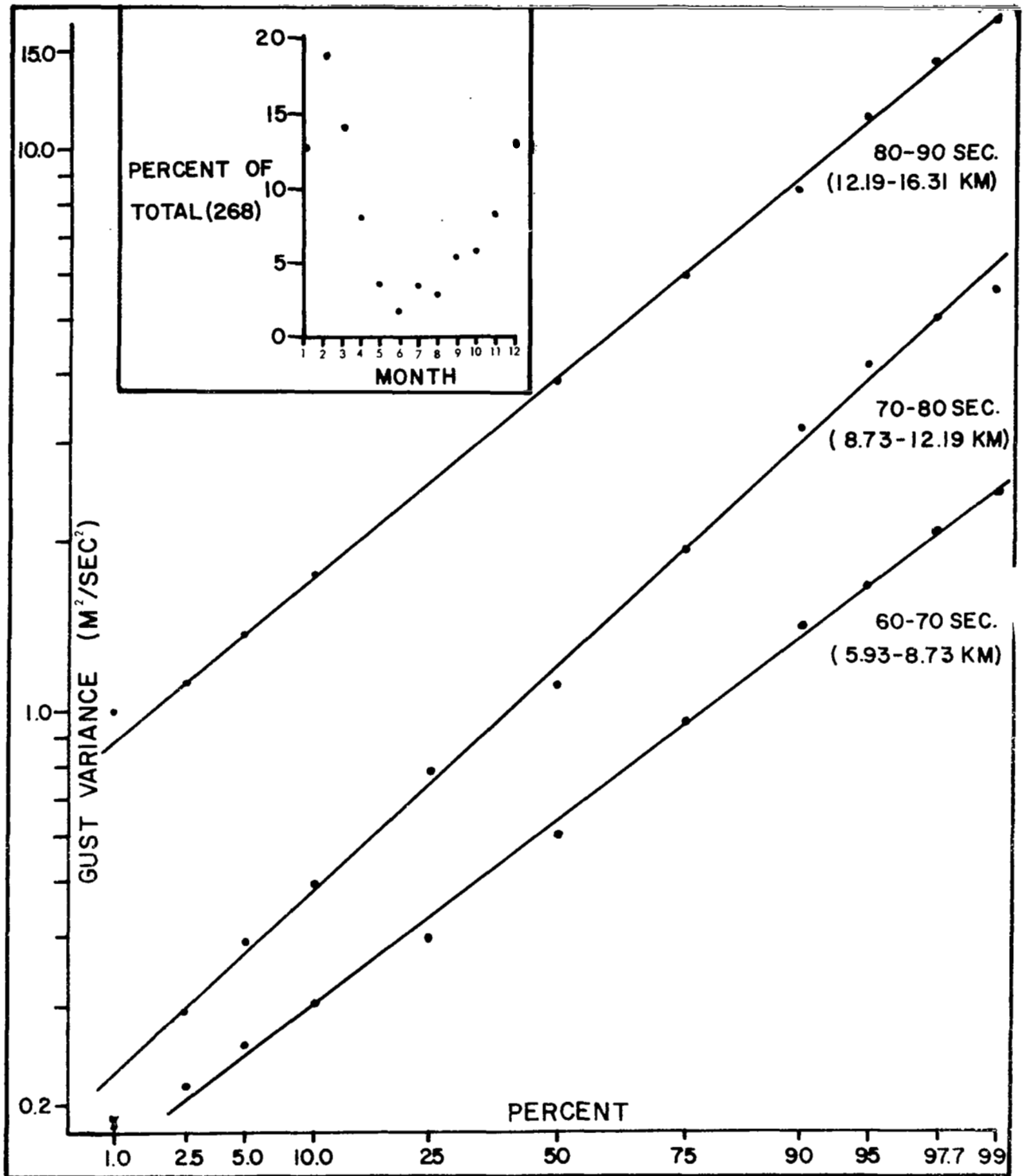


Figure 2.0 Cumulative Distribution of Gust Variance Computed for 268 Jimsphere Profiles for Three 10 Second Intervals of Saturn AS-504 Flight Time; at Upper Left is Distribution by Month of 268 Profiles Used

FREQUENCY (CPS)	PSD [(M/SEC) ² /(CYCLE/FT)]												
	MIN.	1.0	2.3	5.0	CUMULATIVE		FREQUENCY (%)			95.0	97.7	99.0	MAX.
					10.0	25.0	50.0	75.0	90.0				
0.3	0.3728	0.5535	0.6612	0.7731	0.9057	1.3092	1.9327	2.6919	3.5582	4.4052	5.2680	5.7102	7.9160
0.6	0.1365	0.1583	0.1975	0.2317	0.2788	0.3672	0.5123	0.6993	0.8798	1.0055	1.1828	1.3697	1.7266
0.9	0.0498	0.0525	0.0692	0.0813	0.0941	0.1199	0.1613	0.2164	0.2620	0.2983	0.3358	0.3650	0.6652
1.2	0.0202	0.0243	0.0303	0.0351	0.0402	0.0526	0.0690	0.0896	0.1172	0.1345	0.1537	0.1760	0.3916
1.5	0.0107	0.0158	0.0166	0.0185	0.0212	0.0285	0.0374	0.0510	0.0681	0.0868	0.1022	0.1374	0.1941
1.8	0.0063	0.0079	0.0097	0.0108	0.0127	0.0175	0.0237	0.0332	0.0497	0.0658	0.0837	0.1066	0.1583
2.1	0.0037	0.0052	0.0059	0.0077	0.0085	0.0114	0.0161	0.0241	0.0381	0.0554	0.0718	0.1024	0.1453
2.4	0.0021	0.0037	0.0043	0.0052	0.0061	0.0082	0.0120	0.0185	0.0309	0.0453	0.0676	0.0959	0.1621
2.7	0.0014	0.0029	0.0035	0.0044	0.0049	0.0066	0.0098	0.0157	0.0269	0.0412	0.0619	0.0896	0.1703
3.0	0.0013	0.0023	0.0026	0.0032	0.0041	0.0067	0.0093	0.0144	0.0267	0.0384	0.0578	0.0904	0.1555

Table 2.2 Cumulative Distribution of Power Spectrum Densities of 900 Jimsphere Profiles

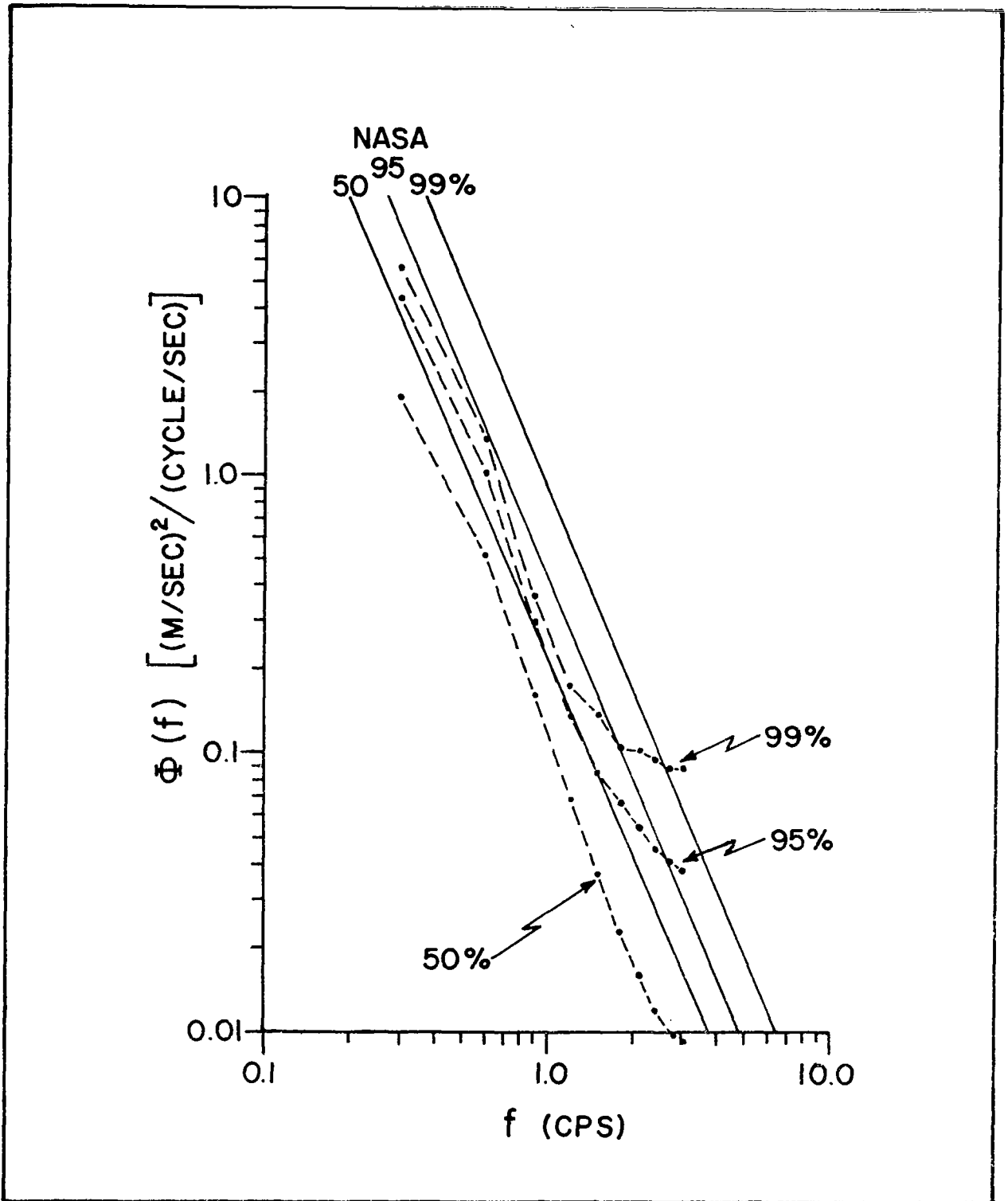


Figure 2.7 Median and 95 and 99% Upper Bounds of Power Spectrum Densities of 900 Jimsphere Wind Speed Gust Profiles from 4 to 14 km Over Cape Kennedy Computed in the Vehicle Time Domain (dots) and MSFC Design Spectra Bounds Computed in Altitude Domain and Transformed to Vehicle Time Domain (lines)

of maximum dynamic pressure, 12 km; for a Saturn vehicle v is 350 m/sec at 12 km and thus,

$$\Phi(f) = 11.4 \Phi(K) \quad (2.8)$$

similarly f (cps) is a function of K ,

$$f = \frac{Kv}{4.10^3} = 0.0875 K \quad (2.9)$$

As illustrated in Figure 2.7 the PSD's at the 50 percent level for the MSFC design spectra are larger by a factor of 1.5 to 2 at all frequencies when compared to the PSD's computed from vehicle time domain profiles; similarly at the 95 and 99 percent level for $f \leq 1.5$ cps the MSFC design spectra are larger by factors of 1.4 to 1.7 and 2.2 to 2.7 respectively; for $f > 1.5$ cps the PSD's at the 95 and 99 percent level for the vehicle time domain profiles decrease at a slower rate with increasing f and thus each are larger than the MSFC PSD's for $f > 2.5$ cps. These comparisons illustrate an apparent difference between spectra of profiles expressed in vehicle time coordinates and spectra of profiles in altitude coordinates; however the transformation of the spectra from one coordinate system to the other implied by Equations 2.8 and 2.9 is strictly valid only when v is not a function of altitude; when v is a function of altitude comparison of the spectra is not possible because a simple transformation does not exist. Therefore the data given in Table 2.2 represent the best estimates, based on Jimsphere profiles, of the distribution of PSD at various frequencies as viewed by a Saturn vehicle; other estimates based on transformation of altitude domain spectra to the vehicle time domain [Equations 2.8 and 2.9] are not strictly comparable.

To study the relation of the distribution of PSD to the distribution of maximum wind speeds and maximum vector shears of 900 Jimsphere profiles, PSD's were computed from 50 sets of 90 profiles that are associated with the deciles (90 profiles per decile for a set 900 data values) of maximum wind speed and maximum 100, 400, 1,000, and 3,000 m. vector shear for wind speeds increasing with altitude (as indicated by (+) sign). The 50, 95, and 99% PSD at 0.3, 0.6, 1.2, and 2.4 cps, plotted as a function of decile

for maximum wind speed and vector shears, are illustrated in the upper half of Figure 2.8. The tendency for the PSD to be larger at higher deciles of wind speed and shear is illustrated quantitatively in the lower half of Figure 8 in which the ratio of PSD at decile N (N = 1, 2 . . . 10) to PSD at decile 1 [PSD (N)/ PSD (1)] is plotted as a function of decile N.

The decile limits used in this analysis are given in Table 3.2 (Page 28)

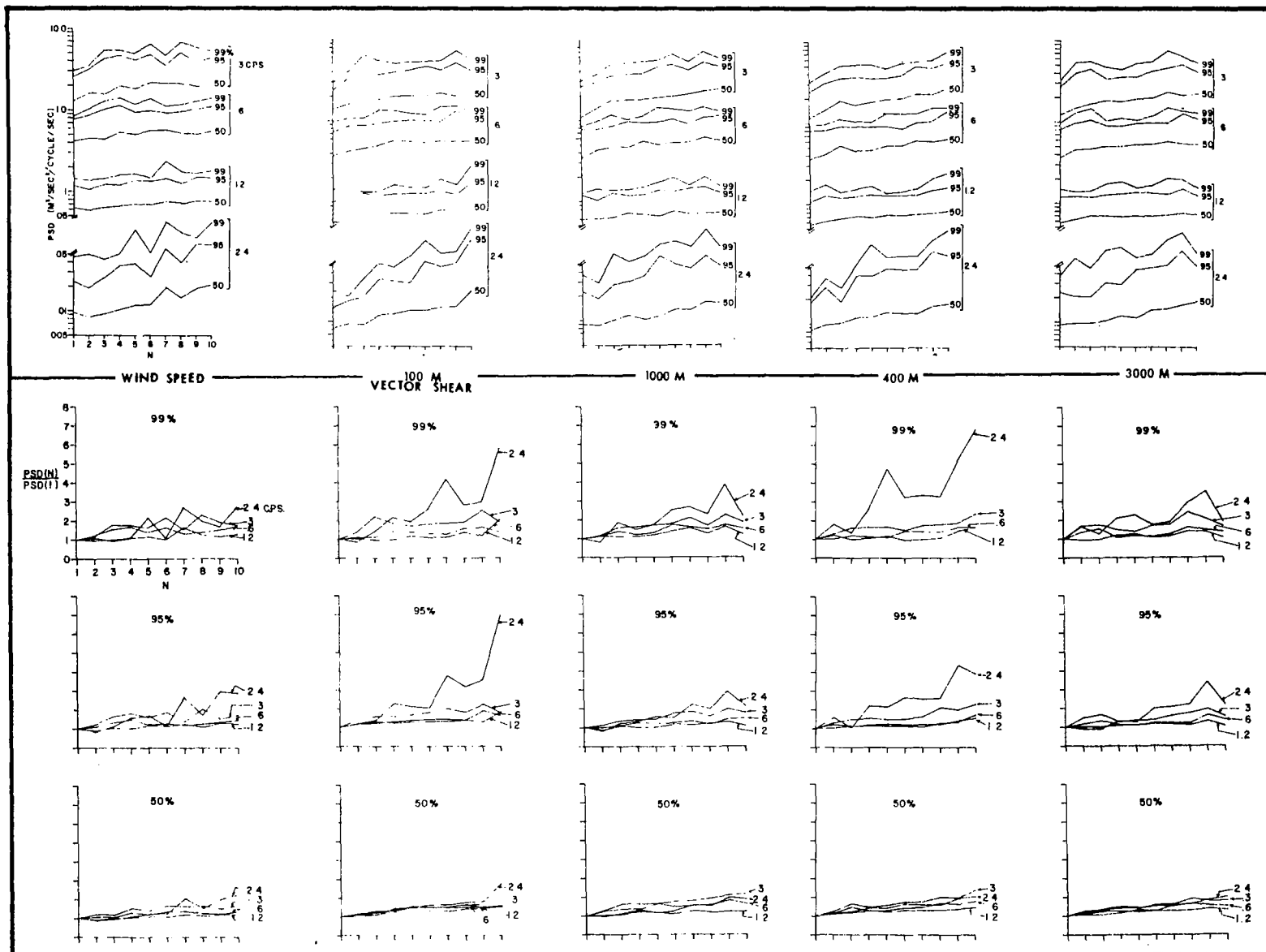


Figure 2.8 Upper Half: Median 95 and 99% Upper Bounds of PSD of Jimsphere Wind Speed Gust Profiles Associated with Deciles (90 Profiles per Decile) of Maximum Wind Speed and Maximum 100, 400, 1,000, and 3,000m Vector Shears; Lower Half: Ratio of Median, 95 and 99% Upper Bounds of PSD at Decile N ($N = 1, 2 \dots 10$) to PSD at Decile 1.

Section 3

WIND PROFILE SAMPLING

3.1 PROFILES

Wind profiles represent the variations with height of the horizontal motions of the atmosphere. In principle, a wind profile is a vector function of height, representing the variation of both the speed and the direction of the air movement, or wind. In practice, however, the variation of wind in the vertical usually is represented by two separate profiles, either for speed and direction or for the magnitudes of two orthogonal wind components. In this report, a method is offered for obtaining a representative sample of profiles from a collection of several hundred (or more) profiles, using order statistics.

Although profiles over a fixed point vary continuously in time, they are obtained routinely only every 6 or 12 hours at major weather stations; occasionally, research or operational requirements provide several consecutive wind observations, from which profiles can be obtained, at hourly intervals, or even more frequently. Horizontal air motion varies continuously with height, but instrumental and computational problems preclude obtaining wind information at intervals of less than 50 meters, usually much more. Routine upper wind information is available only at 1 km intervals, every 12 hours. Even so, in ten years more than 7,300 wind profiles accumulate for each station. For the entire United States during the 1960s, more than 1.5 million profiles were obtained, from the surface to heights of 30 km or more.

Wind profiles must be used in the formulation and testing of designs for vehicles intended to ascend or descend rapidly through the atmosphere, traversing layers in which the air motion may come from widely differing directions at highly variable speeds. But no engineer can hope to use all 1.5 million profiles in developing a new vehicle, or even the thousands available for the specific site from which the vehicle will be launched.

Some method of averaging or otherwise characterizing the profiles must be used.

Straight averages of wind speed and direction, level by level, are available, but are of little use to engineers. Their vehicles are most susceptible to the extremes, not the means, and in particular to the changes of wind with height. The difference between winds at two levels in the vertical shear of the horizontal wind. The difference between speeds of the wind at two levels, regardless of directions, is the scalar shear; the difference between the two wind vectors (involving both speed and direction) is the vector shear, which has both direction and magnitude.

Scalar shear may be positive (speed increasing with height) or negative, but the magnitude of vector shear is always positive. However, strong winds do not change much in direction with height, so very large vector shear magnitudes are virtually equivalent to the absolute values of the corresponding scalar shears. To distinguish between vector shears according to whether the wind speed increases or decreases with height, the vector shears, in this report, are given the sign of the corresponding scalar shears.

3.2 CRITERIA

Wind profiles, available in profusion, must be summarized in some way for the design and testing of aerospace vehicles. Such summaries may be either in the form of statistics representing the entire collection of available profiles, or may be in the form of a few profiles, either actual or synthetic, selected so as to be typical, in some way, or the entire collection.

Many statistical summaries, to varying degrees of sophistication, have been prepared of available wind data. Typically, they are based on winds represented, for each level, by two orthogonal components, the zonal (west-to-east) and meridional (south-to-north). The summaries offer the means and standard deviations of each component at each level, usually 1 km apart, and matrices of correlation coefficients, both within-component and cross-

component.

Within-component correlations are between like components at different levels, so that for a set of n profiles, each offering data at k levels, two sets of correlations are computed, one for each component, for a total of $k^2 - k$ coefficients. Cross-component correlations are between the zonal component at one level and the meridional component at that level as well as each of the other levels, and vice-versa; including the correlations at each of the k levels gives a total of k^2 cross-component correlations. Thus a complete statistical summary (without considering possible serial correlation from one profile to the next) includes $2k$ means, $2k$ standard deviations, $k^2 - k$ within-component correlations, and k^2 cross-component correlations, or a total of $3k + 2k^2$ numbers. When winds are available from the surface up to 20 km, $k = 21$ and the complete statistical summary has 945 numbers.

A few wind profiles have been synthesized from statistical summaries, starting with an extreme wind speed at a level of maximum effect on a vehicle, and using correlations to determine the corresponding winds at other levels. The extreme wind usually is the mean wind speed plus two standard deviations, a value that would have been exceeded in less than 5% of the observations, if the wind speed were normally distributed. Even if such an assumption of normality were justified, the probability of the complete statistical profile cannot be established because of inter-dependence of the correlations.

The first profiles for design of missiles and space vehicles were less sophisticated. Essentially they were the observed profiles which included the strongest winds at the level of maximum effect. Variations on this approach included selection of not only the profiles containing the strongest winds but also those with the greatest wind shears above and below such winds.

Another approach was to calculate the actual effect induced upon a typical space vehicle by each of a great many profiles, and then selecting those profiles which produced the strongest effects. This sample was then presumed to be equally useful for other vehicles having responses to wind not greatly different from those of the typical vehicle.

The considerations inherent in these procedures have been used in the present study in a different way. From a large number of profiles, a sample is selected which has the same characteristics with respect to maximum wind speed and to wind shears over certain thicknesses.

3.3 PROFILE CODING

A wind profile represents wind speeds and directions (or strengths of two components) at many heights. From these values, wind shears for many thicknesses can be computed. While all of these quantities may be of some interest, only a few can be considered critical. After these critical characteristics are identified, from aerodynamic or other considerations, each profile can be classified according to them.

The critical characteristics, designated as c_1, c_2, \dots, c_j , may be, for example, the strongest wind at any level between 5 and 15 km, the greatest positive (speed increasing with height) vector wind shear over a 1 km layer within the same interval, the strongest negative 100 m shear, etc. Once these characteristics have been selected, values of each characteristic for the entire collection of profiles are assembled, and placed in rank order.

Thus, all the soundings are placed in sequence according to the magnitude of c_1 , without regard to date or to any other characteristics. This ordering is then divided into equal numbers of soundings; for the present development, this number is taken as 10, but can be any other convenient number, such as 5 or 8 or 20. Then each profile is given an identifier according to the decile in which its value of c_1 falls. The 10 percent of all the

profiles in which c_1 is smallest receive a code number of 1, the next 10 percent are coded 2, and so up to the 10 percent with the largest values of c_1 , which are coded as 10.

The same process is repeated for each of the other characteristics, so that each profile eventually has a sequence of code numbers, one for each characteristic. The numbers indicate in which decile the profile falls with respect to each critical characteristic, and permit the profiles to be sorted and classified in various ways, including selection of representative samples.

From the large collection of profiles, a sample may be drawn so that each decile of each characteristic is represented by at least m profiles. This criterion can be shown simply by an array, or matrix, in which the rows represent the characteristics and the columns the deciles (Table 3.1).

TABLE 3.1

SCHMATIC OF DECILE CODING SCHEME

	Deciles									
	1	2	3	4	5	6	7	8	9	10
c_1	.	.	.	1
c_2	1
--										
c_j	.	1

In Table 3.1, a single profile with code 4 5 . . . 2 is indicated. As soundings are added to the sample, the number of profiles falling into each cell is tallied, and profiles are accepted until all cells have at least m entries.

Alternatively, an upper limit may be placed on the number of entries per cell. Profiles are added to the sample, one at a time, unless such addition would cause some cell to have more than the desired number, m . Such a profile is rejected, and the next one examined, with the process continuing until all cells have m entries - - or the entire collection is exhausted, with some cells still having less than m entries.

3.4 APPLICATION

To test this procedure for obtaining representative samples of wind profiles, five critical characteristics were established and a collection of 900 Jimsphere wind profiles were classified and sorted. These profiles represent winds observed at 50-meter intervals from the surface to 14 km over Cape Kennedy, Fla.; they were selected from a set of 1194 profiles obtained from 28 Nov. 1964 through 11 May 1967 by discarding all profiles with any missing data at any level from 1 to 14 km. The complete 1194-profile set was examined in detail by Adelfang, Ashburn, and Court (Ref. 1). More intensive study showed that 16 listed profiles actually had no data, and 11 were exact duplicates of previous profiles.

The five critical characteristics, restricted to the range from 4 to 14 km, were:

- c_1 : maximum wind speed at any level in the profile;
- c_2 : maximum "positive" vector shear over any 100-meter interval;
- c_3 : maximum "negative" vector shear over any 100-meter interval;
- c_4 : maximum "positive" vector shear over any 1 km interval;
- c_5 : maximum "negative" vector shear over any 1 km interval.

Thus, the lowest 100-meter shear considered was from 3900 to 4000 meters, while the lowest 1 km shear was from 3000 to 4000 meters. In several cases this definition caused the discarding of strong 100-meter shears below 4000 meters, while 1 km shears including this 100-meter shear were accepted.

Nevertheless these five characteristics were assumed to represent the major aspects of wind profiles of importance in space vehicle design. The sampling methodology would work equally well for other characteristics.

To test the representativeness of samples based on these five characteristics, four other vector shears were identified and coded by deciles for each profile; also only for shears for which the upper boundary was between 4 and 14 km:

- c_6 : maximum "positive" vector shear over any 400-meter interval;
- c_7 : maximum "negative" vector shear over any 400-meter interval;
- c_8 : maximum "positive" vector shear over any 3 km interval;
- c_9 : maximum "negative" vector shear over any 3 km interval.

These nine characteristics and their altitude of occurrence were identified in each of the 900 Jimsphere wind profiles, as shown in Appendix I. Each set of characteristics was then placed in rank order, and grouped into deciles. Limits of the deciles for each of the nine characteristics, for the 900 profiles, are given in Table 3.2 and graphed in Figure 3.1; various cumulative percentiles of the altitude of occurrence are also graphed in Figure 3.1. The only characteristic to have a lower limit of zero was the 3 km negative shear; actually, 41 profiles had no negative 3 km shears, indicating that these profiles, if smoothed by 3 km moving averages, would show winds continually increasing with height.

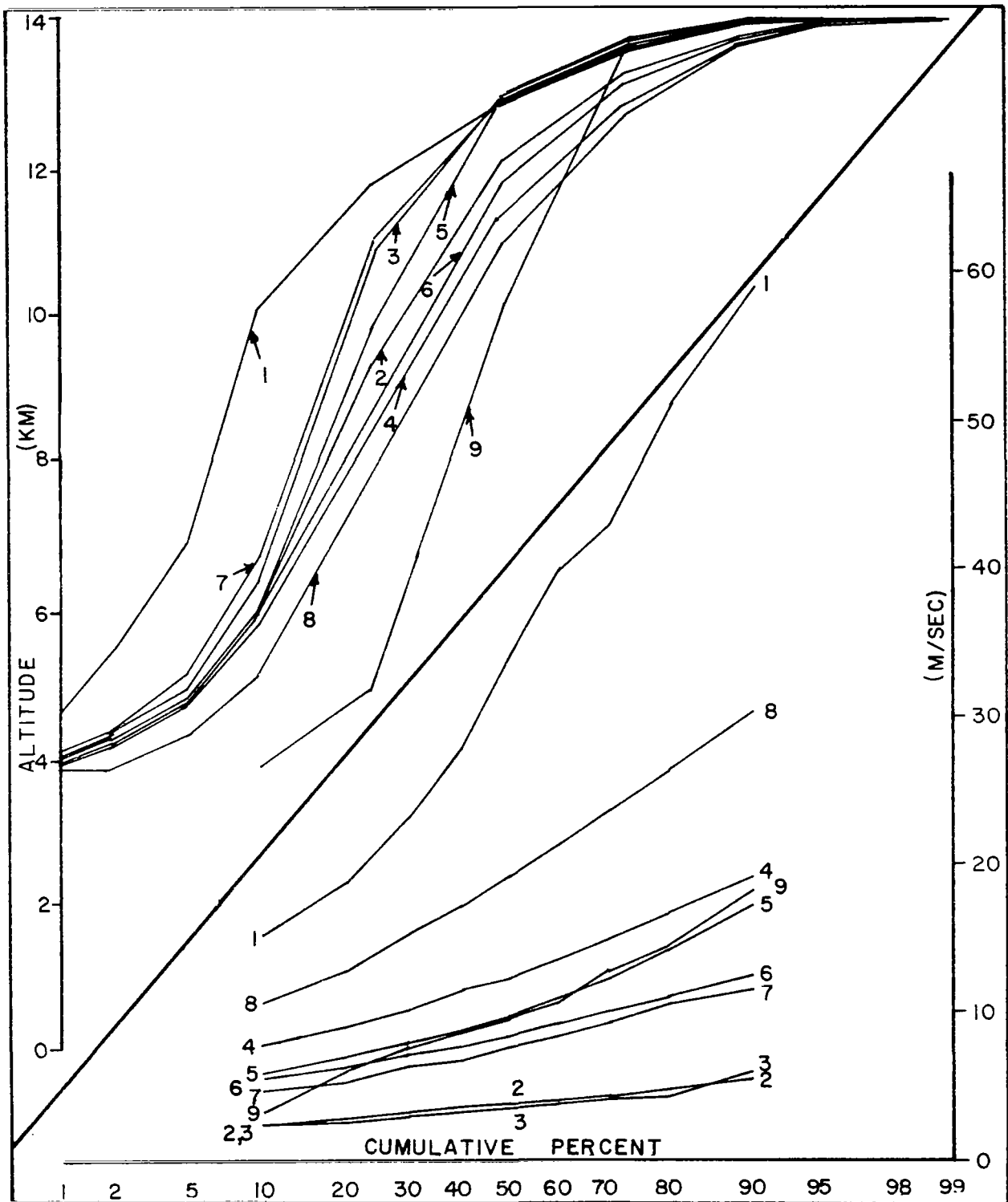


Figure 3.1 Cumulative Decile Limits and Percentiles of Corresponding Altitudes for 5 Selection Characteristics (1-5) and 4 Test Characteristics (6-9).

TABLE 3.2

LIMITS OF DECILES FOR EACH OF 9 CHARACTERISTICS OF
900 JIMSPHERE PROFILES. UNITS ARE METERS PER SECOND.

DECILE:		1	2	3	4	5	6	7	8	9	X
LIMITS:	MIN	10	20	30	40	50	60	70	80	90	MAX
MAX WIND SPEED	5.3	15.1	18.8	23.3	27.5	33.8	39.5	45.3	50.7	59.2	81.7
100m SHEAR POS	1.7	2.6	3.0	3.3	3.6	3.9	4.1	4.5	4.9	5.6	14.2
NEG	1.6	2.5	2.8	3.1	3.4	3.7	4.0	4.4	3.9	5.7	19.1
1 km SHEAR POS	3.7	7.8	9.1	10.2	11.5	12.3	13.5	15.0	17.0	19.5	48.0
NEG	2.3	6.0	7.1	8.0	8.9	9.9	11.0	12.3	14.2	17.4	33.5
400m SHEAR POS	2.8	5.6	6.5	7.2	7.8	8.4	9.3	10.1	11.1	12.6	24.1
NEG	3.1	4.8	5.5	6.4	6.9	7.7	8.5	9.5	10.7	12.7	20.0
3 km SHEAR POS	2.7	10.6	12.8	15.4	17.2	19.1	21.2	23.6	26.4	30.3	97.0
NEG	0.0	3.3	6.1	7.5	8.7	9.9	10.9	12.6	14.7	18.4	38.3

When all nine characteristics are used to typify a profile, 4 pairs of the 900 profiles were identical. Their codings (in codes, the tenth decile is indicated as X) were:

1 11 11 11 13 at 0100Z on 26 Jul 66 and at 1503Z on 9 Aug 66;
 1 11 12 11 13 at 0432Z on 11 Aug 65 and at 0100Z on 20 Aug 65;
 3 11 11 11 13 at 0906Z on 16 Sep 66 and at 0100Z on 21 Sep 66;
 X 7X XX XX XX at 1300Z on 20 Jan 65 and at 0215Z on 24 Feb 66.

These four were among 34 sets of two or more profiles which were coded identically with respect to the five primary characteristics: 1 quintuplet, 3 quadruplets, 3 triplets, and 27 doublets (Table 3.3)

TABLE 3.3

REPEATED CODINGS AMONG 900 JIMSPHERE PROFILES, WITH
TIME AND DATE OF SOUNDINGS. (IN CODE, X = 10)

*11111	1300Z	7Jul65	0100Z	6Aug65	0100Z	26Jul66	1503Z	9Aug66
*11112	1300Z	14Jul65	0432Z	11Aug65	0100Z	20Aug65	0100Z	60ct66
11113	0932Z	11Aug65	1300Z	20Sep65				
11121	1300Z	9Sep65	0159Z	13Jul65	1300Z	8Jul66		
11211	0101Z	18Aug65	1533Z	9Aug66				
11212	0102Z	28Aug65	0100Z	20Sep65				
12111	1300Z	3Aug65	1445Z	11Aug65				
12314	1300Z	16Jul65	1400Z	6Sep66				
21111	1901Z	2Jul65	0100Z	19Aug65	0806Z	16Sep66		
21112	1847Z	2Jul65	1746Z	15Sep66				
21124	0100Z	25Jun66	0100Z	1Dec66				
21213	0330Z	25Aug66	1004Z	12Sep66				
*31111	0906Z	16Sep66	0100Z	21Sep66				
31121	0100Z	29May65	0100Z	16Aug65				
33214	2030Z	14Sep65	0100Z	10Dec65				
37335	2135Z	18Apr67	2240Z	18Apr67				
45153	2300Z	19Oct65	1445Z	15Mar67				
46448	1417Z	28Sep65	0125Z	24May66				
48472	2330Z	22May65	1300Z	21Apr67				
4XX68	0440Z	30May66	0500Z	4Jul66				
69874	1732Z	17Feb67	1732Z	17Feb67				
7XX77	1302Z	24Mar66	2101Z	3Feb67				
886XX	0100Z	3Mar66	1302Z	1Mar67				
9XX99	1228Z	5Apr66	1728Z	5Apr66				
9XXX	0101Z	20Jan65	1300Z	6Jan66				
X6788	1607Z	5Apr66	0835Z	8Apr66				
X797X	2230Z	27Jan65	1715Z	25Feb66				
*X7XXX	1300Z	20Jan65	0215Z	24Feb66				
X8X99	1549Z	28Mar66	0100Z	10Feb67				
X8X9X	1300Z	19Jan66	1306Z	29Nov66				
X8XXX	1213Z	28Mar66	1800Z	7Apr66				
X99XX	0715Z	26Feb66	0945Z	26Feb66	1653Z	28Mar66	1134Z	29Mar66 1300Z 7Apr66
XXX9X	1001Z	10Mar65	0100Z	2Feb66				
XXXXX	0100Z	9Mar65	0151Z	10Mar65	1318Z	27Jan66		

*Identical for all nine characteristics on two of dates listed.

3.5 RELATIONS

Several interesting relations among the 900 profiles were revealed when they were coded by 9-digit numbers, according to the decile of each of 9 characteristics.

The four test characteristics, maximum 400-meter and 3 km positive and negative shears, had been originally selected because of presumed independence from the selection characteristics, maximum wind speed and maximum 100-meter and 1 km positive and negative shears. However, three of the four test characteristics were found to be strongly related to the selection characteristics. The fourth, the maximum 3 km negative shear, had very little relation to any of the other eight characteristics.

These relations were found from bivariate listings of all the 900 profiles by the deciles in which they fell according to pairs of characteristics. The 36 possible two-way comparison tables are given in Appendix II. For quick computation, each table was partitioned into four quarters, and the number of entries in one quarter was counted. Because each line and each column in a table represents a decile, it contains 90 entries, and the sum of two quarters, horizontally or vertically, is 450. Thus the total in each quarter differs from $900/4 = 225$ by the same amount, and only one quarter need be counted. These differences are given in the upper right part of Table 3.4.

The net difference between any quarter's total and 225 is an index of the correlation between the two characteristics of the table. Divided by 225, this number is analogous to a coefficient of medial correlation, because the division into quarters effectively classified the characteristics by their medians. The coefficient of medial correlation, q , from a sample of n independent pairs, has a sampling variance of approximately $(1 - q^2) / n$, so that for $n = 900$ any value of q greater than 0.06 differs from zero at the 95% confidence level.

TABLE 3.4

MEDIAL COMPARISONS BETWEEN PAIRS OF CHARACTERISTICS

MAXIMUM:		(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)
WIND SPEED	(1)	-	73	93	107	77	85	73	143	22
100m SHEAR POS	(2)	.35	-	89	88	53	114	66	73	29
100m SHEAR NEG	(3)	.41	.40	-	80	102	89	134	80	37
1 km SHEAR POS	(4)	.48	.39	.36	-	83	134	60	136	37
1 km SHEAR NEG	(5)	.34	.24	.45	.37	-	74	124	68	66
400m SHEAR POS	(6)	.38	.51	.40	.60	.33	-	38	97	41
400m SHEAR NEG	(7)	.32	.29	.60	.36	.55	.39	-	79	53
3 km SHEAR POS	(8)	.64	.32	.36	.60	.39	.43	.35	-	52
3 km SHEAR NEG	(9)	.10	.13	.16	.16	.29	.18	.24	.23	-

Values of the medial correlation are given in the lower left of Table 3.4. All correlations are positive and significantly greater than 0. Lines separate the first five selection characteristics from the last four test characteristics. The largest correlations appear between the two groups, especially between the positive 100m and 400m maximum shears, the 100m and 400m negative shears, and maximum wind speed and positive 3 km shear. The highest correlation within the selection group is .48, within the test group .43, but 6 of the 20 inter-group correlations are larger than .50. Least correlation is shown by the 3 km negative shear, for which the maximum correlation, .29, is with 1 km negative shear.

3.6 SAMPLING

The 900 profiles were sampled, to fill up the matrix of five characteristics vs. deciles (Table 3.1), in three different ways: in direct chronological order, in reverse chronological order, and after complete randomization; in the following discussion, these are termed Direct, Reverse, and Random. Five different randomizations were used, so that 7 samples were drawn. These sampling orders were used repeatedly, for lower and upper limits of 1, 2, 3, 4, and 5 entries per cell.

The number, n , of profiles in samples with at most m entries per cell, and in samples with at least m entries per cell, for $m = 1, 2, 3, 4, 5$, is given in Table 3.5, together with the ordinal (N) of the last profile used in the sample. These two numbers are presented as a fraction, n/N , which suggests the efficiency of the sampling procedure. For example, when the 900 profiles were examined in Direct (chronological) order to obtain at least $m = 2$ entries per cell, a total of 44 profiles were accepted. The 44th was the 151st profile examined, after which the examination stopped without considering the remaining 749 profiles. But when the same Direct sequence was examined to obtain at most $m = 2$ entries per cell, only 17 profiles were accepted, the 17th being the 571st examined. But since some cells still did not have 2 entries, the remaining 329 profiles were all examined, to no avail.

In general, seeking at least m entries per cell involved examining $N = 2m$ to $3m$ or more profiles in Direct or Inverse order but less than $2m$ Random order profiles to meet the criterion. At most m entries, however, was never attained, even though all 900 profiles were examined. The values of n in Table 3.5 are shown in Figure 3.2, for all five random sampling arrangements. In Figure 3.2, the diagonal line represents the optimum number, if each cell had exactly m entries.

When an upper limit is placed on cell content, the actual number of profiles in the sample is about 90% of optimum, for each sampling sequence. But when a lower limit is imposed, many more profiles are used in the Direct and Reverse procedures than for Random. This effect is also seen in the actual matrices developed for each process: both Direct and Reverse ordering resulting in many cells having larger excesses above the minimum than for any of the 5 Random samples. Hence, further discussion will concentrate on the results of the Random sampling.

The actual numbers of entries per cell for each of the selection characteristics (c_1, c_2, c_3, c_4, c_5), and also the number of entries for the four test characteristics (c_6, c_7, c_8, c_9), are given in Appendix III for each of five Random sampling sequences, used to select at least and at most m entries per cell.

3.7 VALIDATION

To summarize the figures in the fifty 9×10 matrices in Appendix III, the deciles have been grouped into three classes, low (1-3), middle (4-7), and high (8-10). For each class, all the entries for the five selection characteristics were totaled, and similarly for the four test characteristics. Ideally, the low and high classes should each have 30 percent of the entries, and the middle class 40 percent.

The actual proportions, computed to tenths of a percent and expressed as

TABLE 3.5

NUMBER OF PROFILES USED (n) AND ORDINAL (N) OF LAST PROFILE USED,
 IN COMPLETING DECILE MATRIX WITH AT LEAST m PROFILES PER
 CELL AND IN ATTEMPTING TO COMPLETE WITH AT MOST m PROFILES
 PER CELL, FROM 2 ORDERED AND 5 RANDOM SEQUENCES OF 900 WIND PROFILES.

	m: 1	2	3	4	5
<u>At least m</u>					
Direct	-	44/151	62/152	81/158	87/160
Inverse	-	44/158	62/220	80/222	96/229
Random 1	23/32	37/73	52/86	64/100	74/103
Random 2	21/39	40/53	51/100	63/103	75/109
Random 3	21/57	36/62	50/73	59/95	72/102
Random 4	19/63	35/78	50/79	64/86	75/103
Random 5	21/26	33/40	48/57	61/89	75/94
<u>At most m</u>					
Direct	-	17/571	26/571	35/639	46/247
Inverse	-	17/856	24/883	34/280	44/599
Random 1	8/531	17/397	26/567	34/448	46/374
Random 2	8/493	17/256	27/767	38/589	46/831
Random 3	8/842	19/807	26/292	35/842	44/886
Random 4	8/520	16/743	26/561	35/776	45/776
Random 5	8/373	16/821	27/847	36/847	45/720

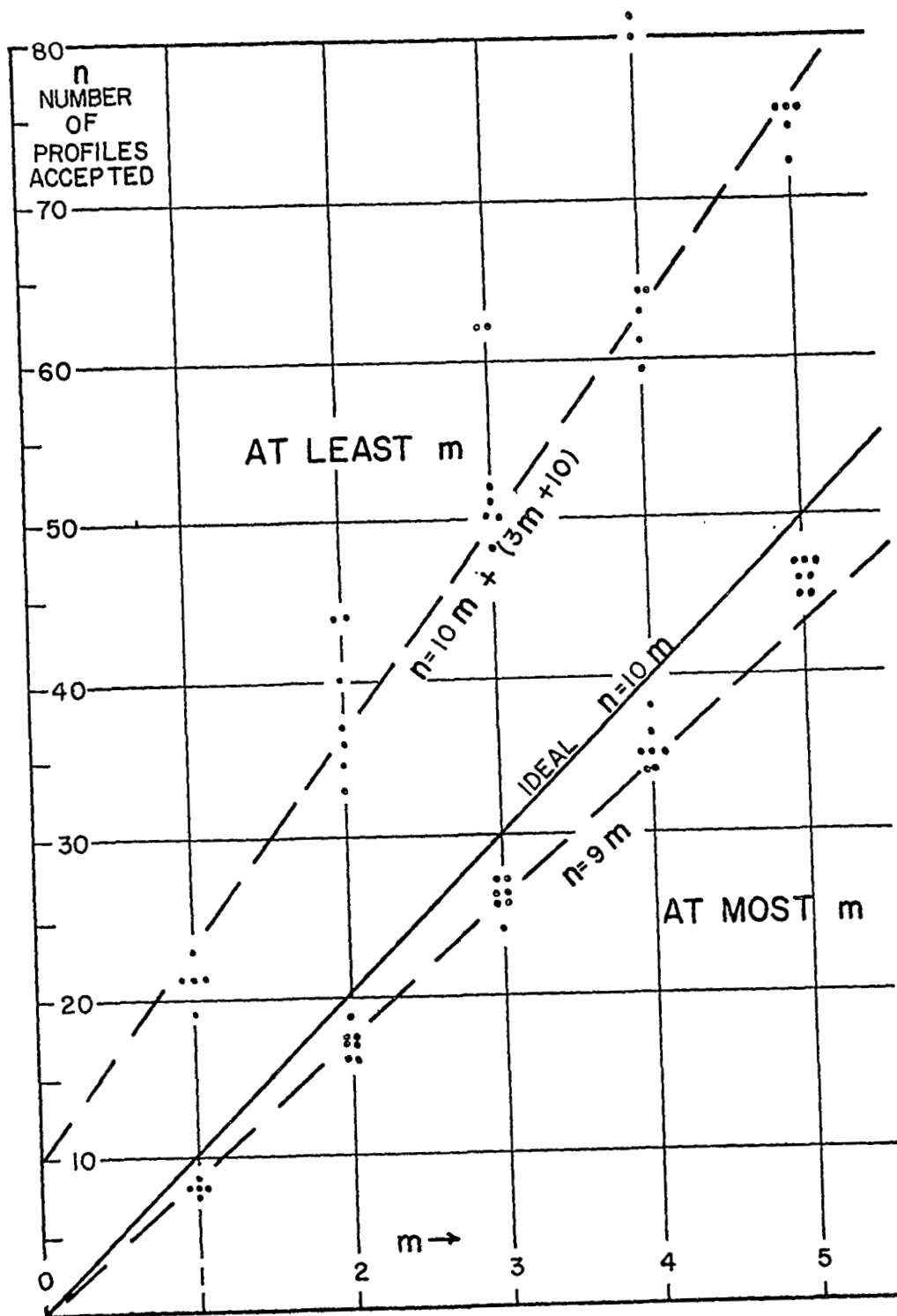


Figure 3.2 Number of Profiles Accepted (n) in Seeking at Least or at Most m Entries per Cell for Five Random Sampling Arrangements; Diagonal Line represents the Optimum Number, if Each Cell has Exactly m Entries.

parts per thousand for convenience (eliminating the decimal point), are given in Table 3.6 for each of the 5 Random sequence selections. These numbers, in turn, are shown by bars in Figure 3.3.

In each of the 50 samples, the number of entries in the three groups was gratifyingly close to the ideal figures. Since the upper extremes of wind speed and wind shear are of greatest practical interest, only the high group need be examined here. The actual percentages obtained in the sampling procedure varied from 26.7 (Random sequence 2 for at least 4) to 37.5 (Random sequence 4 for at most 1), for the selection characteristics, and from 19.0 (Random sequence 5 for at least 1) to 50.0 (Random sequence 1 for at most 1).

Together, the 5 Random sequences slightly overemphasized the high deciles for the selection characteristics, giving them from 29.9 (at most 5) to 34.5 (at least 1) percent of the cell entries. But for the test characteristics the high deciles were underemphasized: 26.1 for at least 1, 31.8 for at most 1. In the grand average, for all sequences for all values of m , the high deciles obtained 31.3 of all entries for selection characteristics, 28.9 for test characteristics.

As another test of how well the decile coding and sorting provided samples representative of the entire population of 900 profiles, spectrum densities for each of the profiles in one sample were extracted. Chosen were the five groups of profiles obtained in seeking at most 3 entries per decile cell. As shown in Table 3.5 and Figure 3.2, three of these groups had 26 profiles each and two had 27 each. For ease in comparison, however, each group was reduced to 25 profiles, by eliminating the 26th and 27th to be selected.

Serial numbers of the 25 profiles making up each stratified sample are given in Table 3.7. Although only 900 profiles were available for sampling, the serial numbers run from 1 to 1186, because 286 profiles in the original tabulation were rejected for not being complete from 1 to 14 km, or being duplicates of other profiles. In each of the five stratified samples, the pro-

TABLE 3.6

RELATIVE NUMBERS (PER THOUSAND) OF ENTRIES IN 3 GROUPS OF DECILES (LOW, MIDDLE, HIGH) FOR ALL 5 SELECTION CHARACTERISTICS (LEFT NUMBERS) AND ALL 4 TEST CHARACTERISTICS (RIGHT NUMBERS) WHEN 5 RANDOM SEQUENCES ARE USED TO SELECT PROFILES TO FILL MATRICES WITH AT LEAST m AND AT MOST m ENTRIES PER CELL.

Random Sequence	AT LEAST m				AT MOST m			
	1-3	4-7	8-10	Deciles	1-3	4-7	8-10	
	\bar{m}			\bar{m}				
1	1	235/228	426/424	339/348	1	300/281	350/219	350/500
	2	303/311	373/385	324/304	2	282/309	400/338	318/353
	3	312/303	377/394	312/303	3	282/308	385/317	323/375
	4	309/281	369/414	322/315	4	300/294	388/360	312/346
	5	308/277	359/405	332/318	5	291/255	400/424	309/321
	Avg	293/280	381/404	326/316	Avg	291/289	385/332	322/379
2	1	343/274	333/440	324/286	1	225/125	425/500	350/375
	2	320/244	400/513	280/244	2	294/250	388/441	318/309
	3	310/260	419/500	271/240	3	289/250	400/440	311/306
	4	324/282	410/480	267/238	4	289/243	400/454	311/303
	5	304/273	408/460	288/267	5	313/293	396/440	291/266
	Avg	320/267	394/479	286/255	Avg	282/232	402/455	316/312
3	1	222/286	472/429	306/286	1	300/281	350/438	350/281
	2	250/285	433/424	317/292	2	305/289	389/408	305/303
	3	268/300	428/405	304/295	3	300/317	400/375	300/308
	4	275/305	420/381	305/314	4	280/329	446/386	274/286
	5	297/299	417/399	286/302	5	286/341	418/375	295/284
	Avg	262/295	434/408	304/298	Avg	294/311	401/396	305/292
4	1	295/289	400/513	305/197	1	325/250	300/531	375/219
	2	274/271	394/471	331/257	2	288/266	375/453	338/281
	3	272/275	392/480	336/245	3	300/269	408/471	292/260
	4	266/270	409/475	325/255	4	297/279	383/443	320/279
	5	293/297	403/460	304/243	5	307/295	382/454	311/251
	Avg	280/280	400/480	320/239	Avg	303/272	370/470	327/258
5	1	343/357	381/452	276/190	1	275/313	425/469	300/219
	2	273/288	376/402	352/311	2	275/297	400/469	325/234
	3	313/318	350/375	338/307	3	304/306	393/417	304/278
	4	331/290	361/423	308/286	4	317/299	378/417	306/285
	5	331/300	357/403	312/297	5	307/294	404/411	289/294
	Avg	318/311	365/411	317/278	Avg	276/302	400/437	305/262
Grand Avg	Avg	295/298	395/436	311/277	Gr.Avg	294/281	391/418	315/301
	1	287/287	402/451	310/261	1	285/250	370/431	345/318
	2	284/280	395/439	321/282	2	289/282	390/422	321/296
	3	295/291	393/431	312/278	3	295/290	397/404	306/305
	4	301/286	394/435	305/279	4	297/289	403/412	300/299
	5	307/289	389/425	304/286	5	301/296	400/421	299/283

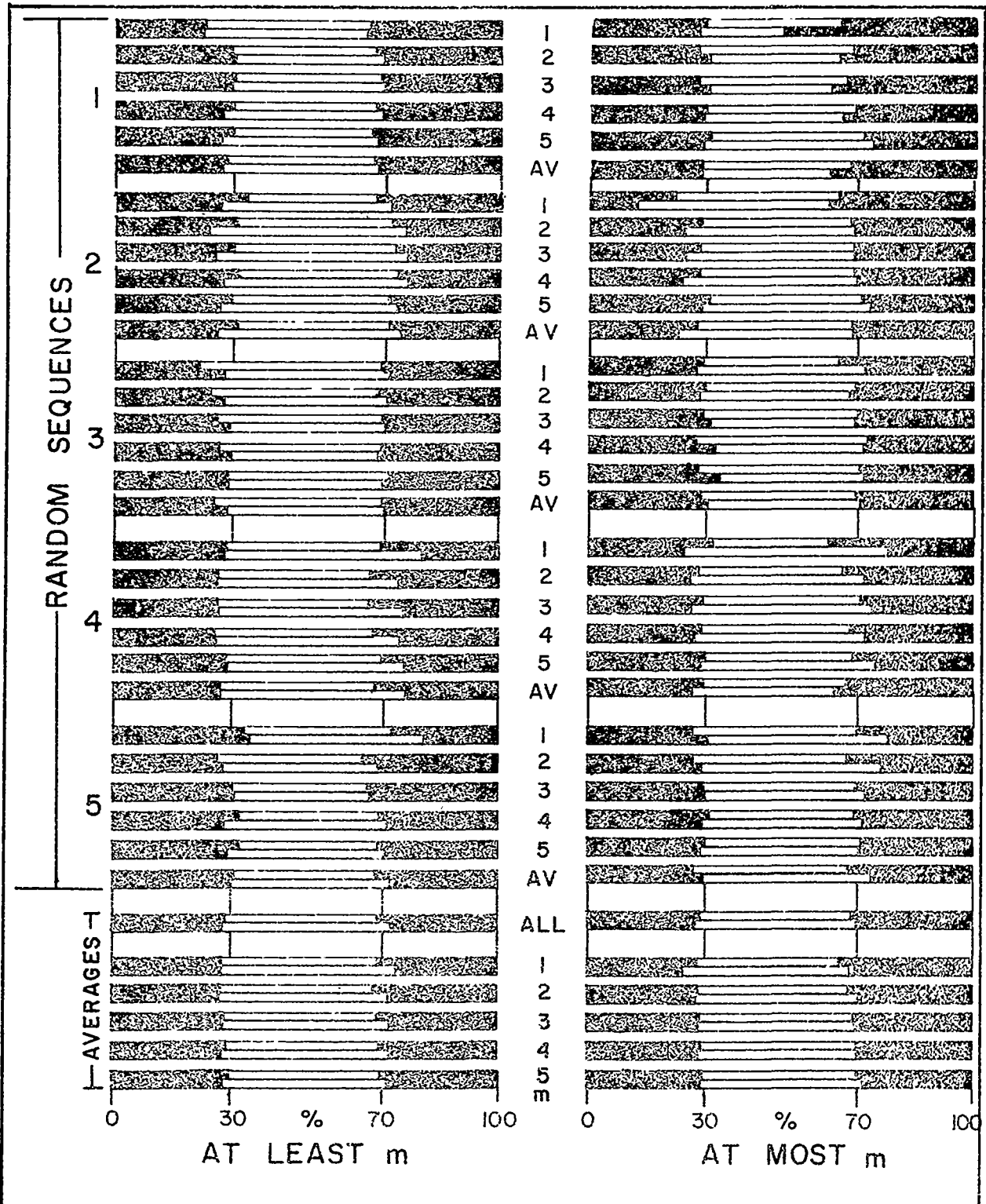


Figure 3.3 Percent of Entries in Low (1-3), Middle (4-7), and High (8-10) Deciles of Wind Characteristics in Samples Obtained from Random Sequences of Wind Profiles.

TABLE 3.7

COMPOSITION OF 5 STRATIFIED RANDOM SAMPLES OF
WIND PROFILES FROM TOTAL SAMPLE OF 900 PROFILES
OVER CAPE KENNEDY, FLORIDA. NUMBERS ARE IDENTIFICATION
NUMBERS OF PROFILES IN BASIC SAMPLE.

<u>RS 1</u>	<u>RS 2</u>	<u>RS 3</u>	<u>RS 4</u>	<u>RS 5</u>
1092	731	511	1042	696
251	323	1157	595	66
997	723	860	679	380
864	820	1034	1144	595
67	533	340	913	1041
197	168	344	1191	413
562	292	917	107	763
665	630	1063	674	492
88	827	715	649	426
802	487	358	1009	933
634	688	973	533	1175
637	1109	878	763	780
457	319	608	113	388
1008	995	4	370	718
878	677	54	13	44
623	348	160	1031	1135
1089	643	392	895	207
455	992	240	271	469
852	735	411	902	324
325	1173	822	653	208
340	85	432	844	56
314	1027	695	492	708
363	299	942	266	200
963	711	1113	707	459
713	791	545	180	470

files appear to have been drawn from the entire number with no bias.

For each group of 25 profiles, six spectrum densities at 10 frequencies are given in Table 3.8, and graphed in Figure 3.4. Values are in $(m/sec)^2/(cyc/sec)$. At each frequency from 0.3 to 3.0 cycles/second, the densities shown are the minimum, 5th, 10th, 15th, and 20th smallest, and the largest. For comparison, the corresponding percentile values of the densities in the entire population are also shown.

In Figure 3.4, the lines connect the densities for the entire 900 profile sample, and the vertical bars indicate the range of the values for the 5 stratified Random samples. At each frequency, the maximum and minimum densities of the 5 samples do not attain the whole-sample values, but at the four intervening percentiles the range of the 5 sample values includes the whole-sample density.

On the whole, the spectrum of any one of the 5 stratified Random samples appears to offer a fair approximation to that of the whole sample. This investigation of 5 stratified samples, chosen arbitrarily from those available from the decile coding procedure, suggests that the method does indeed provide suitable samples of wind profiles.

Whether a stratified sample should be drawn by the "at most m " or "at least m " criterion depends on several factors. The former provides smaller samples, and is the only one available for samples of 25 or less, as long as decile coding is used. However, the selection characteristics could be coded in fewer (q) categories, such as quartiles ($q = 4$) or quintiles ($q = 5$). If quartiles are used, presumably samples of only 6 or 7 would be provided by a criterion of "at most 2" and of 12 to 15 by "at least 2".

The "at least m " criterion is more efficient, in that the selection process stops as soon as the minimum is reached in all cells, while the "at most m " criterion requires scanning of the entire set of available profiles in an

TABLE 3.8

SPECTRUM DENSITIES AT 10 FREQUENCIES OF 5 STRATIFIED RANDOM SAMPLES OF 25 WIND PROFILES EACH, AND OF ENTIRE SAMPLE OF 900 PROFILES OVER CAPE KENNEDY. GIVEN, IN $(\text{m/sec})^2/(\text{cyc/sec})$, ARE MINIMUM AND MAXIMUM VALUES AND 5TH, 10TH, 15TH, AND 20TH ORDERED VALUES IN EACH RANDOM SAMPLE AT EACH FREQUENCY, AND CORRESPONDING PERCENTILE VALUES OF TOTAL SAMPLE.

		CYCLES PER SECOND									
		0.3	0.6	0.9	1.2	1.5	1.8	2.1	2.4	2.7	3.0
<u>MAX</u>											
RS 1		4.553	1.052	.2881	.1467	.0859	.0699	.0594	.0688	.0837	.0879
RS 2		4.923	0.985	.3205	.1467	.1577	.1504	.1296	.1274	.1284	.1233
RS 3		7.748	1.549	.3810	.1537	.1096	.0904	.0709	.0680	.0681	.0907
RS 4		5.275	1.209	.3300	.0528	.0902	.0746	.0718	.0769	.0725	.0667
RS 5		5.246	1.005	.2566	.1240	.0961	.0732	.0622	.0642	.0413	.0263
TOT		7.916	1.727	.6652	.3916	.1941	.1583	.1453	.1621	.1703	.1555
<u>80 %</u>											
RS 1		3.402	0.828	.2397	.0884	.0570	.0421	.0331	.0244	.0174	.0149
RS 2		3.052	0.702	.2240	.0861	.0485	.0363	.0232	.0223	.0208	.0190
RS 3		2.756	0.745	.2439	.0163	.0566	.0430	.0319	.0263	.0200	.0183
RS 4		2.789	0.742	.2072	.0820	.0601	.0384	.0270	.0294	.0215	.0219
RS 5		3.086	0.680	.2181	.0841	.0501	.0355	.0274	.0195	.0138	.0133
TOT		2.955	0.736	.2315	.0983	.0553	.0363	.0271	.0211	.0178	.0166
<u>60 %</u>											
RS 1		2.027	0.722	.1660	.0700	.0400	.0281	.0218	.0149	.0121	.0121
RS 2		2.060	0.540	.1663	.0692	.0398	.0266	.0201	.0179	.0130	.0114
RS 3		2.353	0.567	.1980	.0786	.0451	.0304	.0211	.0149	.0101	.0098
RS 4		2.567	0.552	.1655	.0682	.0430	.0275	.0193	.0133	.0136	.0142
RS 5		2.037	0.523	.1430	.0652	.0387	.0250	.0179	.0128	.0097	.0096
TOT		2.189	0.569	.1809	.0762	.0419	.0267	.0188	.0142	.0116	.0109
<u>40 %</u>											
RS 1		1.632	0.449	.1455	.0617	.0368	.0216	.0137	.0101	.0089	.0087
RS 2		1.558	0.413	.1249	.0575	.0300	.0194	.0133	.0124	.0092	.0082
RS 3		1.479	0.496	.1319	.0528	.0344	.0256	.0168	.0100	.0076	.0066
RS 4		1.741	0.450	.1276	.0584	.0317	.0219	.0148	.0101	.0098	.0109
RS 5		1.623	0.386	.1092	.0568	.0315	.0219	.0131	.0097	.0082	.0066
TOT		1.719	0.450	.1455	.0634	.0343	.0208	.0140	.0103	.0086	.0079
<u>20 %</u>											
RS 1		1.476	0.335	.1248	.0476	.0257	.0158	.0104	.0070	.0060	.0060
RS 2		1.097	0.275	.1068	.0439	.0197	.0113	.0086	.0072	.0065	.0046
RS 3		1.301	0.293	.0958	.0476	.0314	.0162	.0083	.0062	.0054	.0046
RS 4		1.455	0.421	.1100	.0533	.0300	.0162	.0097	.0083	.0080	.0073
RS 5		1.084	0.317	.1020	.0444	.0274	.0175	.0119	.0080	.0070	.0052
TOT		1.177	0.336	.1123	.0489	.0263	.0161	.0103	.0075	.0062	.0054
<u>MIN</u>											
RS 1		0.382	0.142	.0756	.0399	.0182	.0110	.0068	.0053	.0041	.0040
RS 2		0.776	0.263	.0661	.0232	.0133	.0092	.0066	.0036	.0026	.0018
RS 3		0.858	0.197	.0490	.0225	.0130	.0079	.0055	.0034	.0024	.0020
RS 4		0.932	0.281	.0848	.0329	.0145	.0077	.0066	.0041	.0026	.0026
RS 5		0.374	0.147	.0600	.0223	.0115	.0071	.0045	.0050	.0040	.0027
TOT		0.373	0.136	.0490	.0202	.0107	.0063	.0037	.0021	.0014	.0013

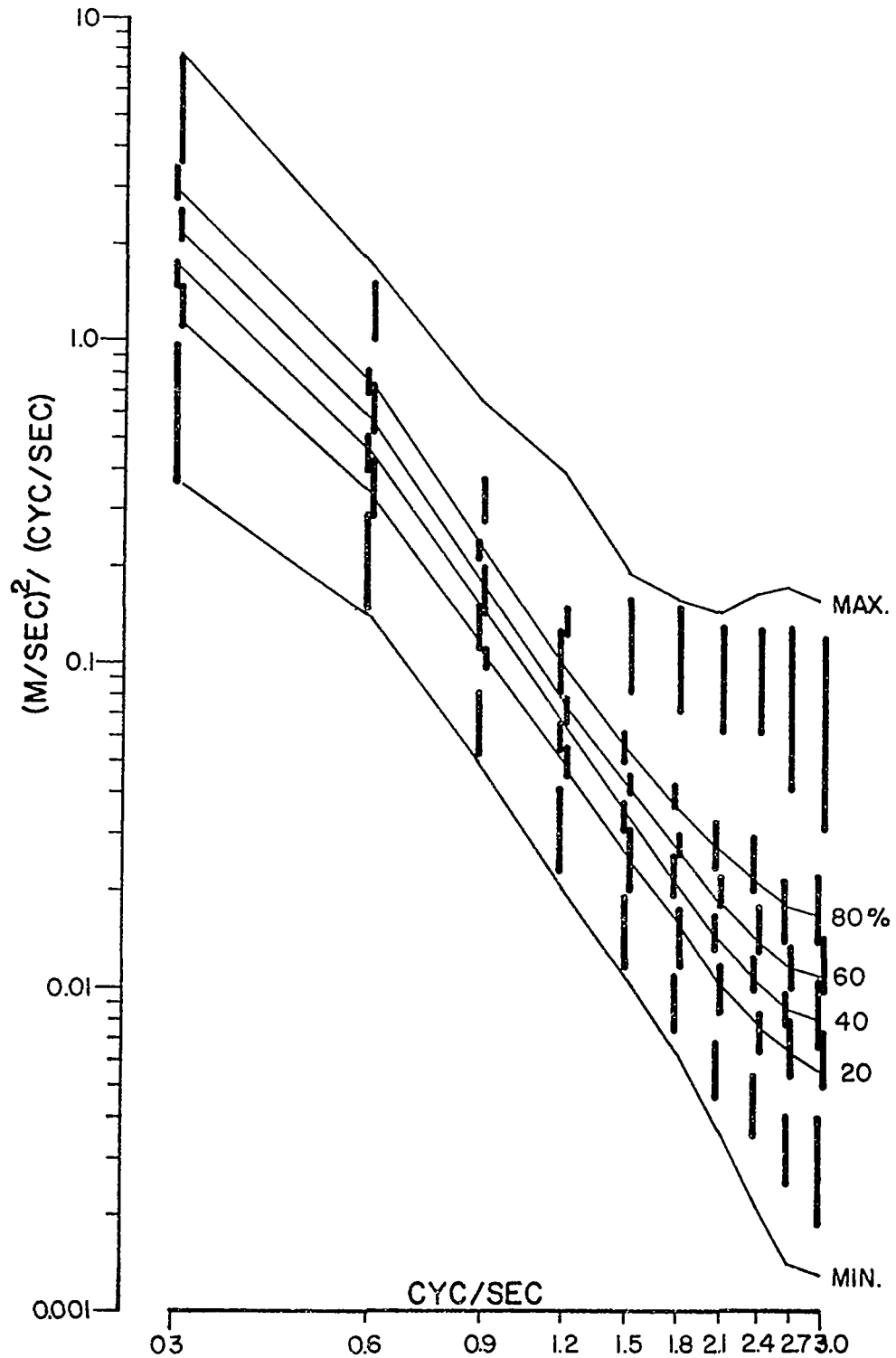


Figure 3.4 Range of Spectrum Densities at 10 Frequencies of 5 Stratified Random Samples, and Densities of Entire Sample of 900 Jimsphere Profiles.

effort to obtain a perfect sample of size $m q$. Decisions on which to use can be made realistically only after actual trials of the method.

Section 4

RELATIONS BETWEEN WIND SHEARS OVER VARIOUS ALTITUDE INTERVALS

4.1 INTRODUCTION

Various analyses of the magnitude of vector wind shears derived from balloon soundings have indicated that the mean and standard deviation of vector shear are functions of layer thickness of the form

$$\bar{w} = C \Delta Z^{n_1} \quad (1)$$

$$\sigma_w = E \Delta Z^{n_2} + D \quad (2)$$

where \bar{w} and σ_w are the mean and standard deviation (m/sec) of vector shear and ΔZ is the layer thickness (m). Adelfang, Ashburn and Court (Ref. 1) showed that Equations 1 and 2 were generally valid for the climatological means and standard deviations computed at particular altitudes for 1194 Cape Kennedy Jimsphere profiles; based on computations at 8, 12, and 16 km for ΔZ from 50 to 5,000 m they found that the constants n_1 and n_2 are equal to $2/3$, C and E are a function of altitude, and $D = 0$. Armendariz and Rider (Ref. 10) also established the validity of Equations 1 and 2 for shear layer thicknesses between 61 and 914 m; their results, which were based upon a series of measurements during August and September 1964, were obtained by detailed tracking of 100 gm. spherical smooth balloons to an altitude of 3.05 km; they found that $n_2 = 0.74 n_1$, $E = 1.1C^{0.74}$, and $D = 0$. Essenwanger (Ref. 11), who first proposed the form of Equations 1 and 2 based on an analysis of detailed wind measurements from rockets, finds that $n_1 = n_2$; Essenwanger and Reiter (Ref. 12) deduce from consideration of Tatarski's turbulence structure function (Ref. 13) that the constant n_1 (or n_2 since $n_1 = n_2$) has a lower bound of zero for an idealized wind profile composed of wind fluctuations with a "white noise" spectrum and an upper bound of unity for wind profiles composed of a linear trend without turbulence or mesostructure.

In the following discussion two sets of Jimsphere profiles are used to study the relation between mean and standard deviation of vector shear and layer thickness.

4.2 DATA

The two sets of Jimsphere profiles used for this study are composed of 1167 profiles measured over Cape Kennedy [ETR (Eastern Test Range)] during the period December 1964 through April 1967 and 83 profiles measured over Point Mugu (PMR) during the period January 1965 through March 1966. Monthly and tri-monthly distributions of the number of soundings for the two sets of data are given in Table 4.1. For an unbiased annual distribution 8.33 and 25 percent of the soundings should occur in any monthly or tri-monthly period respectively; as shown in Table 4.1 both data sets, have a relatively large percentage of the total soundings in the winter strong wind months (1-3), and a relatively small percentage in the fall months (10-12); the principal difference in the two distributions occurs in the spring months (4-6) for which the Point Mugu sample has only 8.43 percent of the soundings compared to 28.91 percent for Cape Kennedy.

Vector shears were computed for all the soundings of the two data sets at 1 km intervals from 8 to 15 km for ΔZ equal to 50, 100, 400, 800, 1,000, 3,000, and 5,000 m. The vector shear at altitude Z is defined as the magnitude of the difference between two horizontal wind vectors, one at altitude Z and the other at $Z - \Delta Z$.

4.3 DISCUSSION

The means (\bar{w}) and standard deviations (σ_w) of vector shears of various layer thicknesses were computed for shear data given at intervals of 1 km between 8 and 15 km; the total number of observations of vector shear for each layer thickness was 8,708 for the Cape Kennedy data and 627 for the Point Mugu data. The means and standard deviations were also computed as a function of altitude

TABLE 4.1

MONTHLY AND TRI-MONTHLY DISTRIBUTIONS OF CAPE KENNEDY AND POINT MUGU JIMSPHERE PROFILES

M O N T H L Y													Total
Month	1	2	3	4	5	6	7	8	9	10	11	12	
Cape Kennedy													
No. of Profiles	92	129	138	169	96	77	83	83	89	81	59	87	
% Total	7.78	10.90	11.67	14.29	8.10	6.51	7.02	7.02	7.52	6.85	4.99	7.35	1183
Point Mugu													
No. of Profiles	8	13	22	2	0	5	11	7	5	0	0	9	83
% Total	10.84	15.67	26.51	2.41	0	6.02	13.26	8.43	6.02	0	0	10.84	

T R I - M O N T H L Y

		<u>1-3</u>	<u>4-6</u>	<u>7-9</u>	<u>8-12</u>
Cape Kennedy		359	342	255	227
% Total		30.34	28.91	21.56	19.19
Point Mugu		44	7	23	9
% Total		53.01	8.44	27.71	10.84

at intervals of 1 km between 8 and 15 km. \bar{w} , σ_w and the constants C, E, n_1 , and n_2 of Equations 4.1 and 4.2, calculated by taking logarithmic least squares, are listed in Table 4.2 for Cape Kennedy and Table 4.3 for Point Mugu. In Figure 4.1 \bar{w} computed for the 8 to 15 km altitude band for various layer thicknesses is compared with the Armendariz-Rider and Essenwanger results obtained from late summer profiles (Ref.10); it is indicated that the mean vector shears computed for relatively large samples of wind profiles from all seasons at ETR and PMR are a function of layer thickness to a significantly larger power (n_1 equals 0.64 at PMR and 0.62 at ETR) than has been observed in a few late summer profiles by Armendariz and Rider at White Sands ($n_1 = 0.38$) and Essenwanger at Cape Kennedy ($n_1 = 0.44$).

For a similar comparison of standard deviations of vector shear, as illustrated in Figure 4.2, the constant power of ΔZ , n_2 , is also significantly larger for the PMR ($n_2 = 0.68$) and ETR ($n_2 = 0.62$) profiles. In addition, the existence of the constant D in Equation 4.2, which implies a deviation from a power law relation between σ_w and ΔZ , that is large for ΔZ small, is not supported by either Armendariz and Rider or the PMR and ETR Jimsphere data.

The significant variations noted above for the exponents n_1 and n_2 of the power law relations (Equations 1 and 2) which may possibly be partially related to season and method of observation is also noted when n_1 and n_2 are derived from data at 1 km altitude intervals. As illustrated in Figure 4.3, n_1 tends to be smaller at altitudes above 12 km and n_2 tends to decrease with altitude for the ETR profiles and is somewhat erratic for the PMR profiles. Similarly, as illustrated in Figure 4.4 the constants C and E generally increase with altitude again showing a relatively steady trend for the ETR sample.

4.4 CONCLUSION

For this study emphasis has been given to statistics of wind shear magnitude

TABLE 4.2

MEANS AND STANDARD DEVIATIONS OF VECTOR SHEARS FOR VARIOUS LAYER THICKNESSES AND CONSTANTS C, E, n_1 ,
AND n_2 OF EQUATIONS 4.1 AND 4.2 FOR CAPE KENNEDY JIMSPHERE PROFILES

Z(km)		50	100	400	$\Delta Z(m)$ 800	1000	3000	5000	No. of Obs.	C	E	n_1	n_2
8	Mean(m/sec)	0.59	0.99	2.62	4.05	4.64	9.79	14.12	1154	0.042		0.68	
	Std. Dev.(m/sec)	0.43	0.67	1.81	2.77	3.15	6.12	8.93			0.031		0.67
9	M.	0.60	0.99	2.75	4.24	4.93	10.16	14.95	1139	0.041		0.69	
	S.D.	0.43	0.66	1.80	2.89	3.31	6.38	9.17			0.028		0.70
10	M.	0.65	1.05	2.83	4.49	5.22	10.44	15.37	1132	0.046		0.68	
	S.D.	0.46	0.69	1.84	3.00	3.57	6.73	9.36			0.030		0.70
11	M.	0.73	1.15	3.13	4.82	5.47	10.87	15.76	1119	0.055		0.67	
	S.D.	0.61	0.87	2.27	3.42	3.81	7.26	9.73			0.050		0.63
12	M.	0.82	1.30	3.47	5.46	6.20	11.25	15.98	1101	0.069		0.64	
	S.D.	0.63	0.90	2.32	3.78	4.30	7.41	9.59			0.046		0.66
13	M.	0.99	1.56	4.07	5.88	6.51	10.71	14.81	1073	0.110		0.58	
	S.D.	0.78	1.08	2.73	3.87	4.23	6.98	8.76			0.078		0.58
14	M.	1.17	1.88	5.02	7.11	7.60	10.05	12.02	1036	0.191		0.51	
	S.D.	0.82	1.14	3.10	4.52	4.87	6.61	7.48			0.071		0.62
15	M.	1.27	2.01	5.35	7.83	8.55	10.87	10.27	957	0.239		0.48	
	S.D.	0.97	1.25	3.06	4.55	4.92	6.33	5.98			0.099		0.57
8-15 km	M.	0.84	1.34	3.60	5.41	6.07	10.51	14.25	8708	0.082		0.62	
	S.D.	0.70	0.99	2.58	3.84	4.23	6.76	8.94			0.061		0.62

TABLE 4.3

MEANS AND STANDARD DEVIATIONS OF VECTOR SHEARS FOR VARIOUS LAYER THICKNESSES AND CONSTANTS C, E, n_1 ,
AND n_2 OF EQUATIONS 4.1 AND 4.2 FOR POINT MUGU JIMSHERE PROFILES

Z(km)		$\Delta Z(m)$							No. of Obs.	C	E	n_1	n_2
		50	100	400	800	1000	3000	5000					
8	Mean(m/sec)	0.56	1.01	2.60	3.84	4.44	8.42	12.54	76	0.047		0.66	
	Std. Dev. (m/sec)	0.44	0.70	1.84	2.57	2.93	5.21	6.39					
9	M.	0.61	1.08	3.40	5.24	5.81	9.48	12.91	77	0.054		0.66	
	S.D.	0.47	0.79	.87	4.41	4.77	7.03	8.03					
10	M.	1.00	1.74	4.90	7.75	8.88	14.37	17.69	77	0.098		0.63	
	S.D.	0.68	1.24	4.08	6.76	7.91	9.56	9.78					
11	M.	0.98	1.46	3.94	5.93	7.33	18.32	21.71	80	0.061		0.70	
	S.D.	0.90	1.20	2.58	3.90	5.22	10.87	11.45					
12	M.	0.85	1.41	3.55	6.00	7.23	17.07	21.77	80	0.051		0.72	
	S.D.	0.54	0.81	2.25	3.23	3.72	10.15	10.93					
13	M.	0.97	1.71	4.28	6.18	6.87	12.52	19.40	81	0.091		0.63	
	S.D.	0.52	0.89	2.32	3.85	4.54	6.43	8.85					
14	M.	1.10	1.90	5.13	6.79	7.48	12.79	15.86	80	0.135		0.58	
	S.D.	0.68	0.92	2.59	3.67	4.13	7.65	8.31					
15	M.	1.17	1.85	5.30	6.29	6.91	12.66	13.56	76	0.160		0.54	
	S.D.	0.61	1.00	2.50	3.38	3.31	6.74	8.07					
8-15 km	M.	0.91	1.52	4.14	6.01	6.88	13.21	16.99	627	0.081		0.64	
	S.D.	0.66	1.01	2.84	2.84	4.26	4.93	8.76					

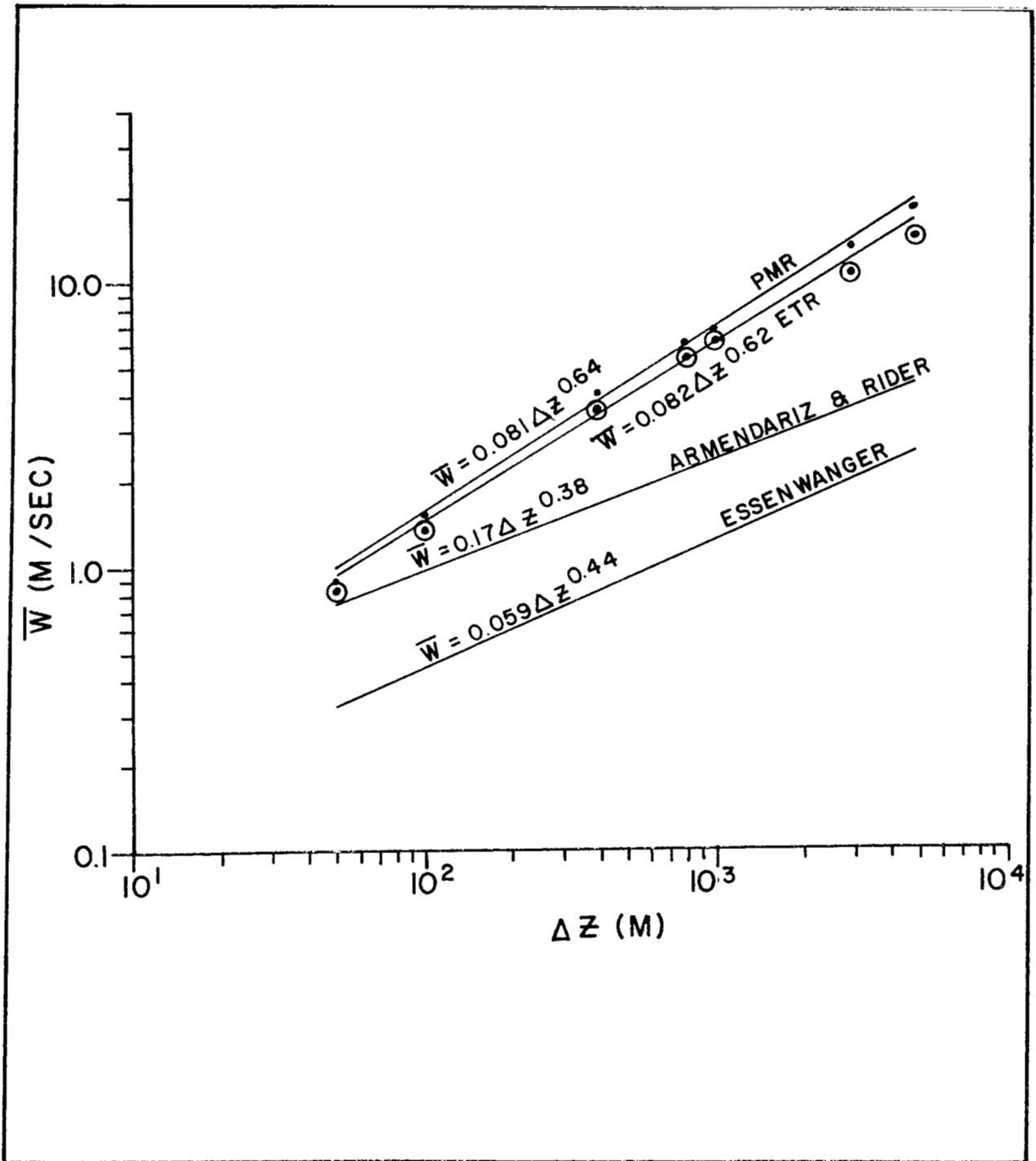


Figure 4.1 Mean Vector Shear as a Function of Layer Thickness

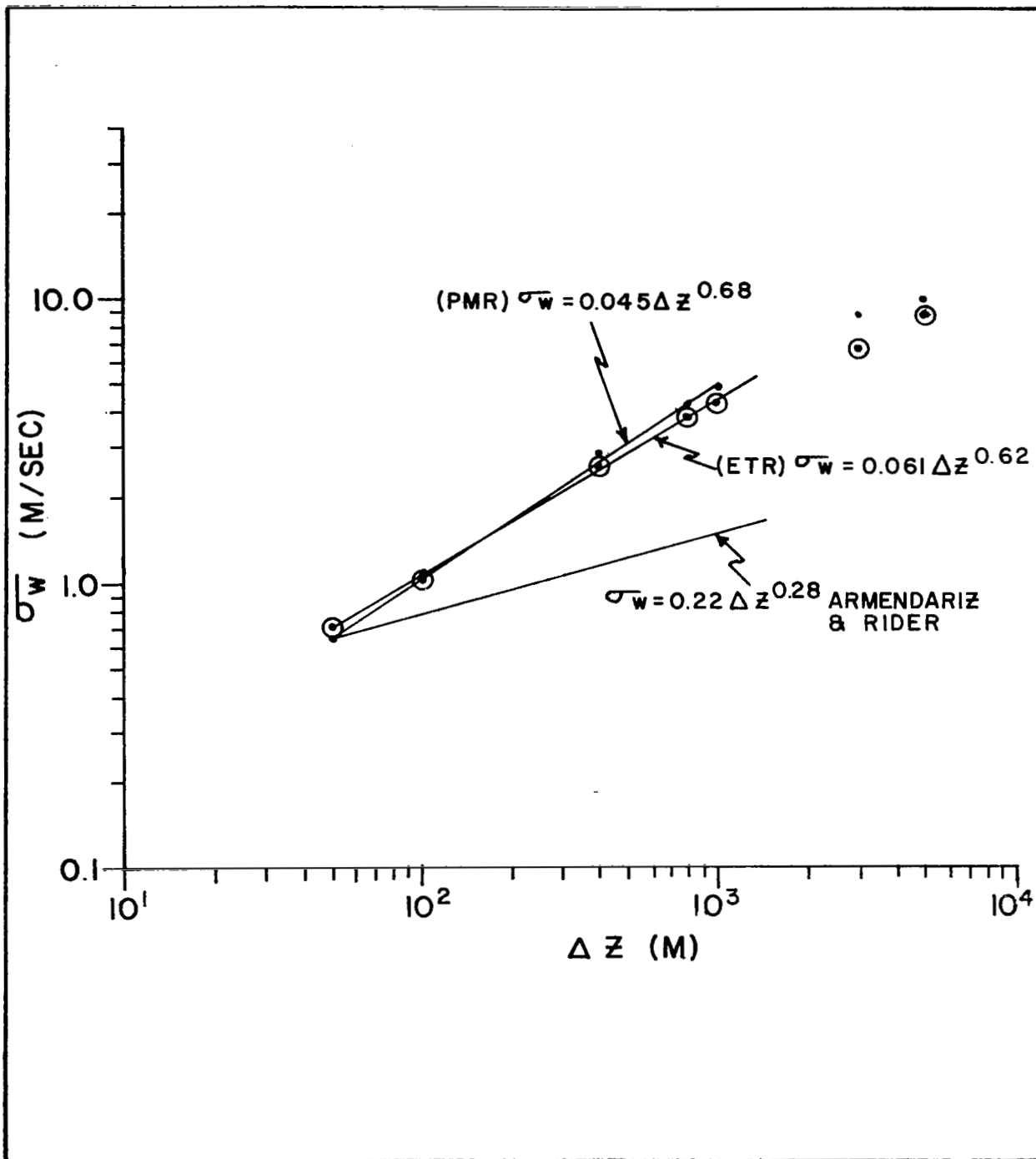


Figure 4.2 Standard Deviation of Vector Shear as a Function of Layer Thickness

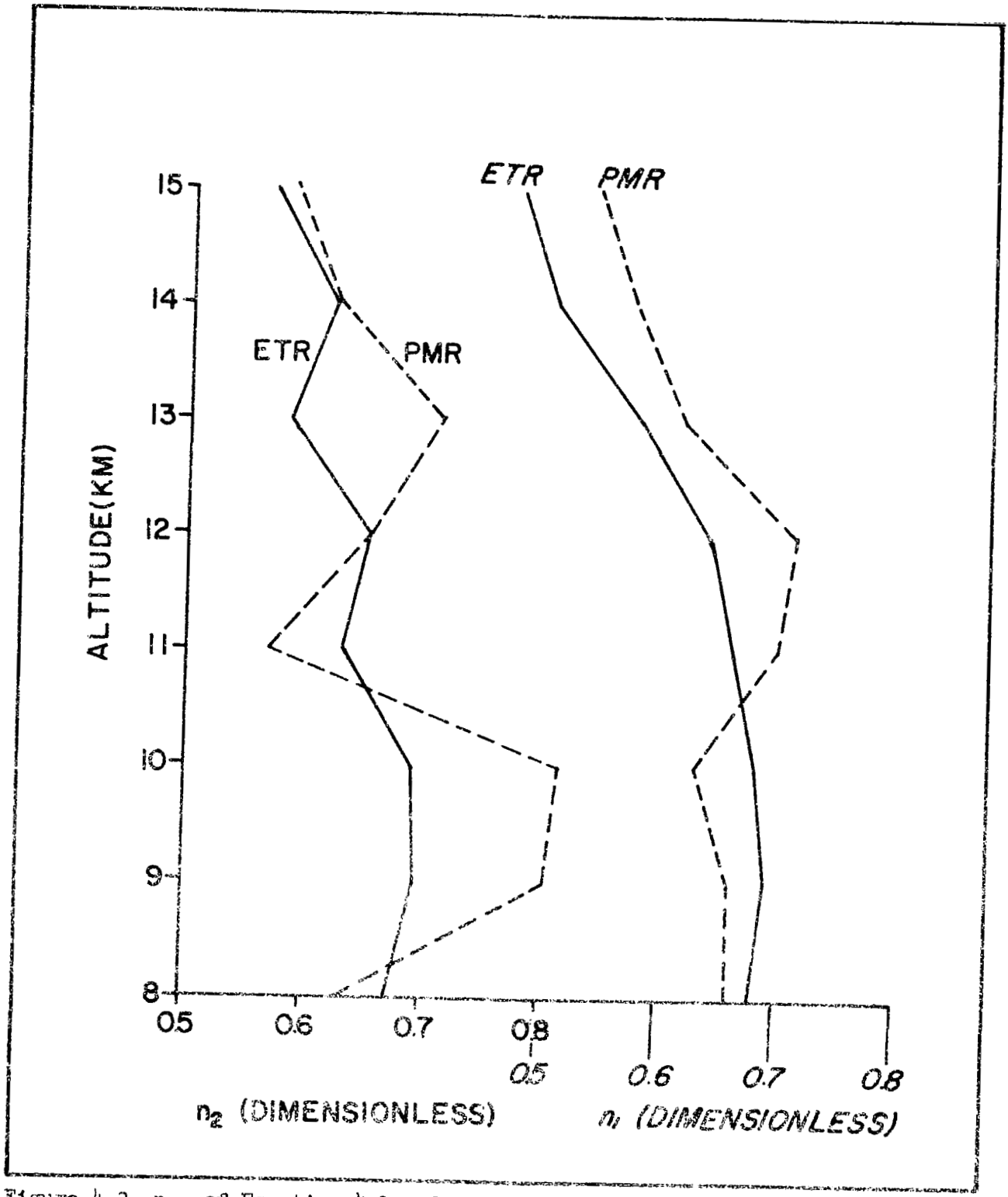


Figure 4.3 n_1 , of Equation 4.1 and n_2 of Equation 4.2 as a Function of Altitude

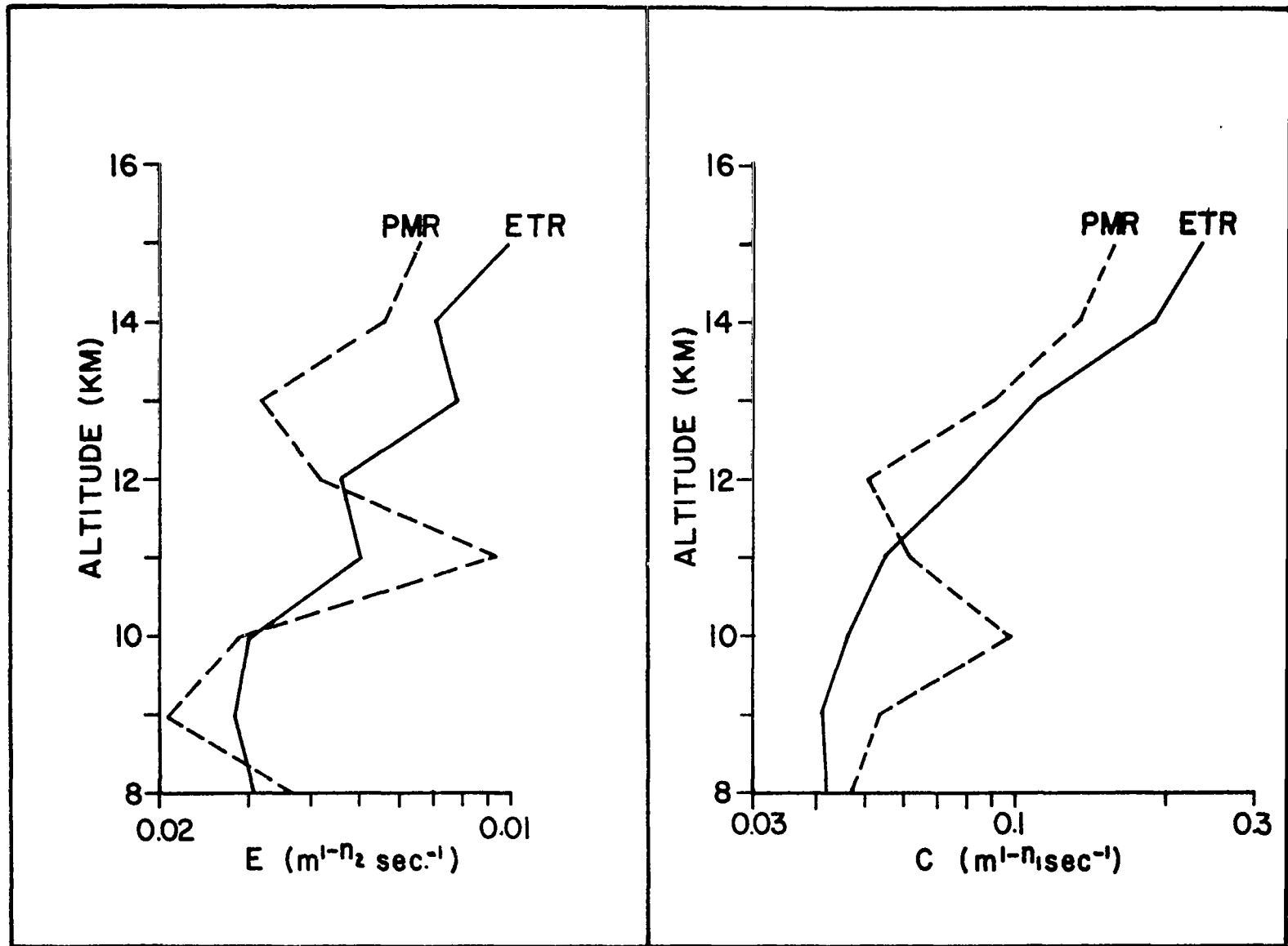


Figure 4.4 C of Equation 4.1 and E of Equation 4.2 as a Function of Altitude

computed from a relatively large sample of data obtained in all seasons. Therefore comparisons with other results derived from a few late summer soundings, which show poor agreement, further support the hypothesis that the constants of the proposed power law relations are a function of season; additional factors which may contribute to the poor agreement are systematic errors associated with the methods of observation (rockets, smooth balloons and Jimsphere) and differences in the altitude range of the observations which was 8 to 15 km for Jimsphere data and surface to 3.05 km for the White Sands data (Armendariz and Rider).

The ETR and PMR vector shear magnitudes, derived from sets of soundings which differ more in size than in their distribution by season, show a distinct similarity in the variation of means and standard deviations as a function of layer thickness.

Section 5

MATHEMATICAL REPRESENTATION OF GUST FUNCTIONS

5.1 INTRODUCTION

In this section the aim is to develop a method of representing gust functions that are observed in detailed Jimsphere wind profiles. This will be achieved by utilizing a technique developed and used by Dutton (Ref. 2). The theory of the technique is discussed and a method of application is suggested.

5.2 THEORY

Dutton used data obtained at low altitudes in a turbulent wind field. Four sets of data were obtained at each of six levels at Cape Kennedy below 150 meters. At each level wind direction and speed were measured at intervals of 1/10 sec over a long period of time. From this a vector wind velocity $\vec{v}(t)$ was defined and an average vector \bar{v} was calculated according to

$$\bar{v} = \frac{1}{T} \int_0^T \vec{v}(t) dt \quad (5.1)$$

where T, the duration of some part of the experiment, is selected to include the portion of the wind record which has the largest gusts. Then the unit vector \vec{i} is taken along this wind direction and \vec{j} orthogonal to it. The longitudinal (u) and lateral (v) components of the turbulent wind are defined by:

$$\begin{aligned} u &= (\vec{u}(t) - \bar{u}) \cdot \vec{i} \\ v &= (\vec{v}(t) - \bar{v}) \cdot \vec{j} \end{aligned} \quad (5.2)$$

Thus, at each level, not only the wind direction and speed, but also the

u and v components are given as a function of time. For a particular run, at each level, ten largest gusts, for each component are chosen for every gust at each level. Assuming the validity of Taylor's hypothesis, a 3,000 ft. sample of data is extracted from the whole record in such a way that the gust falls in the center i.e. 1500 foot of data on each side of the gust. The aim is to find the general shape of these functions at all six levels. To this end a correlation matrix, $R(X_i, X_j)$, $[i, j = 1, \dots, N]$ is defined as follows: u and v are chosen at random points $X_1 \dots, X_n$ on the 3,000 foot sample (in Dutton's case N is taken to be 50) for each of the 10 gust regions at each of the six levels. Let u_i and v_i be the u and v components of i^{th} gust. A correlation matrix is defined for the u component according to

$$R(X_i, X_j) = \frac{1}{10} \sum_{n=1}^{10} u_n(X_i) u_n(X_j) \quad (5.3)$$

This correlation matrix is used for application to the theory which will be developed next. A similar correlation matrix is calculated for the v component. The aim is to represent these gust functions by some set of known functions.

The mathematical problem to be solved is to find an economical method of representing these gusts. There is no reason to believe that any of the classical orthonormal series will be very efficient. The object is to find a set of orthonormal functions, which in some sense, to be decided later, are more like the functions we are trying to represent. For this purpose a theorem in proper orthogonal decomposition given by Loeve (Ref. 14) is used. Given a set of functions $\{f\}$ defined on some finite domain, we would like to find a function ϕ which in some sense is more like most of the functions in the set. So, we first have to agree on a definition of "likeness". We may be tempted to say ϕ is more like f if the correlation between ϕ and f is as large as possible i.e. try to maximize $r = \int f(x) \phi(x) dx$. But, since sign and magnitude are immaterial, and we only need relative magnitude, we may use the normalized quantity

$$p^2 = \frac{\left[\int f(x) \phi(x) dx \right]^2}{\left[\int f^2(x) dx \right] \left[\int \phi^2(x) dx \right]} \quad (5.4)$$

It can be shown that $p^2 \leq 1$. Another measure of likeness may be minimizing of

$$D = \int [f - \phi]^2 dx \quad (5.5)$$

But ϕ could be more like f than it is more "unlike" $-f$; therefore we would like to redefine (5.5) so that ϕ is acceptable if it either is like f or $-f$. Thus we find it more convenient to use

$$D = \int (f - \phi)^2 dx + \int (f + \phi)^2 dx \quad (5.6)$$

In (5.6) we can use the normalized form of f and ϕ , denoted by f_n and ϕ_n and rewrite (5.6) as

$$D_n = \int (f_n - \phi_n)^2 dx + \int (f_n + \phi_n)^2 dx \quad (5.7)$$

A simple calculation shows that

$$D_n = 4(1 - p^2) \quad (5.8)$$

Thus a maximum of $E(p^2)$ gives a minimum of $E(D_n)$. Thus solving the problem, which involves finding a ϕ to satisfy (5.4) is the same as finding a ϕ to satisfy (5.7), and vice versa. Further any ϕ which resembles f or $-f$ will be acceptable. And finally, if we are able to produce such a ϕ , it would be more "like" all the functions of the set simultaneously. Moreover, resemblance is in both senses of (5.4) and (5.7). It only remains to be seen whether there is such a ϕ . A standard method of calculus of variations is used, i.e. it is assumed that there is a maximizing function ϕ which induces a small variation $\epsilon \delta \phi$ in ϕ ; $\phi + \epsilon \delta \phi$ is substituted into Equation (5.4) which is differentiated with respect to ϵ at $\epsilon = 0$. It follows that

the equation

$$\int E [f (x) f (y)] \phi (x) dx = \frac{2}{p} \phi (y) \quad (5.9)$$

must be solved. This is a typical eigen value problem. Therefore, there is not only one, but a whole set of solutions to this integral equation. If we set $\lambda_1, \lambda_2, \dots$ as possible eigen values with $\lambda_1 \geq \lambda_2 \geq \dots$ we get corresponding eigen functions ϕ_1, ϕ_2, \dots upon setting

$$R (x,y) = E [f (x) f (y)] \quad (5.10)$$

from (5.9) we get

$$\int R (x,y) \phi_n (x) dx = \lambda_n \phi_n (y) \quad (5.11)$$

An easy calculation shows that the functions $\{ \phi_n \}$ form an orthogonal set under the inner product $\langle f, g \rangle = \int f (x) g (x) dx$. Upon normalization they form an orthonormal set. Since $R (x,y)$ is defined on a finite domain, a possible choice for the eigen values is a countable set. In case an eigen value has multiplicity more than one, the associated eigen functions can be orthogonalized by the Gram-Schmidt method. Hence, the assumption that $[\phi_n]$ form an orthonormal set is correct. Therefore, any function f of the set has a unique representation

$$f (x) = \sum_{n=1}^{\infty} a_n \phi_n (x) \quad (5.12)$$

where

$$a_n = \int f (x) \phi_n (x) dx \quad (5.13)$$

a straight forward calculation shows that

$$E (a_n a_m) = \lambda_n \delta_{m,n} \quad (5.14)$$

(where $\delta_{m,n} = 0$ if $m \neq n$ and $= 1$ if $m = n$). Thus the coefficients are uncorrelated across the set. The advantage of this analysis is that the tail end of the series is cut off in the formula (5.12) i.e. if we consider the first n terms in the power series expansion of f , we get close enough approximation of it. Of course the larger we choose n , the closer we get to the actual value of the function. But to get a fairly good estimation of the function, n does not have to be very large. For example, in the case of the data discussed in the earlier paragraph, if we take only the first eight eigen functions, they already explain at least 97 percent of the variance in each component. We can, in fact, calculate the error in the estimation of the function by the first n eigen functions; let $e_n(f)$ be the error. It can be shown that

$$e_n(f) = \int [f]^2 dx - \sum_{n=1}^n [a_n]^2 \quad (5.15)$$

Some further argument would lead to $\lim_{n \rightarrow \infty} e_n(f) = 0$ i.e. (5.16)

the error can be made arbitrarily small.

This theory is used to analyze the data mentioned in the earlier paragraph. The correlation matrix (5.3) computed there is used in a summation form of Equation (5.11). A standard eigen value process is applied to the matrix and its eigen values and eigen functions are found. As mentioned earlier, by just using the first eight eigen functions, 97 percent of the variance in each component is explained.

5.3 APPLICATION

To apply the method outlined above it is suggested that a number of Jimsphere profiles closely separated in time be used. The time separation is analagous to the altitude separation of Dutton's data. Random points, x_i , are chosen to be at some fixed altitudes of the profiles. The number of x_i 's used is a function of the degree of accuracy required. For N profiles for the period

of interest the u and v components of the nth profile at the altitude x_i are denoted by $u_n(x_i)$ and $v_n(x_i)$. A correlation matrix is formed for the u component, $R(x_i, x_j) = \frac{1}{N} \sum_{i=1}^N u_n(x_i) u_n(x_j)$, and similarly for the v component. The derivation of the functions which describe the u and v components of each profile from each correlation matrix was described in the previous section.

A variation of the approach suggested above could be attempted by using several groups of closely spaced Jimsphere profiles. Within each group the average value of u and v would be calculated and substituted for u_n and v_n in the above analysis. Another alternative would be to take the vector $\vec{i} u + \vec{j} v$ at each point (altitude) x_i and find its vector sum within each group which again would be substituted for u_n and v_n to find the correlation matrix and carry out the calculation. If the largest gusts are of interest a few of the largest gusts could be chosen in each group and the method could be applied to them. In this case, however, more care is needed. If we only look at the u and v components and choose the largest gusts, depending on the angle of the wind vector with respect to the u and v axis we could get different values for u and v. In other words two different wind vectors with the same magnitude could give completely different u and v components because the angles they make with the axis are not the same. Since we only seek the largest gusts, this may lead us to ignore some gusts which have appreciable magnitudes, but not very large u and v components, because of being situated at a "bad angle". This can be remedied if we first take the magnitude of the wind vectors and choose those with biggest magnitudes, and then go ahead and apply the above method to the u and v component of these chosen vectors.

5.4 CONCLUSION

In applying Dutton's method for representing Jimsphere gust functions one should be careful in interpreting the results and have an understanding of

the extent and limitation of their use. Most important is that this analysis does not reveal significant information about the vertical variation of wind vectors. In addition, in interpreting the results of this analysis as it relates to space vehicles it should be understood that the Jimsphere views the atmosphere in about an hour and a half as it rises from the ground to 18 km compared to the spacecraft which covers the same vertical distance in 94 seconds. What the spacecraft sees requires a further interpretation of the results.

Section 6

CONCLUDING REMARKS AND RECOMMENDATIONS

6.1 GUST STUDIES

Following the approach suggested in an earlier study of Jimsphere profiles (Ref. 1) a set of gust profiles have been derived in the time domain of a Saturn vehicle. An analysis of these gust profiles (Section 2) has revealed that their spectrum densities are generally smaller than spectrum densities of altitude profiles conventionally transformed to the time domain (Equation 2.7). It is suggested that the conventional transformation is invalid for time dependent vehicle velocities and that the spectrum densities of the time domain profiles derived in this study are the most accurate estimate of the spectrum of horizontal wind speeds seen by a Saturn vehicle. It is recommended that other aspects of these newly derived gust profiles be studied. Of particular interest is the variability of gust statistics; for example, the distribution functions and the distribution of spectrum densities of gusts computed for a number of vehicle flight time intervals should be stratified according to season and location (PMR, ETR, Wallops Island, White Sands) to partially explain their variability.

6.2 ANALYSIS OF WIND SHEARS

The mean and standard deviation of vector shear magnitudes at altitudes between 8 and 15 km can be described by similar power law functions of layer thickness (Equations 4.1, 4.2) for Cape Kennedy and Point Mugu Jimsphere profiles. The significant difference between these functions and others derived from a few summer profiles obtained with different measurement techniques is partially attributed to a seasonal variation of the constants in the power law functions. It is recommended that future studies of the magnitude of vector shear establish the constants in the

power law functions for wind profiles grouped according to month or season; also recommended is a test of the hypothesis that the constants are correlated with the vector shear direction.

As suggested by Court (Ref. 1) the observed relations between means and extremes of shears to layer thickness is attributable to the decay of inter-level correlation of zonal and meridional wind speeds for increasing layer thickness; to test this hypothesis, it is suggested that Jimsphere profiles be used for a study of the decay of inter-level correlation beginning at 75 m layer thickness.

6.3 PROFILE SAMPLING

In Section 3, two validation tests of a method for selecting representative profile samples indicated that a) on the average the extremes were slightly over-estimated for the selection characteristics, and slightly under estimated for the test characteristics, and b) the spectra of any one of the five profile sub-sets selected from a random sequence of the parent population offer a fair approximation of that of the whole sample. It is recommended that further tests of the method be performed to establish how well profile samples obtained by using selection characteristics in fewer categories such as quartiles or quintiles, instead of deciles, represent the parent population.

Section 7

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Section 8

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APPENDIX I

MAXIMUM WIND SPEED AND MAGNITUDES OF VARIOUS VECTOR SHEARS, WITH CORRESPONDING ALTITUDES (TOP OF SHEAR LAYER), BETWEEN 4 AND 14 KM IN 900 JIMSPHERE WIND PROFILES OVER CAPE KENNEDY.

PROF NO	MAXIMUM WIND SPEED METER	+1000M SHEAR M/SEC	+1000M SHEAR M/SEC	+1000M SHEAR M/SEC	+1000M SHEAR M/SEC	+1000M SHEAR M/SEC	+1000M SHEAR M/SEC	+1000M SHEAR M/SEC	+1000M SHEAR M/SEC	+1000M SHEAR M/SEC	+1000M SHEAR M/SEC	+1000M SHEAR M/SEC	+1000M SHEAR M/SEC	+1000M SHEAR M/SEC				
1867	36.987	13353	3.129	12908	4.795	13583	14.113	13150	6.543	11908	11.866	13150	9.872	13625	15.725	4680	9.307	5375
1868	37.462	13380	3.886	12953	4.792	13425	14.297	13180	6.193	11980	10.549	13125	8.162	13680	15.862	4650	12.180	5225
1869	36.331	13367	4.225	13125	4.378	13375	11.977	6950	7.769	13975	7.389	13625	8.669	14000	17.967	4950	8.726	4950
1870	47.468	13582	5.331	13450	3.494	13750	17.114	13500	5.915	10875	10.765	12900	4.134	18925	22.681	5425	2.163	12950
1871	58.372	13775	4.914	13775	2.891	7825	14.169	13950	8.342	7925	9.856	13775	6.532	7875	21.843	9575	2.388	12350
1872	46.631	12975	4.898	13375	3.852	13500	12.829	8700	18.410	13900	8.427	13900	9.264	13675	21.711	7500	9.368	13500
1873	76.217	13325	5.181	13375	5.826	13275	17.154	14904	10.642	14000	9.684	18325	17.108	13775	26.689	7850	23.880	13950
1879	45.795	13750	3.282	13575	3.863	13575	9.482	7200	7.755	6300	10.887	13675	6.681	13280	19.636	9350	2.089	13575
1880	48.227	12975	3.267	12950	4.748	12925	11.451	12750	12.086	13375	8.558	13850	8.523	13125	19.256	9780	2.088	13950
1881	52.392	12325	4.988	12450	3.641	12900	18.373	7150	7.964	13975	7.594	6925	8.355	12700	21.611	6975	11.673	14080
1882	47.873	13900	4.872	12975	4.844	12775	12.134	13925	7.863	13425	11.928	13980	18.742	12630	16.288	4175	7.888	14800
1883	53.191	13175	4.316	13375	6.365	12950	11.629	7325	14.471	12950	10.461	12950	18.108	12950	28.915	7375	15.486	12950
1884	54.392	13750	5.619	11575	4.435	12275	13.612	5250	18.714	12525	7.481	5250	16.676	12575	22.852	6825	11.441	14800
1885	47.927	18725	4.923	9125	3.787	12853	23.934	18625	10.166	12925	13.272	9375	11.825	13350	31.671	18725	32.340	13550
1888	49.815	11975	4.872	12950	4.241	13875	15.788	8850	9.229	13525	11.228	13850	18.470	13750	22.344	7775	14.240	14800
1889	26.821	13325	4.624	18050	4.188	18175	15.896	11825	11.838	9075	7.321	11775	18.855	9850	16.591	12850	6.898	7525
1890	27.389	11300	3.456	13175	3.413	12275	12.199	13675	15.271	12450	9.835	13625	18.628	12490	14.454	11350	11.474	4380
1891	24.198	14000	3.737	4375	3.885	4188	12.319	4725	15.908	9275	9.484	4125	8.388	8975	18.133	8725	17.081	16475
1892	31.215	13550	4.584	13550	3.566	13575	12.843	9225	6.483	12950	10.244	13408	11.982	13325	13.828	1780	14.214	9250
1893	44.224	13400	4.886	6500	3.556	13575	6.843	9225	6.483	12950	7.438	9225	5.814	13525	16.692	5925	7.254	13550
1896	32.544	18800	2.538	4725	2.743	12108	8.699	6975	5.785	12950	5.628	6900	4.988	13525	16.238	9875	5.312	12225
1897	32.353	18800	2.693	13775	2.833	12725	12.989	6050	10.999	9900	6.538	6775	5.237	13450	19.502	8900	11.638	13375
1898	38.483	18925	3.880	12350	3.862	13575	9.315	13275	9.447	14800	10.282	12900	9.218	13680	16.323	6425	17.387	13800
1899	33.388	12925	3.522	4200	3.145	14800	15.713	4650	18.886	13375	18.248	4150	5.719	12825	24.457	6300	8.402	4380
1901	36.183	12375	4.415	11450	4.821	12280	14.167	5880	14.329	13775	7.354	5880	9.174	13780	24.843	6175	14.854	8575
1902	31.337	13580	4.568	11425	3.388	13375	18.156	11800	14.451	12850	11.189	11250	14.551	18850	18.552	13180	18.854	18973
1903	45.845	13400	5.881	12980	3.144	12108	12.888	12725	6.486	18975	5.183	12300	8.127	5250	22.824	13750	8.718	4375
1904	25.385	13125	1.763	12200	2.348	6823	11.829	12700	7.225	6925	7.899	12975	6.145	6325	16.544	12775	9.976	4625
1906	45.518	13375	4.518	13975	3.388	11775	9.877	11525	6.594	14800	9.196	13975	6.423	12850	20.680	4600	2.888	4350
1907	45.784	12575	3.868	18200	3.731	11480	26.312	12250	13.822	13925	12.358	11725	12.388	11725	23.910	12950	2.988	11425
1909	41.362	13280	5.188	12525	3.766	14800	16.882	12975	8.376	11925	11.134	12375	8.957	11900	21.184	12950	14.284	4380
1912	52.678	12550	4.143	11125	4.817	11180	13.881	12800	11.438	13490	9.121	12800	9.172	11275	23.738	9550	21.844	9575
1913	49.989	13475	4.881	12480	4.943	13125	19.511	12950	11.388	9350	18.931	12525	19.922	11825	29.881	12525	13.984	9375
1914	45.845	13400	5.881	12980	6.716	11652	22.979	12525	6.946	8200	10.185	12548	18.637	11950	34.893	13475	5.487	14280
1915	47.733	13530	4.819	12775	3.723	14800	17.399	12750	11.253	5575	9.487	12825	6.858	13280	28.272	12825	11.973	7530
1920	26.548	13423	3.569	14400	3.951	12980	9.778	11125	9.188	13900	6.913	12925	8.888	13825	21.884	12800	7.788	5580
1921	10.549	11493	3.791	12980	3.472	11625	8.896	4825	12.714	4575	7.621	13850	11.898	4080	10.212	8625	15.351	6575
1922	35.781	11173	4.866	12700	4.427	12280	11.414	7950	19.744	12225	8.886	13888	12.382	12200	19.139	8575	23.981	14880
1923	43.731	11950	4.518	13750	4.355	13725	15.141	12180	17.135	14480	11.318	14888	18.842	12850	23.863	11950	24.288	13725
1924	35.674	13825	3.489	9325	4.458	13175	19.782	13850	18.397	13275	18.489	13850	9.886	13938	19.123	18675	25.118	14880
1925	24.321	18980	4.981	12175	3.964	12725	12.942	12575	12.492	12575	10.644	13725	11.838	13880	19.145	12950	22.518	12593
1926	11.956	12825	4.797	12380	4.745	11880	9.675	13175	9.139	13625	13.583	12825	6.679	12825	11.775	12825	5.187	8925
1927	21.484	18900	4.289	12980	3.825	12880	13.741	12925	21.288	12725	11.056	12675	10.568	12280	20.838	12280	23.866	13780
1928	28.336	18725	4.197	13880	3.661	13825	17.442	13925	25.805	13750	13.373	13375	19.778	13225	14.367	18525	31.318	13775
1929	22.858	11560	5.198	13575	7.251	13825	28.511	13625	21.192	13725	13.458	13588	13.199	13425	14.985	18875	24.288	13725
1930	23.463	11560	5.347	13580	4.873	13380	28.512	13775	15.884	13900	16.843	13588	14.125	13588	16.809	11275	25.112	13875
1931	22.582	14880	5.479	9325	3.839	13980	13.358	13775	7.455	13900	10.689	13825	19.976	13725	19.365	14880	17.556	13980
1932	28.213	13980	5.813	13750	3.839	13980	13.358	13775	7.455	13900	13.151	13880	6.714	13880	12.946	13880	8.747	11480
1933	11.841	13775	2.938	12523	5.844	13973	7.689	7980	7.733	14880	7.198	12625	6.552	11975	10.821	9925	8.777	6575
1934	17.645	14880	5.155	13923	2.126	11575	12.488	14880	8.984	11988	8.281	14880	6.472	11825	11.384	18375	9.424	4378
1935	11.451	11173	5.321	13988	2.981	13758	8.863	7588	6.271	11825	6.832	6958	5.819	4775	6.375	9558	8.288	13675
1936	16.599	14880	4.738	13988	2.727	13558	18.144	14880	18.372	4225	7.634	12888	4.281	4888	16.158	14880	18.537	4125
1937	18.972	13788	3.390	12988	4.192	13258	10.883	13788	5.462	12458	11.578	13875	8.612	13558	27.321	13725	8.896	12850
1938	13.957	12725	4.776	11480	4.842	13875	9.787	12275	9.238	12988	8.524	11675	6.115	13125	13.837	12725	11.743	13880
1939	23.828	11480	5.784	12480	4.683	11525	14.353	12888	19.888	12425	13.294	12925	12.471	11888	17.182	11588	12.218	14880
1940	23.863	12950	5.779	12980	6.895	12950	11.858	13825	8.436	13575	9.549	12475	6.667	13625	15.468	4775	4.488	13880
1941	15.697	18950	4.884	12880	4.243	12458	8.782	12880	9.872	13475	10.726	13925	9.248	12950	12.265	5575	12.951	4893
1942	22.288	13450	4.186	12925	5.368	12925	5.987	13850	10.072	13180	15.543	13880	14.875	12980	14.739	13125	14.832	13880
1944	23.387	13450	5.987	12925	4.483	13425	9.975	13850	10.274	13975	11.611	13375	10.984	13980	14.445	13980	12.655	12950
1945	26.890	13450	4.886	12958	4.125	13725	14.526	13980	16.448	14880	13.262	13825	14.765	13950	11.123	13925	12.798	14880
1946	25.277	13173	3.483	13125	5.415	14802	12.144	13550	10.193	14880	9.578	13175	13.					

APPENDIX I (Cont.)

Table with 14 columns: PROF NO, MAXIMUM WIND M/SEC, +100MM SHEAR METER, -100MM SHEAR METER, +1000M SHEAR METER, -1000M SHEAR METER, +40CM SHEAR METER, -40CM SHEAR METER, +1000M SHEAR METER, -1000M SHEAR METER, +40CM SHEAR METER, -40CM SHEAR METER, +1000M SHEAR METER, -1000M SHEAR METER. Rows contain numerical data for various profiles.

APPENDIX I (Cont.)

PROF NO	MAXIMUM METER	WIND METER	1-100M M/SEC	SHEAR METER	1-100M M/SEC	SHEAR METER	1-100M M/SEC	SHEAR METER	1-100M M/SEC	SHEAR METER	1-100M M/SEC	SHEAR METER	1-100M M/SEC	SHEAR METER	1-100M M/SEC	SHEAR METER	1-100M M/SEC	SHEAR METER
674	29,387	11725	2,395	12925	3,073	13875	7,919	5058	10,444	13920	4,395	9775	6,931	13950	14,297	11700	8,142	14200
675	27,937	13425	4,442	13425	5,642	13225	12,326	12375	13,715	13075	8,743	13475	10,255	13625	16,992	13450	10,438	13575
676	29,964	12425	3,942	13000	5,153	12775	14,238	10150	14,829	10375	8,772	12150	11,712	12950	22,363	13100	12,556	13100
677	29,412	13300	3,595	13900	3,688	13450	8,763	12325	6,977	13975	6,702	9825	7,485	13700	15,376	13300	12,562	13300
679	29,390	13950	4,737	13450	3,135	13700	13,909	12450	7,649	8675	8,168	13375	6,659	13825	15,672	13675	12,219	10375
680	21,567	13475	4,089	13425	2,413	7952	12,950	13850	11,399	13450	5,600	12750	5,560	12750	12,464	11950	13,729	11500
681	24,111	13575	2,883	13450	3,384	14000	8,437	14042	7,010	9450	8,831	13950	5,273	5275	10,898	7375	11,772	4900
682	20,930	11975	5,097	6375	4,157	5775	12,470	10275	12,902	6775	7,606	9700	10,634	6150	20,445	8600	12,330	13500
683	30,417	12950	3,201	12950	6,112	13500	10,592	12675	19,457	13625	9,855	12225	14,699	13700	25,301	12950	9,906	6350
684	24,357	13300	2,911	6875	2,470	14220	9,237	9725	6,689	10250	6,916	6300	5,671	10700	17,272	13725	10,282	12575
685	23,574	9675	3,174	13775	3,193	13225	13,076	13875	14,201	14000	8,095	13700	6,200	12625	9,421	12750	19,536	9900
686	26,370	11500	3,989	13350	3,927	12725	10,216	9050	12,445	12900	6,200	12625	6,809	13525	11,992	13475	6,704	6700
687	19,778	13475	3,999	12750	3,432	13325	4,789	7850	7,777	13125	4,470	7275	6,799	12550	8,410	9075	12,793	13500
688	22,240	12200	2,989	13725	4,781	12725	9,895	12925	13,706	13100	6,272	12375	11,977	12850	12,370	6425	12,450	10900
689	29,567	12475	3,503	12775	4,569	13475	12,891	13750	20,878	12360	9,756	13475	13,507	12000	21,035	10200	35,627	13775
690	30,407	12775	3,709	13450	3,879	13475	7,687	13350	8,222	14000	7,204	12775	7,594	13600	11,256	7625	5,194	11000
691	24,574	13325	3,169	11575	4,482	13250	9,565	12675	6,965	13750	8,413	13450	9,471	12600	13,562	7050	7,428	13500
692	25,382	11350	3,683	13675	3,904	13325	9,944	5750	8,469	12775	11,053	13650	9,344	13575	17,047	6850	7,893	9325
693	23,776	13375	5,792	13360	5,807	5100	12,776	13000	13,322	4700	11,053	14200	7,573	5300	17,569	13975	9,117	13750
694	26,579	13375	5,424	13250	4,395	13225	24,932	13700	23,823	14000	15,753	13925	19,966	13500	24,640	13000	12,142	14000
695	30,249	13375	4,123	13250	5,474	13850	12,664	13275	15,731	14000	10,474	13275	15,147	13550	22,066	13275	6,651	14000
696	37,874	13475	4,202	13425	5,921	13975	19,626	13540	13,200	14000	9,500	13475	15,668	13975	24,749	13450	8,134	8550
697	50,997	12775	4,264	11425	4,264	13975	18,001	11125	10,250	14000	7,773	11025	10,284	14000	34,513	11150	13,790	14000
703	47,225	12775	4,358	13500	6,657	13750	21,330	12350	10,354	10725	10,348	11950	12,060	13900	45,292	12900	13,010	4000
704	54,245	13550	2,711	12375	2,606	7475	10,658	12675	6,752	7450	5,941	12675	4,208	14000	19,762	13525	13,493	4350
705	37,867	13525	3,454	13350	4,426	14000	13,414	13700	5,793	11275	6,084	11800	4,987	9225	24,458	10300	14,732	4500
706	30,890	13375	5,511	13275	4,297	13925	22,251	10825	20,480	13975	14,401	10775	13,359	13975	40,003	11300	10,970	13775
707	52,246	13575	4,847	9225	3,309	13825	18,545	9725	15,399	14000	9,265	9500	9,257	14000	39,004	11700	14,812	5925
708	40,923	12775	4,237	10700	3,566	13975	18,000	10750	16,708	14200	11,377	10750	10,001	13975	35,785	10225	21,731	13975
709	38,907	13950	4,443	9100	4,038	4175	16,595	9900	9,252	4820	10,839	9375	7,737	4300	32,139	10275	14,222	7400
710	28,715	6525	2,585	6425	3,309	9825	7,496	13520	7,249	11000	5,597	13725	6,599	13675	8,527	4175	15,081	10975
711	16,702	4000	3,153	12975	3,465	11275	8,740	12450	10,130	10725	6,104	11825	6,104	11825	10,097	13975	16,111	10975
712	20,207	13250	2,692	11200	2,733	13900	12,936	11175	7,884	4300	7,035	11725	6,101	14000	25,633	13250	8,489	7375
713	31,615	13125	2,626	4475	5,414	13750	12,790	13100	10,057	4040	5,872	13100	19,140	14000	22,091	13125	6,942	13900
714	29,901	12525	3,164	9400	2,355	9800	11,559	9725	6,333	4225	6,646	9375	4,668	7625	16,926	10200	7,764	6050
715	17,762	13525	4,593	13525	3,962	14200	10,045	13825	6,970	6325	12,816	13825	7,619	13525	11,638	11250	8,721	8350
716	17,956	10400	2,163	4275	4,781	13750	9,685	13650	9,164	4000	5,675	13625	8,622	14200	17,786	10400	13,590	14000
717	15,167	11500	3,870	13450	3,279	13975	7,637	8600	12,587	14000	6,266	13925	8,229	14000	13,658	11525	17,244	14000
718	23,585	13325	3,404	12700	4,028	13925	12,793	13375	7,476	9375	7,491	13175	7,447	14000	10,873	13775	14,460	14000
719	11,774	12925	3,468	4800	3,368	13900	11,835	4000	11,610	13000	8,021	4000	9,029	13775	13,271	12925	14,460	5950
720	18,812	12925	2,926	4425	3,985	13900	6,297	9075	6,190	13950	6,085	4225	4,624	13825	13,298	9500	9,941	8225
721	19,183	13375	3,468	13475	3,389	12950	6,606	13975	6,953	8625	5,750	13950	4,935	6950	10,000	14000	9,408	4525
722	19,260	13350	2,389	13100	2,184	13475	8,144	13175	8,628	12225	4,593	11850	5,930	13775	9,522	9450	9,761	8150
723	31,752	12475	2,767	10325	2,558	13900	13,503	10525	11,872	15975	7,730	10500	5,887	13950	25,439	10950	13,951	8350
724	20,367	11700	3,066	11475	3,359	13575	15,436	11625	10,847	13575	7,577	11000	7,617	13775	25,175	11925	8,071	4325
725	39,204	13400	3,397	13700	4,128	13975	13,902	13500	13,129	13925	9,163	13350	14,851	13925	27,990	13425	15,257	13950
726	39,670	13975	3,762	13975	1,922	7600	16,000	9775	4,446	6020	8,030	9175	3,464	6350	25,707	10975	14,272	5100
735	38,652	13525	2,894	7575	1,932	8450	9,357	7875	9,041	11700	4,775	12775	4,775	12775	14,789	7075	10,834	4925
736	24,597	12250	3,204	8300	2,306	6900	11,972	9050	6,732	7550	10,001	9000	5,381	7050	16,521	10275	11,444	7100
737	25,802	12200	2,508	8100	2,445	13575	8,214	9900	5,720	9500	5,445	10600	4,145	10600	13,103	9590	8,708	7500
738	29,594	13450	2,899	11275	3,812	13775	7,133	10025	7,002	14950	5,426	9850	8,507	14000	13,137	11750	6,302	6325
739	24,944	6125	13,800	8125	12,864	6225	12,736	2425	13,470	6125	12,371	6125	13,029	6525	10,715	6125	13,451	9125
740	24,371	13450	3,714	4175	2,615	7700	8,720	12275	6,086	4600	4,564	4300	4,218	7750	14,904	13425	7,106	7800
741	24,954	12275	1,988	13550	2,016	5975	6,128	5500	6,018	13600	4,753	4900	4,548	12500	11,002	5300	3,861	10150
742	17,171	13525	3,717	13375	1,583	13925	7,376	13525	6,370	10175	6,256	13425	9,448	14000	11,808	13425	5,001	10200
743	22,870	7400	2,404	13975	3,002	13275	6,913	12125	4,718	13975	5,536	11975	7,465	13975	10,936	4825	6,193	9275
744	18,878	7300	3,339	13575	4,100	14200	8,201	13575	8,215	12400	6,415	13975	4,504	7725	11,361	4425	11,040	13550
745	19,151	6350	3,974	13350	3,204	13200	14,180	13750	8,999	11775	11,691	13550	5,167	13975	12,066	4625	10,951	11475
746	19,669	6775	7,215	13950	2,865	13725	9,071	13950	8,339	13600	11,623	13925	7,438	13925	10,991	4725	11,020	5975
747	19,537	14000	3,036	5125	2,711	5200	13,995	13375	13,727	8075	7,441	11725	6,320	12575	13,379	5950	10,043	9775
748	18,525	8525	3,970	8525	3,985	14000	7,034	13750	7,704	13750	4,965	12525	9,329	13650	9,642	13225	6,449	11125
749	16,417	4750	2,432	13925	2,735	11225	14,732	14000	12,094	12925	6,441	13550	10,660					

APPENDIX I (Cont.)

PROF NO	MAXIMUM WIND M/SEC	M/SEC	SHEAR METER	-100M M/SEC	SHEAR METER	-100M M/SEC	SHEAR METER	-100M M/SEC	SHEAR METER	-100M M/SEC	SHEAR METER	-100M M/SEC	SHEAR METER	-100M M/SEC	SHEAR METER	-100M M/SEC	SHEAR METER	-100M M/SEC	SHEAR METER
539	55.864	11125	3.657	12388	4.153	7425	15.439	9375	17.774	14888	9.381	9388	8.342	13625	26.885	11488	21.189	14288	
540	58.279	11225	4.672	9525	4.887	13254	28.841	18888	18.685	13575	18.228	9575	11.626	13488	27.265	11275	23.921	13925	
542	42.353	9588	3.424	7525	3.176	13952	12.981	6475	18.471	13888	8.686	7625	6.673	18588	27.872	8588	14.579	13958	
543	49.897	11258	4.698	18575	3.787	12225	27.486	11825	13.899	12258	15.728	18888	9.844	12388	21.888	11825	17.916	14288	
545	53.423	13788	3.447	8575	6.259	12675	26.425	11225	26.175	11888	10.917	11688	13.889	11275	33.853	13675	15.124	12675	
547	57.368	12325	4.666	11958	6.228	11458	18.359	11258	11.487	12975	8.516	11988	9.966	11588	26.498	11275	19.989	4888	
549	57.879	12958	3.729	11425	3.569	13858	15.785	11375	11.611	13975	18.618	11388	7.573	14888	22.317	11375	15.881	4725	
550	56.426	13158	6.299	11575	4.888	13888	21.848	11988	7.614	14888	14.326	11788	18.078	13888	27.988	18325	15.958	6175	
551	57.149	13725	4.855	12988	3.623	14888	14.256	11775	12.823	14888	9.374	13825	9.189	14888	34.964	13225	19.588	5788	
552	58.556	13425	3.656	11925	4.699	13888	16.566	12888	13.462	14888	8.944	13425	18.498	13958	33.774	13375	12.317	4588	
553	54.743	11188	3.437	18858	4.582	13988	23.551	18425	12.488	12625	11.118	18858	9.418	14888	34.742	11188	17.747	14488	
554	62.595	11258	3.518	12925	5.544	12558	13.662	11275	14.798	13225	8.797	8575	9.874	11658	26.716	11175	21.583	14888	
556	62.267	11358	3.622	13758	4.359	13975	13.635	18888	16.713	13488	7.623	18888	11.331	12625	25.769	18825	24.845	14888	
558	38.927	8288	3.992	5788	3.382	12725	18.984	11175	14.175	13825	6.939	18575	8.781	13758	17.118	4375	15.848	11925	
559	44.761	18175	3.291	11188	4.264	12325	11.886	5688	11.655	11888	8.781	18175	9.831	13958	21.858	5625	19.929	12725	
560	33.832	11575	2.697	11888	2.518	13625	18.725	2588	8.466	8488	7.781	18825	7.278	7888	17.887	18488	14.192	13575	
561	65.115	11225	5.412	18758	4.785	12625	19.328	11158	14.439	13488	12.686	18988	12.583	12825	32.962	11858	26.162	14888	
562	63.971	11475	1.866	9458	4.881	13475	21.849	18988	13.495	13858	12.388	9688	18.839	13775	36.957	11375	15.364	14888	
563	63.169	11525	4.385	9725	5.381	12588	22.432	9788	15.888	13958	13.989	9275	18.917	12558	36.216	18975	24.439	14288	
564	51.888	11188	3.828	9288	3.171	11175	16.784	8188	18.289	13825	12.613	9458	7.558	11558	35.862	11125	18.994	11275	
565	45.349	11375	3.751	11275	3.457	14888	5.923	8788	5.78	4125	7.645	11358	6.455	4188	18.833	18925	8.441	4188	
566	38.674	13958	3.693	12758	3.569	13888	23.237	13288	8.128	5525	13.651	13888	7.355	12625	28.618	13275	8.212	11425	
567	25.178	12328	2.677	13225	4.676	12475	6.919	12858	8.857	13175	6.961	12825	8.478	12788	12.613	9525	12.868	5525	
568	34.253	12925	5.376	12475	2.695	12558	18.542	12753	4.287	13888	8.984	12925	6.824	13325	13.682	9975	4.891	4588	
569	28.386	14888	3.324	12888	3.839	12188	12.787	12825	5.755	12458	8.489	12525	8.665	12375	12.835	9525	11.451	4925	
570	32.964	13558	4.586	12775	3.825	13258	15.383	13158	7.286	14888	11.158	13158	7.945	13525	15.378	13588	2.128	11458	
571	42.968	13775	7.778	13775	12.418	13875	13.635	12458	11.726	12588	12.657	13775	7.834	11925	17.888	14888	9.888	11458	
572	37.837	13775	4.881	13775	3.895	12875	28.497	11158	7.935	12825	11.588	5875	7.473	13958	27.412	11158	2.888	7888	
573	71.464	11225	4.468	11888	5.798	13788	28.475	11988	25.869	13788	12.639	11875	13.182	13758	44.582	11975	21.158	14888	
574	68.128	12888	5.327	12888	5.613	13775	15.168	11925	26.465	13858	13.388	14888	14.198	13158	31.822	12388	22.915	14888	
575	61.749	12375	4.119	12225	5.318	12888	15.518	12358	23.197	13458	9.588	12225	15.968	12875	27.631	12458	15.263	14888	
576	61.714	13125	1.299	9925	3.468	12188	16.339	9958	13.381	13825	10.583	9958	6.463	13388	31.831	18888	8.473	13825	
577	78.966	11388	4.822	13888	7.234	13858	18.528	13958	14.324	12958	11.818	13358	9.278	12788	23.894	4825	11.833	13888	
578	74.432	11788	7.184	13788	7.184	13788	16.882	12958	16.882	12958	16.882	12958	16.882	12958	16.882	12958	16.882	12958	
579	81.864	11458	4.947	11448	5.323	11675	21.856	11425	22.872	12588	13.265	11425	13.984	11875	33.628	11458	15.993	14888	
583	82.924	11925	4.519	11188	4.534	12975	27.783	11988	28.137	12925	11.175	11275	17.335	12325	33.419	11625	21.822	14888	
584	65.778	13375	5.213	14888	5.737	14888	12.643	5225	12.318	13988	11.698	12925	11.996	13358	22.975	5825	8.888	14888	
585	59.783	11775	3.982	12575	3.375	8675	14.723	11458	9.588	12675	9.614	11425	7.885	12825	27.112	11828	8.888	14888	
586	63.465	12525	5.768	11725	3.859	13388	14.825	12888	28.286	8898	11.481	11925	9.158	8288	27.553	12558	8.888	14888	
587	62.333	13575	5.844	11458	5.388	13775	21.476	4825	21.137	5925	14.387	11625	11.988	5288	29.249	4888	21.622	7888	
588	62.475	13575	4.881	9258	3.895	12875	28.497	11158	7.935	12825	11.588	5875	7.473	13958	27.412	11158	2.888	7888	
589	72.674	12258	7.855	13558	6.338	13425	19.868	8825	11.778	13775	13.697	7488	15.573	13658	52.194	9158	15.667	13558	
593	74.783	18775	5.348	13825	4.445	12388	27.844	8975	15.168	13725	15.384	8425	18.293	13248	37.885	18788	15.859	13475	
594	66.484	12975	4.129	6775	5.148	13275	16.396	6775	16.973	13975	18.968	6775	11.819	13425	32.286	8988	18.224	13825	
595	67.248	12588	4.118	6388	7.888	13475	19.816	6658	21.883	13875	12.676	6558	12.888	13888	38.497	12825	7.789	14888	
599	72.754	11175	5.729	11825	5.935	12488	17.952	7825	7.942	12488	13.388	7788	6.891	12448	28.247	11175	4.342	13788	
600	74.388	12825	4.388	18725	4.884	12758	22.385	11175	18.813	13658	11.884	18788	7.289	13375	38.438	11958	9.888	13788	
602	59.218	11175	4.118	6425	3.968	14888	14.113	12975	8.835	8925	8.571	5388	7.358	14888	28.312	13175	15.267	9175	
603	51.914	12958	3.886	12758	3.428	9275	17.912	12958	11.835	9525	11.285	12875	7.914	13975	22.682	13358	21.198	9158	
605	55.238	13188	5.931	13188	5.273	13288	17.864	13388	12.274	7688	14.895	13188	18.447	13888	26.889	13188	18.822	8925	
605	57.819	13558	5.444	13125	8.273	13988	17.521	13788	11.448	13558	11.448	13558	17.713	14888	26.988	13375	11.888	8988	
607	54.948	11425	3.914	13588	4.968	13575	19.184	4725	11.871	13588	9.148	4588	11.151	13575	31.187	8575	16.861	9588	
608	58.469	12925	5.682	6575	3.418	12725	18.244	5588	13.262	13625	11.272	6925	8.516	13158	29.722	5225	11.888	13925	
609	55.558	12558	5.294	6988	7.884	13188	17.265	13188	17.388	14888	12.381	6658	13.881	13188	26.885	6175	22.231	14888	
610	56.446	13288																	

APPENDIX I (Cont.)

PROF NO	MAXIMUM WIND M/SEC	1100M SHEAR METER	1200M SHEAR METER	1300M SHEAR METER	1400M SHEAR METER	1500M SHEAR METER	1600M SHEAR METER	1700M SHEAR METER	1800M SHEAR METER	1900M SHEAR METER	2000M SHEAR METER	2100M SHEAR METER	2200M SHEAR METER	2300M SHEAR METER	2400M SHEAR METER			
395	36.221	13954	4.408	13725	4.454	14084	11.907	11375	12.411	12450	18.344	13825	7.989	11775	19.713	6925	18.268	5575
396	41.617	12204	2.596	11525	3.349	11704	15.741	11650	10.422	4084	6.896	11725	8.131	13725	24.142	11554	13.683	4304
397	41.997	13454	2.789	4544	4.912	13904	10.465	9775	9.236	14044	6.459	5984	9.083	14044	22.649	11825	14.473	5454
398	45.787	13824	4.651	13804	5.158	13524	12.844	10754	14.016	14084	8.117	13274	10.433	13804	24.369	12684	18.927	4324
400	36.348	13924	4.258	12674	3.474	4654	18.433	12184	6.937	10624	11.226	12724	7.298	12674	13.319	13924	5.266	12624
401	39.253	12384	3.626	12254	2.986	11204	12.849	7724	6.579	7150	6.118	5784	7.866	12849	18.434	13174	4.803	13424
402	41.255	11214	3.889	9724	2.935	12754	12.978	12324	6.675	13084	6.194	11124	6.426	14049	20.928	12324	2.873	9754
404	43.952	13174	3.480	11774	6.384	13954	14.938	12224	18.667	13974	10.484	12854	14.254	13824	27.811	12224	7.168	13774
405	27.132	13474	3.567	12474	3.786	5584	11.418	12374	8.426	13774	6.848	12184	7.261	13874	17.886	13474	7.442	6584
410	31.496	12274	2.864	11774	3.568	12904	10.375	8824	8.358	13474	6.383	12224	6.943	12674	14.745	6554	2.868	6584
411	42.947	11584	3.917	13774	5.875	13524	14.687	5574	7.393	12874	7.295	4974	9.962	13404	19.493	4264	5.674	13724
412	22.332	13974	4.525	4574	3.595	13924	11.442	5384	6.993	8894	7.990	4674	5.391	12604	23.992	6174	3.428	8924
413	62.652	13984	3.817	5124	3.202	14284	11.136	5454	4.322	13804	7.395	5154	7.321	13824	21.827	4084	3.304	8924
414	61.543	18924	3.247	13524	4.948	13444	10.841	5154	11.592	13224	7.785	4924	14.262	13624	30.333	5174	13.467	14424
415	53.944	13804	3.575	5774	5.282	13284	9.637	5974	19.410	13924	7.408	6854	12.892	13474	22.454	6884	15.265	4474
416	41.561	11684	3.267	9124	3.323	13754	12.127	9974	14.351	12264	7.753	9384	9.875	12884	22.362	11364	15.728	14444
417	42.811	12524	3.287	8124	3.199	13674	17.162	9054	18.686	13404	9.858	8474	8.878	13954	30.423	9374	15.897	4454
421	53.362	13584	4.754	13474	5.997	13774	18.431	13924	21.191	14044	11.518	13384	18.523	14044	24.839	7454	20.268	4274
422	53.359	13584	3.685	13874	7.245	13674	17.745	14544	13.654	13574	13.654	13574	12.350	14044	25.368	13304	3.238	13304
423	54.431	13954	4.928	13554	6.118	13554	14.443	13324	14.751	14544	7.837	13854	11.916	13924	25.498	13324	11.043	13584
424	44.768	10774	3.325	13584	3.278	13924	15.447	1284	14.751	13424	6.585	8824	7.475	13304	25.119	10224	17.317	13574
425	45.565	13474	3.366	13374	4.663	6524	9.625	8354	7.988	6654	6.584	7854	6.561	13874	13.958	4084	5.727	13374
426	38.488	12474	3.158	13484	3.573	4974	12.869	4124	7.488	8784	5.148	5984	6.674	13374	24.348	4054	5.775	13924
427	32.213	11924	3.935	11774	3.611	11684	8.161	11824	8.585	12454	7.465	11884	6.733	11744	14.728	8524	18.799	13954
428	23.698	12724	3.235	9474	3.493	13974	17.777	14254	7.261	13924	7.913	9724	4.763	13324	19.467	10824	4.412	13924
429	28.243	12984	3.317	12424	2.817	15884	7.235	12124	6.427	7474	4.364	11774	5.598	7884	14.131	9454	3.789	4584
430	28.829	13184	3.351	18124	4.717	12124	8.141	13584	7.488	5374	5.885	5984	5.224	13944	12.238	13304	3.238	13304
431	44.195	13974	3.337	9124	4.912	13174	11.172	9454	22.524	14084	8.449	9074	11.911	13924	25.498	13924	11.043	13924
433	47.463	12524	3.366	7124	4.498	13724	13.163	5854	19.222	13724	9.367	5924	11.866	13624	21.745	5884	13.778	13954
434	46.787	12454	3.189	11524	4.283	13824	12.222	5454	13.721	14044	6.965	7824	12.933	14044	19.729	7654	2.158	4524
435	58.239	18974	3.317	12454	4.413	11254	15.287	7474	13.513	13784	8.323	7154	8.297	11374	29.518	7574	22.147	13924
436	46.794	12884	3.391	13574	4.878	12974	15.211	12884	21.997	13874	8.345	11554	13.588	13254	28.187	12774	15.868	13924
437	47.478	12584	4.511	15574	5.707	12754	16.803	12884	23.739	13674	9.495	12574	13.198	13354	21.582	12684	7.977	13374
438	47.832	13274	4.398	4524	5.496	13624	14.585	12974	14.351	12974	18.367	13674	16.314	13924	21.765	12724	15.428	13484
440	44.195	13974	3.374	13274	6.937	13484	11.774	9124	7.923	12874	8.888	13724	11.201	13674	19.981	13724	3.808	14084
441	45.389	13584	3.682	12224	4.287	13874	9.978	12484	6.381	524	7.874	13884	14.161	14284	18.253	4424	5.782	13974
442	41.429	9374	4.026	12474	3.753	11724	12.452	4224	10.113	12874	7.573	13954	7.886	12924	17.592	4824	1.788	13374
443	53.335	12984	3.462	12474	5.192	13724	17.808	12684	13.114	13754	9.748	12624	11.862	13924	26.513	12984	18.247	14084
444	53.372	13484	3.178	6924	7.443	13824	12.353	13354	11.678	14044	6.373	6324	14.842	13904	23.919	6384	12.383	14084
446	58.355	13574	4.726	13374	4.158	14284	17.291	9174	15.821	12884	12.188	13674	12.183	14084	24.233	11124	5.438	12974
453	42.678	13374	3.513	11774	2.955	12974	12.365	12874	7.892	7874	7.948	12924	5.173	7484	18.443	13374	28.287	4924
454	46.178	12784	3.903	11224	3.251	13124	22.965	13184	9.056	9804	11.268	12884	7.248	13894	29.584	12724	12.248	12784
456	44.667	14884	3.785	11924	4.458	11654	11.314	12224	7.342	11394	8.853	11954	7.913	13924	16.358	12454	14.189	4184
459	29.924	13524	4.771	12174	2.886	13884	13.448	12724	7.553	13874	7.340	12654	7.545	13874	17.476	12884	13.888	7854
459	37.471	14884	5.569	13584	4.573	13154	16.982	13774	7.458	4524	9.475	13724	3.362	6424	17.543	14884	14.242	4584
459	41.808	13974	3.428	13424	3.138	9254	13.995	13774	11.127	5424	9.328	5924	7.454	5424	21.567	7474	17.492	4684
460	39.138	12984	3.859	12774	3.156	13424	13.638	12884	11.383	13424	13.487	12774	7.525	13224	19.778	6774	7.421	13174
461	53.345	13124	5.102	12774	7.288	14584	19.799	13184	24.441	14084	12.376	13284	19.291	13744	27.769	13184	7.998	13874
463	61.577	12954	4.398	13984	3.273	6484	15.949	6874	9.381	12874	8.137	13884	7.529	6884	25.184	7874	3.808	13574
463	51.638	12524	3.346	8924	5.175	8884	21.229	12854	18.866	14524	15.474	11784	18.176	8124	35.649	8274	11.144	9124
466	57.474	12774	3.428	6524	3.799	8824	24.689	6974	14.188	12974	16.165	6784	7.472	7974	38.086	7884	23.452	13984
467	48.472	11574	4.295	7924	3.282	12954	24.684	8854	8.878	13584	11.119	8184	6.638	8624	34.577	9874	24.347	4524
468	45.832	12584	4.296	13954	4.263	12884	13.448	9554	24.336	13554	11.252	13954	12.789	13974	24.385	9754	15.428	4824
469	59.181	13524	4.395	7124	4.875	13924	17.444	8874	24.933	13874	15.787	7584	13.521	13584	31.888	9974	13.722	4874
470	57.381	13974	4.372	6574	4.388	14884	15.354	7284	6.486	13974	12.817	6774	11.256	13874	24.516	6674	8.438	14084
471	54.985	12254	5.287	13884	3.774	14244	11.296	6594	7.768	13884	7.512	7174	4.994	12594	23.417	4824	9.879	13984
474	66.183	9544	5.887	10174	4.413	12454	18.625	5454	18.443	14724	12.428	6574	15.063	12224	31.067	9174	19.761	12884
475	67.335	8774	4.776	4874	4.124	12844	14.351	12224	16.412	13724	14.223	11254	15.881	11154	38.944	7884	28.214	11954
476	58.421	10874	3.781	4174	4.161	12824	11.297	4424	16.413	11984	9.844	9824	11.823	11324	39.659	18984	23.792	13924
477	50.428	11554	4.287	10754	4.577	10674	11.914	11774	8.726	13184	12.297	13624	13.343	13784	26.115	4854	23.887	12724
478	73.197	11554	4.338	13524	5.947	12774	24.444	8274	28.538	13884	13.179	5874	12.796	13884	42.988	8724	12.918	13984
479	65.397	10854	5.311	13584	4.213	13924	15.416	11774	11.486	13884	11.965	5174	13.166					

APPENDIX I (Cont.)

PROF NO	MAXIMUM WIND M/SEC	MIN WIND METER	+100MM SHEAR METER	SHEAR METER	-100MM SHEAR METER	SHEAR METER	+100MM SHEAR METER	SHEAR METER	-100MM SHEAR METER	SHEAR METER	+400MM SHEAR METER	SHEAR METER	-400MM SHEAR METER	+100MM SHEAR METER	SHEAR METER	-100MM SHEAR METER	SHEAR METER	
271	11.442	6175	3.040	6175	3.382	6275	7.660	6175	6.882	6175	5.778	8475	4.981	11500	7.316	6175	5.124	13775
272	11.443	5980	2.644	4558	2.380	13575	5.194	5350	5.958	6925	4.584	18925	4.409	13425	8.510	4850	9.294	13475
273	11.676	4575	3.500	5375	3.705	5675	8.249	12100	7.314	11825	4.802	5575	5.900	8575	13.651	12650	14.713	12125
275	6.778	6825	2.795	13550	2.442	7000	6.274	4700	6.063	7825	5.065	13900	4.037	6425	7.759	6050	5.868	13350
276	5.461	18475	1.869	8375	2.331	13350	6.587	8575	4.153	6080	3.881	18400	4.427	13520	6.610	10550	5.666	7775
277	17.248	12250	3.203	13400	2.335	12400	8.980	13650	11.224	13450	5.446	13700	6.233	12700	18.045	13775	9.972	4800
278	21.908	13225	7.336	13500	12.861	13450	9.433	13000	8.094	8800	8.094	8800	15.482	13425	13.590	11875	7.454	7525
279	11.247	13550	2.862	5150	2.085	7775	6.520	13850	6.578	13825	4.221	6500	3.843	6475	10.321	14000	6.667	4325
280	14.054	13400	2.904	7425	5.439	14000	8.209	13525	9.271	14000	4.847	13150	8.578	14000	12.190	10850	7.127	14000
281	5.305	5150	1.843	9375	1.878	9850	6.287	7425	7.358	6350	4.183	14000	3.908	6275	6.872	14000	5.542	6550
282	6.904	4275	3.251	9500	9.761	9700	6.392	9375	8.749	10600	8.796	9600	8.523	10820	7.810	9600	8.508	12500
283	6.818	4350	2.957	5925	1.565	5925	3.692	14000	5.825	5925	3.564	14000	3.954	7450	4.753	4800	5.068	9375
284	12.187	4700	3.966	12750	3.578	12950	5.956	13275	5.548	9825	5.587	13075	4.121	13975	9.941	11550	8.652	10550
287	23.973	13425	2.984	10700	1.713	5475	8.569	11625	4.817	5625	6.813	11175	3.004	4600	17.292	13725	4.723	7575
288	10.987	18375	2.703	13175	2.480	12900	9.246	13550	13.010	13225	6.454	12150	8.034	13200	12.935	9250	9.474	13275
289	14.941	6375	4.075	13100	2.714	12700	12.521	13575	12.894	12975	7.634	12525	7.532	12500	10.781	11475	13.431	8925
291	12.967	11900	2.891	13525	2.573	6875	8.288	13875	6.521	13400	6.351	13850	4.821	7150	11.562	10725	7.484	6550
292	9.071	13325	2.486	13350	2.727	12625	6.398	13725	5.396	9800	5.125	13725	3.843	7875	6.989	5600	8.508	4475
293	17.945	13150	2.771	12400	2.985	13575	18.412	12950	9.597	13975	5.723	12600	6.754	13650	11.859	13300	7.862	7525
298	19.441	8325	2.187	11525	1.871	13225	5.361	8250	4.594	4350	4.437	8150	3.111	12250	10.876	12375	3.747	6700
295	15.238	13175	4.441	13175	2.435	13275	12.438	11250	18.688	10000	9.366	13175	7.484	10850	20.855	13175	13.925	12550
296	16.678	14000	2.875	13575	2.558	13800	7.135	10525	3.975	11400	4.177	14000	5.274	7550	10.978	12500	5.128	5900
297	16.924	13475	2.880	6150	1.834	13625	8.365	13225	4.496	5500	5.223	12825	5.430	12800	11.205	13075	5.260	5925
298	11.737	10725	1.987	12325	2.185	12750	7.012	9700	6.108	13400	4.789	9725	4.741	12925	9.174	10175	7.213	6175
299	14.645	13725	3.969	13125	2.866	13050	8.811	9200	5.726	6200	5.188	11550	6.334	14000	13.302	13725	7.812	6350
300	19.338	13900	2.468	12950	2.583	13750	6.518	12875	4.440	6825	4.822	12875	3.269	4475	11.887	13575	4.245	6450
301	16.991	13900	5.746	8025	3.298	4550	7.873	8850	6.214	4750	5.285	9225	4.674	4825	9.812	11825	5.528	5900
303	19.182	13950	2.860	5475	2.367	5450	5.079	8275	6.282	5475	4.991	5650	4.708	5600	8.488	7825	5.132	7420
304	21.689	12400	2.620	12175	3.411	13675	6.442	8900	4.537	13975	5.181	12400	7.818	13750	18.544	10925	5.760	13775
305	18.705	13225	2.479	12575	3.189	13350	8.623	12725	9.698	10950	5.811	12750	4.821	12175	18.185	11750	5.410	7125
306	11.816	12400	1.736	13325	2.689	13850	4.454	9100	6.543	14000	3.888	4750	5.644	13970	7.268	11600	5.932	6125
307	18.114	9975	2.565	8000	2.828	10825	7.576	6575	11.396	10000	5.562	11825	6.157	10000	12.453	7400	9.479	11225
308	16.441	8325	3.963	8375	4.711	13225	11.981	8525	13.888	13650	8.053	8350	18.798	13500	11.468	12500	13.237	12175
310	17.998	11950	1.820	8375	3.127	12400	14.774	10450	8.147	13650	7.112	10350	9.976	12550	19.913	11725	8.245	10825
311	12.687	11900	2.303	9100	4.489	12800	7.666	9225	8.975	12475	6.543	13900	7.723	13850	14.148	11710	7.197	10125
313	16.756	13100	2.488	9275	2.614	8725	9.051	13075	6.565	14000	5.286	10100	4.935	14000	14.842	11175	9.522	6925
314	17.228	13575	5.817	12375	2.723	11725	14.182	12575	10.286	11750	11.333	12475	7.154	11175	26.474	13750	6.719	7700
315	34.545	6250	4.841	5525	4.966	9200	13.425	10850	15.336	10850	11.883	5825	9.112	9200	17.958	6875	31.347	10550
316	23.177	12525	2.444	4975	1.879	7825	11.614	12625	8.147	13650	7.874	14925	6.524	5800	15.727	12750	5.489	6125
319	25.558	13575	3.942	5450	4.779	5425	11.655	11675	7.347	7825	9.294	5700	9.918	7800	28.086	13650	12.462	9800
321	23.478	13700	4.438	10475	2.421	11050	8.435	11175	7.726	9500	9.378	10625	4.651	9425	11.259	4925	5.503	10375
322	28.981	14000	4.161	10550	2.318	9450	9.051	11250	6.534	10250	7.962	10825	6.038	13350	10.429	4000	5.608	11100
323	21.424	13975	3.478	4575	3.371	10400	10.823	11275	7.535	12175	7.941	13950	5.237	13425	12.637	4250	5.704	11375
324	11.228	10850	3.963	13475	2.782	13825	5.918	9225	6.044	20850	5.953	13225	5.693	13525	11.678	4925	4.112	13450
325	22.653	18325	3.108	10750	2.669	10925	4.981	12000	8.146	11800	5.239	13300	5.832	11175	10.439	4275	4.917	13150
326	25.886	18775	3.489	13700	3.148	13675	7.327	16775	9.064	11975	9.187	13825	5.533	12800	10.357	4275	4.568	13525
327	24.880	18950	3.711	13725	3.363	13700	6.562	10850	9.666	12175	4.884	13775	8.673	11800	18.059	8000	5.247	13325
328	18.693	7825	3.356	10100	2.672	9400	9.598	10775	9.278	9500	7.121	10225	5.348	9575	10.564	12625	9.387	9300
329	25.979	11275	2.886	10350	2.715	12850	8.921	11300	11.426	12275	5.229	10800	6.951	11675	11.815	7850	5.148	13950
330	17.674	14100	5.646	13775	4.223	10800	48.839	14000	4.097	4325	24.119	14000	11.295	10200	96.979	14000	5.404	4550
331	22.227	13350	4.548	12400	2.923	4275	15.868	12350	8.251	11900	9.128	12175	7.995	12500	29.787	13550	8.243	11800
332	17.755	13550	3.871	12150	4.387	11900	21.385	12225	20.219	12125	14.416	12125	12.821	12975	28.129	13550	22.268	12900
333	16.793	13325	3.538	10525	3.865	10575	19.924	11450	18.891	10775	11.797	10875	5.568	9425	19.059	11475	18.127	7225
334	9.078	13325	2.333	13520	2.638	13625	6.428	13325	6.087	12100	5.388	13275	4.467	11000	9.285	13475	7.831	11125
335	18.841	6100	2.188	13375	2.175	13725	4.626	13275	7.658	11525	4.285	13825	3.664	11025	5.319	9950	8.739	9750
336	15.357	13225	4.432	4000	4.684	4850	7.005	6775	6.319	4325	5.222	4725	6.186	4400	18.399	7325	8.274	4525
337	28.991	9350	1.195	13225	3.246	12850	9.542	5700	10.972	13650	5.419	5100	7.028	13550	13.577	7700	14.266	13740
348	16.788	8325	3.732	6750	3.893	13000	8.251	8250	12.168	7825	7.951	13300	8.465	7500	15.785	6725	14.444	6125
341	31.958	13950	3.711	13725	3.662	13700	6.562	10850	9.666	12175	13.779	13275	18.484	12725	20.187	12375	7.129	5350
342	17.717	13225	3.688	7550	3.344	13600	12.955	11000	8.950	9250	6.749	11200	9.662	13625	15.685	13200	7.292	7500
343	27.787	13625	2.613	9225	6.899	13975	11.843	9700	11.997	8950	7.823	9300	9.675	14000	14.831	11700	11.675	8700
344	24.424	14200	3.938	13000	3.298	8275	10.186	9725	13.318	8750	9.200	14000	9.784	8375	14.743	10725	18.699	8925
345	32.274	13525	4.695	8975	5.184	8875	10.518	12925	8.543	8675	7.884	13625	6.849	13975				

APPENDIX I (Cont.)

PROF NO	MAXIMUM WIND M/SEC	M/SEC	METER	+100M SHEAR M/SEC	METER	-100M SHEAR M/SEC	METER	+1000M SHEAR M/SEC	METER	-1000M SHEAR M/SEC	METER	+400M SHEAR M/SEC	METER	-400M SHEAR M/SEC	METER	+1000M SHEAR M/SEC	METER	-1000M SHEAR M/SEC	METER
148	26.396	13392	4.197	12552	3.789	12720	6.691	10825	7.288	13150	8.794	13980	9.338	13380	10.789	12625	10.415	7100	
141	46.115	14880	3.963	13775	3.773	13225	16.989	13775	17.504	13780	12.256	13525	12.628	13450	24.751	13880	24.589	4380	
142	43.508	18425	3.727	18125	2.613	13925	12.453	18150	6.946	11150	7.638	18150	4.805	12890	26.230	18150	4.299	3125	
143	45.435	13325	1.293	6100	2.937	9025	13.248	10550	6.948	12250	7.733	9950	6.891	9250	21.791	8575	4.131	13225	
144	48.265	13325	3.376	7425	3.705	13450	13.807	18675	8.478	14800	6.942	8250	8.361	13750	23.348	18880	4.049	13780	
146	49.571	13300	5.147	13375	3.195	6700	21.480	13725	8.282	7175	12.494	13550	6.155	6900	28.238	13975	14.388	8575	
147	46.371	13325	3.968	5900	4.385	6925	13.784	13225	12.429	7475	8.072	13150	9.566	7000	25.752	14000	9.339	4900	
148	45.295	13125	3.347	4100	4.822	4350	12.526	7500	9.083	5125	7.961	11350	8.681	4600	21.817	8225	5.072	19500	
149	54.421	13300	4.863	6100	2.857	9320	14.182	12750	5.215	18125	19.565	8050	4.166	8350	19.157	13425	8.289	18580	
150	59.765	13420	4.818	13575	7.292	13525	9.339	7250	9.457	8400	7.499	7320	10.945	13850	25.886	4800	3.893	13300	
151	38.575	13150	7.947	9375	3.255	13480	14.223	9825	13.515	14880	12.193	9375	8.395	13780	21.791	12125	12.147	8275	
152	48.728	13300	1.321	13775	2.419	9450	9.513	8475	8.545	4175	6.166	10850	3.995	9650	23.454	9400	9.255	6150	
153	24.137	13250	3.086	12900	4.924	12425	10.273	13325	11.150	14000	10.779	12825	12.138	13950	12.793	9629	9.238	6380	
154	23.373	13325	3.931	13375	2.534	13725	10.177	11125	5.328	12925	6.098	13625	4.618	14000	14.968	11175	5.273	4575	
155	25.213	12725	3.283	12775	3.521	12825	12.928	12475	13.821	13500	6.999	9175	9.852	13020	16.113	17275	12.415	7425	
156	27.487	13375	3.188	13300	6.745	13600	12.761	13400	6.466	9425	9.708	13250	15.233	13780	16.766	6625	6.058	13980	
157	24.321	12150	2.851	13925	3.673	12575	18.068	6300	10.754	13150	6.754	6225	8.718	12800	11.836	8225	7.281	14400	
158	18.882	9375	2.758	13550	3.949	8525	9.157	5950	9.467	11875	6.381	9325	5.842	13475	13.881	6188	18.642	13530	
159	17.389	12575	3.522	11450	5.194	13325	11.858	9700	12.889	13625	6.615	12590	8.888	13425	18.373	11575	5.405	14200	
160	38.687	13550	3.433	8550	2.613	12800	11.551	13400	6.483	12325	5.142	12425	7.858	12880	12.845	5525	9.762	4200	
162	34.861	13775	2.981	13550	3.129	9200	15.651	8675	7.957	13925	5.169	13400	23.763	9725	11.989	4400			
165	38.269	13575	4.365	8100	3.257	9250	15.848	8750	9.270	9725	10.899	8375	8.936	13975	18.883	9852	13.696	4375	
166	27.796	13925	5.496	13925	3.183	4550	12.869	8450	7.176	10275	7.583	8425	6.222	13250	16.929	9425	13.733	4575	
167	25.187	14300	4.742	13475	3.393	11500	17.251	7600	7.568	13425	9.377	13950	7.198	13650	15.885	8950	14.484	4350	
168	26.868	12575	3.968	13000	2.959	13000	11.442	12100	2.351	8875	6.311	8875	5.131	8875	21.541	12725	7.366	13880	
169	21.968	14200	3.927	7900	11.811	11700	9.958	13825	7.328	13750	7.328	13750	6.434	13780	18.566	7100	7.359	4550	
171	18.098	11225	1.229	13980	2.094	4750	7.463	5100	7.547	5100	4.923	4975	6.675	4750	8.172	8625	7.129	13775	
173	15.612	12425	3.399	11125	1.969	5575	12.967	11825	6.916	11425	5.773	5275	18.189	8725	7.738	7850			
174	15.556	14000	2.388	8325	3.819	8375	9.192	12325	8.051	9800	6.592	12800	5.132	7950	13.177	14000	11.239	8875	
175	26.197	13775	4.687	13925	3.294	11450	13.689	13850	6.763	4150	8.191	13175	4.442	12125	21.443	13975	12.552	6175	
178	18.486	14000	3.552	13925	2.788	4950	9.147	11875	6.786	4575	8.738	14000	5.187	4525	13.203	12780	9.897	4950	
179	22.778	13975	3.711	11450	3.599	11975	12.878	11950	6.387	4675	6.359	6500	6.598	11400	19.146	10500	11.351	4575	
180	21.777	13375	2.768	4875	2.254	13925	13.253	13925	6.511	8875	6.511	8875	5.751	8875	11.808	13880	11.808	13880	
187	17.494	14300	2.433	4180	8.859	11325	9.197	12750	4.924	18675	5.049	12225	16.174	10925	13.849	14200			
188	23.145	14000	4.268	14000	2.899	7625	9.474	10275	9.753	8400	6.455	9675	5.174	7925	13.027	7175	7.767	9275	
189	24.968	13250	3.348	13150	4.515	13975	14.237	13175	10.413	12175	8.816	13150	8.465	14000	17.912	5200	7.995	18250	
189	25.117	12225	3.148	11750	3.239	12775	12.563	12225	11.925	13325	7.997	12225	6.659	12850	13.239	8800	8.260	10250	
190	14.399	7575	2.229	14000	2.891	4575	8.186	4000	11.474	4375	5.928	4650	6.035	4700	15.622	6350	14.723	6300	
191	22.518	12575	2.685	7575	1.847	8025	4.228	4900	5.674	13550	6.317	4825	3.566	12975	12.399	12575	8.863	4375	
193	20.359	12500	3.988	13375	3.911	14080	11.589	11750	8.951	12925	9.688	6725	10.429	12850	18.831	6175	5.486	13880	
194	36.422	12275	3.985	11425	3.133	11275	9.249	12100	10.126	13000	7.911	13525	8.548	13250	20.374	7180	10.110	6550	
196	31.624	12525	3.895	8175	4.568	14000	14.834	8275	11.211	11425	3.507	8275	7.927	13850	20.999	8300	5.845	5550	
197	31.687	13700	4.454	13575	5.913	13875	14.751	12500	9.787	13350	14.767	13425	11.699	14000	17.881	8100	9.499	5530	
198	29.748	14000	3.488	4350	2.787	13075	9.388	11625	14.792	4350	8.403	6350	7.824	4825	15.561	6500	28.811	5575	
199	22.982	13575	4.817	13275	2.922	13750	11.841	10300	4.774	8500	10.226	13500	7.886	13900	13.259	13675	8.481	5275	
200	26.871	13525	3.178	13150	3.747	13880	9.828	8775	7.813	12925	11.442	13375	8.257	12925	18.029	11825	5.351	13380	
201	31.768	12400	4.712	5900	3.991	5775	14.989	12480	12.195	13450	12.849	8200	10.316	13350	18.928	8225	7.348	5525	
202	12.166	13950	4.945	13125	7.538	9180	16.837	12300	8.473	5675	6.473	8375	5.752	6525	16.875	13950	12.418	18550	
204	28.858	13775	2.998	6400	2.921	7875	11.465	12700	4.261	9425	5.545	12525	4.867	6625	24.644	13725	13.556	11780	
205	14.878	8950	3.814	8550	2.632	9450	9.877	9925	6.985	13050	6.622	8925	5.288	9575	10.556	9750	9.881	11525	
207	16.199	14000	2.266	9450	3.318	6920	6.918	13225	7.613	9175	4.896	13950	13.448	8590	13.448	14880	13.343	18175	
208	16.293	4775	2.433	4425	2.469	4900	7.799	4900	6.196	6425	4.952	4300	7.311	5125	5.874	6650	5.489	9550	
209	18.474	12150	2.959	13125	3.359	13975	6.339	18850	9.927	9675	5.945	13375	4.811	14020	10.236	12450	3.378	9375	
210	17.137	13425	3.811	4975	3.315	7325	7.068	13650	7.739	9500	7.352	13375	5.077	10125	10.628	13425	2.928	13800	
213	22.333	12950	4.683	9300	3.876	9180	11.452	12275	10.103	13950	7.372	12150	6.589	13300	23.198	12950	8.853	6975	
216	17.111	13575	4.882	4475	4.346	9550	11.388	4900	11.354	5100	8.611	4625	9.482	4500	13.363	12380	12.694	9180	
217	20.747	13325	2.612	13275	4.941	13600	12.484	13325	7.865	14020	7.789	13325	12.938	13725	17.973	11525	9.953	5425	
219	14.147	5500	3.804	13775	3.478	14200	6.999	8125	13.008	13775	5.565	13775	4.752	13275	7.818	12880	8.215	6550	
221	16.522	13975	2.911	4950	3.653	4875	14.429	13550	7.188	11125	7.187	13750	7.906	5175	15.292	14080	14.242	7450	
222	22.928	12575	3.552	13575	3.112	4825	7.727	6500	18.897	15600	7.225	13600	6.797	12775	13.159	8400	18.257	5875	
223	13.896	12925	3.781	13275	3.138	12475	11.748	13875	6.822	12750	8.207	13680	5.898	8150	7.998	12875	4.438	5980	
224	12.339	13775	2.998	6400	2.921	7875	11.465	12700	4.261	9425	5.545	12525	4.867	6625	24.644	13725	13.556	11780	
225	14.442	14000	4.216	13175	4.357	13350	14.623	14000	7.148	12825	10.891	13975	6.86						

APPENDIX I (Cont.)

PROF NO	MAXIMUM WIND M/SEC	+100MM SHEAR METER	-100MM SHEAR METER	+1000MM SHEAR METER	-1000MM SHEAR METER	+1000MM SHEAR METER	-1000MM SHEAR METER	+400MM SHEAR METER	-400MM SHEAR METER	+1000MM SHEAR METER	-1000MM SHEAR METER							
2	38.822	1335A	3.956	13825	3.876	18088	13.733	13325	6.881	12650	18.758	13875	9.948	18075	26.733	13275	5.565	9808
3	24.741	11775	3.863	11975	3.349	12158	15.355	11975	14.309	11850	8.635	11975	6.831	11225	16.732	13528	19.593	13825
4	14.497	4825	5.073	12558	3.479	12352	11.851	13358	9.324	12425	10.634	12775	7.077	12375	11.749	4728	11.711	12375
5	32.872	12958	3.969	14088	6.153	13375	17.837	12958	23.113	13975	18.338	13558	16.319	13375	21.592	8108	15.993	11188
7	16.279	12575	3.373	11975	2.788	12725	11.699	5458	8.311	12875	9.345	12475	5.668	13958	16.618	5188	13.132	18858
9	13.633	14888	3.268	13325	2.767	12975	11.382	5375	6.311	12875	7.931	13275	7.559	12875	7.559	5225	8.014	18475
10	16.612	14888	4.134	13388	4.281	12975	11.917	5275	8.672	13225	10.965	13258	9.686	13158	14.648	5175	9.936	18325
11	15.248	14888	3.873	12958	2.822	4225	11.361	5688	8.447	8625	9.152	13875	6.268	4225	13.888	5158	9.216	12625
13	17.436	14888	3.118	13325	2.549	4188	8.353	13888	6.983	12658	5.585	5188	5.242	11688	11.834	9258	10.697	4158
15	24.544	13725	3.188	11425	2.518	13958	13.533	13758	6.932	6358	7.354	4888	6.822	13558	17.491	12358	11.235	8358
16	29.378	13557	3.465	11158	3.491	4758	8.882	12888	9.452	5325	6.699	11325	8.888	4775	28.286	12258	11.175	7325
18	37.546	8758	3.312	13588	2.986	13458	13.548	5525	11.753	13658	7.764	13725	6.655	12858	25.845	5358	12.858	13925
19	24.653	12925	4.894	9875	3.876	13375	18.954	12925	15.459	13958	7.784	12575	12.227	13558	22.885	5988	19.845	4725
20	41.659	12375	5.564	11358	4.157	13625	28.538	11758	12.314	14688	15.735	11275	9.327	13988	25.323	12575	5.183	8825
29	55.287	11975	5.838	11558	5.885	12858	22.328	11958	21.594	13258	14.281	11658	11.235	13388	31.159	11958	9.978	13557
30	59.971	11958	4.958	13775	6.179	12152	13.274	11858	23.672	12925	18.989	13988	13.139	12388	29.836	11125	18.698	13587
35	57.847	18158	4.745	18288	6.411	18275	16.412	13475	19.946	13775	9.636	4658	13.667	13758	21.951	7158	15.807	13525
36	68.612	18275	4.551	13588	4.432	18458	11.881	6158	28.324	13925	9.888	8875	12.815	13888	26.519	4175	24.838	13925
37	61.188	18188	4.283	18425	5.395	18275	14.125	6458	24.583	13875	18.838	8425	14.382	13658	27.758	4325	27.732	13875
38	57.848	12875	4.637	8775	3.336	8875	15.397	12625	12.254	14888	9.885	11925	8.993	14888	23.144	12875	11.482	14888
39	63.887	11925	4.978	13125	6.328	12825	17.522	13358	16.653	13325	12.781	13875	14.413	12875	27.468	4975	15.264	14888
40	56.825	12588	4.895	13158	5.379	13288	15.169	11325	14.231	13825	9.259	7975	9.798	13958	28.410	11375	15.578	4888
41	44.963	12925	4.432	12825	4.121	13825	13.585	12958	11.629	12788	10.114	12558	9.534	12488	27.978	12925	8.887	4888
42	35.886	12975	5.336	12525	4.471	13325	14.226	12975	17.413	14888	9.398	12625	9.691	13958	18.969	13888	8.455	6757
43	54.478	13888	3.881	13888	2.641	13888	13.641	18425	8.779	14888	11.524	12158	5.219	14888	28.879	9488	7.537	13888
44	33.697	12875	4.574	11775	3.414	12875	22.183	7575	8.611	13866	4.515	18888	6.515	18888	27.272	12875	11.482	4888
44	33.243	12958	3.879	11525	2.955	4975	19.539	11925	7.524	5325	11.354	11675	6.287	18875	27.533	12475	18.888	4225
47	33.483	12825	4.358	11558	2.924	18888	22.214	11658	6.549	5425	13.381	11658	6.113	18888	27.843	11658	10.565	4275
48	33.523	12858	4.465	18488	2.352	18825	19.354	11758	7.898	8358	10.479	11575	6.277	18825	27.222	11858	9.883	4275
49	34.981	11975	5.232	18225	2.276	18225	19.731	11858	7.937	5888	12.443	11325	5.366	18675	27.967	11925	18.525	4888
52	38.888	13988	5.242	11125	4.215	14888	28.264	11475	9.349	5588	15.687	11258	5.278	5158	25.475	11475	3.872	5388
53	36.257	13875	5.641	11825	3.328	13375	23.246	11688	7.927	13288	15.396	11225	5.263	5688	24.385	13575	1.625	5388
54	79.223	13125	4.251	13125	4.447	11975	21.229	12258	16.264	13258	18.482	12175	11.742	12258	21.815	11858	6.416	18188
55	41.233	11925	5.542	18488	3.538	4988	15.169	18988	11.412	12188	9.871	18858	9.189	5325	21.241	11825	17.582	13858
56	42.138	18925	5.669	18888	3.898	5825	13.398	18925	18.328	11925	10.784	18958	8.651	5625	23.683	18925	16.283	13925
57	43.659	12475	5.161	11125	4.888	11188	17.727	11375	18.448	13925	14.438	11158	15.253	11288	22.737	18788	13.897	13888
59	37.888	11325	4.834	9225	3.887	4158	18.282	18175	12.936	12458	12.953	18888	9.647	12475	26.575	12158	15.534	13825
60	43.235	11775	3.926	11788	5.488	12958	18.999	12125	14.238	13325	9.945	11888	8.641	12175	28.987	12288	16.163	7388
61	36.272	14888	3.446	11325	4.447	11975	21.229	12258	16.264	13258	18.482	12175	11.742	12258	21.815	11858	6.416	18188
62	54.478	13888	3.881	13888	2.641	13888	13.641	18425	8.779	14888	11.524	12158	5.219	14888	28.879	9488	7.537	13888
64	53.218	14888	4.071	11925	4.444	11925	14.196	7575	9.196	18225	18.625	13488	8.695	13258	17.612	9725	8.288	11525
66	56.586	12958	3.884	12388	4.988	14888	11.119	6288	13.726	14888	7.945	5688	8.486	13875	19.215	9888	12.188	13875
67	57.518	13125	3.888	12788	4.368	13575	13.178	6108	11.792	14888	8.297	5225	8.758	13775	28.936	8275	7.221	13858
68	54.338	12725	3.971	12458	2.939	13888	18.865	5575	8.289	14888	7.642	12725	5.244	13825	15.718	9358	8.888	13858
69	55.524	12475	4.473	12458	4.551	13888	12.183	12475	9.978	5588	8.434	12475	4.817	5588	17.424	9675	6.288	11858
70	56.215	12725	4.243	12388	3.328	13975	17.869	4788	7.885	11875	9.865	12488	4.587	13888	17.182	6358	8.888	11858
72	79.223	13125	5.789	13775	8.143	13475	24.141	11775	26.134	13788	13.189	11875	5.619	13758	38.281	18375	28.877	13888
73	74.181	12588	4.243	11125	8.595	12625	19.515	4558	25.892	13275	12.172	12658	15.434	12625	31.245	5858	15.853	13825
75	66.843	12175	5.388	12875	3.299	12475	16.589	12125	17.847	12888	11.615	7275	9.571	11588	31.294	4658	13.817	13925
76	61.894	14888	7.488	13358	6.561	11925	22.896	13358	23.957	12875	14.771	13825	11.588	12725	38.122	5675	22.477	13425
77	69.778	11725	8.848	13788	6.888	12758	19.412	13525	38.484	12758	11.655	6588	15.351	12288	36.238	11725	22.877	14888
80	61.913	13888	9.287	13875	4.285	12825	21.222	13558	24.687	13425	15.629	13925	12.748	12825	27.851	5125	21.172	13425
81	61.798	11458	7.539	13925	3.511	12675	13.794	5188	15.164	13675	13.195	14888	7.988	13175	28.839	5475	3.887	9775
82	68.313	13375	3.781	4325	3.752	13888	16.691	5875	15.727	13888	18.446	5275	8.374	13875	38.573	5275	12.442	13888
84	57.511	12775	4.298	11975	5.215	13975	17.855	4888	9.729	7888	9.899	12388	7.824	13775	32.833	5358	18.872	8957
85	54.222	12825	4.288	12875	4.878	12188	14.782	4888	15.788	13175	18.118	5688	9.448	13788	26.568	4858	15.574	13858
86	54.458	11158	4.382	14858	4.979	13488	18.437	4275	16.274	13225	7.465	13958	11.324	13788	16.982	4888	21.398	12958
87	49.851	18958	4.655	13225	5.818	12925	12.192	18858	9.234	12475	6.017	13888	6.716	12925	28.865	4658	15.878	12925
88	52.895	12775	5.627	12558	5.234	12458	13.435	5888	15.943	14888	13.848	13988	14.874	13888	33.815	4975	8.839	13458
89	51.191	11775	3.233	11588	3.568	12525	16.393	6125	18.154	13875	9.887	5888	6.489	12675	21.933	4888	9.889	14888
90	48.935	12458	3.127	5888	4.542	13525	13.496	13725	12.525	13658	7.725	13188	8.748	13725	22.826	8158	14.887	4888
91	45.867	13888	4.886	12925	6.278	12758	22.987	6675	14.835	13875	13.885	6875	16.328	12988	31.545	6758	11.538	11275
92</																		

APPENDIX II
COMPARISON OF CHARACTERISTICS OF 900 WIND PROFILES

Each 10 X 10 table in this Appendix gives the number of profiles which fell into the indicated deciles with respect to two critical (selection) or test (verification) characteristics. Thus, the upper left entry in the first table shows that in 32 of the 900 profiles both the maximum wind speed and the largest 100-meter positive shear were in the lowest deciles. The upper right figure indicates that 3 profiles in which the maximum wind speed was in the highest decile had no appreciable 100-meter positive shears, because the maximum such shears were in the lowest decile.

*100M S		MAX. WIND									
DEC.	DEC.1	DEC.2	DEC.3	DEC.4	DEC.5	DEC.6	DEC.7	DEC.8	DEC.9	DEC.10	
1	12	16	13	6	4	3	4	5	4	3	
2	28	14	18	11	4	5	4	5	3	6	
3	9	14	16	9	9	9	10	5	3	6	
4	9	12	14	9	11	4	7	8	10	6	
5	8	16	9	18	9	7	10	7	6	8	
6	4	11	9	13	9	11	10	7	12	4	
7	8	5	8	15	13	13	6	9	11	12	
8	3	4	12	10	14	12	7	16	9	6	
9	8	4	3	6	11	15	14	13	14	16	
10	0	0	0	1	6	4	16	15	10	25	

*100M S		MAX. WIND									
DEC.	DEC.1	DEC.2	DEC.3	DEC.4	DEC.5	DEC.6	DEC.7	DEC.8	DEC.9	DEC.10	
1	28	16	16	5	7	7	7	8	2	2	
2	19	19	14	13	8	4	7	3	2	1	
3	13	12	9	11	16	7	6	8	6	2	
4	7	13	9	12	12	14	4	10	3	8	
5	7	16	12	9	11	7	4	6	9	9	
6	8	5	9	13	8	10	16	13	7	1	
7	6	7	8	11	8	11	8	11	7	13	
8	5	2	7	4	6	17	13	10	11	8	
9	2	4	3	8	9	6	4	14	18	21	
10	8	0	3	4	3	7	14	7	25	27	

*100M S		MAX. WIND									
DEC.	DEC.1	DEC.2	DEC.3	DEC.4	DEC.5	DEC.6	DEC.7	DEC.8	DEC.9	DEC.10	
1	18	23	18	4	6	5	2	1	1	0	
2	23	20	16	11	4	6	4	1	0	0	
3	13	12	16	10	11	9	6	5	4	1	
4	9	12	11	12	16	12	4	5	2	2	
5	6	14	10	9	11	14	9	8	7	6	
6	1	2	4	15	9	13	16	5	7	11	
7	0	3	5	11	12	13	15	15	10	6	
8	0	1	10	10	12	15	5	13	13	11	
9	0	2	3	7	8	7	13	21	24	13	
10	0	1	0	3	1	2	6	10	22	35	

*100M S		MAX. WIND									
DEC.	DEC.1	DEC.2	DEC.3	DEC.4	DEC.5	DEC.6	DEC.7	DEC.8	DEC.9	DEC.10	
1	19	10	12	4	13	2	6	6	2	8	
2	8	14	12	11	11	15	7	4	1	2	
3	17	10	12	11	11	7	4	4	5	4	
4	9	12	16	12	6	7	6	10	10	2	
5	13	5	10	13	13	4	6	7	7	2	
6	7	4	0	11	9	7	11	12	4	6	
7	8	4	7	6	12	6	17	7	11	5	
8	4	4	4	10	4	14	13	12	13	12	
9	2	3	5	6	6	10	10	14	15	19	
10	3	1	3	3	3	8	8	4	19	33	

*400M S		MAX. WIND									
DEC.	DEC.1	DEC.2	DEC.3	DEC.4	DEC.5	DEC.6	DEC.7	DEC.8	DEC.9	DEC.10	
1	14	26	9	5	4	5	2	2	1	1	
2	24	14	14	7	5	7	4	3	3	4	
3	12	13	17	9	14	3	6	8	3	5	
4	4	6	11	12	12	11	16	7	4	5	
5	9	11	7	10	11	7	11	11	5	8	
6	2	7	11	14	9	11	6	13	9	4	
7	0	3	6	13	12	13	13	9	13	10	
8	0	3	13	13	13	12	10	12	11	3	
9	8	2	2	7	8	16	17	12	14	14	
10	0	0	8	4	2	4	11	15	22	32	

*400M S		MAX. WIND									
DEC.	DEC.1	DEC.2	DEC.3	DEC.4	DEC.5	DEC.6	DEC.7	DEC.8	DEC.9	DEC.10	
1	23	14	13	11	11	8	3	1	1	1	
2	15	16	17	10	9	16	3	6	3	1	
3	12	14	6	15	9	4	4	9	5	7	
4	10	7	11	16	12	10	9	6	9	6	
5	8	6	15	14	7	8	4	10	7	8	
6	11	8	9	7	8	12	12	10	7	6	
7	4	6	8	4	8	9	10	4	10	7	
8	4	2	3	14	11	9	8	14	17	8	
9	3	6	5	1	6	8	15	16	16	14	
10	0	2	3	3	4	7	9	9	15	33	

*300M S		MAX. WIND									
DEC.	DEC.1	DEC.2	DEC.3	DEC.4	DEC.5	DEC.6	DEC.7	DEC.8	DEC.9	DEC.10	
1	46	25	15	4	3	8	8	8	8	8	
2	26	22	20	7	3	5	2	4	3	8	
3	12	20	23	13	9	5	3	2	3	8	
4	2	16	13	23	17	14	8	2	1	9	
5	2	6	13	18	11	12	12	14	5	1	
6	0	1	4	11	17	16	13	10	8	2	
7	0	0	2	6	19	16	10	19	6	2	
8	0	0	2	7	9	13	10	14	16	13	
9	0	0	0	1	4	11	11	17	21	25	
10	0	0	0	0	1	2	5	10	27	47	

*300M S		MAX. WIND									
DEC.	DEC.1	DEC.2	DEC.3	DEC.4	DEC.5	DEC.6	DEC.7	DEC.8	DEC.9	DEC.10	
1	1	6	14	21	17	5	14	5	6	1	
2	2	10	11	9	17	15	7	16	4	1	
3	1	15	14	14	9	9	11	8	6	3	
4	1	13	11	11	16	10	4	11	5	8	
5	6	9	6	14	11	14	12	10	7	5	
6	15	7	8	8	5	13	9	10	6	9	
7	17	15	7	5	4	4	8	7	20	3	
8	16	7	11	2	6	7	7	14	10	14	
9	17	5	5	4	5	4	8	7	14	16	
10	16	3	3	6	6	4	5	6	11	30	

APPENDIX II (Cont.)

<p style="text-align: center;">-1800 S</p> <p>+1800 S DEC. DEC.1 DEC.2 DEC.3 DEC.4 DEC.5 DEC.6 DEC.7 DEC.8 DEC.9 DEC.10</p> <p>1 27 22 13 6 7 5 3 3 2 2</p> <p>2 22 16 14 9 7 9 9 3 8 1</p> <p>3 18 13 12 12 11 14 9 3 2 4</p> <p>4 11 4 18 9 14 7 11 14 5 5</p> <p>5 6 14 14 11 11 8 3 9 11 3</p> <p>6 4 18 6 12 9 8 11 12 8 8</p> <p>7 4 6 3 8 8 8 12 15 7 19</p> <p>8 1 2 9 18 8 12 17 11 11 9</p> <p>9 3 2 2 8 9 18 8 11 19 18</p> <p>10 2 1 5 5 6 9 7 9 25 21</p>	<p style="text-align: center;">-1800 S</p> <p>-1800 S DEC. DEC.1 DEC.2 DEC.3 DEC.4 DEC.5 DEC.6 DEC.7 DEC.8 DEC.9 DEC.10</p> <p>1 12 18 14 11 7 6 2 8 8 8</p> <p>2 22 18 11 12 14 4 5 3 1 8</p> <p>3 18 13 14 18 11 9 18 3 2 8</p> <p>4 5 13 9 9 11 19 8 18 5 1</p> <p>5 18 13 11 9 12 8 8 18 9 8</p> <p>6 3 6 11 9 9 12 11 11 11 7</p> <p>7 4 3 6 6 11 18 13 16 18 11</p> <p>8 1 5 6 9 4 11 12 16 12 14</p> <p>9 2 2 2 3 5 8 13 13 21 23</p> <p>10 1 1 6 4 6 3 8 8 19 34</p>
<p style="text-align: center;">-1800 S</p> <p>+1800 S DEC. DEC.1 DEC.2 DEC.3 DEC.4 DEC.5 DEC.6 DEC.7 DEC.8 DEC.9 DEC.10</p> <p>1 33 22 11 5 5 2 5 4 3 7</p> <p>2 25 28 9 9 8 8 4 1 4 7</p> <p>3 18 12 16 16 9 18 5 5 5 2</p> <p>4 8 13 8 11 16 8 9 5 7 3</p> <p>5 7 9 13 8 13 18 8 13 6 3</p> <p>6 3 3 16 8 18 15 8 9 12 6</p> <p>7 2 4 5 18 7 8 14 9 15 16</p> <p>8 1 5 5 18 18 13 11 16 8 11</p> <p>9 1 8 5 9 8 18 16 11 8 22</p> <p>10 8 2 2 6 4 6 18 17 28 23</p>	<p style="text-align: center;">-1800 S</p> <p>-1800 S DEC. DEC.1 DEC.2 DEC.3 DEC.4 DEC.5 DEC.6 DEC.7 DEC.8 DEC.9 DEC.10</p> <p>1 43 29 14 6 2 8 8 8 8 8</p> <p>2 28 23 24 7 18 5 8 1 8 8</p> <p>3 8 15 15 22 16 8 6 8 8 7</p> <p>4 5 9 16 13 16 14 18 7 8 8</p> <p>5 8 9 5 18 18 16 13 9 2 7</p> <p>6 8 5 6 9 11 15 17 16 15 8</p> <p>7 4 3 5 5 6 12 14 15 16 9</p> <p>8 2 1 2 3 18 12 12 17 28 11</p> <p>9 8 8 1 3 5 7 11 14 22 27</p> <p>10 8 8 2 3 4 3 7 11 17 43</p>
<p style="text-align: center;">-1800 S</p> <p>+3000 S DEC. DEC.1 DEC.2 DEC.3 DEC.4 DEC.5 DEC.6 DEC.7 DEC.8 DEC.9 DEC.10</p> <p>1 32 19 9 6 7 6 3 5 2 1</p> <p>2 15 17 19 17 16 3 6 4 1 1</p> <p>3 18 15 17 9 7 7 7 7 7 7</p> <p>4 18 7 14 12 5 9 18 7 8 7</p> <p>5 18 14 7 13 8 12 9 5 6 6</p> <p>6 4 5 18 6 13 18 15 11 18 6</p> <p>7 4 4 8 8 8 18 7 17 13 13</p> <p>8 1 3 7 8 17 15 10 9 9 13</p> <p>9 2 3 4 7 6 6 18 11 18 21</p> <p>10 2 3 4 6 5 7 13 14 16 28</p>	<p style="text-align: center;">-1800 S</p> <p>-3000 S DEC. DEC.1 DEC.2 DEC.3 DEC.4 DEC.5 DEC.6 DEC.7 DEC.8 DEC.9 DEC.10</p> <p>1 5 17 15 16 17 9 3 4 3 1</p> <p>2 5 17 13 6 12 14 12 6 2 3</p> <p>3 11 4 18 15 9 13 12 7 4 3</p> <p>4 13 7 6 8 7 11 9 14 11 4</p> <p>5 8 12 9 15 5 3 15 9 7 7</p> <p>6 9 18 7 8 13 7 8 14 8 8</p> <p>7 7 4 9 6 11 9 8 13 8 15</p> <p>8 18 6 9 5 6 6 6 12 15 13</p> <p>9 11 7 5 5 6 8 5 18 14 19</p> <p>10 11 6 7 8 4 18 18 5 12 17</p>
	<p style="text-align: center;">-1800 S</p> <p>-3000 S DEC. DEC.1 DEC.2 DEC.3 DEC.4 DEC.5 DEC.6 DEC.7 DEC.8 DEC.9 DEC.10</p> <p>1 1 17 18 24 17 5 3 7 3 9</p> <p>2 4 28 14 8 15 9 16 7 2 7</p> <p>3 6 6 8 7 13 18 14 16 3 3</p> <p>4 18 18 18 17 6 14 18 12 8 2</p> <p>5 19 5 18 6 11 5 7 8 9 9</p> <p>6 13 7 8 5 4 11 14 11 9 8</p> <p>7 12 7 6 6 8 6 12 9 11 15</p> <p>8 11 7 7 11 3 8 5 8 14 14</p> <p>9 9 9 3 7 4 9 9 9 15 18</p> <p>10 7 2 6 2 9 7 6 11 16 24</p>

APPENDIX II (Cont.)

	<p style="text-align: center;">+10000 S</p> <p>-10000 S DEC. DEC.1 DEC.2 DEC.3 DEC.4 DEC.5 DEC.6 DEC.7 DEC.8 DEC.9 DEC.10</p> <table border="1"> <tr><td>1</td><td>26</td><td>18</td><td>18</td><td>9</td><td>7</td><td>4</td><td>5</td><td>3</td><td>8</td><td>8</td></tr> <tr><td>2</td><td>16</td><td>19</td><td>12</td><td>12</td><td>12</td><td>5</td><td>8</td><td>5</td><td>1</td><td>8</td></tr> <tr><td>3</td><td>13</td><td>18</td><td>4</td><td>19</td><td>21</td><td>15</td><td>5</td><td>4</td><td>2</td><td>1</td></tr> <tr><td>4</td><td>6</td><td>12</td><td>18</td><td>9</td><td>11</td><td>18</td><td>12</td><td>12</td><td>4</td><td>4</td></tr> <tr><td>5</td><td>5</td><td>18</td><td>14</td><td>7</td><td>12</td><td>18</td><td>11</td><td>12</td><td>6</td><td>3</td></tr> <tr><td>6</td><td>6</td><td>18</td><td>14</td><td>7</td><td>7</td><td>6</td><td>12</td><td>12</td><td>11</td><td>5</td></tr> <tr><td>7</td><td>5</td><td>6</td><td>6</td><td>18</td><td>8</td><td>9</td><td>15</td><td>7</td><td>17</td><td>7</td></tr> <tr><td>8</td><td>6</td><td>1</td><td>2</td><td>6</td><td>6</td><td>16</td><td>8</td><td>12</td><td>18</td><td>15</td></tr> <tr><td>9</td><td>3</td><td>1</td><td>3</td><td>6</td><td>5</td><td>18</td><td>18</td><td>18</td><td>17</td><td>25</td></tr> <tr><td>10</td><td>4</td><td>3</td><td>7</td><td>9</td><td>1</td><td>5</td><td>4</td><td>13</td><td>14</td><td>38</td></tr> </table>	1	26	18	18	9	7	4	5	3	8	8	2	16	19	12	12	12	5	8	5	1	8	3	13	18	4	19	21	15	5	4	2	1	4	6	12	18	9	11	18	12	12	4	4	5	5	18	14	7	12	18	11	12	6	3	6	6	18	14	7	7	6	12	12	11	5	7	5	6	6	18	8	9	15	7	17	7	8	6	1	2	6	6	16	8	12	18	15	9	3	1	3	6	5	18	18	18	17	25	10	4	3	7	9	1	5	4	13	14	38																																																																																																														
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<p style="text-align: center;">-4000 S</p> <p>+3000 S DEC. DEC.1 DEC.2 DEC.3 DEC.4 DEC.5 DEC.6 DEC.7 DEC.8 DEC.9 DEC.10</p> <table border="1"> <tr><td>1</td><td>29</td><td>12</td><td>9</td><td>5</td><td>11</td><td>7</td><td>8</td><td>4</td><td>1</td><td>1</td></tr> <tr><td>2</td><td>12</td><td>19</td><td>8</td><td>12</td><td>11</td><td>2</td><td>4</td><td>6</td><td>4</td><td>3</td></tr> <tr><td>3</td><td>14</td><td>12</td><td>12</td><td>11</td><td>9</td><td>6</td><td>6</td><td>6</td><td>18</td><td>2</td></tr> <tr><td>4</td><td>8</td><td>16</td><td>18</td><td>14</td><td>9</td><td>9</td><td>6</td><td>6</td><td>3</td><td>3</td></tr> <tr><td>5</td><td>3</td><td>9</td><td>14</td><td>9</td><td>14</td><td>14</td><td>7</td><td>9</td><td>6</td><td>6</td></tr> <tr><td>6</td><td>18</td><td>7</td><td>18</td><td>8</td><td>8</td><td>14</td><td>8</td><td>18</td><td>6</td><td>9</td></tr> <tr><td>7</td><td>8</td><td>5</td><td>5</td><td>7</td><td>16</td><td>13</td><td>13</td><td>12</td><td>7</td><td>9</td></tr> <tr><td>8</td><td>2</td><td>1</td><td>11</td><td>13</td><td>3</td><td>11</td><td>10</td><td>7</td><td>13</td><td>13</td></tr> <tr><td>9</td><td>2</td><td>5</td><td>4</td><td>6</td><td>7</td><td>7</td><td>8</td><td>19</td><td>15</td><td>17</td></tr> <tr><td>10</td><td>8</td><td>4</td><td>4</td><td>5</td><td>2</td><td>5</td><td>13</td><td>13</td><td>19</td><td>27</td></tr> </table>	1	29	12	9	5	11	7	8	4	1	1	2	12	19	8	12	11	2	4	6	4	3	3	14	12	12	11	9	6	6	6	18	2	4	8	16	18	14	9	9	6	6	3	3	5	3	9	14	9	14	14	7	9	6	6	6	18	7	18	8	8	14	8	18	6	9	7	8	5	5	7	16	13	13	12	7	9	8	2	1	11	13	3	11	10	7	13	13	9	2	5	4	6	7	7	8	19	15	17	10	8	4	4	5	2	5	13	13	19	27	<p style="text-align: center;">-4000 S</p> <p>-3000 S DEC. DEC.1 DEC.2 DEC.3 DEC.4 DEC.5 DEC.6 DEC.7 DEC.8 DEC.9 DEC.10</p> <table border="1"> <tr><td>1</td><td>18</td><td>16</td><td>28</td><td>17</td><td>11</td><td>7</td><td>5</td><td>5</td><td>8</td><td>1</td></tr> <tr><td>2</td><td>9</td><td>13</td><td>11</td><td>11</td><td>13</td><td>18</td><td>13</td><td>1</td><td>6</td><td>3</td></tr> <tr><td>3</td><td>9</td><td>16</td><td>4</td><td>18</td><td>12</td><td>14</td><td>8</td><td>15</td><td>1</td><td>1</td></tr> <tr><td>4</td><td>7</td><td>7</td><td>11</td><td>13</td><td>13</td><td>12</td><td>8</td><td>5</td><td>4</td><td>4</td></tr> <tr><td>5</td><td>17</td><td>5</td><td>9</td><td>8</td><td>7</td><td>7</td><td>18</td><td>11</td><td>12</td><td>3</td></tr> <tr><td>6</td><td>7</td><td>6</td><td>7</td><td>11</td><td>11</td><td>13</td><td>8</td><td>18</td><td>11</td><td>8</td></tr> <tr><td>7</td><td>12</td><td>12</td><td>7</td><td>5</td><td>1</td><td>5</td><td>18</td><td>8</td><td>15</td><td>15</td></tr> <tr><td>8</td><td>4</td><td>7</td><td>18</td><td>5</td><td>14</td><td>5</td><td>14</td><td>12</td><td>12</td><td>11</td></tr> <tr><td>9</td><td>14</td><td>5</td><td>6</td><td>2</td><td>5</td><td>7</td><td>7</td><td>11</td><td>14</td><td>19</td></tr> <tr><td>10</td><td>3</td><td>2</td><td>5</td><td>8</td><td>7</td><td>18</td><td>5</td><td>9</td><td>14</td><td>27</td></tr> </table>	1	18	16	28	17	11	7	5	5	8	1	2	9	13	11	11	13	18	13	1	6	3	3	9	16	4	18	12	14	8	15	1	1	4	7	7	11	13	13	12	8	5	4	4	5	17	5	9	8	7	7	18	11	12	3	6	7	6	7	11	11	13	8	18	11	8	7	12	12	7	5	1	5	18	8	15	15	8	4	7	18	5	14	5	14	12	12	11	9	14	5	6	2	5	7	7	11	14	19	10	3	2	5	8	7	18	5	9	14	27
1	29	12	9	5	11	7	8	4	1	1																																																																																																																																																																																																																			
2	12	19	8	12	11	2	4	6	4	3																																																																																																																																																																																																																			
3	14	12	12	11	9	6	6	6	18	2																																																																																																																																																																																																																			
4	8	16	18	14	9	9	6	6	3	3																																																																																																																																																																																																																			
5	3	9	14	9	14	14	7	9	6	6																																																																																																																																																																																																																			
6	18	7	18	8	8	14	8	18	6	9																																																																																																																																																																																																																			
7	8	5	5	7	16	13	13	12	7	9																																																																																																																																																																																																																			
8	2	1	11	13	3	11	10	7	13	13																																																																																																																																																																																																																			
9	2	5	4	6	7	7	8	19	15	17																																																																																																																																																																																																																			
10	8	4	4	5	2	5	13	13	19	27																																																																																																																																																																																																																			
1	18	16	28	17	11	7	5	5	8	1																																																																																																																																																																																																																			
2	9	13	11	11	13	18	13	1	6	3																																																																																																																																																																																																																			
3	9	16	4	18	12	14	8	15	1	1																																																																																																																																																																																																																			
4	7	7	11	13	13	12	8	5	4	4																																																																																																																																																																																																																			
5	17	5	9	8	7	7	18	11	12	3																																																																																																																																																																																																																			
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7	12	12	7	5	1	5	18	8	15	15																																																																																																																																																																																																																			
8	4	7	18	5	14	5	14	12	12	11																																																																																																																																																																																																																			
9	14	5	6	2	5	7	7	11	14	19																																																																																																																																																																																																																			
10	3	2	5	8	7	18	5	9	14	27																																																																																																																																																																																																																			

APPENDIX II (Cont.)

-1400H S											-1400H S												
*400H S	DEC.	DEC.1	DEC.2	DEC.3	DEC.4	DEC.5	DEC.6	DEC.7	DEC.8	DEC.9	DEC.10	*400H S	DEC.	DEC.1	DEC.2	DEC.3	DEC.4	DEC.5	DEC.6	DEC.7	DEC.8	DEC.9	DEC.10
1	16	18	9	5	12	4	5	5	2	2		1	43	26	13	5	4	2	2	8	1	0	
2	21	15	11	10	11	7	7	4	3	1		2	24	27	13	9	6	4	3	2	8	2	
3	17	5	18	13	3	11	6	7	6	4		3	12	18	16	18	18	7	3	4	2	7	
4	9	11	16	16	4	7	5	7	18	7		4	9	14	12	17	17	10	5	5	2	0	
5	8	12	14	6	11	5	13	16	4	2		5	2	7	17	11	11	12	17	6	5	7	
6	5	5	15	9	7	10	2	8	9	8		6	2	4	3	12	16	17	7	7	2	4	
7	3	8	5	16	11	12	12	8	8	6		7	1	17	5	11	17	16	17	16	9	1	
8	1	6	9	2	13	11	5	9	14	9		8	1	1	1	6	9	12	15	18	21	4	
9	8	8	1	9	7	12	14	13	11	18		9	1	1	1	1	7	9	18	21	26	11	
10	3	3	2	3	2	3	11	18	14	32		10	8	6	4	8	8	1	1	18	18	64	

-1200H S											-1200H S												
*300H S	DEC.	DEC.1	DEC.2	DEC.3	DEC.4	DEC.5	DEC.6	DEC.7	DEC.8	DEC.9	DEC.10	*300H S	DEC.	DEC.1	DEC.2	DEC.3	DEC.4	DEC.5	DEC.6	DEC.7	DEC.8	DEC.9	DEC.10
1	21	19	8	5	11	7	6	7	3	2		1	14	29	17	15	7	7	1	1	2	1	
2	25	15	7	12	9	7	7	5	4	0		2	8	9	15	24	11	9	16	6	1	2	
3	14	11	13	12	11	4	7	5	5	3		3	2	12	12	4	19	12	9	8	1	1	
4	9	5	11	15	11	8	7	4	9	7		4	7	12	11	11	14	11	17	12	2	4	
5	6	13	8	12	12	9	5	5	6	7		5	9	17	3	12	9	16	17	14	6	7	
6	6	7	18	5	5	14	10	18	7	12		6	6	6	6	5	14	11	4	16	11	1	
7	5	8	7	5	10	14	16	12	9	7		7	14	4	9	8	6	11	7	16	6	1	
8	4	4	18	9	5	14	14	10	4	11		8	1	1	1	5	7	16	11	11	17	13	
9	8	7	3	7	8	6	13	12	14	27		9	7	5	5	7	7	3	11	5	16	24	
10	7	1	3	1	1	3	14	12	23	27		10	1	1	1	1	1	3	16	16	16	16	

-1400H S											-1400H S												
*400H S	DEC.	DEC.1	DEC.2	DEC.3	DEC.4	DEC.5	DEC.6	DEC.7	DEC.8	DEC.9	DEC.10	*400H S	DEC.	DEC.1	DEC.2	DEC.3	DEC.4	DEC.5	DEC.6	DEC.7	DEC.8	DEC.9	DEC.10
1	12	12	12	12	12	12	12	12	12	12		1	12	12	12	12	12	12	12	12	12	12	
2	11	10	10	10	10	10	10	10	10	10		2	11	10	10	10	10	10	10	10	10	10	
3	10	10	10	10	10	10	10	10	10	10		3	10	10	10	10	10	10	10	10	10	10	
4	9	9	9	9	9	9	9	9	9	9		4	9	9	9	9	9	9	9	9	9	9	
5	8	8	8	8	8	8	8	8	8	8		5	8	8	8	8	8	8	8	8	8	8	
6	7	7	7	7	7	7	7	7	7	7		6	7	7	7	7	7	7	7	7	7	7	
7	6	6	6	6	6	6	6	6	6	6		7	6	6	6	6	6	6	6	6	6	6	
8	5	5	5	5	5	5	5	5	5	5		8	5	5	5	5	5	5	5	5	5	5	
9	4	4	4	4	4	4	4	4	4	4		9	4	4	4	4	4	4	4	4	4	4	
10	3	3	3	3	3	3	3	3	3	3		10	3	3	3	3	3	3	3	3	3	3	

-1200H S											-1200H S												
*300H S	DEC.	DEC.1	DEC.2	DEC.3	DEC.4	DEC.5	DEC.6	DEC.7	DEC.8	DEC.9	DEC.10	*300H S	DEC.	DEC.1	DEC.2	DEC.3	DEC.4	DEC.5	DEC.6	DEC.7	DEC.8	DEC.9	DEC.10
1	44	22	17	6	7	2	8	1	8	4		1	2	14	21	19	11	3	4	7	2		
2	21	22	12	9	11	4	1	1	1	0		2	5	11	9	13	12	14	14	7	9	0	
3	12	12	13	13	5	12	9	6	2	7		3	10	12	11	8	5	11	9	6	2		
4	6	7	11	12	12	12	16	21	4	7		4	9	9	13	7	5	15	14	11	5		
5	3	7	12	14	11	11	16	11	1	7		5	8	12	13	6	12	7	11	12	7		
6	2	11	9	14	9	14	11	14	11	4		6	12	6	5	7	11	8	14	3	14	15	
7	8	4	11	11	11	12	12	12	12	4		7	14	11	4	6	9	6	9	18	11	12	
8	2	4	5	7	6	14	11	7	28	16		8	13	5	9	5	12	7	6	8	13	6	
9	2	4	3	3	6	6	11	15	14	17		9	18	3	5	5	5	11	9	12	8	14	
10	2	2	5	1	4	5	8	11	19	33		10	6	8	1	5	6	4	14	11	15	23	

APPENDIX III

NUMBER OF ENTRIES PER DECILE CELL FROM 5 RANDOM SEQUENCES

RAND SEQ	DECILE:	At least $n = 1$										At most $n = 1$									
		1	2	3	4	5	6	7	8	9	10	1	2	3	4	5	6	7	8	9	10
1	MAX WIND SPEED	3	1	1	2	4	4	1	1	4	2	1	1	1	0	1	1	1	0	1	1
	100m SHEAR POS	3	5	1	2	1	2	2	1	4	2	1	0	1	0	1	1	1	1	1	1
	100m SHEAR NEG	3	1	1	1	2	1	2	5	3	4	1	1	1	1	1	0	0	1	1	1
	1 km SHEAR POS	3	1	1	2	1	4	4	3	2	2	1	1	1	0	1	1	0	1	1	1
	1 km SHEAR NEG	1	1	1	4	5	3	2	3	1	2	1	0	0	1	1	1	1	1	1	1
	400m SHEAR POS	3	2	1	3	1	2	3	3	2	3	0	2	0	1	1	0	0	2	0	2
	400m SHEAR NEG	2	1	2	1	0	5	1	2	4	5	0	0	2	1	0	1	0	1	1	2
	3 km SHEAR POS	2	4	1	4	4	1	0	2	1	4	0	2	1	2	0	0	0	1	0	2
	3 km SHEAR NEG	2	0	1	4	3	4	3	3	3	0	1	1	0	0	0	0	1	2	2	1
	2	MAX WIND SPEED	3	3	2	3	1	1	1	1	1	5	0	1	1	0	1	1	1	1	1
100m SHEAR POS		4	2	5	1	1	1	2	1	3	1	1	1	1	0	1	1	1	0	1	1
100m SHEAR NEG		1	2	3	3	1	2	1	2	5	1	0	0	1	1	1	1	1	1	1	1
1 km SHEAR POS		3	1	2	2	3	1	1	4	2	2	1	0	1	1	0	1	1	1	1	1
1 km SHEAR NEG		1	1	3	4	3	2	1	2	1	3	0	0	1	1	1	1	1	1	1	1
400m SHEAR POS		4	1	1	2	2	2	4	1	3	1	1	1	0	1	1	1	1	0	0	2
400m SHEAR NEG		1	2	2	3	2	2	3	3	1	2	0	0	0	1	2	0	2	3	0	0
3 km SHEAR POS		3	2	2	0	2	3	2	3	2	2	1	0	0	0	1	0	1	3	1	1
3 km SHEAR NEG		1	1	3	4	1	3	2	4	0	2	0	0	1	2	0	2	1	2	0	0
3		MAX WIND SPEED	1	2	2	2	4	3	1	1	3	2	0	1	1	0	1	1	1	1	1
	100m SHEAR POS	1	2	1	2	2	1	4	3	1	4	1	1	0	1	1	0	1	1	1	1
	100m SHEAR NEG	2	2	2	4	3	1	3	1	1	2	1	1	1	1	1	1	0	1	1	0
	1 km SHEAR POS	1	2	1	2	3	4	2	3	1	2	1	1	1	0	1	1	0	1	1	1
	1 km SHEAR NEG	1	2	2	2	2	1	2	3	5	1	1	0	1	1	0	1	1	1	1	1
	400m SHEAR POS	2	2	1	2	2	3	2	3	1	3	1	1	1	0	1	2	0	0	1	1
	400m SHEAR NEG	3	2	2	2	0	5	3	1	1	2	0	0	0	0	0	3	2	0	1	0
	3 km SHEAR POS	1	3	3	2	1	1	5	1	2	1	1	1	0	1	1	1	1	0	0	0
	3 km SHEAR NEG	0	2	3	0	0	4	3	4	3	2	0	1	1	0	0	1	1	1	1	2
	4	MAX WIND SPEED	1	3	1	2	3	1	1	5	1	1	1	1	0	1	1	0	1	1	1
100m SHEAR POS		1	1	3	1	4	2	1	2	3	1	1	1	1	0	1	1	0	1	1	1
100m SHEAR NEG		1	2	3	2	1	1	1	5	1	2	1	1	1	1	1	0	0	1	1	1
1 km SHEAR POS		2	2	4	1	2	1	3	2	1	1	1	1	1	0	0	1	1	1	1	1
1 km SHEAR NEG		1	2	1	2	3	5	1	1	1	2	1	0	1	0	1	1	1	1	1	1
400m SHEAR POS		2	2	2	2	3	0	3	0	2	3	1	1	0	1	1	0	1	0	1	2
400m SHEAR NEG		1	2	2	3	4	0	1	2	3	1	1	0	0	2	2	1	0	0	0	0
3 km SHEAR POS		2	1	3	3	3	3	2	0	1	1	1	1	1	2	1	0	0	0	1	1
3 km SHEAR NEG		4	0	1	3	1	5	3	1	1	0	2	0	0	2	1	1	2	0	0	0
5		MAX WIND SPEED	3	1	2	1	2	4	1	2	1	4	0	1	1	0	1	1	1	1	1
	100m SHEAR POS	1	6	2	1	1	3	1	2	2	2	1	1	1	1	1	1	0	1	1	0
	100m SHEAR NEG	4	3	2	1	3	2	1	2	2	1	1	1	1	0	1	1	1	1	1	0
	1 km SHEAR POS	2	2	2	4	2	2	2	2	1	2	1	1	0	1	1	1	1	0	1	1
	1 km SHEAR NEG	3	1	2	1	5	2	1	1	2	3	0	1	0	1	1	1	1	1	1	1
	400m SHEAR POS	2	2	3	2	4	2	2	1	1	2	1	1	0	2	1	0	1	1	1	0
	400m SHEAR NEG	3	2	2	4	1	4	0	2	1	2	1	1	1	0	1	2	0	1	0	1
	3 km SHEAR POS	4	1	1	3	2	2	4	1	0	3	1	1	0	0	0	2	2	1	0	1
	3 km SHEAR NEG	4	4	2	3	2	0	3	0	1	2	1	0	2	1	1	0	2	0	1	0

APPENDIX III (Cont.)

RAND SEQ	DECILE:	At least $m = 2$										At most: $m = 2$										
		1	2	3	4	5	6	7	8	9	10	1	2	3	4	5	6	7	8	9	10	
1	MAX WIND SPEED	6	2	2	2	4	6	3	4	6	2	2	2	1	0	2	2	2	2	2	2	2
	100m SHEAR POS	6	6	2	4	2	4	2	4	5	2	2	2	2	2	2	2	1	2	2	2	2
	100m SHEAR NEG	7	3	2	3	3	3	2	6	4	4	2	1	1	2	2	2	2	2	2	2	1
	1 km SHEAR POS	5	2	3	3	2	6	4	7	2	3	2	1	2	2	1	2	2	2	2	1	2
	1 km SHEAR NEG	5	3	2	5	5	3	2	6	2	3	2	1	1	2	2	2	2	2	2	1	2
	400m SHEAR POS	5	6	1	5	2	3	4	4	3	4	3	1	1	2	4	0	2	2	2	2	2
	400m SHEAR NEG	7	2	2	4	2	5	3	4	5	5	1	3	1	1	1	2	2	0	3	3	3
	3 km SHEAR POS	4	7	1	4	4	3	3	3	2	6	0	6	1	1	2	1	1	2	2	2	3
	3 km SHEAR NEG	2	4	5	5	4	5	3	3	5	1	2	0	2	0	1	1	4	2	5	0	0
	2	MAX WIND SPEED	5	4	6	4	5	2	3	4	2	5	2	2	2	1	2	1	2	1	2	2
100m SHEAR POS		6	4	6	3	4	2	3	2	5	5	2	2	2	2	1	0	2	2	2	2	2
100m SHEAR NEG		3	2	7	5	3	7	2	4	5	2	2	0	2	2	2	2	2	2	1	2	2
1 km SHEAR POS		5	3	2	5	5	3	4	6	3	3	2	2	1	2	2	1	1	2	2	2	2
1 km SHEAR NEG		3	3	5	6	5	4	4	4	3	3	2	0	2	2	2	2	2	2	2	2	1
400m SHEAR POS		6	3	1	5	3	5	7	2	4	4	3	2	2	2	2	1	1	1	3	2	2
400m SHEAR NEG		1	2	5	6	4	5	7	7	1	2	1	2	1	2	1	1	6	2	1	0	0
3 km SHEAR POS		4	5	4	2	5	5	4	4	3	3	2	2	1	0	2	1	1	2	4	2	2
3 km SHEAR NEG		2	2	4	8	3	5	7	5	1	3	1	0	2	4	0	5	1	3	1	0	0
3		MAX WIND SPEED	2	5	4	3	5	3	2	4	5	3	2	2	2	2	2	2	2	2	2	1
	100m SHEAR POS	2	2	3	3	5	2	5	6	2	6	2	2	1	2	2	2	2	2	2	2	2
	100m SHEAR NEG	5	2	3	5	4	4	4	5	2	2	2	2	2	2	2	1	2	2	2	2	2
	1 km SHEAR POS	3	2	3	4	5	5	4	5	3	2	2	2	2	2	2	2	1	2	2	2	2
	1 km SHEAR NEG	2	4	3	4	5	3	2	4	6	2	2	2	2	2	1	2	2	2	2	2	2
	400m SHEAR POS	2	5	2	4	3	4	5	4	2	4	3	1	1	1	2	3	4	2	1	1	1
	400m SHEAR NEG	4	4	3	3	2	8	3	5	1	3	4	2	2	0	1	3	2	3	1	3	3
	3 km SHEAR POS	2	6	5	3	1	2	7	3	5	2	2	3	3	2	1	1	2	2	1	2	2
	3 km SHEAR NEG	1	3	4	1	2	9	5	7	4	2	1	1	1	1	1	3	4	3	3	1	1
	4	MAX WIND SPEED	3	4	2	4	5	2	3	7	3	2	1	2	2	2	2	1	1	2	1	2
100m SHEAR POS		3	2	3	4	5	3	4	5	4	2	1	1	2	1	2	2	1	2	2	2	2
100m SHEAR NEG		3	3	4	3	2	2	4	7	5	2	0	2	2	2	1	2	1	2	2	2	2
1 km SHEAR POS		5	3	5	2	2	4	4	5	3	2	2	2	2	1	2	1	2	2	2	2	2
1 km SHEAR NEG		3	2	3	3	4	7	2	6	3	2	2	2	2	0	2	2	2	2	2	2	2
400m SHEAR POS		5	3	2	4	4	0	6	3	2	6	2	2	2	2	1	0	1	1	3	2	2
400m SHEAR NEG		2	2	3	4	7	2	3	4	7	1	2	2	1	2	3	2	2	2	3	1	1
3 km SHEAR POS		4	2	4	6	4	5	3	2	4	1	2	1	3	5	2	0	2	0	2	1	1
3 km SHEAR NEG		5	4	2	5	3	7	3	1	4	1	1	0	1	4	2	5	2	2	1	0	0
5		MAX WIND SPEED	3	2	2	2	3	6	2	4	4	5	1	2	1	0	2	2	2	2	2	2
	100m SHEAR POS	2	6	3	3	2	3	2	5	3	4	1	2	2	2	1	2	2	2	2	2	2
	100m SHEAR NEG	4	3	2	2	5	3	2	4	5	2	2	2	2	2	2	1	1	2	1	1	1
	1 km SHEAR POS	3	2	3	6	2	4	2	4	4	3	2	2	1	2	2	1	2	0	2	2	2
	1 km SHEAR NEG	3	2	5	2	5	2	3	2	3	6	2	1	1	2	2	2	2	2	2	2	2
	400m SHEAR POS	3	2	3	4	5	2	2	3	3	5	2	1	2	1	2	1	2	2	2	1	1
	400m SHEAR NEG	4	3	2	6	3	5	2	3	2	5	2	4	1	2	1	4	1	1	1	1	1
	3 km SHEAR POS	4	1	2	4	2	4	4	5	2	5	3	0	1	2	1	2	3	1	1	2	2
	3 km SHEAR NEG	6	5	3	3	2	1	5	1	4	3	2	2	1	2	1	2	3	0	3	2	2

APPENDIX III (Cont.)

RAND SEQ	DECILE:	At least $n = 3$										At most $n = 3$									
		1	2	3	4	5	6	7	8	9	10	1	2	3	4	5	6	7	8	9	10
1	MAX WIND SPEED	8	3	4	4	5	8	4	5	9	3	3	3	2	3	3	3	1	2	3	3
	100m SHEAR POS	8	8	4	5	4	4	5	5	5	4	3	3	3	1	3	2	2	3	3	3
	100m SHEAR NEG	8	4	3	3	5	5	5	8	5	5	3	3	2	3	3	3	3	3	3	3
	1 km SHEAR POS	5	4	8	5	3	6	4	10	3	4	3	3	1	3	2	3	3	3	2	3
	1 km SHEAR NEG	6	4	4	8	3	3	3	8	3	5	2	2	2	3	3	3	2	3	2	3
	400m SHEAR POS	5	9	3	8	5	3	6	5	4	4	3	4	2	3	3	0	1	2	5	3
	400m SHEAR NEG	9	3	2	5	3	7	5	5	6	7	2	3	2	3	2	2	1	2	4	5
	3 km SHEAR POS	4	9	3	7	7	3	4	6	2	7	2	5	1	5	3	1	2	2	2	5
	3 km SHEAR NEG	4	4	8	5	4	6	4	7	6	4	2	3	3	3	3	1	2	4	4	1
	2	MAX WIND SPEED	6	4	8	5	7	3	5	5	3	5	2	3	3	3	3	1	3	3	3
100m SHEAR POS		6	5	8	6	4	3	4	4	5	6	3	3	3	3	2	2	3	3	3	2
100m SHEAR NEG		3	3	9	6	5	8	3	6	5	3	2	1	3	3	3	3	3	3	3	3
1 km SHEAR POS		5	5	3	6	8	5	5	7	4	3	3	2	3	3	3	3	2	3	3	2
1 km SHEAR NEG		3	6	6	7	5	5	5	5	6	3	2	3	3	3	3	2	3	2	3	3
400m SHEAR POS		6	5	4	5	5	7	7	3	5	4	4	2	1	4	2	5	3	1	2	3
400m SHEAR NEG		1	4	6	7	5	7	9	7	2	2	2	3	3	3	2	1	5	6	7	2
3 km SHEAR POS		4	7	6	5	6	5	4	5	5	4	3	2	3	1	3	3	2	3	5	2
3 km SHEAR NEG		3	3	4	9	3	8	9	5	4	3	3	2	2	5	3	4	5	5	2	2
3		MAX WIND SPEED	4	5	5	4	5	5	5	7	5	3	2	3	3	3	3	3	3	3	3
	100m SHEAR POS	5	3	4	4	5	4	6	8	5	6	2	3	2	2	3	3	3	3	2	3
	100m SHEAR NEG	7	3	3	6	5	6	7	6	4	3	3	3	3	3	2	1	3	3	3	2
	1 km SHEAR POS	6	3	4	6	5	5	5	8	4	4	3	3	2	3	3	3	1	3	2	3
	1 km SHEAR NEG	4	5	5	4	9	3	7	4	6	3	3	2	2	3	3	1	3	3	3	3
	400m SHEAR POS	4	5	3	7	4	6	6	5	4	6	2	8	7	1	2	3	4	3	1	2
	400m SHEAR NEG	6	4	4	4	3	9	4	8	4	4	4	1	3	2	1	5	3	2	2	3
	3 km SHEAR POS	4	7	7	6	2	3	8	4	7	2	2	5	3	2	2	2	2	3	3	2
	3 km SHEAR NEG	4	5	7	1	7	12	6	8	4	3	7	4	1	1	7	4	5	5	4	2
	4	MAX WIND SPEED	4	6	3	5	5	3	5	9	5	4	2	3	3	3	3	2	3	3	1
100m SHEAR POS		4	3	5	4	5	5	5	6	8	5	2	2	3	3	3	3	2	3	3	2
100m SHEAR NEG		3	4	5	4	4	3	6	9	7	4	1	3	3	3	3	1	3	3	3	3
1 km SHEAR POS		6	4	5	7	4	4	6	5	4	4	3	3	3	3	3	2	3	3	3	3
1 km SHEAR NEG		4	5	5	5	5	9	3	7	4	3	3	2	3	1	3	3	3	3	2	3
400m SHEAR POS		6	5	4	6	4	1	8	5	4	7	3	3	3	1	2	2	4	3	4	3
400m SHEAR NEG		4	3	5	6	7	6	5	5	7	2	2	3	1	3	4	5	2	2	4	2
3 km SHEAR POS		6	3	5	7	4	7	7	2	6	3	4	2	2	5	4	2	2	3	3	2
3 km SHEAR NEG		8	4	2	8	5	9	6	2	5	1	3	1	1	5	2	6	4	1	3	2
5		MAX WIND SPEED	3	4	5	4	3	6	4	9	5	5	3	3	1	2	3	3	3	3	3
	100m SHEAR POS	4	7	5	4	3	6	3	6	4	6	3	3	3	2	1	3	3	3	3	3
	100m SHEAR NEG	7	5	4	4	5	4	3	6	6	3	3	3	3	3	3	3	2	3	3	1
	1 km SHEAR POS	6	3	5	6	4	5	3	6	4	6	3	3	1	3	3	3	3	3	2	3
	1 km SHEAR NEG	8	3	5	3	5	4	3	4	4	7	3	3	3	1	3	3	3	3	2	3
	400m SHEAR POS	5	5	4	7	7	2	3	4	4	7	2	3	2	2	5	2	3	2	2	4
	400m SHEAR NEG	7	5	5	8	5	5	1	3	3	7	3	3	2	4	3	4	1	2	2	3
	3 km SHEAR POS	6	3	2	5	4	6	4	8	5	5	4	2	2	2	2	2	4	5	1	3
	3 km SHEAR NEG	6	11	4	3	2	2	7	1	7	5	4	3	3	4	2	2	3	1	5	0

APPENDIX III (Cont.)

RAND SEQ	DECILE:	At least $m = 4$										At most: $m = 4$									
		1	2	3	4	5	6	7	8	9	10	1	2	3	4	5	6	7	8	9	10
1	MAX WIND SPEED	9	4	5	4	5	8	4	6	10	7	4	4	3	3	4	4	1	3	4	4
	100m SHEAR POS	9	9	4	6	5	5	7	6	8	4	4	4	4	0	4	4	3	4	4	3
	100m SHEAR NEG	8	6	5	5	5	6	7	9	6	6	4	4	1	4	4	2	3	4	4	4
	1 km SHEAR POS	6	5	11	6	4	6	5	11	4	6	4	4	2	4	2	4	4	4	2	4
	1 km SHEAR NEG	7	5	5	8	9	5	5	9	4	7	4	3	2	4	4	4	4	4	1	4
	400m SHEAR POS	6	9	4	10	5	3	9	5	8	4	4	4	3	4	3	0	4	4	5	3
	400m SHEAR NEG	10	3	4	6	5	9	6	6	7	8	4	3	3	2	3	5	2	2	3	7
	3 km SHEAR POS	5	9	3	11	8	3	5	7	4	9	3	7	2	6	4	1	1	4	1	5
	3 km SHEAR NEG	5	4	10	7	5	7	5	8	7	5	2	3	2	4	4	4	2	7	5	1
	2	MAX WIND SPEED	6	7	9	6	8	5	6	5	5	6	4	3	4	4	4	3	4	4	4
100m SHEAR POS		8	6	10	6	5	5	5	4	7	6	4	4	4	4	4	3	4	3	4	4
100m SHEAR NEG		5	4	10	9	5	8	4	6	7	4	3	3	4	4	4	4	4	4	4	4
1 km SHEAR POS		7	5	5	8	9	6	6	8	4	5	4	4	2	4	4	4	4	4	4	4
1 km SHEAR NEG		5	8	7	8	7	6	5	5	8	4	4	4	4	4	4	4	2	4	4	4
400m SHEAR POS		8	6	5	7	5	9	9	3	6	5	4	2	3	4	3	8	4	1	5	4
400m SHEAR NEG		4	7	7	8	7	8	9	8	3	2	2	4	5	4	4	3	5	8	3	3
3 km SHEAR POS		6	7	8	7	5	7	6	5	7	4	4	3	3	2	5	5	3	5	5	3
3 km SHEAR NEG		4	4	5	10	3	10	10	6	5	6	1	4	2	8	2	3	6	7	2	3
3		MAX WIND SPEED	4	6	8	4	7	6	5	7	6	6	3	4	4	4	4	4	4	4	4
	100m SHEAR POS	6	4	5	6	5	5	7	9	5	7	2	3	2	4	4	4	4	4	4	4
	100m SHEAR NEG	7	4	5	8	5	7	8	6	4	5	4	2	4	4	4	4	4	4	3	2
	1 km SHEAR POS	6	4	5	7	7	5	5	9	5	6	4	2	4	4	4	4	3	4	3	3
	1 km SHEAR NEG	4	7	5	4	11	4	8	4	7	4	3	4	4	4	4	3	4	4	4	1
	400m SHEAR POS	5	7	3	7	5	6	7	6	7	6	3	4	4	3	2	4	4	4	2	5
	400m SHEAR NEG	7	5	5	5	4	9	5	8	4	6	6	3	3	2	3	5	4	4	3	2
	3 km SHEAR POS	4	9	7	7	2	4	8	7	8	3	3	5	5	3	2	4	5	4	3	1
	3 km SHEAR NEG	4	6	9	2	8	13	6	10	4	5	2	4	4	2	1	6	4	6	4	2
	4	MAX WIND SPEED	6	6	4	11	5	4	7	9	5	6	3	4	2	4	4	2	4	4	4
100m SHEAR POS		6	4	5	7	5	6	5	6	10	8	4	1	4	3	4	4	4	4	4	3
100m SHEAR NEG		4	5	8	5	5	4	6	9	10	7	3	3	4	4	3	2	4	4	4	4
1 km SHEAR POS		7	5	7	10	7	4	8	6	6	4	4	4	4	4	4	1	4	4	2	4
1 km SHEAR NEG		4	6	7	6	7	11	5	7	7	4	4	4	4	2	4	4	2	4	4	3
400m SHEAR POS		8	6	5	7	5	2	13	5	5	8	6	1	4	4	3	0	6	2	5	4
400m SHEAR NEG		5	4	5	7	9	9	6	8	7	5	4	3	3	4	5	4	2	3	5	3
3 km SHEAR POS		7	6	7	9	5	8	8	2	8	4	5	3	2	5	4	4	2	1	5	4
3 km SHEAR NEG		8	6	3	10	7	10	9	2	7	2	4	3	1	7	2	7	4	3	3	1
5		MAX WIND SPEED	4	7	5	7	4	6	5	11	6	6	3	4	4	2	4	4	3	4	4
	100m SHEAR POS	4	8	9	5	4	8	4	7	5	7	4	4	4	3	4	4	1	4	4	4
	100m SHEAR NEG	10	6	7	7	5	4	4	6	6	5	4	4	4	3	4	4	3	4	4	2
	1 km SHEAR POS	7	4	5	9	5	7	5	7	4	7	4	4	2	4	4	3	4	4	3	4
	1 km SHEAR NEG	9	7	8	4	7	4	5	5	4	8	4	4	4	2	4	4	4	3	3	4
	400m SHEAR POS	6	6	4	8	12	4	5	4	5	7	4	4	4	4	5	2	2	2	4	5
	400m SHEAR NEG	10	4	5	11	7	7	2	4	3	8	3	3	3	6	5	5	1	3	2	5
	3 km SHEAR POS	8	3	4	7	5	6	5	12	5	5	4	5	3	3	3	4	5	5	3	3
	3 km SHEAR NEG	6	12	5	5	7	3	7	3	8	5	5	5	2	4	2	2	7	3	3	3

APPENDIX III (Cont.)

At least $n = 5$

At most: $n = 5$

RAND SEQ	DECILE:	At least $n = 5$										At most: $n = 5$									
		1	2	3	4	5	6	7	8	9	10	1	2	3	4	5	6	7	8	9	10
1	MAX WIND SPEED	9	5	7	5	7	10	5	8	11	7	5	3	5	3	5	5	5	5	5	5
	100m SHEAR POS	11	10	5	6	5	6	7	8	9	6	5	5	5	4	5	5	4	5	5	3
	100m SHEAR NEG	9	7	6	6	7	6	8	10	8	7	5	4	4	5	5	4	4	5	5	5
	1 km SHEAR POS	8	6	12	6	5	7	5	12	6	7	5	5	3	4	5	5	5	5	4	5
	1 km SHEAR NEG	7	6	5	9	9	7	6	11	5	8	5	5	3	5	5	5	4	5	4	5
	400m SHEAR POS	9	9	5	12	5	3	10	6	9	5	5	7	2	5	5	3	4	4	5	5
	400m SHEAR NEG	10	4	4	6	7	11	5	7	8	11	6	3	2	5	1	8	5	3	6	7
	3 km SHEAR POS	6	10	3	12	10	3	8	9	4	9	5	7	3	6	4	4	3	6	1	7
	3 km SHEAR NEG	5	5	12	8	5	7	5	10	11	5	3	2	2	7	5	6	5	7	6	2
	2	MAX WIND SPEED	7	8	10	7	9	7	6	6	6	9	5	4	5	5	5	4	5	4	4
100m SHEAR POS		8	9	11	6	5	6	8	6	9	6	5	5	5	5	2	4	5	5	5	5
100m SHEAR NEG		5	5	12	9	7	8	7	8	9	5	4	4	5	5	5	5	5	5	5	3
1 km SHEAR POS		5	7	5	9	10	7	8	9	5	8	5	5	5	5	4	5	5	5	2	5
1 km SHEAR NEG		5	8	7	11	9	7	7	5	9	8	5	5	5	5	5	5	2	5	5	4
400m SHEAR POS		8	6	7	8	5	11	11	4	6	9	6	4	5	4	3	5	5	3	6	5
400m SHEAR NEG		5	8	8	9	7	10	10	9	3	6	4	5	4	6	5	6	6	7	0	3
3 km SHEAR POS		6	8	11	7	5	8	9	6	7	7	5	5	5	2	5	7	5	3	6	3
3 km SHEAR NEG		5	5	5	10	3	11	13	9	6	8	2	4	5	8	3	5	6	5	2	6
3		MAX WIND SPEED	7	7	11	6	8	8	6	7	5	6	4	5	5	5	5	5	4	4	5
	100m SHEAR POS	7	8	5	7	5	6	8	10	6	8	4	5	2	5	5	3	5	5	5	5
	100m SHEAR NEG	9	5	5	11	5	7	9	8	6	6	5	2	5	5	4	5	5	5	4	4
	1 km SHEAR POS	8	5	5	8	8	7	7	11	6	6	5	3	5	5	5	5	2	5	4	5
	1 km SHEAR NEG	5	8	9	6	11	5	11	5	7	5	3	5	5	5	5	4	5	4	5	3
	400m SHEAR POS	5	9	5	10	5	7	7	8	8	7	4	4	5	5	4	4	5	4	2	7
	400m SHEAR NEG	8	5	7	9	5	10	5	8	5	8	6	6	4	4	1	7	4	5	5	2
	3 km SHEAR POS	5	13	8	10	3	4	8	10	8	3	3	9	7	3	2	2	7	4	4	3
	3 km SHEAR NEG	5	6	10	4	4	15	7	11	5	5	3	3	5	2	2	8	6	6	4	4
	4	MAX WIND SPEED	7	7	7	13	5	5	7	10	6	7	5	5	4	5	5	2	5	5	4
100m SHEAR POS		11	5	8	7	5	6	7	6	11	8	5	2	5	3	5	5	5	5	5	5
100m SHEAR NEG		5	6	11	6	5	6	6	10	12	7	4	4	5	4	4	4	5	5	5	5
1 km SHEAR POS		8	7	8	12	8	5	9	6	7	5	5	5	5	5	5	2	5	5	4	4
1 km SHEAR NEG		6	6	8	8	9	12	7	7	7	5	5	5	5	4	4	5	4	5	5	3
400m SHEAR POS		9	9	7	8	5	2	14	6	5	9	7	1	5	4	4	1	10	2	5	6
400m SHEAR NEG		7	6	5	8	10	10	6	10	7	6	6	4	3	6	7	3	2	5	6	3
3 km SHEAR POS		8	8	8	11	5	8	9	3	8	6	6	4	5	7	4	4	3	1	7	4
3 km SHEAR NEG		10	8	4	10	8	12	10	2	9	2	5	4	4	7	7	7	4	3	3	1
5		MAX WIND SPEED	6	7	7	8	5	7	7	12	8	7	3	5	5	3	5	5	4	5	5
	100m SHEAR POS	5	10	9	7	5	10	5	9	7	8	5	5	5	4	5	5	1	5	5	5
	100m SHEAR NEG	10	7	11	7	5	7	5	7	7	8	5	4	5	5	5	5	5	5	3	3
	1 km SHEAR POS	9	5	7	10	5	7	6	10	5	10	5	5	3	5	4	5	5	5	3	5
	1 km SHEAR NEG	10	9	12	5	9	5	5	5	6	8	5	4	5	5	5	5	5	2	4	5
	400m SHEAR POS	8	6	5	9	12	5	6	7	7	10	6	4	4	3	7	4	3	4	4	6
	400m SHEAR NEG	11	6	5	12	8	9	4	6	5	8	6	3	2	8	5	6	2	4	3	5
	3 km SHEAR POS	8	5	5	8	9	7	5	13	7	7	6	4	3	3	4	4	6	8	3	4
	3 km SHEAR NEG	8	15	5	5	8	3	11	4	10	5	7	6	2	5	3	2	8	4	5	3