

A GENERAL MULTIVARIATE FORMULATION OF THE MULTI-ANTENNA GNSS ATTITUDE DETERMINATION PROBLEM

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ABSTRACT

Global Navigation Satellite System (GNSS) carrier phase ambiguity resolution is the key to high precision positioning, navigation and attitude determination. In this contribution we present a general formulation for the multi-antenna GNSS attitude determination problem. This multivariate formulation provides a general framework for solving various GNSS attitude determination problems. With the use of this formulation we show how the constrained integer least-squares carrier phase ambiguities and corresponding attitude matrix can be solved.

1 INTRODUCTION

In this contribution we consider the problem of ambiguity resolution for GNSS attitude determination, see e.g. (*Peng et al.*, 1999), (*Park and Teunissen*, 2003), (*Moon and Verhagen*, 2006), (*Teunissen*, 2006). GNSS ambiguity resolution is the process of resolving the unknown cycle ambiguities of the carrier phase data as integers. The sole purpose of ambiguity resolution is to use the integer ambiguity constraints as a means of improving significantly on the precision of the remaining model parameters. Apart from the current Global Positioning System (GPS) models, carrier phase ambiguity resolution also applies to the future modernized GPS and the future European Galileo GNSS. An overview of GNSS models, together with their applications in surveying, navigation, geodesy and geophysics, can be found in textbooks such as (*Hofmann-Wellenhof et al.*, 1997), (*Le-*

ick, 1995), (Parkinson and Spilker, 1996), (Strang and Borre, 1997) and (Teunissen and Kleusberg, 1998).

Attitude determination based on GNSS is a rich field of current studies, with a wide variety of challenging (terrestrial, air and space) applications. In the present contribution we introduce a general multivariate formulation for the GNSS attitude determination problem and show how the corresponding integer ambiguity resolution problems can be solved. Our formulation applies to an arbitrary multi-antenna situation (2, 3, 4 or more antennas) and it encompasses all GNSS configurations (data type, frequencies, integration of GNSSs). This formulation has the advantage that it provides one general approach to the various individual cases and moreover shows how these individual cases are interrelated.

This contribution is organised as follows. In Section 2, we give a very brief review of the unconstrained integer ambiguity resolution problem. In Section 3, we introduce the multivariate formulation of the GNSS multiple antenna attitude model. In Section 4, we present orthogonal decompositions of the objective function and show how the overall solution can be computed by means of intermediate steps. Finally, in Section 5 we generalize the results to the multi-epoch case.

2 UNCONSTRAINED INTEGER AMBIGUITY RESOLUTION

2.1 The GNSS baseline model

In principle all the GNSS baseline models can be cast in the following frame of linear(ized) observation equations,

$$E(y) = Az + Gb \quad , \quad D(y) = Q_y \quad (1)$$

where $E(\cdot)$ and $D(\cdot)$ denote the expectation and dispersion operator, y is the given GNSS data vector of order m , z and b are the unknown parameter vectors of order n and p , and where A and G are the given design matrices that link the data vector to the unknown parameters. The geometry matrix G contains the unit line-of-sight vectors. The variance matrix of y is given by the positive definite matrix Q_y , which is assumed known. The data vector y will usually consist of the 'observed minus computed' single- or multiple-frequency double-difference (DD) phase and/or pseudorange (code) observations accumulated over all observation epochs. The entries of vector z are then the DD carrier phase ambiguities, expressed in units of cycles rather than range. They are known to be *integers*, $z \in Z^n$. The entries of the vector b will consist of the remaining unknown parameters, such as for instance baseline components (coordinates) and possibly atmospheric delay parameters (troposphere, ionosphere). They are known to be real-valued, $b \in R^p$.

2.2 Integer least-squares estimation

When solving the GNSS model (1), one usually applies the least-squares principle. This amounts to solving the following minimization problem,

$$\min_{z,b} \| y - Az - Gb \|_{Q_y}^2, \quad z \in Z^n, b \in R^p \quad (2)$$

with the weighted squared norm $\|\cdot\|_{Q_y}^2 = (\cdot)^T Q_y^{-1}(\cdot)$. This problem has been called a (mixed) integer least-squares (ILS) problem in *Teunissen (1993)*. To solve this problem, we first apply an orthogonal decomposition and write the quadratic form of (2) as a sum of three squares,

$$\| y - Az - Gb \|_{Q_y}^2 = \| \hat{e} \|_{Q_y}^2 + \| \hat{z} - z \|_{Q_z}^2 + \| \hat{b}(z) - b \|_{Q_{\hat{b}(z)}}^2 \quad (3)$$

with

$$\begin{aligned} \hat{e} &= y - A\hat{z} - G\hat{b} \\ \hat{z} &= (\bar{A}^T Q_y^{-1} \bar{A})^{-1} \bar{A}^T Q_y^{-1} y \\ \hat{b} &= (\bar{G}^T Q_y^{-1} \bar{G})^{-1} \bar{G}^T Q_y^{-1} y \\ \hat{b}(z) &= (G^T Q_y^{-1} G)^{-1} G^T Q_y^{-1} (y - Az) \end{aligned} \quad (4)$$

where $\bar{A} = P_G^\perp A$, $\bar{G} = P_A^\perp G$, with the orthogonal projectors $P_G^\perp = I - P_G$, $P_G = G(G^T Q_y^{-1} G)^{-1} G^T Q_y^{-1}$, $P_A^\perp = I - P_A$ and $P_A = A(A^T Q_y^{-1} A)^{-1} A^T Q_y^{-1}$. The matrix P_G is the orthogonal projector that projects orthogonally onto the range of G (with respect to the metric of Q_y^{-1}). Similarly, P_A is the orthogonal projector that projects orthogonally onto the range of A . The variance matrices of \hat{z} , \hat{b} and $\hat{b}(z)$ are given as

$$\begin{aligned} Q_{\hat{z}} &= (\bar{A}^T Q_y^{-1} \bar{A})^{-1} \\ Q_{\hat{b}} &= (\bar{G}^T Q_y^{-1} \bar{G})^{-1} \\ Q_{\hat{b}(z)} &= (G^T Q_y^{-1} G)^{-1} \end{aligned} \quad (5)$$

The vectors \hat{z} and \hat{b} are referred to as the float ambiguity solution and float baseline solution, respectively. They follow when one solves (2) *without* the integer constraints $z \in Z^n$. The vector \hat{e} is the least-squares residual vector that corresponds with this float solution.

In our case we need to take the integer constraints $z \in Z^n$ into account. It follows, with (3), from (2) that

$$\begin{aligned} &\min_{z \in Z^n, b \in R^p} \| y - Az - Gb \|_{Q_y}^2 = \\ &= \| \hat{e} \|_{Q_y}^2 + \min_{z \in Z^n, b \in R^p} \left(\| \hat{z} - z \|_{Q_z}^2 + \| \hat{b}(z) - b \|_{Q_{\hat{b}(z)}}^2 \right) \\ &= \| \hat{e} \|_{Q_y}^2 + \min_{z \in Z^n} \left(\| \hat{z} - z \|_{Q_z}^2 + \min_{b \in R^p} \| \hat{b}(z) - b \|_{Q_{\hat{b}(z)}}^2 \right) \end{aligned} \quad (6)$$

Note that the last term can be made zero for any z . Hence, the sought for solution is given as

$$\begin{aligned}\check{z} &= \arg \min_{z \in Z^n} \|\hat{z} - z\|_{Q_{\hat{z}}}^2 \\ \check{b} &= \hat{b}(\check{z})\end{aligned}\tag{7}$$

The vectors \check{z} and \check{b} are often referred to as the fixed ambiguity solution and the fixed baseline solution, respectively.

2.3 The LAMBDA method

An integer search is needed to compute \check{z} . Although we will refrain from discussing the computational intricacies of ILS estimation, the conceptual steps of the computational procedure will very briefly be described. The ILS procedure is mechanized in the LAMBDA (Least-squares AMBiguity Decorrelation Adjustment) method (*Teunissen, 1995*). The main steps are as follows. One starts by defining the ambiguity search space

$$\Omega_{\hat{z}} = \{z \in Z^n \mid (\hat{z} - z)^T Q_{\hat{z}}^{-1} (\hat{z} - z) \leq \chi^2\}\tag{8}$$

with χ^2 a suitable chosen positive constant. In order for the search space not to contain too many integer vectors, a small value for χ^2 is required, but one that still guarantees that the search space contains at least one integer grid point.

The boundary of the search space $\Omega_{\hat{z}}$ is ellipsoidal. It is centred at \hat{z} and its shape is governed by the variance matrix $Q_{\hat{z}}$. In case of GNSS, the search space is usually extremely elongated, due to the high correlations between the ambiguities. Since this extreme elongation usually hinders the computational efficiency of the search, the search space is first transformed to a more spherical shape,

$$\Omega_{\hat{a}} = \{a \in Z^n \mid (\hat{a} - a)^T Q_{\hat{a}}^{-1} (\hat{a} - a) \leq \chi^2\}\tag{9}$$

using an admissible ambiguity transformation: $a = Tz$, $\hat{a} = T\hat{z}$, $Q_{\hat{a}} = TQ_{\hat{z}}T^T$. Ambiguity transformations T are said to be admissible when both T and its inverse T^{-1} have integer entries. Such matrices preserve the integer nature of the ambiguities. In order for the transformed search space to become more spherical, the volume-preserving T -transformation is constructed as a transformation that decorrelates the ambiguities as much as possible. Using the triangular decomposition of $Q_{\hat{a}}$, the left-hand side of the quadratic inequality in (9) is then written as a sum-of-squares:

$$\sum_{i=1}^n \frac{(\hat{a}_{i|I} - a_i)^2}{\sigma_{i|I}^2} \leq \chi^2\tag{10}$$

On the left-hand side one recognizes the conditional least-squares estimate $\hat{a}_{i|I}$, and its variance $\sigma_{i|I}^2$, which follows when the conditioning takes place on the integers a_1, a_2, \dots, a_{i-1} (thus the short-hand notation $i|I$ stands for $i|1, 2, \dots, i-1$, and $n|N$ for $n|1, 2, \dots, n-1$).

Using the sum-of-squares structure, one can finally set up the n intervals which are used for the search. These n sequential intervals are given as

$$(\hat{a}_1 - a_1)^2 \leq \sigma_1^2 \chi^2, \dots, (\hat{a}_{n|N} - a_n)^2 \leq \sigma_{n|N}^2 \left(\chi^2 - \sum_{i=1}^{n-1} \frac{(\hat{a}_{i|I} - a_i)^2}{\sigma_{i|I}^2} \right) \quad (11)$$

For more information on the LAMBDA method, we refer to e.g. (*Teunissen, 1993*), (*Teunissen, 1995*) and (*de Jonge and Tiberius, 1996*) or to the textbooks (*Hofmann-Wellenhof et al., 1997*), (*Strang and Borre, 1997*), (*Teunissen and Kleusberg, 1998*), (*Misra and Enge, 2006*).

3 THE GNSS MULTIPLE ANTENNA ATTITUDE MODEL

3.1 A matrix formulation

Let us assume that $n + 1$ antennas simultaneously track $m + 1$ GNSS satellites. The DD phase and code data observed by antenna pair i is collected in the vector y_i . We assume that all the data are observed at a single epoch and on a single frequency. The material that follows is easily extended to the multiple frequency case. The multiple epoch case is considered in Section 5. Hence, the vector y_i will be of order $2m$ (m DD phase observations and m DD code observations). Since there are $n + 1$ antennas, there are n independent antenna pairs and therefore n data vectors y_i . These data vectors will be collected in the $2m \times n$ data matrix $Y = [y_1, \dots, y_n]$. We assume that the atmospheric delays can be neglected and that the separation between the antennas is such that their line-of-sight vectors to the same satellite are the same.

Based on the above assumptions, the linear(ized) GNSS multiple antenna model can be formulated as

$$E(Y) = AZ + GB, \quad Z \in Z^{m \times n}, B \in R^{3 \times n} \quad (12)$$

with $Z = [z_1, \dots, z_n]$ the $m \times n$ matrix of n unknown DD integer ambiguity vectors z_i , $B = [b_1, \dots, b_n]$ the $3 \times n$ matrix of n unknown (incremental) baseline vectors b_i , G the $2m \times 3$ geometry matrix that contains the unit line-of-sight vectors and A the $2m \times m$ matrix that links the DD data to the integer ambiguities. The sets $Z^{m \times n}$ and $R^{3 \times n}$ denote the set of integer matrices of order $m \times n$ and the set of real matrices of order $3 \times n$, respectively. Compare (12) with (1).

The goal of attitude determination is to determine the attitude of a vehicle with respect to a user-defined navigation frame, such as e.g. the ECEF-frame (Earth Centred Earth Fixed) or the ENU-frame (East North Up). We therefore assume that the baseline vectors b_i are expressed in such a user-defined navigation frame. Additionally, we assume that the $n + 1$ antennas are rigidly mounted on a vehicle and that their n baselines are known in the body frame of the vehicle. The n baselines, when expressed in the body frame, are denoted as f_i , $i = 1, \dots, n$, and we collect them in the $3 \times n$ matrix $F^T = [f_1, \dots, f_n]$

(note: the use of the transpose in F^T is simply a matter of notational convenience for the remaining material). The two different expressions of the n baselines are related by a three-dimensional rotation matrix R ($R^T R = I_3$, $\det R = 1$). Thus, $b_i = R f_i$, $i = 1, \dots, n$, or $B = R F^T$. Substitution into (12) gives

$$E(Y) = AZ + G R F^T \quad (13)$$

The unknowns in this matrix observation equation are Z and R .

3.2 A body frame representation

It will be clear that R is underdetermined in the two-antenna or single baseline case ($n = 1$). This case, however, does still allow us to obtain attitude information, namely heading and elevation (or yaw and pitch). To be able to include the case $n < 3$, without affecting the generality of our approach, we give some additional structure to the $3 \times n$ matrix F^T . We assume that the first three baselines define the (not necessarily orthogonal) axes of the body frame and that they are represented in this body frame as an upper-triangular matrix,

$$[f_1, f_2, f_3] = \begin{bmatrix} f_{11} & f_{21} & f_{31} \\ 0 & f_{22} & f_{32} \\ 0 & 0 & f_{33} \end{bmatrix} \quad (14)$$

Hence, if we denote the orthonormal columns of R as r_i , $i = 1, 2, 3$, then

$$\begin{aligned} \text{For } n = 1 : \quad R F^T &= r_1 f_{11} \stackrel{\text{call}}{=} R_1 F_1^T \\ \text{For } n = 2 : \quad R F^T &= [r_1, r_2] \begin{bmatrix} f_{11} & f_{21} \\ 0 & f_{22} \end{bmatrix} \stackrel{\text{call}}{=} R_2 F_2^T \\ \text{For } n = 3 : \quad R F^T &= [r_1, r_2, r_3] \begin{bmatrix} f_{11} & f_{21} & f_{31} \\ 0 & f_{22} & f_{32} \\ 0 & 0 & f_{33} \end{bmatrix} \stackrel{\text{call}}{=} R_3 F_3^T \\ \text{For } n > 3 : \quad R F^T &= [r_1, r_2, r_3] \begin{bmatrix} f_{11} & f_{21} & f_{31} & f_{41} & \cdots & f_{n1} \\ 0 & f_{22} & f_{32} & f_{42} & \cdots & f_{n2} \\ 0 & 0 & f_{33} & f_{43} & \cdots & f_{n3} \end{bmatrix} \stackrel{\text{call}}{=} R_3 F_n^T \end{aligned} \quad (15)$$

Thus with $q = n$ if $n \leq 3$ and $q = 3$ if $n > 3$, we have that R_q is a $3 \times q$ matrix with orthonormal columns and that F_n^T is a $q \times n$ matrix. With the notation of (15), we can write (13) as

$$E(Y) = AZ + G R_q F_n^T, \quad Z \in Z^{m \times n}, R_q \in O^{3 \times q} \quad (16)$$

where $O^{3 \times q}$ denotes the set of $3 \times q$ matrices that have orthonormal columns. With this formulation, we have eliminated the underdeterminacy that occurs in (13) when $n < 3$. Both matrices R_q and F_n have full column rank q .

3.3 The model in standard form

We can now bring (16) in the form of (1) if we make use of the vec -operator. The vec -operator is a linear transformation which transforms a matrix into a vector by stacking the columns of the matrix one underneath the other. We will make a frequent use of the following two properties of the vec -operator: $\text{vec}ABC = (C^T \otimes A)\text{vec}B$ and $\text{trace}ABCD = (\text{vec}D^T)^T(C^T \otimes A)(\text{vec}B)$, where A, B, C and D are four matrices of appropriate order, and \otimes is the Kronecker product. Application of the vec -operator to (16) gives

$$E(\text{vec}Y) = (I_n \otimes A)\text{vec}Z + (F_n \otimes G)\text{vec}R_q, \quad Z \in Z^{m \times n}, R_q \in O^{3 \times q} \quad (17)$$

If we compare with (1), we have the following correspondence: $y \mapsto \text{vec}Y$, $A \mapsto (I_n \otimes A)$, $z \mapsto \text{vec}Z$, $G \mapsto (F_n \otimes G)$ and $b \mapsto \text{vec}R_q$. There is, however, one important difference with (1). In (17) we have the additional constraints $R_q \in O^{3 \times q}$.

The $2mn$ equations of (17) constitute the observations equations for our attitude determination problem. However, in order to be able to estimate Z and R_n , we also need to know the dispersion of $\text{vec}Y$. It is given as

$$D(\text{vec}Y) = Q_{\text{vec}Y} = P \otimes Q \quad (18)$$

in which P and Q are known matrices of order $n \times n$ and $2m \times 2m$, respectively. Matrix P takes care of the correlation that follows from the fact that the n baselines have one antenna in common and matrix Q takes care of the precision of the phase and code data, combined with the fact that these DD data have data from the same reference satellite in common (*Odiijk*, 2002).

4 INTEGER LEAST-SQUARES ATTITUDE ESTIMATION

4.1 Orthogonal decomposition of objective function

It is our goal to solve (17), with (18), in a least-squares sense, thereby taking the constraints on Z and R_n into account. We have in analogy with (6), the following minimization problem

$$\begin{aligned} & \min_{Z \in Z^{m \times n}, R_n \in O^{3 \times n}} \|\text{vec}Y - (I_n \otimes A)\text{vec}Z - (F_n \otimes G)\text{vec}R_n\|_{Q_{\text{vec}Y}}^2 = \\ & = \|\text{vec}\hat{E}\|_{Q_{\text{vec}Y}}^2 + \min_{Z \in Z^{m \times n}, R_n \in O^{3 \times n}} \left(\|\text{vec}\hat{Z} - \text{vec}Z\|_{Q_{\text{vec}\hat{Z}}}^2 + \|\text{vec}\hat{R}_n(Z) - \text{vec}R_n\|_{Q_{\text{vec}\hat{R}_n(Z)}}^2 \right) \\ & = \|\text{vec}\hat{E}\|_{Q_{\text{vec}Y}}^2 + \min_{Z \in Z^{m \times n}} \left(\|\text{vec}\hat{Z} - \text{vec}Z\|_{Q_{\text{vec}\hat{Z}}}^2 + \min_{R_n \in O^{3 \times n}} \|\text{vec}\hat{R}_n(Z) - \text{vec}R_n\|_{Q_{\text{vec}\hat{R}_n(Z)}}^2 \right) \end{aligned} \quad (19)$$

where the minimization is taken with respect to the *integer* matrix Z and the *orthonormal* matrix R_n . The least-squares residual matrix \hat{E} is given as $\hat{E} = Y - A\hat{Z} - G\hat{R}_n F_n^T$, in which \hat{Z} and \hat{R}_n are the least-squares estimators of Z and R_n , respectively, *without* taking the constraints $Z \in Z^{m \times n}$ and $R_n \in O^{3 \times n}$ into account. The $3 \times q$ matrix $\hat{R}_n(Z)$ is the

least-squares estimator of R_n , assuming that Z is known, but without using the constraints $R_n \in O^{3 \times n}$. Note that, in contrast to (6), the third term on the right-hand side of the last equation of (19) can not be made zero for any Z . This is due to the constraints on R_n . As we will see, this complicates the integer search for the DD ambiguities, as compared to the integer search needed for solving the GNSS baseline model (1).

If we define

$$\check{R}_n(Z) = \arg \min_{R_n \in O^{3 \times n}} \| \text{vec} \hat{R}_n(Z) - R_n \|_{Q_{\text{vec} \hat{R}_n(Z)}}^2 \quad (20)$$

then the integer least-squares estimator of Z is given as the minimizer

$$\check{Z} = \arg \min_{Z \in Z^{m \times n}} \left(\| \text{vec} \hat{Z} - \text{vec} Z \|_{Q_{\text{vec} \hat{Z}}}^2 + \| \text{vec} \hat{R}_n(Z) - \text{vec} \check{R}_n(Z) \|_{Q_{\text{vec} \hat{R}_n(Z)}}^2 \right) \quad (21)$$

from which the final sought for solution for R_q follows as

$$\check{R}_q = \hat{R}_q(\check{Z}) \quad (22)$$

From this $3 \times q$ matrix the necessary attitude information can be recovered.

The computation of \check{Z} can be done efficiently by means of the method described in (Teunissen, 2006) and (Park and Teunissen, 2007). It is based on an integer search, with the search space given as

$$\Phi = \{ Z \in Z^{m \times n} \mid \| \text{vec} \hat{Z} - \text{vec} Z \|_{Q_{\text{vec} \hat{Z}}}^2 + \| \text{vec} \hat{R}_n(Z) - \text{vec} \check{R}_n(Z) \|_{Q_{\text{vec} \hat{R}_n(Z)}}^2 \leq \chi^2 \} \quad (23)$$

where χ^2 is a suitably chosen positive constant.

We will now show how the intermediate solutions and the final attitude solution can be computed.

4.2 Intermediate least-squares solutions

We will now first derive the expressions for $\text{vec} \hat{Z}$, $\text{vec} \hat{R}_n$, $\text{vec} \hat{R}_n(Z)$ and their variance matrices. To determine $\text{vec} \hat{Z}$ and $\text{vec} \hat{R}_n$, we need to consider (17) without the integer constraints on Z and without the orthonormality constraints on R . The normal equations of the least-squares solution are then given as,

$$\begin{bmatrix} P^{-1} \otimes A^T Q^{-1} A & P^{-1} F_n \otimes A^T Q^{-1} G \\ F_n^T P^{-1} \otimes G^T Q^{-1} A & F_n^T P^{-1} F_n \otimes G^T Q^{-1} G \end{bmatrix} \begin{bmatrix} \text{vec} \hat{Z} \\ \text{vec} \hat{R}_n \end{bmatrix} = \begin{bmatrix} (P^{-1} \otimes A^T Q^{-1}) \text{vec} Y \\ (F_n^T P^{-1} \otimes G^T Q^{-1}) \text{vec} Y \end{bmatrix} \quad (24)$$

If we solve for $\text{vec} \hat{R}_n$ and thus for \hat{R}_n , the least-squares solution of R_n follows as

$$\hat{R}_n = (\bar{G}^T Q^{-1} \bar{G})^{-1} \bar{G}^T Q^{-1} Y P^{-1} F_n (F_n^T P^{-1} F_n)^{-1} \quad (25)$$

with $\bar{G} = P_A^\perp G$ and $P_A^\perp = I_{2m} - A(A^T Q^{-1} A)^{-1} A^T Q^{-1}$. The variance matrix of $\text{vec} \hat{R}_n$ is given as

$$Q_{\text{vec} \hat{R}_n} = (F_n^T P^{-1} F_n)^{-1} \otimes (\bar{G}^T Q^{-1} \bar{G})^{-1} \quad (26)$$

Similarly, if Z is assumed known, we find the least-squares solution of R_n as

$$\hat{R}_n(Z) = (G^T Q^{-1} G)^{-1} G^T Q^{-1} (Y - AZ) P^{-1} F_n (F_n^T P^{-1} F_n)^{-1} \quad (27)$$

The variance matrix of $\text{vec} \hat{R}_n(Z)$ is given as

$$Q_{\text{vec} \hat{R}_n(Z)} = (F_n^T P^{-1} F_n)^{-1} \otimes (G^T Q^{-1} G)^{-1} \quad (28)$$

The solution $\text{vec} \hat{Z}$ follows as

$$\text{vec} \hat{Z} = [I_n \otimes (A^T Q^{-1} A)^{-1} A^T Q^{-1}] [\text{vec} Y - (F_n \otimes G) \text{vec} \hat{R}_n] \quad (29)$$

Its variance matrix is given as

$$\begin{aligned} Q_{\text{vec} \hat{Z}} &= \left[(P^{-1} \otimes A^T Q^{-1}) (I - P_{F_n} \otimes P_G) (I \otimes A) \right]^{-1} \\ &= \left[P^{-1} \otimes \bar{A}^T Q^{-1} \bar{A} + P^{-1} P_{F_n}^\perp \otimes \tilde{A}^T Q^{-1} \tilde{A} \right]^{-1} \end{aligned} \quad (30)$$

with $\bar{A} = P_G^\perp A$, $\tilde{A} = P_G A$, $P_G^\perp = I - P_G$, $P_{F_n}^\perp = I - P_{F_n}$, $P_G = G(G^T Q^{-1} A)^{-1} A^T Q^{-1}$, and $P_{F_n} = F_n (F_n^T P^{-1} F_n)^{-1} F_n^T P^{-1}$.

The case $n \leq 3$

The above least-squares solutions show a dependence on F_n , i.e. on the relative geometry of the antenna configuration as expressed in the body frame. This is of practical importance, since it allows one to improve the precision of these estimators by designing an appropriate geometry of the antenna configuration. In case of four or less than four antennas ($n \leq 3$), however, the situation is somewhat different. In that case matrix F_n is square and invertible, see (15), which implies that $P_{F_n} = I$, $P_{F_n}^\perp = 0$ and $(F_n^T P^{-1} F_n)^{-1} F_n^T P^{-1} = F_n^{-1}$. The least-squares solutions reduce then to

$$\begin{aligned} \hat{R}_n &= (\bar{G}^T Q^{-1} \bar{G})^{-1} \bar{G}^T Q^{-1} Y F_n^{-T} \\ \hat{R}_n(Z) &= (G^T Q^{-1} G)^{-1} G^T Q^{-1} (Y - AZ) F_n^{-T} \end{aligned} \quad (31)$$

For the variance matrices describing the precision, we have

$$\begin{aligned} Q_{\text{vec} \hat{R}_n} &= F_n^{-1} P F_n^{-T} \otimes (\bar{G}^T Q^{-1} \bar{G})^{-1} \\ Q_{\text{vec} \hat{R}_n(Z)} &= F_n^{-1} P F_n^{-T} \otimes (G^T Q^{-1} G)^{-1} \\ Q_{\text{vec} \hat{Z}} &= P \otimes (\bar{A}^T Q^{-1} \bar{A})^{-1} \end{aligned} \quad (32)$$

This shows, although the precision of \hat{R}_n and $\hat{R}_n(Z)$ is still dependent on the choice of antenna configuration, that the precision of \hat{Z} is now independent of this configuration. The well-known fact that longer baselines improve the attitude capability is also clear from the above. For instance, we have for $n = 1$, that $Q_{\text{vec} \hat{R}_1(Z)} = (P/f_{11}^2) \otimes (G^T Q^{-1} G)^{-1}$, with f_{11} the length of the baseline.

4.3 Solving for the attitude matrix

4.3.1 Nonlinear least-squares

The computation of $\check{R}_q(Z)$, see (20), requires for each Z , that one solves the minimization problem

$$\min_{R_q \in O^{3 \times q}} \|\text{vec}\hat{R}_q(Z) - \text{vec}R_q\|_{Q_{\text{vec}\hat{R}_q(Z)}}^2 \quad (33)$$

This minimization problem is a *nonlinear* least-squares problem due to the nonlinear constraints on $\text{vec}R_q$. Geometrically it amounts to finding that point on a nonlinear or curved manifold which has the smallest distance to the given data vector, which in our case is $\text{vec}\hat{R}_q(Z)$. Distance is here measured with respect to the metric of the $3q \times 3q$ variance matrix $Q_{\text{vec}\hat{R}_q(Z)}$. If $n = 1$, we have one constraint, namely the unit length of R_1 , and $\text{vec}R_1$ is of order 3×1 . Hence, in this case the curved manifold is of dimension 2 and it is embedded in the 3-dimensional space. If $n = 2$, we have three constraints, namely one orthogonality and two unit length constraints of the two columns of R_2 , and $\text{vec}R_2$ is of order 6×1 . Hence in this case the curved manifold is of dimension 3 and it is embedded in the 6-dimensional space. If $n \geq 3$, we have six constraints, namely three orthogonality and three unit length constraints of the three columns of R_3 , and $\text{vec}R_3$ is of order 9×1 . Hence, in this case the curved manifold is of dimension 3 and it is embedded in the 9-dimensional space.

The constraints $R_q \in O^{3 \times q}$ can be taken into account by a suitable parametrization of R_q (e.g. by using one of the different ways in which rotations can be parametrized). Once this is done, one has an unconstrained nonlinear least-squares problem, which can be iteratively solved by means of the Gauss-Newton method (with a local linear rate of convergence) or by the Newton method (with a local quadratic rate of convergence), see e.g. (*Teunissen, 1990*). These iterations are initialized with an appropriate approximation of R_q (see below).

4.3.2 Using the singular value decomposition

Under certain conditions it is also possible to solve (33) directly by means of a singular value decomposition (SVD). Let $M = G^T Q^{-1} G$ and $N = F_n^T P^{-1} F_n$. Then $Q_{\text{vec}\hat{R}_q(Z)} = N^{-1} \otimes M^{-1}$ and the objective function of (33) can be written as

$$\begin{aligned} \|\text{vec}\hat{R}_q(Z) - \text{vec}R_q\|_{Q_{\text{vec}\hat{R}_q(Z)}}^2 &= \text{trace}([\hat{R}_q(Z) - R_q]^T M [\hat{R}_q(Z) - R_q] N) \\ &= \text{trace}(\hat{R}_q(Z)^T M \hat{R}_q(Z) N) - 2\text{trace}(N \hat{R}_q(Z)^T M R_q) \\ &\quad + \text{trace}(R_q^T M R_q N) \end{aligned} \quad (34)$$

This function is, in general, quadratic in R_q . It will be linear in R_q , if the last term of the above equation becomes independent of R_q .

The quadratic case

With one exception, the quadratic case requires iterative solution techniques as the ones described above. The exception occurs when $n = 1$. Recall that matrix N is a $q \times q$ matrix, with $q = n$ if $n \leq 3$ and $q = 3$ if $n > 3$. Thus N is a scalar, if $n = 1$. The above minimization problem can then be written as

$$\min_{R_1 \in \mathbb{R}^3} N \|\hat{R}_1(Z) - R_1\|_{M^{-1}}^2 \text{ subject to } R_1^T R_1 = 1 \quad (35)$$

This problem can be solved by means of the singular value decomposition (SVD), see e.g. (*Golub and Van Loan*, 1989). We can formulate problem (35) also as the problem of projecting orthogonally (with respect to the standard Euclidean metric) onto an ellipsoid. To see this, let $\hat{\rho}(Z) = M^{-1/2} \hat{R}_1(Z)$ and $\rho = M^{-1/2} R_1$. Then (35) is equivalent to

$$\min_{\rho \in \mathbb{R}^3} N \|\hat{\rho}(Z) - \rho\|_{I_3}^2 \text{ subject to } \rho^T M^{-1} \rho = 1 \quad (36)$$

This problem of finding the closest point on a 2-dimensional ellipsoid is equivalent to the problem of computing geodetic coordinates from Cartesian coordinates.

The case $n = 1$ occurs when one wants to determine heading and elevation (or yaw and pitch) from one GNSS-baseline (two antennas). This method was followed in (*Park and Teunissen*, 2003).

The linear case

The objective function becomes linear in R_q , when M is a scaled unit matrix, $M = \lambda I_3$, or when N is a scaled unit matrix, $N = \mu I_q$, where λ, μ are scalars and $n \geq 3$. When $M = \lambda I_3$, we have $\text{trace}(R_q^T M R_q N) = \lambda \text{trace}(N)$, which is independent of R_q . And when $N = \mu I_q$, we have $\text{trace}(R_q^T M R_q N) = \mu \text{trace}(M R_q R_q^T) = \mu \text{trace}(M)$, if $q = 3$ and thus if $n \geq 3$.

If (34) is linear in R_q , then the minimization of the objective function is equivalent to solving a maximization problem of the form

$$\max_{R_q \in O^{3 \times q}} \text{trace}(T R_q) \quad (37)$$

with the $q \times 3$ matrix T given. If $M = \lambda I_3$, then $T = \lambda N \hat{R}_q(Z)^T$, which is a $q \times 3$ matrix. And when $N = \mu I_q$ and $n \geq 3$, then $T = \mu \hat{R}_q(Z)^T M$, which is a $q \times 3$ matrix, with $q = 3$. Let $T = U \Lambda V^T$ be the SVD of T , with orthogonal matrices U and V of order $q \times q$ and 3×3 , respectively, and with the $q \times 3$ matrix $\Lambda = (\Lambda_q, 0)$, where Λ_q is the diagonal matrix containing the q singular values. Then the solution of (37) is given as

$$\check{R}_q = V \begin{bmatrix} I_q \\ 0 \end{bmatrix} U^T \quad (38)$$

To see this, we write $\text{trace}(T R_q) = \text{trace}(U \Lambda V^T R_q) = \text{trace}(V^T R_q U \Lambda) = \sum_{i=1}^q (V^T R_q U)_{ii} \lambda_i$, in which the λ_i are the q nonnegative entries of the $q \times q$ diagonal matrix Λ_q in $\Lambda = (\Lambda_q, 0)$.

Note that the q columns of the $3 \times q$ matrix $V^T R_q U$ are orthonormal. Hence, $\text{trace}(T R_q)$ is maximal if $(V^T R_q U)_{ii} = 1$ for $i = 1, \dots, q$, and thus if $U^T R_q^T V = (I_q, 0)$. From this the result (38) follows.

Designing the antenna configuration

In practice one has not much control over the matrices G and Q in $M = G^T Q^{-1} G$. Matrix G is dictated by the relative receiver-satellite geometry and matrix Q is dictated by the precision of the observables. Hence, in practice, one can not expect that $M = \lambda I_3$ holds true. The corresponding method of solution given above is therefore no option for solving (33). At most one can use $M = \lambda I_3$ as an approximation of $G^T Q^{-1} G$ and thereby compute an approximate solution to (33), useful, for instance, for linearization purposes.

In contrast to $M = G^T Q^{-1} G$, one can, however, exercise control over $N = F_n^T P^{-1} F_n$ by means of a suitable choice of the antenna configuration, that is, by means of choosing a suitable fixed body frame F_n . Let $P = C C^T$, with C a lower triangular matrix, be the Cholesky decomposition of P . Then $P^{-1} = C^{-T} C^{-1}$, with C^{-T} an upper triangular matrix. If we now choose F_n as

$$F_n = C \begin{bmatrix} \mu I_q \\ 0 \end{bmatrix} \quad (39)$$

then $F_n^T P^{-1} F_n = \mu I_q$. With this choice for the antenna configuration, we have $Q_{\text{vec}\hat{R}_q(Z)} = \mu I_q \otimes (G^T Q^{-1} G)^{-1}$ and therefore

$$\| \text{vec}\hat{R}_q(Z) - \text{vec}R_q \|^2_{Q_{\text{vec}\hat{R}_q(Z)}} = (1/\mu) \sum_{i=1}^q \| \hat{r}_i(Z) - r_i \|^2_{(G^T Q^{-1} G)^{-1}} \quad (40)$$

The constrained minimizer of this objective function can then be found, for $q = 1$ and $q = 3$, with the SVD-approach as discussed above.

5 MULTIPLE EPOCH ATTITUDE DETERMINATION

So far we considered single epoch attitude determination. Now consider the multi epoch, multi antenna case. The matrix observation equation for epoch t is then given as

$$E(Y_t) = AZ + G_t R_{q,t} F_n^T \quad t = 1, \dots, k \quad (41)$$

Matrices A and F_n are assumed to be time-invariant. This implies a constant tracking of the same satellites. Matrices G_t and $R_{q,t}$ are assumed to depend on time. The geometry matrix G_t changes over time due to the changing relative receiver-satellite geometry and the orthonormal matrix $R_{q,t}$ changes over time, because of the changing attitude of the vehicle.

When we collect all observation equations for the k epochs, we may write them in vector-matrix form as

$$E \begin{bmatrix} \text{vec} Y_1 \\ \vdots \\ \text{vec} Y_k \end{bmatrix} = \begin{bmatrix} I_n \otimes A & F_n \otimes G_1 & & \\ & \vdots & \ddots & \\ & & & F_n \otimes G_k \end{bmatrix} \begin{bmatrix} \text{vec} Z \\ \text{vec} R_{q,1} \\ \vdots \\ \text{vec} R_{q,k} \end{bmatrix} \quad (42)$$

The variance matrix is assumed to be block diagonal. Thus with $Y = (Y_1, \dots, Y_k)$, we have $D(\text{vec} Y) = \text{blockdiag}(P_1 \otimes Q_1, \dots, P_k \otimes Q_k)$.

In analogy with our earlier orthogonal decomposition of the objective function, we may decompose the objective function for (42) as

$$H(Z, R_{q,1}, \dots, R_{q,k}) = \|\text{vec} \hat{E}_k\|_{Q_{\text{vec} Y}}^2 + \|\text{vec} \hat{Z}_k - \text{vec} Z\|_{Q_{\text{vec} \hat{Z}_k}}^2 + \sum_{i=1}^k \|\text{vec} \hat{R}_{q,i}(Z) - \text{vec} R_{q,i}\|_{Q_{\text{vec} \hat{R}_{q,i}(Z)}}^2 \quad (43)$$

The unknowns are the $m \times n$ integer matrix Z and the $3 \times q$ orthonormal matrices $R_{q,i}$, $i = 1, \dots, k$. Matrix \hat{Z}_k is the real-valued least-squares estimator of Z , based on all the data up to and including epoch k , but without taking the integerness of Z and the orthonormality of the $R_{q,i}$ into account. Matrix $\hat{R}_{q,i}(Z)$ is the least-squares estimator of $R_{q,i}$, again based on all the data up to and including epoch k and without taking the orthonormality constraints into account, but now assuming that Z is known. Note, due to the structure of (42) and the block diagonality of $D(\text{vec} Y)$, that $\hat{R}_{q,i}(Z)$ only depends on Y_i and not on Y_j for $j \neq i$. This is also the reason why the last term in (43) can be written as a summation of k terms.

The least-squares solution of (42) follows from minimizing the objective function $H(Z, R_{q,1}, \dots, R_{q,k})$ subject to the integer constraints on Z and the orthonormality constraints on $R_{q,i}$. Thus if we define

$$\check{R}_{q,i}(Z) = \arg \min_{R_{q,i} \in O^{3 \times q}} \|\text{vec} \hat{R}_{q,i}(Z) - \text{vec} R_{q,i}\|_{Q_{\text{vec} \hat{R}_{q,i}(Z)}}^2, \quad i = 1, \dots, k \quad (44)$$

then the integer least-squares estimator of Z is given as

$$\check{Z}_k = \arg \min_{Z \in Z^{m \times n}} \left(\|\text{vec} \hat{Z}_k - \text{vec} Z\|_{Q_{\text{vec} \hat{Z}_k}}^2 + \sum_{i=1}^k \|\text{vec} \hat{R}_{q,i}(Z) - \text{vec} \check{R}_{q,i}(Z)\|_{Q_{\text{vec} \hat{R}_{q,i}(Z)}}^2 \right) \quad (45)$$

The sought for least-squares estimators of the k orthonormal matrices $R_{q,i}$, based on all the data up to and including epoch k , are then given as

$$\check{R}_{q,i} = \hat{R}_{q,i}(\check{Z}_k), \quad i = 1, \dots, k \quad (46)$$

The integer solution \check{Z}_k is obtained by means of an integer search, similar to the one described in the previous sections.

For practical applications it would be very useful if the above solution can be obtained in a recursive manner. It will be clear that the structure of (42) and $D(\text{vec}Y)$ is such that the least-squares estimator \hat{Z}_k can indeed be obtained recursively. It is not difficult to show that \hat{Z}_k can be obtained from \hat{Z}_{k-1} and Y_k . However, if we now consider (45), it will be clear that \check{Z}_k can not be obtained in a recursive manner. This is due to the orthonormality constraints on $R_{q,i}$, $i = 1, \dots, k$. That is, in order to determine \check{Z}_k , and thus also $\check{R}_{q,k}$, it does not suffice to have $\hat{R}_{q,k}$ available, but we also need to store $\hat{R}_{q,i}$ for $i < k$. The conclusion is therefore reached that it is not possible to determine the integer least-squares estimator of $R_{q,k}$ in a recursive manner, if the orthonormality constraints on all k matrices $R_{q,i}$ are used. Hence, a rigorous recursive integer least-squares solution of (42) is not possible.

The above analysis suggest, however, that it is possible to construct a recursive procedure, provided one is willing to accept a suboptimal integer solution for Z . We define this suboptimal solution as

$$\check{Z}'_k = \arg \min_{Z \in \mathbb{Z}^{m \times n}} \left(\|\text{vec}\hat{Z}_k - \text{vec}Z\|_{Q_{\text{vec}\hat{Z}_k}}^2 + \|\text{vec}\hat{R}_{q,k}(Z) - \text{vec}\check{R}_{q,k}(Z)\|_{Q_{\text{vec}\hat{R}_{q,k}(Z)}}^2 \right) \quad (47)$$

This is the integer least-squares estimator of Z , that follows when one does not take the orthonormality constraints on the matrices $R_{q,i}$, $i = 1, \dots, (k-1)$, into account. Compare (47) with (45).

When use is made of (47), the updating steps in the recursion go as follows. From \hat{Z}_{k-1} and Y_k , we obtain \hat{Z}_k . Similarly, Y_k and Z , gives $\hat{R}_{q,k}(Z)$ and $\check{R}_{q,k}(Z)$. From this information \check{Z}'_k can be computed, which then finally leads to the output $\check{R}_{q,k} = \hat{R}_{q,k}(\check{Z}'_k)$. This recursion is thus made possible by only taking the orthonormality constraints into account, that pertain to the current epoch k .

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