

Research Article

A Hybrid Computational Method of Desirability, Fuzzy Logic, ANFIS, and LAPO Algorithm for Multiobjective Optimization Design of Scott Russell Compliant Mechanism

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Flexure-based compliant mechanisms are increasingly promising in precision engineering, robotics, and other applications, thanks to the excellent advantages of no friction, no backlash, no wear, and minimal assembly. However, their design and analysis are still challenging due to the coupling of kinematic-mechanical behaviors with large nonlinear deflections in comparison to their rigid-body counterparts. Optimal design is an important aspect in the field of compliant mechanisms and has attracted much attention during the last decades. Especially, when considering a multiobjective optimization design for compliant mechanisms, the problem is becoming more complicated. Thus, this article presents a new efficient hybrid computational method to resolve multiobjective optimization design of compliant mechanisms. A Scott Russell compliant mechanism is employed as the design example and to show the advantages of the proposed optimizing method. The proposed method is developed by hybridizing the desirability function approach, fuzzy logic system, adaptive neuro-fuzzy inference system (ANFIS), and lightning attachment procedure optimization (LAPO). First of all, a 3D finite element model is created and central composite design is employed to build a numerical matrix. First, design variables are refined by using analysis of variance and Taguchi approach in terms of considerably eliminating space of design variables. Subsequently, desirability values of two objective functions are determined and transferred into the fuzzy logic system. The output of the fuzzy logic system is considered as a single combined objective function. Next, modeling for fuzzy output is established via developing the ANFIS model. At last, the LAPO algorithm is adopted for solving the multiobjective optimization problem for the mechanism. Three numerical examples are investigated to validate the feasibility and the effectiveness of performance efficiency of the proposed methodology. The results find that the proposed methodology is more efficient than traditional Taguchi-based fuzzy logic. Besides, the performance efficiency of the proposed approach outperforms the Jaya algorithm and TLBO algorithm through the Wilcoxon signed rank test and Friedman test. The results of this article give a useful approach for complex optimization problems.

1. Introduction

Scott Russell compliant mechanism (SRCM) is utilized as a shuttle to transform two input motions into output one. It is exerted by a piezoelectric actuator in applications of high precision positioning systems. The mechanism can achieve its performances through elastic deformation of flexure hinges [1–4]. It benefits a monolithic structure, lightweight, and free friction. Nonlinear behaviors of the mechanism are

facing challenges for researchers in compliant mechanism. Over the past several decades, researchers have tried to make approaches and methods to synthesize compliant mechanisms, e.g., kinematic-based methods [5–8]. They showed that physical behaviors and performances of compliant mechanism should analyze displacement, stress, frequency, and parasitic error. Kinematic-based methods are still valid, but some are difficult to resolve the performances of SRCM because of their complicated applications.

In the past decades, a lot of analytical methods and numerical methods have been proposed for designing and analyzing compliant mechanisms, such as the pseudorigid-body model (PRBM) [9], Castigliano's second theorem [10], compliance matrix method [11], empirical method [12], beam constraint model [13], Euler–Bernoulli beam theory [14], and finite element method [15]. However, these methods are useful in advancing simple compliant mechanisms with existing configurations. But they are critically challenging in analyzing the static and dynamic behaviors for complex compliant mechanisms, such as irregular shapes of flexure hinges and complex configurations and large deflections. It is known that the PRBM is still a valuable technique for modeling, but it is limited in highly nonlinear deformation of flexure hinges. For complex loads and complicated configurations of flexure hinges, the PRBM is not suitable. Especially, the PRBM is strongly dependent on the location of torsional springs, the number of torsional springs, and designer's experiences in the field of compliant mechanisms. Castigliano's second theorem can analyze the strain energies of flexure hinges such as tensile, shear, and bending strains, but this theorem is critically complicated for complex structures. Compliance matrix method is actually difficult for analyzing when compliant mechanisms subject multiple complicated actuation forces. Elastic beam theory is related to the deformation energy of compliant mechanisms, but it is still complicated for complex structures. Based on the two-port dynamic stiffness model, statics and dynamics can be effectively solved, but it becomes more complicated for modeling irregular structures. Compliance matrix method is used to transfer the compliance of flexure hinges from the local coordinate frame into a reference coordinate system. This method is still complicated for a more complex structure of compliant mechanisms. Empirical modeling can analyze compliant mechanisms with high accuracy, but it is very costly and time-consuming. It is difficult to analyze a large deformation of flexure hinges using the beam constraint model. Finite element method (FEM) analyzes complex geometric shapes of compliant mechanisms by discretizing compliant mechanisms into elements and nodes.

Although the previous methods are still valid, they are still challenging to analyze the complex compliant mechanisms. The estimating accuracy of modeling are based on a complexity degree of kinematic and mechanical coupling of compliant mechanisms. Especially for a large nonlinear deflections and irregular shapes, the abovementioned methods are limited. For optimal design of multiple performances of compliant mechanisms, the problem is becoming more complex. Therefore, data-driven approach, computing intelligence, and machine learning have attracted much attention to model complex systems [16–18]. Data-driven approaches-coupled computing intelligence is an effective tool that has not extended to the field of compliant mechanisms yet. From reviewing the literature review, the motivation of this article is to develop a new hybrid computational method to solve the optimal design for compliant mechanisms. The proposed method is extended to solve for most compliant mechanisms from a basic structure to a

complex one. Specifically, it is an efficient approach for the SRCM. In order meet wide applications, the SRCM requires both a large displacement, a high frequency, and a good enough working strength. In order to solve three quality performances simultaneously, size, shape, or topology of the proposed mechanism can be changed. However, a such random change spends a lot of computational time. At the same time, a parameter optimization is conducted by researchers to enhance the physical performances. Optimization problem includes a single response or more than two ones. In the past, the structural optimization problem of a compliant mechanism separates into three main types, e.g., topology optimization [19], shape optimization, and size optimization [14, 20, 21]. In this work, size optimization is chosen to find the best geometrical parameters of SRCM.

In order to solve multiple objective responses, a multiobjective optimization (MOO) problem is investigated. The aim of the MOO problem is to reach a trade-off between characteristics. Nowadays, the MOO problem has received a great interest for compliant mechanisms [22–24]. However, a MOO optimal design for the proposed SRCM has not been studied in depth. So, parameter optimization is proposed in the present article. In a real structure of SRCM, it includes possible design parameters affecting desired performances. Besides, it is well-known that physical behaviors of the SRCM are very sensitive to a change in shape, material, or geometrical parameters. Shape and material may be directly varied according to customer's demands. Meanwhile, structural parameters should be optimized to improve the performances. The most critical parameters strongly contribute on the performances, while some nonsignificant parameters lead high computational cost. Hence, before implementing the MOO process, this study determines the most significant design variables and nonsignificant parameters.

Basically, before dealing with a MOO problem for a specific compliant mechanism, a mathematical model is expected to be established through kinematic-based analytical approaches such as pseudorigid-body model [25], semianalytical model [26], and compliance matrix [27]. Although mentioned approaches are still used, they are complicated for modeling the SRCM. In other words, analytical methods are limited to feature its behaviors of more complex structures. In order to avoid an imprecise optimization solution since approximate approaches may be complicated, data-driven approaches are more advantageous to adopt for the MOO problem. Data-driven approach is utilized to directly map the inputs and outputs data; therefore, this approach has a good predicting accuracy in comparison with the analytical methods. During the last decades, a lot of methods have been developed to solve the MOO problems, such as desirability function approach (DFA) [28], grey relational analysis (GRA) [29], Taguchi method-based fuzzy logic (TMFL) [30]. Both DFA and GRA need a weight factor for each objective function, but weighting factor is largely dependent on experience or users. Meanwhile, TMFL is a statistical-based approach without the weight factor. Although TMFL has more benefits, it searches optimal values at discrete points from the Taguchi

method. In order to avoid a local result, surrogate models are employed to connect inputs and outputs, e.g., response surface method (RSM) [31], Kriging technique [32], artificial neural network (ANN) [33–35], adaptive neuro-fuzzy inference system (ANFIS) [36–38], RSM-ANN [39], ANN machine learning [40], and fuzzy logic theory [41]. Among them, ANFIS is proved as an effective technique to modeling and predicting, which is applied for different engineering fields. For example, ANFIS was developed to predict for various fields, e.g., the hydropower generation [17], the scour hole shape [18], and mercury emissions in combustion flue gases [42]. However, ANFIS has not extended for modeling the Scott Russell compliant mechanism yet.

Up to now, nature-based metaheuristic algorithms have been developing very fast, e.g., genetic algorithm [43], particle swarm optimization (PSO) [44], differential evolution [45], cuckoo search algorithm [46], and other algorithms [47–50]. Some of them have successfully been applied in various fields, such as grey wolf optimization for temperature-based oil-water relative permeability [16] and PSO algorithm for predicting the scour depth around bridge piers [51]. More recently, several algorithms with less or nontuned parameters have been suggested such as teaching learning-based algorithm (TLBO) [52, 53], Jaya algorithm [54], and lightning attachment procedure optimization (LAPO) algorithm [55]. Among three less-parameter algorithms, LAPO algorithm is an effective approach for a lot of engineering areas, but it has not been applied for the SRCM mechanism yet. Therefore, this article chooses the LAPO algorithm to extend the MOO design. In summary, highlight contributions of this study are as follows: (i) limit nonsignificant parameters and refine space of design variables; (ii) transfer the desirability value of objective functions into the fuzzy logic reasoning; (iii) develop the ANFIS structure to model the output of FIS system; (iv) LAPO algorithm is proposed for implementing the MOO problem to find global solution; (v) performances of proposed methodology are compared with other algorithms using statistical techniques.

The goal of this article is to develop new hybrid computational methodology to conduct MOO optimal design for the SRCM mechanism. As mentioned above, the proposed method is considered as statistical-based intelligent computation. A 3D model is created by the finite element method, and central composite design is employed to make design of experiments. Initial space of design variables is determined and then refined via analysis of variance and Taguchi technique. New spaces of design parameters are generated through sensitivity investigation. Next, desirability values of quality responses are calculated and transferred into the fuzzy logic system. ANFIS technique is developed to connect design variables and output of the FIS. MOO problem is then solved by using the LAPO algorithm. Numerical examples are investigated to evaluate the computational efficiency and performance of proposed method. In addition, performances of the proposed approach are compared with the ANFIS-based Jaya and ANFIS-based TLBO by implementing the Wilcoxon signed rank test and Friedman test.

2. Proposed Hybrid Methodology

Figure 1 describes a new computational method which is hybridized by the integrating desirability approach, fuzzy logic reasoning, ANFIS, and LAPO algorithm. The proposed method is applied to solve a MOO design for a Scott Russell compliant mechanism. Practically, this mechanism is combined with a piezoelectric actuator (PA) for use in ultrahigh precision positioning devices. Because the PA limited its travel and responding speed, the mechanism needs to improve its displacement and a high natural frequency. In addition, a small equivalent stress is considered as an additional constraint to ensure a good working strength. According to background of compliant mechanism, these specifications are very sensitive to geometrical parameters of flexure hinges. In other words, a change in any geometrical factor may lead to a change in performances. In order to achieve an improvement in performances, design parameters are optimized simultaneously. Proposed hybrid methodology consists of five main phases as follows: (i) design and analysis, (ii) desirability calculation, (iii) fuzzy logic system analysis, (iv) ANFIS modeling, and (v) conduct MOO problem by LAPO algorithm.

2.1. Phase 1: Design and Analysis. This phase concerns about a mechanical design and analysis problem. In this study, a MOO design for a SRCM is investigated. It is an example to show effective application to validate the performance effectiveness of proposed methodology. This phase experiences the following main steps.

Step 1. Mechanical structure

As discussed above, the mechanism needs a large displacement and a high frequency but must guarantee a small stress for a long operation without plastic failure.

Step 2. Define initial design variables

Structure of the mechanism has a lot of possible geometrical parameters affecting the quality responses. Such influences must be considered before implementing further the optimization process. Some factors with actual influences as well as no influences are evaluated through sensitivity investigation in this study.

Step 3. Define quality responses

After determining the initial design variables, a large displacement and a high frequency are assigned as two desired outputs. In order to satisfy in terms of enough working strength, equivalent stress is an extra constraint.

Step 4. Create 3D finite element model

A 3D finite element model (FEM) is created, and then finite element analysis (FEA) is implemented to retrieve numerical data. To complete this work, design variables and quality responses are assigned to be parametric factors during FEA simulations.

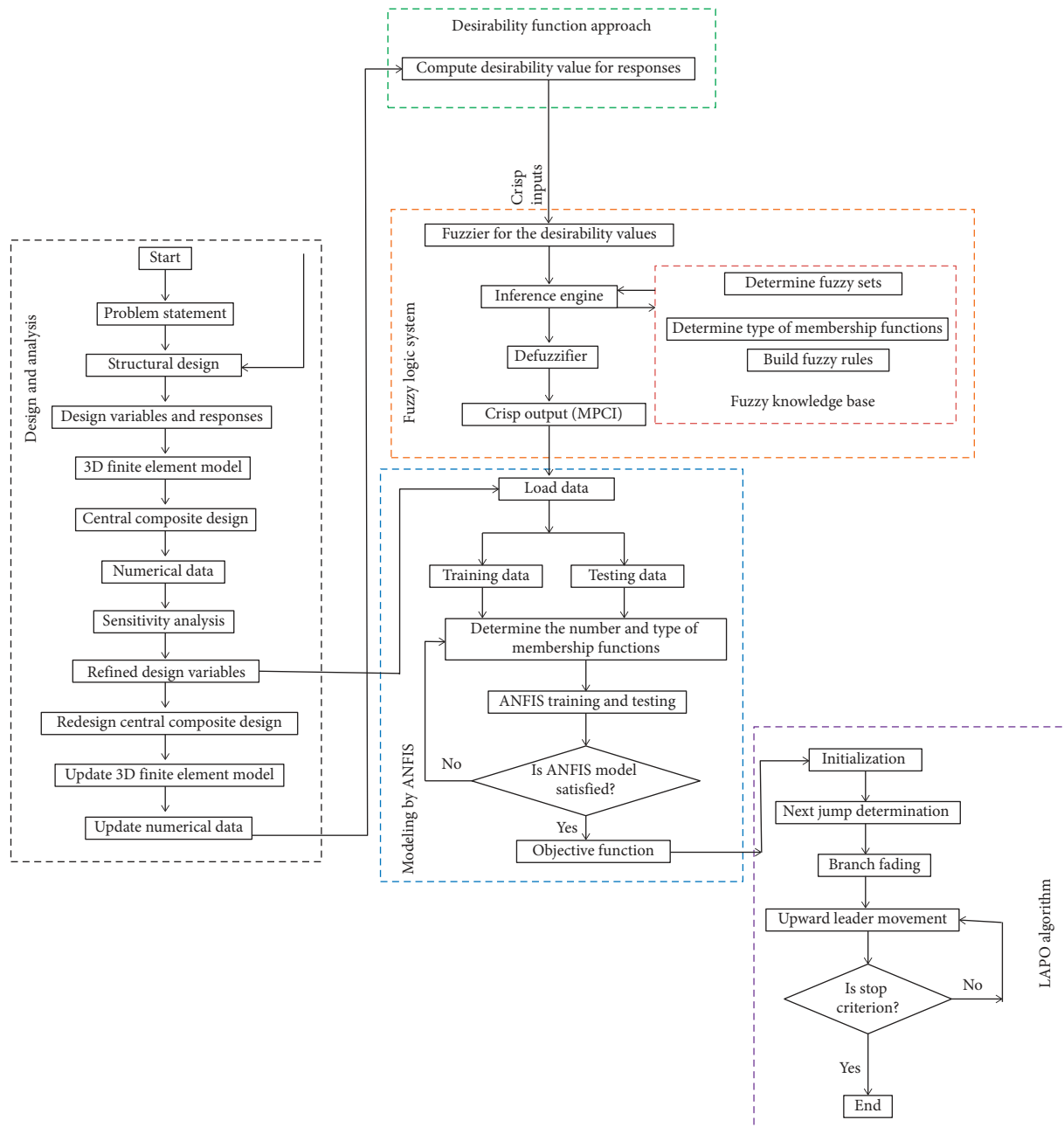


FIGURE 1: Flowchart of proposed hybrid methodology for multiobjective optimization design.

Step 5. Central composite design

While a 3D model is created, an experimental matrix is also initialized by using central composite design (CCD). Face centered is used in this work.

Step 6. Run numerical data

Boundary conditions, load, and material are set up for the 3D model. Subsequently, a set of numerical data is collected by running simulations.

Step 7. Sensitivity analysis

This is a critically important step. It determines several parameters directly affecting the quality characteristics to be design variables. Besides, some parameters with no influence

are ignored. This process is conducted through analysis of variance (ANOVA) and the Taguchi method.

Step 8. Eliminate design variables

The results of sensitivity analysis in Step 7 identify some nonsignificant parameters. And then, such parameters are ignored or eliminated while other important factors are defined as key design variables. The results of refining parameters perhaps create several new population spaces for population-based optimization metaheuristic algorithms. This is a preparing step for further optimization process. The goal of Step 8 is to determine a suitable searching space so as to reduce the computational cost and make more reliable solution.

Step 9. Repeat central composite design

Several new spaces of design variables are created in Step 8. Each space of refined variables is considered as a case study. And then, Step 9 will rebuild a number of experimental matrixes by using CCD.

Step 10. Refine 3D finite element model

In order to conduct the numerical simulations, a 3D FEM model is created with respect to each case study. Subsequently, simulations are implemented to get the numerical data for each case study.

2.2. Phase 2: Desirability Calculation

Step 11. Recollect numerical data

Numerical data for each of case study are collected through FEA simulations, individually.

Step 12. Compute desirability value for performances

According to theory of the desirability function approach [56], the exponential type is transformed to each response into a desirability function. Principle of this technique is to compute the i th quality response (y^*) to become the i th desirability (d_i), and then all values of desirability are combined into a single desirability function (D). Desirability value can reach unity when the response's target is achieved, and otherwise. Each individual desirability function is divided into three types based on user's specific demand. It includes three target types, i.e., smaller-the-best, higher-the-best, and normal-the-best. Desirability for two specifications of the mechanism is computed. Displacement is millimeter, while natural frequency is in Hertz. Based on calculating the desirability, influence and difference of units are neglected during the optimization process. So, such difference no longer affects later optimal solution.

2.2.1. *Smaller-the-Best.* The response's value is expected lower than an upper limit. The desirability function is identified by

$$\begin{cases} d_i = 0, & y^* \geq U_b, \\ d_i = \left(\frac{y^* - U_b}{L_b - U_b} \right)^r, & L_b \leq y^* \leq U_b, \\ d_i = 1, & y^* \leq L_b, \end{cases} \quad (1)$$

where d_i is the desirability value, y^* is the i th response, and L_b and U_b are the lower and upper limits of the response.

2.2.2. *Normal-the-Best.* The response's value is expected toward a target value (T). The desirability function can be determined by

$$\begin{cases} d_i = \left(\frac{y^* - L_b}{T - L_b} \right)^p, & L_b \leq y^* \leq T, \\ d_i = \left(\frac{y^* - U_b}{T - U_b} \right)^q, & T \leq y^* \leq U_b, \\ d_i = 0, & y^* \leq L_b \text{ or } y^* \geq U_b, \\ d_i = 1, & y^* = T, \end{cases} \quad (2)$$

where p and q are specific parameters defined by users ($p, q > 0$) which determine the shape of d_i .

2.2.3. *Higher-the-Best.* The response's value is expected higher than a lower limit. The desirability function can be described by

$$\begin{cases} d_i = 0, & y^* \leq L_b, \\ d_i = \left(\frac{y^* - L_b}{U_b - L_b} \right)^r, & L_b \leq y^* \leq U_b, \\ d_i = 1, & y^* \geq U_b, \end{cases} \quad (3)$$

where r is the desirability function index.

All individual desirability's values of responses are transformed into overall desirability, D , which is considered as a single quality index. This index is determined by assigning the corresponding weight factor for different quality responses. However, weight factor of each response is dependent on priority or customer's demands. A combined desirability index is computed as

$$D = ((d_1)^{w_1} (d_2)^{w_2} \dots (d_n)^{w_n})^{1/\sum w_i}, \quad (4)$$

where D is the overall desirability index and w_i is the weight of the i th response. D is equal to one as each d_i is also equal to one. Otherwise, at least, one of d_i is zero and D is zero.

In this paper, a larger type is used for both desired targets (displacement and frequency). Previously, in order to solve a MOO problem, a set of optimal parameters may be found by maximizing the single quality index D . Although this approach is still an effective tool, an optimal result is varied when the weight factor of each response is changed. It may result in an imprecisely optimal value. In order to overcome this uncertainty, a fuzzy logic system is then developed to deal with all individual values of desirability of both responses since this system does not require any weight factor.

2.3. Phase 3: Fuzzy Logic Reasoning System. A fuzzy logic reasoning system includes knowledge base, fuzzifier, inference engine, and defuzzifier. Details can be briefly described as follows [57].

2.3.1. Fuzzifier. Fuzzifier plays a role to transform real value into a fuzzy system. Inputs of the fuzzy logic system are called as crisp values which contain precise information of a real world. Through the fuzzifier, real value is transformed into linguistic variable.

Knowledge base: knowledge base consists of rule base that forms a number of fuzzy rules (if-then). Moreover, the knowledge base contains a database which defines membership function (MF) of the fuzzy sets.

Inference engine system: based on fuzzy rules, fuzzy inference system (FIS) is considered as decision-making. It handles how the rules are combined.

2.3.2. Defuzzifier. It transfers the output of the FIS system into a crisp value. In the defuzzification method, the centroid method is used to the transformation. The output of the FIS system, a nonfuzzy value, is called as a multicharacteristic performance index (MPCI).

In order to implement the FIS system, the Mamdani method is employed in the present paper. Subsequently, trapezoidal MFs are adopted for the inputs and outputs of the FIS so as to form fuzzy sets. MFs are in the range from zero to one, and MFs can describe the way a variable matches a fuzzy set. Inputs and outputs of fuzzification system are then transformed into linguistic variables. The trapezoidal MFs are defined as

$$\mu_A(x, k, l, m, p) = \begin{cases} \frac{(x-k)}{(l-k)}, & k \leq x \leq l, \\ 1, & l < x < p, \\ \frac{(x-m)}{(p-m)}, & p \leq x \leq m, \\ 0, & x \leq k \text{ or } m \leq x, \end{cases} \quad (5)$$

where μ_A denotes the MFs while $k, l, m,$ and p are parameters and x is a variable.

In this study, desirability of frequency and desirability of displacement are calculated, and then they are considered as two input variables for the FIS. These linguistic input variables will be combined into an output for the FIS. The trapezoidal MFs are employed for both the fuzzification and defuzzification. The following fuzzy rules are briefly described.

Fuzzy rule: if x_{1i} is A_1 and x_{2i} is B_{1i} , then y_i is C_i else ($i = 1, 2, 3, \dots, n$), where x_{1i} and x_{2i} are the two i th inputs and y_i is the i th output. $A_i, B_i,$ and C_i are defined by corresponding MFs ($\mu_{A_i}, \mu_{B_i},$ and μ_{C_i}), and these parameters are regarded as fuzzy subsets.

In order to compute the fuzzy logic reasoning, max-min operation of Mamdani is adopted. Subsequently, the FIS output is retrieved. The MFs of the FIS output can be described by

$$\mu_{ci}(y_i) = \max \left[\min \{ \mu_{A_{1i}}(x_1), \mu_{A_{2i}}(x_2), \dots, \mu_{A_{si}}(x_s) \} \right], \quad i = 1, 2, \dots, n. \quad (6)$$

At last, the FIS output is transformed into real values through the defuzzification. Subsequently, a nonfuzzy value y_0 , which is called as MPCI, is defined by

$$y_0 = \frac{\sum y_i \mu_{C_{0i}}(y_i)}{\sum \mu_{C_{0i}}(y_i)}. \quad (7)$$

Based on the theory of FIS system, the best solution for overall responses and a set of optimal design variables can be found by maximizing the MPCI index through the Taguchi method. This technique is divided into three types such as (i) higher-the-better, (ii) normal-the-best, and (iii) smaller-the-better. The larger-the-better type is chosen for maximizing the MPCI, which is described as

$$\eta = -10 \log \left(\frac{1}{n} \sum_{i=1}^n \frac{1}{\text{MPCI}_i^2} \right), \quad (8)$$

where MPCI_i is the i th MPCI index and n is the number i th experiment's repetition.

A Taguchi-based fuzzy logic can find optimal candidates in a MOO problem, but this approach may be a local optimum solution. The reason is because the Taguchi technique is employed to minimize or maximize a single fitness function in terms of discrete values. Meanwhile, a real problem desires to search a global optimum solution. In order to overcome such situation, ANFIS is then extended to model the MPCI, and the MOO design for the SRCM mechanism can be effectively solved by using the LAPO algorithm.

2.4. Phase 4: Adaptive Neuro-Fuzzy Inference System. As aforementioned, the FIS system is a modeling technique in terms of linguistic variables where the Mamdani method is used for the FIS. Meanwhile, ANFIS is an artificial technique which is developed by integrating neural network and the FIS. Nowadays, ANFIS is considered as an intelligent modeling which creates a connection between inputs and outputs. In theory of ANFIS, the Sugeno model is employed to create fuzzy rules [58]. The fuzzy rules for the ANFIS model can be defined as

$$\text{if } x_1 \text{ is } A_1 \text{ and } x_2 \text{ is } A_2, \quad \text{then } y = a \times x_1 + b \times x_2 + c, \quad (9)$$

where x_1 and x_2 are inputs with respect to A_1 and A_2 term sets, y is the output, and $a, b,$ and c are constant values.

Figure 2 illustrates the ANFIS structure which consists of five-layer feed-forward neural network.

Layer 1 is the fuzzification layer that assigns the membership degrees for input factors based on the given MFs. The output of layer 1 can be described as

$$M_1^i = \mu_{A_i}(x), \quad (10)$$

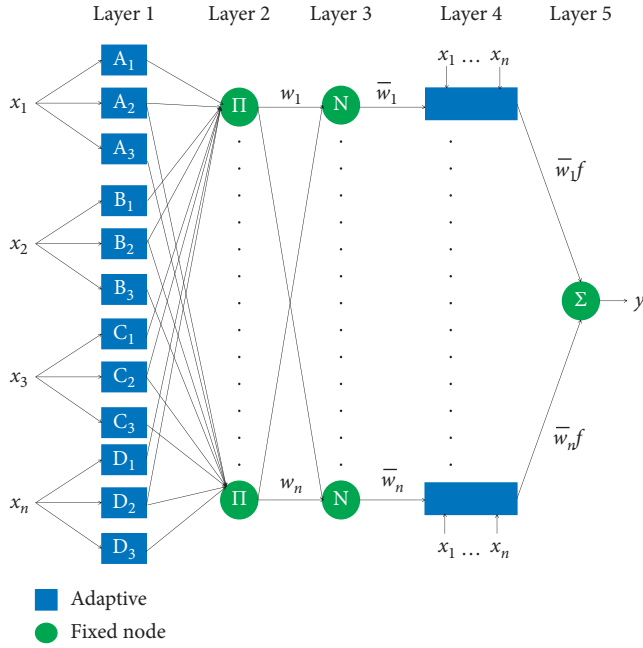


FIGURE 2: The proposed ANFIS system.

where x is the input with respect to node i th and A_i is a linguistic label. M_1^i is the MF of A_i .

Layer 2 includes the fuzzy rule and a rule node which gets inputs and identifies firing strength of the rule. Each node is labeled as a circle node, Π . Each node output can be defined as

$$w_i = \mu A_i(x) \times \mu A_i(y), \quad i = 1, 2, 3, \dots, n. \quad (11)$$

Layer 3 is a normalized layer which is used to estimate a ratio of firing strength of a given rule to total of firing strengths of all rules. Every node is labeled as a circle node, N . In this layer, \bar{w} is named for normalized firing strength of rules and defined as

$$\bar{w} = \frac{w_i}{w_1 + w_2 + w_3 + \dots + w_n}, \quad i = 1, 2, 3, \dots, n. \quad (12)$$

Layer 4 is the defuzzification process, and the i th node is labeled as square node by

$$M_1^i = \bar{w}_i f_i(ax + by, \dots, c), \quad i = 1, 2, 3, \dots, n. \quad (13)$$

Layer 5 is an overall output and sum of all signals, which is defined as

$$M_5^i = \sum_i \bar{w}_i f_i \frac{\sum_i w_i f_i}{w_i}. \quad (14)$$

In this article, the trapezoidal MFs are adopted for the ANFIS system as well.

2.5. Phase 5: Lightning Attachment Procedure Optimization Algorithm. LAPO is a new algorithm based on a physically lightning phenomena [59]. It is one of the most nontuned parameter algorithms. LAPO algorithm can solve a lot of different engineering problems, and it is superior to other

metaheuristic algorithms [60]. Therefore, this study adopts the LAPO algorithm to expand its application capacity for the MOO design for the bridge amplification compliant mechanism. Readers can find details in literatures [59, 60]. It consists of five substeps as follows.

Step 1. Initialization

The algorithm needs an initial population in a search space of design variables. Unlike previous studies, the present work evaluates and refines the search spaces in which a set of decision variables are defined based on statistical analysis. In the LAPO, some test points are assigned in the cloud and ground surface, which can be defined as

$$x_{\text{testpoint}}^i = x_{\text{min}}^i + (x_{\text{max}}^i - x_{\text{min}}^i) \times \text{rand}[0, 1], \quad (15)$$

where x_{min}^i and x_{max}^i denote the upper and lower bounds of design variables. Rank is a randomly given parameter in range from zero to one. Fitness of the solution is defined as

$$F_{\text{testpoint}}^i = \text{obj}(x_{\text{testpoint}}^i). \quad (16)$$

Step 2. Next jump determination

The average value of the overall test points and the value of fitness of the points are computed as in equations (17) and (18), respectively:

$$x_{\text{average}} = \text{mean}(x_{\text{testpoint}}), \quad (17)$$

$$f_{\text{average}} = \text{obj}(x_{\text{average}}), \quad (18)$$

where x_{average} and f_{average} denote the average value and value of fitness of the points.

If the electric field, fitness function, of potential point h is greater than the average value of the test points, it is calculated as

$$x_{\text{testpoint_new}}^i = x_{\text{testpoint}}^i + \text{rand}[0, 1] \times (x_{\text{average}} + \text{rand}[0, 1] \times (x_{\text{potential point}}^h)). \quad (19)$$

Otherwise, it is calculated as

$$x_{\text{testpoint_new}}^i = x_{\text{testpoint}}^i - \text{rand}[0, 1] \times (x_{\text{average}} + \text{rand}[0, 1] \times (x_{\text{potential point}}^h)). \quad (20)$$

Step 3. Branch fading

If the fitness function of new test point is better than the previous point, the branch sustains; otherwise, the branch fades as

$$\begin{cases} x_{\text{testpoint}}^i = x_{\text{testpoint_new}}^i, & f_{\text{testpoint_new}}^i < f_{\text{testpoint}}^i, \\ x_{\text{testpoint_new}}^i = x_{\text{testpoint}}^i, & \text{otherwise.} \end{cases} \quad (21)$$

This step is carried out for overall the test points so as to rest points moving down.

Step 4. Upward leader movement

Upward leader movement calculates an exponent factor based on the charge of downward leader as

$$S = 1 - \frac{\text{noi}}{\text{noi}_{\max}} \times \exp\left(-\frac{\text{noi}}{\text{noi}_{\max}}\right), \quad (22)$$

where noi and noi_{\max} denote a number of iterations and maximum number of iterations, respectively. The upward leaders are defined for the next strategy of test point as

$$x_{\text{testpoint_new}} = x_{\text{testpoint_new}} + \text{rand}[0, 1] \times S(x_{\min} - x_{\max}), \quad (23)$$

where x_{\min} and x_{\max} denote the best value and the worst solution of the population.

Step 5. Final jump

The process is ended when the upward leader meets the downward leader to each other. It is noted that the optimization process is ended if stop criterion is achieved. In addition, the maximum iteration is met, and the process is ended herein.

3. Case Studies: MOO Design for Scott Russell Compliant Mechanism

MOO design of the Scott Russell compliant mechanism is studied. This article considers three numerical examples, and the obtained results are to evaluate application's capability and effectiveness of the proposed hybrid computational method.

3.1. Structural Description and Problem Statement.

Figure 3 describes a structural design of the Scott Russell compliant mechanism (SRCM). Bottom end of the mechanism is fixed by screws, and top end is output. The mechanism is a type of bridge amplifier, but four bridge legs are alternated by using four Scott Russell mechanisms. The purpose of alternative is to enhance stiffness of traditional bridge mechanism. Each Scott Russell mechanism includes four flexure hinges and rigid links, as shown in Figure 3. The output, end effector, is at the middle rigid link. Based on symmetry, the end effector can move along the y -axis by exciting two input loads from a piezoelectric actuator. Based on this design, the mechanism can amplify a large working stroke along the y -direction, but its natural frequency is decreased. Another problem is how to ensure an enough working strength, i.e., a long fatigue working life without plastic failure. In a such situation, this study proposes a new optimal design methodology to resolve a balance between displacement and frequency. The main parameters of SRCM are illustrated, as given in Figures 3 and 4. In this article, AL T73-7075 material is chosen for the mechanism. In this structure, some parameters are design variables and others are constant values.

Table 1 gives geometrical factors and material properties of the proposed mechanism. According to the designer's experiences and expert's knowledge in the field, spaces of

design variables are determined based on a capacity of fabrication device.

The purpose of this study is to develop a new hybrid computational approach to deal with the MOO problem for compliant mechanisms. The SRCM is an application example. Numerical investigations are carried out to validate the proposed hybrid computational method. To address about the MOO problem for the SRCM, the design variables, objective functions, and constraints are firstly identified. According to the theory and investigations on compliant mechanisms [10, 61–64], geometry and locations of flexure hinges mainly contribute on the performances. As seen in Figures 3 and 4, the dimensional parameters are represented as a vector $\mathbf{X} = [\theta, L_0, L_1, L_2, L_3, L_4, L_5, L_6, D, T, R, H, L, W]^T$ in which the key design variables are affecting the performances, including $\theta, L_1, L_2, L_3, L_4,$ and D . Regarding objective functions and constraints, the SRCM is expected to achieve a fast speed, a large working space, and a good strength. In order to reach a desired speed, the first natural frequency of the SRCM must be improved accordingly. Meanwhile, a large displacement of the SRCM can help toward a large working stroke. At last, a good strength can be gained if the resulting equivalent stress of SRCM is under the yield strength of material [10, 61–64]. In addition, based on the experiences in designing and analyzing kinematics of compliant mechanisms, the mentioned parameters ($\theta, L_1, L_2, L_3, L_4,$ and D) are very sensitive to the performances. They can be chosen properly to improve the performances. The formulation of the optimization problem of the SRCM is briefly stated as follows.

Find vector of design variable: $\mathbf{X} = [\theta, L_1, L_2, L_3, L_4, D]^T$

$$\begin{aligned} &\text{Maximize } F_1(\mathbf{X}) \\ &\text{Maximize } F_2(\mathbf{X}). \end{aligned} \quad (24)$$

Subject to constraints:

$$F_3(\mathbf{X}) \leq \frac{\sigma_a}{SF}. \quad (25)$$

Initial space of design variables:

$$\left\{ \begin{array}{l} 12.5^\circ \leq \theta \leq 16.5^\circ, \\ 4.9 \text{ mm} \leq L_1 \leq 7.7 \text{ mm}, \\ 14.5 \text{ mm} \leq L_2 \leq 18.7 \text{ mm}, \\ 8.5 \text{ mm} \leq L_3 \leq 11.825 \text{ mm}, \\ 14 \text{ mm} \leq L_4 \leq 18.7 \text{ mm}, \\ 2.25 \text{ mm} \leq D \leq 3.5 \text{ mm}, \end{array} \right. \quad (26)$$

where $F_1(\mathbf{X}), F_2(\mathbf{X}),$ and $F_3(\mathbf{X})$ denote the frequency, displacement, and equivalent stress, respectively. σ_a is the yield stress of proposed AL T73-7075. Specifically, $F_1(\mathbf{X})$ and $F_2(\mathbf{X})$ are two objective functions, while $F_3(\mathbf{X})$ is regarded as the constraint. SF is the safety factor that is chosen as 1.5.

3.2. Numerical Simulation. A 3D FEM model is created, and numerical experiments are formulated via the CCD. Numerical data are then collected by implementing FEA simulations. The boundary conditions and loads are given

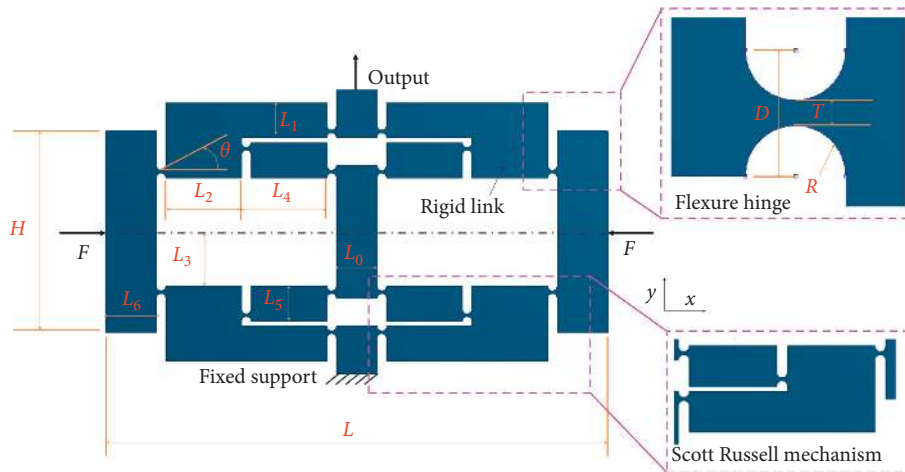


FIGURE 3: Schematics of the Scott Russell compliant mechanism.

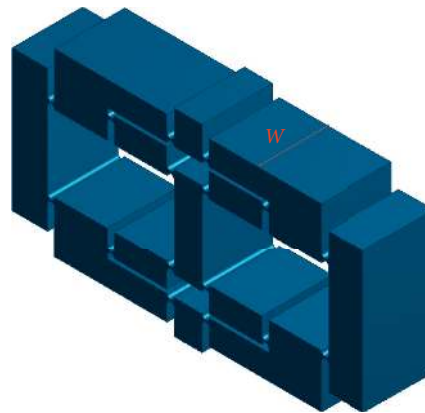


FIGURE 4: 3D model of the Scott Russell compliant mechanism (unit: mm).

TABLE 1: Design parameters and material properties of the SRCM mechanism.

Parameter	Symbol	Value
Incline angle	θ	$12.5^\circ \leq \theta \leq 16.5^\circ$
Width of rigid link 1	L_1	$4.9 \text{ mm} \leq L_1 \leq 7.7 \text{ mm}$
Length of segment 1	L_2	$14.5 \text{ mm} \leq L_2 \leq 18.7 \text{ mm}$
Distance from actuator to rigid link	L_3	$8.5 \text{ mm} \leq L_3 \leq 11.825 \text{ mm}$
Length of segment 2	L_4	$14 \text{ mm} \leq L_4 \leq 18.7 \text{ mm}$
Distance between circle's centers	D	$2.25 \text{ mm} \leq D \leq 3.5 \text{ mm}$
Width of shuttle link	L_0	8 mm
Width of rigid link 2	L_5	7 mm
Width of input link	L_6	10 mm
Radius of flexure hinge	R	1 mm
Thickness of flexure hinge	T	(D-R) mm
Width of the mechanism	W	10 mm
Height of the mechanism	H	40 mm
Length of the mechanism	L	100 mm
Total size of the mechanism	S	$100 * 40 * 10 \text{ mm}^3$
Mechanical properties of Al T73-7075		
Density		2810 kg/m ³
Young's modulus		71700 MPa
Yield strength		503 MPa
Poisson's ratio		0.33

from Figure 3. A force, F , of 70 N is applied toward an end of inputs, and the output response is measured. Automatic technique is utilized for meshing. Meshing of flexure hinges is refined again in order to achieve accurate analysis, as shown in Figure 5. The meshing results give a number of elements of 1544 and a number of nodes of 9897. Skewness criteria, metric performance, are used to evaluate the quality of meshing. Its value is in the range from zero to one. The results found that the average value of skewness is approximately 0.3745, as given in Figure 6. On the contrary, this value guarantees the quality of meshing is a relatively good result.

4. Results and Discussion

4.1. Sensitivity Investigation and Refinement of Design Variables. The CCD is utilized to build the numerical matrix by using space of all initial design variables. And then, the most critical important parameters and suppress nonsignificant parameters are identified. Secondly, this analysis refines space of design variables prior to implement the MOO problem of proposed mechanism. In this article, six factors are divided into three levels, as given in Table 2. Each numerical experiment retrieves two quality specifications and one constraint, including natural frequency ($F_1(\mathbf{X})$ —Hz), displacement ($F_2(\mathbf{X})$ —mm), and equivalent stress ($F_3(\mathbf{X})$ —MPa). Forty-five experiments are generated, and the numerical results are given, as in Table 3.

As mentioned above, this article considers displacement, frequency, and stress for MOO design of the Scott Russell compliant mechanism. Geometrical parameters directly affecting those specifications are identified and may be suppressed for further optimization process. Sensitivity investigation of design variables with respect to the three specifications is analyzed, individually. In this study, analysis of variance and Taguchi approach are used and implemented by using Minitab software 18.

Case 1, considering the displacement, ANOVA is utilized to analysis of sensitivity at 95% confidence interval. The result of ANOVA in Table 4 found that the contribution of parameters θ (the-ta), L_1 , and L_2 on this quality response is about 0.03%, 0.02%, and 0.01%, respectively. These contributions are too small compared to remaining parameters. It means that the contributions of θ , L_1 , and L_2 can be ignored in further modeling and optimization process. In addition, the Taguchi method with the larger-the-better type is used for the displacement, as shown in Figure 7. The results also found that factors θ , L_1 , and L_2 are also two nonsignificant factors because the displacement is a little change when those parameters are varied. Meanwhile, other parameters are very sensitive to the displacement which are taken as key variables for case study 1.

Considering the frequency, the ANOVA results in Table 5 reveal that parameters L_3 and L_4 have a lowest contribution on the displacement with respect to 0.09% and 0.22%, respectively. As a result, these two factors are nonsignificant variables that can be neglected in modeling and optimization process for case study 2.

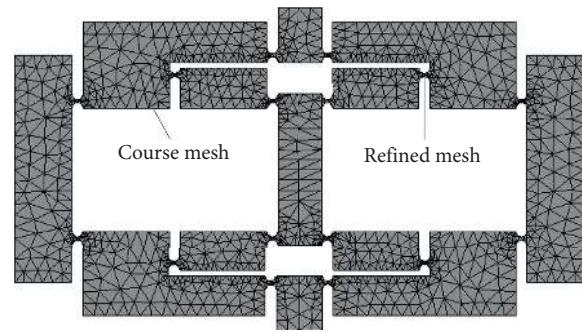


FIGURE 5: Meshing model of Scott Russell compliant mechanism.

Figure 8 describes the sensitivity of full variables on the frequency via using the Taguchi method with the larger-the-better type. It also notes that the parameters L_3 and L_4 have a very small influence on this response compared to other parameters. On the contrary, if these parameters are varied, the frequency is somehow changed. Meanwhile, a change in the other parameters has a sharp change.

Case 3 considers the equivalent stress, and the ANOVA results in Table 6 indicate that three parameters θ , L_2 , and L_4 have the lowest contribution on the stress with 0% contribution. These three factors are nonsignificant and can be suppressed in further modeling and the MOO process. A smaller-the-better type is utilized for the stress. The results of the Taguchi analysis show that three parameters also have a very small contribution on the stress response, as shown in Figure 9.

4.2. Optimization Implementation

4.2.1. Selection of Membership Functions. Each real value of physical response is transformed into linguistic variables which are assigned for the fuzzy reasoning inference process. The linguistic variables are determined based on expert's knowledge and designer's institution. Table 7 gives the linguistic variables, including tiny, very small, small, small-medium, medium, medium-large, large, very large, and huge.

In this article, two inputs of FIS structure consist of desirability of frequency and desirability of displacement. The MFs for desirability of frequency are divided into three levels such as small, medium, and large, as illustrated in Figure 10(a). Meanwhile, the MFs of the desirability of displacement are separated into seven levels, including tiny, very small, small-medium, medium, medium-large, large, very large, and huge, as depicted in Figure 10(b). At last, the MFs of the output MPCFI also include seven levels, as shown in Figure 11. All the MFs are defined by trapezoidal shape because this is a popular MF type for both the FIS and ANFIS models.

The results of sensitivity analysis are used to decrease space of design variables. Through this analysis, computational time is lowered and reliable solution is increased. Particularly, some parameters may be redundant, while others are critically important factors. Based on the sensitivity results, initial design variables are eliminated. From

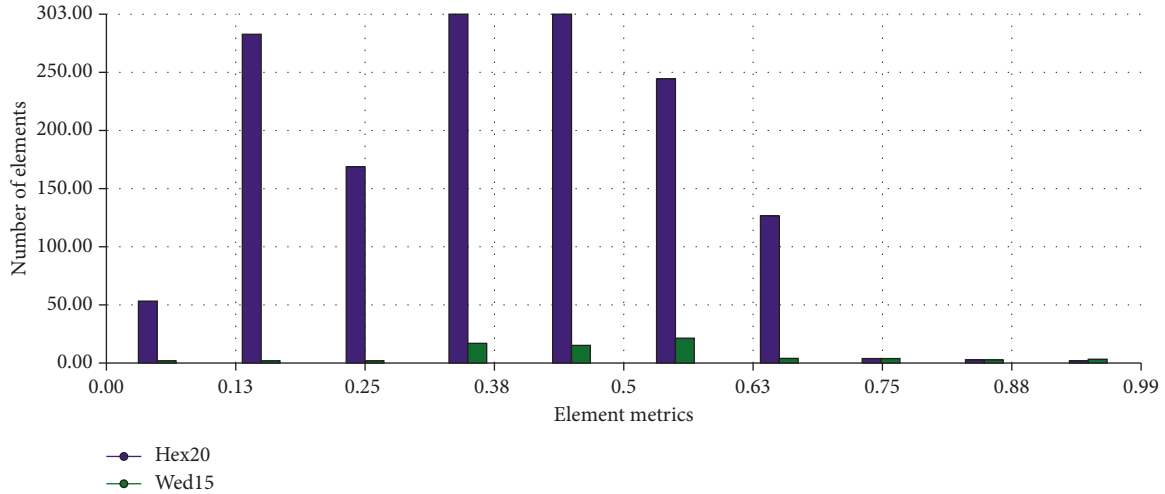


FIGURE 6: Quality distribution of meshing elements by skewness criteria.

TABLE 2: Level of design variables.

Symbol	Value	Level 1	Level 2	Level 3
θ	$12.5^\circ \leq \theta \leq 16.5^\circ$	12.5	14.5	16.5
L_1	$4.9 \text{ mm} \leq L_1 \leq 7.7 \text{ mm}$	4.9	6.3	7.7
L_2	$14.5 \text{ mm} \leq L_2 \leq 18.7 \text{ mm}$	14.5	16.6	18.7
L_3	$8.5 \text{ mm} \leq L_3 \leq 11.825 \text{ mm}$	8.5	10.1625	11.825
L_4	$14 \text{ mm} \leq L_4 \leq 18.7 \text{ mm}$	14	16.35	18.7
D	$2.25 \text{ mm} \leq D \leq 3.5 \text{ mm}$	2.25	2.825	3.5

that, three following numerical examples are considered to evaluate the performance effectiveness of proposed computational methodology.

If full initial space is used, it may take a long time to search for optimum solutions. Therefore, this study limits design space and following case studies are separated to investigate and evaluate the efficiency of the proposed hybrid approach.

4.2.2. Case Study 1. By using the results of sensitivity analysis in Table 4 and Figure 7, some nonsignificant factors are suppressed since their influences are very small on the displacement. Real influencing factors with large contributions are taken in account as key design variables. Case study 1 takes two objective functions to be optimized simultaneously with the spaces of design variables being relatively reduced. In order to solve the MOO problem, the desirability of displacement and the desirability of frequency are transformed into a single combined objective function, which is called as the MPCFI of the FIS system. Subsequently, the MPCFI is maximized by using the proposed hybrid approach. The optimization problem of case study 1 is stated as follows.

Find vector of design variable: $\mathbf{X} = [D, L_3, L_4]^T$:

$$\text{Maximize MPCFI}(\mathbf{X})_{\text{case study 1}} \quad (27)$$

s.t.

$$\left\{ \begin{array}{l} F_3(\mathbf{X}) \leq \frac{\sigma_a}{SF}, \\ 2.25 \text{ mm} \leq D \leq 3.5 \text{ mm}, \\ 8.5 \text{ mm} \leq L_3 \leq 11.825 \text{ mm}, \\ 14 \text{ mm} \leq L_4 \leq 18.7 \text{ mm}. \end{array} \right. \quad (28)$$

Case study 1 evaluates three design variables (D , L_2 , and L_1) and two objective functions and one constraint. Such design variables and both responses are set as parametric variables in the FE model. Based on the number of design variables and their levels, CCD is used again to build 15 experiments. The results of frequency, displacement, and equivalent stress are collected, simultaneously.

Next, desirability of frequency and desirability of displacement are calculated, as given in Table 8. Real values of two responses have different units, and it is a main cause resulting in unprecise solutions. Therefore, desirability function approach is proposed to overcome this limitation because desirability has no unit and its value is from zero to one. The results found all stress values are satisfied in terms of allowable stress of material.

In order to conduct the MOO problem for case study 1, the MFs for desirability of frequency include three levels and the desirability of displacement is divided into seven levels, while the MFs of fuzzy MPCFI output are separated into seven levels, as given in Table 9. Subsequently, matrix of fuzzy rules is built in this table.

In this study, center of gravity method is employed for defuzzification and Mamdani method is utilized for fuzzy operation. The FIS is implemented in Matlab R2015a. Figure 12 illustrates a relation of the fuzzy MPCFI with the

TABLE 3: Initially numerical results: frequency, displacement, and equivalent stress.

No.	Design variables						Frequency $F_1(X)$ (Hz)	Displacement $F_2(X)$ (mm)	Stress $F_3(X)$ (MPa)
	θ (degree)	L_1 (mm)	L_2 (mm)	L_3 (mm)	L_4 (mm)	D (mm)			
1	14.5	6.3	16.6	10.1625	16.35	2.875	144.8765116	0.0131662	20.2101534
2	12.5	6.3	16.6	10.1625	16.35	2.875	145.6511486	0.0100512	17.3713011
3	16.5	6.3	16.6	10.1625	16.35	2.875	142.7061870	0.0124471	21.6504283
4	14.5	4.9	16.6	10.1625	16.35	2.875	144.5375979	0.0111032	19.3343769
5	14.5	7.7	16.6	10.1625	16.35	2.875	147.0998526	0.0101186	22.7858141
6	14.5	6.3	14.5	10.1625	16.35	2.875	153.7702955	0.0089541	14.8769691
7	14.5	6.3	18.7	10.1625	16.35	2.875	138.4140708	0.0104084	18.2311317
8	14.5	6.3	16.6	10.1625	16.35	2.25	29.1033323	0.2783916	413.3649425
9	14.5	6.3	16.6	10.1625	16.35	3.5	247.7177837	0.0042301	9.1823943
10	14.5	6.3	16.6	8.5	16.35	2.875	151.3503923	0.0132612	20.5864700
11	14.5	6.3	16.6	11.825	16.35	2.875	139.8224967	0.0132187	19.7278662
12	14.5	6.3	16.6	10.1625	14	2.875	158.4167103	0.0106565	18.8481276
13	14.5	6.3	16.6	10.1625	18.7	2.875	137.7014871	0.0139512	19.6035371
14	12.5	4.9	14.5	8.5	14	2.25	35.2827371	0.0126286	41.9016251
15	16.5	4.9	14.5	8.5	18.7	2.25	29.7282702	0.0319123	68.4134201
16	12.5	7.7	14.5	8.5	18.7	2.25	30.3150364	0.0440975	83.1659146
17	16.5	7.7	14.5	8.5	14	2.25	35.2125256	0.0541169	118.3677978
18	12.5	4.9	18.7	8.5	18.7	2.25	26.5880362	0.0605043	110.0556179
19	16.5	4.9	18.7	8.5	14	2.25	30.2587478	0.0314902	81.1699723
20	12.5	7.7	18.7	8.5	14	2.25	31.1153254	0.0262748	63.8299904
21	16.5	7.7	18.7	8.5	18.7	2.25	661.0920453	0.0000156	8.3148176
22	12.5	4.9	14.5	8.5	18.7	3.5	236.4448793	0.0020741	7.3108765
23	16.5	4.9	14.5	8.5	14	3.5	284.3688928	0.0034154	11.4796060
24	12.5	7.7	14.5	8.5	14	3.5	296.0385722	0.0028695	10.0679057
25	16.5	7.7	14.5	8.5	18.7	3.5	722.6186705	0.0000161	2.3844190
26	12.5	4.9	18.7	8.5	14	3.5	249.2833206	0.0037318	9.8955675
27	16.5	4.9	18.7	8.5	18.7	3.5	216.1175651	0.0056673	10.8787519
28	12.5	7.7	18.7	8.5	18.7	3.5	660.5761253	0.0000153	2.4110693
29	16.5	7.7	18.7	8.5	14	3.5	723.9722661	0.0000184	2.3225403
30	12.5	4.9	14.5	11.825	18.7	2.25	26.7029456	0.0095992	28.5990240
31	16.5	4.9	14.5	11.825	14	2.25	32.3612774	0.0773006	175.6411982
32	12.5	7.7	14.5	11.825	14	2.25	33.5994617	0.0998207	203.6469876
33	16.5	7.7	14.5	11.825	18.7	2.25	26.4888400	0.2497774	343.3155557
34	12.5	4.9	18.7	11.825	14	2.25	28.9826859	0.2040589	377.6240900
35	16.5	4.9	18.7	11.825	18.7	2.25	22.7266747	0.1692049	257.2457599
36	12.5	7.7	18.7	11.825	18.7	2.25	23.4218271	0.1117737	173.0523059
37	16.5	7.7	18.7	11.825	14	2.25	671.0395540	0.0000197	8.0316806
38	12.5	4.9	14.5	11.825	14	3.5	254.0503542	0.0020926	8.4557853
39	16.5	4.9	14.5	11.825	18.7	3.5	222.0867129	0.0038711	11.9575653
40	12.5	7.7	14.5	11.825	18.7	3.5	226.4134777	0.0034449	8.6649529
41	16.5	7.7	14.5	11.825	14	3.5	728.8362254	0.0000215	2.0182197
42	12.5	4.9	18.7	11.825	18.7	3.5	200.9526441	0.0042152	10.8241011
43	16.5	4.9	18.7	11.825	14	3.5	237.2856932	0.0032948	10.7328140
44	12.5	7.7	18.7	11.825	14	3.5	668.7600073	0.0000200	1.9910749
45	16.5	7.7	18.7	11.825	18.7	3.5	610.9395221	0.0000201	2.3080380

TABLE 4: ANOVA results for the displacement.

Source	DF	Seq. SS	Adj. SS	Adj. MS	Contribution (%)
Model	6	0.073316	0.073316	0.012219	38.01
Linear	6	0.073316	0.073316	0.012219	38.01
θ	1	0.000060	0.000060	0.000060	0.03
L_1	1	0.000033	0.000033	0.000033	0.02
L_2	1	0.000018	0.000018	0.000018	0.01
L_3	1	0.012798	0.012798	0.012798	6.64
L_4	1	0.000935	0.000935	0.000935	0.48
D	1	0.059470	0.059470	0.059470	30.83
Error	38	0.119565	0.119565	0.003146	61.99
Total	44	0.192880			100.00

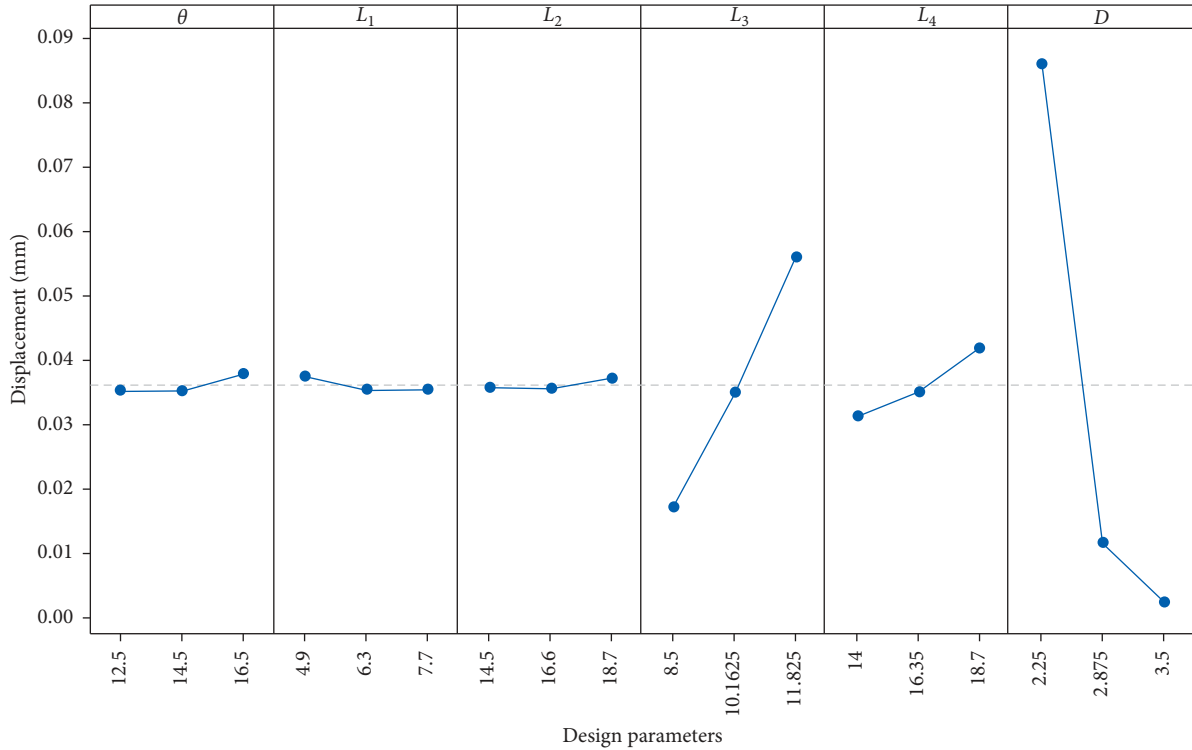


FIGURE 7: Effect plot of design variables on the displacement.

TABLE 5: ANOVA results for the frequency.

Source	DF	Seq. SS	Adj. SS	Adj. MS	Contribution (%)
Model	6	1465058	1465058	244176	62.89
Linear	6	1465058	1465058	244176	62.89
Θ	1	145431	145431	145431	6.24
L_1	1	475254	475254	475254	20.40
L_2	1	98197	98197	98197	4.22
L_3	1	2079	2079	2079	0.09
L_4	1	5138	5138	5138	0.22
D	1	738958	738958	738958	31.72
Error	38	864635	864635	22754	37.11
Total	44	2329692			100.00

desirability of displacement and desirability of frequency. The value of inputs and outputs of the FIS is in range from zero to one. In this study, the weight of each rule is assumed to be unity.

Based on 27 fuzzy rules in Table 9, the output of FIS system is computed, as shown in Figure 13.

The results of MPCFI output are determined with respect to each value of desirability of frequency and desirability of displacement, as given in Table 10.

By taking the values of design variables in Table 8 and the MPCFI value in Table 10, a proper ANFIS model is developed for modeling the MPCFI. Modeling is coded in Matlab. The results of ANFIS parameters are given in Table 11. In this study, 75% of data and the remaining 25% of data are utilized for the training and testing, respectively.

In order to evaluate the built ANFIS model, some performances metrics are employed, such as mean absolute

percentage error (MAPE), root mean square error (RMSE), and correlation coefficient (R^2) [18, 65]. Mathematical equations of MAPE, RMSE, and R^2 are described by

$$\text{MAPE} = \frac{100\%}{n} \sum_{i=1}^n \left| \frac{y_i - \hat{y}_i}{y_i} \right|, \quad (29)$$

$$\text{RMSE} = \sqrt{\frac{1}{n} \sum_{i=1}^n (y_i - \hat{y}_i)^2}, \quad (30)$$

$$R^2 = 1 - \frac{\sum_{i=1}^n (y_i - \hat{y}_i)^2}{\sum_{i=1}^n (y_i - \bar{y})^2}, \quad (31)$$

where y_i is the i th of the measured result, \hat{y}_i is the i th of the predicted result, \bar{y} is the mean value of measured results, and n is the number of observations.

As the discussion in Section 3.1, a high frequency, a large displacement, and a minimal stress are desired simultaneously. According to the fuzzy logic theory [30], the largest value of the MPCFI is expected to achieve the optimal solution. In other words, the MPCFI must be maximized so as to achieve a global optimal solution for the SRCM. The results found that the MAPE and RMSE are close to zero, while R^2 reaches one. It means that the built ANFIS model is relatively good. In order to evaluate the effectiveness and robustness of the proposed hybrid approach, the optimal results are compared with those obtained from a traditional combination of the Taguchi method and fuzzy logic (TMFL), and the optimal parameters from the TMFL are determined at

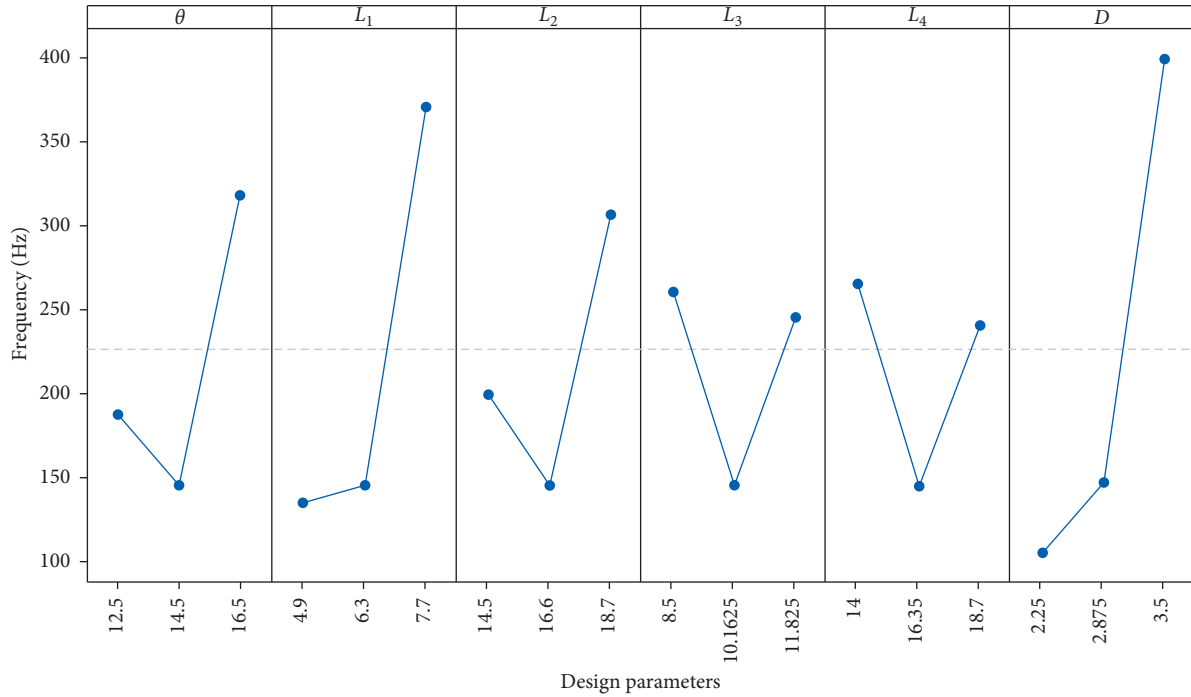


FIGURE 8: Effect plot of design variables on the frequency.

TABLE 6: ANOVA results for the equivalent stress.

Source	DF	Seq. SS	Adj. SS	Adj. MS	Contribution (%)
Model	6	204005	204005	34001	43.37
Linear	6	204005	204005	34001	43.37
Θ	1	15	15	15	0.00
L_1	1	1005	1005	1005	0.21
L_2	1	2	2	2	0.00
L_3	1	28901	28901	28901	6.14
L_4	1	0	0	0	0.00
D	1	174082	174082	174082	37.01
Error	38	266343	266343	7009	56.63
Total	44	470348			100.00

$D = 2.25$ mm, $L_3 = 8.5$ mm, and $L_4 = 18.7$ mm, as given in Table 12. The optimal results of TMFL find that the frequency and displacement are approximately 24.4574 Hz and 0.1691 mm with a small equivalent stress of 251 MPa, respectively. It also ensures a high safety factor. However, these optimal values are found at discrete points according to theory of the Taguchi approach. Such points can lead to local optimum solutions. To overcome this limitation, LAPO algorithm is used to search a global optimum solution. Based on the established ANFIS modeling, a pseudoobjective function of MPCl is well established. And then, a LAPO programming is implemented in Matlab R2019b, and the results of the proposed approach found that the optimal design parameters are at $D = 2.30$ mm, $L_3 = 8.5$ mm, and $L_4 = 18.7$ mm. By using proposed methodology, the optimal solutions find the frequency and displacement are about 26.592 Hz and 0.1539 mm, respectively. The equivalent stress is also lower than the yield strength of Al material. It permits a good enough working condition with a safety factor of

1.98. Moreover, the MPCl predicted from the TMFL is smaller than that predicted from the proposed hybrid methodology. According to a larger-the-better value is best for the MPCl, the proposed approach is efficient, robust, and better than the TMFL. The optimal results are satisfied with initial requirements.

4.2.3. Case Study 2. Based on the results of sensitivity analysis in Table 5 and Figure 8, some unimportant factors are neglected in modeling and optimization problem. The factors with actual contributions are considered as key design variables. The space of design parameters is decreased, accordingly. Similarly, case study 2 also maximizes $F_1(\mathbf{X})$ and maximizes $F_2(\mathbf{X})$, simultaneously. Two objective functions are transferred into desirability values and then transformed to the MPCl value. The optimization problem is briefly expressed as below.

Find design variable $\mathbf{X} = [\theta, L_1, L_2, D]^T$:

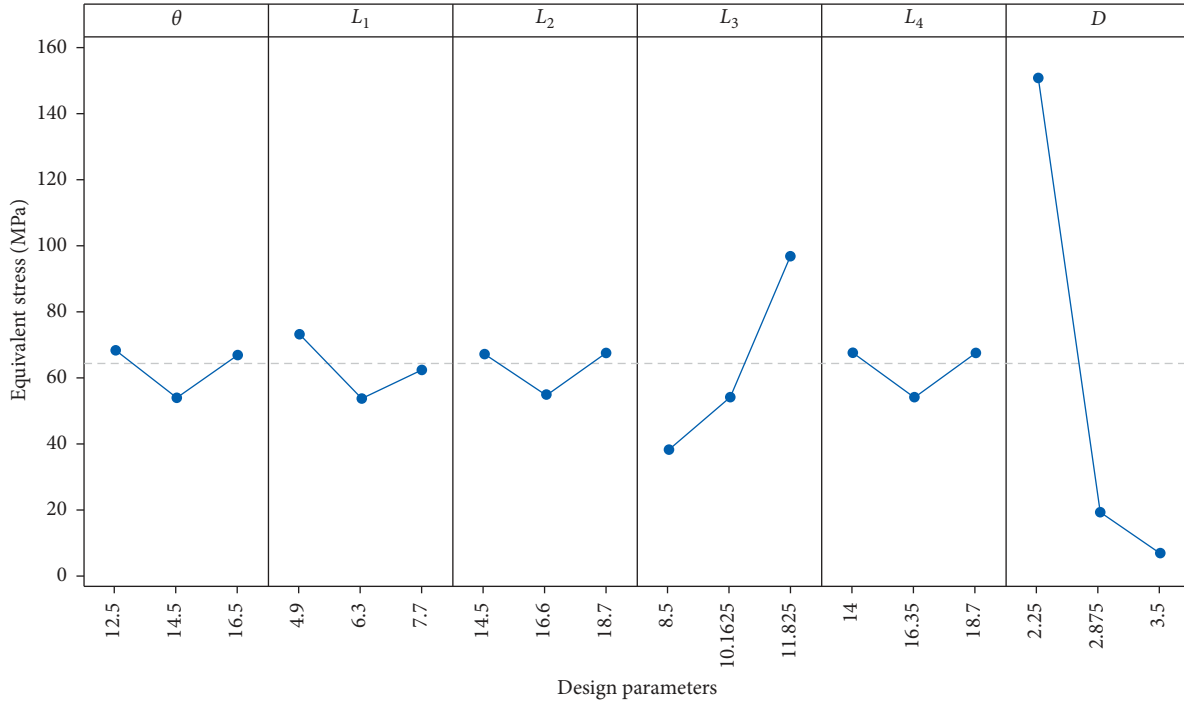


FIGURE 9: Effect plot of design variables on the stress.

TABLE 7: Linguistic variables for the fuzzy reasoning process.

Symbol	T	VS	S	SM	M	ML	L	VL	H
Linguistic variables	Tiny	Very small	Small	Small-medium	Medium	Medium-large	Large	Very large	Huge

$$\text{Maximize MPCl}(\mathbf{X})_{\text{case study 2}} \quad (32)$$

s.t.

$$\left\{ \begin{array}{l} F_3(\mathbf{X}) \leq \frac{\sigma_a}{SF}, \\ 12.5^\circ \leq \theta \leq 16.5^\circ, \\ 4.9 \text{ mm} \leq L_1 \leq 7.7 \text{ mm}, \\ 14.5 \text{ mm} \leq L_2 \leq 18.7 \text{ mm}, \\ 2.25 \text{ mm} \leq D \leq 3.5 \text{ mm}. \end{array} \right. \quad (33)$$

Case study 2 considers two design variables and two objective functions and three constraints. CCD is also used to build 25 numerical experiments. The results of frequency, displacement, and equivalent stress are collected by simulations. And then, desirability of displacement and desirability of frequency are calculated, as given in Table 13. The resulting stress values are under the allowable stress of Al T73-7075.

Next, the MFs for desirability of frequency also are divided into three levels, and the desirability of displacement is seven levels, while the MFs of fuzzy MPCl output are separated into seven levels, as given in Table 9. Subsequently, matrix of fuzzy rules is built in Table 14.

The results of MPCl output are calculated corresponding to the desirability two responses, as given in Table 15.

By taking the values of design variables in Table 13 and the MPCl value of Table 15, ANFIS model is formed for modeling the MPCl. The ANFIS parameters for case study 2 are developed, as given in Table 16. The predicting accuracy of the ANFIS model is well evaluated through equations (29) and (31) before conducting the MOO problem for the SRCM.

By using the TMFL, the optimal parameters are determined at $\theta = 16.5^\circ$, $L_1 = 7.7$ mm, $L_2 = 18.7$ mm, and $D = 2.25$ mm, as given in Table 17. Based on the TMFL, the optimal frequency and displacement are found at 28.94823 Hz and 0.1527 mm, respectively. Subsequently, LAPO algorithm is used to search a global optimum value. The results of the proposed hybrid approach determined that the optimal design parameters are $\theta = 16.5^\circ$, $L_1 = 8.0$ mm, $L_2 = 14.5$ mm, and $D = 2.25$ mm. Using the proposed methodology, the optimal results found that the frequency and displacement are about 651 Hz and 0.1981 mm, respectively. Finally, the predicted MPCl from the proposed approach is greater than that predicted from the TMFL. It means that the estimated solution from the proposed methodology is robust and better than that from the TMFL. Moreover, it finds that the equivalent stress is under the allowable stress of Al T73-7075. The optimal results are satisfied with design constraints.

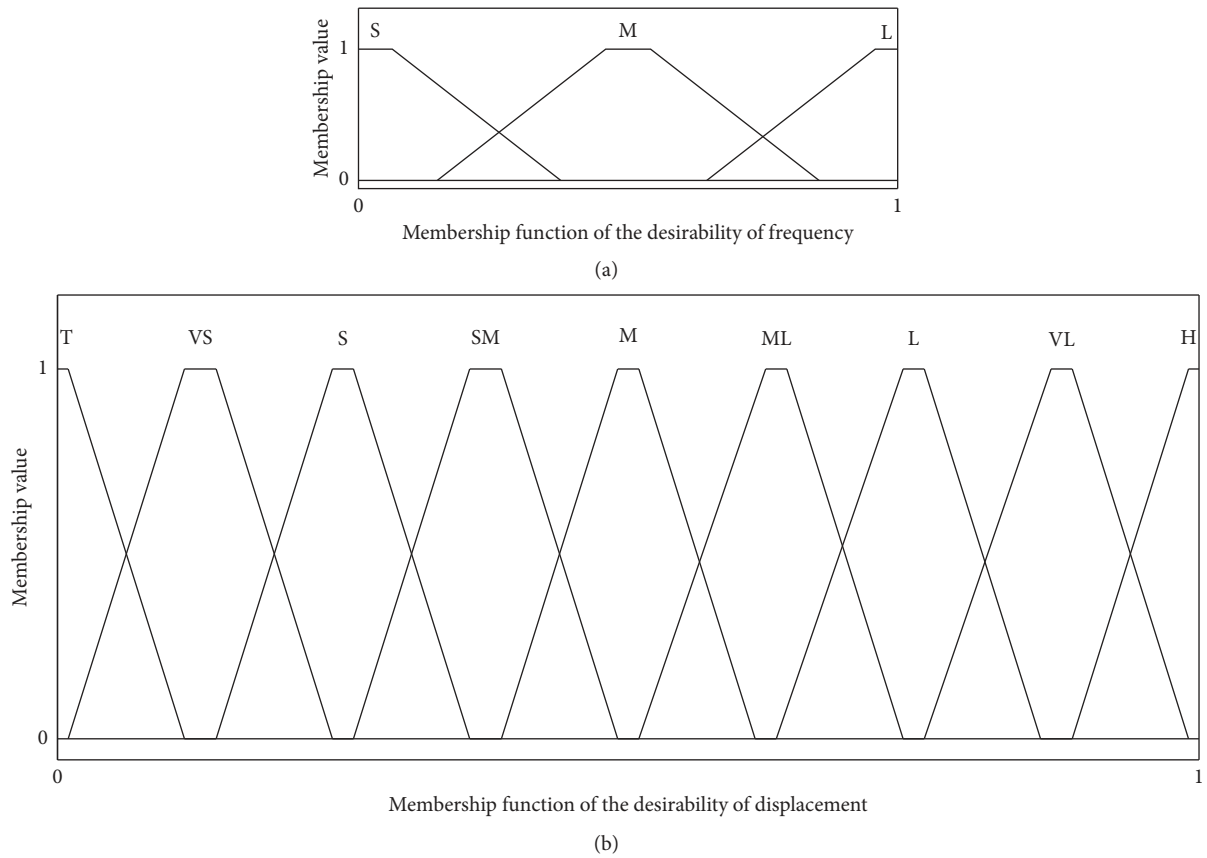


FIGURE 10: Membership functions plot: (a) frequency; (b) displacement.

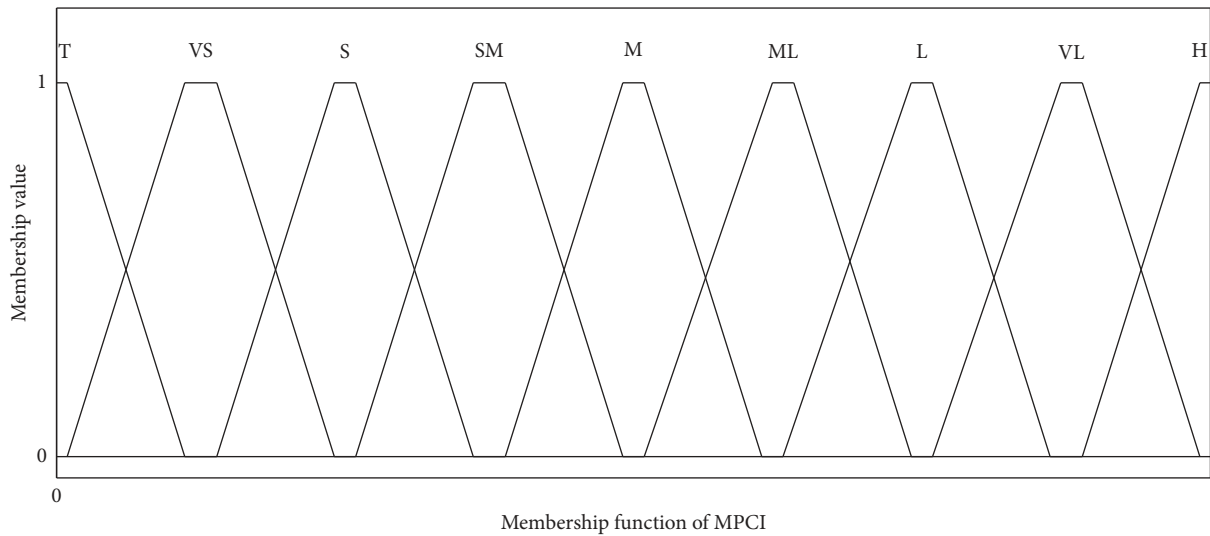


FIGURE 11: Membership functions plot for the MPCl.

4.2.4. Case Study 3. Based on the results of sensitivity analysis in Table 6 and Figure 9, the space of design variables is relatively shortened. Case study 3 also simultaneously

maximizes $F_1(\mathbf{X})$ and maximizes $F_2(\mathbf{X})$. The computational principle is similar to previous cases. The statement of optimization is stated as follows.

TABLE 8: Desirability results of the case study 1.

No.	Design variables (unit: mm)			Frequency	Frequency	Stress	Desirability of $F_1(X)$	Desirability of $F_2(X)$
	D	L_3	L_4	$F_1(X)$ (Hz)	$F_2(X)$ (mm)	$F_3(X)$ (MPa)	D_1	D_2
1	2.875	10.1625	16.35	145.7347	0.010851	18.4667631	0.167540611	0.032475676
2	2.25	10.1625	16.35	27.81286	0.079585	147.3155439	0.004206109	0.51031939
3	3.5	10.1625	16.35	684.6259	1.93E-05	2.059713964	0.91132379	0
4	2.875	8.5	16.35	152.266	0.010928	17.72299244	0.186110214	0.065979996
5	2.875	11.825	16.35	139.8676	0.010781	18.28006101	0.149565911	0.067869119
6	2.875	10.1625	14	156.5233	0.007468	16.80767677	0.190016733	0
7	2.875	10.1625	18.7	136.4378	0.01453	23.57711698	0.146800947	0.230293298
8	2.25	8.5	14	32.2812	0.036407	85.94278072	0.008724268	0.218602991
9	3.5	8.5	14	749.2335	1.84E-05	2.584933531	0.993446922	0.051737375
10	2.25	11.825	14	29.85823	0.036103	84.18491871	0.006099755	0.219639916
11	3.5	11.825	14	685.0373	2.24E-05	2.116902014	0.91388315	0.047684449
12	2.25	8.5	18.7	26.21778	0.178381	262.0338394	9.3986E-05	0.93699663
13	3.5	8.5	18.7	680.4317	1.69E-05	2.38866496	0.906545952	0
14	2.25	11.825	18.7	24.3866	0.18053	265.9814502	0.006569152	0.9448278
15	3.5	11.825	18.7	628.8354	2.03E-05	2.115335728	0.836081859	0

TABLE 9: Fuzzy rules matrix for case 1.

No.	Desirability for $F_1(X)$	Desirability for $F_2(X)$	MPCI
1	S	T	T
2	M	T	VS
3	L	T	S
4	S	VS	VS
5	M	VS	S
6	L	VS	SM
7	S	S	S
8	M	S	SM
9	L	S	ML
10	S	SM	S
11	M	SM	SM
12	L	SM	M
13	S	M	SM
14	M	M	M
15	L	M	ML
16	S	ML	SM
17	M	ML	M
18	L	ML	ML
19	S	L	ML
20	M	L	ML
21	L	L	L
22	S	VL	ML
23	M	VL	L
24	L	VL	VL
25	S	H	ML
26	M	H	L
27	L	H	H

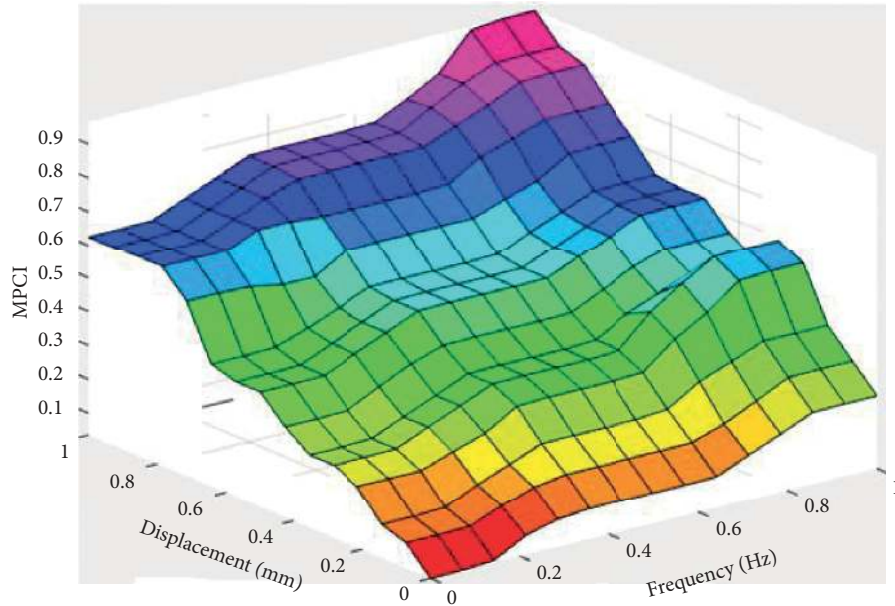


FIGURE 12: Plot of input vs. output in the FIS system.

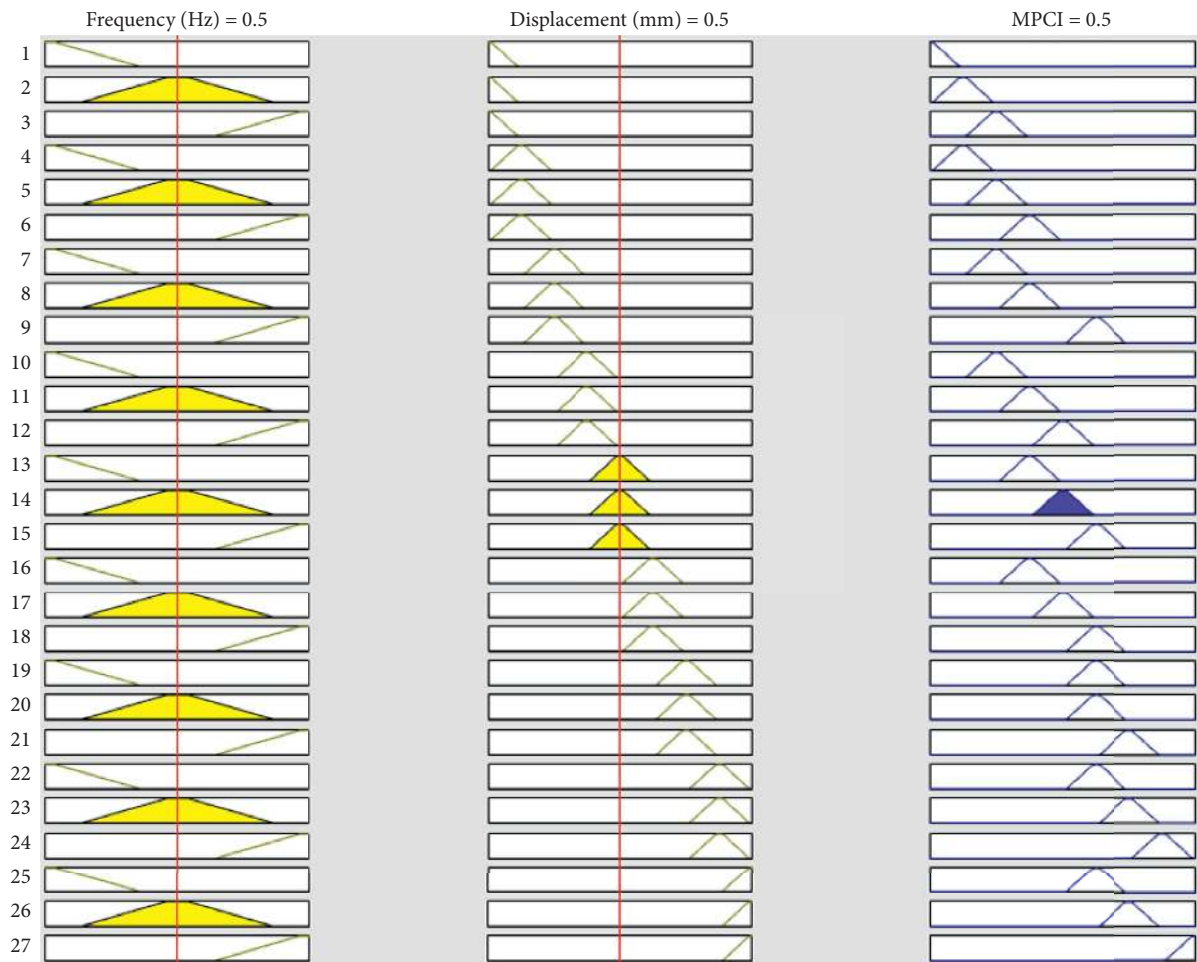


FIGURE 13: Twenty-seven fuzzy rules.

TABLE 10: Results of fuzzy MPCl for case 1.

No.	Desirability of $F_1(X)$	Desirability of $F_2(X)$	MPCl
1	0.167540611	0.032475676	0.107
2	0.004206109	0.51031939	0.375
3	0.91132379	0	0.25
4	0.186110214	0.065979996	0.133
5	0.149565911	0.067869119	0.114
6	0.190016733	0	0.0779
7	0.146800947	0.230293298	0.24
8	0.008724268	0.218602991	0.222
9	0.993446922	0.051737375	0.301
10	0.006099755	0.219639916	0.223
11	0.91388315	0.047684449	0.297
12	9.3986E-05	0.93699663	0.625
13	0.906545952	0	0.25
14	0.006569152	0.9448278	0.625
15	0.836081859	0	0.235

TABLE 11: ANFIS parameters for case 1.

Number of nodes	78
Number of linear parameters	108
Number of nonlinear parameters	27
Total number of parameters	135
Number of training data pairs	15
Number of testing data pairs	0
Number of fuzzy rules	27

Find design variable $\mathbf{X} = [L_1, L_3, D]^T$:

$$\text{Maximize MPCl}(\mathbf{X})_{\text{case study 3}} \tag{34}$$

s.t.

$$\left\{ \begin{array}{l} F_3(\mathbf{X}) \leq \frac{\sigma_a}{SF}, \\ 4.9 \text{ mm} \leq L_1 \leq 7.7 \text{ mm}, \\ 8.5 \text{ mm} \leq L_3 \leq 11.825 \text{ mm}, \\ 2.25 \text{ mm} \leq D \leq 3.5 \text{ mm}. \end{array} \right. \tag{35}$$

Case study 3 regards three design variables and two objective functions and one constraint. CCD is used to build 15 numerical experiments. The results of frequency, displacement, and equivalent stress are collected. And then, desirability of two responses is calculated, as given in Table 18. The results found all stress values are smaller than the allowable stress of the proposed material.

The MFs for desirability of frequency include three levels, and the desirability of displacement is consisted of seven levels, while the MFs of fuzzy MPCl output are divided into seven levels. Subsequently, a matrix of fuzzy rules is built in Table 19. The value of MPCl is determined according to each value of desirability for objective functions, as given in Table 20.

Subsequently, using the values of design variables in Table 18 and the MPCl value of Table 20, the ANFIS model is

formed for mapping the design variables and the MPCl. The ANFIS parameters for case study 2 are given in Table 21. The predicting accuracy of the ANFIS model is well confirmed through equations (29) and (31) prior to implement the MOO problem for the SRCM.

By using the TMFL, the optimal parameters are determined at $L_1 = 7.7$ mm, $L_3 = 10.1625$ mm, and $D = 2.25$ mm, as shown in Table 22. Based on the TMFL, the optimal frequency and displacement are found at 158.970 Hz and 0.0957 mm, respectively. Such optimal points are local optimum solutions. Subsequently, the results of proposed hybrid methodology found that the optimal design parameters are at $L_1 = 6.3793$ mm, $L_3 = 9.73$ mm, and $D = 2.25$ mm. Using these, the proposed approach, the optimal frequency, and displacement are found at 27.006 Hz and 0.2203 mm, respectively. At last, the predicted MPCl from the proposed methodology is effective and better than that from the TMFL. In addition, the equivalent stress is also lower than the allowable stress. The optimal results are satisfied with designer's requirements.

5. Results and Discussion

As discussed above, three cases studies are taken as numerical examples to describe application capacity and effectiveness of the proposed method. The performances of proposed methodology are compared with the TMFL. Table 23 summarizes all the optimal solutions for this comparison. In each case study, the optimal parameters are used to create a 3D model in SolidWorks 2018 software and then imported into ANSYS 2018 software to evaluate the robustness of the proposed hybrid approach by calculating the relative error. This error is calculated as follows:

$$\varepsilon(\%) = \left(\frac{R_p - R_a}{R_a} - 1 \right) * 100, \tag{36}$$

where ε , R_p , and R_a represent the relative error, predicted result from proposed method, and actual result, respectively.

Case study 1: using the TMFL, the results found the optimal frequency and displacement are 24.4574 Hz and 0.1691 mm, respectively. Meanwhile, the proposed hybrid approach predicts the frequency and displacement are about 26.592 Hz and 0.1679 mm, respectively. By using the proposed method, the relative errors between predicted values and FEA values are very small (around 5%), while the error value is around 7% via using TMFL. Both the proposed methods are reliable tools in this case. According to the Taguchi method, a larger-the-better value of MPCl is a desired value for the MOO problem. On the contrary, the proposed hybrid approach has a better performance than the TMFL because the MPCl from the proposed method is higher than that from the TMFL.

Case study 2: through the TMFL, the results found the optimal frequency and displacement are 28.9482 Hz and 0.1527 mm, respectively. By using the proposed hybrid integration, the optimal frequency and displacement are found at 651.08 Hz and 0.1981 mm, respectively. By using the proposed hybrid approach, the relative errors between

TABLE 12: Comparison of different methods for case study 1.

Method	Optimal parameters	Optimal results			
		Frequency (Hz)	Displacement (mm)	Stress (MPa)	SF MPCl
Hybrid of Taguchi method and fuzzy logic	$D = 2.25$ mm $L_3 = 8.5$ mm $L_4 = 18.7$ mm	24.4574	0.1691	251.463	2 0.510
Proposed approach of desirability, fuzzy-ANFIS-LAPO algorithm	$D = 2.30$ $L_3 = 8.5$ mm $L_4 = 18.7$ mm	26.592	0.1539	253.847	1.98 0.570

TABLE 13: Desirability results of the case study 2.

No.	Design variables (unit: mm)				Frequency $F_1(X)$ mm	displacement $F_2(X)$ (Hz)	Stress $F_3(X)$ (MPa)	Desirability of $F_1(X)$ D_1	Desirability of $F_2(X)$ D_2
	θ	L_1	L_2	D					
1	14.5	6.3	16.6	2.875	140.2838	0.013508	20.136932	0.126042291	0.102725633
2	12.5	6.3	16.6	2.875	141.5087	0.010046	17.092119	0.089296146	0.049191484
3	16.5	6.3	16.6	2.875	139.9513	0.013255	20.756254	0.264504072	0.098396331
4	14.5	4.9	16.6	2.875	139.9384	0.010927	18.907122	0.016411556	0.055559464
5	14.5	7.7	16.6	2.875	142.1834	0.010787	20.473748	0.338359234	0.081632844
6	14.5	6.3	14.5	2.875	148.7576	0.008941	13.90206	0.105418876	0.070044602
7	14.5	6.3	18.7	2.875	133.6071	0.011627	18.555608	0.249708039	0.059644029
8	14.5	6.3	16.6	2.25	54.02425	0.091965	155.65601	0	0.520514669
9	14.5	6.3	16.6	3.5	224.1544	0.004473	12.163485	0.375575312	0.106083045
10	12.5	4.9	14.5	2.25	29.63534	0.010148	31.923139	0.036724691	0.150747816
11	16.5	4.9	14.5	2.25	30.0422	0.040185	87.9122	0.013316419	0.413327968
12	12.5	7.7	14.5	2.25	30.81703	0.055528	108.84574	0	0.456367237
13	16.5	7.7	14.5	2.25	28.94823	0.152702	249.32714	0.214726673	0.70638882
14	12.5	4.9	18.7	2.25	26.82343	0.086202	160.20452	0.022707379	0.504418284
15	16.5	4.9	18.7	2.25	24.99238	0.0898	160.62031	0.05839604	0.461010103
16	12.5	7.7	18.7	2.25	25.76424	0.065583	119.20462	0.19869231	0.36014185
17	16.5	7.7	18.7	2.25	649.3008	1.78E-05	7.9628582	0.632518439	0.304175099
18	12.5	4.9	14.5	3.5	238.0543	0.002067	7.4382126	0.393236144	0
19	16.5	4.9	14.5	3.5	235.5158	0.003742	12.915726	0.309825869	0
20	12.5	7.7	14.5	3.5	245.0752	0.003262	8.3554397	0.463009101	0.033847584
21	16.5	7.7	14.5	3.5	706.8922	1.89E-05	2.0140876	0.777736293	0.175665459
22	12.5	4.9	18.7	3.5	212.0324	0.004153	11.315538	0.264022704	0.206278396
23	16.5	4.9	18.7	3.5	211.4283	0.004882	10.593629	0.239709361	0.054666508
24	12.5	7.7	18.7	3.5	648.699	1.77E-05	2.1232273	0.706507805	0
25	16.5	7.7	18.7	3.5	646.6069	1.97E-05	1.998213	1	0

predicted values and simulated values are around 4.65%, while the error between the predicted value by the TMFL and FEA value is around 9.5%. In addition, the MPCl predicted by the proposed hybrid approach is greater than that from TMFL. In other words, the performance and prediction accuracy of proposed methodology outperforms the TMFL.

Case study 3: the results found the optimal frequency and displacement are 158.970 Hz and 0.0957 mm, respectively, by using TMFL. Meanwhile, the proposed hybrid approach finds the optimal frequency and displacement approximately 651.08 Hz and 0.1981 mm, respectively. The relative errors between predicted values and simulated values are around 6%, while the error between the TMFL and FEA is about 484%. Moreover, the MPCl predicted by the proposed hybrid approach is higher than that from TMFL. It can conclude that the performance and precision of the proposed approach outperforms the TMFL.

The results of three numerical examples show that the proposed optimization scheme is better than the traditional TMFL. Among three numerical examples, case study 3 may be chosen as an optimal solution for MOO design of the SRCM because the MPCl is the highest value. The optimal design variables are at $L_1 = 6.3793$ mm, $L_3 = 9.73$ mm, and $D = 2.25$ mm. Other remain parameters are constant values. It concludes that the proposed hybrid approach is a robust optimization tool and effectiveness for solving the MOO design for the mechanism and related complex optimization fields.

6. Comparison with Metaheuristic Optimization Algorithms

As discussed above, the proposed method outperformed the traditional TMFL to solve MOO design for the mechanism. Continuously, the proposed algorithm is compared with

TABLE 14: Fuzzy rules matrix for case 2.

No.	Desirability for $F_1(X)$	Desirability for $F_2(X)$	MPCI
1	S	T	T
2	M	T	VS
3	L	T	S
4	S	VS	VS
5	M	VS	S
6	L	VS	SM
7	S	S	S
8	M	S	SM
9	L	S	ML
10	S	SM	S
11	M	SM	SM
12	L	SM	M
13	S	M	SM
14	M	M	M
15	L	M	ML
16	S	ML	SM
17	M	ML	M
18	L	ML	ML
19	S	L	ML
20	M	L	ML
21	L	L	L
22	S	VL	ML
23	M	VL	L
24	L	VL	VL
25	S	H	ML
26	M	H	L
27	L	H	H

TABLE 15: Results of fuzzy MPCI for case 2.

No.	Desirability for $F_1(X)$	Desirability for $F_2(X)$	MPCI
1	0.126042291	0.102725633	0.123
2	0.089296146	0.049191484	0.0934
3	0.264504072	0.098396331	0.19
4	0.016411556	0.055559464	0.099
5	0.338359234	0.081632844	0.204
6	0.105418876	0.070044602	0.109
7	0.249708039	0.059644029	0.17
8	0	0.520514669	0.375
9	0.375575312	0.106083045	0.238
10	0.036724691	0.150747816	0.146
11	0.013316419	0.413327968	0.286
12	0	0.456367237	0.333
13	0.214726673	0.70638882	0.517
14	0.022707379	0.504418284	0.375
15	0.05839604	0.461010103	0.338
16	0.19869231	0.36014185	0.284
17	0.632518439	0.304175099	0.375
18	0.393236144	0	0.125
19	0.309825869	0	0.12
20	0.463009101	0.033847584	0.156
21	0.777736293	0.175665459	0.445
22	0.206278396	0.264022704	0.261
23	0.054666508	0.239709361	0.163
24	0	0.706507805	0.164
25	0	1	0.25

recent less-parameter optimization algorithms such as Jaya algorithm and TLBO algorithm. Case 3 is chosen as the final optimal candidate for the proposed mechanism. Therefore,

the ANFIS structure of case 3 is then coupled with Jaya and TLBO algorithms for this comparison. The results indicated that the optimal frequency and displacement predicted by

TABLE 16: ANFIS parameters for case 2.

Number of nodes	92
Number of linear parameters	192
Number of nonlinear parameters	30
Total number of parameters	222
Number of training data pairs	27
Number of testing data pairs	0
Number of fuzzy rules	32

TABLE 17: Comparison of differential methods for case study 2.

Method	Optimal parameters	Optimal results				
		Frequency (Hz)	Displacement (mm)	Stress (MPa)	SF	MPCI
Hybrid of Taguchi method and fuzzy logic	$\theta = 16.5^\circ$ $L_1 = 7.7$ mm $L_2 = 18.7$ mm $D = 2.25$ mm	28.94823	0.1527	7.9628	63.16	0.375
Proposed approach of desirability, fuzzy-ANFIS-LAPO algorithm	$\theta = 16.5^\circ$ $L_1 = 8.0$ mm $L_2 = 14.5$ mm $D = 2.5$ mm	651.08	0.1981	4.4641	112.67	0.517

TABLE 18: Desirability results of the case study 3.

No.	Design variables (unit: mm)			Frequency $F_1(X)$ (Hz)	Displacement $F_2(X)$ (mm)	Stress $F_3(X)$ (MPa)	Desirability of $F_1(X)$ D_1	Desirability of $F_2(X)$ D_2
	L_1	L_3	D					
1	6.3	10.1625	2.875	142.1428	0.013839	20.34068	0.257697	0.159738122
2	4.9	10.1625	2.875	135.4637	0.01317	21.402	0.327272	0.085867476
3	7.7	10.1625	2.875	684.347	1.76E-05	2.829244	0.752914	0
4	6.3	10.1625	2.25	27.02455	0.242625	365.8681	0	0.726699252
5	6.3	10.1625	3.5	260.1458	0.004596	10.77186	0.434028	0.240793486
6	6.3	8.5	2.875	147.0101	0.013744	20.2492	0.158614	0.030275021
7	6.3	11.825	2.875	135.084	0.013954	20.45499	0.133502	0.032371983
8	4.9	8.5	2.25	29.8364	0.134483	238.4694	0	0.609908353
9	7.7	8.5	2.25	28.4018	0.044736	83.66811	0.090806	0.265631968
10	4.9	8.5	3.5	235.2483	0.00462	12.88278	0.242549	0
11	7.7	8.5	3.5	708.6937	1.64E-05	2.275569	1	0
12	4.9	11.825	2.25	27.5078	0.137112	235.3041	0	0.617415632
13	7.7	11.825	2.25	26.37316	0.044389	85.38369	0.074579	0.266912238
14	4.9	11.825	3.5	221.0946	0.004669	12.09392	0.208551	0
15	7.7	11.825	3.5	653.4564	1.98E-05	2.137794	0.952076	0

the proposed algorithm are better than those estimated by the Jaya and TLBO algorithms, as given in Table 24. On the contrary, the proposed methodology has a prediction accuracy better than other metaheuristic optimization algorithms.

In order to evaluate and validate the effectiveness of three abovementioned algorithms, the nonparametric tests are used for comparing the performances of the proposed hybrid approach with other algorithms [66, 67]. The Wilcoxon’s rank signed test and Friedman test, two performance metrics, are utilized as the nonparametric tests. Both these statistical techniques consider that both different algorithms behave unsimilarly. Recently, the nonparametric tests have been widely applied in comparing the performances between

algorithms, e.g., [68, 69]. The comparing results are almost based on the p value. In the present article, the computational simulations are conducted with 60 runs for each algorithm. The Wilcoxon’s rank signed test is performed for frequency and displacement at 5% significant level and 95% confidence intervals. The statistical analysis is implemented in Minitab 18 software. The results in Tables 25 and 26 show that the p value is less than 0.05 (5% significance level). According to nonparametric tests [66, 67], it reveals that there is a statistical difference between the proposed approach and other algorithms. Besides, the results confirm that the proposed hybrid algorithm has a performance effectiveness greater than ANFIS-based Jaya and ANFIS-based TLBO algorithms.

TABLE 19: Fuzzy rules matrix for case 3.

No.	Desirability for $F_1(X)$	Desirability for $F_2(X)$	MPCI
1	S	T	T
2	M	T	VS
3	L	T	S
4	S	VS	VS
5	M	VS	S
6	L	VS	SM
7	S	S	S
8	M	S	SM
9	L	S	ML
10	S	SM	S
11	M	SM	SM
12	L	SM	M
13	S	M	SM
14	M	M	M
15	L	M	ML
16	S	ML	SM
17	M	ML	M
18	L	ML	ML
19	S	L	ML
20	M	L	ML
21	L	L	L
22	S	VL	ML
23	M	VL	L
24	L	VL	VL
25	S	H	ML
26	M	H	L
27	L	H	H

TABLE 20: Results of fuzzy output for case 3.

No.	Desirability for $F_1(X)$	Desirability for $F_2(X)$	MPCI
1	0.257697	0.159738122	0.237
2	0.327272	0.085867476	0.205
3	0.752914	0	0.189
4	0	0.726699252	0.585
5	0.434028	0.240793486	0.375
6	0.158614	0.030275021	0.0958
7	0.133502	0.032371983	0.0741
8	0	0.609908353	0.375
9	0.090806	0.265631968	0.25
10	0.242549	0	0.105
11	1	0	0.25
12	0	0.617415632	0.375
13	0.074579	0.266912238	0.25
14	0.208551	0	0.0886
15	0.952076	0	0.25

TABLE 21: ANFIS parameters for case 3.

Number of nodes	34
Number of linear parameters	32
Number of nonlinear parameters	18
Total number of parameters	50
Number of training data pairs	15
Number of testing data pairs	0
Number of fuzzy rules	8

Another way, the Friedman test, is used for the behavior comparison of the abovementioned algorithms. The results find that the p value is less than 0.05. Therefore, it confirms that there the proposed hybrid approach differs from two other algorithms, as given in Tables 27 and 28. Moreover, the effectiveness of the proposed hybrid algorithm is better than ANFIS-based Jaya algorithm and ANFIS-based TLBO algorithm. Besides, the median responses for the proposed algorithm are greater than those of two other algorithms. So,

TABLE 22: Comparison of differential methods for case study 3.

Method	Optimal parameters	Frequency (Hz)	Optimal results			
			Displacement (mm)	Stress (MPa)	SF	MPCI
Hybrid of Taguchi method and fuzzy logic	$L_1 = 7.7$ mm $L_3 = 10.1625$ mm $D = 2.25$ mm	158.970	0.0957	155.800	3.22	0.496
Proposed approach of desirability, fuzzy-ANFIS-LAPO algorithm	$L_1 = 6.3793$ mm $L_3 = 9.73$ mm $D = 2.25$ mm	27.006	0.2203	332.8096	1.511	0.611

TABLE 23: Comparison of the optimal results for three cases.

Case study	Method	Optimal factors	Frequency (Hz)	Optimal responses			MPCI
				Displacement (mm)	Stress (MPa)		
Case 1	Hybrid of Taguchi method and fuzzy logic	$D = 2.25$ mm $L_3 = 8.5$ mm $L_4 = 18.7$ mm	Predicted: $F_1 = 24.4574$ FEA: $F_1 = 26.283$ $\epsilon = 6.94\%$	Predicted: $F_2 = 0.1691$ FEA: $F_2 = 0.1772$ $\epsilon = 4.57\%$	Predicted: $F_3 = 251.463$ FEA: $F_3 = 259.42$ $\epsilon = 3.06\%$	0.510	
	Proposed hybrid approach of fuzzy-ANFIS-LAPO algorithm	$D = 2.30$ mm $L_3 = 8.5$ mm $L_4 = 18.7$ mm	Predicted: $F_1 = 26.592$ FEA: $F_1 = 25.828$ $\epsilon = 2.95\%$	Predicted: $F_2 = 0.1679$ FEA: $F_2 = 0.1766$ $\epsilon = 4.92\%$	Predicted: $F_3 = 253.847$ FEA: $F_3 = 260.570$ $\epsilon = 2.58\%$	0.570	
Case 2	Hybrid of Taguchi method and fuzzy logic	$\theta = 16.5^\circ$ $L_1 = 7.7$ mm $L_2 = 18.7$ mm $D = 2.25$ mm	Predicted: $F_1 = 28.9482$ FEA: $F_1 = 649.3$ $\epsilon = 2.58\%$	Predicted: $F_2 = 0.1527$ FEA: $F_2 = 0.1782$ $\epsilon = 9.55\%$	Predicted: $F_3 = 7.9628$ FEA: $F_3 = 7.8629$ $\epsilon = 1.28\%$	0.375	
	Proposed hybrid approach of fuzzy-ANFIS-LAPO algorithm	$\theta = 16.5^\circ$ $L_1 = 8.0$ mm $L_2 = 14.5$ mm $D = 2.5$ mm	Predicted: $F_1 = 651.08$ FEA: $F_1 = 682.8535$ $\epsilon = 4.65\%$	Predicted: $F_2 = 0.1981$ FEA: $F_2 = 0.1907$ $\epsilon = 3.88\%$	Predicted: $F_3 = 4.4641$ FEA: $F_3 = 4.288$ $\epsilon = 4.10\%$	0.517	
Case 3	Hybrid of Taguchi method and fuzzy logic	$L_1 = 7.7$ mm $L_3 = 10.1625$ mm $D = 2.25$ mm	Predicted: $F_1 = 158.970$ FEA: $F_1 = 27.175$ $\epsilon = 484\%$	Predicted: $F_2 = 0.0957$ FEA: $F_2 = 0.0443$ $\epsilon = 116\%$	Predicted: $F_3 = 155.8$ FEA: $F_2 = 86.112$ $\epsilon = 80\%$	0.496	
	Proposed hybrid approach of fuzzy-ANFIS-LAPO algorithm	$L_1 = 6.3793$ mm $L_3 = 9.73$ mm $D = 2.25$ mm	Predicted: $F_1 = 27.0063$ FEA: $F_1 = 27.178$ $\epsilon = 6.31\%$	Predicted: $F_2 = 0.2203$ FEA: $F_2 = 0.2233$ $\epsilon = 1.34\%$	Predicted: $F_3 = 332.8096$ FEA: $F_2 = 343.3$ $\epsilon = 0.03\%$	0.611	

TABLE 24: Comparison between other algorithms with the proposed approach.

Approaches	Frequency (Hz)	Displacement (mm)
ANFIS-Jaya ($L_1 = 6.3790$, $L_3 = 9.7305$ mm, and $D = 2.25$ mm)	26.6803	0.2199
ANFIS-TLBO ($L_1 = 6.6134$, $L_3 = 10.8097$ mm, and $D = 2.25$ mm)	26.0994	0.1959
Proposed algorithm ($L_1 = 6.3793$, $L_3 = 9.7300$ mm, and $D = 2.25$ mm)	27.0063	0.2203

the proposed approach is a more effective tool than the other algorithms.

Although the proposed hybrid computational method has specific advantages in terms of solving MOO design of

the SRCM, it has still some drawbacks: the running time is also long because the datasets are transferred into different stages. This may take a long time and high computational cost for more complex structures. It is known that the time

TABLE 25: Wilcoxon signed rank test for displacement.

Number of tests	Wilcoxon statistic	Proposed algorithm versus ANFIS-Jaya	
		<i>p</i> value	Estimated median difference
60	0.0	0.000	-0.004
Number of tests	Wilcoxon statistic	Proposed algorithm versus ANFIS-TLBO	
		<i>p</i> value	Estimated median difference
60	0.0	0.000	-0.0244

TABLE 26: Wilcoxon signed rank test for frequency.

Number of tests	Wilcoxon statistic	Proposed algorithm versus ANFIS-Jaya	
		<i>p</i> value	Estimated median difference
60	0.0	0.000	-0.326
Number of tests	Wilcoxon statistic	Proposed algorithm versus ANFIS-TLBO	
		<i>p</i> value	Estimated median difference
60	0.0	0.000	-0.9069

TABLE 27: Friedman test for displacement.

Algorithm	Number of tests	Median	Sum of ranks
ANFIS-Jaya	60	0.219900	120
ANFIS-TLBO	60	0.195900	60
Proposed algorithm	60	0.220300	180
Overall	180	0.212033	
DF	Chi-square	<i>p</i> value	
2	120	0.000	
Null hypothesis	H0: all treatment effects are zero		
Alternative hypothesis	H1: not all treatment effects are zero		

TABLE 28: Friedman test for frequency.

Algorithm	Number of tests	Median	Sum of ranks
ANFIS-Jaya	60	26.6803	120
ANFIS-TLBO	60	26.0994	60
Proposed algorithm	60	27.0063	180
Overall	180	26.5953	
DF	Chi-square	<i>p</i> value	
2	120	0.000	
Null hypothesis	H0: all treatment effects are zero		
Alternative hypothesis	H1: not all treatment effects are zero		

and space complexity of an algorithm is very important. For a more complicated problem with large datasets, it needs more better memory space of a computer. These disadvantages of the proposed method can be solved as follows: (i) FEM analysis is time consuming, but this problem can be solved by using parallelism computation by using multiple processors or a high-performance computer. (ii) Automatically adaptive combination of statistical method, FEM, and metaheuristic algorithms is a feasible approach to reduce the computational cost. In other words, the proposed optimization scheme should automatically update new data if there is an adjustment of space or range of design variables. The aim of the present work is to recommend a new hybrid computational approach in solving the MOO design for compliant mechanisms. In future work, the time, space, and

algorithm complexity need to be investigated to improve the proposed approach.

7. Conclusions

A new hybrid computational method is developed to solve a MOO design for a Scott Russell compliant mechanism in this article. The methodology can be considered as a combination of statistical techniques, finite element method, and intelligent computation. It is an integration of the desirability function technique, fuzzy logic reasoning, ANFIS, and LAPO algorithm. A 3D FEM model is created, and CCD is used to build the experimental matrix. Next, numerical data are collected through FEM simulations. Based on the numerical results, a sensitivity investigation is analyzed by

using ANOVA and Taguchi method. The refinement process for design variables is to determine really searching spaces of design parameters. As a result, three case studies are assigned as application example of the proposed approach. Next, the desirability of two responses is computed and transferred into the FIS system. ANFIS technique is then utilized to model the MPCI, which is considered as a combined objective function. LAPO algorithm is adopted for optimizing the MPCI. The results find that the predicting accuracy of proposed hybrid methodology is better than that of the traditional Taguchi-based fuzzy logic. Case study 3 is chosen to be optimal candidate. Finally, the Wilcoxon signed rank test and Friedman test are analyzed to compare the performances of the proposed approach with the ANFIS-based Jaya algorithm and ANFIS-based TLBO algorithm. The results found the performance efficiency of proposed approach is better than those of other approaches. The proposed methodology can be an efficient tool for more complex optimization problems, including multiple objective functions, design variables, and constraints.

The results of the present study will be extended to more complex compliant mechanisms. Future research will concentrate on fabricating physical prototypes, and then an extra number of testing experiments is performed to validate the theoretical models and simulations.

Data Availability

The data used to support the findings of this study are included within the article.

Conflicts of Interest

The authors declare that they have no conflicts of interest.

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