

A Low-cost Optimization Design for Minimizing Chromatic Aberration by Doublet Prisms

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A low-cost optimal double-prism method is proposed by using the developed MATLAB program to correct chromatic aberration. We present an efficient approach to choose a couple of low-cost glasses to obtain a low aberration double prism. The doublet prisms were made of two lead-free glasses. The relative partial dispersion of the two lead-free glasses is identical and their Abbe numbers are different greatly. The proposed design aims to minimize chromatic aberration, such as in apochromats, for paraxial ray tracing. Finally, an optimization design for real ray tracing can be evaluated by the chromatic aberration curve with a minimal area.

Keywords : Doublet prisms, Optimization, Chromatic aberration, Ray tracing

OCIS codes : (080.1010) Aberrations; (080.2740) Geometric optical design; (230.5480) Prisms

I. INTRODUCTION

The image quality of a lens design can be good but the cost of the glass from which it is made can be quite high. Kidger [1] considered variation in cost between glasses used for this purpose. In the large size lenses, the cost of expensive glass could be prohibitive; but in small size lenses, the materials make up only a small percentage of the total cost of the lens, so expensive materials might well be acceptable in this case. Chromatic aberration occurs because of the different refractive indices of lenses for different wavelengths of light [2, 3]. If two different types of glasses are combined into a thin two-element system, a paraxial chromatic aberration will develop [4]. Robb [5] developed a method using two different types of glass for the correction of axial color for at least three wavelengths. Certain combinations might be found for correction at four and five wavelengths. In 1983, Sharma and Gopal [6] used the double-graph technique to produce doublet designs. Then, in 2001, Rayces and Rosete-Aguilar [7, 8] described a method to select pairs of glasses for both thin cemented achromatic doublets and thin aplanatic achromatic doublets with a reduced secondary spectrum. In another study, Banerjee and Hazra [9] used a genetic algorithm for the

structural design of cemented doublets. The aim of this work is to minimize chromatic aberration by using a low-cost optimal double-prism method. An efficient approach for finding an optimum design is also proposed.

II. METHODS

An illustration of ray tracing in and out of a prism is shown in Fig. 1. The angle of a ray in the normal direction from the prism surface is positive in the anticlockwise

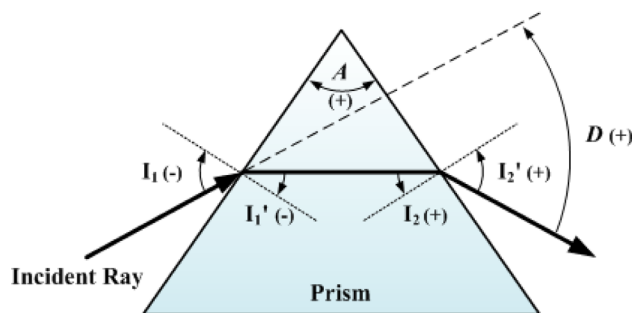


FIG. 1. Angle of deviation of a prism.

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direction, and negative in the clockwise direction. In this figure, I_1 and I_2 are the incident angles of the first and the second surfaces, respectively; I_1' and I_2' are the refractive angles of the first and the second surfaces, respectively; A is the apex angle of the prism. The sign of the apex angle is positive in the vertical, and negative in the inverse direction. The ray thus deviates through an angle of $(I_1' - I_1)$ at the first surface. At the second surface, the ray deviates by $(I_2' - I_2)$, so the angle of deviation D of the ray is given by

$$D = (I_1' - I_1) + (I_2' - I_2) \quad (1)$$

If we consider real ray tracing, the deviation angle [10] presented by

$$D = -I_1 - A + \sin^{-1}((n^2 - \sin^2 I_1)^{1/2} \sin A + \cos A \sin I_1) \quad (2)$$

2.1. Single Prism Paraxial Chromatic Aberration

If all the angles of the design are small, the equations for the paraxial ray tracing can be obtained, and the paraxial deviation angle [11] given by

$$D = (n - 1)A. \quad (3)$$

The paraxial primary color $\varepsilon_{F,C}$ is the difference in deviation angles between F line (0.48613 μm) and C line (0.65627 μm) as shown. Thus

$$\varepsilon_{F,C} = D_F - D_C = \frac{D_d}{V_d}, \quad (4)$$

where D_d is the paraxial deviation angle of d line (0.58756 μm); $V_d = (n_d - 1)/(n_F - n_C)$ is the Abbe number; and n_C , n_d , n_F are the refractive indices of C, d, and F lines, respectively. Consequently, the paraxial second spectrum $\varepsilon_{d,C}$ is the difference in the deviation angles between d line and C line. This can show as

$$\varepsilon_{d,C} = D_d - D_C = \frac{P_{d,C}}{V_d} D_d, \quad (5)$$

where $P_{d,C} = (n_d - n_C)/(n_F - n_C)$ is the relative partial dispersion.

2.2. Doublet Prisms Paraxial Chromatic Aberration

In the paraxial ray tracing of doublet prisms, the angle of deviation of d-line light is defined as 3° , so the primary color $\varepsilon_{F,C}$ is zero [4, 5]. These equations can be written as

$$D_d = D_{d_1} + D_{d_2} = 3^\circ, \quad (6)$$

$$\varepsilon_{F,C} = \frac{D_{d_1}}{V_{d_1}} + \frac{D_{d_2}}{V_{d_2}} = 0, \quad (7)$$

where the paraxial deviation angles of the doublet prisms are D_{d_1} and D_{d_2} , respectively. The primary chromatic aberration is $\varepsilon_{F,C}$. Solving for D_{d_1} and D_{d_2} from the above equations, we obtain

$$D_{d_1} = \frac{V_{d_1}}{V_{d_1} - V_{d_2}} D_d, \quad (8)$$

and

$$D_{d_2} = \frac{-V_{d_2}}{V_{d_1} - V_{d_2}} D_d. \quad (9)$$

The apex angles of the doublet prisms are expressed as

$$A_1 = \frac{D_{d_1}}{n_{d_1} - 1}, \quad (10)$$

and

$$A_2 = \frac{D_{d_2}}{n_{d_2} - 1}. \quad (11)$$

Accordingly the paraxial primary color is zero, but there are still some paraxial secondary spectra. Thus the paraxial secondary spectrum can be defined as

$$\begin{aligned} \varepsilon_{d,C} &= \varepsilon_{d,C_1} + \varepsilon_{d,C_2} \\ &= \frac{P_{d,C_1}}{V_{d_1}} D_{d_1} + \frac{P_{d,C_2}}{V_{d_2}} D_{d_2} \\ &= \frac{(P_{d,C_1} - P_{d,C_2})}{(V_{d_1} - V_{d_2})} D_d \end{aligned} \quad (12)$$

where the paraxial primary chromatic aberrations of the doublet prisms are ε_{F,C_1} and ε_{F,C_2} , respectively.

2.3. Schott Glasses Selection

We choose the Schott glass [12] for the design because of the large number of types of glasses that are available. The Abbe numbers of the different glasses have been ranked. There are 119 different optical glasses all with different prices. The price of N-BK7 is the lowest. The relative price (RP) is found by comparison and the results are indexed. To avoid using the most expensive types of glass in the design, the twenty-nine types with a relative price $\text{RP} \geq 17$ as well as those with no marked prices are eliminated. The costs of glasses such as N-KZFS11, N-PK51, and N-LASF31A, are much higher than the others. Those with no marked prices are molding glasses or new types of glasses. The internal transmittance is the transmittance of light excluding reflection loss. The N-SF6HT and N-SF57HT glasses offer improved transmittance in the

visible spectral range especially in the blue-violet area. Moreover, since the V_d , n_d , and $P_{d,C}$ of N-SF6HT and N-SF57HT are all the same as those of N-SF6 and N-SF57, the corrected chromatic aberrations will be almost the same. Thus we can neglect the N-SF6HT and N-SF57HT glasses. A total of seventy types of glasses were chosen for doublet prisms design to correct chromatic aberration.

2.4. Merit Function

In Eqs. (2) and (3), it can be seen that there is a difference in the deviation angles between the real ray and the paraxial ray. The deviation angle of the paraxial ray is unconcerned with the incident angle I_1 , but the deviation angle of the real ray is related to the incident angle I_1 . When the incident angle increases, the real and paraxial chromatic aberrations will be very different. The real chromatic aberration is corrected for optimization. The damped least-squares method [13-15] is applied for an optimization design of the chromatic aberration. A merit function is defined as the summation of the squared values of the weighting differences between the aberrations and their target values. The formula can be written as

$$\phi = \sum_{i=1}^m w_i^2 (e_i - t_i)^2, \tag{13}$$

where m is the total summation number; the w_i is the weighting factor; e_i is the aberration and t_i is the target value. We define the function $f_i(x_1, x_2, \dots, x_n)$ as

$$f_i = w_i (e_i - t_i). \tag{14}$$

Before optimization, the n variables are denoted as $x_{10}, x_{20}, \dots, x_{n0}$; the m aberrations before the optimization are $f_{10}, f_{20}, \dots, f_{m0}$. After the optimization process, the variables are denoted as x_1, x_2, \dots, x_n , and the aberrations as f_1, f_2, \dots, f_m . Here, we define a matrix A , in which the elements are

$$A_{ij} = \frac{\partial f_i}{\partial x_j}. \tag{15}$$

We then get the equation

$$X = -(A^T A + pI)^{-1} A^T f_0, \tag{16}$$

where A^T is the transpose matrix of A ; I is a unit matrix, p is a damping factor; and f_0 is the matrix containing the elements $f_{10}, f_{20}, \dots, f_{m0}$. If x and x_0 are the matrices containing the elements x_1, x_2, \dots, x_n , and $x_{10}, x_{20}, \dots, x_{n0}$, respectively, we can obtain

$$x = x_0 + X. \tag{17}$$

III. RESULTS

3.1. Minimizing the Paraxial Chromatic Aberration

The doublet prisms have two apex angles. The angle of deviation of d line is 3° , and the primary color is eliminated. The steps are repeated to reduce the secondary spectra of the doublet prisms. Using Eq. (12), the correct doublet prisms combination can be found by choosing the smaller $(P_{dC1} - P_{dC2})$ and the larger $(V_{d1} - V_{d2})$. When the $(P_{dC1} - P_{dC2}) / (V_{d1} - V_{d2})$ is close to zero, the chromatic aberration is smaller. Figure 2 shows the relative partial dispersion with respect to the V_d number. We chose six groups from A to F for minimizing the paraxial chromatic aberration. The design results are listed in Table 1, where the CA is the area of the chromatic aberration curve. Figure 3 shows the chromatic aberration curves. The

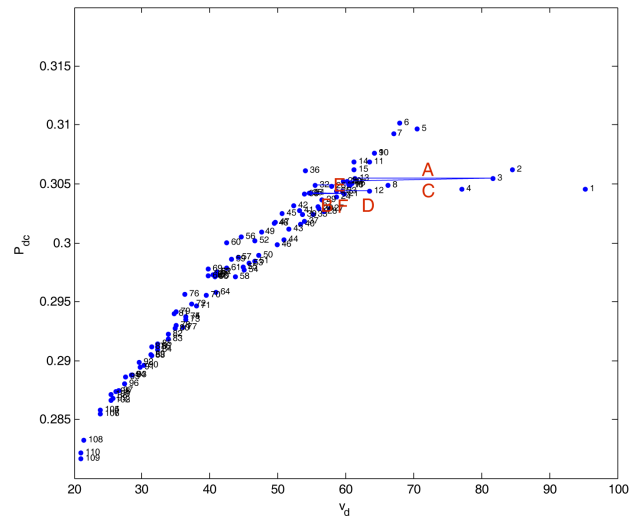


FIG. 2. $P_{d,C} - V_d$ mapping for the selected doublet prisms.

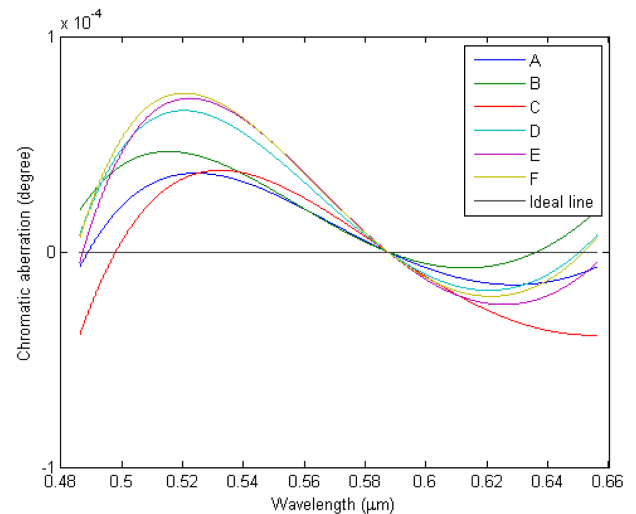


FIG. 3. Minimizing paraxial chromatic aberration curves for doublet prisms groups A to F.

TABLE 1. Design data and area of paraxial chromatic aberration curves for doublet prisms A To F

$D_d = 3^\circ, E_{F,C} = 0$						
No.	Glass 1 (No.)	Glass 2 (No.)	A_1 Degree	A_2 Degree	$E_{d,C}$ Degree	CA $\mu\text{m} \times \text{Degree}$
A	N-Pk52A(3)	N-Sk5(13)	24.215	-15.336	7.092×10^{-6}	3.029×10^{-6}
B	N-Bak2(21)	N-Lak34(35)	63.681	-43.043	-1.916×10^{-5}	3.432×10^{-6}
C	N-Pk52A(3)	N-Lak21(20)	22.903	-13.088	3.870×10^{-5}	4.165×10^{-6}
D	N-Psk53A(12)	N-Lak7(25)	63.161	-55.300	-7.641×10^{-6}	4.952×10^{-6}
E	N-Sk14(17)	N-Lak14(32)	58.115	-45.996	5.195×10^{-6}	5.612×10^{-6}
F	N-Bak2(21)	N-Lak8(38)	56.447	-38.540	-6.270×10^{-6}	5.568×10^{-6}

TABLE 2. Initial values for optimization of the doublet prism design (group A)

N-PK52A (3), N-SK5 (13)							
I_1 degree	I_3 degree	A_1 degree	A_2 degree	D_d degree	$\varepsilon_{d,C}$ degree	$\varepsilon_{F,C}$ degree	CA $\mu\text{m} \times \text{degree}$
0	0	24.215	-15.336	4.148	6.332×10^{-3}	2.078×10^{-2}	9.083×10^{-4}

horizontal ideal line, which denotes the angle of deviation of d line is 3° , has been set to zero for the chromatic aberration. The other lines are described as the chromatic aberration of doublet prisms groups from A to F.

3.2. OPTIMIZATION DESIGN FOR THE REAL CHROMATIC ABERRATION

We choose group A from Table 1 as an example as the initial value. The doublet prisms are made of N-PSK52A and N-SK5 glasses. We set I_1 and I_3 as the incident angles for the first surface of the first and the second prisms, respectively; A_1 and A_2 are the apex angles of the first and the second prisms, respectively. An illustration of the ray tracing of the doublet prisms is shown in Fig. 4. At the initial values, we set $I_1 = 0$, $I_3 = 0$, $A_1 = 24.215^\circ$, and $A_2 = -15.336^\circ$, as listed in Table 2. We can calculate the $D_d = 4.148^\circ$, $\varepsilon_{d,C} = 6.332 \times 10^{-3}$, $\varepsilon_{F,C} = 2.078 \times 10^{-2}$, and $CA = 9.083 \times 10^{-4}$ for the real ray tracing. The D_d and chromatic aberrations between the real and the paraxial rays ($\varepsilon_{F,C}$, $\varepsilon_{d,C}$, CA) are very different. The real chromatic aberration is corrected by an optimization program.

The merit function consists of three terms. The first term is the deviation angle D_d of the real ray for the doublet prisms, the second is the real primary color aberration $\varepsilon_{F,C}$ of the doublet prisms, and the last is the real secondary spectrum $\varepsilon_{d,C}$ of the doublet prisms. If the target values are $t_{D_d} = 3$, $t_{\varepsilon_{d,C}} = 0$, and $t_{\varepsilon_{F,C}} = 0$, then the merit function is given by

$$\phi = \sum_{i=1}^3 f_i^2 = w_1^2(D_d - 3)^2 + w_2^2(\varepsilon_{d,C} - 0)^2 + w_3^2(\varepsilon_{F,C} - 0)^2, \quad (18)$$

where the weighting factors are $w_1 = 1$, $w_2 = 20$, $w_3 = 20$, respectively. During the doublet prisms optimization, we

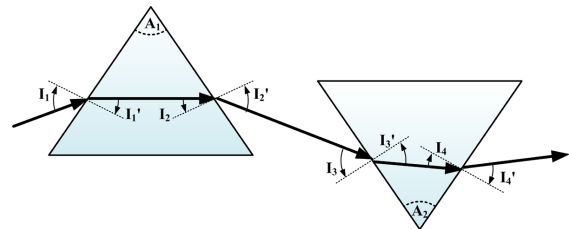


FIG. 4. Ray tracing in the doublet prisms.

will consider some sort of aberration balance, a sensible choice of weighting factors is essential if we are to achieve the best possible performance. In the optimization process, we think that two aberrations of $\varepsilon_{d,C}$ and $\varepsilon_{F,C}$ are more rigorous than that of D_d , and then the target values of both $|\varepsilon_{d,C}|$ and $|\varepsilon_{F,C}|$ are twenty times smaller than those of $|D_d - 3|$. It is therefore sensible, often but not always, for weighting factors to be smaller for larger target values.

We use four variables as x_1 , x_2 , x_3 , and x_4 , to represent the incident angle I_1 of the first prism, the incident angle I_3 of the second prism, the apex angle A_1 of the first prism, the apex angle A_2 of the second prism, respectively. Before optimization, the variables are denoted as x_{10} , x_{20} , x_{30} , and x_{40} , which correspond to $I_1 = 0$, $I_3 = 0$, $A_1 = 24.215$, and $A_2 = -15.336$, respectively. The optimization results are listed in Table 3, and the real chromatic aberration curve is shown in Fig. 5.

Except for fixing the deviation angle of real ray $D_d = 3^\circ$, we can optimize the area CA of the real chromatic aberration curve to obtain an optimization design. The merit function is defined as

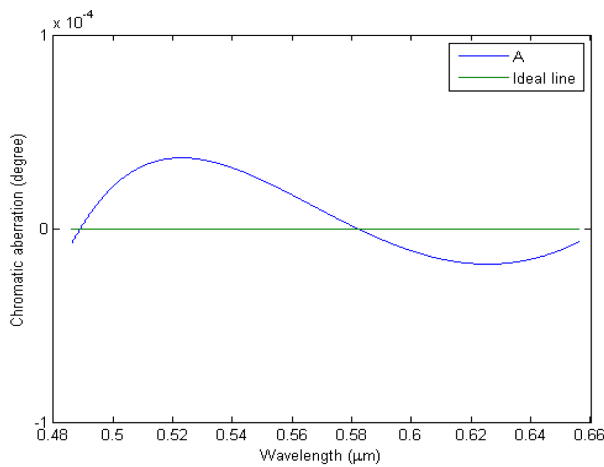
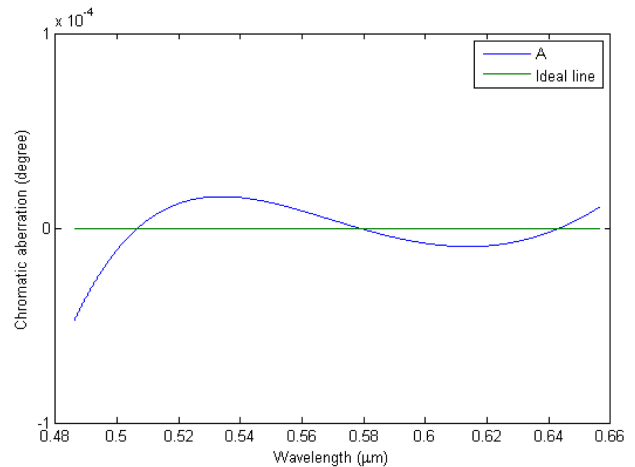
$$\phi = w_1^2(D_d - t_{D_d})^2 + w_2^2(CA - t_{CA})^2, \quad (19)$$

TABLE 3. Design results (group A) for target values: $t_{D_d} = 3$, $t_{\epsilon_{d,C}} = 0$, and $t_{\epsilon_{F,C}} = 0$

N-PK52A(3), N-SK5(13)							
I_1 degree	I_3 degree	A_1 degree	A_2 degree	D_d degree	$\epsilon_{d,C}$ degree	$\epsilon_{F,C}$ degree	CA $\mu\text{m} \times \text{degree}$
-6.4399	-0.30885	23.9821	-15.6298	3	2.873×10^{-6}	-8.664×10^{-7}	3.214×10^{-6}

TABLE 4. Design results (group A) for target values: $t_{D_d} = 3$, $t_{CA} = 0$

N-PK52A(3), N-SK5(13)							
I_1 degree	I_3 degree	A_1 degree	A_2 degree	D_d degree	$\epsilon_{d,C}$ degree	$\epsilon_{F,C}$ degree	CA $\mu\text{m} \times \text{degree}$
-6.6347	-0.29965	23.9982	-15.6213	3	-1.430×10^{-5}	-5.786×10^{-5}	1.702×10^{-6}

FIG. 5. Real chromatic aberration curve for group A for optimized target values: $t_{D_d} = 3$, $t_{\epsilon_{d,C}} = 0$, and $t_{\epsilon_{F,C}} = 0$.FIG. 6. Real chromatic aberration curve for group A for optimized target values: $t_{D_d} = 3$, $t_{CA} = 0$.

where the target values are $t_{D_d} = 3$, and $t_{CA} = 0$. The optimized results are listed in Table 4, and the real chromatic aberration curve is shown in Fig. 6.

3.3. Total Internal Reflection

As mentioned before, figure 4 shows the ray tracing of the doublet prisms, where I_1 , I_1' , A_2 , I_4 , and I_4' are negative and A_1 , I_2 , I_2' , I_3 , and I_3' are positive. When the incident angle of the first prism is $I_2 > \theta_C$, the total internal reflection of the ray appears. The critical angle θ_C is given by

$$\theta_C = \pm \sin^{-1} \frac{1}{n}, \quad (20)$$

where n is the refractive index of the prism.

We choose group B from Table 5 as an example. The two types of glass used in the doublet prisms are N-BAK2 and N-LAK34, their refractive indices are $n_{d_1} = 1.53996$ and $n_{d_2} = 1.72916$, respectively, and the critical angles are $\theta_{C_1} = 40.494^\circ$ and $\theta_{C_2} = 35.332^\circ$, respectively. In order to avoid total reflection, the incident angle I_1 of the first surface of

the first prism must be

$$I_1 < \sin^{-1} [n_1 \sin(\theta_{C_1} - A_1)], \quad (21)$$

and the incident angle I_3 of the first surface of the second prism is required to be

$$I_3 < \sin^{-1} [n_2 \sin(\theta_{C_2} - A_2)]. \quad (22)$$

3.4. Design of The Optimization Program

A flow-chart of the optimization program for the doublet prisms design is shown in Fig. 7. First, the program selects $(P_{dC_1} - P_{dC_2}) / (V_{d_1} - V_{d_2})$, the minimal value of the doublet glasses. Second, the program uses the paraxial ray equations from Eq. (6) to Eq. (11) to fix the deviation angle $D_d = 3^\circ$, and eliminate the primary color. Then, the two apex angles are obtained. Third, the program sets $t_{D_d} = 3$, $t_{\epsilon_{d,C}} = 0$, and $t_{\epsilon_{F,C}} = 0$ to optimize the real primary color. Finally, $t_{D_d} = 3$ and $t_{CA} = 0$ are used to optimize the area of the real chromatic aberration curve, until the real chromatic aberration is a minimum. The

TABLE 5. Optimization designs for doublet prisms from group A to group F

$D_d = 3^\circ$							
NO.	Glass 1	Glass 2	I_1 degree	I_3 degree	A_1 degree	A_2 degree	CA $\mu\text{m} \times \text{degree}$
A	N-PK52A	N-SK5	-6.6347	-0.29965	23.9982	-15.6213	1.702×10^{-6}
B	N-BAK2	N-LAK34	-50.1947	1.1397	15.8195	-12.3902	4.405×10^{-6}
C	N-PK52A	N-LAK21	3.0797	0.17857	22.7408	-14.9452	2.699×10^{-6}
D	N-PSK53A	N-LAK7	-48.8909	-0.54463	14.5904	-14.1276	4.468×10^{-6}
E	N-SK14	N-LAK14	-47.9023	0.16197	15.4029	-13.4042	4.949×10^{-6}
F	N-BAK2	N-LAK8	-49.0944	1.0355	16.0228	-12.4993	4.729×10^{-6}

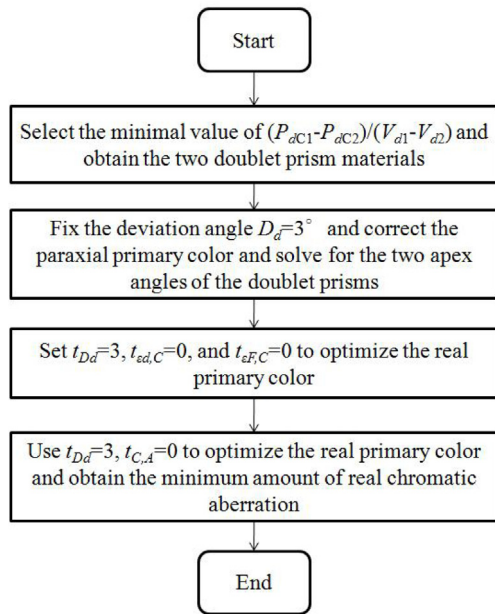


FIG. 7. Flow chart of optimization program for doublet prisms.

results for the optimized designs A to F are listed in Table 5. The chromatic aberration curves A to E corresponding to the optimal designs are shown in Fig. 8. This indicates that the proposed design method is effective in minimizing the chromatic aberration.

IV. CONCLUSION

A low-cost optimal double-prism method combined with the developed MATLAB program to correct chromatic aberration has been presented. In comparison of the doublet-prism designs shown in Tables 1 and 5, shows that the areas between the paraxial and real chromatic aberration curves are similar. We can quickly find the best combination of doublet prisms by choosing the materials with small differences in relative partial dispersion and large differences in V_d number, and minimizing the real

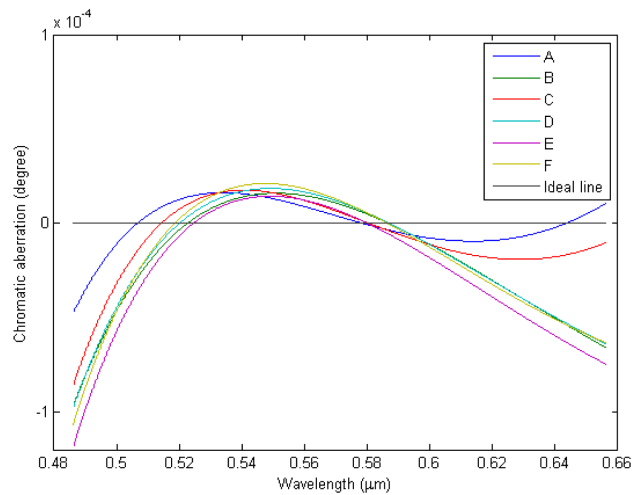


FIG. 8. Chromatic aberration curves A to E for the optimal designs.

chromatic aberration of doublet prisms by an optimization program.

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