A Measurement of the Hadronic Decay Current and the ν_{τ} -helicity in $\tau^- \rightarrow \pi^- \pi^- \pi^+ \nu_{\tau}$

The OPAL Collaboration

$\mathbf{A}\mathbf{b}\mathbf{s}\mathbf{t}\mathbf{r}\mathbf{a}\mathbf{c}\mathbf{t}$

The decay $\tau^- \to \pi^- \pi^- \pi^+ \nu_{\tau}$ has been studied using data collected with the OPAL detector at LEP during 1992 to 1994. Models of Kühn and Santamaria and of Isgur et al. are used to fit distributions of the 3π invariant mass squared as well as 2π invariant mass squared projections of the Dalitz plot, and the model dependent mass and width of the a₁ resonance are measured for both models. Neither model, however, is found to provide a completely satisfactory description of the data. The hadronic structure functions for this decay are measured in a model independent framework. No evidence for vector or scalar currents has been found. In addition, the parity violating asymmetry parameter is measured in a model independent way to be $\gamma_{VA} = 1.29 \pm 0.26 \pm 0.11$.

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1 Introduction

Semihadronic τ decays provide an ideal laboratory to study strong interactions in a region currently not accessible to precise theoretical calculations. The decay $au^- o \pi^- \pi^- \pi^+
u_{ au}^{-1}$, studied in this paper, is expected by the partially conserved axial-vector current hypothesis (PCAC) and by G-parity conservation to be dominated by the axial-vector current, mainly the a_1 resonance, through the decay $\tau^- \to a_1^- \nu_{\tau}$ followed by the decay chain $a_1^- \to \rho^0 \pi^-$ and $ho^0 o \pi^+ \pi^-$. The correct modelling of the $au^- o \pi^- \pi^- \pi^+
u_ au$ decay dynamics is important in a variety of studies, from setting limits on the τ neutrino mass using three-prong τ decays to measuring the τ polarization. Based on a previous paper [1], two different approaches have been used to study the $\tau^- \rightarrow \pi^- \pi^- \pi^+ \nu_{\tau}$ decay. First, the model of Kühn and Santamaria [2], which is used to model the $\tau^- \to \pi^- \pi^- \pi^+ \nu_{\tau}$ decay in TAUOLA 2.4[3], and the model of Isgur, Morningstar, and Reader [4] are both compared with the OPAL data. The a₁ resonance parameters are extracted for both models, and the comparison between the data and model predicted distributions is discussed. In the second approach, a model independent analysis is used to extract the structure of the weak hadronic current using a general description of hadronic τ decays as proposed by Kühn and Mirkes [5]. In this paper, the OPAL data collected in 1994 has been combined with the previously analysed 1992 and 1993 data, allowing the measurement of the model independent structure functions in the Dalitz plane. In addition, non-axial-vector contributions in the decay have been investigated.

A brief description of the OPAL detector is given in Section 2. The data selection, based on a likelihood method, is described in Section 3, and the theoretical framework of the $\tau^- \to \pi^- \pi^- \pi^+ \nu_{\tau}$ decay is presented in Section 4. In Section 5, the two models are compared with OPAL data, and the a_1 resonance parameters are extracted for each model. The structure functions are measured in section 6 and compared with model predictions. In Section 7, vector and scalar contributions to the $\tau^- \to \pi^- \pi^- \pi^+ \nu_{\tau}$ decay are measured using a model independent as well as a model dependent approach. The measurement of the parity violating asymmetry parameter γ_{VA} , in both the model independent and model dependent frameworks, is described in Section 8. Finally, the results are summarized in Section 9.

2 The OPAL detector

A detailed description of the OPAL detector can be found in [6]. Only the most important elements for this analysis are mentioned here.

The innermost detector for the measurement of charged tracks is a silicon microvertex detector. Outside the microvertex detector is the central tracking system, consisting of a precision vertex drift chamber, a large volume jet chamber, and a set of z-chambers which provide measurements of the track coordinates along the beam direction. Two tracks can be resolved by the central tracking system when separated by 2.5 mm or more. The central tracking detector is immersed in a 0.435 T axial magnetic field. The momentum resolution of the jet chamber is approximately $\sigma_{p_t}/p_t = \sqrt{0.0004 + (0.0015p_t)^2}$, where the momentum p_t , in GeV, is the component transverse to the beam direction. The resolution on the invariant mass of the 3π system can be parametrized as $\sigma(Q) = 0.011 + 0.011Q^2$, where Q is in GeV.

¹References in this paper to specific charge states apply to the charge conjugate states also.

The jet chamber also provides measurements of the specific energy loss of tracks in gas, with a resolution of $\sigma(dE/dx)/(dE/dx) = 3.5\%$ for tracks with a full 159 samplings.

The electromagnetic energy is measured by a lead-glass calorimeter located outside the magnet coil and in the two end caps, while hadronic energy is measured by several planes of limited streamer tubes which are interleaved with the iron layers of the magnet return yoke. The energy resolution of the lead-glass calorimeter for 45.6 GeV electrons is $\sigma_E/E = 2.1\%$ in the barrel region and $\sigma_E/E = 3.1\%$ in the two end caps. The lead-glass calorimeter position resolution is about 11 mm.

A preshower system (presampler) is situated in front of the lead-glass calorimeter to improve the position and energy measurement of electromagnetic showers initiating in the magnet coil. Finally, the magnet return yoke is surrounded by a muon detector.

3 Selection of $\tau^- \rightarrow \pi^- \pi^- \pi^+ \nu_{\tau}$ decays

The selection of $\tau^- \to \pi^- \pi^- \pi^+ \nu_{\tau}$ candidate events, outlined below, differs only slightly from the selection described in [1]. 114381 τ pairs have been selected, irrespective of the decay mode, from the 1992 – 1994 data sample using the τ pair preselection described in [7]. The polar angle θ_{jet} of each τ -jet relative to the beam direction is determined using charged tracks and clusters in the lead-glass calorimeter. Events are selected only if the average of $|\cos \theta_{jet}|$ for the two jets is less than 0.95. The 1992 – 1994 data sample represents 74% of the data collected at center-of-mass energies around $\sqrt{s} = M_{Z^0}$ with the OPAL detector at LEP, and corresponds to an integrated luminosity of 104 pb⁻¹.

For the Monte Carlo simulation we have used KORALZ 4.0 [8] to produce a sample of approximately four times the number of events in the data sample. A modified version² of TAUOLA 2.4 [3] is used to generate the τ leptons and model their decays, where the model of Kühn and Santamaria [2] is incorporated for the $\tau^- \to \pi^- \pi^- \pi^+ \nu_{\tau}$ decay. The Monte Carlo generated events are passed through a full simulation of the OPAL detector [11].

The $\tau^- \rightarrow h^- h^- h^+ \nu_{\tau}$ candidates have been selected from the τ pair sample using a channel likelihood method [12]. Four variables are used in the likelihood selection to discriminate against specific background channels. Background from one-prong decays accompanied by an additional pair of electron and positron tracks from photon conversion is suppressed by using the specific energy loss (dE/dx) to separate pions from electrons, and by using the probability of the χ^2 of a 3-dimensional vertex fit of the three tracks. Three-prong events with additional neutrals in the final state are separated from the signal channel by using the calorimetric energy sum divided by the sum of the track momenta, and also the sum of the energy of the reconstructed photons in the decay.

Reference samples have been selected for each of the four variables by applying stringent cuts on the three variables not under examination and also using information from the presampler. Although the overall agreement is satisfactory, some discrepancies between data and Monte Carlo have been observed. The Monte Carlo reference distributions have therefore been modified for the final data selection according to correction functions taken from the comparison.

²Unlike the standard version of TAUOLA2.4, the description of the $\tau^- \to \pi^- \pi^- \pi^+ \pi^0 \nu_{\tau}$ decay is taken here from [9]. In this description, the modelling of the ρ and ω resonances is in better agreement with the data [10].

From the selected $\tau^- \rightarrow h^- h^- h^+ \nu_{\tau}$ sample, final states with kaons are suppressed by applying a cut on the specific energy loss of the tracks. Since the events have to be kinematically well reconstructed for the following analysis, a cut is also applied on the probability of the χ^2 of the three-dimensional vertex fit. The tracks of the remaining events have been constrained to the fitted vertex and the four-momenta then re-evaluated. Finally, events whose values of the reconstructed kinematical variables lie outside the physical region are rejected. A total of 7443 events pass the full selection criteria, with an estimated purity of $(84.8\pm2.2)\%$. The error is dominated by the uncertainty in the branching ratio of three-prong decays with kaons in the final state, and small discrepancies in the reference samples used for the likelihood selection between data and Monte Carlo. Estimated background contributions are itemized in table 1.

4 Theoretical description of the decay

The partial decay width of the decay $au^- o \pi^- \pi^- \pi^+
u_ au$ can be written as

$$d\Gamma \left(\tau^{-} \to \pi^{-} \pi^{-} \pi^{+} \nu_{\tau}\right) = \sum_{\mu\nu} \frac{G_{F}^{2}}{4m_{\tau}} \cos^{2} \theta_{C} L_{\mu\nu} H^{\mu\nu} dPS^{(4)}$$
$$= \sum_{X} \frac{G_{F}^{2}}{4m_{\tau}} \cos^{2} \theta_{C} L_{X} W_{X} dPS^{(4)}.$$
(1)

 G_F is the Fermi constant, θ_C the Cabbibo angle, m_{τ} is the mass of the τ lepton and dPS⁽⁴⁾ symbolizes the phase space integration. The sixteen leptonic functions L_X (X = A, B...I, SA, ...SG) are symmetric and antisymmetric combinations of the components of the leptonic tensor $L_{\mu\nu}$. The hadronic structure functions W_X , the subject of our measurement, are composed in the same way from the hadronic tensor $H_{\mu\nu}$ [5].

The L_X can be calculated within the framework of the electroweak theory as functions of the τ polarization P_{τ} , the parity violating asymmetry parameter γ_{VA} , the invariant mass squared $Q^2 = (p_1 + p_2 + p_3)^2$ of the hadronic system, and four decay angles α , β , γ , and $\cos \theta^*$. In the Standard Model, $\gamma_{VA} = 2g_V g_A / (g_V^2 + g_A^2) = 1$, where g_V and g_A are the vector and axial-vector couplings in the τ decay. The definitions of the decay angles and the detailed form of the L_X can be found in [5]. Assuming universality of the neutral current couplings as predicted by the Standard Model, the value for $P_{\tau} = -0.144 \pm 0.003$ [13] is taken from a Standard Model fit which has very little dependence on measurements in the τ sector.

The hadronic structure functions W_X depend on the four-momenta of the outgoing pions in a Lorentz invariant way, that is, $W_X \equiv W_X (Q^2, s_1, s_2)$. The Dalitz plot variables s_1 and s_2 are defined in terms of the pion momenta as $s_1 = (p_2 + p_3)^2$ and $s_2 = (p_1 + p_3)^2$, with the labels chosen such that $|\vec{p}_2| > |\vec{p}_1|$ for the two like-sign pions and p_3 refers to the unlike-sign pion. In the most general description of the hadronic decay current, contributions from pseudoscalar, vector and axial-vector components have to be taken into account [14]. However, the $\tau^- \to \pi^- \pi^- \pi^+ \nu_{\tau}$ decay is dominated by the axial-vector current, decaying predominantly through the decay chain $\tau^- \to a_1^- \nu_{\tau}$, $a_1^- \to \rho^0 \pi^-$ and $\rho^0 \to \pi^+ \pi^-$. Vector currents are not expected because of G-parity conservation, and pseudoscalar contributions should be small due to the PCAC hypothesis. The detailed structure of the hadronic current cannot, however, yet be predicted from theory. Furthermore, there is no way to derive the decay structure from e^+e^- data as can be done for decays with an even number of pions in the final state through the conserved vector current hypothesis (CVC). Chiral perturbation theory methods can be used in the low energy region [15], but in the resonance region accessible here, only model predictions are available.

For this work, two techniques are used to measure the structure of the hadronic current:

- 1. The models give predictions for the structure functions and therefore the shapes of the distributions of the kinematic variables. The comparison between data distributions and model predictions is a measure of the quality of the model. The model parameters, such as the mass and width of the a_1 meson, can also be extracted experimentally.
- 2. The hadronic structure functions can be extracted directly in a model independent approach. For a pure axial-vector current, only four out of 16 structure functions contribute. Using the notation defined in [5], these four structure functions are W_A , W_C , W_D and W_E .

5 Model analysis of the three-pion and two-pion mass squared distributions

Two models for the $\tau^- \to \pi^- \pi^- \pi^+ \nu_{\tau}$ decay will be investigated in this analysis. These are the models of Kühn and Santamaria [2] and of Isgur et al. [4], henceforth referred to as the KS model and IMR model, respectively. The KS model uses point-like strong form factors, and incorporates only the lowest dimensional Born term in the decay amplitude. In the present analysis, the $\rho(1450)$ is included in the KS model parametrization with a strength $\beta_{o(1450)} = -0.145$, as specified for model 1 of table 1 in ref. [2]. The IMR model, in contrast, uses strong form factors with full off-shell dependence, derived from a flux-tube breaking model [16]. The IMR model is formulated with two distinct $a_1 \rho \pi$ couplings which allows a prediction of the D/S amplitude ratio, the ratio of the amplitudes for the two possible angular momentum states of the intermediate $\rho\pi$ state. For the IMR model, the K^{*}K decay channel is allowed to contribute to the total decay width, however the pseudoscalar contribution $(\pi(1300) \text{ production})$ is not included in the present analysis since the decay is dominated by the axial-vector current $(W_{SA}(Q^2, s_1, s_2) = 0)$. Several effects, such as model deficiencies and possible nonresonant contributions, are accounted for in the IMR model by employing a three parameter polynomial background term. Further details of the models can be found in [2] and [4], and a comparison of the phenomenology of the two models in [17].

Least-squares fits between predicted and data distributions have been carried out for both the models. The 3π invariant mass squared distribution is used for both the KS and IMR model fits. For the IMR model, three 2π invariant mass squared Dalitz-plot projections in different Q^2 intervals are also used in order to measure the D/S amplitude ratio. The three Dalitz-plot projections are formed by cutting around the ρ mass squared at $0.5 < s_1 < 0.7 \,\text{GeV}^2$ and then projecting onto s_2 , and vice versa, for three separate intervals in Q^2 . The polynomial background term in the IMR model is employed when fitting the 3π mass squared distribution, but not for the three 2π mass squared projections since the cut on the ρ mass squared should suppress any possible nonresonant contributions. The non- 3π background, the selection efficiency, and the OPAL detector resolution for each of the four histograms are estimated by analysing Monte Carlo simulated events. The non- 3π background is subtracted from each histogram, and then each histogram is corrected for efficiency. The detector resolution is accounted for by folding into the fit function the estimated resolution function. The model fits, shown in fig. 1 and summarized in table 2, will be discussed below.

The systematic errors on the a_1 resonance parameters are summarized in table 3. Several checks were made concerning the background. The effects of removing the cut against kaons and the effects of using the standard version of TAUOLA 2.4 [3] to model the background from $\tau^- \rightarrow \pi^- \pi^- \pi^+ \pi^0 \nu_{\tau}$ decays were investigated. For the kaon cut variations, half of the change from the nominal fits is taken as the error, reflecting the uncertainty in the corresponding branching ratios. The background fraction was also varied by ± 0.020 from the nominal value of $f_{bgd} = 0.152$. The effects of the detector resolution were investigated by varying the mass resolution by ± 10 %. This has a negligible effect on the extracted parameters.

5.1 The KS model fits

As noted above, the $a_1 \max m_{a_1}$ and width Γ_{a_1} are extracted using the KS model by fitting the 3π distribution. The normalization term for the 3π distribution is also allowed as a free parameter. In the previous OPAL a_1 model analysis [1], the 3π and three 2π distributions were fitted simultaneously with the KS model, using one normalization for all four histograms. There was already some evidence in [1] that the normalization for the 2π distributions was lower than that for the 3π distribution. This discrepancy is apparently due to the cut on the ρ mass squared when forming the 2π distributions, since the model overestimates the ρ peak contribution. With the improved statistics of the present study, the discrepancy is even more serious. With the present data, the $\chi^2/d.o.f$. from a global fit of the 3π and three 2π distributions with the KS model is 111/49, making the extraction of the resonance parameters from a global fit unreliable.

As can be seen in fig. 1, the KS model gives a reasonably good description of the shape of the 3π distribution. The three 2π distributions shown for the KS model are not fits, but are derived from the parameters, including the normalization, obtained from the fit to the 3π distribution. The model is significantly high in the region of the ρ peak of the 2π distributions. If the three 2π distributions are fitted separately from the 3π distribution, with the a_1 mass and width fixed at the values determined from the fit to the 3π distribution and only the normalization allowed as a free parameter, the normalization of the fitted 2π distributions is found to be approximately 10% lower than that of the 3π distribution. This suggests the presence of contributions to the decay not predicted by the model. Such contributions would affect the 3π and 2π plots differently because of the cut on the ρ resonance region when forming the 2π plots.

5.2 The IMR model fits

With the IMR model fit, the normalization is applied only to the part of the 3π distribution lying above the polynomial background. As noted in [1], this serves to compensate the normalization discrepancy between the 3π and the three 2π distributions, for which the polynomial background is not employed. A global analysis of all four histograms can therefore be carried out with the IMR model. In order to extract the D/S amplitude ratio, the strengths of the $f_{\mathbf{a}_1 \rho \pi}$ and $g_{\mathbf{a}_1 \rho \pi}$ form factors (see ref. [4]) are allowed to vary independently from their nominal flux-tube breaking model values. The relative strengths of these two form factors are most sensitive to the shapes of the three 2π distributions. All other form factor parameters are held fixed at their nominal values, $\beta_{HO} = 0.4 \text{ GeV}$ and $\gamma_{\circ} = 0.39$. For the fits to the data with the IMR model, the free parameters of the fit are the \mathbf{a}_1 mass, the overall normalization, the three parameters which govern the strength and shape of the polynomial background underlying the 3π distribution, and the two strengths for the $f_{\mathbf{a}_1 \rho \pi}$ and $g_{\mathbf{a}_1 \rho \pi}$ form factors.

As can be seen in fig. 1, the IMR model also gives a reasonably good description of the 3π distribution, with χ^2 = 34.3 for 23 bins. As mentioned above, the polynomial background term employed by the IMR model serves as a correction for the inconsistencies seen with the KS model fit. However, if the polynomial background is excluded from the IMR model, the χ^2 increases to 138.7 for 48 *d.o.f.* and the extracted parameters shift significantly. The three parameters for the polynomial background of the IMR model fit are $c_1 = -1.86$, $c_2 = 5.65$, and $c_3 = -0.78$ (see [4] for the parametrization of the polynomial background). These three parameters are highly correlated and have errors ranging from 50% to 130%. The normalization for the polynomial background term is such that the background contribution is $(13.8\pm2.4)\%$ of the total 3π distribution, where the error is statistical only. As can be seen in table 2, the a₁ mass and width extracted from the IMR model fit differ significantly from those extracted from the KS model fit. This has been shown in [17] to be due primarily to the employment of off-shell dependent strong form factors by the IMR model, in contrast to the pointlike strong form factors used by the KS model. The overall features of the 2π distributions are also reproduced by the IMR model. As can be seen in fig. 1(c), however, the model is systematically low in the low $s_{1,2}$ region. The results for the strong decay on-shell $a_1 \rho \pi$ form factors and the D/S amplitude ratio of the IMR model fit are $f_{\mathrm{a}_1}, m_{\mathrm{a}_1}^2, m_{
ho}^2) = 5.0 \pm 0.1$ GeV, $g_{a_1\rho\pi}(m_{a_1}^2, m_{\rho}^2) = 3.7 \pm 1.3$ GeV, and $D/S = -0.10 \pm 0.02 \pm 0.02$. These values are in reasonable agreement with the predictions of $f_{a_1\rho\pi}(m_{a_1}^2,m_{\rho}^2) = 4.8 \text{ GeV}, g_{a_1\rho\pi}(m_{a_1}^2,m_{\rho}^2) = 6.0$ GeV, and D/S = -0.15 from the flux-tube breaking model [4], which is used by the IMR model to compute the strong form factors.

5.3 Further discussion of the model fits

The problems noted above with the model fits to the data can be seen more clearly if we investigate the 2π mass squared Dalitz-plot projection with no cuts on either the a_1 mass or the ρ mass. The data have been overlaid by the two models in fig. 2, with the model parameters held fixed at their nominal best fit values. The normalization for the KS model was taken from the fit to the 3π distribution, and the normalization for the IMR model, determined from the 3π distribution in the IMR global fit, has also been included for that model.

It is clearly evident that the KS model overestimates the ρ peak contribution relative to the high and low s_1 regions, especially the low s_1 region. The total χ^2 for the KS model overlay is 95.4 for 28 bins. The IMR model gives an improved description of the uncut 2π distribution, although it remains systematically low in the low s_1 region. The IMR model's inclusion of the $g_{a_1\rho\pi}$ term is responsible for the steeper rise toward the low s_1 region. The total χ^2 for the IMR model overlay is 50.2 for 28 bins. Without the inclusion of the polynomial background term, the total χ^2 for the IMR model overlay increases to 115 for 28 bins. To investigate whether the apparent poor modelling of the data in the low s_1 region could be due to incorrect modelling of the $\tau^- \to \pi^- \pi^- \pi^+ \pi^0 \nu_{\tau}$ decay mode, which is the predominant background in this region, a data selection was generated with the purity improved to 89.8 %. The improvement in purity was aimed primarily at reducing the background due to $\tau^- \to \pi^- \pi^- \pi^+ \pi^0 \nu_{\tau}$ decays. The ratio of data events to Monte Carlo simulated events remains unchanged in the low s_1 region with this selection, which provides evidence that the discrepancy of the models with the data in the low s_1 region is not due to incorrect background modelling.

It should be pointed out that the Q^2 dependence of the polynomial background term of the IMR model has largely been integrated out when it is projected onto the s_1 axis for the 2π mass projection. The residual s_1 dependent shape is due to the kinematic boundaries of the physical region in (Q^2, s_1, s_2) space. Also, since the polynomial background term is a function of Q^2 only, the IMR model is of limited use for Monte Carlo simulation of the $\tau^- \rightarrow \pi^- \pi^- \pi^+ \nu_{\tau}$ decay. The limited available statistics prohibit a reliable determination of the the full (Q^2, s_1, s_2) dependence of the background term. Nonetheless, in the framework of the IMR model it is evident that the data do require some sort of additional term with a magnitude of $(13.8 \pm 2.4)\%$.

The high model dependence of the measured a_1 resonance parameters, and also the failure of either model to provide a completely satisfactory description of the data, strongly suggest that caution must be exercised when carrying out measurements which rely on models for predicting the decay dynamics in $\tau^- \to \pi^- \pi^- \pi^- \pi^+ \nu_{\tau}$.

6 Extraction of the structure functions

The hadronic decay current can be measured in a model independent way by extracting the hadronic structure functions directly. This can be done in two steps.

1. As the axial-vector current dominates the decay, all structure functions other than W_A , W_C , W_D , and W_E can be fixed to zero. To measure the Q^2 -dependence, the structure functions are integrated over the Dalitz plane,

$$w_X\left(Q^2\right) = \int W_X\left(s_1, s_2, Q^2\right) \mathrm{d}s_1 \mathrm{d}s_2 , \qquad (2)$$

and the selected events are put into nine equal sized Q^2 bins between 0.5 and 2.75 GeV². No binning is used for the angles.

2. To study the full structure of the hadronic decay current, and accepting larger errors, the events are binned not only in Q^2 but also in (s_1, s_2) , as shown in table 4. This is only possible due to the increased data sample compared with [1]. Structure functions that include scalar (W_{SB} and W_{SD}) and vector (W_F, W_G, W_H , and W_I) contributions have also been taken into account, neglecting only those that are pure vector (W_B), pure scalar (W_{SA}), or interference terms between vector and scalar currents (W_{SF}) as they are expected to be very small. Since the respective angular dependences of W_G and W_{SD} and of W_I and W_{SB} are very similar, they cannot be separated with the available data sample. Therefore they are combined in the fit parameters $X_1 = -\bar{K}_3/\bar{K}_2W_G - W_{SD}$ and $X_2 = -\bar{K}_3/\bar{K}_2W_I + W_{SB}$ (See [5] for the definitions of \bar{K}_3 and \bar{K}_2). Both measurements can be made, following the method described in [1], by applying an extended maximum likelihood fit [18] to the data events. With z representing the kinematic variables Q^2 , s_1 , s_2 , $\cos \theta^*$, $\cos \beta$, and γ , and $dz = dQ^2 ds_1 ds_2 d \cos \theta^* d \cos \beta d\gamma$, the likelihood function can be written as

$$(\ln \mathcal{L})_j = \sum_{i}^{N_j} \ln\left(\frac{\mathrm{d}\Gamma}{\mathrm{d}z}\left(z_i; W_X^j\right) \frac{N}{C_{corr}\Gamma_{3\pi}}\right) - \Gamma_{\Delta_j}\left(W_A^j\right) \frac{N}{C_{corr}\Gamma_{3\pi}}.$$
(3)

Here the W_X^j are the average values of the structure functions W_X within bin j (referring only to Q^2 in the first step and to Q^2 , s_1 , s_2 in the second step). They are the parameters of the fit. N_j is the number of events in bin j and N is the total number of selected events. $\Gamma_{3\pi}$ is the partial decay width of the τ decay into three pions, calculated from ref. [13] $(\Gamma_{3\pi}/\Gamma_{tot} = 9.31$ %, with $\Gamma_{3\pi} = 2.11 \times 10^{-4} \text{ eV}$). The factor C_{corr} (with $C_{corr} = 0.996$) corrects $\Gamma_{3\pi}$ for events with Q^2 outside of the selected range of 0.5 GeV² $< Q^2 < 2.75 \text{ GeV}^2$. The decay distribution $d\Gamma/dz$ is defined in eq. (1). The normalization term Γ_{Δ_j} is the integral of $d\Gamma/dz$ over the full ranges of the kinematic angles and the bin width. Because of the increased value of BR($\tau^- \to \pi^- \pi^- \pi^+ \nu_{\tau}$) relative to the value taken in the previous analysis [1], the integral and therefore the values of the structure functions have also increased.

The detector resolution has been taken into account by applying a smearing function to each of the kinematic variables on an event by event basis. To correct for migration effects between neighbouring bins, a bin to bin correction is included [19]. A smooth efficiency correction derived from Monte Carlo is incorporated in the fit by multiplying $d\Gamma/dz$ by a correction function for each of the respective four (in the case of $w_X(Q^2)$) and six (for the $W_X(Q^2, s_1, s_2)$ measurement) kinematic variables. The background is included in the fit by replacing $d\Gamma/dz$ in eq. (3) by

$$f_{sig} \frac{\mathrm{d}\Gamma}{\mathrm{d}z}(z; W_X) + f_{bgd} \frac{\mathrm{d}\Gamma}{\mathrm{d}z}(z; W_X^{bgd}) , \qquad (4)$$

where $f_{sig} = 1 - f_{bgd}$ and f_{bgd} are the overall fractions of signal and background, and W_X^{bgd} are the background structure functions taken from the Monte Carlo prediction. These background structure functions have no physical meaning — they are simply a way to include the background in the fit function.

6.1 Results

The results of the measurements of the hadronic structure functions w_A , w_C , w_D , and w_E are presented in fig. 3 and table 5. The measurements of the hadronic structure functions W_A , W_C , W_D , W_E , W_F , W_H , X_1 , and X_2 are summarized in tables 6 and 7.

The systematic errors have been derived for both measurements in a similar way. The uncertainty in the background and migration between bins dominate the systematic errors. The different contributions have been estimated in the same way as described in section 5. The background fraction f_{bgd} has been changed in the fit by ± 0.020 . The cut against three-prong events with kaons was removed and half of the change is quoted as the error. To derive the uncertainty from the background description, the change from varying the background structure functions W_X^{bgd} within their statistical errors and the change obtained

when using the original version of TAUOLA 2.4 for the description of the background from $\tau^- \rightarrow \pi^- \pi^- \pi^+ \pi^0 \nu_{\tau}$ decays are added in quadrature.

Effects due to detector efficiency and resolution were estimated by varying the correction functions for the efficiencies within one standard deviation and by increasing by 10% the widths of the Gaussians for the resolution simultaneously for all kinematic variables. The migration corrections have been varied within the errors. Furthermore, the value taken for P_{τ} has been varied within the errors (see section 4).

Table 8 itemizes the estimated systematic error contributions averaged over all bins. The systematic error determined for each bin separately is used in tables 5–7, where the measured values including statistical and systematic errors are given bin by bin. The correlations between the values of the structure functions typically range between -15% and +15%.

6.2 Comparison of the structure functions with the model predictions

In fig. 4 the measured structure functions w_A , w_C , w_D , and w_E are compared with the KS and IMR model predictions using the fit parameters extracted in section 5. For the IMR model, the polynomial background term is included in w_A . The ratio w_X/w_A , which is only weakly dependent on m_{a_1} and Γ_{a_1} , is plotted for each of the other three structure functions w_C , w_D , and w_E . For w_A , which is closely related to the a_1 resonance shape, the KS model fits the data distribution very well, with $\chi^2_{KS} = 6.2$ for 9 bins. The IMR model, however, shows some discrepancies, with $\chi^2_{IMR} = 16.9$ for 9 bins. The structure visible in the IMR model prediction at $Q^2 = 1.9 \text{ GeV}^2$, which is related to the $a_1 \rightarrow K^*\overline{K}$ decay channel, is not visible in the data. This suggests that the IMR modelling of that decay channel is not correct. For the description of w_C/w_A , w_D/w_A , and w_E/w_A , both models agree well with the measurement, with $\chi^2_{KS} = 19.6$ for 27 bins and $\chi^2_{IMR} = 17.6$ for 27 bins.

To demonstrate how the structure functions are distributed in the Dalitz plane, the axialvector structure functions W_A , W_C , W_D , and W_E are shown in fig. 5 in comparison with the KS model. The results for the KS model are evaluated at $Q^2 = 1.3 \text{ GeV}^2$, while the fit results are integrated over the range $1.21 \text{ GeV}^2 < Q^2 < 1.44 \text{ GeV}^2$. The structure functions W_F , W_H , X_1 , and X_2 all vanish for the model predictions.

7 Non-axial-vector contributions

If there are non-axial-vector contributions in the hadronic decay current, they should be visible in the angular distributions and therefore manifest themselves in the hadronic structure functions W_F and W_H and in the fit parameters X_1 and X_2 . The fit results, shown in fig. 6, can therefore be compared to the null prediction of vanishing vector and scalar components. This leads to $\chi^2 = 81.2$ for 84 *d.o.f.* No deviation from a pure axial-vector current is observed.

For a quantitative measurement of the non-axial-vector contributions, a different method has been applied. Because of strong correlations between W_A , W_B and W_{SA} the fit result for W_A^{fit} includes possible scalar or vector contributions. The pure axial-vector part of W_A can be calculated from W_C , W_D and W_E ($W_A^2 = W_C^2 + W_D^2 + W_E^2$) since these structure functions are independent of vector or scalar contributions.³ An estimate of the non-axialvector components can be calculated as $\Delta^{non-AV} = W_A^{fit} - \sqrt{W_C^2 + W_D^2 + W_E^2}$. This

 $^{{}^{3}}W_{SF}$, a combination of vector and scalar components, is neglected here.

leads to the first model independent measurement of non-axial-vector contributions, with an upper limit at the 95% confidence level of

$$rac{\Gamma^{non-AV}(au^- o \pi^- \, \pi^- \, \pi^+ \,
u_ au)}{\Gamma^{tot}(au^- o \pi^- \, \pi^- \, \pi^+ \,
u_ au)} ~<~ 26.1\% \,.$$

The deviation from zero non-axial-vector contributions was also measured using samples of Monte Carlo generated events which include different amounts of non-axial-vector contributions. In addition to the systematic errors considered in the previous section, an error of 14% from this test with Monte Carlo events has been included.

The contribution of a scalar component to the decay can be measured model dependently under the assumption that it can be fully described through the decay chain $\tau^- \rightarrow \pi^-(1300)\nu_{\tau}$, $\pi^-(1300) \rightarrow \rho^0 \pi^-$ and $\rho^0 \rightarrow \pi^+ \pi^-$. In this approach, the axial-vector current is described by the KS or IMR model. The scalar contribution can be incorporated in both models; only the strength of the scalar current is not fixed. The structure functions in eq. 3 can now be replaced by the model predictions when performing the extended maximum likelihood fit, with the contribution from the scalar current being the only fit parameter. The result of the fit shows no evidence for a scalar current, and leads to the 95% confidence level upper limit

$$rac{\Gamma^{scalar}(au^- o \pi^-(1300)\,
u_ au\;)}{\Gamma^{tot}(au^- o \pi^-\,\pi^-\,\pi^+\,
u_ au)} < 0.84\%\;,$$

in agreement with a model dependent analysis by ARGUS [20]. In addition to the systematic errors described above, the dependence on model (KS or IMR) used for the axial-vector part of the decay has been investigated and included in the systematic error.

8 The parity violating asymmetry parameter γ_{VA}

As explained in section 4, the leptonic current depends on the parity violating asymmetry parameter γ_{VA} . For the measurement of the hadronic structure functions described in the previous sections, the value was fixed at the Standard Model value of $\gamma_{VA} = 1$. If instead γ_{VA} is varied in the fit along with the structure functions, the parity violating asymmetry parameter can be measured. Non-axial-vector contributions are neglected here. The likelihood function summed over all bins is shown in fig. 7, leading to a model independent measurement of $\gamma_{VA} = 1.29 \pm 0.26 \pm 0.11$, consistent with the Standard Model prediction of $\gamma_{VA} = 1$ for left-handed tau neutrinos. This result is in agreement with a recent measurement by SLD [21] where the sign of the helicity of the tau neutrino has also been measured model independently, and with other more precise measurements based on different techniques [22]. The systematic error is derived from the same variations described above. The dominant effects come from the uncertainty in the detector resolution and the background, especially from three-prong events with kaons in the final state. The error contributions are summarized in table 9.

The model independent result can be compared to the model dependent measurements when the fit parameters W_X^j in eq. (3) are replaced by the hadronic structure functions derived from the two models. The model dependent values obtained for the parity violating asymmetry parameter are $\gamma_{VA}^{\text{KS}} = 0.87 \pm 0.16 \pm 0.04$ for the KS model and $\gamma_{VA}^{\text{IMR}} = 1.20 \pm 0.21 \pm 0.14$ for the IMR model. The systematic errors for the model dependent measurements have been derived from the same variations described above, and also by varying the model parameters within the errors given in section 5. A summary of the different error contributions is given in table 9. The largest systematic error contribution for the IMR model is due to the uncertainty in the D/S amplitude ratio. No variation of this parameter is possible for the KS model. The strong model dependence demonstrated in the measurements again emphasizes that caution must be exercised when carrying out precision measurements which rely on model descriptions for the hadronic decay current in $\tau^- \to \pi^- \pi^- \pi^+ \nu_{\tau}$.

9 Conclusions

We have studied the structure of the decay $\tau^- \to \pi^- \pi^- \pi^+ \nu_{\tau}$ using two different approaches. First, the models of Kühn and Santamaria [2] and of Isgur et al. [4] have been used to fit the distributions of the 3π invariant mass squared as well as 2π mass projections of the corresponding Dalitz plot. The a_1 resonance model parameters have been measured for both models, and are summarized in table 2. Both models describe reasonably well the shape of the 3π mass squared distribution. For the uncut 2π mass projection, however, the KS model overestimates the ρ peak, and both models underestimate the low $s_{1,2}$ region. By including the Q^2 dependent polynomial background term in the 2π mass projection for the IMR model, the agreement with the data is improved. This suggests the possibility that some additional contribution to the decay, other than the a_1 intermediate resonance, of magnitude (13.8 ± 2.4)% is required by the data within the framework of that model. The failure of either model to provide a completely satisfactory description of the data strongly suggests that caution must be used when carrying out measurements which rely on model descriptions for the decay dynamics in $\tau^- \to \pi^- \pi^- \pi^+ \nu_{\tau}$, and calls for further theoretical input to the modelling of this decay.

A model independent measurement has been presented of the structure functions w_A , w_C , w_D , and w_E , as well as W_A , W_C , W_D , W_E , W_F , W_H , X_1 , and X_2 . No evidence for non-axial-vector contributions in the decay current has been found. In the model independent approach we have obtained, at the 95% confidence level,

$$rac{\Gamma^{non-AV}(au^- o \pi^- \, \pi^- \, \pi^+ \,
u_ au)}{\Gamma^{tot}(au^- o \pi^- \, \pi^- \, \pi^+ \,
u_ au)} ~<~ 26.1\% ~.$$

When model descriptions for the decay are used, we obtain as the 95% confidence level upper limit

$$rac{\Gamma^{scatar}(au^- o \pi^-(1300)\,
u_ au^-)}{\Gamma^{tot}(au^- o \pi^-\,\pi^-\,\pi^+\,
u_ au^-)} < 0.84\% \,.$$

Finally, the value for the parity violating asymmetry parameter has been determined in a model independent way to be

$$\gamma_{VA} = -1.29 \pm 0.26 \pm 0.11$$
,

which is consistent with the Standard Model prediction of $\gamma_{VA} = 1$ for left-handed tau neutrinos. The model dependent values have also been measured, but demonstrate a strong model dependence in the value obtained.

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decay channel	background fraction
$ au^- o \pi^- \ \pi^- \ \pi^+ \ \pi^0 \ u_ au$	$(11.7\pm 0.5)\%$
$ au^- ightarrow { m K}^- \ \pi^- \ \pi^+ \ u_ au$	$(2.3\pm 0.3)\%$
$ au^- ightarrow \pi^- \mathrm{K}^- \mathrm{K}^+ u_ au$	$(0.5\pm 0.1)\%$
$ au^- ightarrow \pi^- \pi^- \pi^+ 2 \pi^0 u_ au$	$(0.3\pm 0.1)\%$
others	$(0.4\pm 0.1)\%$

Table 1: Estimated background fractions in the final data sample. The errors are thestatistical errors from the Monte Carlo only.

	Kühn et al. [2]	Isgur et al. [4]
$m_{\mathbf{a}_1} (\mathrm{GeV})$	$1.262 \pm 0.009 \pm 0.007$	$1.210 \pm 0.007 \pm 0.002$
Γ_{a_1} (GeV)	$0.621 \pm 0.032 \pm 0.058$	$0.457 \pm 0.015 \pm 0.017$
D/S amplitude ratio	_	$-0.10 \pm 0.02 \pm 0.02$
$\chi^2/d.o.f.$	$25.2/20~(3\pi)$	—
	$111/49~({ m global})$	$91.9/45~{ m (global)}$
polynomial background fraction		$(13.8 \pm 2.4)\%$

Table 2: Model parameters extracted from fitting the KS and IMR models to OPAL data. The errors quoted are statistical followed by systematic. Note that Γ_{a_1} and the D/S amplitude ratio for the IMR model are calculated quantities, not parameters of the fit. Also listed is the polynomial background fraction for the IMR model.

	KS model error		IMR model error		
	Δm_a	$\Delta\Gamma_a$	Δm_a	$\Delta\Gamma_a$	
	(GeV)	(GeV)	(GeV)	(GeV)	$\Delta D/S$
Kaon channels	± 0.002	± 0.014	± 0.001	± 0.005	± 0.01
$egin{array}{cccccccccccccccccccccccccccccccccccc$	± 0.006	± 0.055	± 0.001	± 0.016	± 0.01
modelling					
Background fraction	± 0.001	± 0.011	± 0.001	< 0.001	< 0.01
Detector resolution	± 0.003	± 0.007	± 0.001	± 0.002	< 0.01
Total systematic error	± 0.007	± 0.058	± 0.002	± 0.017	± 0.02
Statistical error	± 0.009	± 0.032	± 0.007	± 0.015	± 0.02

Table 3: Estimated error contributions for each of the KS and IMR model fits.

	$\sqrt{Q^2}$	s_1	s_2	N_{j}
	in (GeV)	in (GeV^2)	in (GeV^2)	-
Bin 1	0.8 - 1.0	$s_1^{min}-0.4$	$s_2^{min}-s_1$	417
Bin 2	0.8 - 1.0	0.4-0.5	$s_2^{min}-s_1$	462
Bin 3	0.8 - 1.0	$0.5-s_1^{max}$	$s_2^{min}-0.25$	359
Bin 4	0.8 - 1.0	$0.5-s_1^{max}$	$0.25-s_1$	140
Bin 5	1.0 - 1.1	$s_1^{min}-0.5$	$s_2^{min}-s_1$	392
Bin 6	1.0 - 1.1	0.5-0.65	$s_2^{min}-0.35$	537
Bin 7	1.0 - 1.1	0.5-0.65	$0.35 - s_1$	372
Bin 8	1.0 - 1.1	$0.65 - s_1^{max}$	$s_2^{min}-s_1$	315
Bin 9	1.1 - 1.2	$s_1^{min}-0.5$	$s_2^{min}-s_1$	247
Bin 10	1.1 - 1.2	0.5-0.7	$s_2^{min}-0.3$	352
Bin 11	1.1 - 1.2	0.5-0.7	0.3-0.5	377
Bin 12	1.1 - 1.2	0.5-0.7	$0.5-s_1$	324
Bin 13	1.1 - 1.2	$0.7-s_1^{max}$	$s_2^{min}-s_1$	408
Bin 14	1.2 - 1.4	$s_1^{min}-0.5$	$s_2^{min}-s_1$	137
Bin 15	1.2 - 1.4	0.5-0.7	$s_2^{min}-0.45$	461
Bin 16	1.2 - 1.4	0.5-0.7	$0.45 - s_1$	339
Bin 17	1.2 - 1.4	$0.7-s_1^{max}$	$s_2^{min}-0.6$	743
Bin 18	1.2 - 1.4	$0.7-s_1^{max}$	$0.6-s_1$	434
Bin 19	1.4 - 1.7	$s_1^{min}-0.7$	$s_2^{min}-s_1$	111
Bin 20	1.4 - 1.7	$0.7 - s_1^{max}$	$s_2^{min}-0.6$	173
Bin 21	1.4 - 1.7	$0.7 - s_1^{max}$	$0.6 - s_1$	209

Table 4: Binning employed in Q^2 , s_1 , and s_2 for the second structure function fit. $s_1^{min/max}$ and $s_2^{min/max}$ are the values at the phase space boundaries. Only the lower half of the Dalitz plane $(s_1 > s_2)$ is used in the fit.

$Q^2 \left({ m GeV}^2 ight)$	N_j	i	$v_A ({ m GeV}^4$)	ı	$v_C \; (\mathrm{GeV}^4)$)
0.5 - 0.75	334	32	± 6	± 18	0	± 34	± 21
0.75 - 1.00	1178	670	± 20	± 36	630	± 200	±70
1.00 - 1.25	1920	2316	± 59	± 77	1800	± 530	± 60
1.25 - 1.50	1793	3870	± 100	± 150	3800	± 1100	± 200
1.50 - 1.75	1133	4290	± 130	± 170	5900	± 1900	± 700
1.75 - 2.00	655	4140	± 180	± 260	2900	± 1900	± 500
2.00 - 2.25	269	3400	± 220	± 270	7300	± 3800	± 1400
2.25 - 2.50	106	3330	± 350	± 390	3300	± 7400	± 5700
2.50 - 2.75	55	2170	± 290	± 360	9400	± 6800	± 2800
		$w_D \; ({ m GeV}^4)$					
$Q^2 \left({ m GeV}^2 ight)$	N_j	ı	$v_D \ ({ m GeV}^4$)	ı	$v_E \ ({ m GeV}^4$)
$\boxed{\begin{array}{c} Q^2 \left({\rm GeV}^2 \right) \\ 0.5 - 0.75 \end{array}}$	N _j 334	1 v 24	$v_D \ ({ m GeV}^4 \ \pm 36$	± 24	v 	$v_E \ ({ m GeV}^4 \ \pm 27$) ±6
${\begin{array}{c} \hline Q^2 ~({\rm GeV}^2) \\ \hline 0.5-0.75 \\ \hline 0.75-1.00 \end{array}}$	$\frac{N_j}{334}$ 1178	24 160	$v_D ({ m GeV}^4 egg {\pm} 36 egg {\pm} 180$	(1) ± 24 ± 30	$\begin{array}{c c} & & & \\ & & -22 \\ & & 20 \end{array}$	$\frac{v_E \ ({\rm GeV}^4)}{\pm 27}$) extstyle e
$\begin{array}{c} Q^2 \left({\rm GeV}^2 \right) \\ \hline 0.5 - 0.75 \\ 0.75 - 1.00 \\ 1.00 - 1.25 \end{array}$	N _j 334 1178 1920	$ \begin{array}{c c} $	$\begin{array}{r} & \\ & \\ & \\ \hline & \\ & \\ \hline & \\ & \\ & \\ & \\$	(1) (± 24) (± 30) (± 100)	$\begin{array}{c c} & & \\ & -22 \\ & 20 \\ & -220 \end{array}$	$ \frac{v_E \left(\text{GeV}^4\right.}{\pm 27} \\ \frac{\pm 120}{\pm 270} $) $\pm 6 \\ \pm 50 \\ \pm 70$
$\begin{array}{c} Q^2 \left({\rm GeV}^2 \right) \\ \hline 0.5 - 0.75 \\ 0.75 - 1.00 \\ \hline 1.00 - 1.25 \\ \hline 1.25 - 1.50 \end{array}$	$\begin{array}{c c} N_{j} \\ \hline 334 \\ 1178 \\ 1920 \\ 1793 \end{array}$	$ \begin{array}{ c c c c } 224 \\ 160 \\ 1430 \\ 2500 \\ \end{array} $	$v_D ({ m GeV}^4) = \frac{\pm 36}{\pm 180} = \frac{\pm 530}{\pm 1000}$	$\begin{array}{c} \pm 24 \\ \pm 30 \\ \pm 100 \\ \pm 500 \end{array}$	$\begin{array}{c c} & & & & \\ & -22 & & \\ & 20 & & \\ & -220 & & \\ & -600 & & \end{array}$	$v_E ({ m GeV}^4) \ \pm 27 \ \pm 120 \ \pm 270 \ \pm 430 \ end{tabular}$) $\pm 6 \\ \pm 50 \\ \pm 70 \\ \pm 100$
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{c} N_{j} \\ \hline 334 \\ 1178 \\ 1920 \\ 1793 \\ 1133 \end{array}$	24 160 1430 2500 2900	$ \begin{array}{r} & v_D \ ({\rm GeV}^4 \\ \hline $	$\begin{array}{c} \pm 24 \\ \pm 30 \\ \pm 100 \\ \pm 500 \\ \pm 1000 \end{array}$	$ \begin{array}{c c} & & & \\ & -22 \\ & 20 \\ & -220 \\ & -600 \\ & -1180 \\ \end{array} $	$v_E ({ m GeV}^4 \ \pm 27 \ \pm 120 \ \pm 270 \ \pm 430 \ \pm 540 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$) $\pm 6 \\ \pm 50 \\ \pm 70 \\ \pm 100 \\ \pm 180$
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{c} N_{j} \\ \hline 334 \\ 1178 \\ 1920 \\ 1793 \\ 1133 \\ 655 \end{array}$	v 24 160 1430 2500 2900 900	$ \begin{array}{r} & v_D (\text{GeV}^4 \\ \hline \pm 36 \\ \pm 180 \\ \pm 530 \\ \pm 1000 \\ \pm 1700 \\ \pm 2500 \end{array} $	$\begin{array}{c} \pm 24 \\ \pm 30 \\ \pm 100 \\ \pm 500 \\ \pm 1000 \\ \pm 800 \end{array}$	$ \begin{array}{c c} & & & & \\ & -22 \\ & 20 \\ & -220 \\ & -600 \\ & -1180 \\ & -40 \\ \end{array} $	$ \begin{array}{r} & \\ \hline v_E ({\rm GeV}^4 \\ \hline \pm 27 \\ \pm 120 \\ \pm 270 \\ \hline \pm 270 \\ \pm 540 \\ \pm 540 \\ \pm 650 \end{array} $) ± 6 ± 50 ± 70 ± 100 ± 180 ± 240
$\begin{array}{c} Q^2 \left({\rm GeV}^2 \right) \\ \hline 0.5 - 0.75 \\ 0.75 - 1.00 \\ \hline 1.00 - 1.25 \\ \hline 1.25 - 1.50 \\ \hline 1.50 - 1.75 \\ \hline 1.75 - 2.00 \\ \hline 2.00 - 2.25 \end{array}$	$\begin{array}{c} N_j \\ \hline 334 \\ 1178 \\ 1920 \\ 1793 \\ 1133 \\ 655 \\ 269 \end{array}$	v 24 160 1430 2500 2900 900 800	$ \begin{array}{c} v_D \ ({\rm GeV}^4 \\ \hline \pm 36 \\ \pm 180 \\ \pm 530 \\ \pm 1000 \\ \pm 1700 \\ \pm 2500 \\ \pm 3800 \end{array} $	$\begin{array}{c} \pm 24 \\ \pm 30 \\ \pm 100 \\ \pm 500 \\ \pm 1000 \\ \pm 800 \\ \pm 500 \end{array}$	$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$	$ \begin{array}{r} & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ & $) ± 6 ± 50 ± 70 ± 100 ± 180 ± 240 ± 360
$\begin{array}{c} Q^2 \left({\rm GeV}^2 \right) \\ \hline 0.5 - 0.75 \\ 0.75 - 1.00 \\ 1.00 - 1.25 \\ 1.25 - 1.50 \\ 1.50 - 1.75 \\ 1.75 - 2.00 \\ 2.00 - 2.25 \\ 2.25 - 2.50 \end{array}$	$\begin{array}{c} N_j \\ \hline 334 \\ 1178 \\ 1920 \\ 1793 \\ 1133 \\ 655 \\ 269 \\ 106 \\ \end{array}$	v 24 160 1430 2500 2900 900 800 6600	$ \begin{array}{c} v_D \ ({\rm GeV}^4 \\ \hline \pm 36 \\ \pm 180 \\ \pm 530 \\ \pm 1000 \\ \pm 1700 \\ \pm 2500 \\ \pm 3800 \\ \pm 7200 \end{array} $	$\begin{array}{c} \pm 24 \\ \pm 30 \\ \pm 100 \\ \pm 500 \\ \pm 1000 \\ \pm 800 \\ \pm 500 \\ \pm 3300 \end{array}$	$\begin{tabular}{ c c c c c }\hline & & & & & & & & & & & & & & & & & & &$	$ \begin{array}{c} \hline \\ v_E ({\rm GeV}^4 \\ \hline \pm 27 \\ \pm 120 \\ \pm 270 \\ \pm 430 \\ \pm 540 \\ \pm 650 \\ \pm 770 \\ \pm 1300 \end{array} $	$\begin{array}{c} \pm 6 \\ \pm 50 \\ \pm 70 \\ \pm 100 \\ \pm 180 \\ \pm 240 \\ \pm 360 \\ \pm 400 \end{array}$

Table 5: The hadronic structure functions w_A , w_C , w_D , and w_E as measured in each Q^2 bin. For each structure function, the central value, statistical and systematic errors are given. N_j is the number of decays in the given Q^2 bin. The contributions shown in table 8 are included in the systematic errors.

		W_A			W_C	
Bin 1	1100	± 100	± 500	800	± 680	± 250
Bin 2	3100	± 180	± 390	3000	± 1200	± 400
Bin 3	8230	± 500	± 830	7800	± 4000	± 2300
Bin 4	9200	± 800	± 3300	2800	± 7800	± 3800
Bin 5	2780	± 140	± 540	1500	± 1600	± 600
Bin 6	10090	± 500	± 750	10300	± 4000	± 1200
Bin 7	12130	± 680	± 1410	1600	± 5500	± 2800
Bin 8	5630	± 370	± 920	3100	± 3200	± 900
Bin 9	3870	± 320	± 880	3800	± 3100	± 1100
Bin 10	9080	± 560	± 740	2900	± 4600	± 700
Bin 11	8000	± 460	± 920	14700	± 4100	± 2100
Bin 12	24700	± 1500	± 2500	37000	± 13000	± 5900
Bin 13	3290	± 200	± 390	3300	± 2000	± 600
Bin 14	1940	± 210	± 670	700	± 2600	± 1300
Bin 15	5830	± 310	± 750	1900	± 4000	± 900
Bin 16	11500	± 700	± 1500	13900	± 8300	± 2100
Bin 17	2810	± 120	± 230	2900	± 1500	± 400
Bin 18	9900	± 500	± 1100	15900	± 6700	± 1900
Bin 19	2750	± 290	± 530	-6500	± 5100	± 1400
Bin 20	1010	± 90	± 220	1800	± 1500	± 400
Bin 21	2940	± 220	± 730	6100	± 3700	± 1700
		W_D			W_E	
Bin 1	450	W_D ± 640	± 410	-250	$W_E = \pm 470$	± 130
Bin 1 Bin 2	450 500	$W_D \ \pm 640 \ \pm 1200$	$egin{array}{c} \pm 410 \ \pm 300 \end{array}$	$\begin{array}{c} -250 \\ -1370 \end{array}$	$W_E \ \pm 470 \ \pm 810$	${\pm 130 \over \pm 530}$
Bin 1 Bin 2 Bin 3	$\begin{array}{c} 450\\ 500\\ 500\end{array}$	$W_D \ \pm 640 \ \pm 1200 \ \pm 3500$	$egin{array}{c} \pm 410 \ \pm 300 \ \pm 1200 \end{array}$	$-250 \\ -1370 \\ 4300$	$W_E \ \pm 470 \ \pm 810 \ \pm 2100$	$egin{array}{c} \pm 130 \ \pm 530 \ \pm 600 \ \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4	450 500 500 3300	$W_D \ \pm 640 \ \pm 1200 \ \pm 3500 \ \pm 5800$	$\begin{array}{r} \pm 410 \\ \pm 300 \\ \pm 1200 \\ \pm 1600 \end{array}$	$-250 \\ -1370 \\ 4300 \\ -40$	$W_E \ \pm 470 \ \pm 810 \ \pm 2100 \ \pm 3600$	$\begin{array}{r} \pm 130 \\ \pm 530 \\ \pm 600 \\ \pm 700 \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5	450 500 500 3300 4000	$egin{array}{c} W_D \ \pm 640 \ \pm 1200 \ \pm 3500 \ \pm 5800 \ \pm 1800 \ \end{array}$	$\begin{array}{r} \pm 410 \\ \pm 300 \\ \pm 1200 \\ \pm 1600 \\ \pm 600 \end{array}$	$ \begin{array}{r} -250 \\ -1370 \\ 4300 \\ -40 \\ -500 \end{array} $	$egin{array}{c} W_E \ \pm 470 \ \pm 810 \ \pm 2100 \ \pm 3600 \ \pm 720 \ \end{array}$	$\begin{array}{r} \pm 130 \\ \pm 530 \\ \pm 600 \\ \pm 700 \\ \pm 180 \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6	450 500 500 3300 4000 7500	$egin{array}{c} W_D \ \pm 640 \ \pm 1200 \ \pm 3500 \ \pm 5800 \ \pm 1800 \ \pm 4200 \ \end{array}$	$\pm 410 \\ \pm 300 \\ \pm 1200 \\ \pm 1600 \\ \pm 600 \\ \pm 900$	$-250 \\ -1370 \\ 4300 \\ -40 \\ -500 \\ -4100$	$egin{array}{c} W_E \ \pm 470 \ \pm 810 \ \pm 2100 \ \pm 3600 \ \pm 720 \ \pm 2000 \ \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 530 \\ \pm 600 \\ \pm 700 \\ \pm 180 \\ \pm 400 \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7	450 500 3300 4000 7500 1100	$egin{array}{c} W_D \ \pm 640 \ \pm 1200 \ \pm 3500 \ \pm 5800 \ \pm 1800 \ \pm 4200 \ \pm 5600 \ \end{array}$	$\pm 410 \\ \pm 300 \\ \pm 1200 \\ \pm 1600 \\ \pm 600 \\ \pm 900 \\ \pm 2600$	$\begin{array}{c} -250 \\ -1370 \\ 4300 \\ -40 \\ -500 \\ -4100 \\ 300 \end{array}$	$egin{array}{c} W_E \ \pm 470 \ \pm 810 \ \pm 2100 \ \pm 3600 \ \pm 720 \ \pm 2000 \ \pm 2800 \ \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 530 \\ \pm 600 \\ \pm 700 \\ \pm 180 \\ \pm 400 \\ \pm 600 \end{array}$
Bin 1 Bin 2 Bin 3 Bin 5 Bin 6 Bin 7 Bin 8	450 500 500 3300 4000 7500 1100 1400	$egin{array}{c} W_D \ \pm 640 \ \pm 1200 \ \pm 3500 \ \pm 5800 \ \pm 1800 \ \pm 4200 \ \pm 4200 \ \pm 5600 \ \pm 3000 \ \end{array}$	$\pm 410 \\ \pm 300 \\ \pm 1200 \\ \pm 1600 \\ \pm 600 \\ \pm 900 \\ \pm 2600 \\ \pm 1200$	$\begin{array}{c} -250 \\ -1370 \\ 4300 \\ -40 \\ -500 \\ -4100 \\ 300 \\ 1300 \end{array}$	$egin{array}{c} W_E \ \pm 470 \ \pm 810 \ \pm 2100 \ \pm 3600 \ \pm 22000 \ \pm 22000 \ \pm 2800 \ \pm 1600 \ \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 530 \\ \pm 600 \\ \pm 700 \\ \pm 180 \\ \pm 400 \\ \pm 600 \\ \pm 400 \\ \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9	450 500 3300 4000 7500 1100 1400 2700	$egin{array}{c} W_D \ \pm 640 \ \pm 1200 \ \pm 3500 \ \pm 5800 \ \pm 1800 \ \pm 4200 \ \pm 3600 \ \pm 3000 \ \pm 3100 \ \end{array}$	± 410 ± 300 ± 1200 ± 1600 ± 900 ± 2600 ± 1200 ± 1200	$\begin{array}{r} -250 \\ -1370 \\ 4300 \\ -40 \\ -500 \\ -4100 \\ 300 \\ 1300 \\ 1500 \end{array}$	$egin{array}{c} W_E \ \pm 470 \ \pm 810 \ \pm 2100 \ \pm 3600 \ \pm 22000 \ \pm 2800 \ \pm 2800 \ \pm 1600 \ \pm 1300 \ \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 530 \\ \pm 600 \\ \pm 700 \\ \pm 180 \\ \pm 400 \\ \pm 600 \\ \pm 400 \\ \pm 600 \\ \pm 600 \\ \pm 600 \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9 Bin 10	$\begin{array}{c} 450 \\ 500 \\ 500 \\ 3300 \\ 4000 \\ 7500 \\ 1100 \\ 1400 \\ 2700 \\ 6700 \end{array}$	$egin{array}{c} W_D \ \pm 640 \ \pm 1200 \ \pm 3500 \ \pm 5800 \ \pm 5800 \ \pm 4200 \ \pm 4200 \ \pm 3000 \ \pm 3000 \ \pm 3100 \ \pm 55000 \ \end{array}$	± 410 ± 300 ± 1200 ± 1600 ± 900 ± 2600 ± 1200 ± 900 ± 1500	$\begin{array}{c} -250 \\ -1370 \\ 4300 \\ -40 \\ -500 \\ -4100 \\ 300 \\ 1300 \\ 1500 \\ 1200 \end{array}$	$egin{array}{c} W_E \ \pm 470 \ \pm 810 \ \pm 2100 \ \pm 2600 \ \pm 2800 \ \pm 1600 \ \pm 1300 \ \pm 2200 \ \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 530 \\ \pm 600 \\ \pm 700 \\ \pm 180 \\ \pm 400 \\ \pm 600 \\ \pm 400 \\ \pm 600 \\ \pm 400 \\ \pm 600 \\ \pm 700 \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9 Bin 10 Bin 11	450 500 3300 4000 7500 1100 1400 2700 6700 6100	$egin{array}{c} W_D \ \pm 640 \ \pm 1200 \ \pm 3500 \ \pm 5800 \ \pm 5800 \ \pm 4200 \ \pm 4200 \ \pm 3000 \ \pm 3100 \ \pm 3100 \ \pm 3600 \ \end{array}$	± 410 ± 300 ± 1200 ± 1600 ± 900 ± 2600 ± 1200 ± 1200 ± 1200 ± 1400	$\begin{array}{c} -250 \\ -1370 \\ 4300 \\ -40 \\ -500 \\ -4100 \\ 300 \\ 1300 \\ 1500 \\ 1200 \\ -4000 \\ \end{array}$	$egin{array}{c} W_E \ \pm 470 \ \pm 810 \ \pm 2100 \ \pm 2600 \ \pm 2000 \ \pm 2800 \ \pm 1600 \ \pm 1300 \ \pm 1300 \ \pm 1300 \ \pm 1900 \ \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 530 \\ \pm 600 \\ \pm 700 \\ \pm 180 \\ \pm 400 \\ \pm 600 \\ \pm 400 \\ \pm 600 \\ \pm 700 \\ \pm 1000 \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9 Bin 10 Bin 11 Bin 12	450 500 3300 4000 7500 1100 1400 2700 6700 6100 5000	$egin{array}{c} W_D \ \pm 640 \ \pm 1200 \ \pm 3500 \ \pm 3500 \ \pm 1800 \ \pm 4200 \ \pm 5600 \ \pm 3000 \ \pm 3100 \ \pm 3600 \ \pm 13000 \ \pm 13000 \ \end{array}$	± 410 ± 300 ± 1200 ± 1600 ± 900 ± 2600 ± 1200 ± 1500 ± 1400 ± 2000	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$egin{array}{c} W_E \ \pm 470 \ \pm 810 \ \pm 2100 \ \pm 2000 \ \pm 2800 \ \pm 1600 \ \pm 1300 \ \pm 2200 \ \pm 1900 \ \pm 5900 \ \hline \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 530 \\ \pm 600 \\ \pm 700 \\ \pm 180 \\ \pm 400 \\ \pm 600 \\ \pm 400 \\ \pm 600 \\ \pm 1000 \\ \pm 1800 \\ \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9 Bin 10 Bin 11 Bin 12 Bin 13	$\begin{array}{c} 450 \\ 500 \\ 500 \\ 3300 \\ 4000 \\ 7500 \\ 1100 \\ 1400 \\ 2700 \\ 6700 \\ 6100 \\ 5000 \\ 3000 \\ \end{array}$	$egin{array}{c} W_D \ \pm 640 \ \pm 1200 \ \pm 3500 \ \pm 5800 \ \pm 5800 \ \pm 4200 \ \pm 3000 \ \pm 3000 \ \pm 3000 \ \pm 3100 \ \pm 3600 \ \pm 13000 \ \pm 13000 \ \pm 1900 \ \end{array}$	$\begin{array}{c} \pm 410 \\ \pm 300 \\ \pm 1200 \\ \pm 1600 \\ \pm 900 \\ \pm 2600 \\ \pm 1200 \\ \pm 1200 \\ \pm 1200 \\ \pm 1400 \\ \pm 1400 \\ \pm 2000 \\ \pm 2000 \\ \pm 600 \end{array}$	$\begin{array}{c} -250 \\ -1370 \\ 4300 \\ -500 \\ -4100 \\ 300 \\ 1300 \\ 1500 \\ 1200 \\ -4000 \\ -7800 \\ 30 \\ \end{array}$	$egin{array}{c} W_E \ \pm 470 \ \pm 810 \ \pm 2100 \ \pm 2000 \ \pm 2800 \ \pm 1600 \ \pm 1300 \ \pm 2200 \ \pm 1900 \ \pm 5900 \ \pm 760 \ \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 530 \\ \pm 600 \\ \pm 700 \\ \pm 180 \\ \pm 400 \\ \pm 400 \\ \pm 400 \\ \pm 400 \\ \pm 1000 \\ \pm 1800 \\ \pm 1800 \\ \pm 280 \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9 Bin 10 Bin 11 Bin 12 Bin 13	450 500 3300 4000 7500 1100 1400 2700 6700 6100 5000 3000 1400	$egin{arred} & W_D \ & \pm 640 \ & \pm 1200 \ & \pm 3500 \ & \pm 5800 \ & \pm 1800 \ & \pm 4200 \ & \pm 5600 \ & \pm 3000 \ & \pm 3100 \ & \pm 3100 \ & \pm 3600 \ & \pm 3600 \ & \pm 13000 \ & \pm 1900 \ & \pm 1900 \ & \pm 2500 \ & \end{arred}$	± 410 ± 300 ± 1200 ± 1600 ± 900 ± 2600 ± 1200 ± 1200 ± 1200 ± 1400 ± 2000 ± 600 ± 1300	$\begin{array}{c} -250 \\ -1370 \\ 4300 \\ -40 \\ -500 \\ -4100 \\ 300 \\ 1300 \\ 1300 \\ 1200 \\ -4000 \\ -7800 \\ 30 \\ -3500 \\ \end{array}$	$egin{array}{c} W_E \ \pm 470 \ \pm 810 \ \pm 2100 \ \pm 2000 \ \pm 2800 \ \pm 1600 \ \pm 1300 \ \pm 2200 \ \pm 1900 \ \pm 2900 \ \pm 5900 \ \pm 760 \ \pm 900 \ \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 530 \\ \pm 600 \\ \pm 700 \\ \pm 180 \\ \pm 400 \\ \pm 240 \\ \pm 1000 \\ \pm 1800 \\ \pm 280 \\ \pm 1300 \\ \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9 Bin 10 Bin 11 Bin 12 Bin 13 Bin 14 Bin 15	450 500 3300 4000 7500 1100 1400 2700 6700 6100 5000 3000 1400	$egin{array}{c} W_D \ \pm 640 \ \pm 1200 \ \pm 3500 \ \pm 5800 \ \pm 5800 \ \pm 4200 \ \pm 5600 \ \pm 3000 \ \pm 3100 \ \pm 3100 \ \pm 3100 \ \pm 3600 \ \pm 13000 \ \pm 13000 \ \pm 1900 \ \pm 1900 \ \pm 2500 \ \pm 3800 \ \end{array}$	$\begin{array}{c} \pm 410 \\ \pm 300 \\ \pm 1200 \\ \pm 1600 \\ \pm 600 \\ \pm 900 \\ \pm 2600 \\ \pm 1200 \\ \pm 1200 \\ \pm 1200 \\ \pm 1300 \\ \pm 1300 \\ \pm 1300 \\ \pm 1400 \end{array}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$egin{array}{c} W_E \ \pm 470 \ \pm 810 \ \pm 2100 \ \pm 2000 \ \pm 2800 \ \pm 1600 \ \pm 1300 \ \pm 2200 \ \pm 1900 \ \pm 1900 \ \pm 5900 \ \pm 760 \ \pm 900 \ \pm 1100 \ \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 530 \\ \pm 600 \\ \pm 700 \\ \pm 180 \\ \pm 400 \\ \pm 400 \\ \pm 400 \\ \pm 400 \\ \pm 1000 \\ \pm 280 \\ \pm 1300 \\ \pm 1300 \\ \pm 500 \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9 Bin 10 Bin 11 Bin 12 Bin 13 Bin 14 Bin 15 Bin 16	450 500 3300 4000 7500 1100 1400 2700 6700 6700 6100 5000 3000 1400 5800 -9400	$egin{array}{c} W_D \ \pm 640 \ \pm 1200 \ \pm 3500 \ \pm 3500 \ \pm 5800 \ \pm 1800 \ \pm 4200 \ \pm 5600 \ \pm 3000 \ \pm 3000 \ \pm 3600 \ \pm 13000 \ \pm 13000 \ \pm 1900 \ \pm 2500 \ \pm 3800 \ \pm 3800 \ \pm 8000 \ \end{bmatrix}$	± 410 ± 300 ± 1200 ± 1600 ± 900 ± 2600 ± 1200 ± 1200 ± 1200 ± 1500 ± 1400 ± 2000 ± 1300 ± 1400 ± 1400	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$egin{array}{c} W_E \ \pm 470 \ \pm 810 \ \pm 2100 \ \pm 2100 \ \pm 2800 \ \pm 1600 \ \pm 1300 \ \pm 2200 \ \pm 1900 \ \pm 1900 \ \pm 1900 \ \pm 1900 \ \pm 1100 \ \pm 2500 \ \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 530 \\ \pm 600 \\ \pm 700 \\ \pm 180 \\ \pm 400 \\ \pm 400 \\ \pm 600 \\ \pm 400 \\ \pm 1000 \\ \pm 280 \\ \pm 1300 \\ \pm 280 \\ \pm 1300 \\ \pm 500 \\ \pm 700 \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9 Bin 10 Bin 11 Bin 12 Bin 13 Bin 14 Bin 15 Bin 16 Bin 17	450 500 3300 4000 7500 1100 1400 2700 6700 6100 5000 3000 1400 5800 -9400 1600	$egin{array}{c} W_D \ \pm 640 \ \pm 1200 \ \pm 3500 \ \pm 3500 \ \pm 5800 \ \pm 5800 \ \pm 4200 \ \pm 5600 \ \pm 3000 \ \pm 3000 \ \pm 3000 \ \pm 3000 \ \pm 13000 \ \pm 130000 \ \pm 1300000 \ \pm 1300000 \ \pm 130000 \ \pm 130000 \ \pm 13000000 \ \pm 1300000 \ \pm 13000000 \ \pm 130$	± 410 ± 300 ± 1200 ± 1600 ± 900 ± 2600 ± 1200 ± 1200 ± 1200 ± 1200 ± 1300 ± 1300 ± 1400 ± 2800 ± 2800	$\begin{array}{c} -250 \\ -1370 \\ 4300 \\ -500 \\ -40 \\ 300 \\ 1300 \\ 1300 \\ 1300 \\ 1200 \\ -4000 \\ -7800 \\ 30 \\ -3500 \\ -200 \\ -4200 \\ -30 \\ \end{array}$	$egin{array}{c} W_E \ \pm 470 \ \pm 810 \ \pm 2100 \ \pm 2100 \ \pm 2000 \ \pm 2800 \ \pm 1600 \ \pm 1600 \ \pm 1300 \ \pm 2200 \ \pm 1900 \ \pm 5900 \ \pm 760 \ \pm 760 \ \pm 2500 \ \pm 1100 \ \pm 2500 \ \pm 430 \ \hline \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	$\begin{array}{c} \pm 130 \\ \pm 530 \\ \pm 600 \\ \pm 700 \\ \pm 180 \\ \pm 400 \\ \pm 400 \\ \pm 400 \\ \pm 400 \\ \pm 280 \\ \pm 1300 \\ \pm 1800 \\ \pm 1800 \\ \pm 280 \\ \pm 1300 \\ \pm 500 \\ \pm 700 \\ \pm 80 \\ \pm $
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9 Bin 10 Bin 11 Bin 12 Bin 13 Bin 14 Bin 15 Bin 16 Bin 17 Bin 18	450 500 3300 4000 7500 1100 1400 2700 6700 6100 5000 3000 1400 5800 -9400 1600 10100	$egin{arred} & W_D \ \pm 640 \ \pm 1200 \ \pm 3500 \ \pm 3500 \ \pm 5800 \ \pm 4200 \ \pm 5600 \ \pm 3000 \ \pm 3000 \ \pm 3100 \ \pm 3000 \ \pm 3600 \ \pm 13000 \ \pm 1900 \ \pm 2500 \ \pm 3800 \ \pm 1500 \ \pm 1500 \ \pm 1500 \ \pm 6100 \ \hline \pm 6100 \ \hline \end{bmatrix}$	± 410 ± 300 ± 1200 ± 1600 ± 2600 ± 2600 ± 1200 ± 1200 ± 1200 ± 1300 ± 1400 ± 1400 ± 1400 ± 2800 ± 200 ± 200	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$egin{array}{c} W_E \ \pm 470 \ \pm 810 \ \pm 2100 \ \pm 2000 \ \pm 2800 \ \pm 1600 \ \pm 1300 \ \pm 2200 \ \pm 1900 \ \pm 2500 \ \pm 1900 \ \pm 5900 \ \pm 760 \ \pm 2500 \ \pm 1100 \ \pm 2500 \ \pm 430 \ \pm 1800 \ \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 530 \\ \pm 600 \\ \pm 700 \\ \pm 180 \\ \pm 400 \\ \pm 280 \\ \pm 1300 \\ \pm 280 \\ \pm 1300 \\ \pm 500 \\ \pm 500 \\ \pm 300 \\ \pm 300 \\ \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9 Bin 10 Bin 11 Bin 12 Bin 13 Bin 14 Bin 15 Bin 16 Bin 17 Bin 18	450 500 3300 4000 7500 1100 1400 2700 6700 6700 6700 6100 5000 3000 1400 5800 -9400 1600 10100	$egin{arred} & W_D \ & \pm 640 \ & \pm 1200 \ & \pm 3500 \ & \pm 5800 \ & \pm 5800 \ & \pm 1800 \ & \pm 4200 \ & \pm 5600 \ & \pm 3000 \ & \pm 3100 \ & \pm 3100 \ & \pm 3600 \ & \pm 3600 \ & \pm 13000 \ & \pm 1900 \ & \pm 1900 \ & \pm 1900 \ & \pm 3800 \ & \pm 1500 \ & \pm 4800 \ & \pm 4800 \ & \end{bmatrix}$	± 410 ± 300 ± 1200 ± 1600 ± 2600 ± 2600 ± 1200 ± 1200 ± 1200 ± 1300 ± 1400 ± 1400 ± 1300 ± 1400 ± 2800 ± 2000 ± 13100	$\begin{array}{c} -250 \\ -1370 \\ 4300 \\ -40 \\ -500 \\ -4100 \\ 300 \\ 1300 \\ 1300 \\ 1300 \\ 1200 \\ -4000 \\ -7800 \\ -300 \\ -200 \\ -200 \\ -4200 \\ -30 \\ -2100 \\ -1300 \\ \end{array}$	$egin{array}{c} W_E \ \pm 470 \ \pm 810 \ \pm 2100 \ \pm 2000 \ \pm 2800 \ \pm 1600 \ \pm 1300 \ \pm 1300 \ \pm 1300 \ \pm 1900 \ \pm 1900 \ \pm 5900 \ \pm 760 \ \pm 1100 \ \pm 2500 \ \pm 1100 \ \pm 1800 \ \pm 1100 \ \pm 11000 \ \pm 110000 \ \pm 110000 \ \pm 11000 \ \pm 11000 \ \pm 11000 \ \pm 110000$	$\begin{array}{c} \pm 130 \\ \pm 530 \\ \pm 600 \\ \pm 700 \\ \pm 180 \\ \pm 400 \\ \pm 280 \\ \pm 1300 \\ \pm 280 \\ \pm 1300 \\ \pm 500 \\ \pm 300 \\ \pm 300 \\ \pm 500 \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9 Bin 10 Bin 11 Bin 12 Bin 13 Bin 14 Bin 15 Bin 16 Bin 17 Bin 18 Bin 19 Bin 20	450 500 3300 4000 7500 1100 1400 2700 6700 6700 6100 5000 3000 1400 5800 -9400 1600 10100 4900 1500	$egin{arred} & W_D \ & \pm 640 \ & \pm 1200 \ & \pm 3500 \ & \pm 3500 \ & \pm 5800 \ & \pm 1800 \ & \pm 4200 \ & \pm 5600 \ & \pm 3000 \ & \pm 3100 \ & \pm 3100 \ & \pm 3100 \ & \pm 3100 \ & \pm 3600 \ & \pm 3800 \ & \pm 13000 \ & \pm 13000 \ & \pm 1500 \ & \pm 48000 \ & \pm 1500 \ & \pm 6100 \ & \pm 4800 \ & \pm 1700 \ & \pm 11700 \$	± 410 ± 300 ± 1200 ± 1600 ± 900 ± 2600 ± 1200 ± 1200 ± 1200 ± 1500 ± 1400 ± 2000 ± 1400 ± 2800 ± 1400 ± 2800 ± 1400 ± 1400 ± 1500 ± 1500	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$egin{array}{c} W_E \ \pm 470 \ \pm 810 \ \pm 2100 \ \pm 2100 \ \pm 2000 \ \pm 2800 \ \pm 1600 \ \pm 1300 \ \pm 2200 \ \pm 1900 \ \pm 1900 \ \pm 1900 \ \pm 1900 \ \pm 1100 \ \pm 2500 \ \pm 430 \ \pm 1800 \ \pm 1100 \ \pm 320 \ \hline \end{bmatrix}$	$\begin{array}{c} \pm 130 \\ \pm 530 \\ \pm 600 \\ \pm 700 \\ \pm 180 \\ \pm 400 \\ \pm 400 \\ \pm 400 \\ \pm 400 \\ \pm 280 \\ \pm 1000 \\ \pm 1000 \\ \pm 1300 \\ \pm 280 \\ \pm 1300 \\ \pm 500 \\ \pm 300 \\ \pm 300 \\ \pm 500 \\ \pm 90 \\ \end{array}$

Table 6: The hadronic structure functions W_A , W_C , W_D and W_E for each (Q^2, s_1, s_2) bin. For each structure function, the central value, statistical and systematic errors are given. The contributions shown in table 8 are included in the systematic errors.

		W_F			W_H	
Bin 1	-1600	± 630	± 340	60	± 700	± 200
Bin 2	130	± 1300	± 400	-100	± 1300	± 600
Bin 3	1300	± 3200	± 1000	-7000	± 3600	± 1000
Bin 4	-600	± 7000	± 1200	8400	± 6200	± 3700
Bin 5	30	± 1900	± 700	-400	± 1600	± 500
Bin 6	-5600	± 4100	± 1100	-5300	± 4300	± 1800
Bin 7	4300	± 5600	± 1100	1000	± 6000	± 1200
Bin 8	-4900	± 3200	± 1200	-5900	± 3000	± 1700
Bin 9	-2000	± 2900	± 1600	100	± 3100	± 700
Bin 10	3500	± 5700	± 1000	6700	± 5200	± 1100
Bin 11	-3100	± 4600	± 900	-2800	± 4800	± 700
Bin 12	-700	± 14800	± 4900	-14000	± 15000	± 4000
Bin 13	3200	± 2100	± 400	1900	± 2100	± 400
Bin 14	800	± 3100	± 1400	-4300	± 2400	± 1800
Bin 15	1700	± 3900	± 1900	-1100	± 4000	± 900
Bin 16	7800	± 8400	± 1700	3500	± 8400	± 2300
Bin 17	-300	± 1500	± 200	2000	± 1600	± 300
Bin 18	-5000	± 5700	± 1700	3800	± 7200	± 1600
Bin 19	4000	± 5100	± 1100	-1900	± 5600	± 900
Bin 20	100	± 1800	± 400	-1500	± 1800	± 1000
Bin 21	-5400	± 3800	± 1800	10200	± 4700	± 2500
		X_1			X_2	
Bin 1	-50	X_1 ± 150	±110	-10	X_2 ± 150	± 130
Bin 1 Bin 2	$-50\\120$	$egin{array}{c} X_1 \ \pm 150 \ \pm 280 \end{array}$	$\pm 110 \\ \pm 130$	-10 -80	$egin{array}{c} X_2 \ \pm 150 \ \pm 310 \end{array}$	$egin{array}{c} \pm 130 \ \pm 60 \end{array}$
Bin 1 Bin 2 Bin 3	$-50 \\ 120 \\ 1040$	$egin{array}{c} X_1 \ \pm 150 \ \pm 280 \ \pm 810 \ \end{array}$	$\begin{array}{r} \pm 110 \\ \pm 130 \\ \pm 540 \end{array}$	-10 -80 450	$ \begin{array}{r} X_2 \\ $	
Bin 1 Bin 2 Bin 3 Bin 4	$-50 \\ 120 \\ 1040 \\ -1900$	$egin{array}{c} X_1 \ \pm 150 \ \pm 280 \ \pm 810 \ \pm 1200 \ \end{array}$	$\begin{array}{r} \pm 110 \\ \pm 130 \\ \pm 540 \\ \pm 1000 \end{array}$	$ \begin{array}{c c} -10 \\ -80 \\ 450 \\ 1900 \end{array} $	$egin{array}{c} X_2 \ \pm 150 \ \pm 310 \ \pm 800 \ \pm 1400 \ \end{array}$	$\begin{array}{r} \pm 130 \\ \pm 60 \\ \pm 320 \\ \pm 900 \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5	$ \begin{array}{c c} -50 \\ 120 \\ 1040 \\ -1900 \\ 20 \\ \end{array} $	$egin{array}{c} X_1 \ \pm 150 \ \pm 280 \ \pm 810 \ \pm 1200 \ \pm 310 \ \end{array}$	$egin{array}{c} \pm 110 \ \pm 130 \ \pm 540 \ \pm 1000 \ \pm 70 \ \end{array}$	$ \begin{array}{c c} -10 \\ -80 \\ 450 \\ 1900 \\ 40 \\ \end{array} $	$\begin{array}{c} X_2 \\ \pm 150 \\ \pm 310 \\ \pm 800 \\ \pm 1400 \\ \pm 350 \end{array}$	$ \begin{array}{r} \pm 130 \\ \pm 60 \\ \pm 320 \\ \pm 900 \\ \pm 80 \end{array} $
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6	$-50 \\ 120 \\ 1040 \\ -1900 \\ 20 \\ 370$	$egin{array}{c} X_1 \ \pm 150 \ \pm 280 \ \pm 810 \ \pm 1200 \ \pm 310 \ \pm 870 \ \end{array}$	$\pm 110 \\ \pm 130 \\ \pm 540 \\ \pm 1000 \\ \pm 70 \\ \pm 460 \\ \end{bmatrix}$	$ \begin{array}{c c} -10 \\ -80 \\ 450 \\ 1900 \\ 40 \\ -160 \\ \end{array} $	$egin{array}{c} X_2 \ \pm 150 \ \pm 310 \ \pm 800 \ \pm 1400 \ \pm 350 \ \pm 850 \ \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 60 \\ \pm 320 \\ \pm 900 \\ \pm 80 \\ \pm 220 \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7		$egin{array}{c} X_1 \ \pm 150 \ \pm 280 \ \pm 810 \ \pm 1200 \ \pm 310 \ \pm 310 \ \pm 870 \ \pm 1400 \ \end{array}$	$\pm 110 \\ \pm 130 \\ \pm 540 \\ \pm 1000 \\ \pm 70 \\ \pm 460 \\ \pm 300$	$ \begin{array}{c c} -10 \\ -80 \\ 450 \\ 1900 \\ 40 \\ -160 \\ 100 \\ \end{array} $	$egin{array}{c} X_2 \ \pm 150 \ \pm 310 \ \pm 800 \ \pm 1400 \ \pm 350 \ \pm 850 \ \pm 1300 \ \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 60 \\ \pm 320 \\ \pm 900 \\ \pm 80 \\ \pm 220 \\ \pm 300 \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8	$\begin{array}{c} -50\\ 120\\ 1040\\ -1900\\ \hline 20\\ 370\\ -600\\ -560\\ \end{array}$	$egin{array}{c} X_1 \ \pm 150 \ \pm 280 \ \pm 810 \ \pm 1200 \ \pm 310 \ \pm 310 \ \pm 870 \ \pm 1400 \ \pm 630 \ \hline \end{array}$	$\begin{array}{c} \pm 110 \\ \pm 130 \\ \pm 540 \\ \pm 1000 \\ \pm 70 \\ \pm 460 \\ \pm 300 \\ \pm 300 \end{array}$	$\begin{array}{c c} -10 \\ -80 \\ 450 \\ 1900 \\ 40 \\ -160 \\ 100 \\ 380 \\ \end{array}$	$egin{array}{c} X_2 \ \pm 150 \ \pm 310 \ \pm 800 \ \pm 1400 \ \pm 350 \ \pm 850 \ \pm 1300 \ \pm 680 \ \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 60 \\ \pm 320 \\ \pm 900 \\ \pm 220 \\ \pm 300 \\ \pm 140 \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9	$\begin{array}{c} -50\\ 120\\ 1040\\ -1900\\ \hline 20\\ 370\\ -600\\ -560\\ \hline -690\\ \end{array}$	$egin{array}{c} X_1 \ \pm 150 \ \pm 280 \ \pm 810 \ \pm 1200 \ \pm 310 \ \pm 310 \ \pm 870 \ \pm 1400 \ \pm 630 \ \pm 610 \ \hline \end{array}$	$\begin{array}{c} \pm 110 \\ \pm 130 \\ \pm 540 \\ \pm 1000 \\ \pm 70 \\ \pm 460 \\ \pm 300 \\ \pm 300 \\ \pm 240 \end{array}$	$\begin{array}{ c c c c }\hline & -10 \\ & -80 \\ 450 \\ \hline 1900 \\ \hline 40 \\ -160 \\ \hline 100 \\ 380 \\ \hline 810 \\ \hline \end{array}$	$\begin{array}{c} X_2 \\ \pm 150 \\ \pm 310 \\ \pm 800 \\ \pm 1400 \\ \pm 350 \\ \pm 850 \\ \pm 1300 \\ \pm 680 \\ \pm 620 \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 60 \\ \pm 320 \\ \pm 900 \\ \pm 220 \\ \pm 300 \\ \pm 140 \\ \pm 220 \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9 Bin 10	$\begin{array}{c} -50\\ 120\\ 1040\\ -1900\\ \hline 20\\ 370\\ -600\\ -560\\ \hline -690\\ -800\\ \end{array}$	$egin{array}{c} X_1 \ \pm 150 \ \pm 280 \ \pm 810 \ \pm 1200 \ \pm 310 \ \pm 310 \ \pm 630 \ \pm 630 \ \pm 610 \ \pm 1100 \ \end{array}$	± 110 ± 130 ± 540 ± 1000 ± 70 ± 460 ± 300 ± 300 ± 240 ± 200	$\begin{array}{ c c c c c }\hline & -10 \\ & -80 \\ \hline & 450 \\ \hline & 1900 \\ \hline & 40 \\ & -160 \\ \hline & 100 \\ \hline & 380 \\ \hline & 810 \\ & -3500 \\ \hline \end{array}$	$\begin{array}{c} X_2 \\ \pm 150 \\ \pm 310 \\ \pm 800 \\ \pm 1400 \\ \pm 350 \\ \pm 350 \\ \pm 850 \\ \pm 1300 \\ \pm 680 \\ \pm 620 \\ \pm 1100 \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 60 \\ \pm 320 \\ \pm 900 \\ \pm 220 \\ \pm 300 \\ \pm 140 \\ \pm 220 \\ \pm 600 \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9 Bin 10 Bin 11	$\begin{array}{c} -50 \\ 120 \\ 1040 \\ -1900 \\ \hline 20 \\ 370 \\ -600 \\ -560 \\ \hline -690 \\ -800 \\ -1330 \\ \end{array}$	$\begin{array}{c} X_1 \\ \pm 150 \\ \pm 280 \\ \pm 810 \\ \pm 1200 \\ \pm 310 \\ \pm 310 \\ \pm 630 \\ \pm 630 \\ \pm 610 \\ \pm 1100 \\ \pm 770 \end{array}$	$\begin{array}{c} \pm 110 \\ \pm 130 \\ \pm 540 \\ \pm 1000 \\ \pm 70 \\ \pm 460 \\ \pm 300 \\ \pm 300 \\ \pm 240 \\ \pm 200 \\ \pm 260 \end{array}$	$\begin{array}{c c} -10 \\ -80 \\ 450 \\ 1900 \\ 40 \\ -160 \\ 100 \\ 380 \\ 810 \\ -3500 \\ -210 \end{array}$	$\begin{array}{c} X_2 \\ \pm 150 \\ \pm 310 \\ \pm 800 \\ \pm 1400 \\ \pm 350 \\ \pm 850 \\ \pm 1300 \\ \pm 680 \\ \pm 620 \\ \pm 1100 \\ \pm 890 \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 60 \\ \pm 320 \\ \pm 900 \\ \pm 220 \\ \pm 300 \\ \pm 140 \\ \pm 220 \\ \pm 600 \\ \pm 220 \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9 Bin 10 Bin 11 Bin 12	$\begin{array}{c} -50 \\ 120 \\ 1040 \\ -1900 \\ \hline 20 \\ 370 \\ -600 \\ -560 \\ \hline -560 \\ -800 \\ -1330 \\ -3100 \\ \end{array}$	$egin{array}{c} X_1 \ \pm 150 \ \pm 280 \ \pm 810 \ \pm 1200 \ \pm 310 \ \pm 310 \ \pm 630 \ \pm 1400 \ \pm 630 \ \pm 610 \ \pm 1100 \ \pm 2700 \ \pm 2700 \ \hline \end{array}$	$\begin{array}{c} \pm 110 \\ \pm 130 \\ \pm 540 \\ \pm 1000 \\ \pm 70 \\ \pm 460 \\ \pm 300 \\ \pm 300 \\ \pm 240 \\ \pm 200 \\ \pm 260 \\ \pm 800 \end{array}$	$\begin{array}{c c} -10 \\ -80 \\ 450 \\ 1900 \\ 40 \\ -160 \\ 100 \\ 380 \\ 810 \\ -3500 \\ -210 \\ 1900 \\ \end{array}$	$\begin{array}{c} X_2 \\ \pm 150 \\ \pm 310 \\ \pm 800 \\ \pm 1400 \\ \pm 350 \\ \pm 850 \\ \pm 1300 \\ \pm 680 \\ \pm 620 \\ \pm 1100 \\ \pm 890 \\ \pm 3000 \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 60 \\ \pm 320 \\ \pm 900 \\ \pm 200 \\ \pm 300 \\ \pm 140 \\ \pm 220 \\ \pm 600 \\ \pm 220 \\ \pm 600 \\ \pm 220 \\ \pm 700 \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9 Bin 10 Bin 11 Bin 12 Bin 13	$\begin{array}{c} -50\\ 120\\ 1040\\ -1900\\ \hline 20\\ 370\\ -600\\ -560\\ \hline -690\\ -800\\ -1330\\ \hline -3100\\ 130\\ \end{array}$	$egin{array}{c} X_1 \ \pm 150 \ \pm 280 \ \pm 810 \ \pm 1200 \ \pm 310 \ \pm 310 \ \pm 630 \ \pm 630 \ \pm 610 \ \pm 1100 \ \pm 2700 \ \pm 2700 \ \pm 360 \ \hline \end{array}$	$\begin{array}{c} \pm 110 \\ \pm 130 \\ \pm 540 \\ \pm 1000 \\ \pm 70 \\ \pm 460 \\ \pm 300 \\ \pm 300 \\ \pm 240 \\ \pm 200 \\ \pm 260 \\ \pm 800 \\ \pm 320 \end{array}$	$\begin{array}{c c} -10 \\ -80 \\ 450 \\ 1900 \\ \hline 40 \\ -160 \\ 100 \\ 380 \\ \hline 810 \\ -3500 \\ -210 \\ 1900 \\ -340 \\ \end{array}$	$\begin{array}{c} X_2 \\ \pm 150 \\ \pm 310 \\ \pm 800 \\ \pm 1400 \\ \pm 350 \\ \pm 850 \\ \pm 1300 \\ \pm 680 \\ \pm 620 \\ \pm 1100 \\ \pm 890 \\ \pm 3000 \\ \pm 380 \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 60 \\ \pm 320 \\ \pm 900 \\ \pm 220 \\ \pm 300 \\ \pm 140 \\ \pm 220 \\ \pm 600 \\ \pm 220 \\ \pm 600 \\ \pm 220 \\ \pm 700 \\ \pm 700 \\ \pm 70 \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9 Bin 10 Bin 11 Bin 12 Bin 13 Bin 14	$\begin{array}{c} -50\\ 120\\ 1040\\ -1900\\ \hline \\ 20\\ 370\\ -600\\ -560\\ \hline \\ -690\\ -800\\ -1330\\ \hline \\ -3100\\ 130\\ \hline \\ 130\\ \hline \\ -10\\ \end{array}$	$egin{array}{c} X_1 \ \pm 150 \ \pm 280 \ \pm 810 \ \pm 1200 \ \pm 310 \ \pm 310 \ \pm 630 \ \pm 1400 \ \pm 630 \ \pm 1400 \ \pm 630 \ \pm 1100 \ \pm 2700 \ \pm 2700 \ \pm 360 \ \pm 450 \ \hline \end{array}$	± 110 ± 130 ± 540 ± 1000 ± 70 ± 460 ± 300 ± 240 ± 200 ± 260 ± 800 ± 320	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{c} X_2 \\ \pm 150 \\ \pm 310 \\ \pm 800 \\ \pm 1400 \\ \pm 350 \\ \pm 850 \\ \pm 1300 \\ \pm 680 \\ \pm 620 \\ \pm 1100 \\ \pm 890 \\ \pm 3000 \\ \pm 380 \\ \pm 530 \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 60 \\ \pm 320 \\ \pm 900 \\ \pm 80 \\ \pm 220 \\ \pm 300 \\ \pm 140 \\ \pm 220 \\ \pm 600 \\ \pm 220 \\ \pm 600 \\ \pm 220 \\ \pm 700 \\ \pm 70 \\ \pm 70 \\ \pm 310 \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9 Bin 10 Bin 11 Bin 12 Bin 13 Bin 14 Bin 15	$\begin{array}{c} -50\\ 120\\ 1040\\ -1900\\ \hline 20\\ 370\\ -600\\ -560\\ \hline -690\\ -800\\ -1330\\ \hline -13100\\ 130\\ \hline -10\\ 170\\ \end{array}$	$egin{array}{c} X_1 \ \pm 150 \ \pm 280 \ \pm 810 \ \pm 1200 \ \pm 310 \ \pm 310 \ \pm 310 \ \pm 1400 \ \pm 630 \ \pm 1400 \ \pm 630 \ \pm 1100 \ \pm 2700 \ \pm 2700 \ \pm 260 \ \pm 450 \ \pm 450 \ \pm 650 \ \hline \end{array}$	± 110 ± 130 ± 540 ± 1000 ± 70 ± 460 ± 300 ± 240 ± 200 ± 260 ± 800 ± 320 ± 250 ± 200	$\begin{array}{c c} -10 \\ -80 \\ 450 \\ 1900 \\ 40 \\ -160 \\ 100 \\ 380 \\ 810 \\ -3500 \\ -210 \\ 1900 \\ -340 \\ -100 \\ -100 \\ -100 \end{array}$	$\begin{array}{c} X_2 \\ \pm 150 \\ \pm 310 \\ \pm 800 \\ \pm 1400 \\ \pm 350 \\ \pm 850 \\ \pm 1300 \\ \pm 680 \\ \pm 620 \\ \pm 1100 \\ \pm 890 \\ \pm 3000 \\ \pm 380 \\ \pm 530 \\ \pm 650 \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 60 \\ \pm 320 \\ \pm 900 \\ \pm 220 \\ \pm 300 \\ \pm 140 \\ \pm 220 \\ \pm 600 \\ \pm 220 \\ \pm 700 \\ \pm 700 \\ \pm 710 \\ \pm 310 \\ \pm 250 \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9 Bin 10 Bin 11 Bin 12 Bin 13 Bin 14 Bin 15 Bin 16	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$egin{array}{c} X_1 \ \pm 150 \ \pm 280 \ \pm 810 \ \pm 1200 \ \pm 310 \ \pm 310 \ \pm 310 \ \pm 470 \ \pm 1400 \ \pm 630 \ \pm 1400 \ \pm 2700 \ \pm 2700 \ \pm 360 \ \pm 450 \ \pm 650 \ \pm 1400 \ \end{array}$	$\begin{array}{c} \pm 110 \\ \pm 130 \\ \pm 540 \\ \pm 1000 \\ \pm 70 \\ \pm 460 \\ \pm 300 \\ \pm 200 \\ \pm 240 \\ \pm 200 \\ \pm 260 \\ \pm 260 \\ \pm 250 \\ \pm 250 \\ \pm 200 \\ \pm 200 \\ \pm 300 \end{array}$	$\begin{array}{c c} -10 \\ -80 \\ 450 \\ 1900 \\ \hline 40 \\ -160 \\ 100 \\ 380 \\ \hline 810 \\ -3500 \\ -210 \\ 1900 \\ -340 \\ \hline -100 \\ -100 \\ -1900 \\ \hline \end{array}$	$\begin{array}{c} X_2 \\ \pm 150 \\ \pm 310 \\ \pm 800 \\ \pm 1400 \\ \pm 350 \\ \pm 850 \\ \pm 1300 \\ \pm 680 \\ \pm 620 \\ \pm 1100 \\ \pm 890 \\ \pm 3000 \\ \pm 380 \\ \pm 530 \\ \pm 650 \\ \pm 1400 \\ \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 60 \\ \pm 320 \\ \pm 900 \\ \pm 220 \\ \pm 300 \\ \pm 140 \\ \pm 220 \\ \pm 600 \\ \pm 220 \\ \pm 600 \\ \pm 220 \\ \pm 700 \\ \pm 700 \\ \pm 700 \\ \pm 310 \\ \pm 250 \\ \pm 600 \\ \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9 Bin 10 Bin 11 Bin 12 Bin 13 Bin 14 Bin 15 Bin 16 Bin 17	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$egin{array}{c} X_1 \ \pm 150 \ \pm 280 \ \pm 810 \ \pm 1200 \ \pm 310 \ \pm 310 \ \pm 630 \ \pm 1400 \ \pm 630 \ \pm 610 \ \pm 1100 \ \pm 2700 \ \pm 360 \ \pm 450 \ \pm 450 \ \pm 650 \ \pm 1400 \ \pm 2200 \ \end{array}$	$\begin{array}{c} \pm 110 \\ \pm 130 \\ \pm 540 \\ \pm 1000 \\ \pm 70 \\ \pm 460 \\ \pm 300 \\ \pm 300 \\ \pm 240 \\ \pm 200 \\ \pm 260 \\ \pm 260 \\ \pm 320 \\ \pm 250 \\ \pm 220 \\ \pm 200 \\ \pm 200 \\ \pm 300 \\ \pm 100 \end{array}$	$\begin{array}{c c} -10 \\ -80 \\ 450 \\ 1900 \\ \hline \\ 40 \\ -160 \\ 100 \\ 380 \\ \hline \\ 810 \\ -3500 \\ -210 \\ 1900 \\ -340 \\ \hline \\ -100 \\ -100 \\ -100 \\ \hline \\ 350 \\ \end{array}$	$\begin{array}{c} X_2 \\ \pm 150 \\ \pm 310 \\ \pm 800 \\ \pm 1400 \\ \pm 350 \\ \pm 850 \\ \pm 1300 \\ \pm 680 \\ \pm 620 \\ \pm 1100 \\ \pm 890 \\ \pm 3000 \\ \pm 380 \\ \pm 530 \\ \pm 530 \\ \pm 650 \\ \pm 1400 \\ \pm 230 \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 60 \\ \pm 320 \\ \pm 900 \\ \pm 220 \\ \pm 300 \\ \pm 140 \\ \pm 220 \\ \pm 600 \\ \pm 220 \\ \pm 600 \\ \pm 220 \\ \pm 700 \\ \pm 700 \\ \pm 700 \\ \pm 250 \\ \pm 600 \\ \pm 50 \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9 Bin 10 Bin 11 Bin 12 Bin 13 Bin 14 Bin 15 Bin 16 Bin 17 Bin 18	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$egin{array}{c} X_1 \ \pm 150 \ \pm 280 \ \pm 810 \ \pm 1200 \ \pm 1200 \ \pm 310 \ \pm 630 \ \pm 1400 \ \pm 630 \ \pm 610 \ \pm 1100 \ \pm 2700 \ \pm 2700 \ \pm 360 \ \pm 450 \ \pm 450 \ \pm 450 \ \pm 1400 \ \pm 200 \ \pm 1100 \ \end{array}$	± 110 ± 130 ± 540 ± 1000 ± 70 ± 460 ± 300 ± 240 ± 200 ± 260 ± 200 ± 250 ± 200 ± 200 ± 200 ± 100	$\begin{array}{c c} -10 \\ -80 \\ 450 \\ 1900 \\ \hline \\ 40 \\ -160 \\ 100 \\ 380 \\ \hline \\ 810 \\ -3500 \\ -210 \\ 1900 \\ -340 \\ \hline \\ -100 \\ -100 \\ -1900 \\ 350 \\ -400 \\ \hline \end{array}$	$\begin{array}{c} X_2 \\ \pm 150 \\ \pm 310 \\ \pm 800 \\ \pm 1400 \\ \pm 350 \\ \pm 850 \\ \pm 1300 \\ \pm 680 \\ \pm 620 \\ \pm 1100 \\ \pm 680 \\ \pm 630 \\ \pm 530 \\ \pm 3000 \\ \pm 380 \\ \pm 530 \\ \pm 530 \\ \pm 650 \\ \pm 1400 \\ \pm 230 \\ \pm 1000 \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 60 \\ \pm 320 \\ \pm 900 \\ \pm 300 \\ \pm 220 \\ \pm 300 \\ \pm 140 \\ \pm 220 \\ \pm 600 \\ \pm 220 \\ \pm 700 \\ \pm 700 \\ \pm 700 \\ \pm 700 \\ \pm 50 \\ \pm 600 \\ \pm 50 \\ \pm 200 \\ \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9 Bin 10 Bin 11 Bin 12 Bin 13 Bin 14 Bin 15 Bin 16 Bin 17 Bin 18 Bin 19	$\begin{array}{c} -50 \\ 120 \\ 1040 \\ -1900 \\ \hline \\ 20 \\ 370 \\ -600 \\ -560 \\ \hline \\ -560 \\ -3100 \\ \hline \\ 130 \\ -110 \\ 130 \\ \hline \\ 130 \\ -10 \\ 170 \\ 2000 \\ \hline \\ 300 \\ -1900 \\ \hline \\ -260 \\ \hline \end{array}$	$egin{array}{c} X_1 \ \pm 150 \ \pm 280 \ \pm 810 \ \pm 1200 \ \pm 310 \ \pm 310 \ \pm 630 \ \pm 1400 \ \pm 630 \ \pm 610 \ \pm 1100 \ \pm 2700 \ \pm 360 \ \pm 450 \ \pm 450 \ \pm 650 \ \pm 1400 \ \pm 200 \ \pm 1100 \ \pm 2780 \ \end{array}$	± 110 ± 130 ± 540 ± 1000 ± 70 ± 460 ± 300 ± 240 ± 200 ± 260 ± 200 ± 320 ± 250 ± 200 ± 100 ± 100 ± 400	$\begin{array}{c c} -10 \\ -80 \\ 450 \\ 1900 \\ \hline \\ 40 \\ -160 \\ 100 \\ 380 \\ 810 \\ -3500 \\ -210 \\ 1900 \\ -340 \\ -100 \\ -100 \\ -100 \\ -100 \\ 350 \\ -400 \\ \hline \\ 10 \\ \end{array}$	$\begin{array}{c} X_2 \\ \pm 150 \\ \pm 310 \\ \pm 800 \\ \pm 1400 \\ \pm 350 \\ \pm 850 \\ \pm 1300 \\ \pm 680 \\ \pm 620 \\ \pm 1100 \\ \pm 680 \\ \pm 530 \\ \pm 380 \\ \pm 530 \\ \pm 530 \\ \pm 530 \\ \pm 650 \\ \pm 1400 \\ \pm 230 \\ \pm 1000 \\ \pm 710 \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 60 \\ \pm 320 \\ \pm 900 \\ \pm 80 \\ \pm 220 \\ \pm 300 \\ \pm 140 \\ \pm 220 \\ \pm 600 \\ \pm 220 \\ \pm 700 \\ \pm 700 \\ \pm 700 \\ \pm 700 \\ \pm 50 \\ \pm 600 \\ \pm 50 \\ \pm 200 \\ \pm 140 \\ \end{array}$
Bin 1 Bin 2 Bin 3 Bin 4 Bin 5 Bin 6 Bin 7 Bin 8 Bin 9 Bin 10 Bin 11 Bin 12 Bin 13 Bin 14 Bin 15 Bin 16 Bin 17 Bin 18 Bin 19 Bin 19 Bin 20	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$egin{array}{c} X_1 \ \pm 150 \ \pm 280 \ \pm 810 \ \pm 1200 \ \pm 310 \ \pm 310 \ \pm 310 \ \pm 310 \ \pm 470 \ \pm 1400 \ \pm 630 \ \pm 1400 \ \pm 2700 \ \pm 360 \ \pm 450 \ \pm 450 \ \pm 650 \ \pm 1400 \ \pm 200 \ \pm 1100 \ \pm 200 \ \pm 1100 \ \pm 240 \ \pm 240 \ \end{array}$	± 110 ± 130 ± 540 ± 1000 ± 70 ± 460 ± 300 ± 240 ± 240 ± 200 ± 260 ± 200 ± 320 ± 250 ± 200 ± 300 ± 400 ± 400 ± 400	$\begin{array}{c c} -10 \\ -80 \\ 450 \\ 1900 \\ \hline 40 \\ -160 \\ 100 \\ 380 \\ 810 \\ -3500 \\ -210 \\ 1900 \\ -340 \\ -100 \\ -100 \\ -100 \\ -100 \\ -100 \\ 350 \\ -400 \\ 10 \\ 110 \\ \end{array}$	$\begin{array}{c} X_2 \\ \pm 150 \\ \pm 310 \\ \pm 800 \\ \pm 1400 \\ \pm 350 \\ \pm 850 \\ \pm 1300 \\ \pm 680 \\ \pm 620 \\ \pm 1100 \\ \pm 680 \\ \pm 630 \\ \pm 530 \\ \pm 380 \\ \pm 530 \\ \pm 530 \\ \pm 1400 \\ \pm 230 \\ \pm 1000 \\ \pm 240 \\ \end{array}$	$\begin{array}{c} \pm 130 \\ \pm 60 \\ \pm 320 \\ \pm 900 \\ \pm 80 \\ \pm 220 \\ \pm 300 \\ \pm 140 \\ \pm 220 \\ \pm 600 \\ \pm 220 \\ \pm 600 \\ \pm 220 \\ \pm 700 \\ \pm 310 \\ \pm 250 \\ \pm 310 \\ \pm 250 \\ \pm 600 \\ \pm 200 \\ \pm 140 \\ \pm 80 \\ \end{array}$

Table 7: The hadronic structure functions W_F , W_H , X_1 , and X_2 for each (Q^2, s_1, s_2) bin. For each structure function, the central value, statistical and systematic errors are given. The contributions shown in table 8 are included in the systematic errors.

	ΔW_A	ΔW_C	ΔW_D	ΔW_E
Efficiency	$\pm 22~\%$	$\pm7~\%$	$\pm 2~\%$	$\pm 3~\%$
Detector resolution	< 0.1~%	$\pm 13~\%$	$\pm 17~\%$	$\pm 3~\%$
Migration	$\pm 52~\%$	$\pm 19~\%$	$\pm 11~\%$	$\pm 14~\%$
Background contribution	$\pm 1~\%$	$\pm 2~\%$	$\pm 1~\%$	$\pm 1~\%$
$ au^- o \pi^- \pi^- \pi^+ \pi^0 u_ au ext{decay modelling}$	$\pm 23~\%$	$\pm 22~\%$	$\pm 30~\%$	$\pm 28~\%$
Kaon channels	$\pm 1~\%$	$\pm 17~\%$	$\pm 19~\%$	$\pm 28~\%$
Monte Carlo statistics	$\pm 0.5~\%$	$\pm 20~\%$	$\pm 20~\%$	$\pm 24~\%$
$P_{ au}$	< 0.1~%	$\pm 0.1~\%$	$\pm 0.1~\%$	$\pm 0.1~\%$
	ΔW_F	ΔW_H	ΔX_1	ΔX_2
Efficiency	$\Delta W_F \ \pm 3~\%$	$\Delta W_H \ \pm 6~\%$	$\Delta X_1 \ \pm 5~\%$	$\Delta X_2 \ \pm 3~\%$
Efficiency Detector resolution	$egin{array}{c c} \Delta W_F \ \pm 3\ \% \ \pm 20\ \% \end{array}$	$egin{array}{c} \Delta W_{H} \ \pm 6~\% \ \pm 21~\% \end{array}$	$\Delta X_1 \ \pm 5 \ \% \ \pm 5 \ \%$	$egin{array}{c} \Delta X_2 \ \pm 3 \ \% \ \pm 5 \ \% \end{array}$
Efficiency Detector resolution Migration	$egin{array}{c c} \Delta W_F \ \pm 3 \ \% \ \pm 20 \ \% \ \pm 9 \ \% \end{array}$	$egin{array}{c} \Delta W_{H} \ \pm 6~\% \ \pm 21~\% \ \pm 11~\% \end{array}$	$\Delta X_1 \ \pm 5 \ \% \ \pm 5 \ \% \ \pm 13 \ \%$	$\Delta X_2 \ \pm 3 \ \% \ \pm 5 \ \% \ \pm 10 \ \%$
Efficiency Detector resolution Migration Background contribution	$egin{array}{ c c c c c c c c c c c c c c c c c c c$	$egin{array}{c} \Delta W_{H} \ \pm 6~\% \ \pm 21~\% \ \pm 11~\% \ \pm 1~\% \ \end{array}$	$\Delta X_1 \ \pm 5 \ \% \ \pm 5 \ \% \ \pm 13 \ \% \ \pm 1 \ \%$	$egin{array}{c} \Delta X_2 \ \pm 3 \ \% \ \pm 5 \ \% \ \pm 10 \ \% \ \pm 1 \ \% \ \end{array}$
Efficiency Detector resolution Migration Background contribution $\tau^- \to \pi^- \pi^- \pi^+ \pi^0 \nu_\tau$ decay modelling	$egin{array}{c c} \Delta W_F \ \pm 3\ \% \ \pm 20\ \% \ \pm 9\ \% \ \pm 1\ \% \ \pm 1\ \% \ \pm 11\ \% \ \end{array}$	$egin{array}{c} \Delta W_{H} \ \pm 6\ \% \ \pm 21\ \% \ \pm 11\ \% \ \pm 1\ \% \ \pm 13\ \% \ \end{array}$	$\Delta X_1 \ \pm 5 \% \ \pm 5 \% \ \pm 13 \% \ \pm 1 \% \ \pm 24 \%$	$\begin{array}{c c} \Delta X_2 \\ \hline \pm 3 \ \% \\ \pm 5 \ \% \\ \pm 10 \ \% \\ \hline \pm 1 \ \% \\ \pm 34 \ \% \end{array}$
Efficiency Detector resolution Migration Background contribution $\tau^- \to \pi^- \pi^- \pi^+ \pi^0 \nu_\tau$ decay modelling Kaon channels	$egin{array}{c c} \Delta W_F \ \pm 3 \ \% \ \pm 20 \ \% \ \pm 9 \ \% \ \pm 1 \ \% \ \pm 11 \ \% \ \pm 23 \ \% \ \end{array}$	$egin{array}{c} \Delta W_H \ \pm 6~\% \ \pm 21~\% \ \pm 11~\% \ \pm 13~\% \ \pm 21~\% \ \end{array}$	$egin{array}{c} \Delta X_1 \ \pm 5 \ \% \ \pm 5 \ \% \ \pm 13 \ \% \ \pm 13 \ \% \ \pm 24 \ \% \ \pm 23 \ \% \ \end{array}$	$egin{array}{c} \Delta X_2 \ \pm 3 \ \% \ \pm 5 \ \% \ \pm 10 \ \% \ \pm 1 \ \% \ \pm 34 \ \% \ \pm 21 \ \% \ \end{array}$
EfficiencyDetector resolutionMigrationBackground contribution $\tau^- \rightarrow \pi^- \pi^- \pi^+ \pi^0 \nu_\tau$ decay modellingKaon channelsMonte Carlo statistics	$egin{array}{ c c c c c c c c c c c c c c c c c c c$	$egin{array}{c} \Delta W_H \ \pm 6~\% \ \pm 21~\% \ \pm 11~\% \ \pm 13~\% \ \pm 21~\% \ \pm 21~\% \ \pm 27~\% \ \end{array}$	$\Delta X_1 \ \pm 5 \ \% \ \pm 5 \ \% \ \pm 13 \ \% \ \pm 13 \ \% \ \pm 24 \ \% \ \pm 23 \ \% \ \pm 31 \ \% \ $	$egin{array}{c} \Delta X_2 \ \pm 3 \ \% \ \pm 5 \ \% \ \pm 10 \ \% \ \pm 10 \ \% \ \pm 34 \ \% \ \pm 21 \ \% \ \pm 26 \ \% \ \end{array}$

Table 8: Estimated contributions to the total systematic errors for the hadronic structure functions, averaged over the bins.

	$\Delta \gamma_{VA}$	$\Delta \gamma_{VA}^{ m KS}$	$\Delta\gamma_{VA}^{\mathrm{IMR}}$
Background fraction	< 0.01	< 0.01	< 0.01
Kaon channels	± 0.06	± 0.03	± 0.05
$ au^- o \pi^- \pi^- \pi^+ \pi^0 u_ au ext{decay modelling}$	< 0.01	< 0.01	< 0.01
Efficiency	< 0.01	< 0.01	< 0.01
Detector resolution	± 0.09	± 0.02	± 0.03
Migration	± 0.01	< 0.01	< 0.01
$P_{ au}$	± 0.03	± 0.01	± 0.02
Variation of the model parameters		± 0.01	± 0.12
total systematic error	± 0.11	± 0.04	± 0.14
statistical error	± 0.26	± 0.16	± 0.21

Table 9: Estimated error contributions for the measurements of γ_{VA} . $\Delta \gamma_{VA}$ represents the model independent measurement errors, while $\Delta \gamma_{VA}^{\text{KS}}$ and $\Delta \gamma_{VA}^{\text{IMR}}$ represent the errors for the KS and IMR models.



Figure 1: The model fits of the 3π (a) and 2π (b, c, and d) data distributions. The data shown have been corrected for background and efficiency. The detector resolution is folded into the models. The solid line is the KS model fit and the dashed line is the IMR model fit. The dotted line under the 3π distribution is the polynomial background contribution of the IMR model. For the KS model, the three 2π distributions are derived using the parameters, including the normalization, from the fit to the 3π distribution. The IMR model fit is a global fit of all four histograms. The Q^2 intervals for the 2π distributions, indicated by the arrows in (a), are (b) $0.81 < Q^2 < 1.10 \text{ GeV}^2$, (c) $1.10 < Q^2 < 1.44 \text{ GeV}^2$, and (d) $1.44 < Q^2 < 1.96 \text{ GeV}^2$.



Figure 2: The data for the uncut Dalitz-plot projection is overlaid by each of the two models. The data has been corrected for background and efficiency. The detector resolution is folded into the models. The solid line is the KS model and the dashed line is the IMR model. The Q^2 dependent polynomial background term of the IMR model has been included for that model, and its contribution is shown as the dotted line.



Figure 3: Measured structure functions w_A , w_C , w_D , and w_E as functions of Q^2 . The error bars represent the statistical and systematic errors added in quadrature.



Figure 4: Comparison of the measured structure functions w_A , w_C/w_A , w_D/w_A , and w_E/w_A (points with error bars) with the predictions of the KS model (solid line) and the IMR model (dashed line). The IMR model prediction for w_A includes the polynomial background term. With both models there is good agreement between the model predicted and the data angular distributions for w_C/w_A , w_D/w_A , and w_E/w_A . For the w_A distribution, however, the KS model is preferred over the IMR model.



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Figure 5: Qualitative comparison of the axial-vector structure functions W_A , W_C , W_D , and W_E between the measurement (for $1.21 \text{GeV}^2 < Q^2 < 1.44 \text{GeV}^2$) and the KS model prediction (for $Q^2 = 1.3 \text{GeV}^2$) in the Dalitz plane. The fit result from the lower half of the Dalitz plane ($s_1 > s_2$) is mirrored to the upper half for improved clarity. The shapes of the distributions are correctly predicted by the model.



Figure 6: Comparison of the measured structure functions W_F , W_H , X_1 , and X_2 (points with error bars) with the null hypothesis for scalar and vector components for each bin. See table 4 for an explanation of the bin numbers.



Figure 7: The likelihood as a function of γ_{VA} (points), with arbitrary normalisation. The solid line is a Gaussian interpolation.