

# A multi basin SWAT model analysis of runoff and sedimentation in the Blue Nile, Ethiopia

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**Abstract.** A multi basin analysis of runoff and erosion in the Blue Nile Basin, Ethiopia was conducted to elucidate sources of runoff and sediment. Erosion is arguably the most critical problem in the Blue Nile Basin, as it limits agricultural productivity in Ethiopia, degrades benthos in the Nile, and results in sedimentation of dams in downstream countries. A modified version of the Soil and Water Assessment Tool (SWAT) model was developed to predict runoff and sediment losses from the Ethiopian Blue Nile Basin. The model simulates saturation excess runoff from the landscape using a simple daily water balance coupled to a topographic wetness index in ways that are consistent with observed runoff processes in the basin. The spatial distribution of landscape erosion is thus simulated more correctly. The model was parameterized in a nested design for flow at eight and sediment at three locations in the basin. Subbasins ranged in size from 1.3 to 174 000 km<sup>2</sup>, and interestingly, the partitioning of runoff and infiltrating flow could be predicted by topographic information. Model predictions showed reasonable accuracy (Nash Sutcliffe Efficiencies ranged from 0.53–0.92) with measured data across all sites except Kessie, where the water budget could not be closed; however, the timing of flow was well captured. Runoff losses increased with rainfall during the monsoonal season and were greatest from areas with shallow soils and large contributing areas. Analysis of model results indicate that upland landscape erosion dominated sediment delivery to the main stem of the Blue Nile in the early part of the growing season when tillage occurs and before the soil was wetted up and plant cover was established. Once plant cover was established in mid August landscape erosion

was negligible and sediment export was dominated by channel processes and re-suspension of landscape sediment deposited early in the growing season. These results imply that targeting small areas of the landscape where runoff is produced can be the most effective at controlling erosion and protecting water resources. However, it is not clear what can be done to manage channel erosion, particularly in first order streams in the basin.

## 1 Introduction

Watershed management strategies are critical to efficiently utilize the natural resources base while maintaining environmental quality. Of the many resources at risk in the Ethiopian Highlands soil and water are arguably the most critical, as nearly 80% of the population depends on subsistence agriculture. One process that threatens the resource base is soil erosion. The Ethiopian Highlands provide nearly 85% of flow in the main stem of Nile in Egypt, and support 80% of the Ethiopian population (Swain, 1997). Thus it is critical to understand the processes and sources impacting water quantity, quality and, most importantly erosive losses and sedimentation mechanisms that threaten both agricultural productivity (Constable, 1984) and the considerable infrastructure in downstream countries, including Sudan and Egypt.

Ethiopia has abundant yet underutilized water resource potential, and 3.7 million hectare of potentially irrigable land that can be used to improve agricultural production and productivity (Awulachew et al., 2007; MoWR, 2002). However, agricultural productivity in Ethiopia lags other, similar, regions, which is attributed to unsustainable environmental degradation mainly from erosion and loss of soil fertility



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(Grunwald and Norton, 2000). Therefore, understanding the hydrological processes of different parts of the basin is crucial to water and land resource management. Soil erosion by water represents a major threat to the long-term productivity of agriculture in the Ethiopian Highlands where the estimated soil erosion rates range from as low as  $16 \text{ t ha}^{-1} \text{ y}^{-1}$  (Gizawchew, 1995) to as much as  $300 \text{ t ha}^{-1} \text{ y}^{-1}$  (Hurni, 1993; Herweg and Stillhardt, 1999).

Ethiopia, often referred to as the water tower of East Africa, is dominated by mountainous topography, and the rainfall-runoff processes on the mountainous slopes are the source of the surface water for much of Ethiopia (Derib, 2009), and thus, understanding the rainfall-runoff processes is critical to controlling erosion and enhancing agricultural productivity. The majority of the sedimentation of rivers in the basin occurs during the early period of the rainy season and peaks of sediment are consistently measured before peaks of discharge for a given rainy season (Steenhuis et al., 2009). Thus, reservoir management in Sudan and Egypt can be adjusted to allow the highest concentrations of sediment to pass, while still allowing adequate water to fill the reservoirs. Despite this, sedimentation originating from the Ethiopian Highlands results in reduced capacity of reservoirs in downstream Sudan and Egypt. The Roseires reservoir in Sudan is reported to be almost 60 percent filled with sediment, and the Sennar reservoir, downstream of Roseires is equally impaired (Garzanti et al., 2006).

Soil loss from a watershed can be estimated based on an understanding of the underlying hydrological processes, climatic conditions, landforms, land management, and soil factors. Assessing and mitigating soil erosion at the basin level is complex both spatially and temporally. Hence, watershed models that are capable of capturing these complex processes in a dynamic manner can be used to provide an enhanced understanding of the relationship between hydrologic processes, erosion/sedimentation, and management options. There are many models that can continuously simulate stream flow, erosion/sedimentation, or nutrient loss from a watershed. However, most were developed in temperate climates and were never intended to be applied in monsoonal regions, like Ethiopia, with an extended dry period. In monsoonal climates a given rainfall volume at the onset of the monsoon produces a drastically different runoff volume than the same rainfall volume at the end of the monsoon (Liu et al., 2008). Steenhuis et al. (2009) and Liu et al. (2008) showed that the ratio of discharge to precipitation – evapotranspiration ( $Q/(P-ET)$ ) increases with cumulative precipitation and consequently the watersheds behave differently depending on how much moisture is stored in the watershed, suggesting that saturation excess processes play an important role in the watershed runoff response. One characteristic of Ethiopian Blue Nile hillslopes is that most have infiltration rates in excess of the rainfall intensity, thus most runoff is produced when the soil saturates (Ashagre, 2009) or from degraded, shallow soils. Indeed, data from Soil Conservation

Reserve Program (SCRIP) watersheds (Bayabil, 2009; Engda, 2009) show the probability of rainfall intensity exceeding the measured soil infiltration rate to be very low, only 7.8% of storm intensities exceeded the lowest measured infiltration rate. Of course defining sources of landscape erosion require knowledge of both where runoff is generated, and of how the landscape is managed (e.g., tillage, livestock, vegetative cover, etc.). Few models have been developed that can predict both the distributed runoff sources and the sedimentation dynamics in the Blue Nile.

Many of the commonly used watershed models employ some form of the Soil Conservation Service Curve Number (CN) to predict runoff, which links runoff response to soils, land use, and 5-day antecedent rainfall (AMC), and not the cumulative seasonal rainfall volume. The Soil and Water Assessment Tool (SWAT) model is a basin scale model where runoff is based on land use and soil type (Arnold et al., 1998), and not on topography, therefore, runoff and sediment transport on the landscape is only correctly predicted for infiltration excess overland flow and not when saturation excess overland flow from variable source areas (VSA) dominates. Thus critical sediment source areas might not be explicitly recognized and unique source areas. SWAT determines an appropriate CN for each simulated day by using this CN-AMC distribution in conjunction with daily soil moisture values determined by the model. This daily CN is then used to determine a theoretical storage capacity,  $S$ , of the watershed for each day. While a theoretical storage capacity is assigned and adjusted for antecedent moisture for each land use/soil combination, the storage is not used to directly determine the amount of water allowed to enter the soil profile. Since this storage is a function of the lands infiltration properties, as quantified by the CN-AMC, SWAT indirectly assumes that only infiltration excess processes govern runoff generation. Prior to any water infiltrating, the exact portion of the rainfall that will runoff is calculated via these infiltration properties. This determination of runoff volume before soil water volume is an inappropriate approach for all but the most intense rain events, particularly in monsoonal climates where rainfall is commonly of low intensity and long duration and saturation processes generally govern runoff production. Several studies in the Blue Nile basin or nearby watersheds have suggested that saturation excess processes control overland flow generation (Liu et al., 2008; Collick et al., 2008; Ashagre, 2009; Engda, 2009; Tebebu, 2009; Tebebu et al., 2010; White et al., 2010) and that infiltration-excess runoff is rare (Liu et al., 2008; Engda, 2009).

Based on the finding discussed above, White et al. (2010) and Easton et al. (2010) recently modified SWAT to more effectively model hydrological processes in monsoonal climates such as Ethiopia. This new version of SWAT, SWAT-Water Balance (SWAT-WB), calculates runoff volumes based on the available storage capacity of a soil and distributes the storages across the watershed using a soil topographic wetness index (Easton et al., 2008), and can lead to more

accurate simulation of where runoff occurs in watersheds dominated by saturation-excess processes (White et al., 2010). White et al. (2010) compared the performance of SWAT-WB and the standard SWAT model in the Gumera watershed in the Lake Tana Basin, Ethiopia, and found that even following an unconstrained calibration of the CN, the SWAT model the results were between 17 and 23% worse than the SWAT-WB model.

We briefly present how the SWAT-WB model calculates the hydrologic response of the basin and then apply the SWAT-WB model to the Ethiopian portion of the Blue Nile Basin that drains via the main stem of the river at El Diem on the border with Sudan (the Rahad and Dinder subbasins that drain the Northeast region of Ethiopia were not considered). We show that incorporating a redefinition how hydrologic response units (HRUs) are delineated combined with a water balance to predict runoff can improve our analysis of when and where runoff and erosion occur in a watershed. The SWAT-WB model is initialized for eight subbasins ranging in size from 1.3 km<sup>2</sup> to 174 000 km<sup>2</sup>. We calibrate the model for flow using a priori topographic information and validated with an independent time series of flows. For sediment, since there is little data to split into calibration and validation data sets, we employ leave-one-out cross-validation (McCuen, 2005) (e.g., model is calibrated with one n-1 data points to predict the withheld point and repeated until each data point has been withheld from the calibration and predicted using the corresponding n-1 calibrated model). We show that the tested methodology captures the observed hydrologic and erosive processes quite well across multiple scales, while significantly reducing the calibration data requirements. The reduced data requirements for model initialization have implications for model applicability to other data scarce regions. Finally, we discuss the implications of watershed management with respect to the model results.

## 2 Materials and methods

### 2.1 Summarized SWAT model description

The Soil and Water Assessment Tool (SWAT) model is a river basin model created to run with readily available input data so that general initialization of the modeling system does not require overly complex data gathering, or calibration. SWAT was originally intended to model long-term runoff and nutrient losses from rural watersheds, particularly those dominated by agriculture (Arnold et al., 1998). SWAT requires soils data, land use/management information, and elevation data to drive flows and direct sub-basin routing. While these data may be spatially explicit, SWAT lumps the parameters into hydrologic response units (HRUs), effectively ignoring the underlying spatial distribution. Traditionally, HRUs are defined by the coincidence of soil type slope and land use. Simulations require meteorological input data including pre-

cipitation, temperature, and solar radiation. Model input data and parameters were initially parsed using the ARCSWAT 9.2 interface. The interface combines SWAT with the ARCGIS platform to assimilate the soil input map, digital elevation model and land use coverage.

### 2.2 SWAT-WB saturation excess model overview

The modified SWAT model (SWAT-WB, White et al., 2010) uses a water balance in place of the CN for each HRU to predict runoff losses. Based on this water balance, runoff, interflow and infiltration volumes are calculated. While these assumptions simplify the processes that govern water movement through porous media (in particular, partly-saturated regions), for a daily model, water balance models have been shown to better capture the observed responses in numerous African watersheds (Guswa et al., 2002). For Ethiopia, water balance models outperform models that are developed in temperate regions (Liu et al., 2008; Collick et al., 2009; Steenhuis et al., 2009; White et al., 2010). For the complete model description see (Easton et al., 2010; and White et al., 2010). In its most basic form the water balance defines a threshold moisture content over which the soil profile can neither store nor infiltrate more precipitation, thus additional water become either runoff, interflow or percolates to the next soil layer ( $q_{E,i}$ ):

$$q_{E,i} = \begin{cases} (\theta_s) - (\theta_{i,t})d_i + P_t - E_{t_i} & \text{for: } P_t > (\theta_s - \theta_{i,t})d_i - E_{t_i} \\ 0 & \text{for: } P_t \leq (\theta_s - \theta_{i,t})d_i - E_{t_i} \end{cases} \quad (1)$$

where  $\theta_s$  (cm<sup>3</sup> cm<sup>-3</sup>) is the soil moisture content above which storm runoff is generated and  $\theta_{i,t}$  (cm<sup>3</sup> cm<sup>-3</sup>) is the current soil moisture content,  $d_i$  (mm) is the depth of the soil profile,  $P_t$  (mm) is the precipitation and  $E_{t_i}$  (mm) is the evapotranspiration. We recognize that in SWAT, there is no lateral routing of interflow among watershed units, and thus no means to distribute watershed moisture, thus Eq. (1) will result in the same excess moisture volume everywhere in the watershed given similar soil profiles.

To account for the differences in runoff generation in different areas of the landscape, White et al. (2010) proposed the following threshold function for storm runoff that varies across the watershed as a function of topography:

$$\tau = (\rho_i \theta_s - \theta_{i,t}) \quad (2)$$

where  $\rho_i$  is a number between 0 and 1 that reduces  $\theta_s$  to account for water that should drain down-slope, and is a function of the topography (as defined by a topographic wetness index ( $\lambda$ ), e.g., Beven and Kirkby, 1979). Note that Eq. 2 applies only to the first soil layer. Once the soil profile has been adequately filled Eq. 2 can be used to write an expression for the depth of runoff,  $q_{R,i}$ , (mm) from a wetness index,  $i$ :

$$q_{R,i} = \begin{cases} P_t - \tau_i d_i & \text{for } P_t > \tau_i d_i \\ 0 & \text{for } P_t \leq \tau_i d_i \end{cases} \quad (3)$$

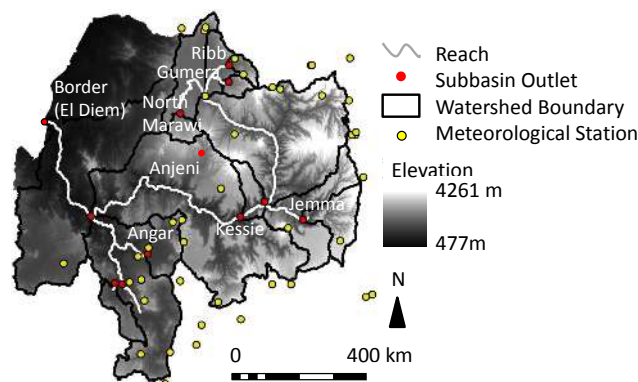
While the approach outlined above captures the spatial patterns of VSAs and the distribution of runoff and infiltrating fractions in the watersheds, Easton et al. (2010) noted that the need to maintain more water in the wettest wetness index classes for evapotranspiration (ET), and proposed adjusting the available water content (AWC) of the soil layers below the first soil layer (recall, the top soil layer is used to establish our runoff threshold, Eq. 2) so that higher topographic wetness index classes retain water longer, i.e., have AWC adjusted higher, and the lower classes dry quicker, i.e., AWC is adjusted lower by normalizing by the mean  $\rho_i$  value (e.g., similar to Easton et al., 2008).

Note, since this model generates runoff when the soil is above saturation, total rainfall determines the amount of runoff. When results are presented on daily basis rainfall intensity is assumed to be inconsequential. We recognize that under high intensity storms (e.g., storms with rainfall intensities greater than the infiltration capacity of the soil) we might under predict the amount of runoff generated, but this is the exception rather than the rule (Liu et al., 2008; Engda, 2009).

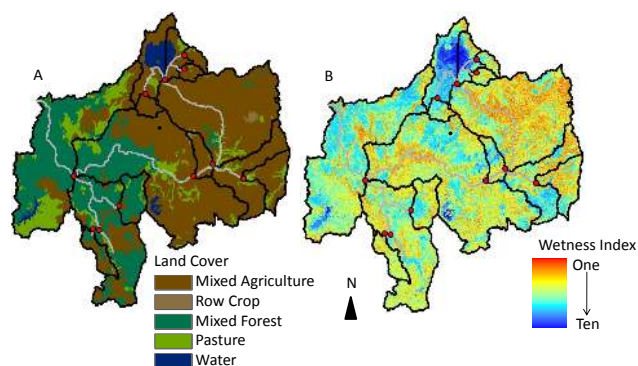
### 2.3 Watershed description

The Blue Nile Basin covers approximately 312 000 km<sup>2</sup> in Ethiopia and Sudan. The Upper Blue Nile Basin in Ethiopia that drains via the main stem of the Blue Nile River covers 174 000 km<sup>2</sup> (Fig. 1) (9.86° N 37.69° E basin centroid) is typified by mountainous terrain with steep hill slopes and relatively flatter highlands. The elevations range from 477 m at the border with Sudan to 4261 m in the central region of the basin. Temperatures and precipitation levels vary greatly in the basin. Temperatures in the basin show large elevation (6–25 °C) and diurnal variation but small seasonal changes, with an annual average of 18 °C (Conway, 2000). The climate of the basin is tropical highland monsoonal with the majority of the rain falling between June and October. Annual rainfall amounts decrease from the south-west (>2000 mm) to the north-east (1000 mm), with approximately 80% occurring between June and October. The average annual precipitation from 1994–2005 was 1470 mm (measured at 37 gauges data courtesy of the Ethiopian Ministry of Water Resources), with average potential evapotranspiration losses of 1220 mm.

Predominant soils are generally characterized as vertisols, luvisols, and leptosols (FAO-AGL, 2003). Soil profiles in the highlands are characterized by permeable soils, underlain by bedrock at depth. Soils are generally deeper in the lower reaches of the basin while soil depth is less on the steeper slopes. The basin is predominantly agricultural in the Highland portion, consisting of pasture and crops (64%) and forested (34%) in the western regions where elevations decline and slopes are steep. Water and wetland comprise (2%), (Fig. 2). Impervious surfaces or urban areas occupy <1% of the watershed and were thus excluded from consideration in the model.



**Fig. 1.** Digital Elevation Model (DEM), reaches, subbasins and sub-basin outlets initialized in the Blue Nile Basin SWAT model. Also displayed is the distribution of meteorological station used in the model.



**Fig. 2.** Landuse/landcover (A) in the Blue Nile Basin (source EN-TRO), and the Wetness Index (B) used in the SWAT-WB Blue Nile Model.

The specific subbasins that were utilized were Anjeni, Gumer, Ribb, North Marawi, Angar, Jemma, Kessie, and the Ethiopian Abbay Blue Nile Basin (BNB) at El Diem. A short description of each follows.

The Anjeni watershed covers an area of 113.4 ha. The watershed is oriented North-South and flanked on three sides by plateau ridges. It is located at 37° 31'E and 10° 40'N and lies 370 km NW of Addis Ababa to the south of the Choke Mountains. The mean annual rainfall is 1690 mm with a low variability of 10% with mean daily temperature ranges from 9 °C to 23 °C. Agriculture is the dominant landuse. See SCRIP (2000) for additional data on the Anjeni watershed.

The Gumer, Ribb, and North Marawi watersheds are located in the Lake Tana Basin, Ethiopia and range in size from approximately 1200 to 1600 km<sup>2</sup>. All are heavily (~95%) cultivated, with elevations ranging from 1700 to 4000 m above sea level and predominant soils are generally characterized as chromic and haplic luvisols (FAO-AGL, 2003).

The Jemma subbasin is located on the eastern edge of the Abbay Blue Nile Basin, and is characterized by relatively low

rainfall (less than  $1000 \text{ mm y}^{-1}$ ). Agriculture dominates the landuse (90%), and elevations range from 1300 to 3800 m. Dominate soil types are eutric vertisols and eutric leptosols.

The Angar subbasin is located in the southern region of the BNB. Elevations range from 860 to 3210 m. The area has some of the highest rainfall in the entire basin (between 1200 and 2000 mm). Unlike other subbasins, Angar is predominately forested, with some pastoral land (Fig. 2). The dominant soils in the basin are alisols, acrisols, nitosols and leptosols.

Kessie (Fig. 1) drains an area of approximately  $65,000 \text{ km}^2$ , and integrates the Gumera, Ribb, North Marawi, and Jemma subbasin. The Kessie station is located on the main stem of the Blue Nile. Landuse above Kessie is predominately agriculture, and elevations range from 1000 to nearly 4300 m.

## 2.4 Input data

*Spatial Data:* Required landscape data includes tabular and spatial soil data, tabular and spatial land use information, and elevation data. The spatial extent of upper Blue Nile Basin soils were taken from the FAO soil data base (FAO-AGL, 2003) (Fig. 2). Soil properties used in the SWAT model were obtained from several sources. Several soil properties are imbedded in the FAO soils data base, however, many properties needed by SWAT are not included in the FAO soil, thus a review studies in the region, and literature search for specific soil type properties was conducted. Arithmetic means were used for all soils properties for which a range of values were found. We created a soil topographic index, ( $\lambda$ ) – soil hybrid map for each subbasin and used it in place of the standard soils input map (as per Easton et al., 2008). The associated soils properties for the  $\lambda$ -soils hybrid map were extracted from the FAO database and look up tables were linked to the map using the ARCSWAT 9.2 interface. We lumped the watershed's  $\lambda$  into 10 equal area intervals ranging from 1 to 10, with index class 1 covering the 10% of the watershed area with the lowest  $\lambda$  (i.e. lowest propensity to saturate) and index class 10 containing the 10% of the watershed with the highest  $\lambda$  (i.e. highest propensity to saturate) (Fig. 2). These wetness index classes were intersected with the land use to create 962 HRUs in 16 subbasins (Fig. 2). A digital elevation model (DEM) of the basin was obtained from the International Water Management Institute (IWMI) with  $76 \text{ m} \times 76 \text{ m}$  horizontal and 1 m vertical resolutions. Land use/land cover maps containing 19 land cover classifications were obtained from the Eastern Nile Technical Regional Office (ENTRO), and reclassified into five dominant land use/land covers (Fig. 2).

### 2.4.1 Required meteorological data

Daily precipitation and minimum and maximum temperature data were obtained from the Ethiopian Ministry of Wa-

ter Resources for 37 stations distributed throughout the basin (Fig. 1). Daily solar radiation, wind speed and humidity data were obtained from the United States National Climatic Data Center. Daily potential evapotranspiration rates were calculated in the SWAT model using the Penmen-Monteith method and default values were used for all unavailable parameters.

## 3 Model calibration

### 3.1 Hydrology

The water balance methodology requires very little direct calibration, as most parameters can be determined a priori. Soil storage was calculated as the product of soil porosity and soil depth from the soils data. Soil storage values were distributed via the  $\lambda$  described above, and the effective depth coefficient ( $\rho_i$ , varies from 0 to 1) was adjusted along a gradient in  $\lambda$  values. We assume that the distribution of  $\rho_i$  values is inversely proportional to  $\lambda_i$  (averaged across each wetness index class or HRU) and that the lowest  $\lambda$ , ( $\lambda_o$ ) corresponds to the highest  $\rho_i$  ( $\rho_o$ ) (Easton et al., 2010):

$$\rho_i = \frac{\lambda_o}{\lambda_i}(\rho_o). \quad (4)$$

In this manner, the  $\rho_i$  distribution (Fig. 3) requires information on the topography (and perhaps soil) and the upper bound effective depth coefficient,  $\rho_o$ , for the driest wetness index class; without any additional information about the watershed, we assume  $\rho_o = 1$ . Equation (4) gives us an initial estimate of the distribution of  $\rho_i$ -values with no calibration (Fig. 3a).

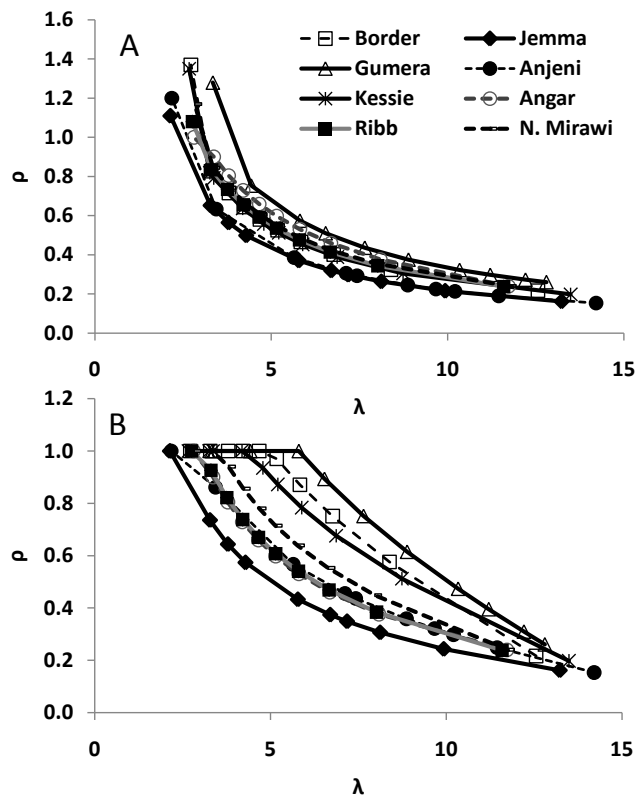
To constrain or “calibrate”  $\rho_o$ , we recognize that, since the  $\rho$ -value controls how much precipitation is routed as runoff, it also controls how much precipitation water can enter the soil for a given wetness index class. Thus, a larger fraction of the precipitation that falls on an area with a large  $\rho_i$  will potentially recharge the ground water than in an area with a small  $\rho_i$ . As a first approximation, then, we assume  $\rho_i$  can be equated the ratio of groundwater recharge,  $q_{B,i}$  to total excess precipitation.,  $q_{E,i}$ , i.e., precipitation falling on wetness class  $i$  that eventually reaches the watershed outlet:

$$\rho_i = \frac{q_{B,i}}{q_{E,i}} \quad (5)$$

Here we assume that the area-weighted sum of  $\rho_i$  must equal the watershed baseflow index,  $\Pi_B$ :

$$\Pi_B = \frac{Q_B}{Q_E} \quad (6)$$

where  $Q_E$ , (mm) and  $Q_B$ , (mm) are the basin average excess precipitation (stream flow) and baseflow, respectively. Baseflow is determined directly from digital signal filter baseflow separation technique of several years of daily streamflow hydrographs (Arnold et al., 1995; Hewlett and Hibbert, 1967).



**Fig. 3.** Distribution of the effective depth coefficient ( $\rho_i$ ) values defined by Eq. (4) (a) and Eq. (8) (b) for the various sub-basins.

The  $\rho_o$ -parameter (Eq. 4) can be constrained by the area-weighted average of  $\rho_i$ , using Eq. 4 as  $\rho_i$  and rearranging to solve for  $\rho_o$ :

$$\rho_o = \frac{\Pi_B \sum A_i}{\sum \left( \frac{\lambda_o}{\lambda_i} A_i \right)} \quad (7)$$

where  $A_i$  is the area of the wetness index class. If  $\rho_o > 1$ , we set  $\rho_o = 1$  and adjust the distribution of  $\rho_i$  iteratively until the sum of the spatially averaged  $\rho_i$  equal  $\Pi_B$ . To do this we assume that for all wetness classes with  $\lambda > \lambda^*$ ,  $\rho_i = 1$  and below  $\lambda^*$  the adjusted  $\rho_i$  linearly approach the initial distribution such that the adjusted and initial  $\rho_i$  values are equal at the maximum  $\lambda$   $\lambda_M$ , (Fig. 1). Let  $\rho_e^*$  be the value of the unadjusted  $\rho_i$  at  $\lambda^*$  and the adjusted  $\rho_i$  are calculated as:

$$\rho_i = \begin{cases} 1 & \text{for } \lambda_0 < \lambda < \lambda^* \\ \left( \frac{1 - \rho_e^*}{\lambda^* - \lambda_M} \right) (\lambda_i \lambda_M) + \rho_{ei} & \text{for } \lambda^* < \lambda < \lambda_M \end{cases} \quad (8)$$

While Eq. (8) can be solved iteratively by adjusting  $\lambda^*$ , we found the following approximation for  $\lambda^*$  worked well.

$$\lambda^* = \lambda_{ei} + (\lambda_{ei} - \lambda_0) \quad (9)$$

where  $\lambda_{ei}$  is the value of  $\lambda$  where the unadjusted  $\rho_i = 1$  (Fig. 3) (See Easton et al., 2010 for complete details).

The primary difference between the CN based SWAT and the water balance based SWAT is that runoff is explicitly attributable to source areas according to a wetness index distribution, rather than by land use and soil infiltration properties as in original SWAT (Easton et al., 2008). Soil properties that control saturation-excess runoff generation (saturated conductivity, soil depth) affect runoff distribution in SWAT-WB since they are included in the wetness index via Eq. (4). Flow calibration was validated against an independent time series that consisted of at least one half of the observed data. To insure good calibration, we also made sure that our result maximized the coefficient of determination ( $r^2$ ) and the Nash-Suttcliffe efficiency (NSE) (Nash and Suttcliffe, 1970). Table 1 summarizes the calibrated  $\rho_i$  values for each wetness index class and Table 2 summarizes the calibration statistics. Since flow data at some of the available gauge locations was available at the monthly time step (Angar, Kessie, Jemma), and daily at others (Anjeni, Gumera, Ribb, North Marawi, El Diem), the model was run for both time steps, and the results presented accordingly.

### 3.2 Sediment

Sediment export from the Blue Nile Basin was calibrated to measured daily sediment discharge at the El Diem station on the Sudan/Ethiopia border during 2003 and 2004 (Ahmed, 2003), and in the Anjeni micro-watershed in 1995–1996 and 2000. Since limited calibration data precludes the use of more traditional calibration and validation data sets sediment parameters were calibrated using a leave-one-out cross validation time series (McCuen, 2005) to ensure the model stability. For the leave-one-out cross validation one observation point is successively omitted in a series of steps. The model is calibrated with one data point withheld and the resultant calibration, based on n-1 data points, is used to predict the withheld point. This process is repeated until each data point has successively been withheld from the calibration and predicted using the corresponding n-1 calibrated model. The predicted data points are then combined into a leave-one-out cross validation time series that can be compared to the data to derive goodness of fit statistics, referred to as a leave-one-out cross validation statistics. Since each point in the leave-one-out cross validation time series is predicted by a model that was calibrated with the corresponding data point excluded, it represents a model prediction that is independent of the model calibration. A small amount of sediment data was available during 1995–1996 in the Ribb subbasin, which was used as a check of the calibration.

Based on SCRIP watershed data we assumed that approximately 25% of the steeply sloped agricultural land utilized terraces or bunding to reduce erosion (Werner, 1986). To include this management practice in the model the HRU slope (HRU\_SLP) was reduced by 37.5% and the slope length (SLSUBBASIN) was reduced by 50% for areas with slope greater than 5%. Ashagre (2009) working in the Anjeni

**Table 1.** Effective depth coefficients ( $\rho_i$ ) for each wetness index class and watershed in the Blue Nile Basin model from Eq. (8). The  $\Pi_B$  is determined from baseflow separated runoff of the streamflow hydrograph and distributed.

Wetness Index Class	$\rho_i$ (Border)	$\rho_i$ (Kessie)	$\rho_i$ (Jemma)	$\rho_i$ (Angar)	$\rho_i$ (Gumera)	$\rho_i$ (Ribb)	$\rho_i$ (N. Marawi)	$\rho_i$ (Anjeni)
10 (Most Saturated)	0.22	0.20	0.16	0.15	0.26	0.24	0.24	0.15
9	0.58	0.51	0.24	0.22	0.31	0.41	0.43	0.25
8	0.75	0.68	0.31	0.26	0.40	0.51	0.53	0.30
7	0.87	0.78	0.35	0.30	0.47	0.59	0.62	0.32
6	0.97	0.87	0.37	0.34	0.61	0.66	0.69	0.36
5	1.00	0.94	0.43	0.38	0.75	0.72	0.75	0.44
4	1.00	1.00	0.57	0.42	0.89	0.80	0.83	0.46
3	1.00	1.00	0.64	0.47	1.00	0.88	0.91	0.57
2	1.00	1.00	0.74	0.52	1.00	0.99	1.00	0.86
1 (Least saturated)	1.00	1.00	1.00	0.63	1.00	1.00	1.00	1.00
* $\Pi_B$	0.84	0.80	0.48	0.37	0.67	0.68	0.70	0.47

\*  $\Pi_B$  partitions moisture in above saturation to runoff and infiltration.

**Table 2.** Calibrated subbasins (Fig. 1), drainage area, model fit statistics (coefficient of determination,  $r^2$  and Nash-Sutcliffe Efficiency, NSE), and observed and predicted flows.

Subbasin	Area (km <sup>2</sup> )	$r^2$	NSE	Observed Annual Discharge (Mm <sup>3</sup> )	Mean	Observed Normalized Discharge (mm yr <sup>-1</sup> )	Predicted Direct Runoff (mm yr <sup>-1</sup> )	Predicted Ground Water (mm yr <sup>-1</sup> ) <sup>3</sup>
Anjeni <sup>1</sup>	1.3	0.76	0.84	0.40		563	44	453
Gumera <sup>1</sup>	1286	0.83	0.81	501		390	22	316
Ribb <sup>1</sup>	1295	0.74	0.77	495		382	25	306
North Marawi <sup>1</sup>	1658	0.78	0.75	646		390	17	274
Jemma <sup>2</sup>	5429	0.91	0.92	1142		210	19	177
Angar <sup>2</sup>	4674	0.87	0.79	1779		381	34	341
Kessie <sup>2</sup>	65 385	0.73	0.53	19 237		294	19	259
Border (El Diem) <sup>1</sup>	174 000	0.92	0.87	56 021		322	13	272

<sup>1</sup> Statistics are calculated on daily time step

<sup>2</sup> Statistics are calculated on monthly time step

<sup>3</sup> Includes both base and interflow.

SCRIP watershed and Engda (2009) working the Andit Tid SCRIP watershed showed that steeper slopes resulted in less runoff and lower erosion rates thus, we adjusted the overland Mannings-n (OV\_N) values as a function of slope steepness. Since SWAT is incapable of realistically modeling gully erosion, and gully formation can be an important erosion mechanism in the Ethiopian highlands the soil erodibility factor (USLE\_K) in the Modified Universal Soil Loss Equation (MUSLE) (Williams, 1975) equation was increased by 25% to reflect this. This might result in specific field based erosion estimates being over-predict to correctly predict sub-basin scale erosion. Landscape erosion in SWAT is computed using the MUSLE, which determines sediment yield using a runoff factor that estimates the energy that governs the transport of eroded sediment in surface flow. Thus the sediment

delivery ratio is incorporated into the equation and does not need to be specified separately.

The most sensitive parameters controlling erosion in the watershed were those used for calculating the maximum amount of sediment that can be entrained during channel routing. The channel properties, Manning's-n (CH\_N) value for tributary channels affects the time of concentration and indirectly the peak discharge in the channel. Factors like the channel cover (CH\_COV) and the channel erodibility (CH\_EROD) linearly influence the soil loss from channels. Channel sediment yield was also very sensitive to the effective hydraulic conductivity (CH\_K) of the main channel alluvium. Table 3 gives the calibrated channel sediment parameters for the three sites with measured data (Anjeni, Ribb, and El Diem) against which to calibrate. We determined

**Table 3.** Parameters affecting channel degradation and deposition of sediment calibrated using leave one out cross validation for Anjeni, Ribb, and El Diem.

Parameter	Upper Bound	Lower Bound	Anjeni	Ribb <sup>1</sup>	El Diem <sup>2</sup>
			Calibrated Values		
SPCON	0.01	0.001	0.004		
SPEXP	2	1	1.34		
Channel Erodability Factor (CH_EROD)*	1	0	0.734	0.589	0.38
Channel Cover Factor (CH_COV)*	1	0	0.893	0.741	0.62
Channel Manning's N (CH_N)*	0.15	0.025	0.067	0.076	0.095
Channel Saturated Hydraulic Conductivity (CH_K)*	>100	0	13.4	26.7	6.4

\* Varies by reach

<sup>1</sup> Parameters calibrated for the Ribb subbasin were transferred to Gumera, North Marawi, and the remaining land area in the Lake Tana Basin.

<sup>2</sup> Parameters calibrated at the El Diem station were transferred to all subbasins upstream except for Anjeni, and those in the Lake Tana Basin.

the respective amounts of landscape and channel sediment by comparing the sediment yield from each HRU summed within a subbasin to the channel sediment yield, which, when summed, equal the subbasin sediment export. The HRU sediment yield is an estimate of sediment delivery from an HRU into the main channel during the time step, while the channel sediment yield is any sediment eroded or re-entrained from the channel. Thus, sediment export from a subbasin includes both the sediment yield from the HRUs and any sediment eroded or entrained from the channel.

## 4 Results

### 4.1 Hydrology

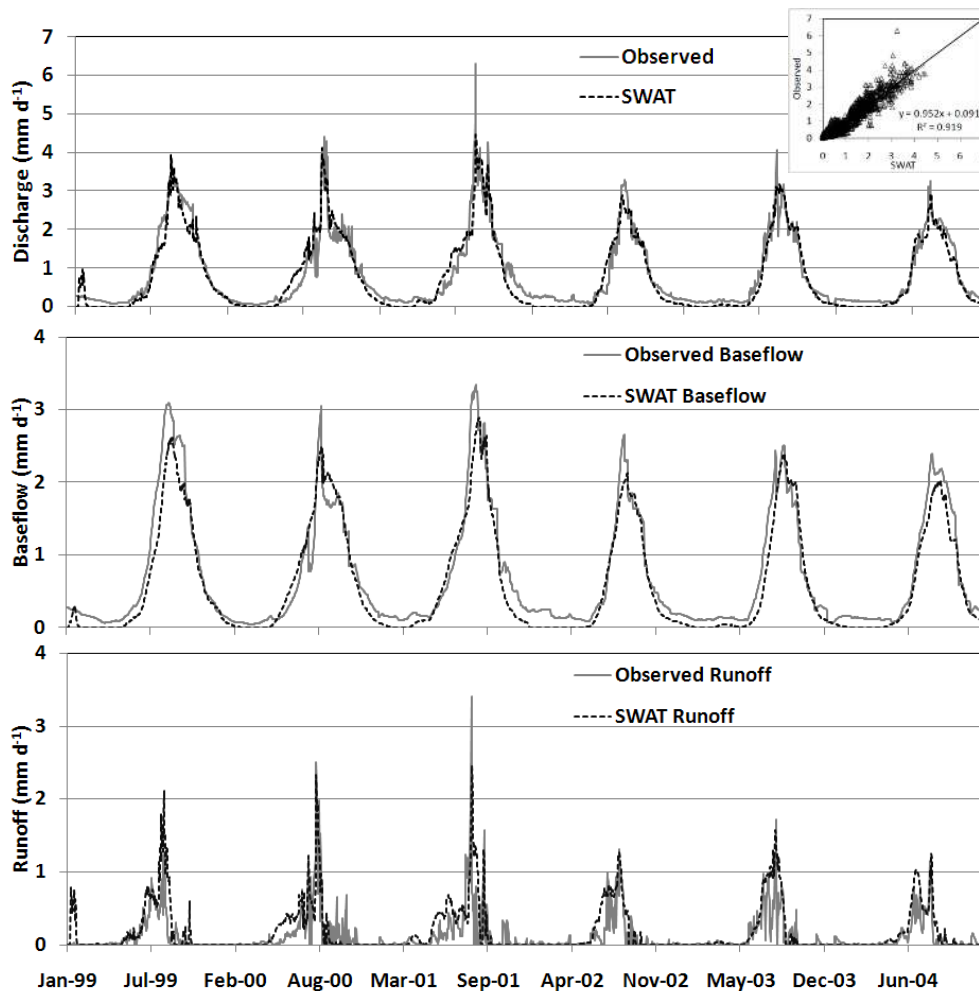
Runoff and subsurface flow from the watershed were summed at the watershed outlet to predict streamflow. The graphical comparison of the modeled and measured daily streamflow at the El Diem station at the Sudan border (e.g., integrates all subbasins above) is shown in Fig. 4. The model was able to capture the dynamics of the basin response well (NSE=0.87,  $r^2=0.92$ ) (Table 2, Fig. 4). Both baseflow and storm flow were correctly predicted with a slight over prediction of peak flows and a slight under prediction of low flows (Table 2), however, all statistical evaluation criterion indicted the model predicted well. In fact all calibrated subbasins predicted streamflow at the outlet reasonably well (e.g. Table 2). Model predictions showed good accuracy (NSE ranged from 0.53–0.92) with measured data across all sites except Kessie, where the water budget could not be closed; however, the timing of flow was well captured. The error at Kessie appears to be due to under estimated precipitation at the nearby gauges, as measured flow was nearly 15% higher than precipitation-evapotranspiration. Never the less, the prediction is within 25% of the measured data. Observed normalized discharge (Table 2) across the subbasins shows a large gradient, from 210 mm at Jemma to 563 mm

at Anjeni. For the basin as a whole, approximately 25% of precipitation exits the BNB at El Diem.

Table 1 shows the adjusted  $\rho_i$  parameter values (e.g. Eq. 8) for the various subbasin in the BNB, and that the parameter values are scalable, and can be determined from topographical information (i.e., the  $\rho_i$  values in vary by subbasin, but the distribution is similar, Fig. 3). The SWAT-WB model was able to accurately reproduce the various watershed responses across the range of scales. Notice for instance that the hydrographs at the Border (174 000 km<sup>2</sup>) (Fig. 4), Jemma (5400 km<sup>2</sup>) (Fig. 5), Gumera (1200 km<sup>2</sup>) (Fig. 6), and Anjeni, (1.13 km<sup>2</sup>) (Fig. 7), reasonably capture the observed dynamics (i.e., both the rising and receding limbs and the peak flows are well represented). There was a slight tendency for the model to bottom out during baseflow, likely due to over estimated ET, but the error is relatively minor. More importantly the model captures peak flows, which are critical to correctly predict to asses sediment transport and erosion.

Runoff and streamflow are highly variable both temporally (over the course of a year) (Fig. 4) and spatially (across the Ethiopian Blue Nile Basin) (Table 2). Daily watershed outlet discharge during the monsoonal season at Gumera is four to eight times larger than at the border (after normalizing flow by the contributing area) (Figs. 4 and 6). Anjeni, the smallest watershed had the largest normalized discharge, often over 20 mm d<sup>-1</sup> during the rainy season (Fig. 7). Discharges (in Mm<sup>3</sup> y<sup>-1</sup>) intuitively increase with drainage area, but precipitation also has a large impact on overall subbasin discharge. Both Jemma and Angar are approximately the same size (Jemma is actually slightly bigger) yet discharge from Angar is nearly 40% higher, a result of the higher precipitation in the south-western region of the basin. Temporally, outlet discharges typically peak in August for the small and medium sized basins and slightly later for Kessie and the border, a result of the lag time for lateral flows to travel the greater distances. Due to the monsoonal nature of the basin, there is a very low level of baseflow in all tributaries, and in fact some dry up completely during the dry season, which the





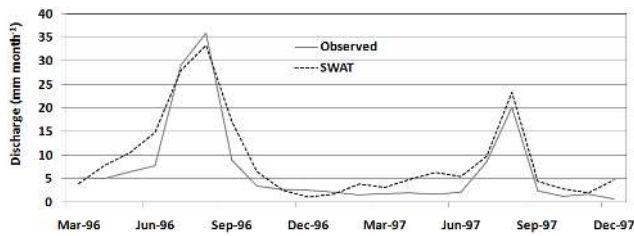
**Fig. 4.** Daily observed and predicted discharge, runoff, and baseflow at the Sudan border.

model reliably predicts, which is important when considering the impacts of intervention measures to augment flow.

Runoff losses predicted by the model varied across the basin as well, and were generally well corroborated by runoff estimates from baseflow separation of the streamflow hydrograph. Predicted runoff losses (averaged across the entire subbasin) varied from as low as  $13 \text{ mm y}^{-1}$  for the BNB as a whole subbasin to as high as  $44 \text{ mm y}^{-1}$  in Anjeni. Of course, small areas of the individual subbasins produce significantly higher runoff losses and others significantly less. These differences are well reflected in the average baseflow coefficient ( $\Pi_B$ ) for the subbasins (Table 1). Notice that the  $\Pi_B$  for Anjeni (smallest watershed, highest runoff losses) is significantly lower than for Gumera and the Border (Table 1). A lower  $\Pi_B$  reflects less average available storage in the watershed, (i.e. more rainfall ends up as runoff). This  $\Pi_B$  value is determined from the baseflow separation of the streamflow hydrograph (Hewlett and Hibbert, 1967), and can thus be considered a measured parameter. It is also interesting to note how the distribution of the individual  $\rho_i$  differs between

basins. For instance there are more classes (areas) in Anjeni and Angar that are prone to saturate, and would thus have a comparatively lower available storage than the other subbasins. This is relatively clear in looking at the streamflow hydrographs (Figs. 4–7) where the smaller watersheds tend to generate substantially more surface runoff. Conversely, as basin size increases (Kessie, Border) the saturated fraction of the watershed decreases, more of the rainfall infiltrates, resulting in greater baseflow, as reflected in the higher  $\Pi_B$ , or in terms of runoff the smaller upland watersheds have higher runoff losses than the larger basins. This is not unexpected, as the magnitude of the subsurface flow paths have been shown to increase with the size of the watershed, because as watershed size increases more and more deep flow paths become activated in transport (Steenhuis et al., 2009).

The ability to predict the spatial distribution of runoff source areas has important implications for watershed intervention, where information on the location and extent of source areas is critical to effectively managing the landscape. For instance, the inset of Fig. 8 shows the predicted spatial



**Fig. 5.** Monthly observed and predicted discharge at the Jemma subbasin.

distribution of average runoff losses for the Gumera watershed for an October 1997 event. As is evident from Fig. 8, runoff losses vary quite dramatically across the landscape, some HRUs are expected to produce no runoff, while others produced more than 90 mm of runoff. When averaged spatially at the outlet, runoff losses were 22 mm (Table 2). Other subbasins responded in a similar manner. These results are consistent with data collected in the Anjeni SCRP watershed (SCRP, 2000; Ashagre, 2009), which showed that runoff losses roughly correlate with topography.

#### 4.2 Sediment

Based on SCRP data from several of the micro watershed sites (Anjeni, Andit Tid) that shows sediment losses to be inversely related to slope position (e.g., steeper slopes produce less erosion) it appears that the hydrologic underpinning of the SWAT-WB model (e.g. less runoff is generated on steeper slopes) provides a conceptually correct platform to assess erosive processes. Figure 9 shows the SWAT model predicted and observed sediment export at El Diem. The daily NSE for the simulation period was 0.74, indicating acceptable model performance. Nearly 128 million tons per year were delivered during the 2 years of measurements (Ahmed, 2003), with a measured daily average during the rainy season of 1.22 million tons. The model predicted 121 million tons over the 2 yrs, with a rainy season daily average of 1.16 million tons. The average sediment concentration at El Diem was  $3.751 \text{ g L}^{-1}$ , while the model predicted a slightly higher concentration of  $4.123 \text{ g L}^{-1}$ . The higher concentration was somewhat counter balanced by the slightly under predicted flow (Fig. 4). Despite this, model performance appears to be adequate.

Interestingly the model predicted that landscape based erosion from agricultural areas, particularly tilled fields dominated sediment delivery to the reaches during the early part of the growing season (approximately mid-end August), after which landscape based erosion was predicted to decrease. The reduction in landscape borne sediment reflects the growth stage of plants in the highlands, which in mid-late August are reasonably mature, or at least have developed a canopy and root system that effectively reduces rill and sheet erosion (Zegeye, 2009). After that sediment export

from the various subbasins was controlled by channel erosion and re-entrainment/re-suspension of landscape sediment deposited in the reaches in the early part of the growing season. This sediment was subsequently mobilized during the higher flows that typically peak after the sediment peak is observed [e.g., the sediment peak occurs approximately two weeks (in July) before the flow peak (in August)] (compare Figs. 4 and 9). Figure 10 shows significant hysteresis between the rising and receding limbs of the sediment concentration hydrograph (natural log transformed data). The sediment concentration on the rising limb of the hydrograph has a lower slope, and higher intercept than the receding limb. While we do not know the mechanisms behind this difference it seems logical that there are different processes controlling the sediment dynamics during different parts of the year (e.g., as illustrated by the hysteresis). This, of course, has implications for reservoir management in downstream countries, in that much of the high sediment flow can pass through the reservoir during the rising limb, and the relatively cleaner flows stored during the receding limb. Never the less, the sheer volume of sediment exported from the Ethiopian highlands threatens many downstream structures regardless of their operation and clearly impacts agricultural productivity in the highlands.

SWAT predicts that the sediment later in the growing season is channel based (either from landscape sources deposited during lower velocity flows or directly from the channel itself). However, there is significant gully erosion in many areas of the highlands, that, in fact become active at approximately the same time as the flow peak occurs and SWAT predicts channel processes to be the source. Gully activation occurs once the soil has wet up and lost its cohesive nature. Soil wets up from the interflow from upslope areas, and thus it does not always occur simultaneously with landscape sources of erosion (Tebebu, 2009; Zegeye, 2009). In actuality, the receding limb of the sediment hydrograph (Fig. 10) is likely a combination of both channel re-suspension of landscape sources, channel erosion, and gully erosion. However, it should be noted that much of the main stem of the Blue Nile cuts through a rocky canyon composed of basalt lavas, granites, and sandstones, and thus direct channel and bank erosion is likely a small contributor. Smaller reaches where flow velocities are high likely do contribute sediment from both channel and bank sources.

While the model was only calibrated to the sediment concentrations and export at El Diem, and at the micro-watershed scale, both predicted similar phenomena. At both the basin and Anjeni scales the model predicted landscape sediment to be the dominant source until approximately mid August, after which there was a shift to (what the model predicts) channel erosion. Perhaps not surprisingly, the sediment hydrographs for Anjeni and El Diem were quite different. In Anjeni, the sediment hydrograph (Fig. 11) mimicked the flashy nature of the streamflow hydrograph, while at El Diem sediment export was much less flashy (Fig. 9). Table 4

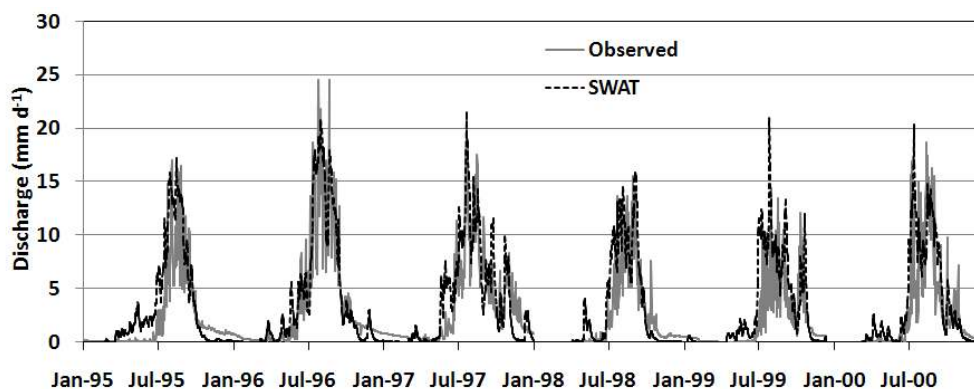


Fig. 6. Daily observed and predicted discharge from the Gumera subbasin.

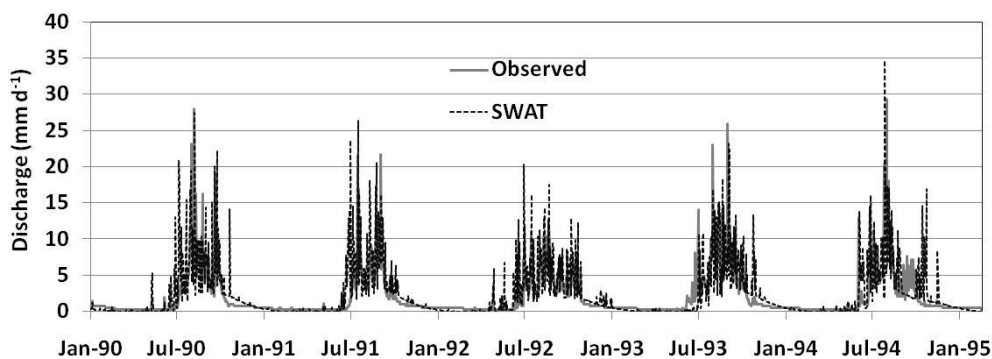


Fig. 7. Daily observed and predicted discharge from the Anjeni micro watershed.

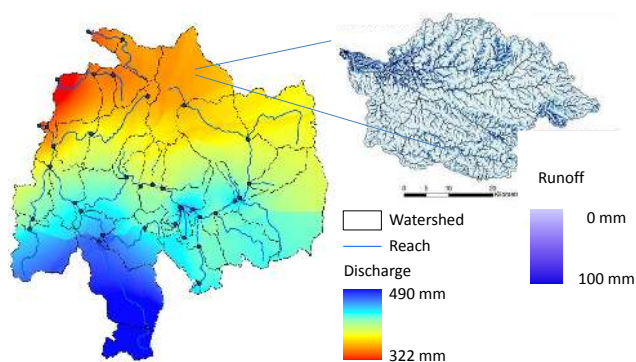


Fig. 8. Predicted average yearly spatial distribution of discharge in the Blue Nile Basin (main) and predicted runoff distribution in the Gumera sub watershed for an October 1997 event (inset).

shows the measured and predicted sediment export for the Border, Ribb and Anjeni. While the total sediment export intuitively increases with basin size, the normalized sediment export ( $\text{t km}^2$ ) was inversely proportional to the basin size (Table 4). This is a direct result of the difference in the base-flow coefficients ( $\Pi_B$ ) among the various sized basins, (e.g., 0.47 for Anjeni to 0.84 for the Border).

Indeed, based on the surficial geology and assuming the predicted runoff source areas reasonably reflect the actual hydrology, it seems reasonable to assume the predicted distribution of sediment sources are accurate, if not in exact location, than in magnitude. Certainly more information and data are needed to better parameterize the model and to ensure accurate calibration. Figure 12 displays the predicted sediment distribution in the Gumera subbasin. Although it is hard to discern in Fig. 12, there is a huge variation in sediment yield, ranging from areas with essentially no erosion to areas producing significant sediment losses. Indeed, these high sediment source areas are also high runoff source areas. Clearly some areas of the basin are predicted to be comparatively larger sources of sediment than others. For instance, the Lake Tana subbasin is predicted to have some of the highest sediment yields in the basin, as high as  $200 \text{ t ha}^{-1}$  resulting from cultivation on the steep slopes, and the relatively high runoff losses that prevail in the region. The Jemma subbasin also shows high predicted sediment losses, mainly a result of the surficial geology (e.g., leptosols and vertisols overlaying a basalt formation), high agricultural activity, and steep slopes. A third area that has relatively high sediment yield is located in the Upper Didessa subbasin (where Angar is located) where there are some of the highest rainfall and

**Table 4.** Model fit statistics (coefficient of determination,  $r^2$  and Nash-Sutcliffe Efficiency, NSE), and sediment export for the Anjeni, Ribb, and Border (El Diem) Subbasins during the rainy season.

Subbasin	$r^2$	NSE	Measured Sediment Export	Modeled Sediment Export	Modeled Sediment Export
			ton d <sup>-1</sup>		ton km <sup>2</sup> d <sup>-1</sup>
Anjeni	0.80	0.74	239	227	201.2
Ribb*	0.74	0.71	30,657	29 456	22.7
Border (El Diem)	0.67	0.64	1 229 821	1 232 468	7.1

\* Consists of four measurements.

**Table 5.** Annual predicted sediment yield for each wetness index class (basin average) and for the pasture, crop, and forest land covers. Wetness Index one produces the lowest runoff; wetness class ten produces the most runoff.

Landcover	Wetness Index Class Sediment Yield (ton ha yr <sup>-1</sup> )									
	One	Two	Three	Four	Five	Six	Seven	Eight	Nine	Ten
Pasture	1.2	3.6	3.4	3.6	3.9	5.6	8.8	10.1	12.5	14.3
Crop	2.1	2.3	3.4	3.5	4.6	5.9	10.7	9.9	14.2	15.6
Forest	0.3	0.5	0.9	1.5	1.7	1.6	2.8	3.1	3.7	4.1

runoff levels in the basin. The Fincha region, in the southern area of the basin, was not specifically a subbasin in the model, but the area was also predicted to have high sediment yields. Conversely, sediment yields are considerably lower (on average) in subbasins along the along the main stem of the Blue Nile (Fig. 12), mainly a result of the lower slopes, and more forested areas, particularly in the north-western region. However, the model still predicts some large sources of sediment in these areas, specifically, agricultural land on steep, or saturated soils.

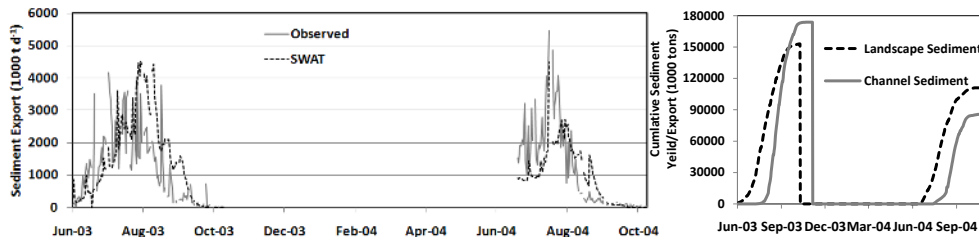
The predicted gradient in sediment yield within subbasins is illustrated in Fig. 12. Inset, where the Gumera watershed in the Lake Tana subbasin is shown. The model predicts only a relatively small portion of the watershed to contribute the bulk of the sediment (75% of the sediment yield originates from 10% of the area, while much of the area contributes low sediment yield. The high sediment yield areas are generally predicted to occur at the bottom of steep agricultural slopes, where subsurface flow accumulates, and the stability of the slope is reduced from tillage and or excessive livestock traffic. Note also that these are the areas that gully formation is likely (Tebebu, 2009; Tebebu et al., 2010).

## 5 Discussion

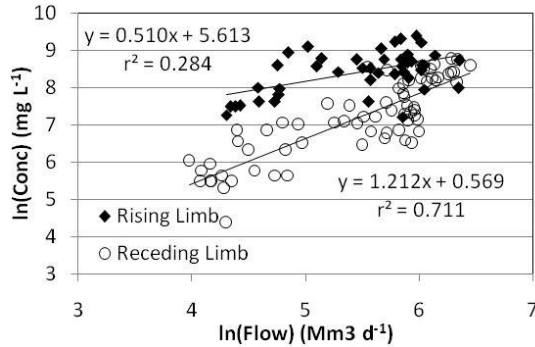
Flows in the Blue Nile Basin in Ethiopia show large variability across scales and locations. Sediment and water yields from areas of the basin range more than an order of magnitude. Smaller basins showed both higher runoff and sediment losses per unit area. Furthermore, even within smaller watersheds such as the Anjeni micro-catchment there are ar-

reas that produce virtually no runoff or erosion, and areas that produce very high levels of both runoff and erosion. Much of the erosion in the Anjeni catchment was generated from a large gully in the low-lying area (Ashagre, 2009). While the SWAT model cannot predict the formation of gullies, the SWAT-WB model can indicate where the formation of gullies is probable. In most cases gullies form where the soil is saturated either from a large contributing area for water to accumulate or where slopes flatten and the effective hydraulic conductivity is reduced (Tebebu et al., 2010). These areas tend to occur at the bottom of long slopes in the wetter valley bottom areas, which, not surprisingly also support intensive animal agriculture. Indeed, Table 5 shows these areas (higher wetness index classes, or areas with higher  $\lambda$  values) to produce substantially higher sediment yields than other areas, inevitable, since these areas produce higher runoff losses as well. This seems to agree with what has been observed in the basin (e.g., Tebebu, 2009), and points towards the need to develop management strategies that incorporate landscape position into the decision making process. Interestingly, both pasture and crop land in the higher wetness classes had approximately equivalent sediment losses, while forest in these same areas had substantially lower erosive losses, likely due to the more consistent ground cover and better root system.

The use of the modified SWAT-WB model that more correctly predicts the spatial location of runoff source areas is a critical step in improving the ability to manage landscapes, such as the Blue Nile, to provide clean water supplies, enhance agricultural productivity, and reduce the loss of valuable top soil. Obviously, the erosion routines (USLE, RUSLE, MUSLE, sediment rating curves) in many of the



**Fig. 9.** Observed and SWAT modeled sediment export at the Sudan/Ethiopia border (a) and the predicted landscape sediment yield and channel sediment export (b).



**Fig. 10.** Natural log of the sediment concentration vs natural log of the flow at El Diem gauge for the rising and receding limb of the discharge hydrograph.

large scale watershed models are crude, at best, and do not incorporate the appropriate mechanistic processes to reliably predict when and where erosion occurs, at least at the scale needed to manage complex landscapes. For instance, the MULSE routine in SWAT does not predict gully erosion, which is a large component of the sediment budget in the Blue Nile. To correctly capture the integrated watershed wide export of sediment the original SWAT predicts erosion to occur more or less equally across the various land covers (e.g., crop land produces approximately equal erosive losses, pasture produces approximately equal erosive losses) provided they have similar soils and land management practices throughout the basin. The modified version of SWAT used here recognizes that different areas of a basin (or landscape) produce differing runoff losses and thus differing sediment losses (Table 5). However, all crop or pasture with in a wetness index class in the modified SWAT produces the same erosive losses, and is rill or sheet erosion (as predict by MUSLE), not gully erosion. Thus, rill and sheet erosion are likely over predicted to obtain the correct sediment export from the basin.

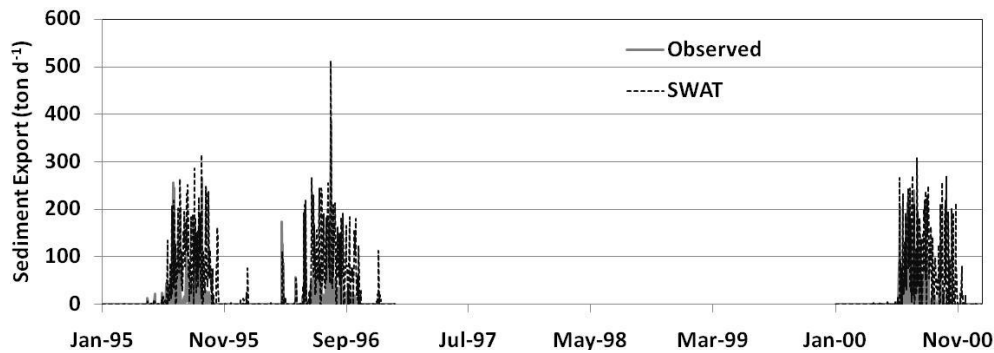
It is interesting to note that the model can predict that the sediment load peaks before the flow, and that it predicts the cause to be the result of relating the sediment concentration to the time when the watershed becomes covered by vegetation. The model indicates that later in the rainy season on

the receding limb of the sediment hydrograph, sediment export is dominated by channel processes. However, as noted earlier, gully erosion is also a large sediment source later in the season, as interflow causes the soil to saturate and increases the hydrostatic pressure in the gully (e.g., a water table forms above the gully bottom) (Tebebu et al., 2010). Based on watershed outflow measurements, we cannot discriminate between these mechanisms since both signals appear at the same time. However, the gully explanation seems to be reasonable since during the rainy season high sediment concentrations are observed in the basin and relatively sediment free water is observed after the surface runoff has ended, and interflow continues.

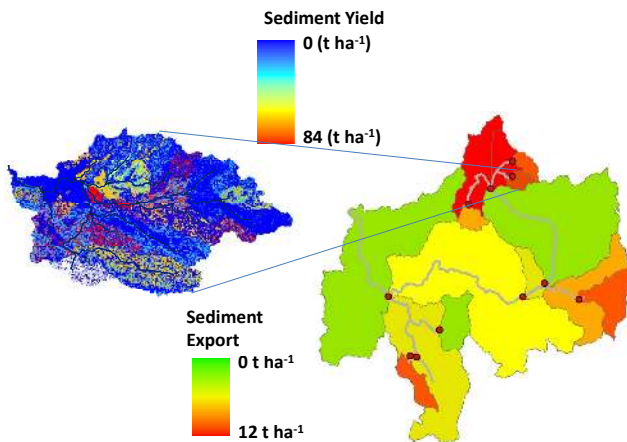
The next logical work with these basin scale models should explore incorporating more realistic processes controlling erosion. Models such as the Water Erosion Prediction Project (WEPP) model incorporate mechanistic process based erosion modeling capabilities, but are applicable only to the hillslope or small watershed scale. There is an additional need to increase the parsimony of the basin scale models. The modification made to SWAT (SWAT-WB) provides a good first step towards more correctly capturing distributed hydrologic responses while significantly reducing calibration needs. This provides a useful platform on which to base sediment predictions, but still does not overcome the inherent weakness of empirical erosion routines such as those used in SWAT. Models that utilize USLE and its derivatives often require (excessive) calibration, and there exist very few data sets that can reliably provide both the integrated and distributed data to calibrate against. Translating these capabilities to basin scale models will be challenging, but are critical to the future of land and water resource management, particularly in regions where there is little measured data to calibrate these models to.

## 6 Conclusions

A modified version of the SWAT model appropriate for monsoonal climates is presented as a tool to quantify the hydrologic and sediment fluxes in the Blue Nile Basin, Ethiopia. The model requires very little direct calibration to obtain good hydrologic predictions. All parameters needed to



**Fig. 11.** Measured and SWAT predicted sediment export from the Anjeni micro-watershed.



**Fig. 12.** Sediment export ( $\text{t ha}^{-1} \text{ yr}^{-1}$ ) in the subbasins predicted by the model (main figure) and sediment yield by hydrologic response unit (HRU) for the Gumera subbasins (inset).

initialize the model to predict runoff are obtained from base-flow separation of the hydrograph ( $\Pi_B$ ), and from topographical information derived from a DEM and soils data ( $\lambda$ ). The reduced parameterization/calibration effort is valuable in environments such as Ethiopia where there are limited data to build and test complicated biogeochemical models.

Using the model we were able to quantify the relative contributions from the various areas of the BNB with relatively good accuracy, particularly at a daily time step. The analysis showed that not all subbasins contribute flow or runoff equally. In fact there is large variation in average flow and runoff across the watershed. Additionally, within any one watershed the model indicates that there are areas that produce significantly more runoff and areas that produce almost no runoff, which, of course has implications for the management of these areas. This model is helpful to identify areas of a basin that are susceptible to erosive or other contaminant losses, due to high runoff production. These areas should be targeted for management intervention to improve water quality.

An analysis of sedimentation and erosion in the Blue Nile Basin was conducted to determine the relative sources of sediment. The model showed good fit to observed sediment load at the El Diem station. The model predicted several areas of the watershed to be relatively large sediment contributors, however, more work should be done to corroborate the subbasin and intra-watershed predicted sediment yields. The processes governing the erosion and sedimentation dynamics are not fully understood in the Blue Nile, thus the sediment predictions should be considered tentative until more testing is done.

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