NASA - 7M- 84267

COPY

TIRDARY

<u>1987 - 1987</u>

LINCLEY RESEARCH DENTER LICRARY, NASA HUMPION, VIRGINIA

NASA Technical Memorandum 84267

NASA-TM-84267 19820023768

A New Numerical Method for the Simulation of Three-Dimensional Flow in a Pipe

A. Leonard and A. Wray

July 1982



11日本の「日本の「日本の」」、「日本の日本の日本の「日本の」

ENTER:

3 1 1 RN/NASA-TM-84267 DISPLAY 03/6/1

82N31644*# ISSUE 22 PAGE 3131 CATEGORY 34 RPT#: NASA-TM-84267 A-8980 NAS 1.15:84267 82/07/00 11 PAGES UNCLASSIFIED DOCUMENT

UTTL: A new numerical method for the simulation of three dimensional flow in a pipe

AUTH: A/LEONARD, A.; B/WRAY, A.

CORP: National Aeronautics and Space Administration. Ames Research Center, Moffett Field, Calif. AVAIL.NTIS SAP: HC A02/MF A01 MAJS: /*COMPUTERIZED SIMULATION/*PIPE FLOW/*THREE DIMENSIONAL FLOW MINS: / ACCURACY/ FOURIER SERIES/ GEOMETRY/ HYPERGEOMETRIC FUNCTIONS/ INCOMPRESSIBLE FLOW/ UNSTEADY FLOW/ VELOCITY DISTRIBUTION

ABA: R.J.F.

.

A New Numerical Method for the Simulation of Three-Dimensional Flow in a Pipe

A. Leonard A. Wray, Ames Research Center, Moffett Field, California



Ames Research Center Moffett Field. California 94035

N82 - 316414#

. • . • .

A NEW NUMERICAL METHOD FOR THE SIMULATION OF THREE-DIMENSIONAL

FLOW IN A PIPE

A. Leonard and A. Wray

NASA Ames Research Center Moffett Field, CA 94035 U.S.A.

INTRODUCTION

In the last few years, major advances have been made in the numerical simulation of wall-bounded transitional and turbulent shear flows. So far, most of the emphasis has been on flows with planar boundaries. Transitional flows in a flatplate boundary layer (ref. 1) and in a channel (ref. 2), as well as turbulent channel flow (ref. 3), have been investigated without modeling the near-wall region; Moin (ref. 4) gives a critique of these investigations. Except for the study of Patera and Orszag (ref. 5) of axisymmetric pipe flow and the simulation of turbulent flow in annuli by Schumann (ref. 6), using modeled boundary conditions, very little work has been reported on nonplanar flows.

In this paper we present a new numerical technique for simulating threedimensional, unsteady, incompressible pipe flows and demonstrate its utility and accuracy. Each vector function in the expansion of the velocity field is divergencefree and satisfies the boundary conditions for viscous flow. Some of the benefits of the expansion technique are as follows: (1) pressure is eliminated from the dynamics, (2) only two unknowns per "mesh point" are required, (3) it provides implicit treatment of the viscous terms at no extra computational cost, and (4) no fractional time-steps are required.

In addition, the method uses spectral expansions: Fourier series in the azimuthal (θ) and streamwise (x) directions and global polynomials in the radial (r) direction. Thus, for smooth velocity fields, we expect rapid convergence of our expansions, independent of boundary constraints, as long as the radial polynomials are eigenfunctions of a singular Sturm-Liouville problem (ref. 7). In general, Chebychev or Legendre polynomials are good candidates, but we show that for cylindrical geometry a certain choice of the Jacobi polynomials is particularly advantageous in minimizing the coupling of the resulting equations for the expansion coefficients while satisfying the analytical behavior of the flow variables near r = 0. As discussed below, the method has been tested on the linear stability problem for Poiseuille flow.

The governing equations are the incompressible Navier-Stokes equations for the velocity u and the disturbance pressure p,

$$\frac{\partial \mathbf{u}}{\partial t} + \underline{\omega} \times \underline{\mathbf{u}} = -\nabla(\mathbf{p} + \frac{1}{2}\mathbf{u}^2) - \frac{d\mathbf{P}}{d\mathbf{x}}\hat{\mathbf{e}}_{\mathbf{x}} + \frac{1}{Re}\nabla^2\underline{\mathbf{u}}$$
(1)

$$\nabla \cdot \underline{\mathbf{u}} = \mathbf{0} \quad . \tag{2}$$

Here $\underline{\omega} = \nabla x \underline{u}$ is the vorticity, Re is the Reynolds number, $\frac{dP}{dx}$ is the constant mean pressure gradient, and the density $\rho = 1$ everywhere. The boundary condition at the pipe wall (r = 1) is $\underline{u}|_{r=1} = 0$. We assume periodic boundary conditions in the x direction with period L.

We proceed formally by defining the projection operator \mathscr{P} which projects an arbitrary vector field into the space of divergence-free fields satisfying tangency at the boundary; that is, if $\underline{\Omega}$ is an arbitrary vector field, then we have the unique decomposition,

$$\Omega = \psi + \nabla \varphi \tag{3}$$

where ψ satisfies

$$\nabla \cdot \underline{\psi} = 0$$
, $\underline{\psi} \cdot \underline{n} = 0$ (4)
boundary

and \mathscr{P} is the operator that accomplishes this decomposition,

$$\mathscr{P}\underline{\Omega} = \underline{\Psi} \tag{5}$$

By applying this operator to the momentum equation, we obtain the time-evolution of the divergence-free velocity field as (ref. 8)

$$\frac{\partial \underline{\mathbf{u}}}{\partial t} + \frac{1}{Re} \, \boldsymbol{\mathscr{P}}(\nabla \mathbf{x} \, \nabla \mathbf{x} \, \underline{\mathbf{u}}) = -\boldsymbol{\mathscr{P}}(\underline{\boldsymbol{\omega}} \mathbf{x} \, \underline{\mathbf{u}}) - \frac{dP}{dx} \, \hat{\mathbf{e}}_{\mathbf{x}}$$
(6)

Our overall strategy is to expand \underline{u} in terms of divergence-free vector functions satisfying the viscous boundary conditions and periodicity in x and θ . We then substitute this expansion into equation (1) and apply a weighted residual method which mimics the application of the projection operator to obtain evolution equations for the expansion coefficients.

We write the velocity field <u>u</u> as the expansion

$$\underline{u}(\mathbf{r},\theta,\mathbf{x},t) = \sum_{n,k,l} a_{n,k,l}^{(t)} \underbrace{\chi}_{n}(\mathbf{r}) \exp(i\mathbf{k}\mathbf{x} + il\theta)$$
(7)

where each expansion vector satisfies

$$\nabla \cdot \left[\underline{\chi}_{n}(\mathbf{r}) \exp(i\mathbf{k}\mathbf{x} + i\boldsymbol{\ell}\boldsymbol{\theta}) \right] = 0$$
(8)

and

$$\underline{\chi}_{n}(1) = 0 \tag{9}$$

We derive a system of ordinary differential equations (ODE's) for the coefficients $a_{n,k,l}$ by substituting the above expansion into the momentum equation and taking the inner product of the result with a set of weight vectors which are divergence-free,

$$\nabla \cdot \left[\underline{\xi}_{m}(\mathbf{r}) \exp(-i\mathbf{k}\mathbf{x} - i\mathbf{l}\theta) \right] = 0$$
 (10)

and satisfy the inviscid boundary condition,

$$\underline{\xi}_{\mathrm{m}}(1) \cdot \hat{\mathrm{e}}_{\mathrm{r}} = 0 \tag{11}$$

[The (k, ℓ) dependence of χ_n and ξ_m is suppressed.] This weighted residual method mimics the application of the projection operator. For example if $\zeta = \xi_m(r) \exp(-ikx - i\ell\theta)$ then

$$\int_{\mathbf{V}} \underline{\zeta} \cdot \nabla \varphi \, \mathrm{dV} = -\int_{\mathbf{V}} (\nabla \cdot \underline{\zeta}) \varphi \, \mathrm{dV} + \int_{\mathbf{S}} \varphi (\underline{\zeta} \cdot \underline{\mathbf{n}}) \, \mathrm{dS}$$
(12)

= 0

for an arbitrary scalar field φ with periodic boundary conditions in x.

The result for each wave vector (k,l) is a system of ODE's

$$A\underline{\dot{a}} + \frac{1}{Re} B\underline{a} = \underline{f}$$
(13)

where

$$A_{mn} = \int_{0}^{1} \frac{\xi_{m}}{\xi_{m}} \cdot \chi_{n} r dr$$
(14a)

$$B_{mn} = \int_{0}^{1} \underline{\xi}_{m} \cdot \nabla \mathbf{x} \nabla \mathbf{x} \underline{\chi}_{n} r dr$$
(14b)

$$f_{m} = -\int_{0}^{1} \xi_{m} \cdot \left[\underbrace{\omega \times u}_{m} + 2\pi L \frac{dP}{dx} \hat{e}_{x} \right] r dr \qquad (14c)$$

and where \sim denotes double-Fourier transformation in x and θ . Thus, except for the nonlinear term, the coupling of the equations occurs only through the radial modes.

The choice of radial functions in χ_n and ξ_m must be made carefully to (1) minimize the coupling between radial modes (that is, obtain a banded structure for A and B if possible); (2) allow construction of A and B with relative ease; (3) obtain efficient computation of <u>f</u>; and (4) obtain rapid convergence while satisfying the constraints imposed on χ_n and ξ_n , including the correct behavior as $r \to 0$.

We find that the sequence of expansion vectors $\{\underline{x}_{-1}, \underline{x}_{0}^{+}, \underline{x}_{0}^{-}, \dots, \underline{x}_{n}^{+}, \underline{x}_{n}^{-}, \dots\}$ defined in the following satisfies the above requirements. For $n \ge 0$ the (r, θ, x) components are

$$\underline{\chi}_{n}^{\pm} = \begin{pmatrix} \chi_{n,r}^{\pm} \\ \chi_{n,\theta}^{\pm} \\ \chi_{n,x}^{\pm} \end{pmatrix} = \begin{pmatrix} \pm i k q_{n}^{\ell \pm 1} \\ k q_{n}^{\ell \pm 1} \\ \pm \frac{1}{r} \frac{d}{dr} (r q_{n}^{\ell \pm 1}) - \frac{\ell}{r} q_{n}^{\ell \pm 1} \end{pmatrix} \quad (k \neq 0)$$
(15)

where

$$q_{n}^{\ell} = r^{|\ell|} (1 - r^{2})^{2} g_{n}^{(|\ell|)}(r^{2})$$
(16)

and $g_n^{(l)}(y)$ is the shifted Jacobi polynomial (ref. 9),

$$g_n^{(l)}(y) = P_n^{(o,l)}(2y - 1)$$
 (17)

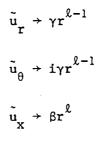
satisfying the orthogonality condition

$$\int_{0}^{1} y^{\ell} g_{m}^{(\ell)}(y) g_{n}^{(\ell)}(y) dy = C_{m}^{\ell} \delta_{m,n}$$
(18)

For the case k = 0, the above expansion vectors clearly are not complete and must be replaced by an alternative set. A convenient choice is given by $(n \ge 0)$

$$\chi_{n}^{-} = \begin{pmatrix} -\frac{i \ell q_{n}^{\ell}}{r} \\ \frac{d q_{n}^{\ell}}{dr} \\ 0 \end{pmatrix} \qquad \chi_{n}^{+} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ q_{n}^{\ell} \end{pmatrix}$$
(19)

It is a simple matter to verify that the expansion vectors defined above yield the correct behavior of $\underline{\tilde{u}}(r,k,l)$ as $r \rightarrow 0$; for example, if l > 0,



where γ and β are complex constants. The additional vector $\underline{\chi}_{-1}$ is required because $\tilde{u}_{\theta}(k \neq 0)$ and $\tilde{u}_{x}(k = 0)$ would otherwise have a double zero at the wall.

The corresponding weight vectors are essentially the curl of the $\,\chi\,'s.\,$ More specifically, if $k \neq 0$ the weight vectors may be expressed as

$$\underline{\xi}_{m}^{\pm} = \nabla \mathbf{x} \nabla \mathbf{x} \begin{pmatrix} \mp i q_{n}^{\ell \pm 1} \\ q_{n}^{\ell \pm 1} \\ q_{n}^{\ell} \end{pmatrix}$$
(20)

while the $\underline{\chi}_{n}^{\pm}$ have the form

$$\chi_{n}^{\pm} = \widetilde{\nabla x} \begin{pmatrix} -iq_{n}^{\ell \pm 1} \\ \mp q_{n}^{\ell \pm 1} \\ 0 \end{pmatrix}$$
(21)

As a result, the (+) vectors are uncoupled from the (-) vectors. The resulting matrices A and B are nonadiagonal, except for an additional nonzero row and a column owing to the vector $\underline{\chi}_{-1}$. The limited bandwidth of the viscous matrix B results from the particular choice of the polynomials $g_n^{(l)}$ given by

equation (17). In particular, the Laplacian operator in the (r,θ) plane is equivalent to a tridiagonal matrix in the following sense:

$$\nabla^{2} \left[q_{n}^{\ell}(\mathbf{r}) \exp(i\ell\theta) \right] = \left(\frac{1}{\mathbf{r}} \frac{d}{d\mathbf{r}} \mathbf{r} \frac{d}{d\mathbf{r}} - \frac{\ell^{2}}{\mathbf{r}^{2}} \right) q_{n}^{\ell}(\mathbf{r}) \exp(i\ell\theta)$$
$$= \mathbf{r}^{\ell} \left[b_{n}^{\ell} g_{n-1}^{(\ell)}(\mathbf{r}^{2}) + c_{n}^{\ell} g_{n}^{(\ell)}(\mathbf{r}^{2}) + d_{n}^{\ell} g_{n}^{(\ell)}(\mathbf{r}^{2}) \right] \exp(i\ell\theta)$$

CONVERGENCE TESTS

As a test, the method described above was applied to the problem of determining the time eigenvalues for linearized flow in a pipe. The calculations were performed on a CDC 7600 computer. We assume $u \sim \exp(\lambda t)$ and order the eigenvalues such that Real $(\lambda_1) \ge \text{Real} (\lambda_2) \ge \ldots$. The results for λ_1 with Re = 9600, $\ell = 1$, k = 1, are given in the table below, where N + 2 is the number of radial modes in the expansion.

N	<u> </u>	λ					
20	D	-0.02312	-	i	0.95050		
2	5	-0.02317074	-	i	0.95048142		
3	D	-0.023170795769	-	i	0.950481396659		
3	5	-0.023170795764	-	i	0.950481396668		

Note that the convergence is exponential in N or some power of N, typical of spectral methods (ref. 7), and that there is no indication of significant round-off errors. The results agree with that of Salwen et al. (ref. 10), who obtained $\lambda_1 = 0.02317 - i(0.95048)$, using an expansion in Stokes' eigenfunctions to solve the linear stability problem.

In figure 1 we show convergence of some of the higher eigenvalues for the case k = 1, l = 1, Re = 3000, a Reynolds number in the range where a number of interesting transitional phenomena have been observed experimentally. Note that a large number of eigenvalues are predicted accurately for 30 to 35 radial expansion functions. In figure 2, the amplitudes of the coefficients of χ_n for the eigenvalue λ_1 are shown as a function of n for four Reynolds numbers with k = 1 and l = 1. Each of the χ_n are normalized so that

$$\int_{0}^{1} \left|\underline{\chi}_{n}\right|^{2} r dr = 1$$

and the radial expansion N = 35 (37 expansion functions) was used for all cases. Again, the coefficients approach zero exponentially in some power of n.

SUMMARY

A new numerical method has been developed to investigate three-dimensional, unsteady ripe flows using a new velocity-vector expansion method. Each vector function in the expansion set is divergence-free and satisfies the boundary conditions for viscous flow. Other features of the general technique are as follows: (1) pressure is eliminated from the dynamics; (2) only two unknowns per "mesh point" are required; (3) there is rapid convergence of spectral methods; (4) there is implicit treatment of the viscous term at no extra computational cost; and (5) no fractional time-steps are required. In the present application of the method to flow in a pipe, the behavior of each flow variable near the computational singular point is treated rigorously and expansions in Jacobi polynomials have been shown to be particularly advantageous. The method has been tested on the linear stability problem for Poiseuille flow and has demonstrated rapid convergence of the eigenvalues and eigenfunctions as the number of radial modes is increased.

ACKNOWLDEGMENT

The authors wish to thank Dr. Parviz Moin and Mr. Robert Moser for many helpful discussions.

REFERENCES

- 1. Wray, A., and Hussaini, Y.: Numerical Experiments in Boundary Layer Stability, AIAA Paper 80-0275, Pasadena, Calif., 1980.
- 2. Orszag, S. A., and Kells, L. C.: Transition to Turbulence in Plane Poiseuille and Plane Couette Flow, J. Fluid Mech., Vol. 96, 1980, p. 159.
- Moin, P., and Kim, J.: Numerical Investigation of Turbulent Channel Flow, J. Fluid Mech., Vol. 118, 1982, p. 341.
- Moin, P.: Numerical Simulation of Wall-Bounded Turbulent Shear Flows, <u>Proceed-ings 8th International Conference on Numerical Methods in Fluid Dynamics</u> (this issue).
- 5. Patera, A. T., and Orszag, S. A.: Finite-Amplitude Stability of Axisymmetric Pipe Flow, J. Fluid Mech., Vol. 112, 1981, p. 467.
- Schumann, U.: Subgrid Scale Model for Finite Difference Simulations of Turbulent Flows in Plane Channels and Annuli, J. Comp. Phys., Vol. 18, 1975, p. 376.

- 7. Orszag, S. A.: Spectral Methods for Problems in Complex Geometries, J. Comp. Phys., Vol. 37, 1980, p. 70.
- 8. Chorin, A. J., and Marsden, J. E.: <u>A Mathematical Introduction to Fluid</u> <u>Mechanics</u>. Springer-Verlag, New York, 1979.
- 9. <u>Handbook of Mathematical Functions</u>. M. Abramowitz and I. A. Stegun, eds., NBS AMS 55, Sec. 22, 1968.
- 10. Salwen, H., Cotton, F. W., and Grosch, C. E.: Linear Stability of Poiseuille Flow in a Circular Pipe, <u>J. Fluid Mech.</u>, Vol. 98, 1980, p. 273.

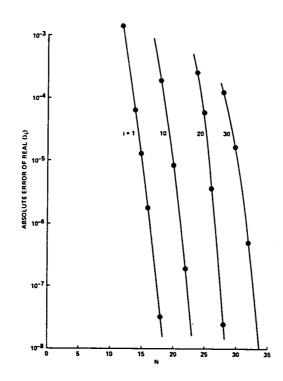


Fig. 1. Convergence of Real (λ_i) ; k = ℓ = 1, Re = 3000.

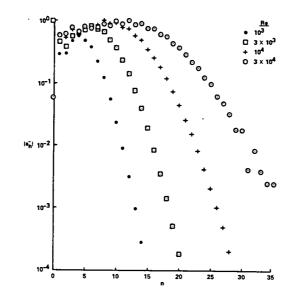


Fig. 2. Amplitudes of the expansion coefficients for the eigenvector corresponding to λ_1 ; $k = \ell = 1$.

1. Report No.	2. Government Acce	ssion No.	3. Recipient's Catalo	g No.						
4. Title and Subtitle			5. Report Date	··· ·· =······						
A New Numerical Method f	or the Simula	tion of								
Three-Dimensional Flow i			the second s							
Infee-Dimensional Flow I	n a ripe		6. Performing Organi	ization Code						
7. Author(s)			8. Performing Organi	zation Report No.						
A. Leonard and A. Wray			A 8980							
j			10. Work Unit No.							
9. Performing Organization Name and Address										
NASA Ames Research Cente	r	<u>T 9517</u>								
Moffett Field, Californi	-	11. Contract or Grant No.								
Morrect Field, Carlornia	a 94035									
		ŀ	13. Type of Report a	nd Period Covered						
12. Sponsoring Agency Name and Address										
National Aeronautics and	Space Admini	stration		Memorandum						
Washington, DC 20546	•		14. Sponsoring Agence							
,		505-31-91-01								
15. Supplementary Notes		<u> </u>		······································						
Point of contact: Anthon	ny Leonard, A	mes Research Ce	nter MS 202	Δ_1						
				,						
Moffett Field, California 94035 (415) 965-6459 FTS: 448-6459										
16. Abstract			· · · · · · · · · ·							
A new numerical tec	hnique for ci	mulating throa-	dimonsionsl	unatoolu						
A new numerical Lec	anique ioi si		dimensional,	unsteady,						
incompressible pipe flow										
shown. Each vector func										
divergence-free and sati	divergence-free and satisfies the boundary conditions for viscous flow.									
Some of the benefits of	Some of the benefits of the expansion technique are as follows: (1)									
pressure is eliminated f	rom the dynam	1 only t	wo unknowns	ner "mesh						
pressure is eliminated from the dynamics, (2) only two unknowns per "mesh										
point" are required, (3) it provides implicit treatment of the viscous terms at no extra computational cost, and (4) no fractional time-steps										
are required. The metho										
azimuthal (θ) and stream	wise (x) dire	ctions and Jaco	bi polynomin	als in the						
radial (r) direction.										
17. Key Words (Suggested by Author(s))		18. Distribution Statement								
Numerical Simulation, Tu	bulence.	i io. Distribution statement	L							
Transition, Pipe Flow, C	•									
Geometry, Incompressible		Unlimited								
Method										
Method		Subject Category 34								
19. Security Classif. (of this report)	20. Security Classif. (c	of this page)	21. No. of Pages	22, Price*						
19. Security Classif. (of this report) Uncl	20. Security Classif. (c Uncl		21. No. of Pages 10	22. Price* AO2						

.

*For sale by the National Technical Information Service, Springfield, Virginia 22161

.

.

; • • .

: 1 -•

•