

## A Novel Method to Estimate the Maximum Power for a Photovoltaic Inverter System

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**Abstract**—This paper describes a novel method to approximate the maximum power for a photovoltaic inverter system for solar distributed generation. It is designed for power systems applications and utilities. The proposed method takes in consideration the interaction between solar panels, photovoltaic inverter, Maximum Power Point Tracking (MPPT) control, solar panel dc side dynamic model and the effective intensity of light over the solar panel. The new method has the advantage to provide a new simple way to approximate the optimal voltage or rated voltage ( $V_{op}$ ), the optimal or rated current ( $I_{op}$ ) and maximum power rating ( $P_{max}$ ) produced by a solar panel and the photovoltaic inverter. Furthermore, this straightforward method will be named Linear Reoriented Coordinates Method (LRCM) with the advantage that  $P_{max}$  and  $V_{op}$  can be approximated using the same variables as the dynamic model without using complicate approximations or Taylor series. Finally, some simulations results are presented.

**Keywords**— Photovoltaic power systems, solar energy, solar power generation

### I. INTRODUCTION

The use of renewable and green energies (i.e. solar energy, wind energy, geothermic energy, etc.) is growing in many countries and the contribution to reduce the global warming and protection of the environment is increasingly important. Since the last thirty years the interest to use the solar energy in applications of power distribution are growing very fast. Applications for the solar energy are in urban areas, electric drives, satellites, etc. Today, solar energy is considered as a real alternative resource of energy to be used for production of electrical energy.

To convert solar energy into electrical energy, it is required the basic components such that solar panels, inverters, control (i.e. Maximum Point Power Tracking) and sensors, to produce electric energy. The PV arrays are linked in series to achieve the sufficient dc voltage for generating an ac output voltage at the inverter. Unfortunately, the dynamic models used to describe, the interaction of solar panels, control and PV inverter are too complicated, with a lot of required parameters and the models cannot produce a symbolic solution to obtain the optimal voltage and maximum power produced by the PV inverter giving the necessity to use long and tedious iterations. Also, these models are not very practical for

straightforward power flow analysis. To solve this problem, this paper proposes a novel mathematical dynamic model for utility applications, using the dc side dynamic equations for a solar panel and the linear reoriented coordinates method.

This dynamic model has the advantage to take in consideration the behavior of the solar panels for different intensities of light and initial conditions of the current. It describes the power and current produced by PV inverter, the operations of the MPPT with the interaction of the inverter and the effects of the intensity of light. Also, an approximate symbolic solution is given to determine the optimal voltage of operation and the maximum power using MPPT. The method to approximate the optimal voltage ( $V_{op}$ ) and maximum power ( $P_{max}$ ) is named Linear Reoriented Coordinates Method (LRCM). The LRCM is a simple method which it uses the same variables as the proposed dynamic model and it is a time saver to calculate  $V_{op}$  and  $P_{max}$  reducing the long and tedious iterations. In addition, the simulated results will show that the proposed technique is very effective giving a small error between the real values and estimated values, inclusive if the effective intensity of light is changing over the solar panel.

### II. DC SIDE DYNAMIC EQUATIONS FOR A PV INVERTER SYSTEM

A PV Inverter System is a series connection of solar panels or photovoltaic modules with a dc-ac power electronics inverter circuit, and novel generation control circuit, (MPPT) control [5] to generate ac voltage from a solar source. The MPPT can compensate for the reduction in output power caused by the shadow covering the photovoltaic modules [3]. Also, the MPPT controls the inverter to produce the maximum power and the ac power to be connected to the load or utility grid. Fig. 1 shows a PV inverter system with the three principal stages of operation.

The proposed I-V characteristic model equation (1) takes into consideration the percentage of effective intensity of the light over the solar panels, the characteristic constant for the I-V curves, a shading linear factor, the short-circuit current rating and the open-circuit voltage for each panel [1]. Now to obtain the dynamic equation of the current with respect to the voltage, lets differentiate (1) with respect to the voltage

will produce the dynamic model equation for the current (2) with respect to the voltage.

$$I(V) = \alpha \times I_{max} - \alpha \times I_{max} \times \exp\left(\frac{V}{b \times (\gamma \times \alpha + 1 - \gamma) \times V_{max}} - \frac{1}{b}\right) \quad (1)$$

$$\frac{dI(V)}{dV} = \frac{I(V) - \alpha \times I_{max}}{b \times (\gamma \times \alpha + 1 - \gamma) \times V_{max}} \quad (2)$$

(1) is multiplied by V to obtain the P-V characteristic equation as shown in (3). Now, (3) is differentiated with respect to the voltage giving (4). The dynamic equation of the Power with respect to the voltage is obtained (4). Fig. 2 shows the I-V and P-V characteristic curves for different percentages of effective intensities of light over the solar panels. If we want the dynamic equations for P(V) and I(V) in time, we just need to multiply the equations (2) and (4) by dV/dt.

$$P = V \times I(V) = \alpha \times V \times I_{max} - \alpha \times V \times I_{max} \times \exp\left(\frac{V}{b \times (\gamma \times \alpha + 1 - \gamma) \times V_{max}} - \frac{1}{b}\right) \quad (3)$$

$$\frac{dP}{dV} = i + \frac{P \times (1 - \alpha \times I_{max}/i)}{b \times (\gamma \times \alpha + 1 - \gamma) \times V_{max}} \quad (4)$$

The meaning for the variable, P is the PV inverter total output power. V is the voltage of operation for the PV inverter system. I(V) is the PV inverter total output current. I(0) is the short circuit current rating and V<sub>max</sub> is the open-circuit voltage rating of the solar panels array, for an effective intensity of light of 100 over the solar panels. I<sub>max</sub> depends on I(0), their relationship is in (5). I<sub>max</sub> is obtained by solving (1), when V = 0 using the experimental I-V characteristic curve (100 ) as illustrated in Fig. 3. (5) shows the relationship between I<sub>max</sub> and the short-circuit current for the solar panel.

The experimental I-V characteristic curve is used to calculate α, b, γ, V<sub>min</sub> and V<sub>max</sub> as shown in Fig. 3. α is the percentage/100 of effective intensity of the light over the solar panels (i.e. 100 of intensity if light over the solar panels is α = 1). b is the exponential I-V characteristic constant. The characteristic constant, b, is calculated from the (6). The voltage (V<sub>b</sub>) is approximated, when the current is 0.6321 I(0) using the experimental I-V characteristic curve (100 ) as illustrated in Fig. 3. γ is the shading linear factor depending of V<sub>max</sub>. The shading linear factor for V<sub>max</sub>, γ, is defined as the percent of voltage (V<sub>max</sub>) loss from a maximum intensity of light to a minimum intensity of light as indicated in (7). V<sub>min</sub> is the open-circuit voltage rating of the solar panels array for an effective intensity of light less than 20 over the solar panels.

From Fig. 2, it can be observed that at any particular intensity of light, there is a unique point for the maximum power; this value is named the MPP. The MPP is calculated

exactly by differentiating (3) and solving for the optimal voltage (V<sub>op</sub>), as indicated in (8). Unfortunately, it is not possible to find a symbolic solution hence the only way to solve (8) is numerically and this solution requires long and tedious iterations, making the solution not practical.

$$I_{max} = \frac{I(0)}{\alpha - \alpha \times \exp\left(\frac{-1}{b}\right)} \quad (5)$$

$$b = 1 - V_b / ((\gamma \times \alpha + 1 - \gamma) \times V_{max}) \quad (6)$$

$$\gamma = 1 - V_{min} / V_{max} \quad (7)$$

$$\alpha \times I_{max} + \exp\left(\frac{V_{op}}{b \times (\gamma \times \alpha + 1 - \gamma) \times V_{max}} - \frac{1}{b}\right) \times \left(-\alpha \times I_{max} - \frac{\alpha \times V_{op} \times I_{max}}{b \times (\gamma \times \alpha + 1 - \gamma) \times V_{max}}\right) = 0 \quad (8)$$

A novel method called Linear Reoriented Coordinates Method (LRCM) is proposed in the paper, to solve (8) and then to find an approximate symbolic solution for the Pmax calculated by the MPP.

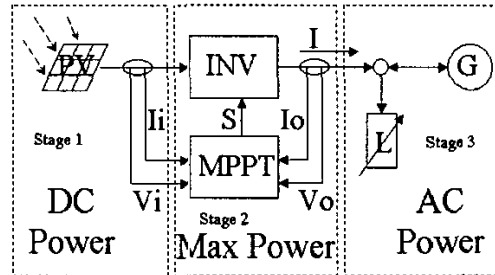


Fig. 1. PV Inverter System for utility applications

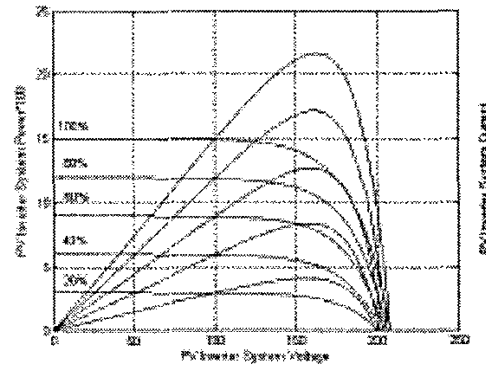


Fig. 2. P-V and I-V Characteristics for different intensities of light

### III. LINEAR RE ORIENTED COORDINATES METHOD

The main idea for the LRCM is to find the I-V curve knee point, sees Fig. 4. The I-V curve knee point is the optimal current ( $I_{op}$ ) and the optimal voltage ( $V_{op}$ ) that produces  $P_{max}$ . Using the I-V Curve, see Fig. 4, a linear current equation can be determined from the initial and final values, (9). The slope of the I-V Curve at the knee point is approximated by the slope of the linear current equation, (10). From this approximation, we will approximate  $V_{op}$  with  $V_{ap}$ . The current equation, (1) and the linear current equation, (9) are differentiated ((11) and (12)) and set equal to each other to solve for V then the solution is  $V_{ap}$ . The equations of  $V_{ap}$  are given in (14) and (15).  $V_{ap}$  is substituted in (1) to obtain  $I_{ap}$ .

$$IL(V) = \alpha \times I(0) \times (1 - V/V_{max}) \quad (9)$$

$$\frac{dIL(V)}{dV} \equiv \frac{dI(V)}{dV} \quad (10)$$

$$\frac{dI}{dV} = \left( -\frac{\alpha \times I_{max}}{b \times (\gamma \times \alpha + 1 - \gamma) \times V_{max}} \right) \times \exp\left( \frac{V}{b \times (\gamma \times \alpha + 1 - \gamma) \times V_{max}} - \frac{1}{b} \right) \quad (11)$$

$$\frac{dIL}{dV} = \frac{-\alpha \times I(0)}{V_{max}} \quad (12)$$

$$V_{ap} = b \times (\gamma \times \alpha + 1 - \gamma) \times V_{max} \times \left( \frac{1}{b} + \ln\left( \frac{(\gamma \times \alpha + 1 - \gamma) \times b \times I(0)}{\alpha \times I_{max}} \right) \right) \quad (13)$$

After substituting (5) into (13), a simplified  $V_{ap}$  is given by (15).

$$V_{ap} = (\gamma \times \alpha + 1 - \gamma) \times V_{max} + b \times (\gamma \times \alpha + 1 - \gamma) \times V_{max} \times \ln\left[ b \times (\gamma \times \alpha + 1 - \gamma) \times \left( 1 - \exp\left( \frac{-1}{b} \right) \right) \right] \quad (14)$$

Now, lets substitute (15) into (1) to obtain  $I_{ap}$ .

$$I_{ap} = \alpha \times I_{max} \times \left[ 1 - b \times (\gamma \times \alpha + 1 - \gamma) \times \left( 1 - \exp\left( \frac{-1}{b} \right) \right) \right] \quad (15)$$

$$P_{max} = V_{op} \times I_{op} \equiv V_{ap} \times I_{ap} \quad (16)$$

An approximated  $P_{max}$ , (16) is given by the multiplication of (14) and (15). Finally, if  $V_{ap}$  solves (8) hence we found the exact solutions for  $P_{max}$ ,  $I_{op}$  and  $V_{op}$ . To prove how good it is the range of our approximation for  $P_{max}$ , lets use Fig. 4 to do a geometric analysis and lets define some physical constraints for the different constants. As a note, for the value  $b = 0$ , is for an ideal solar panels array without losses, (22).

$$P \in A \text{ where } A \text{ is } \{P \in \mathbb{R} \ 0 \leq P \leq P_{max}\} \quad (17)$$

$$V \in B \text{ where } B \text{ is } \{V \in \mathbb{R} \ 0 \leq V \leq V_{max}\} \quad (18)$$

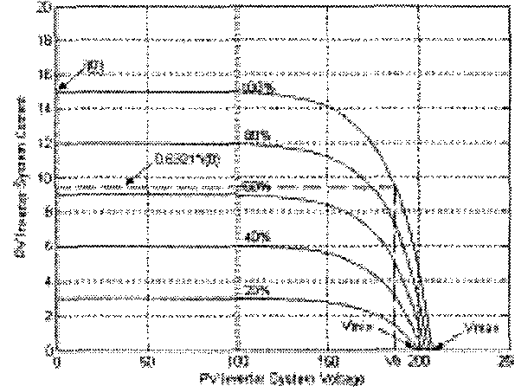


Fig. 3. Experimental I-V Characteristics

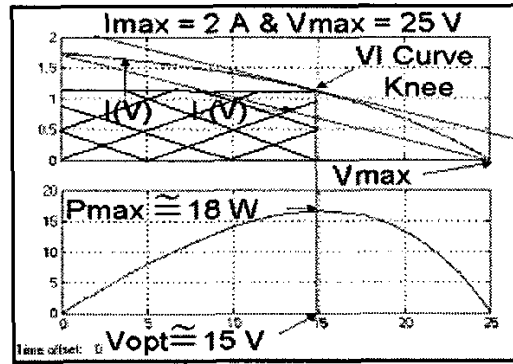


Fig. 4. P-V and I-V Curves with LRCM

$$I \in C \text{ where } C \text{ is } \{I \in \mathbb{R} \ 0 \leq I \leq I(0)\} \quad (19)$$

$$\alpha \in D \text{ where } D \text{ is } \{\alpha \in \mathbb{R} \ 0 < \alpha\} \quad (20)$$

$$b \in E \text{ where } E \text{ is } \{b \in \mathbb{R} \ 0 < b < 1\} \quad (21)$$

$$P_{max} = I(0) \times V_{max} \text{ if and only if } b = 0 \quad (22)$$

By geometric analysis, we can obtain the following two inequalities (23) and (24) for  $P_{max}$ , where  $P_{max}$  can be seen as the maximum rectangular area inside of the curve produced by (1). It is trivial that  $P_{max}$  is less than the total area current curve, (23). Using the fact that the P-V Characteristic Curve has a unique maximum point, we know that  $P_{max}$  is more or equal than our approximate  $P_{max}$ . To prove the last part of (24), the author did some computer simulations presented in the Fig. 5 where it can be seen that the estimated  $P_{max}$  is always more than (22) multiplied by 0.315. Now, (23) and (24) can give us the range of our approximation for  $P_{max}$ .

$$\int_0^{V_{max}} I(s) ds > I(V_{op}) \times V_{op} = P_{max} \quad (23)$$

$$P_{max} \geq I_{ap} \times V_{ap} > 0.315 \times I(0) \times V_{max} \quad (24)$$

Finally, the LRCM is a simple method where, instead of calculating the optimal voltage (rated voltage) and maximum power solutions using the power equations, the solutions are obtained using the current equation and the linear current equation to obtain  $V_{ap}$  and  $I_{ap}$ ,  $P_{max}$  is then estimated. Also, the LRCM has the advantage of giving an approximated symbolic solution for  $V_{op}$ . The LRCM can produce the same results as the old models without the use of Taylor series, continuous fraction expansion or other approximations and it is more practical for simulations and power flow analysis providing symbolic solutions. The following results will prove that the proposed technique is very effective, giving a small error between the actual values and estimated values, inclusive if the effective intensity of light is changing over the solar panels.

IV. LRCM RESULTS FOR A PV INVERTER SYSTEM WITH MPPT

The main advantage of the LRCM is that only the characteristic constants of the VI curve (i.e.  $b, \alpha, \gamma, V_{max}$ ) are required to estimate  $P_{max}$ . Also, approximate symbolic solutions for  $P_{max}, I_{op}$  and  $V_{op}$  are given when (8) has no symbolic solution to calculate  $P_{max}$ . If  $V_{ap}$  is a solution for (8) then we found the exact solution for  $P_{max}, I_{op}$  and  $V_{op}$ . Figs. 6-7 show the simulation results for a PV Inverter System with the estimated curve for  $P_{max}$  and the knee points. The parameters for the simulation results are,  $I_{max}$  is 15 A,  $V_{max}$  is 208 V,  $\gamma$  is 0.05 and  $\alpha$  is 1.

Fig. 6 shows the P-V Curve for different characteristic constants and the estimated curve for  $P_{max}$ . It is very close to  $P_{max}$ . The characteristic constant will determine the initial current and the location of the knee point. The  $P_{max}$  will be more for small characteristic constant, hence an I-V curve with  $b$  equal to 0.1 produces a bigger  $P_{max}$  than a I-V curve with  $b$  equal to 0.5. Fig. 7 shows the P-V Curve for different characteristic constants and the estimated curve for  $P_{max}$ . It is very close to  $P_{max}$ . The maximum error using the LRCM to estimate  $P_{max}$  in the normalized form was approximately to 0.3 as illustrated in Fig.8.

The power and current dynamics equations were given to describe a PV Inverter System for utility applications. The proposed P-V and I-V dynamic equations have the advantage of being simple, but at the same time powerful, describing the interaction between solar cells, a photovoltaic inverter, Maximum Power Point Tracking (MPPT) control, and the effective intensity of light over the solar cell. The LRCM has the advantage that it is guaranteed that an approximate symbolic solution will be found for exponential functions without symbolic solutions. Finally, it has been proved that the LRCM has a maximum error for the estimation of  $P_{max}$  near to 0.3 changing  $b$  to obtain different V-I characteristic curve. These results prove that the LRCM is valid for different values of  $I_{max}, V_{max}, \gamma$  and  $\alpha$ .

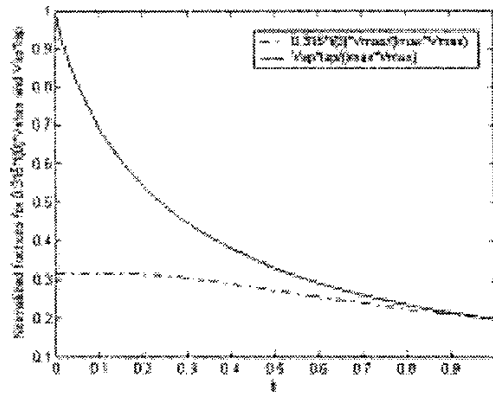


Fig. 5. Simulation to prove  $I_{ap} \times V_{ap} > 0.315 \times I(0) \times V_{max}$

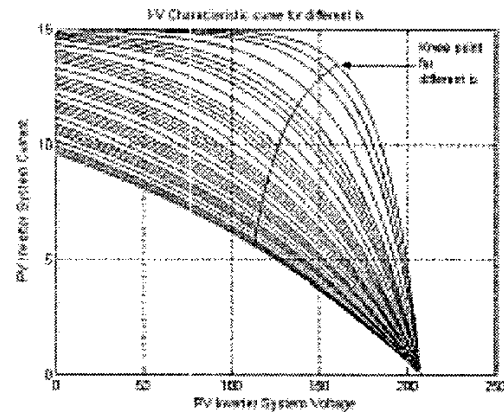


Fig. 6. I-V Curves with estimated knee points

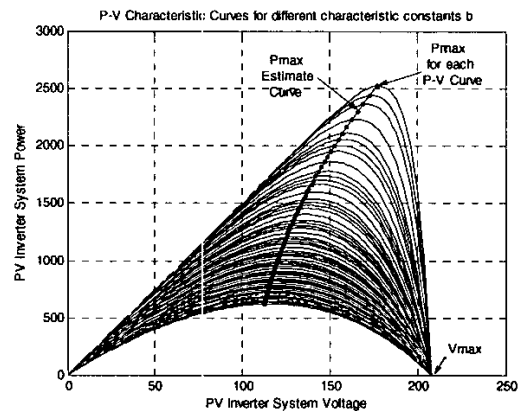


Fig. 7. P-V Curves with estimated Pmax curve

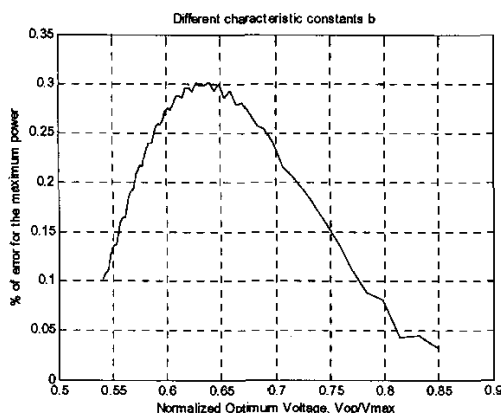


Fig. 8. Error Curve for Pmax and Pmax estimated

## V. CONCLUSIONS

A novel simple method named Linear Reoriented Coordinates Method (LRCM) is used to estimate  $P_{max}$ ,  $V_{op}$  and  $I_{op}$  for a PV Inverter System. The LRCM is very effective, to solve exponential functions without the homeomorphism property. Finally, an approximate symbolic and numerical solution is found for a Photovoltaic Inverter System.

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## REFERENCES

- [1] Ortiz-Rivera, Eduardo "Dynamic Equations for Solar Distributed Generation." *Proceedings of the Society of Hispanic Professional Engineers National Technical and Career Conference 2004*, Chicago, Illinois, January 8, 2003, Page(s): 61-65
- [2] Shengyi Liu; Dougal, R.A.; "Dynamic multiphysics model for solar array", *IEEE Transactions on Energy Conversion*, Volume: 17 Issue: 2, June 2002, Page(s): 285-294
- [3] Vaschning, V.; Hanitsch, R.; "Influence of shading on electrical parameters of solar cells", *Photovoltaic Specialists Conference, 1996.*, Conference Record of the Twenty Fifth IEEE, 13-17 May 1996, Page(s): 1287-1290
- [4] Tae-eop Kim; Ho-Gyun Ahn; Seung Kyu Park; Joun-Kyun Lee; "A novel maximum power point tracking control for photovoltaic power system under rapidly changing solar radiation", *Proceedings. ISIE 2001. IEEE International Symposium on Industrial Electronics, 2001*, Volume: 2, 12-16 June 2001, Page(s): 1011-1014
- [5] Han Hong Lim; Hamill, D.C.; "Simple maximum power point tracker for photovoltaic arrays" *Electronics Letters*, Volume: 36 Issue: 11, 25 May 2000, Page(s): 997-999
- [6] Lloyd, S.H.; Smith, G.A.; Infield, D.G.; "Design and construction of a modular electronic photovoltaic simulator" *Eighth International Conference on Power Electronics and Variable Speed Drives, 2000.* (IEE Conf. Publ. No. 475), 18-19 Sept. 2000, Page(s): 120-123
- [7] Watanabe, H.; Shimizu, T.; Kimura, G.; "A novel utility interactive photovoltaic inverter with generation control circuit", *IEC N 98. Proceedings of the 24th Annual Conference of the IEEE Industrial Electronics Society, 1998*, Volume: 2, 31 Aug.-4 Sept. 1998 Page(s): 721-725

- [8] Hussein, A.; Hirasawa, K.; Ingu Hu; Murata, S.; "The dynamic performance of photovoltaic supplied dc motor fed from DC-DC converter and controlled by neural networks." *ICNN 02. Proceedings of the 2002 International Joint Conference on Neural Networks, 2002*, Volume: 1, 12-17 May 2002, Page(s): 607-612
- [9] Wang, F.-L.; Kwan, C.-Y.; Li, T.-S.; "Dynamic modeling of rotating flexible platforms" *Proceedings of the 31st IEEE Conference on Decision and Control, 1992.*, 16-18 Dec. 1992, Page(s): 1315-1316