

## A TRANSPORT THEOREM FOR MOVING INTERFACES\*

BY

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**1. The theorem.** When studying surface effects within the framework of continuum mechanics one is often confronted with terms of the form

$$\frac{d}{dt} \int_{\mathcal{S}(t)} f(\mathbf{x}, t) da(\mathbf{x}), \quad (1)$$

where  $\mathcal{S}(t)$  is a surface which evolves with time  $t$ ,  $f(\mathbf{x}, t)$ , defined for all  $\mathbf{x} \in \mathcal{S}(t)$  and all  $t$ , is the density (per unit area) of a superficial quantity such as energy, and  $da(\mathbf{x})$  is the area measure on surfaces in  $\mathbb{R}^3$ . The evaluation of (1) is nontrivial when  $\mathcal{S}(t)$  evolves within a fixed region  $\Omega \subset \mathbb{R}^3$  and  $\partial\mathcal{S}(t) \subset \partial\Omega$  is nonempty, for then a portion of (1) must balance an outflow of  $f$  due to the transport of portions of  $\mathcal{S}(t)$  across  $\partial\Omega$ .

We assume that  $\mathcal{S}(t)$  is smooth and oriented by  $\mathbf{n}(\mathbf{x}, t)$ , a particular choice of continuous unit-normal field, and we write  $V(\mathbf{x}, t)$  and  $\kappa(\mathbf{x}, t)$  for the **normal velocity** and **total curvature**. (Total curvature is twice the normal curvature.) It is the purpose of this note to prove the **transport theorem**:<sup>1</sup>

$$\begin{aligned} \frac{d}{dt} \int_{\mathcal{S}(t)} f da &= \int_{\mathcal{S}(t)} (f^\circ - f\kappa V) da - \text{outflow}(f, \partial\mathcal{S}(t)), \\ \text{outflow}(f, \partial\mathcal{S}(t)) &= \int_{\partial\mathcal{S}(t)} f V p (1 - p^2)^{-1/2} ds, \quad p = \mathbf{n} \cdot \boldsymbol{\nu}. \end{aligned} \quad (2)$$

Here  $f^\circ$  is the normal time derivative of  $f$  as defined below,  $ds$  is the measure of length on curves in  $\mathbb{R}^3$ , and  $\boldsymbol{\nu}(\mathbf{x})$  is the outward unit normal on  $\partial\Omega$ .

**2. Assumptions and preliminary definitions.** It is convenient to identify  $\mathbb{R}^4$  with  $\mathbb{R}^3 \times \mathbb{R}$ .

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<sup>1</sup>An argument in support of (2) is contained in the work Moeckel [1]. Moeckel assumes that the interface can be identified with a "fictitious" (sic) evolving membrane whose boundary coincides with the boundary of the interface at each time, and then appeals to a standard transport theorem for membranes. Unfortunately, Moeckel expresses the outflow in terms of the *membrane* velocity, which is not intrinsic, and which obscures the influence of the confining region  $\Omega$ . Moreover, the existence of such an evolving membrane is not at all obvious, and, in fact, seems to constitute a mathematical problem more difficult than the original problem of verifying (2). Angenent and Gurtin [2] establish (2) for an evolving curve in a two-dimensional space, but their proof does not extend.

We assume that  $\Omega \subset \mathbb{R}^3$  is a bounded, open region with smooth boundary  $\partial\Omega$ , and write  $\nu(\mathbf{x})$  for the outward unit normal on  $\partial\Omega$ . We assume that  $\mathcal{S}(t) \subset \mathbb{R}^3$  is defined for all  $t$  in an open interval  $T$  and: (S1)  $\mathcal{S}(t)$  is the intersection with  $\Omega$  of a smooth, nonintersecting, oriented surface, and  $\partial\mathcal{S}(t) \subset \partial\Omega$ ; (S2)  $\mathbf{n}(\mathbf{x}, t)$ , the unit normal to  $\mathcal{S}(t)$ , satisfies  $|\mathbf{n}(\mathbf{x}, t) \cdot \nu(\mathbf{x})| \neq 1$  on  $\partial\mathcal{S}(t)$ ; (S3) the set

$$\mathcal{S}_T = \{(\mathbf{x}, t) : \mathbf{x} \in \mathcal{S}(t), t \in T\}$$

is a smooth three-dimensional surface in  $\mathbb{R}^4$  with normal never parallel to the time direction.

We assume that  $f(\mathbf{x}, t)$  is a smooth scalar field on  $\mathcal{S}_T$ .

We write  $\mathbf{N}(\mathbf{x}, t)$  and  $\mathbf{U}(\mathbf{x})$ , respectively, for  $\mathbf{n}(\mathbf{x}, t)$  and  $\nu(\mathbf{x})$  considered as unit vectors in  $\mathbb{R}^4$ , and  $\mathbf{E}$  for the unit vector in  $\mathbb{R}^4$  in the time direction:

$$\mathbf{N} = (\mathbf{n}, 0), \quad \mathbf{U} = (\nu, 0), \quad \mathbf{E} = (\mathbf{0}, 1). \tag{3}$$

By (S3) there is a scalar field  $V$  such that  $\mathbf{N} - V\mathbf{E}$  is normal to  $\mathcal{S}_T$ ; the field  $V$  represents the **normal velocity** of the surface in the direction  $\mathbf{n}$ . We write  $\mathbf{M}$  for the unit vector in the direction of  $\mathbf{N} - V\mathbf{E}$ :

$$\mathbf{M} = q(\mathbf{N} - V\mathbf{E}), \quad q = (1 + V^2)^{-1/2}. \tag{4}$$

Then  $\mathbf{M}(\mathbf{x}, t)^\perp$  is the tangent plane to  $\mathcal{S}_T$  at  $(\mathbf{x}, t)$ . We write  $\mathbf{E}^*$  for the normalized projection of  $\mathbf{E}$  onto  $\mathbf{M}^\perp$ :

$$\mathbf{E}^* = q(V\mathbf{N} + \mathbf{E}). \tag{5}$$

Given any field  $\Phi$  on  $\mathcal{S}_T$ , we write  $\nabla\Phi$  for the surface gradient<sup>2</sup> of  $\Phi$  in  $\mathcal{S}_T$ :  $\nabla\Phi(\mathbf{x}, t)$  is a vector in  $\mathbf{M}(\mathbf{x}, t)^\perp$  if  $\Phi$  is scalar-valued; it is a linear transformation from  $\mathbf{M}(\mathbf{x}, t)^\perp$  into  $\mathbb{R}^4$  if  $\Phi$  is vector-valued. For  $\Phi$  a scalar field, we define the **normal time derivative**  $\Phi^\circ$  through

$$\Phi^\circ = \nabla\Phi \cdot (V\mathbf{N} + \mathbf{E}). \tag{6}$$

We write  $\text{div}$  for the surface divergence on  $\mathcal{S}_T$ : if  $\Phi$  is a vector field on  $\mathcal{S}_T$ ,  $\text{div } \Phi = \text{trace}[\mathbf{P}\nabla\Phi]$ , where  $\mathbf{P}(\mathbf{x}, t)$  is the projection of  $\mathbb{R}^4$  onto  $\mathbf{M}(\mathbf{x}, t)^\perp$ . It is not difficult to verify that

$$\kappa = -\text{div } \mathbf{N} \tag{7}$$

is the **total curvature** of  $\mathcal{S}(t)$ .

The identity

$$\text{div } \mathbf{E}^* = -q\kappa V \tag{8}$$

is useful. Its verification is not difficult: since  $\nabla q = -q^3 V \nabla V$  and  $q - q^3 V^2 = q^3$ , (5) and (7) yield

$$\text{div } \mathbf{E}^* = qV \text{div } \mathbf{N} + q^3 \nabla V \cdot \mathbf{N} - q^3 V \nabla V \cdot \mathbf{E} = -qV\kappa + q^3 \nabla V \cdot (\mathbf{N} - V\mathbf{E})$$

which implies (8), since  $\mathbf{N} - V\mathbf{E}$  is normal to  $\mathcal{S}_T$  (cf. (4)).

<sup>2</sup>Many of the definitions and identities that we use concerning surfaces can be found in [3, 4].

**3. Proof of the transport theorem.** Given a time interval  $R = [t_0, t_1] \subset T$ , the surface divergence theorem applied to the vector field  $f\mathbf{E}^*$  on

$$\mathcal{S}_R = \{(\mathbf{x}, t) : \mathbf{x} \in \mathcal{S}(t), t \in R\}$$

has the form

$$\int_{\partial \cdot \mathcal{J}_R} f\mathbf{E}^* \cdot \mathbf{W} dA_2 = \int_{\mathcal{J}_R} \operatorname{div}(f\mathbf{E}^*) dA_3. \tag{9}$$

Here  $dA_n$  ( $n = 1, 2, 3$ ) is the ‘‘area’’ measure on  $n$ -dimensional surfaces in  $\mathbb{R}^4$ , while  $\mathbf{W}$  is the outward unit normal to  $\partial \mathcal{S}_R$ .  $\partial \mathcal{S}_R$  is the union of the sets

$$\operatorname{top}(\mathcal{S}_R) = \{(\mathbf{x}, t_1) : \mathbf{x} \in \mathcal{S}(t_1)\},$$

$$\operatorname{bot}(\mathcal{S}_R) = \{(\mathbf{x}, t_0) : \mathbf{x} \in \mathcal{S}(t_0)\},$$

$$\operatorname{side}(\mathcal{S}_R) = \{(\mathbf{x}, t) : \mathbf{x} \in \partial \mathcal{S}(t), t \in T\},$$

whose intersection has zero  $A_1$ -measure, and, trivially,

$$\mathbf{E}^* \cdot \mathbf{W} = 1 \quad \text{on } \operatorname{top}(\mathcal{S}_R), \quad \mathbf{E}^* \cdot \mathbf{W} = -1 \quad \text{on } \operatorname{bot}(\mathcal{S}_R). \tag{10}$$

The computation of  $\mathbf{E}^* \cdot \mathbf{W}$  on  $\operatorname{side}(\mathcal{S}_R)$  is not so simple. Since

$$p = \mathbf{n} \cdot \boldsymbol{\nu} = \mathbf{N} \cdot \mathbf{U}, \tag{11}$$

(4) and (5) yield

$$\mathbf{U} \cdot \mathbf{M} = qp, \quad \mathbf{U} \cdot \mathbf{E}^* = qpV. \tag{12}$$

If  $\mathbf{A} = \mathbf{U} - (\mathbf{U} \cdot \mathbf{M})\mathbf{M}$ , the projection of  $\mathbf{U}$  onto  $\mathbf{M}^\perp$ , then  $\mathbf{W} = \mathbf{A}/|\mathbf{A}|$  on  $\operatorname{side}(\mathcal{S}_R)$ . Thus, using (12),

$$\mathbf{W} = (1 - q^2p^2)^{-1/2}(\mathbf{U} - qp\mathbf{M}) \quad \text{on } \operatorname{side}(\mathcal{S}_R), \tag{13}$$

and, since  $\mathbf{M} \cdot \mathbf{E}^* = 0$  and

$$(1 - q^2p^2) = (1 - p^2 + V^2)/(1 + V^2), \tag{14}$$

a simple calculation using (12) leads to

$$\mathbf{E}^* \cdot \mathbf{W} = Vp(1 - p^2 + V^2)^{-1/2} \quad \text{on } \operatorname{side}(\mathcal{S}_R). \tag{15}$$

By (5), (6), and (8),  $\operatorname{div}(f\mathbf{E}^*) = q(-fV\kappa + f^\circ)$ ; thus (9) yields

$$\begin{aligned} & \int_{\operatorname{top}(\mathcal{J}_R)} f dA_2 - \int_{\operatorname{bot}(\mathcal{J}_R)} f dA_2 + \int_{\operatorname{side}(\mathcal{J}_R)} f Vp(1 - p^2 + V^2)^{-1/2} dA_2 \\ &= \int_{\mathcal{J}_R} q(f^\circ - f\kappa V) dA_3. \end{aligned} \tag{16}$$

Further,

$$\int_{\operatorname{top}(\mathcal{J}_R)} f dA_2 = \int_{\mathcal{J}'(t_1)} f da, \quad \int_{\operatorname{bot}(\mathcal{J}_R)} f dA_2 = \int_{\mathcal{J}'(t_0)} f da. \tag{17}$$

The final step is to rewrite the remaining terms in (16) as iterated integrals. For any function  $g$  on  $\mathcal{S}_R$ ,

$$\int_{\mathcal{J}_R} g dA_3 = \int_{t_0}^{t_1} \left\{ \int_{\mathcal{J}'(t)} g(\mathbf{E}^* \cdot \mathbf{E})^{-1} da \right\} dt = \int_{t_0}^{t_1} \left\{ \int_{\mathcal{J}'(t)} gq^{-1} da \right\} dt, \tag{18}$$

where we have used (5). On the other hand,

$$\int_{\text{side}(\partial\mathcal{S}_R)} g dA_2 = \int_{t_0}^{t_1} \left\{ \int_{\partial\mathcal{S}(t)} g(\mathbf{B} \cdot \mathbf{E})^{-1} ds \right\} dt, \tag{19}$$

where  $\mathbf{B}(\mathbf{x}, t)$  with  $\mathbf{B} \cdot \mathbf{E} > 0$  is that unit vector in the tangent plane to  $\text{side}(\partial\mathcal{S}_R)$  which is normal to  $\partial\mathcal{S}(t)$ . In fact,  $\mathbf{B} = \mathbf{C}/|\mathbf{C}|$ , where  $\mathbf{C}$  is the projection of  $\mathbf{E}^*$  onto  $\mathbf{W}^\perp$ :

$$\mathbf{C} = \mathbf{E}^* - (\mathbf{E}^* \cdot \mathbf{W})\mathbf{W}.$$

By (4)<sub>2</sub> and (15),

$$|\mathbf{C}|^2 = q^{-2}(1 - p^2)/(1 - p^2 + V^2).$$

Further, since  $\mathbf{E}^* \cdot \mathbf{M} = \mathbf{U} \cdot \mathbf{E} = 0$ , (4), (5), (12), and (13) yield

$$\mathbf{E}^* \cdot \mathbf{E} = q, \quad \mathbf{E}^* \cdot \mathbf{W} = q p V(1 - q^2 p^2)^{-1/2}, \quad \mathbf{E} \cdot \mathbf{W} = q^2 p V(1 - q^2 p^2)^{-1/2},$$

and hence, using (14),

$$\mathbf{B} \cdot \mathbf{E} = (1 - p^2)^{1/2}(1 - p^2 + V^2)^{-1/2}.$$

Thus (19) yields

$$\int_{\text{side}(\partial\mathcal{S}_R)} g dA_2 = \int_{t_0}^{t_1} \left\{ \int_{\partial\mathcal{S}(t)} g \{ (1 - p^2 + V^2)/(1 - p^2) \}^{1/2} ds \right\} dt. \tag{20}$$

Finally, in view of (17), (18), and (20), (16) reduces to

$$\begin{aligned} & \int_{\mathcal{S}(t_1)} f da - \int_{\mathcal{S}(t_0)} f da + \int_{t_0}^{t_1} \left\{ \int_{\partial\mathcal{S}(t)} f V p / (1 - p^2)^{1/2} ds \right\} dt \\ & = \int_{t_0}^{t_1} \left\{ \int_{\mathcal{S}(t)} (f^\circ - f \kappa V) da \right\} dt; \end{aligned}$$

and differentiation with respect to  $t_1$  yields (2).

REMARK 1.  $\mathcal{S}(t)$  is the intersection with  $\Omega$  of an oriented surface  $\mathcal{M}(t)$ ; let  $\boldsymbol{\mu}(\mathbf{x}, t)$ , a tangent vector to  $\mathcal{M}(t)$  at  $\mathbf{x} \in \mathcal{M}(t)$ , denote the outward unit normal to  $\partial\mathcal{S}(t)$  as a curve in  $\mathcal{M}(t)$ . The calculation of the outflow term in (2) is essentially the calculation of the velocity  $\boldsymbol{\sigma}(\mathbf{x}, t)$  of  $\partial\mathcal{S}(t)$  in the direction  $\boldsymbol{\mu}(\mathbf{x}, t)$ . In fact, if we consider an arbitrary (smoothly-evolving) patch  $\mathcal{S}(t)$  of an evolving surface  $\mathcal{M}(t)$ , then

$$\frac{d}{dt} \int_{\mathcal{S}(t)} f da = \int_{\mathcal{S}(t)} (f^\circ - f \kappa V) da + \int_{\partial\mathcal{S}(t)} f \boldsymbol{\sigma} ds. \tag{21}$$

REMARK 2. It is important to identify the term  $\text{outflow}(f, \partial\mathcal{S}(t))$  in (2) as a term representing an outflow of  $f(\mathbf{x}, t)$  due to the transport of portions of  $\mathcal{S}(t)$  across  $\partial\Omega$ . If one writes, for example, balance of energy for a continuous body  $\Omega$  consisting of two phases separated by an interface  $\mathcal{S}(t)$  with interfacial energy  $f$ , then a term of the form  $\text{outflow}(f, \partial\mathcal{S}(t))$  should appear (cf. Gurtin [4]). Moeckel [1] fails to include such an outflow in his balance laws. Fernandez-Diaz and Williams [5] point this out, but unfortunately the outflow term they propose is incorrect, as it does not include the scale factor  $(1 - p^2)^{-1/2}$ .

**REMARK 3.** It is possible to write the transport identity (2) in terms of a nonnormal velocity. Indeed, for  $\mathbf{v} = V\mathbf{n} + \mathbf{u}$  with  $\mathbf{u} \cdot \mathbf{n} = 0$ ,

$$\frac{d}{dt} \int_{\mathcal{S}'(t)} f da = \int_{\mathcal{S}'(t)} (f^\circ + f \operatorname{div} \mathbf{u}) da - \operatorname{outflow}(f, \partial \mathcal{S}(t)) \quad (22)$$

where  $f^\circ = \nabla f \cdot (\mathbf{v} + \mathbf{E})$  is the derivative following  $\mathbf{v}$ ,  $\operatorname{div}$  is the surface divergence on  $\mathcal{S}(t)$ , and

$$\operatorname{outflow}(f, \partial \mathcal{S}(t)) = \int_{\partial \mathcal{S}'(t)} f [Vp(1-p^2)^{-1/2} + \mathbf{u} \cdot \boldsymbol{\nu} (1+p^2)^{-1/2}] ds, \quad p = \mathbf{n} \cdot \boldsymbol{\nu}. \quad (23)$$

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