

**A WATER-QUALITY SIMULATION
MODEL FOR WELL MIXED ESTUARIES
AND COASTAL SEAS: VOLUME IX,
THE COMPUTER PROGRAM**

J. J. LEENDERTSE, A. B. NELSON

R-2298-RC

APRIL 1978

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PREFACE

This report is the last of a series of reports on modeling Jamaica Bay, New York. Even though previous reports in the series have described in much detail all the steps that were taken in these studies, the program itself was never published. In one of the reports it was indicated that the program would be made available to other investigators, and this promise is being fulfilled herewith.

Considerable time has elapsed between this publication and the previous one in the series. Our contractual agreement ended with the publication of Volume VIII in 1975, and the investigators turned their attention to other projects. They have worked only intermittently on this publication, which was sponsored by The Rand Corporation.

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I. INTRODUCTION

The publication of a computer program is generally a difficult task for an investigator. Not only does he lay bare exactly what he did in the investigation, he also must choose a final set from different versions of the program he has developed in the course of his studies. Large computer programs in intensive use are generally in a state of constant flux to meet the demands of specific investigators or to correct errors in options that were not fully tested.

We decided to publish the version that completely reflects the detailed descriptions given in Volume II of the report series. No modifications in the method of computation were made for the experiments described in subsequent reports. Only from time to time modifications in outputs were made to satisfy particular demands in our investigation.

The program as published should be seen as documentation of our work. The model can be used for other investigations, but the user must satisfy himself that all the approximations in the model are applicable in his case.

The model as presented is not a generalized model which can be used for a certain class of estuaries and coastal seas; it is limited in its boundary conditions, and changes are required if the model boundary is not on the left side of the model array.

The model was a tool for engineering analyses, and thus we did not go further in its development than to be able to solve the problem at hand; we refrained from making an extended analysis of the computational properties of the finite difference scheme used in the model. We took, in a few instances, first-order approximations of certain terms of the differential equations, which in our case was satisfactory.

For a more general application, the computational method has some shortcomings. The most important and troublesome is that the advection terms are taken at the lower time level, which introduces a stability condition upon time step and grid size.

For large arrays, the possibility also exists that nonlinear instabilities are generated by the choice of the primitive form of the finite difference expression in the advection terms.

In the Jamaica Bay study, it was not necessary to incorporate advection terms which would not generate these instabilities, because the primitive terms used did not generate troublesome instabilities and because more stable expressions for these terms would have increased the computation time.

II. PROGRAM USAGE

PROGRAM CAPABILITIES

The program in its present form can be used to compute the flow and pollutant distributions in a certain region if:

1. The hydrodynamic and transport equations described in Refs. 1 and 2 are representative of the fluid motions and transport of constituents.
2. Information is available about depth to a certain reference level.
3. The bathymetry can be approximated with sufficient detail. (Computer memory and computer time requirements per run are proportional to the second and roughly third power, respectively, of the reciprocal of the space grid size.)
4. Sufficient data are available for model adjustment.
5. Input water level histories at a single boundary at the left side of the model are available for forcing the model.
6. Time-varying wind and discharge information is available.
7. Currents are relatively weak and the system quite well dampened so that stability conditions of the advection terms are not exceeded.

MODEL LAYOUT

The area for which the simulations are made is covered by a two-dimensional grid on a horizontal plane. All descriptions of spatially varying parameters and of all variables are made on this grid. The grid system is described in Refs. 1 and 2.

The indices of variables in the Y direction (north) are mentioned first in the array description; the variables in the X direction are the second values. The large number of two-dimensional arrays which are required have dimensions NMAX, MMAX, where NMAX is the total number of points in the Y direction and MMAX the total number of points in the X direction. In the Jamaica Bay study the dimensions were 61, 78. In addition to the two-dimensional arrays, three-dimensional arrays are

used for the constituents R, RP. Usage of a large number of constituents is discouraged, as the computation time for the reaction model increases with the second power of the number of constituents.

The model is for the foot-pound system. If the metric system is used, certain constants in the program have to be changed. In subroutine CVAL, for example, the constant in the relationship between Chezy values and Manning's values has to be modified.

The required computation times can become considerable, particularly if a fine grid is used, which necessitates the use of a small time step. The investigator will do well to first try to make a Jamaica Bay run to familiarize himself with computer memory and time requirements before making estimates for other runs. The Jamaica Bay model as presented requires about 400,000 bytes of memory.

INPUT DATA DESCRIPTION

General

The data input is divided into roughly three sections. The first section contains control data for the computation, the second section array values for system initialization and control, and the third section presents time-varying inputs.

Control Data

The main control variables are described below. To identify the method of input, we will use the following designation containing three groups of numbers. The first group is the card number, the second the column number range, and the third the format. For example, NMAX (2:1-4:I4) is found on card 2, in columns 1 through 4, and the format is I4. The control variables and parameters are listed in the order in which they are inserted.

TITL	(1:1-72:18A4)	Title of the run; it appears in the beginning of the print and data sets written on tape.
NMAX	(2:1-4:I4)	Number of grid points in Y direction of the computational grid.

MMAX (2:5-8:I4) Number of grid points in X direction of the computational grid.

NB1 (2:9-12:I4) Lower value of the open boundary at the left side of the computational grid.

NB2 (2:13-16:I4) Upper value of the open boundary at the left side of the computational grid. A linear interpolation is used for intermediate boundary points between $N=NB1$ and $N=NB2$.

ANGLAT(2:17-21:E5.0) Latitude in the center of the computational grid; expressed in degrees and positive in the northern hemisphere.

AL (2:22-26:E5.0) Distance between points of the computational grid.

AG (2:27-31:E5.0) Value of the gravitational acceleration.

AT (2:32-36:E5.0) Half the time step which is the time increment between the two levels of the transport equation.

CSET (2:37-41:E5.0) Chezy value for the flow computation when the tidal flat is becoming dry. This value is used when the temporal depth is smaller than $2*VAR$.

VAR (2:42-46:E5.0) Threshold depth on tidal flat. If temporal depth is smaller than this value during the time that this computation checks for flooding, then the point is taken out of the computation.

SEINV (2:47-51:E5.0) Water level to start the computation. This value should *not* be identically zero (i.e., 0.0), as during initialization a zero water level means a dry point.

GAMM (2:52-56:E5.0) Weighting factor describing that portion of pollution value which is replaced by surrounding values (spatial smoothing). This operation is performed only on the pollution checkpoints before writing the data on tape.

DCO (2:57-61:E5.0) Maximum depth not affected by the depth multiplier DML.

DML (2:62-66:E5.0) Depth multiplier. The array values of the depth can all be multiplied by DML for a sensitivity analysis of depth schematization in amplitudes and phases of the computed tidal wave in the system.

DEPDEF(2:67-71:E5.0) Default value for the depth. If no depth value is used in the depth array, DEPDEF is used. It is advantageous to use a value less than the minimum depth during flood. In that case DEPDEF is negative, as the depth is positive downward.

NST (3:1-4:I4) Time step number to start the integration.

NTAPE (3:5-8:I4) Time step number at which the computation is restarted from data from the restart tape. If no restart is made, NTAPE=0.

MAXST (3:9-12:I4) Time step number to terminate the computation. At this time step all data required for a restart are written on tape.

NTFREQ(3:13-16:I4) Frequency to write data on restart tape. This feature protects long computation against loss because of system failure. It should be used sparingly, as much data are written. The records written can also be used for graphical output programs.

NWLC (3:21-24:I4) Frequency to print the selected water level and current station values.

NSMO (3:25-28:I4) Frequency to time smooth. At this interval the computation is backstepped half a time step and restarted from time-averaged values a full time step apart. A time correction is made in the time step of the computation to allow for the loss of the half time step.

NCVAL (3:29-32:I4) Frequency to compute C values from Manning's coefficient.

NREQ (3:33-36:I4) Number of time steps between input values of the water level boundary inputs. A linear interpolation of water levels is used for intermediate time steps.

NFL (3:37-40:I4) Number of time steps in which the concentrations at the boundary return to the preset value.

NSRC (3:41-44:I4) Number of discharges (outfalls) in the system; number of constituent sources.

NPOL (3:45-48:I4) Number of constituent measuring stations in the model. At these stations concentrations are written on tape.

NOWL (3:49-52:I4) Number of water level stations in the model.

NOCUR (3:53-56:I4) Number of current stations.

NFLOD (3:57-60:I4) Frequency to check for flooding. Note that very small intervals are not necessarily more accurate, as more noise is generated in the computation. It is preferable to use odd numbers.

NTRA (3:61-64:I4) Number of sections through which flow and constituent transports in the U direction are computed.

LMAX (3:65-68:I4) Number of constituents used in the computation.

NWLT (3:69-72:I4) Frequency to write history tape.

NST (4:1-5:I5))

NTAPE (4:6-10:I5) } As shown on card 3, but these values will override

MAXST (4:11-15:I5) } the ones on the card, allowing more time steps.

WSTR (5:1-8:E8.0) Wind stress coefficient.

DAIR (5:9-16:E8.0) Density of air.

DWAT (5:17-24:E8.0) Density of water.

WCONV (5:25-32:E8.0) Conversion factor for units used to insert wind speed to units used in computation.

CDCON (5:33-40:E8.0) Factor for the computation of the longitudinal diffusion coefficient from the temporal depth velocity and the Chezy coefficient (Eq. (2.38) of Ref. 1).

LOX (6:1-5:I5) Constituent used for computation of dissolved oxygen.

SOX (6:6-15:E10.0) Saturation value for dissolved oxygen.

AKTP (6:16-25:E10.0) Reaction rate in BOD-DO system. (This value overrides the one in the reaction matrix.)

LRMX (6:26-30:I5) Number of constituents which interact. These constituents are listed first. Constituent numbers greater than LRMX should be conservative or only decaying.

NPRINT(7:1-80:16I5))

NPRINT(8:1-80:16I5) } Time steps to print all computational array values.

NPRINT(9:1-80:16I5) } Time steps should be in increasing order.

Array Data

Arrays of data are inserted after the control cards. The number of cards in each group has to be the same as that listed in the control card group.

Water Level Stations (NOWL Cards)

I	(1-5:I5)	Water level station number.
MWL	(6-10:I5)	Location of water level station in X direction.
NWL	(11-15:I5)	Location of water level station in Y direction.

Current Stations (NOCUR Cards)

I	(1-5:I5)	Current station number.
MC	(6-10:I5)	Location of current station in X direction.
NC	(11-15:I5)	Location of current station in Y direction.

Discharge (Outfall) Locations (NSRC Cards)

I	(1-5:I5)	Location number.
MINT	(6-15:I5)	Location of outfall in X direction.
NINT	(11-15:I5)	Location of outfall in Y direction.

Constituent Measuring Stations (KPOL Cards)

I	(1-5:I5)	Location number.
MPOL	(6-15:I5)	Location of station in X direction.
NPOL	(11-15:I5)	Location of station in Y direction.

Cross Sections in which Transports are Computed (NTRA Cards)

I	(1-5:I5)	Section number.
MIT	(6-10:I5)	Column at which cross section is located.
NIT1	(11-15:I5)	First point in N direction of cross section.
NIT2	(16-20:I5)	Last point in N direction of cross section.
BIT	(21-24:A4)	Cross section identification letters.

Return Concentrations at the Open Boundary (LMAX Cards)

RBND	(1-10:E10.0)	Concentration of particular constituent at open boundary and default concentration if not later specified.
POLT	(11-70:15A4)	Identification of concentration.

Reaction Matrix (LMAX Cards)

AKK (Format 8E8.0) Interaction matrix K. The card contains matrix row for Kth concentration.

Depth Array ($M*((N+15)/16)$ Cards)

H (Format 16E4.1) First 16 depth for M=1, then first 16 depth for M=2, etc., to M=MMAX, then second 16 depth for M=1, etc. Depth values are to be multiplied by ten before inserting. Depth is positive downward. The last row should always be above water.

Diffusion Coefficients

The first value inserted is the default value (E5.0), which can be overridden in sections of a row. This procedure allows easy adjustment without inserting a whole array. At the end of the diffusion value, a blank card should be inserted.

The sections are inserted in format 3I5,10E5.0. The first three values are the row number (N=...), the second number the first value of the row, and the third number the last value of the row followed by the actual diffusion values.

Manning's Coefficient

Again, the first value inserted is the default value (E5.0), which can be overridden in sections of a row. Subsequently, the sections are inserted in format 3I5,10E5.0. A blank card should be placed at the end.

Constituent Arrays

A single card with the number of the array (1-5-I5) is first inserted, then the array values, as in the depth array. A blank card should be at the end of the array, as well as at the end of all constituent array groups. Thus, if only default values are used, only one blank card is required for the constituents.

Time-Varying Data

The time-varying tide and wind data are supplied at time intervals

NREQ*2.*AT. Tide data are interpolated. Wind data are kept constant until the next change. If no wind data are supplied, wind intensity and direction are maintained. Each time-varying tide card also has an indicator showing how many discharge changes are following.

Each tide card has the format (F5.0,F7.0,I3,2F5.0). The first value is a sequence number starting with zero; the second is the boundary tide value; the third is a value (NPC) indicating the number of cards following for the discharges; and finally the wind intensity and wind angle data are given.

For each time-varying discharge there is one card. Cards are to be inserted in increasing outfall order in format (I2,7E10.0). The first value is the outfall number, followed by the discharge in ft^3/sec , and then the new concentration values. If the concentration values are omitted, then that particular concentration is unchanged.

Time-varying tide data for a longer period than the simulation time should be supplied, as otherwise the run will be terminated without writing the data sets on tape at the indicated maximum time step.

COMMON

The dimensions in COMMON depend generally on the variables in the control section of the computation. The description and the array dimensions are presented as they appear in the listing of the program.

A(MNMAX)	= Recursion factor array. (MNMAX is the largest value of MMAX and NMAX.)
B(MNMAX)	= Recursion factor array.
P(MNMAX)	= Recursion factor array.
Q(MNMAX)	= Recursion factor array.
RX(MNMAX)	= Recursion factor array.
S(MNMAX)	= Recursion factor array.
DISCH(NSRC)	= Discharge rate.
NA(MNMAX)	= Temporary storage array.
TITL(18)	= Title name array.
NPRINT(48)	= Temporary print array.
F(MNMAX)	= Coriolis value array.
NINT(NSRC)	= N location of discharge.
MINT(NSRC)	= M location of discharge.

NFLI (MAX2) = Temporary storage array.
MAX2=2*(MMAX+NMAX).

XLAND(1) = Graphics array which is not used.

YLAND(1) = Graphics array which is not used.

LAND(2) = Graphics array which is not used.

NPOL (KPOL) = N location of pollution measuring stations.

MPOL (KPOL) = M location of pollution measuring stations.

ATR(LMAX,NTRA) = Cumulative advective transport through cross sections.

DTR(LMAX,NTRA) = Cumulative diffusive transport through cross sections.

CTR(LMAX,NTRA) = Cumulative total transport through cross sections.

GRO(LMAX,KPOL) = Value of concentrations at pollution measuring stations.

MWL(NOWL) = M location of water level stations.

NWL(NOWL) = N location of water level stations.

MC(NOCUR) = M location of current stations.

NC(NOCUR) = N location of current stations.

ZWL(NOWL) = Value at water level station.

ZCUR(NOCUR) = Value at current station.

MIT(NTRA) = M location of cross section.

NIT1(NTRA) = Lower N value of cross section.

NIT2(NTRA) = Upper N value of cross section.

FLTR(NTRA) = Cumulative water transport.

BIT(NTRA) = Name of cross section.

SINT(LMAX,NSRC) = Array used for computation of constituent mass added at discharges.

SX(LMAX) = Temporary array.

R1(LMAX) = Temporary array.

R2(LMAX) = Temporary array.

R3(LMAX) = Temporary array.

R4(LMAX) = Temporary array.

CONC(LMAX) = Concentration at outfall.

POLTP(NOWL) = Temporary array.

POLT(LMAX,NOWL) = Temporary array.

PLEV(10,LMAX+3) = Temporary array.

RBND(LMAX) = Concentration at boundary.

NVOL(80) = Temporary array.
MVOL(80) = Temporary array.
AX(MNMAX) = Recursion factor array.
CX(MNMAX) = Recursion factor array.
BZ(MNMAX) = Recursion factor array.
R(LMAX,NMAX,MMAX) = Constituent array (first level).
RP(LMAX,NMAX,MMAX) = Constituent array (second level).
FX(LMAX,MNMAX) = Recursion factor array.
DFL(LMAX,MNMAX) = Recursion factor array.
E(LMAX,MNMAX) = Recursion factor array.
PZ(LMAX,MNMAX) = Recursion factor array.
VMAN(NMAX,MMAX) = Manning's value array.
REACT(LMAX,LMAX) = Reaction matrix array.
TINDAT(10) = Temporary array.
ROX(NMAX,MMAX) = Reaeration value array.
DIFCO(NMAX,MMAX) = Diffusion coefficient array.
AKK(LMAX,LMAX) = Reaction matrix values.
AKM(LMAX) = Temporary array.
AKP(LMAX) = Temporary array.
VOLDP(MNMAX) = Temporary value array for volumes.
VOLDM(MNMAX) = Temporary value array for volumes.
C(NMAX,MMAX) = Chezy value array.
H(NMAX,MMAX) = Depth value array.
SEN(NMAX,MMAX) = Water level at lowest time level.
SES(NMAX,MMAX) = Water level at time that point becomes dry.
CZ(61,78) = Chezy value array.

III. PROGRAM DESCRIPTION

The program consists of 13 subroutines. These subroutines are *not* all called from the MAIN subroutine. All subroutines share COMMON, except that six two-dimensional arrays are specified in each subroutine. COMMON is listed in Appendix A, the simulation program in Appendix B.

For simplicity, the input will be described as cards, and the output of a simulation will be printed values and data sets on two tape units. These tapes can then be used for graphical outputs, to be prepared according to the investigator's own specification and compatible with the plotting devices available to him.

The subroutines do not all have clear functions. In some cases more than one function were combined in a subroutine if that was convenient. This is usually indicated in the description of the different routines.

MAIN

This subroutine controls most of the computation. It reads the time-varying inputs, prepares them for usage in the computation, controls the output, and does part of the time-smoothing of the array variable when this is requested. Also, certain counters are set in this subroutine.

SUBROUTINE SETUP

As the name indicates, this subroutine sets many of the arrays used in the computation. It determines the location of water level stations, current stations, and sources and pollution measurement stations in the model. Subsequently, it determines the reaction matrix, sets certain often-used variables, and inserts zero in the main computation arrays. Furthermore, it calls subroutines like DEPTH, SINVAL, INDAT1, CVAL, and POLIN, which read initial array values. Finally, it performs such functions as reading the restart tape and printing values in several two-dimensional arrays.

SUBROUTINE SEPU

This subroutine computes part of the fluid flow. In particular, it solves Eqs. (19) and (20) of Ref. 2 for the whole computational field. It also calls the subroutine in which the transport is computed (DIFU) and checks if any of the computation points become dry. The recursion formulas which are used are described in Chapter IV of Ref. 2.

SUBROUTINE FLO

This subroutine determines if a dry point should be taken into the computation. The procedures are described in Ref. 2, under Tidal Flat Computations.

SUBROUTINE SEPV

This subroutine also computes part of the fluid flow. In this case it solves Eqs. (22) and (23) of Ref. 2 for the whole computational field. It performs the same function as SEPU, only here water levels and the V velocity are computed implicitly, rather than water levels and the U velocity.

SUBROUTINE DIFU

In this subroutine the transport equations belonging to the hydrodynamic equations of SEPU are computed, as are the reactions between the different pollution constituents.

Since the cross sections at the velocity point and the temporal depth at the water level point are computed, it was convenient to check here if these values could become negative. The procedures are designed so that if this occurs, it is prevented by blocking the pollutant transport through the section and making the point dry, as described in Ref. 2. This procedure should more logically have been in FLO, but could be more efficiently made here. If a point becomes dry because of a negative volume, this rare occurrence is indicated by a printed message.

SUBROUTINE DIFV

This subroutine has the same function as DIFU, but only belongs to SEPU.

SUBROUTINE DEPTH

This subroutine reads the depth cards.

SUBROUTINE SINVAL

This subroutine sets the initial water level at all grid points with water.

SUBROUTINE CVAL

This subroutine computes the Chezy value from the Manning's coefficient. It also sets the C value to a preset value if only a limited depth is available.

SUBROUTINE INDAT1

This subroutine reads the diffusion coefficients and Manning's coefficients.

SUBROUTINE POLIN

This subroutine reads the initial values of the constituent distributions.

TAPE UNIT (8)

Tape Unit (8) is used to write the time step and all array values at certain intervals and at the end of the simulation. This tape can then be used to restart the computation or to abstract data from the tape for further processing.

IV. JAMAICA BAY DATA

The data set shown in Appendix C is a typical simulation performed in a series of experiments to determine the impact of different overflows in Jamaica Bay. The tide input data are shown in Fig. 21 of Ref. 3.

Four constituents were used in the simulation: dissolved oxygen (DO), biochemical oxygen demand (BOD), salinity, and coliform. During the simulation, a rainstorm occurs which generates the discharges at the outfalls. The data set is complete, and can be considered the documentation of the main adjusted variables of the Jamaica Bay system.

This example was selected because it was a simulation with only a few constituents and the characteristics of the constituents were widely varying.

To make data management of the two-dimensional arrays in the input more effective, control values are added in the last eight columns of each input card. Those values in the depth array are part of the state coordinates at the location of the first depth point of the row. In the concentration arrays the type of constituent is shown, plus sequence numbers.

To reduce the volume of this report, only 15.5 hours of time-varying tide data are included in the data set description. This should be sufficient to test computational procedures. The complete data set, together with the program, is available in digital form upon request.

Appendix A

LISTING OF COMMON

1

```
C.....
C JAMAICA BAY COMMON FROM 1972 N.N2640. JAMCOM72
C SE,SEP,V,VP,U,UP ARE DIMENSIONED IN EACH SUBROUTINE (SWITCHED IN DIFV)
C
COMMON A(78),B(78),P(78),Q(78),RX(78),S(78),DISCH(13)
COMMON NA(61),TITL(18),NPRINT(48),F(78)
COMMON ATAL,ATAL2,ATL,AKTP,AKTM,ALD,ALDED,CDAL
COMMON NSRC,NINT(13),MINT(13),NFL,AFL,NFLI(8)
COMMON NMAX,MMAX,NMAXN,MMAXM
COMMON NST,AT,CSET,NB1,NB2
COMMON C1,C2,C3,C4,AK1,SDEN,VAR,GAMM,X0,Y0,XOM,YOM,DX,DY
COMMON DX2,DY2,FDX,FDY,IM,JM,XL,YL,Z(200)
COMMON XLAND(700),YLAND(700),LAND(20)
COMMON ANGLAT,AL,MAXST,SBND,RINIT,KBND,FF,S20,S21,S22,S0X
COMMON KPOL,NPOL(12),MPOL(12),ATR(4,5),DTR(4,5),CTR(4,5),GRO(4,12)
COMMON NWLC,NCVAL,FREQ,NOWL,NOCUR,NWLT
COMMON MWL(18),NWL(18),MC(9),NC(9)
COMMON ZWL(18),ZCUR(9),VALMAN,DCO,DML,NFLOD,LRMX
COMMON NTRA,MIT(5),NIT1(5),NIT2(5),FLTR(5),BIT(5)
COMMON WINDU,WINDV,COEF,PWIND,PWINDA
COMMON SINT(4,13),SX(4),R1(4),R2(4),R3(4),R4(4),CONC(4)
COMMON POLTP(18),POLT(4,18),PLEV(3,10),RBND(4),NVGR
COMMON NVOL(80),MVOL(80)
COMMON AX(78),CX(78),BZ(4,78),LMAX,DEPDEF
COMMON R(4,61,78),RP(4,61,78),FX(4,78),DFL(4,78),E(4,78),PZ(4,78)
COMMON VMAN(61,78),REACT(4,4),TINDAT(10),ROX(61,78),LOX
COMMON DIFCO(61,78),AKK(4,4),AKM(4),AKP(4),VOLDP(78),VOLDM(78)
COMMON C(61,78),H(61,78),SEN(61,78),FOFD,EDY,AG,CD,ZC1,ZC2
COMMON M,N,NZ,KMAX,INI,SEINV,NTFREQ,NSM0,SES(61,78)
DIMENSION CZ(61,78)
EQUIVALENCE (C(1,1),CZ(1,1))
C.....
```

Appendix B

PROGRAM LISTING

1

```
C*.....
C*.....
C*
C*
C*
C* ESTUARY POLLUTION MODEL
C* 1972 VERSION N.N2640. .PRINT72
C* SE,SEP,V,VP,U,UP ARE SPECIFIED IN EACH SUBROUTINE (SWITCHED IN DIFV)
C*
C*.....
C*.....
COMMON SE(61,78),SEP(61,78),V(61,78),VP(61,78),U(61,78),UP(61,78)
// DD DISP=OLD,DSN=N.N2640.A1700.JAMCOM72
// DD *.DCB=BLKSIZE=80
C
GO TO 87
C SET OPEN BOUNDS AS FUNCTIONS OF TABLEVALUES (XIA(K),ETC.)
C OR AS FUNCTIONS OF HALFTIMESTEP NUMBER (K).
89 CONTINUE
KBND=KBND-1
IF (KBND.NE.0) GO TO 22
KBND=FREQ
20 READ (5,21) BNDK,BNDS,NPC,WIND,WINDA
C 21 FORMAT (2E12.0,I3,37X,2E4.0)
21 FORMAT (F5.0,F7.0,I3,2F5.0)
IF (NPC.EQ.0) GO TO 640
DO 630 N1=1,NPC
READ (5,610) IN2,DISCHI,(CONC(L),L=1,LMAX)
610 FORMAT (I2,7E10.0)
WRITE (6,650) BNDK
650 FORMAT (I10,'BNDK= ',E13.6)
WRITE (6,611) IN2,DISCHI,(CONC(L),L=1,LMAX)
611 FORMAT (IX,'DISCHARGES',IX,I3,7(IX,E13.6))
DISCHI=DISCHI/(AL*AL)
DISCH(IN2)=DISCHI
DO 620 L=1,LMAX
C IF CONC(L)=0.0, SINT(L,IN2) IS UNCHANGED.
C IF CONC(L)<0.0, SINT(L,IN2)=0.0
IF (CONC(L).EQ.0.0) GO TO 620
SINT(L,IN2)=0.0
IF (CONC(L).GT.0.0) SINT(L,IN2)=-DISCHI*CONC(L)
620 CONTINUE
630 CONTINUE
640 CONTINUE
NBND=.5*FREQ*BNDK
IF (WINDA.EQ.0.0) GO TO 180
WRITE (6,650) BNDK
WRITE (6,641) WIND,WINDA
641 FORMAT (IX,'WIND CHANGE',2X,E13.6,IX,E13.6)
WINDA=WINDA/57.29578
TEMW=4.*AT*COEF*WIND*WIND
WINDU=TEMW*SIN(WINDA)
WINDV=TEMW*COS(WINDA)
PWIND=WIND
PWINDA=WINDA
180 CONTINUE
IF (NBND.GT.NST) GO TO 25
SBND=BNDS
GO TO 20
25 CONTINUE
DBND=(BNDS-SBND)/FREQ
22 CONTINUE
SBND=SBND+DBND
```

```
1      DO 170 NK=NB1,NB2
      SEP(NK,1)=SBND
170  CONTINUE
      DO 172 IN2=1,NSRC
      NY=NINT(IN2)
      MY=MINT(IN2)
      SE(NY,MY)=SE(NY,MY)+AT*DISCH(IN2)
172  CONTINUE
      IF(ISTEP.EQ.1) GO TO 96
      GO TO 301
C
87  CONTINUE
      REWIND 8
      REWIND 9
C      SET DIMENSIONS OF THE SYSTEM
      CALL SETUP
C
      IP=1
          ICFLG= 0
          KADE = 1
      ISTEP=2
      GO TO 500
C
88  ISTEP=1
      NST =NST +1
      K=2*NST-1
C      SET OPEN BOUND
      IF (NST.LE.MAXST) GO TO 89
530  CONTINUE
      WRITE (8) NST
      WRITE (8) SE,SEP,SEN,SES
      WRITE (8) U,UP,V,VP
      WRITE (8) R
      WRITE (8) RP
      WRITE (8) C,DFL,NFLI
      WRITE (8) ATR,DTR,CTR,FLTR
      REWIND 8
C*****
      STOP
96  CONTINUE
100 CONTINUE
C
C      COMPUTE UP AND SEP ON ROW N ( FIRST HALF TIMESTEP)
      CALL SEPU
      CALL FLOW
      IF (MOD(NST,NFLOD).NE.0) GO TO 190
      DO 185 M=1,MMAX
      DO 185 N=1,NMAX
      IF (SEP(N,M).EQ.0.0) GO TO 179
      IF (C(N,M).NE.0.0) GO TO 185
      C(N,M)=CSET
      GO TO 185
179 C(N,M)=0.0
185 CONTINUE
190 CONTINUE
      IF (MOD(NST,NSM0).NE.2) GO TO 191
      DO 202 N=1,NMAX
      DO 202 M=1,MMAX
      R(1,N,M)=SEN(N,M)
      R(2,N,M)=U(N,M)
202 CONTINUE
191 CONTINUE
      DO 201 N=1,NMAX
      DO 201 M=1,MMAX
```

```
1      SEN(N,M)=SE(N,M)
      SE(N,M)=SEP(N,M)
      U(N,M)=UP(N,M)
      201 CONTINUE
C*****
      IF (MOD(NST,NCVAL).EQ.0) CALL CVAL
C
C          PRINT INSTRUCTIONS
C
500  IF (ISTEP-2)297,296,297
296  CONTINUE
C
      ICFLG=0
C
      300 CONTINUE
      IF(NST.EQ.NPRINT(IP)) GO TO 295
      IF (NST.LT.NPRINT(IP)) GO TO 297
      IP=IP+1
      GO TO 300
295  CONTINUE
      IP = IP+1
C
      CALL OUT
C
      ICFLG=1
297  NUM = 1
      GO TO(299,88),ISTEP
299  ISTEP=2
      K=2*NST
C          SET OPEN BOUNDS
      GO TO 89
C
      301 CONTINUE
C          COMPUTE VP AND SEP ON COLUMN M ( SECOND HALF TIMESTEP )
      CALL SEPV
C
      IF (MOD(NST,NTFREQ).NE.0) GO TO 500
      IF (NST.EQ.0) GO TO 500
      WRITE (8) NST
      WRITE (8) SE,SEP,SEN,SES
      WRITE (8) U,UP,V,VP
      WRITE (8) R
      WRITE (8) RP
      WRITE (8) C,DFL,NFLI
      WRITE (8) ATR,DTR,CTR,FLTR
      GO TO 500
      END
```

```
1
SUBROUTINE SETUP
COMMON SE(61,78),SEP(61,78),V(61,78),VP(61,78),U(61,78),UP(61,78)
// DD DISP=OLD,DSN=N.N2640. JAMCOM72
// DD *,DCB=BLKSIZE=80
C*****
  READ(5,4)(TITL(J),J=1,18)
4  FORMAT(18A4)
  WRITE(6,1)(TITL(J),J=1,18)
1  FORMAT(1H1,18A4)
  READ(5,200) NMAX,MMAX,NB1,NB2,ANGLAT,AL,AG,AT,CSET,VAR,SEINV,
  * GAMM,DCO,DML,DEPDEF
200 FORMAT(4I4,12E5.0)
  WRITE(6,201)
201 FORMAT(1H0,34H N M NB1 NB2 ANGLAT AL,7X,2HAG,7X,2HAT,
  * 5X,33HCSET VAR SEINV GAMM,
  * 25H DCO DML DEPDEF)
  WRITE(6,202) NMAX,MMAX,NB1,NB2,ANGLAT,AL,AG,AT,CSET,VAR,SEINV,
  * GAMM,DCO,DML,DEPDEF
202 FORMAT(4(1X,I4),12(1X,F8.3))
C*****
  READ(5,210) NST,NTAPE,MAXST,NTFREQ,NWLC,NSMO,NCVAL,
  * NREQ,NFL,NSRC,KPOL,NOWL,NOCUR,NFLOD,NTRA,LMAX,NWLT
  READ(5,212) NST,NTAPE,MAXST
210 FORMAT(20I4)
  WRITE(6,211)
211 FORMAT(1H0,49H NST NTAP MAXT NTFR NWLC NSMO NCVL NREQ NFL,
  * 40H NSRC KPOL NOWL NOCR NFLD NTRA LMAX NWLT)
  WRITE(6,212) NST,NTAPE,MAXST,NTFREQ,NWLC,NSMO,NCVAL,
  * NREQ,NFL,NSRC,KPOL,NOWL,NOCUR,NFLOD,NTRA,LMAX,NWLT
212 FORMAT(20I5)
  FREQ=NREQ+NREQ
  NFL=NFL+NFL
  IF(NSMO.EQ.0) GO TO 51
  ASMO=NSMO
  AT=AT*(ASMO+.5)/ASMO
51 CONTINUE
  READ(5,300) WSTR,DAIR,DWAT,WCONV,CDCON
300 FORMAT(8E8.0)
  COEF=WSTR*DAIR*WCONV*WCONV/DWAT
  WINDU=0.0
  WINDV=0.0
  PWIND=0.0
  PWINDA=0.0
  WRITE(6,305)
305 FORMAT(1H0,3X,4HCOEF,10X,4HWSTR,10X,4HDAIR,10X,4HDWAT,
  * 9X,5HWCONV,9X,5HCDCON)
  WRITE(6,310) COEF,WSTR,DAIR,DWAT,WCONV,CDCON
310 FORMAT(8(1X,E13.6))
  READ(5,311) LOX,SOX,AKTP,LRMX
311 FORMAT(15,2E10.0,15)
  WRITE(6,312) LOX,SOX,AKTP,LRMX
312 FORMAT(1H0,2X,'LOX',7X,'SOX',10X,'AKTP'2X,'LRMX',/,
  * 1H ,15,2(1X,E13.6),1X,15)
  READ(5,25) (NPRINT(N),N=1,16)
  READ(5,25) (NPRINT(N),N=17,32)
  READ(5,25) (NPRINT(N),N=33,48)
25 FORMAT(16I5)
  WRITE(6,212) (NPRINT(N),N=1,48)
  DO 250 J=1,NOWL
  READ(5,410) I,MWL(J),NWL(J)
  WRITE(6,212) I,MWL(J),NWL(J)
  IF(I.NE.J) GO TO 420
250 CONTINUE
```

```
1      DO 260 J=1,NOCUR
      READ (5,410) I,MC(J),NC(J)
      WRITE (6,212) I,MC(J),NC(J)
      IF (I.NE.J) GO TO 420
260   CONTINUE
      DO 400 J=1,NSRC
      READ (5,410) I,MINT(J),NINT(J)
      WRITE (6,212) I,MINT(J),NINT(J)
      IF (I.NE.J) GO TO 420
400   CONTINUE
      DO 405 J=1,KPOL
      READ (5,410) I,MPOL(J),NPOL(J)
      WRITE (6,212) I,MPOL(J),NPOL(J)
      IF (I.NE.J) GO TO 420
405   CONTINUE
410   FORMAT (10I5)
      DO 270 J=1,NTRA
      FLTR(J)=0.0
      READ (5,411) I,MIT(J),NIT1(J),NIT2(J),BIT(J)
      WRITE (6,411) I,MIT(J),NIT1(J),NIT2(J),BIT(J)
      IF (I.NE.J) GO TO 420
270   CONTINUE
411   FORMAT (4I5,A4)
      GO TO 430
420   PRINT 425
425   FORMAT (1X,18HCARDS OUT OF ORDER)
      STOP
430   CONTINUE
      WRITE (9) TITL
      WRITE (9) NTRA,MIT,NIT1,NIT2,BIT,NOWL,MWL,NWL,NOCUR,MC,NC,NWLC,
      *      KPOL,MPOL,NPOL,AT
      DO 800 L=1,LMAX
      READ (5,432) RBND(L),(POLT(L,J),J=1,15)
432   FORMAT (E10.0,15A4)
      WRITE (6,433) RBND(L),(POLT(L,J),J=1,15)
433   FORMAT (1H0,E12.5,2X,15A4)
800   CONTINUE
801   FORMAT (10E8.0)
      LTT=LMAX+1
901   FORMAT(110,10F4.1)
902   FORMAT(/'  VEL.CONTOUR TIMES',15.5X,' CONTOURS AT',10F8.4)
      WRITE (6,433)
      DO 435 L1=1,LMAX
      READ (5,300) (AKK(L1,L2),L2=1,LMAX)
      WRITE (6,310) (AKK(L1,L2),L2=1,LMAX)
435   CONTINUE
C*****
      KBND=1
      MMAX=MMAX -1
      NMAX=NMAX -1
      RANGL=3.1415927*ANGLAT/180.
      FF=3.1415927*SIN(RANGL)/21600.
      NST = 0
      C1 = AT*AG/AL
      C2 = AT/AL
      C3 = AT/4.
      C4 = 8.*AT*AG
      NVGR=99999
      FOFD=0.0
      EDY=25.
      CD=CDCON*SQRT(AG+AG)
      ZC1=1.0
      ZC2=1.0
      ATAL=AT/AL
```

```
1      ATL=ATAL/4.0
      ALD=2.0/AL
      ALDED=ALD*EDY
      CDAL=CD*ALD
      SDEN=3.05*3.05*3.05*AL*AL
      DO 35 IZ=1,13
      DISCH(IZ)=0.0
      DO 35 L=1,LMAX
      SINT(L,IZ)=0.0
35     CONTINUE
      AFL=NFL
      J1=NB2-NB1+1
      DO 495 J=1,J1
      DO 680 L=1,LMAX
680    DFL(L,J)=0.0
495    NFLI(J)=NFL
      DO 496 L=1,LMAX
      DO 496 I=1,NTRA
      ATR(L,I)=0.0
      DTR(L,I)=0.0
      CTR(L,I)=0.0
496    CONTINUE
      DO 6 N=1,NMAX
      DO 8 M=1,MMAX
      DO 700 L=1,LMAX
      R(L,N,M)=0.0
      RP(L,N,M)=0.0
700    CONTINUE
      ROX(N,M)=AKTP
      VP(N,M)=0.0
      UP(N,M)=0.0
      V(N,M)=0.
      SE(N,M)=0.0
      SEP(N,M)=0.0
      SEN(N,M)=0.0
      SES(N,M)=0.0
      U(N,M) = 0.
      C(N,M) = 0.
8      H(N,M) = 0.
6      F(N) = FF
      S21=0.0
      S22=0.0
      CALL DEPTH
      CALL SINVAL
      M=1
      DO 31 N=NB1,NB2
      C(N,M) = 75.
      SEN(N,M)=SEINV
      SEP(N,M)=SEINV
32    SE(N,M) =SEINV
31    CONTINUE
      SBND=SEINV
      IP=0
      CALL INDAT1
      CALL CVAL
      DO 30 N=1,NMAX
      DO 30 M=1,MMAX
      DO 740 L=1,LMAX
      R(L,N,M)=RBND(L)
      RP(L,N,M)=RBND(L)
740    CONTINUE
      30 CONTINUE
      CALL POLIN
```

C

```
1      IF (NTAPE.EQ.0) GO TO 101
100 CONTINUE
      READ (8) NST
      READ (8) SE,SEP,SEN,SES
      READ (8) U,UP,V,VP
      READ (8) R
      READ (8) RP
      READ (8) C,DFL,NFL1
      READ (8) ATR,DTR,CTR,FLTR
      IF (NST.LT.NTAPE) GO TO 100
101 CONTINUE
C      WRITE INITIAL VALUES
      INI=0
C
      WRITE(6,1) (TITL(J),J=1,18)
12  FORMAT(/1X,29HINITIAL DEPTHS IN .1          ,3HN= .13,2H .,13)
      NPR1=1
      NPR2=32
13  CONTINUE
      IF (NPR2.GT.NMAX) NPR2=NMAX
      WRITE (6,12) NPR1,NPR2
      DO 9 M=1,MMAX
      DO 40 N=NPR1,NPR2
40  NA(N)=H(N,M)*10.+.01
      9  WRITE(6,6001) M,(NA(N),N=NPR1,NPR2)
6001 FORMAT(1H .12,1X,3214)
      NPR1=NPR2+1
      NPR2=NPR2+32
      IF (NPR1.LE.NMAX) GO TO 13
      WRITE(6,1) (TITL(J),J=1,18)
15  FORMAT(/1X,28HC VALUES UNTIL NEXT PRINTOUT,5X,3HN= .13,2H .,13)
10  FORMAT(1H .12,1X,32F4.0)
      NPR1=1
      NPR2=32
14  CONTINUE
      IF (NPR2.GT.NMAX) NPR2=NMAX
      WRITE (6,15) NPR1,NPR2
      DO 16 JA=1,MMAX
16  WRITE(6,10) JA,(C(N,JA),N=NPR1,NPR2)
      NPR1=NPR2+1
      NPR2=NPR2+32
      IF (NPR1.LE.NMAX) GO TO 14
      NPR1=1
      NPR2=16
62  CONTINUE
      IF (NPR2.GT.NMAX) NPR2=NMAX
      WRITE (6,60) NPR1,NPR2
      DO 64 JA=1,MMAX
64  WRITE (6,61) JA,(DIFCO(N,JA),N=NPR1,NPR2)
      NPR1=NPR2+1
      NPR2=NPR2+16
      IF (NPR1.LE.NMAX) GO TO 62
60  FORMAT (/1X,'DIFFUSION COEFFICIENTS',5X,'N= ',13,' ',13)
61  FORMAT (1X,12,16(1X,F6.1))
      NPR1=1
      NPR2=16
67  CONTINUE
      IF (NPR2.GT.NMAX) NPR2=NMAX
      WRITE (6,65) NPR1,NPR2
      DO 69 JA=1,MMAX
69  WRITE (6,66) JA,(VMAN(N,JA),N=NPR1,NPR2)
      NPR1=NPR2+1
      NPR2=NPR2+16
      IF (NPR1.LE.NMAX) GO TO 67
```



```
1 65 FORMAT (/1X,'MANNING COEFFICIENTS',5X,'N= ',13.1,' ',13)
66 FORMAT (1X,12,16(1X,F6.3))
RETURN
END
```

1

```
      SUBROUTINE SEPU
      COMMON SE(61,78),SEP(61,78),V(61,78),VP(61,78),U(61,78),UP(61,78)
// DD DISP=OLD,DSN=N.N2640.          JAMCOM72
// DD *,DCB=BLKSIZE=80
      N=2
111  CONTINUE
      IF(N.EQ.NMAX) GO TO 110
      NNN=N+1
      NN=N-1
      M=1
      ST=SEP(N,M)
      IF(ST.EQ.0.) GO TO 124
C    WATER BOUND ONLY AT M=1
      GAMMA=0.5
      MF=2
      MFF =MF-1
      TEMP10=U(NNN,MFF)
      IF(TEMP10.EQ.0.) TEMP10=          U(NN,MFF)
      TEMP11=U(NN,MFF)
      IF(TEMP11.EQ.0.) TEMP11=          U(NNN,MFF)
      ALPHA=1.
      TEMP12 =SORT(U(N,MFF)**2+(((V(N,MF) + V(NN,MF))**2)/16.)) /
2    ((SE(N,MFF) + SE(N,MF) + H(N,MFF) + H(NN,MFF))*((C(N,MFF) +C(N,MF))
3    **2)**C4
      RX(MFF)=C1/(1. +C2*(U(N,MF) - U(N,MFF))*(1.-ALPHA)*2.0+TEMP12)
      S(MFF)=(U(N,MFF) + C1* SEP(N,MFF)-C1*(SEN(N,MF)-SEN(N,MFF))
1    -U(N,MFF)*TEMP12
3    + (V(N,MF) +V(NN,MF))* 0.5*(AT* F(N) -((1.-GAMMA)* C2 *
4    (TEMP10 -U(N,MFF)) -GAMMA*C2*(U(N,MFF) - TEMP11 )))/
5    (1. + C2*(U(N,MF) - U(N,MFF))*(1.-ALPHA)*2.0+TEMP12)
      M=M+1
      GO TO 123
121  CONTINUE
      RX(M)=0.0
      S(M)=0.
      M=M+1
122  CONTINUE
      P(M)=0.
      Q(M)=0.
      IF(M.EQ.MMAXM) GO TO 150
124  CONTINUE
      RX(M)=0.0
      S(M)=0.
      M=M+1
      CE=C(N,M)
      IF(CE.EQ.0.) GO TO 122
123  CONTINUE
      MMM=M+1
      MM=M-1
      HVT=H(N,M) + H(N,MM)+SE(N,M) +SE(NNN,M)
      HVB=H(NN,M)+H(NN,MM)+SE(N,M)+SE(NN,M)
      HUR=H(N,M) + H(NN,M) +SE(N,M)+SE(N,MMM)
      HUL=H(N,MM)+H(NN,MM)+SE(N,M)+SE(N,MM)
      TEMP2= 1. + .5*C2*HUL* RX(MM)
      A(M)=SE(N,M) +.5*C2*(HVB*V(NN,M) - HVT *V(N,M))
      P(M)=.5*C2* HUR/TEMP2
      Q(M)=(A(M) +.5*C2*HUL*S(MM))/TEMP2
      IF(M.EQ.MMAXM) GO TO 150
      CE=C(N,MMM)
      IF(CE.EQ.0.) GO TO 121
      GAMMA = 0.5
      TEMP10=U(NNN,M)
      IF(TEMP10.EQ.0.) TEMP10 =          U(NN,M)
```

```
1      TEMP11=U(NN,M)
      IF(TEMP11.EQ.0.) TEMP11 =          U(NNN,M)
      TEMP6 =AT*F(N) -(1.-GAMMA)*C2*(TEMP10 -U(N,M))- GAMMA* C2*
1(U(N,M) - TEMP11)
      TEMP6 = 0.5*TEMP6
      TEMP7 =SQRT( U(N,M)**2 +(((V(N,M)+V(N,MMM) +V(NN,M) + V(NN,MMM)
2)**2)/16.)))/(HUR*((C(N,M)+C(N,MMM))**2))* C4
      B(M) = U(N,M) + TEMP6 *(V(N,M)+V(N,MMM)+V(NN,M) +V(NN,MMM))
1-U(N,M)*TEMP7-C1*(SEN(N,MMM)-SEN(N,M))-WINDU/HUR
      ALPHA = 0.5
      TEMP1 =1.+C2*(AG*P(M)+U(N,MMM)-U(N,MM))+TEMP7
      RX(M)= C1/TEMP1
      S(M)=(B(M)+ C1*Q(M))/TEMP1
      M=M+1
      GO TO 123
150  CONTINUE
      UP(N,M)=0.
151  CONTINUE
112  CONTINUE
      MM=M-1
      SEP(N,M) = -P(M)*UP(N,M)+Q(M)
      IF (C(N,M).EQ.0.0) GO TO 152
      WET=H(N,M)+H(NN,M)+H(N,MM)+H(NN,MM)+SEP(N,M)*4.0
      IF(WET.LT.0.) GO TO 113
152  CONTINUE
      UP(N,MM) =-RX(MM)*SEP(N,M)+S(MM)
106  M = M-1
      IF(M.NE.1) GO TO 112
      N=NNN
      GO TO 111
113  C(N,M)=0.
      SEP(N,M)=0.
      V(N,M)=0.
      V(NN,M)=0.
      U(N,M)=0.
      U(N,MM)=0.
      SES(N,M)=SE(N,M)
      SE(N,M)=0.
      SEN(N,M)=0.
      WRITE(6,115) NST,N,M,SES(N,M)
115  FORMAT(1X,4HNST=,14,2X,2HN=,13,2HM=,13,2X,4HSES=,F7.4,
*16HVOLUME NEG. SEPU)
      N=NN
      IF(N.EQ.1) N=2
      GO TO 111
110  CONTINUE
C*****
      CALL DIFU
      DO 173 IN2=1,NSRC
      NY=NINT(IN2)
      MY=MINT(IN2)
      SE(NY,MY)=SE(NY,MY)-AT*DISCH(IN2)
173  CONTINUE
      IF (MOD(NST,NFLOD).NE.0) GO TO 190
      CSETH=.5*CSET
      DO 360 M=2,MMAXM
      MM=M-1
      MMM=M+1
      N=2
      CT2=C(2,M)
      CT3=C(3,M)
363  CONTINUE
      IF(N.EQ.NMAXN) GO TO 367
      NN=N
```

1

```
N=N+1
NNN=N+1
CT1=CT2
CT2=CT3
CT3=C(NNN,M)
CL2=C(N,MM)
CR2=C(N,MMM)
IF(CT2.EQ.0.) GO TO 364
  ST=SE(N,M)
STP=SEP(N,M)
IF(ST.LT.STP) STP=ST
SET=STP+STP
T1=SET+H(N,M)+H(N,MM)-VAR
IF (T1.LT.0.0) GO TO 366
T2=SET+H(NN,M)+H(NN,MM)-VAR
IF (T2.LT.0.0) GO TO 366
T3=SET+H(N,M)+H(NN,M)-VAR
IF (T3.LT.0.0) GO TO 366
T4=SET+H(N,MM)+H(NN,MM)-VAR
IF (T4.LT.0.0) GO TO 366
IF (T1.LT.VAR) GO TO 10
IF (T2.LT.VAR) GO TO 10
IF (T3.LT.VAR) GO TO 10
IF (T4.LT.VAR) GO TO 10
GO TO 363
10 CONTINUE
  C(N,M)=CSETH
  GO TO 363
366 CONTINUE
  H1=H(N,M)+H(N,MM)
  H2=H(N,M)+H(NN,M)
  H3=H(NN,M)+H(NN,MM)
  H4=H(N,MM)+H(NN,MM)
  IF (H1.GT.H2) GO TO 7
  IF (H1.GT.H3) GO TO 6
  IF (H1.GT.H4) GO TO 5
  HMIN=H1
  GO TO 4
7 IF (H2.GT.H3) GO TO 6
  IF (H2.GT.H4) GO TO 5
  HMIN=H2
  GO TO 4
6 IF (H3.GT.H4) GO TO 5
  HMIN=H3
  GO TO 4
5 HMIN=H4
4 CONTINUE
  STA=SEP(N,M)
  DRY=STA+.5*HMIN
  IF(DRY.LT.0.) GO TO 11
  SES(N,M)=STA
  GO TO 12
11 CONTINUE
  SES(N,M)=STA
  WRITE (6,13) NST,M,N,SES(N,M),STA,WATADD,S21
13 FORMAT (1X,4HNST=,15,2X,2HM=,13,2X,2HN=,13,2X,4HSES=,F7.4,
  * 2X,4HSTA=,F7.4,2X,7HWATADD=,F10.2,2X,'S21=',E13.6)
12 CONTINUE
  SEP(N,M)=0.
  SE(N,M)=0.
  UP(N,M)=0.
  UP(N,MM)=0.
  V(N,M)=0.
  V(NN,M)=0.
```

```
1      VP(N,M)=0.  
      VP(NN,M)=0.  
      C(N,M)=0.0  
      CT2=0.0  
      GO TO 363  
364    CONTINUE  
C**** BEGIN TESTS FOR FLOODING  
      CALL FLO(CT1,CT2,CT3,CL2,CR2,NN,NNN,MM,MMM)  
      GO TO 363  
367    CONTINUE  
360    CONTINUE  
190   CONTINUE  
      RETURN  
      END
```

1

```
      SUBROUTINE FLO(CT1,CT2,CT3,CL2,CR2,NN,NNN,MM,MMM)
      COMMON SE(61,78),SEP(61,78),V(61,78),VP(61,78),U(61,78),UP(61,78)
// DD DISP=OLD,DSN=N.N2640.      .JAMCOM72
// DD *,DCB=BLKSIZE=80
      SS=SE(N,M)
      VAP=SS+SS
      KCO=1
      IF(CT1.NE.0.) KCO=KCO+1
      IF(CT3.NE.0.) KCO=KCO+1
      IF(CL2.NE.0.) KCO=KCO+1
      IF(CR2.NE.0.) KCO=KCO+1
      GO TO (363,391,392,393,374),KCO
391  IF(CT3.NE.0.) GO TO 365
      IF(CT1.NE.0.) GO TO 394
      IF(CL2.NE.0.) GO TO 381
      GO TO 380
392  CONTINUE
      IF(CT1.NE.0.) GO TO 395
      IF((CL2.NE.0.).AND.(CR2.NE.0.)) GO TO 382
      IF((CL2.NE.0.).AND.(CT3.NE.0.)) GO TO 384
      GO TO 385
395  CONTINUE
      IF(CT3.NE.0.) GO TO 368
      IF(CR2.NE.0.) GO TO 372
      GO TO 371
393  CONTINUE
      IF(CT3.EQ.0.) GO TO 370
      IF(CR2.EQ.0) GO TO 375
      IF(CL2.EQ.0.) GO TO 376
      GO TO 386
394  CONTINUE
      ST=SE(NN,M)
      STP=SEP(NN,M)
      IF(ST.LT.STP) STP=ST
      SET=STP+STP-VAP
      IF (SET.LT.0.0) GO TO 363
      DRY=H(NN,M)+H(NN,MM)+SS+SEP(NN,M)
      IF (DRY.LT.0.0) GO TO 363
      SEP(N,M)=SS
      SE(N,M)=SS
      SEN(N,M)=SS
      GO TO 363
365  CONTINUE
      ST=SE(NNN,M)
      STP=SEP(NNN,M)
      IF(ST.LT.STP) STP=ST
      SET=STP+STP-VAP
      IF (SET.LT.0.0) GO TO 363
      DRY=H(N,M)+H(N,MM)+SS+SEP(NNN,M)
      IF (DRY.LT.0.0) GO TO 363
      SE(N,M)=SS
      SEP(N,M)=SS
      SEN(N,M)=SS
      GO TO 363
368  CONTINUE
      SET=SEP(NN,M)+SEP(NNN,M)-VAP
      STP =SE(NN,M)+SE(NNN,M) -VAP
      IF(STP.LT.SET) SET=STP
      IF (SET.LT.0.0) GO TO 363
      DRY=H(NN,M)+H(NN,MM) +SS+SEP(NN,M)
      IF (DRY.LT.0.) GO TO 363
      DRY=H(N,M)+H(N,MM) +SS+SEP(NNN,M)
      IF (DRY.LT.0.) GO TO 363
```

1

```
SE(N,M)=SS
SEP(N,M)=SS
SEN(N,M)=SS
GO TO 363
370 CONTINUE
SET=(SEP(NN,M)+SEP(N,MMM)+SEP(N,MM))*2./3.-VAP
IF (SET.LT.0.0) GO TO 363
DRY=H(NN,M)+H(NN,MM)+SS +SEP(NN,M)
IF (DRY.LT.0.) GO TO 363
DRY=H(N,M)+H(NN,M)+SS+SEP(N,MMM)
IF (DRY.LT.0.) GO TO 363
DRY=H(N,MM)+H(NN,MM)+SS +SEP(N,MM)
IF (DRY.LT.0.) GO TO 363
SE(N,M)=SS
SEP(N,M)=SS
SEN(N,M)=SS
GO TO 363
371 CONTINUE
SET=SEP(NN,M)+SEP(N,MM)-VAP
IF (SET.LT.0.0) GO TO 363
DRY=H(NN,MM)+H(NN,M)+SS+SEP(NN,M)
IF (DRY.LT.0.) GO TO 363
DRY=H(NN,MM)+H(N,MM)+SS+SEP(N,MM)
IF (DRY.LT.0.) GO TO 363
SE(N,M)=SS
SEP(N,M)=SS
SEN(N,M)=SS
GO TO 363
372 CONTINUE
SET=SEP(NN,M)+SEP(N,MMM)-VAP
IF (SET.LT.0.0) GO TO 363
DRY=H(NN,MM)+H(NN,M)+SS+SEP(NN,M)
IF (DRY.LT.0.) GO TO 363
DRY=H(NN,M)+H(N,M)+SS+SEP(N,MMM)
IF (DRY.LT.0.) GO TO 363
SE(N,M)=SS
SEP(N,M)=SS
SEN(N,M)=SS
GO TO 363
374 CONTINUE
C ALL 4 POINTS WATER
SET=(SEP(NNN,M)+SEP(NN,M)+SEP(N,MMM)+SEP(N,MM))/2.-VAP
IF (SET.LT.0.0) GO TO 363
DRY=H(NN,MM)+H(NN,M)+SS+SEP(NN,M)
IF (DRY.LT.0.) GO TO 363
DRY=H(NN,M)+H(N,M)+SS+SEP(N,MMM)
IF (DRY.LT.0.) GO TO 363
DRY=H(NN,MM)+H(N,MM)+SS+SEP(N,MM)
IF (DRY.LT.0.) GO TO 363
DRY=H(N,M)+H(N,MM)+SS+SEP(NNN,M)
IF (DRY.LT.0.) GO TO 363
SE(N,M)=SS
SEP(N,M)=SS
SEN(N,M)=SS
GO TO 363
375 CONTINUE
SET=(SEP(NNN,M)+SEP(NN,M)+SEP(N,MM))*2./3.-VAP
IF (SET.LT.0.0) GO TO 363
DRY=H(N,M)+H(N,MM)+SS+SEP(NNN,M)
IF (DRY.LT.0.) GO TO 363
DRY=H(NN,MM)+H(NN,M)+SS+SEP(NN,M)
IF (DRY.LT.0.) GO TO 363
DRY=H(NN,MM)+H(N,MM)+SS+SEP(N,MM)
IF (DRY.LT.0.) GO TO 363
```

1

```
SE(N,M)=SS
SEP(N,M)=SS
SEN(N,M)=SS
GO TO 363
376 CONTINUE
SET=(SEP(NNN,M)+SEP(NN,M)+SEP(N,MMM))*2./3.-VAP
IF (SET.LT.0.0) GO TO 363
DRY=H(N,M)+H(N,MM)+SS+SEP(NNN,M)
IF (DRY.LT.0.) GO TO 363
DRY=H(NN,M)+H(NN,MM)+SS+SEP(NN,M)
IF (DRY.LT.0.) GO TO 363
DRY=H(N,M)+H(NN,M)+SS+SEP(N,MMM)
IF (DRY.LT.0.) GO TO 363
SE(N,M)=SS
SEP(N,M)=SS
SEN(N,M)=SS
GO TO 363
380 CONTINUE
ST=SE(N,MMM)
STP=SEP(N,MMM)
IF (ST.LT.STP) STP=ST
SET=STP+STP-VAP
IF (SET.LT.0.0) GO TO 363
DRY=H(N,M)+H(NN,M)+SS+SEP(N,MMM)
IF (DRY.LT.0.0) GO TO 363
SE(N,M)=SS
SEP(N,M)=SS
SEN(N,M)=SS
GO TO 363
381 CONTINUE
ST=SE(N,MM)
STP=SEP(N,MM)
IF (ST.LT.STP) STP=ST
SET=STP+STP-VAP
IF (SET.LT.0.0) GO TO 363
DRY=H(N,MM)+H(NN,MM)+SS+SEP(N,MM)
IF (DRY.LT.0.0) GO TO 363
SE(N,M)=SS
SEP(N,M)=SS
SEN(N,M)=SS
GO TO 363
382 CONTINUE
SET= SEP(N,MM)+SEP(N,MMM) -VAP
STP =SE(N,MM)+SE(N,MMM) -VAP
IF (STP.LT.SET) SET=STP
IF (SET.LT.0.0) GO TO 363
DRY=H(NN,MM)+H(N,MM)+SS+SEP(N,MM)
IF (DRY.LT.0.) GO TO 363
DRY=H(NN,M)+H(N,M)+SS+SEP(N,MMM)
IF (DRY.LT.0.) GO TO 363
SE(N,M)=SS
SEP(N,M)=SS
SEN(N,M)=SS
GO TO 363
386 CONTINUE
SET=(SEP(NNN,M)+SEP(N,MM)+SEP(N,MMM))*2./3.-VAP
IF (SET.LT.0.0) GO TO 363
DRY=H(N,M)+H(N,MM)+SS+SEP(NNN,M)
IF (DRY.LT.0.) GO TO 363
DRY=H(NN,MM)+H(N,MM)+SS+SEP(N,MM)
IF (DRY.LT.0.) GO TO 363
DRY=H(NN,M)+H(N,M)+SS+SEP(N,MMM)
IF (DRY.LT.0.) GO TO 363
SE(N,M)=SS
```



```
1      SEP(N,M)=SS
      SEN(N,M)=SS
      GO TO 363
384    CONTINUE
      SET=SEP(NNN,M)+SEP(N,MM)-VAP
      STP =SE(NNN,M)+SE(N,MM)-VAP
      IF(STP.LT.SET) SET=STP
      IF (SET.LT.0.0) GO TO 363
      DRY=H(N,M)+H(N,MM)+SS+SEP(NNN,M)
      IF(DRY.LT.0.) GO TO 363
      DRY=H(NN,MM)+H(N,MM)+SS+SEP(N,MM)
      IF(DRY.LT.0.) GO TO 363
      SE(N,M)=SS
      SEP(N,M)=SS
      SEN(N,M)=SS
      GO TO 363
385    CONTINUE
      SET=SEP(NNN,M)+SEP(N,MMM)-VAP
      STP =SE(NNN,M)+SE(N,MMM)-VAP
      IF(STP.LT.SET) SET=STP
      IF (SET.LT.0.0) GO TO 363
      DRY=H(N,M)+H(N,MM)+SS+SEP(NNN,M)
      IF(DRY.LT.0.) GO TO 363
      DRY=H(NN,M)+H(N,M)+SS+SEP(N,MMM)
      IF(DRY.LT.0.) GO TO 363
      SE(N,M)=SS
      SEP(N,M)=SS
      SEN(N,M)=SS
      GO TO 363
363    CONTINUE
      RETURN
      END
```

```
1
SUBROUTINE SEPV
COMMON SE(61,78),SEP(61,78),V(61,78),VP(61,78),U(61,78),UP(61,78)
// DD DISP=OLD,DSN=N,N2640. .JAMCOM72
// DD *,DCB=BLKSIZE=80
M=2
111 CONTINUE
IF(M.EQ.MMAX) GO TO 110
MM=M-1
MMM=M+1
N=1
ST=SEP(N,M)
IF(ST.EQ.0.) GO TO 324
C WATERBOUND ONLY AT N=1
NF=2
NFF=NF-1
TEMP10=V(NFF,MMM)
IF(TEMP10.EQ.0.) TEMP10= V(NFF,MM)
TEMP11=V(NFF,MM)
IF(TEMP11.EQ.0.) TEMP11= V(NFF,MMM)
DELTA=0.5
BETA =1.
TEMP12 =SQRT(V(NFF,M)**2 +(((U(NF,M)+U(NF,MM))**2)/16.)) /
2(((SE(NFF,M)+SE(NF,M)+ H(NFF,M) +H(NFF,MM))**((C(NFF,M)+C(NF,M))
3**2))*C4
RX(NFF)=C1/(1.+C2*(V(NF,M)-V(NFF,M))*(1.-BETA)*2.0+TEMP12)
S(NFF)=(V(NFF,M)+C1*SEP(NFF,M)-C1*(SEN(NF,M)-SEN(NFF,M))
1-V(NFF,M)*TEMP12
3 -0.5*(AT* F(N) + (1.-DELTA)*C2*(TEMP10-V(NFF,M))
4+DELTA *C2*(V(NFF,M)- TEMP11))*(U(NF,M)+ U(NF,MM)))/
5(1.+C2*(1.-BETA) *(V(NF,M)- V(NFF,M))*2.0+TEMP12)
N=N+1
GO TO 323
321 CONTINUE
RX(N)=0.0
S(N)=0.
N=N+1
322 CONTINUE
P(N)=0.
Q(N)=0.
IF(N.EQ.NMAXN) GO TO 350
324 CONTINUE
RX(N)=0.0
S(N)=0.
N=N+1
CE=C(N,M)
IF(CE.EQ.0.) GO TO 322
323 CONTINUE
NNN=N+1
NN=N-1
HUL=H(N,MM)+H(NN,MM)+SE(N,M)+SE(N,MM)
HVT=H(N,M)+ H(N,MM)+SE(N,M) +SE(NNN,M)
HVB=H(NN,M)+H(NN,MM)+SE(N,M)+SE(NN,M)
HUR=H(N,M)+ H(NN,M) +SE(N,M)+SE(N,MMM)
TEMP2=1.+ .5*C2*HVB*RX(NN)
A(N)=SE(N,M)+.5*C2*(HUL*U(N,MM) - HUR* U(N,M))
P(N)=.5*C2*HVT/TEMP2
Q(N)=(A(N)+ .5*C2*HVB*S(NN))/TEMP2
IF(N.EQ.NMAXN) GO TO 350
CE=C(NNN,M)
IF(CE.EQ.0.) GO TO 321
DELTA = 0.5
TEMP10=V(N,MMM)
IF(TEMP10.EQ.0.) TEMP10 = V(N,MM)
```

```
TEMP11=V(N,MM)
IF(TEMP11.EQ.0.) TEMP11 = V(N,MMM)
TEMP6 =AT*F(N)+(1.-DELTA)*C2*(TEMP10-V(N,M))
1 +DELTA*C2*(V(N,M)-TEMP11)
TEMP6 = 0.5*TEMP6
TEMP7 = SQRT (V(N,M)**2 +(((U(N,M)+ U(NNN,M) +U(N,MM)+ U(NNN,M
2M))**2)/16.)) / (HVT*((C(N,M)+C(NNN,M))**2))*C4
B(N) = V(N,M) -TEMP6 *(U(N,M) + U(NNN,M) +U(NNN,MM)+U(N,MM))
1- V(N,M) * TEMP7-C1*(SEN(NNN,M)-SEN(N,M))-WINDV/HVT
BETA = 0.5
TEMP1 =1.+C2*(AG*P(N)+V(NNN,M)-V(NN,M))+TEMP7
RX(N)= C1/TEMP1
S(N)=(B(N)+ C1*Q(N))/TEMP1
N=N+1
GO TO 323
350 CONTINUE
VP(N,M)=0.
351 CONTINUE
112 CONTINUE
NN =N-1
SEP(N,M) = -P(N)*VP(N,M)+Q(N)
IF (C(N,M).EQ.0.0) GO TO 152
WET=H(N,M)+H(NN,M)+H(N,MM)+H(NN,MM)+SEP(N,M)*4.
IF(WET.LT.0.) GO TO 113
152 CONTINUE
VP(NN,M) =-RX(NN)*SEP(N,M)+S(NN)
306 N = N-1
IF(N.NE.1) GO TO 112
M=MMM
GO TO 111
113 C(N,M)=0.
SEP(N,M)=0.
V(N,M)=0.
V(NN,M)=0.
U(N,M)=0.
U(N,MM)=0.
SES(N,M)=SE(N,M)
SE(N,M)=0.
SEN(N,M)=0.
WRITE(6,115) NST,N,M,SES(N,M)
115 FORMAT(1X,4HNST=,14,2X,2HN=,13,2HM=,13,2X,4HSES=,F7.4,
*16HVOLUME NEG. SEPV)
M=MM
IF(M.EQ.1) M=2
GO TO 111
110 CONTINUE
310 CONTINUE
IF (MOD(NST,NSM0).NE.2) GO TO 191
DO 202 N=1,NMAX
DO 202 M=1,MMAX
SEP(N,M) =.5*(SEP(N,M)+SEN(N,M))
SE(N,M) =.5*(SE(N,M)+R(1,N,M))
VP(N,M) =.5*(VP(N,M)+V(N,M))
U(N,M) =.5*(U(N,M)+R(2,N,M))
202 CONTINUE
DO 192 IN2=1,NSRC
NY=NINT(IN2)
MY=MINT(IN2)
SE(NY,MY)=SE(NY,MY)+.5*AT*DISCH(IN2)
192 CONTINUE
191 CONTINUE
C*****
CALL DIFV
DO 174 IN2=1,NSRC
```

```
1      NY=NINT(IN2)
      MY=MINT(IN2)
      SE(NY,MY)=SE(NY,MY)-AT*DISCH(IN2)
174  CONTINUE
390  CONTINUE
      IF(MOD(NST ,NVGR).EQ.0) GO TO 1192
1193 CONTINUE
      DO 401 N=1,NMAX
      DO 401 M=1,MMAX
      SEN(N,M)=SE(N,M)
      SE(N,M)=SEP(N,M)
      V(N,M)=VP(N,M)
401  CONTINUE
      GO TO 1191
1192 CONTINUE
      IF(MOD(NST,NSMD).EQ.1) GO TO 1193
      DO 1401 N=1,NMAX
      DO 1401 M=1,MMAX
      STEMP=V(N,M)
      V(N,M)=VP(N,M)
      VP(N,M)=STEMP
      SEN(N,M)=SE(N,M)
      SE(N,M)=SEP(N,M)
1401 CONTINUE
1191 CONTINUE
      RETURN
      END
```

1

```
      SUBROUTINE OUT
      COMMON SE(61,78),SEP(61,78),V(61,78),VP(61,78),U(61,78),UP(61,78)
// DD DISP=OLD,DSN=N.N2640...      .JAMCOM72
// DD *.DCB=BLKSIZE=80
      2 FORMAT (16(1X,F7.3))
      3 FORMAT (1H0,8X,19HSECOND HALF OF STEP,16,4X,2HL=,11)
      5 FORMAT (1H1,8X,18HFIRST HALF OF STEP,16,4X,2HL=,11)
      6 FORMAT (1X,18A4)
C      GO TO 8200
      DO 8200 L=1,LMAX
      WRITE (6,5) NST,L
      WRITE (6,6) (POLT(L,J),J=1,15)
      WRITE (6,200)
      200 FORMAT (10X,'INCLUDING PROCESSES IN TIDAL FLATS')
      7110 FORMAT (1H0,5X,3HN= .13,2H .,13)
      WRITE (6,3) NST,L
      WRITE (6,6) (POLT(L,J),J=1,15)
      WRITE (6,200)
      NPR1=1
      NPR2=16
      1351 CONTINUE
      IF (NPR2.GT.NMAX) NPR2=NMAX
      WRITE (6,7110) NPR1,NPR2
      DO 100 M=1,MMAX
      100 WRITE(6,2) (R(L,N,M),N=NPR1,NPR2)
      NPR1=NPR2+1
      NPR2=NPR2+16
      IF (NPR1.LE.NMAX) GO TO 1351
      8200 CONTINUE
      5020 FORMAT(1H1,26HSE FOR SECOND HALF OF STEP 15)
      WRITE(6,5020) NST
      NPR1=1
      NPR2=32
      7100 CONTINUE
      IF (NPR2.GT.NMAX) NPR2=NMAX
      WRITE (6,7110) NPR1,NPR2
      DO 6000 M=1,MMAX
      DO 6006 N=NPR1,NPR2
      6006 NA(N)=SEN(N,M)*100.
      6000 WRITE(6,6001) M,( NA(N),N=NPR1,NPR2)
      NPR1=NPR2+1
      NPR2=NPR2+32
      IF (NPR1.LE.NMAX) GO TO 7100
      6001 FORMAT(1H .12,1X,3214)
      WRITE(6,7020) NST
      7020 FORMAT(1H1,27HSEP FOR SECOND HALF OF STEP 15)
      NPR1=1
      NPR2=32
      7101 CONTINUE
      IF (NPR2.GT.NMAX) NPR2=NMAX
      WRITE (6,7110) NPR1,NPR2
      DO 7000 M=1,MMAX
      DO 7006 N=NPR1,NPR2
      7006 NA(N)=SEP(N,M)*100.
      7000 WRITE(6,6001) M,( NA(N),N=NPR1,NPR2)
      NPR1=NPR2+1
      NPR2=NPR2+32
      IF (NPR1.LE.NMAX) GO TO 7101
C      GO TO 8201
      5021 FORMAT(1H1,41HAVERAGED V AND VP FOR SECOND HALF OF STEP 15)
      WRITE(6,5021) NST
      NPR1=1
      NPR2=32
```

```
1 7102 CONTINUE
      IF (NPR2.GT.NMAX) NPR2=NMAX
      WRITE (6,7110) NPR1,NPR2
      DO 6003 M=1,MMAX
      DO 6007 N=NPR1,NPR2
6007      NA(N)=VP(N,M)*100.
6003 WRITE(6,6001) M,(      NA(N),N=NPR1,NPR2)
      NPR1=NPR2+1
      NPR2=NPR2+32
      IF (NPR1.LE.NMAX) GO TO 7102
5022 FORMAT(1H1,41HAVERAGED U AND UP FOR SECOND HALF OF STEP 15)
      WRITE(6,5022) NST
      NPR1=1
      NPR2=32
7103 CONTINUE
      IF (NPR2.GT.NMAX) NPR2=NMAX
      WRITE (6,7110) NPR1,NPR2
      DO 6004 M=1,MMAX
      DO 6008 N=NPR1,NPR2
6008      NA(N)=U(N,M)*100.
6004 WRITE(6,6001) M,(      NA(N),N=NPR1,NPR2)
      NPR1=NPR2+1
      NPR2=NPR2+32
      IF (NPR1.LE.NMAX) GO TO 7103
8201 CONTINUE
      WRITE (6,8000) (L,L=1,LMAX)
8000 FORMAT (1H0,4X,1HM,4X,1HN,4X,
      *           2HSE,5X,3HSEN,5X,3HSEP,7X,1HU,7X,1HV,
      *           6X,1HR,6(11,7X))
8050 FORMAT (1X,2I5,11(1X,F7.4))
      DO 8100 K=1,KPOL
      M=MPOL(K)
      N=NPOL(K)
      WRITE (6,8050) M,N,
      *           SE(N,M),SEN(N,M),SEP(N,M),U(N,M),VP(N,M),
      *           (R(L,N,M),L=1,LMAX)
8100 CONTINUE
      RETURN
      END
```

```
1
SUBROUTINE FLOW
COMMON SE(61,78),SEP(61,78),V(61,78),VP(61,78),U(61,78),UP(61,78)
// DD DISP=OLD,DSN=N.N2640. JAMCOM72
// DD *,DCB=BLKSIZE=80
DO 820 I=1,NTRA
M=MIT(I)
N1=NIT1(I)
N2=NIT2(I)
DO 810 N=N1,N2
IF (C(N,M).EQ.0.0) GO TO 810
IF (C(N,M+1).EQ.0.0) GO TO 810
STEMP=.5*(SE(N,M)+SEP(N,M)+SE(N,M+1)+SEP(N,M+1))
HTEMP=AT*UP(N,M)*(H(N,M)+H(N-1,M)+STEMP)*AL
FLTR(I)=FLTR(I)+HTEMP
TCR=H(N-1,M)+H(N,M)+SEP(N,M)+SEP(N,M+1)
DX1=CDAL*ABS(UP(N,M))*TCR/(C(N,M)+C(N,M+1))*AL
*
+DIFCO(N,M)+DIFCO(N,M+1)
DO 1 L=1,LMAX
RP1=RP(L,N,M)
RP2=RP(L,N,M+1)
ATR(L,I)=ATR(L,I)+HTEMP*(RP1+RP2)*.5
DTR(L,I)=DTR(L,I)+DX1*(RP1-RP2)*TCR*AT*.5
CTR(L,I)=DTR(L,I)+ATR(L,I)
1 CONTINUE
810 CONTINUE
820 CONTINUE
DO 700 I=1,NOWL
M=MWL(I)
N=NWL(I)
ZWL(I)=(SEN(N,M)+SE(N,M)+SEP(N,M))/3.0
700 CONTINUE
DO 710 I=1,NOCUR
M=MC(I)
N=NC(I)
ZCUR(I)=.25*SQRT((U(N,M)+UP(N,M)+U(N,M-1)+UP(N,M-1))*2
*
+(VP(N,M)+VP(N,M)+VP(N-1,M)+VP(N-1,M))*2)
710 CONTINUE
IF (MOD(NST,NWLC).NE.0) GO TO 780
WRITE (6,720) NST
720 FORMAT (1H1,5X,5HTIME=,15/1H0,3X,1HM,4X,1HN,5X,2HWL)
WRITE (6,730) ((MWL(I),NWL(I),ZWL(I)),I=1,NOWL)
730 FORMAT (1X,14,1X,14,2X,F7.4)
WRITE (6,740)
740 FORMAT (1H0,3X,1HM,4X,1HN,2X,7HCURRENT)
WRITE (6,730) ((MC(I),NC(I),ZCUR(I)),I=1,NOCUR)
WRITE (6,830)
830 FORMAT (2H0 ,3HLOC,4X,9HTRANSPORT)
DO 835 I=1,NTRA
WRITE (6,840) BIT(I),FLTR(I)
WRITE (6,845) (ATR(L,I),L=1,LMAX)
WRITE (6,845) (DTR(L,I),L=1,LMAX)
WRITE (6,845) (CTR(L,I),L=1,LMAX)
835 CONTINUE
780 IF (MOD(NST,NWLT).NE.0) GO TO 790
DO 2 K=1,KPOL
M=MPOL(K)
N=NPOL(K)
DO 3 L=1,LMAX
GRO(L,K)=(1.0-GAMM)*RP(L,N,M)+.25*GAMM*(RP(L,N,M+1)+RP(L,N,M-1)
*
+RP(L,N+1,M)+RP(L,N-1,M))
3 CONTINUE
2 CONTINUE
WRITE (9) NST,FLTR,ATR,DTR,CTR,ZWL,ZCUR,GRO
```

```
1 790 CONTINUE  
   RETURN  
   840 FORMAT (1X,A4,1X,E12.5)  
   845 FORMAT (5X,6(1X,E12.5))  
   END
```


1

```
SUBROUTINE DIFU
COMMON SE(61,78),SEP(61,78),V(61,78),VP(61,78),U(61,78),UP(61,78)
// DD DISP=OLD,DSN=N.N2640. JAMCOM72
// DD *,DCB=BLKSIZE=80
IS=0
DO 80 N=NB1,NB2
J=N-NB1+1
IF (UP(N,1).LT.0.0) GO TO 70
IF (NFLI(J).LT.NFL) GO TO 60
DO 500 L=1,LMAX
500 DFL(L,J)=(R(L,N,1)-RBND(L))
60 NFLI(J)=NFLI(J)-1
ASFL=NFLI(J)
ASFL=ASFL*3.1416
AST=(COS(ASFL/AFL)-1.0)*.5
DO 505 L=1,LMAX
505 RP(L,N,1)=RBND(L)-DFL(L,J)*AST
IF (NFLI(J).GT.0) GO TO 65
DO 510 L=1,LMAX
510 RP(L,N,1)=RBND(L)
65 CONTINUE
GO TO 80
70 NFLI(J)=NFL
DO 515 L=1,LMAX
515 RP(L,N,1)=R(L,N,1)-ATAL*UP(N,1)*(R(L,N,2)-R(L,N,1))
80 CONTINUE
90 CONTINUE
DO 300 N=2,NMAXN
CZ00=CZ(N,1)
DO 520 L=1,LMAX
E(L,2)=0.0
FX(L,2)=0.0
IF (CZ00.NE.0.0) FX(L,2)=RP(L,N,1)
520 CONTINUE
M=2
MMM=3
CZ00=CZ(N,M)
IF(CZ00.EQ.0.) GO TO 122
GO TO 123
121 CONTINUE
M=MMM
MMM=M+1
IF (M.EQ.MMAX) GO TO 150
122 CONTINUE
AX(M)=0.0
CX(M)=0.0
VOLD=.25*(H(N,M)+H(N,M-1)+H(N-1,M)+H(N-1,M-1))+SES(N,M)
VOLDP(M)=VOLD
VOLDM(M)=VOLD
DO 525 L=1,LMAX
BZ(L,M)=VOLD
PZ(L,M)=VOLD*R(L,N,M)
525 CONTINUE
124 CONTINUE
M=MMM
MMM=M+1
IF (M.EQ.MMAX) GO TO 150
CZ00=CZ(N,M)
IF(CZ00.EQ.0.) GO TO 122
123 CONTINUE
CZ00=CZ(N,M)
CZ01=CZ(N,M-1)
CZ02=CZ(N,M+1)
```

```
1      CZ20=C(N+1,M)
      CZ10=C(N-1,M)
      SP00=SEP(N,M)
      S00=SE(N,M)
      S20=SE(N+1,M)
      S10=SE(N-1,M)
      SP02=SEP(N,M+1)
      SP01=SEP(N,M-1)
      SP20=SEP(N+1,M)
      SP10=SEP(N-1,M)
      S02=SE(N,M+1)
      S01=SE(N,M-1)
      IF(CZ02.NE.0.) GO TO 20
      SP02=SP00
      S02=S00
20     CONTINUE
      IF(CZ01.NE.0.) GO TO 21
      SP01=SP00
      S01=S00
21     CONTINUE
      IF(CZ20.NE.0.) GO TO 22
      SP20=SP00
      S20=S00
22     CONTINUE
      IF(CZ10.NE.0.) GO TO 23
      SP10=SP00
      S10=S00
23     CONTINUE
      H00=H(N,M)
      H01=H(N,M-1)
      H10=H(N-1,M)
      H11=H(N-1,M-1)
      U00=UP(N,M)
      U01=UP(N,M-1)
      V00=V(N,M)
      V10=V(N-1,M)
      VAT=ATAL2*V10
      VAL=ATAL2*V00
      G3=(H00+H10+H01+H11)/4.0
      C3B=G3+SP00
      C6=H00+H10+S00+S02
      C7=H01+H11+S00+S01
      C8=H00+H10+SP00+SP02
      C9=H01+H11+SP00+SP01
      C10=H00+H01+SP00+SP20
      C11=H10+H11+SP00+SP10
      IF(C8.LT.0.) GO TO 400
      IF(C9.LT.0.) GO TO 400
      IF(C10.LT.0.) GO TO 400
      IF(C11.LT.0.) GO TO 400
401    CONTINUE
      G1=ATL*C7
      G1A=ATL*C9
      G2=ATL*C6
      G2A=ATL*C8
      C3P=G3+S00
      G4=H00+H01+S00+S20
      C5=H10+H11+S00+S10
      VOLDP(M)=C3B
      VOLDM(M)=C3P
      DIFA=DIFCO(N,M)
      DX00=CDAL*ABS(U00)*C8/(CZ00+CZ02)+(DIFA+DIFCO(N,M+1))/AL
      DX01=CDAL*ABS(UP(N,M-1))*C9/(CZ00+CZ01)+(DIFA+DIFCO(N,M-1))/AL
      DY00=CDAL*ABS(V00)*G4/(CZ00+CZ(N+1,M))+DIFA+DIFCO(N+1,M))/AL
```

```
1      DY10=CDAL*ABS(V(N-1,M))*C5/(CZ00+CZ(N-1,M))+(DIFA+DIFCO(N-1,M))/AL
      IF (CZ01.EQ.0.0) DX01=0.0
      IF (CZ02.EQ.0.0) DX00=0.0
      IF (CZ10.EQ.0.0) DY10=0.0
      IF (CZ20.EQ.0.0) DY00=0.0
      O1=1.0
      O2=1.0
      O3=1.0
      O4=1.0
      DO 530 L=1,LMAX
      R1(L)=R(L,N-1,M)
      R2(L)=R(L,N,M)
      R3(L)=R(L,N,M)
      R4(L)=R(L,N+1,M)
      SX(L)=0.0
530    CONTINUE
C****
      DO 8400 K=1,NSRC
      NIN=NINT(K)
      MIN=MINT(K)
      IF (N.NE.NIN) GO TO 8240
      IF (M.NE.MIN) GO TO 8200
      DO 535 L=1,LMAX
535    SX(L)=SINT(L,K)
      C3P=C3P-AT*DISCH(K)
8000   IF (U00.GT.0.0) GO TO 8020
      IF (U01.GT.0.0) GO TO 8010
      O2=2.0
      O3=0.0
      GO TO 8100
8010   O1=2.0
      O2=2.0
      O3=0.0
      O4=0.0
      GO TO 8100
8020   IF (U01.LT.0.0) GO TO 8100
      O1=2.0
      O4=0.0
8100   IF (V00.LT.0.0) GO TO 8120
      IF (V10.LT.0.0) GO TO 8400
      DO 540 L=1,LMAX
540    R2(L)=R1(L)
      GO TO 8400
8110   CONTINUE
      DO 545 L=1,LMAX
      R2(L)=R1(L)
      R3(L)=R4(L)
545    CONTINUE
      GO TO 8400
8120   IF (V10.GT.0.0) GO TO 8110
      DO 550 L=1,LMAX
550    R3(L)=R4(L)
      GO TO 8400
8200   IF (M.NE.MIN+1) GO TO 8220
8210   IF (U01.GT.0.0) GO TO 8400
      O1=0.0
      O4=2.0
      GO TO 8400
8220   IF (M.NE.MIN-1) GO TO 8400
8230   IF (U00.LT.0.0) GO TO 8400
      O2=0.0
      O3=2.0
      GO TO 8400
8240   IF (M.NE.MIN) GO TO 8400
```

```
1      IF (N.NE.NIN+1) GO TO 8260
8250  IF (V10.GT.0.0) GO TO 8400
      DO 555 L=1,LMAX
      555  R1(L)=R2(L)
      GO TO 8400
8260  IF (N.NE.NIN-1) GO TO 8400
8270  IF (V00.LT.0.0) GO TO 8400
      DO 560 L=1,LMAX
      560  R4(L)=R3(L)
8400  CONTINUE
      IF (M.NE.2) GO TO 8401
      IF (U01.GE.0.0) GO TO 8401
      O1=0.0
      O4=2.0
8401  CONTINUE
      AX(M)=-G1*ZC1*U01*O1-G1A*DX01
      CX(M)=G2*ZC1*U00*O2-G2A*DX00
      DO 570 L=1,LMAX
      BZ(L,M)=C3B          +G2*ZC1*U00*O3+G2A*DX00-G1*ZC1*U01*O4+G1A*DX01
      PZ(L,M)=C3P          *R(L,N,M)-AT*SX(L)
      *  +ATL*(C5*(ZC2*V10*(R1(L)+R2(L))-(R(L,N,M)-R(L,N-1,M)))*DY10)
      *  -G4*(ZC2*V00*(R3(L)+R4(L))+(R(L,N,M)-R(L,N+1,M))*DY00))
570  CONTINUE
      IF (CZ02.EQ.0.) GO TO 121
      M=MMM
      MMM=M+1
      IF (M.EQ.MMAX) GO TO 150
      GO TO 123
150  CONTINUE
```

C
C
C

REACTION MODEL

```
DO 201 L=1,LMAX
DO 575 M=2,MMAXM
MMM=M+1
TEM=0.0
RTEM=R(L,N,M)
IF (L.GT.LRMX) GO TO 6
IF (L.EQ.1) GO TO 1
LJM=L-1
DO 2 LJ=1,LJM
IF (LJ.GT.LRMX) GO TO 3
RTEM=RP(LJ,N,M)
IF (RTEM.LE.0.0) GO TO 2
AKF=AKK(L,LJ)
IF ((RTEM.LE.0.0).AND.(AKF.GE.0.0)) GO TO 2
TEM=TEM+AKF*RTEM*VOLDP(M)
2 CONTINUE
1 CONTINUE
IF (L.EQ.LMAX) GO TO 3
LJM=L+1
DO 4 LJ=LJM,LMAX
IF (LJ.GT.LRMX) GO TO 3
RTEM=R(LJ,N,M)
IF (RTEM.LE.0.0) GO TO 4
AKF=AKK(L,LJ)
IF ((RTEM.LE.0.0).AND.(AKF.GE.0.0)) GO TO 4
TEM=TEM+AKF*RTEM*VOLDM(M)
4 CONTINUE
3 CONTINUE
IF (L.NE.LOX) GO TO 6
AKF=ROX(N,M)
TEM=TEM-AKF*(SOX-.5*RTEM)
TEMM=.5*AKF*AT
```

```
1
GO TO 7
6 CONTINUE
AKF=.5*AKK(L,L)
TEM = TEM +AKF*VOLDM(M)*RTEM1
TEMM=AKF *VOLDP(M)*AT
7 CONTINUE
D1=BZ(L,M)+AX(M)*E(L,M)+TEMM
FX(L,MMM)=(PZ(L,M)-TEM*AT-AX(M)*FX(L,M))/D1
E(L,MMM)=-CX(M)/D1
575 CONTINUE
M=MMAX
DO 200 J=2,MMAX
MM=M-1
RP(L,N,MM)=E(L,M)*RP(L,N,M)+FX(L,M)
M=MM
200 CONTINUE
IF(NST.GT.2) GO TO 210
IF(L.GT.2) GO TO 210
IF(N.LT.2) GO TO 210
IF(N.GT.5) GO TO 210
WRITE(6,211) NST,L,N
211 FORMAT(1X,3I5)
DO 212 MX=15,17
WRITE(6,213) BZ(L,MX),PZ(L,MX),AX(MX),CX(MX),FX(L,MX),E(L,MX),
*ROX(N,MX),RP(L,N,MX),R(L,N,MX),SES(N,MX),SE(N,MX),SEP(N,MX)
212 CONTINUE
210 CONTINUE
213 FORMAT(1X,1P12E10.3)
201 CONTINUE
300 CONTINUE
GO TO 404
400 CONTINUE
IF(C8.LT.0.) C8=0.
IF(C9.LT.0.) C9=0.
IS=IS+1
NVOL(IS)=N
MVOL(IS)=M
IF(C3B.GT.0.) GO TO 402
STA=.25*VAR -G3
WATADD= (STA-SEP(N,M))*AL*AL
S21=S21+WATADD
WRITE(6,403) NST,M,N,STA,SEP(N,M),WATADD,S21
403 FORMAT (1X,4HNST=,I5,2X,2HM=,I3,2X,2HN=,I3,2X,4HSET=,F7.4,
*2X,4HSEP=,F7.4,2X,7HWATADD=,F10.2,2X,4HCUM=,E13.6,2X,4HDIFU)
SEP(N,M)=STA
402 CONTINUE
GO TO 401
404 CONTINUE
IF(IS.LT.1) GO TO 405
DO 406 IST=1,IS
N=NVOL(IST)
M=MVOL(IST)
C(N,M)=0.
SES(N,M)=SEP(N,M)
SEP(N,M)=0.
SE(N,M)=0.
SEN(N,M)=0.
U(N,M)=0.
UP(N,M)=0.
UP(N,M-1)=0.
U(N,M-1)=0.
V(N,M)=0.
V(N-1,M)=0.
406 CONTINUE
```

1 405 CONTINUE
RETURN
END

1

```
      SUBROUTINE DIFV
C
C*****
C*****
C
C COMMON IS SHUFFLED IN THIS SUBROUTINE
C THIS IS THE USUAL COMMON
C   COMMON SE(61,78),SEP(61,78),V(61,78),VP(61,78),U(61,78),UP(61,78)
C THIS IS THE COMMON USED IN THIS SUBROUTINE
C   COMMON SEP(61,78),SE(61,78),VP(61,78),V(61,78),UP(61,78),U(61,78)
C
C*****
C*****
// DD DISP=OLD,DSN=N.N2640.      .JAMCOM72
// DD *,DCB=BLKSIZE=80
C
      IS=0
      DO 380 N=NB1,NB2
      J=N-NB1+1
      IF (UP(N,1).LT.0.0) GO TO 370
      IF (NFLI(J).LT.NFL) GO TO 360
      DO 500 L=1,LMAX
500 DFL(L,J)=(R(L,N,1)-RBND(L))
360 NFLI(J)=NFLI(J)-1
      ASFL=NFLI(J)
      ASFL=ASFL*3.1416
      AST=(COS(ASFL/AFL)-1.0)*.5
      DO 505 L=1,LMAX
505 R(L,N,1)=RBND(L)-DFL(L,J)*AST
      IF (NFLI(J).GT.0) GO TO 380
      DO 510 L=1,LMAX
510 RP(L,N,1)=RBND(L)
      GO TO 380
370 NFLI(J)=NFL
      DO 515 L=1,LMAX
515 R(L,N,1)=RP(L,N,1)-ATAL*UP(N,1)*(RP(L,N,2)-RP(L,N,1))
380 CONTINUE
390 CONTINUE
      DO 900 M=2,MMAXM
      CZ00=CZ(1,M)
      DO 520 L=1,LMAX
      E(L,2)=0.0
520 FX(L,2)=0.0
      N=2
      NNN=3
      CZ00=CZ(N,M)
      IF (CZ00.EQ.0.) GO TO 122
      GO TO 123
121 CONTINUE
      N=NNN
      NNN=N+1
      IF (N.EQ.NMAX) GO TO 150
122 CONTINUE
      AX(N)=0.0
      CX(N)=0.0
      VOLD=.25*(H(N,M)+H(N,M-1)+H(N-1,M)+H(N-1,M-1))+SES(N,M)
      VOLDP(N)=VOLD
      VOLDM(N)=VOLD
      DO 525 L=1,LMAX
      BZ(L,N)=VOLD
      PZ(L,N)=VOLD*RP(L,N,M)
525 CONTINUE
124 CONTINUE
```

```
1      N=NNN
      NNN=N+1
      IF (N.EQ.NMAX) GO TO 150
      CZ00=CZ(N,M)
      IF (CZ00.EQ.0.) GO TO 122
123   CONTINUE
      CZ00=CZ(N,M)
      CZ10=CZ(N-1,M)
      CZ20=CZ(N+1,M)
      CZ01=C(N,M-1)
      CZ02=C(N,M+1)
      SP00=SEP(N,M)
      S00=SE(N,M)
      S02=SE(N,M+1)
      S01=SE(N,M-1)
      S20=SE(N+1,M)
      S10=SE(N-1,M)
      SP02=SEP(N,M+1)
      SP01=SEP(N,M-1)
      SP20=SEP(N+1,M)
      SP10=SEP(N-1,M)
      IF (CZ02.NE.0.) GO TO 920
      SP02=SP00
      S02=S00
920   CONTINUE
      IF (CZ01.NE.0.) GO TO 21
      SP01=SP00
      S01=S00
21    CONTINUE
      IF (CZ20.NE.0.) GO TO 22
      SP20=SP00
      S20=S00
22    CONTINUE
      IF (CZ10.NE.0.) GO TO 23
      SP10=SP00
      S10=S00
23    CONTINUE
      H00=H(N,M)
      H01=H(N,M-1)
      H10=H(N-1,M)
      H11=H(N-1,M-1)
      V00=V(N,M)
      V10=V(N-1,M)
      U00=UP(N,M)
      U01=UP(N,M-1)
      UAT=ATAL2*U01
      UAL=ATAL2*U00
      G3=(H00+H10+H01+H11)/4.0
      C3B=G3+S00
      C6=H00+SP00+H01+SP20
      C7=H10+H11+SP00+SP10
      C8=H00+H01+S00+S20
      C9=H10+H11+S00+S10
      C10=H00+H10+S00+S02
      C11=H01+H11+S00+S01
      IF (C8.LT.0.) GO TO 400
      IF (C9.LT.0.) GO TO 400
      IF (C10.LT.0.) GO TO 400
      IF (C11.LT.0.) GO TO 400
401   CONTINUE
      G1=ATL*C7
      G1A=ATL*C9
      G2=ATL*C6
      G2A=ATL*C8
```


1

```
C3P=G3+SP00
G4=H00+H10+SP00+SEP(N,M+1)
C5=H01+H11+SP00+SEP(N,M-1)
VOLDP(N)=C3P
VOLDM(N)=C3B
DIFA=DIFCO(N,M)
DX00=CDAL*ABS(U00)*G4/(CZ00+CZ(N,M+1))+(DIFA+DIFCO(N,M+1))/AL
DX01=CDAL*ABS(UP(N,M-1))*C5/(CZ00+CZ(N,M-1))
*      +(DIFA+DIFCO(N,M-1))/AL
DY00=CDAL*ABS(V00)*C8/(CZ00+CZ20)+(DIFA+DIFCO(N+1,M))/AL
DY10=CDAL*ABS(V(N-1,M))*C9/(CZ00+CZ10)+(DIFA+DIFCO(N-1,M))/AL
IF (C(N-1,M).EQ.0.0) DY10=0.0
IF (C(N+1,M).EQ.0.0) DY00=0.0
IF (C(N,M-1).EQ.0.0) DX01=0.0
IF (C(N,M+1).EQ.0.0) DX00=0.0
O1=1.0
O2=1.0
O3=1.0
O4=1.0
DO 530 L=1,LMAX
R1(L)=RP(L,N,M-1)
R2(L)=RP(L,N,M)
R3(L)=RP(L,N,M)
R4(L)=RP(L,N,M+1)
SX(L)=0.0
20  CONTINUE
530 CONTINUE
C****
DO 8900 K=1,NSRC
NIN=NINT(K)
MIN=MINT(K)
IF (M.NE.MIN) GO TO 8740
IF (N.NE.NIN) GO TO 8700
DO 535 L=1,LMAX
535 SX(L)=SINT(L,K)
C3P=C3P-AT*DISCH(K)
8500 IF (V00.LT.0.0) GO TO 8520
IF (V10.LT.0.0) GO TO 8600
O1=2.0
O4=0.0
GO TO 8600
8510 O1=2.0
O2=2.0
O3=0.0
O4=0.0
GO TO 8600
8520 IF (V10.GT.0.0) GO TO 8510
O2=2.0
O3=0.0
8600 IF (U00.GT.0.0) GO TO 8620
IF (U01.GT.0.0) GO TO 8610
DO 540 L=1,LMAX
540 R3(L)=R4(L)
GO TO 8900
8610 CONTINUE
DO 545 L=1,LMAX
R2(L)=R1(L)
R3(L)=R4(L)
545 CONTINUE
GO TO 8900
8620 IF (U01.LT.0.0) GO TO 8900
DO 550 L=1,LMAX
550 R2(L)=R1(L)
GO TO 8900
```

```
1 8700 IF (N.NE.NIN+1) GO TO 8720
8710 IF (V10.GT.0.0) GO TO 8900
      O1=0.0
      O4=2.0
      GO TO 8900
8720 IF (N.NE.NIN-1) GO TO 8900
8730 IF (V00.LT.0.0) GO TO 8900
      O2=0.0
      O3=2.0
      GO TO 8900
8740 IF (N.NE.NIN) GO TO 8900
      IF (M.NE.MIN+1) GO TO 8760
8750 IF (U01.GT.0.0) GO TO 8900
      DO 555 L=1,LMAX
      555 R1(L)=R2(L)
      GO TO 8900
8760 IF (M.NE.MIN-1) GO TO 8900
8770 IF (U00.LT.0.0) GO TO 8900
      DO 560 L=1,LMAX
      560 R4(L)=R3(L)
8900 CONTINUE
      IF (M.NE.2) GO TO 8950
      IF (U01.GE.0.0) GO TO 8950
      DO 565 L=1,LMAX
      565 R1(L)=R2(L)
8950 CONTINUE
      AX(N)=-G1*ZC2*V10*O1-G1A*DY10
      CX(N)=G2*ZC2*V00*O2-G2A*DY00
      DO 570 L=1,LMAX
      BZ(L,N)=C3B +G2*ZC2*V00*O3+G2A*DY00-G1*ZC2*V10*O4+G1A*DY10
      PZ(L,N)=C3P *RP(L,N,M)-AT*SX(L)
      * +ATL*(C5*(ZC1*U01*(R1(L)+R2(L))-(RP(L,N,M)-RP(L,N,M-1))*DX01)
      * -G4*(ZC1*U00*(R3(L)+R4(L))+(RP(L,N,M)-RP(L,N,M+1))*DX00))
570 CONTINUE
      IF (CZ20.EQ.0.) GO TO 121
      N=NNN
      NNN=N+1
      IF (N.EQ.NMAX) GO TO 150
      GO TO 123
150 CONTINUE
C
C           REACTION MODEL
C
      L=LMAX
      DO 200 LP=1,LMAX
      DO 575 N=2,NMAXN
      NNN=N+1
      TEM=0.0
      RTEM1=RP(L,N,M)
      IF (L.GT.LRMX) GO TO 6
      IF (L.EQ.1) GO TO 1
      LJM=L-1
      DO 2 LJ=1,LJM
      IF (LJ.GT.LRMX) GO TO 3
      RTEM=RP(LJ,N,M)
      IF (RTEM.LE.0.0) GO TO 2
      AKF=AKK(L,LJ)
      IF ((RTEM1.LE.0.0).AND.(AKF.GE.0.0)) GO TO 2
      TEM=TEM+AKF*RTEM*VOLDP(N)
2 CONTINUE
1 CONTINUE
      IF (L.EQ.LMAX) GO TO 3
      LJM=L+1
      DO 4 LJ=LJM,LMAX
```

```
1      IF (LJ.GT.LRMX) GO TO 3
      RTEM=R(LJ,N,M)
      IF (RTEM.LE.0.0) GO TO 4
      AKF=AKK(L,LJ)
      IF ((RTEM1.LE.0.0).AND.(AKF.GE.0.0)) GO TO 4
      TEM=TEM+AKF*RTEM*VOLDM(N)
4     CONTINUE
3     CONTINUE
      IF (L.NE.LOX) GO TO 6
      AKF=ROX(N,M)
      TEM=TEM-AKF*(SOX-.5*RTEM1)
      TEMM=.5*AKF*AT
      GO TO 7
6     CONTINUE
      AKF=.5*AKK(L,L)
      TEM =TEM +AKF *VOLDP(N)* RTEM1
      TEMM= AKF*VOLDM(N)*AT
7     CONTINUE
      D1=BZ(L,N)+AX(N)*E(L,N)+TEMM
      FX(L,NN)=(PZ(L,N)-TEM*AT-AX(N)*FX(L,N))/D1
      E(L,NN)=-CX(N)/D1
575  CONTINUE
      N=NMAX
580  CONTINUE
      DO 201 J1=2,NMAX
      NN=N-1
      R(L,NN,M)=E(L,N)*R(L,N,M)+FX(L,N)
      N=NN
201  CONTINUE
      IF(NST.GT.2) GO TO 210
      IF(L.GT.2) GO TO 210
      IF(M.LT.15) GO TO 210
      IF(M.GT.16) GO TO 210
      WRITE (6,211) NST,L,M
211  FORMAT(IX,3I5)
      DO 212 NX=2,5
      WRITE(6,213) BZ(L,NX),PZ(L,NX),AX(NX),CX(NX),FX(L,NX),E(L,NX),
*ROX(NX,M),R(L,NX,M),RP(L,NX,M),SES(NX,M),SE(NX,M),SEP(NX,M)
213  FORMAT(IX,1P12E10.3)
212  CONTINUE
210  CONTINUE
      L=L-1
200  CONTINUE
900  CONTINUE
      GO TO 404
400  CONTINUE
      IF(C8.LT.0.) C8=0.
      IF(C9.LT.0.) C9=0.
      IS=IS+1
      NVOL(IS)=N
      MVOL(IS)=M
      IF(C38.GT.0.) GO TO 402
      STA=.25*VAR -G3
      WATADD = (STA-SE(N,M))*AL*AL
      S21=S21+WATADD
      WRITE(6,403) NST,M,N,STA,SE(N,M),WATADD,S21
403  FORMAT (IX,4HNST=,15,2X,2HM=,13,2X,2HN=,13,2X,4HSET=,F7.4,
*2X,3HSE=, F7.4,2X,7HWATADD=,F10.2,2X,4HCUM=,E13.6,2X,4HDIFV)
      SE(N,M)=STA
402  CONTINUE
      GO TO 401
404  CONTINUE
      IF(IS.LT.1) GO TO 405
      DO 406 IST=1,IS
```

1

```
N=NVOL(IST)
M=MVOL(IST)
C(N,M)=0.
SES(N,M)=SE(N,M)
SE(N,M)=0.
SEP(N,M)=0.
SEN(N,M)=0.
UP(N,M)=0.
UP(N,M-1)=0.
V(N,M)=0.
V(N-1,M)=0.
U(N,M)=0.
U(N,M-1)=0.
VP(N,M)=0.
VP(N-1,M)=0.
```

```
406 CONTINUE
405 CONTINUE
RETURN
END
```

1

```
      SUBROUTINE DEPTH
      COMMON SE(61,78),SEP(61,78),V(61,78),VP(61,78),U(61,78),UP(61,78)
// DD DISP=OLD,DSN=N.N2640.      .JAMCOM72
// DD *,DCB=BLKSIZE=80
      NR1=1
      NR2=16
10  CONTINUE
      IF (NR2.GT.NMAX) NR2=NMAX
      DO 12 M=1,MMAX
      READ (5,3) (H(N,M),N=NR1,NR2)
12  CONTINUE
      NR1=NR2+1
      NR2=NR2+16
      IF (NR1.LE.NMAX) GO TO 10
      DO 1 N=1,NMAX
      DO 2 M=1,MMAX
      HT=H(N,M)
      IF (HT.GE.DCO) H(N,M)= DML*H(N,M)
      IF (HT.EQ.0.) H(N,M)=-DEPDEF
2   CONTINUE
1   CONTINUE
      RETURN
3   FORMAT(16E4.1)
      END
```

1

```
SUBROUTINE SINVAL
COMMON SE(61,78),SEP(61,78),V(61,78),VP(61,78),U(61,78),UP(61,78)
// DD DISP=OLD,DSN=N.N2640. .JAMCOM72
// DD *,DCB=BLKSIZE=80
TEMP=4. *VAR
TR1=SEINV+SEINV-VAR
DO 1 N=2,NMAX
NN=N-1
DO 2 M=2,MMAX
MM=M-1
H1=H(N,M)+H(N,MM)
H2=H(N,M)+H(NN,M)
H3=H(NN,M)+H(NN,MM)
H4=H(N,MM)+H(NN,MM)
IF (TR1+H1.LT.0.0) GO TO 8
IF (TR1+H2.LT.0.0) GO TO 8
IF (TR1+H3.LT.0.0) GO TO 8
IF (TR1+H4.LT.0.0) GO TO 8
SE(N,M)=SEINV
SEP(N,M)=SEINV
SEN(N,M)=SEINV
GO TO 3
8 CONTINUE
IF (H1.GT.H2) GO TO 7
IF (H1.GT.H3) GO TO 6
IF (H1.GT.H4) GO TO 5
HMIN=H1
GO TO 4
7 IF (H2.GT.H3) GO TO 6
IF (H2.GT.H4) GO TO 5
HMIN=H2
GO TO 4
6 IF (H3.GT.H4) GO TO 5
HMIN=H3
GO TO 4
5 HMIN=H4
4 SES(N,M)=.5*(VAR-HMIN)
3 CONTINUE
2 CONTINUE
1 CONTINUE
RETURN
END
```

1

```
      SUBROUTINE CVAL
      COMMON SE(61,78),SEP(61,78),V(61,78),VP(61,78),U(61,78),UP(61,78)
// DD DISP=OLD,DSN=N.N2640.A1700.JAMCOM72
// DD *,DCB=BLKSIZE=80
C
C
      CSETH=.5*CSET
      SEXP=1./6.
      DO 1 N=2,NMAX
      NN=N-1
      DO 2 M=2,MMAX
      ST=SEP(N,M)
      IF(ST.EQ.0.) GO TO 2
      MM=M-1
      SET=SEN(N,M)+SE(N,M)
      T1=SET+H(N,M)+H(N,MM)
      IF (T1.LT.0.0) GO TO 366
      T2=SET+H(NN,M)+H(NN,MM)
      IF (T2.LT.0.0) GO TO 366
      T3=SET+H(N,M)+H(NN,M)
      IF (T3.LT.0.0) GO TO 366
      T4=SET+H(N,MM)+H(NN,MM)
      IF (T4.LT.0.0) GO TO 366
      IF (T1.LT.VAR) GO TO 10
      IF (T2.LT.VAR) GO TO 10
      IF (T3.LT.VAR) GO TO 10
      IF (T4.LT.VAR) GO TO 10
      C(N,M)=1.49*(.25*(H(N,M)+H(NN,M)+H(N,MM)+H(NN,MM))+.5*SET)
1      **SEXP/VMAN(N,M)
      GO TO 363
10 CONTINUE
      C(N,M)=CSETH
      GO TO 363
366 C(N,M)=0.0
      IF (NST.NE.0) WRITE (6,13) NST,M,N,SES(N,M),SET
13 FORMAT (1X,4HNST=,15,2X,2HM=,13,2X,2HN=,13,2X,4HSES=,F7.4,
*        2X,4HSET=,F7.4)
      SES(N,M)=SE(N,M)
      U(N,M)=0.0
      U(N,M-1)=0.0
      UP(N,M)=0.0
      UP(N,M-1)=0.0
      V(N,M)=0.0
      V(N-1,M)=0.0
      VP(N,M)=0.0
      VP(N-1,M)=0.0
      SE(N,M)=0.0
      SEN(N,M)=0.0
      SEP(N,M)=0.0
363 CONTINUE
2 CONTINUE
1 CONTINUE
      RETURN
      END
```

```
1
SUBROUTINE INDAT1
COMMON SE(61,78),SEP(61,78),V(61,78),VP(61,78),U(61,78),UP(61,78)
// DD DISP=OLD,DSN=N.N2640. JAMCOM72
// DD *,DCB=BLKSIZE=80
READ (5,100) DIFDEF
100 FORMAT (E5.0)
DO 110 N=1,NMAX
DO 110 M=1,MMAX
110 DIFCO(N,M)=DIFDEF
120 READ (5,130) M,N1,N2,(TINDAT(M),M1=1,10)
130 FORMAT (3I5,10E5.0)
IF (M+N1+N2.EQ.0) GO TO 150
M1=0
DO 140 N=N1,N2
M1=M1+1
140 DIFCO(N,M)=TINDAT(M1)
GO TO 120
150 CONTINUE
READ (5,100) VMDEF
DO 160 N=1,NMAX
DO 160 M=1,MMAX
160 VMAN(N,M)=VMDEF
170 READ (5,130) M,N1,N2,(TINDAT(M),M1=1,10)
IF (M+N1+N2.EQ.0) GO TO 190
M1=0
DO 180 N=N1,N2
M1=M1+1
180 VMAN(N,M)=TINDAT(M1)
GO TO 170
190 CONTINUE
RETURN
END
```


1

```
      SUBROUTINE POLIN
      COMMON SE(61,78),SEP(61,78),V(61,78),VP(61,78),U(61,78),UP(61,78)
// DD DISP=OLD,DSN=N.N2640.      .JAMCOM72
// DD *,DCB=BLKSIZE=80
      3 FORMAT (16E4.1)
      4 FORMAT (15)
      5 READ (5,4) L
      IF (L.EQ.0) RETURN
      NR1=1
      NR2=16
10 CONTINUE
      IF (NR2.GT.NMAX) NR2=NMAX
      DO 12 M=1,MMAX
      READ (5,3) (R(L,N,M),N=NR1,NR2)
      DO 20 N=NR1,NR2
      RAPP=R(L,N,M)
      IF (RAPP.EQ.0.) R(L,N,M)=RBND(L)
20 CONTINUE
C
12 CONTINUE
      NR1=NR2+1
      NR2=NR2+16
      IF (NR1.LE.NMAX) GO TO 10
      DO 15 N=1,NMAX
      DO 15 M=1,MMAX
      RP(L,N,M)=R(L,N,M)
15 CONTINUE
      GO TO 5
      END
```

//

Appendix C
DATA SET, JAMAICA BAY MODEL

(05-20-72) 2 WK (WPCF UP X ROCK BR C) WQ23A R=4135,H=4156,G=4953
61 78 3 8 40.6 500. 32.2 30.0 30.0 0.8 -.2 .4 3.5 1.06 9.9
0 05953 372 30 40 20 6 248 13 12 18 9 5 5 4 6
0 0 101
.0026 .00237 1.9362 1.68 14.3
1 7.2 .000030 2
100
248 744 1488 2232 2976 3720 4464 5208 5952 6696 7440 8184 8928 96721041611160
11904119141192314136148801562416368171121785618600188481909619344195921984020088
1 9 4
2 48 19
3 10 45
4 59 48
5 77 49
6 10 6
7 31 15
8 51 23
9 69 36
10 52 34
11 56 49
12 10 31
13 11 45
14 19 52
15 30 56
16 44 58
17 26 38
18 1 4
1 5 5
2 5 6
3 4 7
4 39 15
5 25 38
6 14 47
7 69 35
8 55 36
9 52 36
1 50 55
2 37 14
3 18 57
4 62 60
5 77 56
6 16 57
7 6 52
8 3 56
9 77 54
10 43 28
11 33 13
12 49 30
13 22 60
1 10 6
2 31 15
3 51 23
4 69 36
5 52 34
6 56 49
7 10 31
8 11 45
9 16 50
10 30 56
11 44 58

20	10	10	5-110-120-100-110-110-	32	18	28	30	226	231	251	14405345
50	30	30	10-110-110-100-105-100-100-	8	10	6	28	348	354		15405350
5	5	8	10- 28- 88- 98-100-110-110-100	6	15	18	46	324			16405355
- 5-	5	5	10 10- 85-110-115-110-108-106-	50	8	16	35	200			17405360
13	13	13	13 15- 30-105-100-100-105-105-	80	3	16	35	51			18405365
65	25	8-	5 18 8- 32- 60- 8- 8- 60-	70	60	48	49	51			19405370
20-	8	20-	8 15 18 15- 5 15 12 10 18	26	22	25	28				20405375
138	110	83	35 28 12 15 10 12- 8- 2	25	18	12	16	15			21405380
102	120	109	127 61 12- 1 5- 6- 5 2 18	9	14	18	12				22405385
25	28	25	45 177 82- 10- 3- 10 13 16	15	17	9	12	6			23405390
- 10	8	3	34 98 133- 6- 4- 10 3- 1 2	8	11	2-	35				24405395
- 4	5-	3-	8 45 137 3- 1 5 3 2- 5-	10	12	2-	22				25405400
- 8	4	8	4 35 108 132- 10 3- 10 5 5	4	12	6-	1				26405405
- 18-	9-	1	6 15 28 161- 8- 1- 5- 15-	1-	10	14-	5-	10			27405410
- 3-	4	1	10 15 30 140- 5- 1- 2- 2 1	8	14-	8-	4				28405415
123	78	75	47 48 88 138 50- 1- 1 10 12	2	8-	3	11				29405420
- 10-	5-	5	8 15 26 105 65 12 6 3 13 12	16	18	2					30405425
- 15-	12-	35-	12 2 5 79 60- 3- 8- 12 9 12	16	18	8					31405430
- 10-	8-	5-	10 2 5 88 99 38 8 12 9-	2	2	3	104				32405435
- 3-	1	7	15 15 15 55 275 100 28 8-	8-	6-	2-	1	4			33405440
- 12-	6	3	7 12 16 225 300 123 115 28	28-	6-	2-	1-	5			34405445
- 12-	5	15	18- 15 2 28 12 47 60 85 117	59	32-	5-	10				35405450
8-	8	8-	100-100 2- 8- 10- 10- 2 31 32	36	85	89	38				36405455
12	15	2-	111- 2- 90- 80- 8- 10- 8 3 32	32	30	34	67				37405460
35	15	8-	65- 2- 72- 2- 80- 12- 13- 9 3-	2-	12-	5	28				38405465
8	5	3	3- 2- 60- 2- 42- 80- 16- 14-	12-	28-	39-	38				39405470
5	10	8	3- 57- 10- 62- 42- 32- 35- 28-	43-	47-	100-	150-	150			40405475
25	28	4	2- 65- 30- 28- 70-125-150-150-	110-	60-	45-	42-	22			41405480
35	15-	15-	50- 50- 50-150-135- 60- 35- 50-	65-	38-	29-	50-	2			42405485
41-	50-	51-	110- 48- 28- 23- 28- 48 2 4 6-	2-	2-	50-	60				43405490
15	1-	40-	10- 2- 2- 2- 2- 2- 42- 42-	38-	85-	45	6				44405495
- 50-	55-	55-	30- 42- 42- 52- 52- 85- 48- 46-	32-	40-	16	12	30			45405500
- 15-	25-	45-	60- 48- 48- 28- 10- 6 12- 38-	18-	18-	25	6	50			46405505
- 35-	25-	10-	15 10 15 5- 5 12 14 12 10-	3-	22-	16	12				47405510
30	30	30	30 10 40 18 12 28 26- 24 1-	24-	26	16	240				48405515
85	40	35	35 25 30 6- 8- 10- 32- 12- 48	300	300	421	405				49405520
143	148	42	42 5- 5 67 261 296 300 318 300	300	300	433	413	476			50405525
85	100	147	125 234 345 313 260 250 250	250	250	420	413	420			51405530
248	256	260	288 200 200 250 250 22 14	19	16	28	331	378	403		52405535
250	85	30	20 15- 38- 36- 12- 12- 28- 18	16	18	331	393	337			53405540
15	30	80	25 38- 33- 30- 1- 28- 23- 28-	6	35	430	380	436			44
35	35	35	80 35 22 28- 1 3- 18- 22- 41	12	393	236	261				55405550
25-	20-	5	20 25 80 38 28 30 18- 45- 23	12	350	261	320				56405555
50-	10-	30-	15- 5 12 42 42 70 28 23 14	48	300	284	293				57405560
- 10-	25-	35-	25- 5- 30- 38- 28 38 34 100	390	292	283	300				58405565
- 35-	38-	28-	15- 18- 30- 40- 30- 22- 10 28	350	291	315	288	278			59405570
- 10-	34-	38-	40- 30- 40- 40- 33- 30- 25 28	292	312	290	283	245			60405575
- 28-	30-	36-	43- 42- 40- 40- 36- 30- 12 60	370	305	275	261	233			61405580
- 30-	26-	28-	38- 41- 33- 40- 29- 28 5 48	220	268	262	244	35			62405585
- 28-	22-	10-	38- 38- 22- 28- 24-110-110	3	42	140	192	195	22		63405590
513-	33-	25	10 8 2- 15- 18-115- 90-112-	35	18	28	29	4			64405595
557-	30-	28-	12 80 400 120 6-105-115-100-100	8	1						65405600
534	367-	42-	28 282 326 330 378 205 150-	12-	105-	105-	100-	100			66405605
498	520	350	295 334 314 360 380 387 380	267	42-	100					67405610
372	518	549	305 398 375 365 200 407 413	260	98	3-	98				68405615
57	75	260	218 225 375 374 394 245	219	241	135	91-	32			69405620
50	15	160	218 183 213 264 354 315	243	250-	50-	50				70405625
28-	100	10	136 160 12 120 140 91 88-	100-	125						71405630
-118-	110	55	170 35 138 106 52 32- 43-	122-	105						72405635
-143-	156	35	170- 50- 50 88 148 121-	61-	100						73405640
-150-	150	38	180-111- 35- 75 32 149 210	45	12-	100					74405645

-120-100	35	180-	52-110-	75	32	28	210	207	247	247	180	180	270	75405650		
-120	120	170	170-	12-105-	45-	60	18	19	209	213	299	240	240	270	76405655	
170	170	50	50	170	12-	50-	35	30	18	202	162	287	278	280	270	77405660
																78405665
																1485280
130	130	120	120	120	120	120	120									2485285
130	130	120	120	120	120	120	120									3485290
																4485295
																5485300
																6485305
																7485310
																8485315
																9485320
																10485325
- 95																11485330
- 50-100																12485335
- 25-	50	170	170													13485340
25	20	150	80													14485345
230	63	80	80													15485350
371	101	42-	150													16485355
427	404	36-	98-	150												17485360
66	250	319	64	31	120	80	70	60								18485365
38	73	370	240	174	120	80	70	60								19485370
35	38	68	357	385	129-	50										20485375
25	28	30	355	342	296-	68										21485380
16	18	22	88	398	396	310-	50-	100								22485385
13	12	24	26	350	380	285	16-	150								23485390
2	10	12	26	54	387	424	24-	150-	150							24485395
- 18	8	12	16	22	47	410	188-	28	6	52	76					25485400
1-	5	10	15	22	34	371	222	150	150	150	150					26485405
- 10-	4	6	12	20	40	339	227	35	35	35	28					27485410
- 2-	1	7	13	20	28	307	207	35	22-	12-	22					28485415
3-	8-	3	8	8	35	276	338	28-	100-	150-	150					29485420
- 2-	4-	2-	12	6	25	120	316	26-	120-	150-	150					30485425
- 4-	3-	3-	22	8	123	459	234	28-	150	150	150					31485430
6	4	8	14	18	34	303	292	22-	135	150	150					32485435
18	22	16	18	15	29	235	295	35-	120	150	150					33485440
6	16	18	26	18	24	213	227	254-	70	150	150					34485445
1	12	14	16	20	35	283	227	261-	50	150	150					35485450
- 1	6	12	35	70	220	203	227	195	20	150	150					36485455
42	44	28	65	161	50	35	60	277	85	110	110					37485460
113	162	218	123	55	45	55	58	232	294	10	2					38485465
14	6-	35-	100-	68	35	60	70	245	287	35-	22					39485470
- 52-	120-	120-	32	12	18	35	45	282	120	14	38					40485475
-120-	88-	25	6	5	8	30	35	245	95	140	150					41485480
- 28-	2-	80	12	5	8	35	35	280	35	10	12					42485485
- 2-	2-	80	4-	2	2	30	35	168	20	22	8					43485490
- 50-	85-	85-	50-	58	16	320	340	343	316	15	2					44485495
12	14	280	393	326	372	355	340	338	272	220	170					45485500
45	340	372	396	375	363	350	292	283	230	130	120					46485505
45	340	348	368	343	291	292	290	255	35	150	150					47485510
350	368	272	258	368	289	330	193	198-	22	140	140					48485515
443	368	347	398	308	260	335	250	35-	110	140	140					49485520
385	243	399	403	248	321	295	194-	23-	135	140	140					50485525
375	375	456	333	255	320	218	22-	120		140	140					51485530
380	405	392	248	258	222	194	4-	120		140	140					52485535
420	385	260	265	263	200	18-	140			140	140					53485540
500	425	180	257	233	180-	100-	135			140	140					54485545
233	378	433	255	35	12-	120				140	140					55485550
270	295	283	220	12-	100-	135				130	130					56485555
310	293	262	188-	32-	85					130	130					57485560
288	272	158	12-	100-	135					130	130					

46	58	59	80.	80.									
47	48	57	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.
47	58	59	80.	80.									
48	48	57	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.
48	58	58	80.										
49	48	57	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.
49	58	58	80.										
50	48	57	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.
51	47	56	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.
51	57	57	80.										
52	46	55	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.
52	56	56	80.										
53	45	54	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.
53	55	55	80.										
54	45	54	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.
54	55	55	80.										
55	45	54	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.
56	45	53	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.	
57	45	53	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.	
58	45	53	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.	
59	45	52	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.	
60	45	51	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.	
61	43	51	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.	
62	43	50	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.	
63	43	50	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.	
64	44	49	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.	
65	45	48	80.	80.	80.	80.	80.	80.	80.	80.	80.	80.	

END DIFF COEF
MANNING DEFAULT COEFFICIENT

.031													
37	56	58	.026	.026	.026								
38	56	58	.026	.026	.026								
39	56	58	.026	.026	.026								
40	56	58	.026	.026	.026								
41	56	58	.026	.026	.026								
42	56	58	.026	.026	.026								
43	56	58	.026	.026	.026								
44	56	58	.026	.026	.026								
45	56	58	.026	.026	.026								
47	23	30	.026	.026	.026	.026	.026	.026	.026	.026	.026	.026	
48	29	30	.026	.026									
49	29	32	.026	.026	.026	.026							
50	31	32	.026	.026									
51	31	34	.026	.026	.026	.026							
51	40	48	.026	.026	.026	.026	.026	.026	.026	.026	.026	.026	
52	31	40	.026	.026	.026	.026	.026	.026	.026	.026	.026	.026	.026
72	39	41	.026	.026	.026								
73	39	41	.026	.026	.026								
74	40	41	.026	.026									
22	9	18	.034	.034	.034	.034	.034	.034	.034	.034	.034	.034	.034
23	10	18	.034	.034	.034	.034	.034	.034	.034	.034	.034	.034	
24	10	18	.034	.034	.034	.034	.034	.034	.034	.034	.034	.034	
25	10	18	.034	.034	.034	.034	.034	.034	.034	.034	.034	.034	
26	11	18	.034	.034	.034	.034	.034	.034	.034	.034	.034	.034	
27	12	18	.034	.034	.034	.034	.034	.034	.034	.034	.034	.034	
28	13	18	.034	.034	.034	.034	.034	.034	.034				
29	13	18	.034	.034	.034	.034	.034	.034	.034				
30	13	18	.034	.034	.034	.034	.034	.034	.034				
31	13	18	.034	.034	.034	.034	.034	.034	.034				
32	13	18	.034	.034	.034	.034	.034	.034	.034				
33	13	18	.034	.034	.034	.034	.034	.034	.034	.034			
34	13	18	.034	.034	.034	.034	.034	.034	.034				

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35 13 18 .034 .034 .034 .034 .034 .034
36 13 18 .034 .034 .034 .034 .034 .034
37 13 18 .034 .034 .034 .034 .034 .034
38 14 18 .034 .034 .034 .034 .034
39 14 19 .034 .034 .034 .034 .034 .034
40 15 20 .034 .034 .034 .034 .034 .034
41 15 20 .034 .034 .034 .034 .034 .034
42 15 21 .034 .034 .034 .034 .034 .034 .034
43 16 21 .034 .034 .034 .034 .034 .034
44 16 21 .034 .034 .034 .034 .034 .034
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46 17 21 .034 .034 .034 .034 .034
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70 33 40 .034 .034 .034 .034 .034 .034 .034 .034
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76 35 37 .034 .034 .034
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76 51 57 .034 .034 .034 .034 .034 .034 .034
77 34 38 .034 .034 .034 .034 .034
77 42 50 .034 .034 .034 .034 .034 .034 .034 .034 .034
77 51 56 .034 .034 .034 .034 .034 .034

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END MANN COEF

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1
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0.0 0.0 4.5 4.5 4.5 4.5 4.5 4.5 4.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
0.0 0.0 4.5 4.5 4.5 4.5 4.5 4.5 4.5 0.0 0.0 0.0 0.0 0.0 0.0 3.7 3.6
0.0 0.0 4.5 4.5 4.5 4.5 4.5 4.5 4.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0 3.6
DO 1 1
DO 1 2
DO 1 3
DO 1 4

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0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	BOD 4 68
0.0 0.0 0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.0	BOD 4 69
0.0 0.0 0.0 0.6 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	BOD 4 70
0.0 0.0 0.0 0.6 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	BOD 4 71
0.0 0.0 0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.0	BOD 4 72
0.0 0.0 0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.0	BOD 4 73
0.0 0.6 0.6 0.6 0.6 0.0 0.0 0.0 0.0 0.0 0.6 0.6 0.0	BOD 4 74
0.0 0.6 0.6 0.6 0.6 0.0 0.0 0.0 0.0 0.6 0.6 0.6 0.0	BOD 4 75
0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.0 0.0 0.0 0.6 0.6 0.0	BOD 4 76
0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.0 0.0 0.0 0.0 0.0	BOD 4 77
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	BOD 4 78

3

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	S1 1 46
	S1 1 47
	S1 1 48
	S1 1 49

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	S1 1 51
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	S1 1 76
	S1 1 77
	S1 1 78
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15.315.315.315.315.215.215.215.215.215.115.115.115.1	S1 2 15
15.315.315.315.215.215.215.215.215.115.115.115.115.1	S1 2 16
15.315.315.215.215.215.215.215.215.115.115.115.115.0	S1 2 17
15.315.215.215.215.215.215.215.115.115.115.115.015.0	S1 2 18
15.215.215.215.215.215.215.115.115.115.115.015.015.0	S1 2 19
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15.215.215.215.115.115.115.1 0. 0. 0. 0. 15.015.015.015.014.9	S1 2 22
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	S1 2 74
	S1 2 75
	S1 2 76
	S1 2 77
	S1 2 78
	S1 3 1
	S1 3 2
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	S1 3 78
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	S1 4 2
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14.0 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 14.0 0.	S1 4 62
	S1 4 63
	S1 4 64
	S1 4 65
	S1 4 66
	S1 4 67
	S1 4 68
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14.014.014.014.014.014.0 0. 0. 0. 14.014.0 0.	S1 4 76
14.014.014.014.014.014.014.0 0. 0. 0. 0. 0.	S1 4 77
	S1 4 78

0 END OF POLLUTANT ARRAYS

0.-0.2720	7	11.	60.		
1 119.8	3.0		13.0	.28	.024
2 33.9	4.4		55.0	1.36	.024
3 127.3	5.5		11.5	1.44	.024
9 6.0	0.0		0.0	0.0	0.0
10 0.6	4.4		55.0	1.36	1000.0
12 0.33	4.4		55.0	1.36	1000.0
13 0.0	0.0		0.0	0.0	0.0
0.-0.2720		11.	60.		
1.-0.2106		11.	60.		
2.-0.1615					
3.-0.1213					
4.-0.0763		11.	60.		
5.-0.0075					
6. 0.0810					
7. 0.1752		11.	60.		
8. 0.2596					
9. 0.3341					
10. 0.4095		11.	60.		
11. 0.4898					
12. 0.5758					
13. 0.6675		11.	57.		
14. 0.7650					
15. 0.8641					
16. 0.9739		12.	54.		
17. 1.1025					
18. 1.2336					
19. 1.3499		12.	51.		
20. 1.4498					
21. 1.5473					
22. 1.6456		12.	48.		
23. 1.7447					
24. 1.8496					
25. 1.9553		13.	45.		
26. 2.0626					
27. 2.1683					
28. 2.2559		13.	42.		
29. 2.3124					
30. 2.3689					
31. 2.4713		13.	39.		
32. 2.6057					

33.	2.7286		
34.	2.8236	13.	36.
35.	2.9063		
36.	2.9841		
37.	3.0570	14.	33.
38.	3.1431		
39.	3.2397		
40.	3.3192	14.	30.
41.	3.3782		
42.	3.4429		
43.	3.5232	14.	31.
44.	3.6067		
45.	3.6829		
46.	3.7427	14.	32.
47.	3.7763		
48.	3.7902		
49.	3.8019	15.	33.
50.	3.8262		
51.	3.8661		
52.	3.9077	15.	34.
53.	3.9388		
54.	3.9564		
55.	3.9673	15.	35.
56.	3.9708		
57.	3.9534		
58.	3.9259	15.	36.
59.	3.9023		
60.	3.8941		
61.	3.9032	15.	37.
62.	3.9144		
63.	3.8992		
64.	3.8471	16.	38.
65.	3.7809		
66.	3.7206		
67.	3.6659	16.	39.
68.	3.6039		
69.	3.5277		
70.	3.4336	16.	40.
71.	3.3295		
72.	3.2364		
73.	3.1617	16.	39.
74.	3.0963		
75.	3.0169		
76.	2.9062	16.	38.
77.	2.7756		
78.	2.6534		
79.	2.5482	16.	37.
80.	2.4433		
81.	2.3294		
82.	2.2195	16.	36.
83.	2.1245		
84.	2.0325		
85.	1.9324	17.	35.
86.	1.8230		
87.	1.7099		
88.	1.6012	17.	34.
89.	1.4997		
90.	1.4083		
91.	1.3216	17.	33.
92.	1.2305		
93.	1.1329		

94.	1.0324	17.	32.
95.	0.9297		
96.	0.8158		
97.	0.6953	17.	31.
98.	0.5857		
99.	0.4932		
100.	0.4208	17.	30.
101.	0.3620		
102.	0.3072		
103.	0.2460	17.	32.
104.	0.1717		
105.	0.0925		
106.	0.0134	17.	34.
107.	-0.0629		
108.	-0.1350		
109.	-0.2050	17.	36.
110.	-0.2679		
111.	-0.3212		
112.	-0.3731	17.	38.
113.	-0.4269		
114.	-0.4752		
115.	-0.5096	18.	40.
116.	-0.5331		
117.	-0.5580		
118.	-0.5831	18.	42.
119.	-0.6064		
120.	-0.6292		
121.	-0.6436	18.	44.
122.	-0.6422		
123.	-0.6175		
124.	-0.5837	18.	46.
125.	-0.5530		
126.	-0.5229		
127.	-0.4891	18.	48.
128.	-0.4445		
129.	-0.3908		
130.	-0.3265	18.	50.
131.	-0.2501		
132.	-0.1677		
133.	-0.0824	18.	49.
134.	0.0019		
135.	0.0869		
136.	0.1849	17.	48.
137.	0.2970		
138.	0.4145		
139.	0.5253	17.	47.
140.	0.6259		
141.	0.7294		
142.	0.8392	16.	46.
143.	0.9511		
144.	1.0560		
145.	1.1505	16.	45.
146.	1.2448		
147.	1.3491		
148.	1.4724	16.	44.
149.	1.6072		
150.	1.7262		
151.	1.8142	15.	43.
152.	1.8849		
153.	1.9640		
154.	2.0619	15.	42.

REFERENCES

1. Leendertse, J. J., *A Water Quality Simulation Model for Well-Mixed Estuaries and Coastal Seas: Vol. I, Principles of Computation*, The Rand Corporation, RM-6230-RC, February 1970.
2. Leendertse, J. J., and E. C. Gritton, *A Water-Quality Simulation Model for Well Mixed Estuaries and Coastal Seas: Vol. II, Computation Procedures*, The Rand Corporation, R-708-NYC, July 1971.
3. Leendertse, J. J., *A Water-Quality Simulation Model for Well Mixed Estuaries and Coastal Seas: Vol. IV, Jamaica Bay Tidal Flows*, The Rand Corporation, R-1009-NYC, July 1972.