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Achieving anti-sintering of supported platinum nanoparticles using a thermal management strategy

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ABSTRACT Sintering inhibition of a catalyst at high temperatures is a challenge during heterogeneous catalysis. In this paper, we report that hexagonal boron nitride (h-BN) is an optimal material for anti-sintering γ -Al₂O₃-supported Pt nanoparticles (NPs) originating from the high thermal conductivity of h-BN. The high thermal conductivity of h-BN ensures maximal heat dissipation from Pt NPs to γ -Al₂O₃, thereby causing both Ostwald ripening and particle coalescence of Pt NPs to be decelerated at elevated temperatures. Inhibition of Pt NP sintering is also shown in the reducible TiO₂-supported Pt NPs with the help of h-BN. The proposed anti-sintering strategy using thermal management is universal, providing new insight into the design of anti-sintering materials and structures for a wide range of applications in heterogeneous catalysis.

Keywords: anti-sintering, thermal management, molecular dynamics, hexagonal boron nitride

INTRODUCTION

Heterogeneous catalysis converts resources and raw materials into energy and valuable chemicals in an economically efficient manner. Transition metal (TM) particles are commonly used catalysts and are often prepared in small sizes to maximize the atomic utilization efficiency. Sintering is a natural phenomenon in heterogeneous catalysis at elevated temperatures, wherein nanoand micron-sized particles aggregate into larger particles because of reduced surface energy [1,2]. Numerous important industrial catalytic reactions, including the production of chemicals, pharmaceuticals, clean fuels, and exhaust treatments for automobiles and stationary power plants, undergo a large loss of catalytic reactivity due to the sintering of supported metal nanoparticles (NPs) [3]. To minimize sintering, the strengthening of metalsupport interactions has allowed various methods and technologies to be established [4-12]. For example, TM sintering can also be decelerated by the strong steric hindrance effect, such as by encapsulating metal particles into core-shell or yolk-shell structures [13-19], anchoring metal particles into pores of the large surface area of catalytic supports [20-22], controlling the uniformity of the metal NPs [23-25], and synthesizing multi-element alloys [26-28]. However, active sites are often covered and cannot participate in chemical reactions in such strategies, decreasing the catalytic performance of TM NPs. Understanding the sintering mechanism and developing efficient approaches to inhibit TM NP sintering are desirable, yet continue to pose a challenge.

In this paper, we report a new strategy to achieve metal NP sintering resistance using thermal management from the microscale to macroscale. Molecular dynamic (MD) simulations were first performed to study the sintering mechanisms of Pt NPs over a γ -Al₂O₃ support, two-dimensional (2D) hexagonal boron nitride (h-BN), graphene, and hexagonal boron arsenide (h-BAs), which are materials with high conductivities. We identified h-BN as an optimal material for Pt NP anti-sintering. Pt NP sintering was conducted at 800 K on a γ -Al₂O₃ support. The introduction of h-BN into a Pt/ γ -Al₂O₃ catalyst can inhibit the sintering of the highly dispersed Pt NPs at temperatures up to 1000 K by effectively dissipating ex-

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cess heat. The inhibition of sintering can be extended to reducible TiO_2 -supported Pt NPs. Our work provides a new approach for anti-sintering TM NPs on a broad range of supports at elevated temperatures.

EXPERIMENTAL AND THEORETICAL SECTION

MD simulations of particle migration and coalescence

MD simulations were performed using large-scale atomic/molecular massively parallel simulation code to study Pt NP sintering using a particle migration and coalescence (PMC) mechanism. Nose-Hoover implementations of the thermostats were used to control the temperature. The relative sintered density was obtained using mass-conservation in Equation (S1). Further details about non-isothermal sintering behaviors of different models are discussed in the Supplementary information (Table S1).

Phonon spectrum and phonon density of states

Density functional theory (DFT) calculations were performed within the projector-augmented wave pseudopotential as implemented with the Vienna *Ab-initio* Simulation Package (VASP). The generalized gradient approximation was adopted. The plane-wave cutoff energies were set at 350 eV. The Monkhorst-Pack sampling in the first Brillouin zone was gamma-centered. A 15-Å vacuum layer was set perpendicular to the surface and the ionic positions were fully optimized until the difference in total electronic energies was <10⁻⁵ eV.

After structural relaxation, the phonon spectrum and phonon density of states (Phonon DOS) were calculated using the finite displacement method [29]. Force constant calculations were performed using reduced *k*-point sampling meshes of $4 \times 4 \times 4$, $2 \times 2 \times 2$, and $6 \times 6 \times 1$ for the Pt, γ -Al₂O₃, and h-BN, respectively. The phonon frequencies were sampled on an $8 \times 8 \times 8$ *q*-point mesh for Pt and γ -Al₂O₃ and on a $10 \times 10 \times 1$ *q*-point mesh for h-BN.

Material preparation and characterization

h-BN was introduced into the substrate by using a mechanical mixture. Pt NPs were chemically deposited onto the substrate by using wet impregnation. Further preparation details are provided in the Supplementary information. Fourier transform infrared spectroscopy (FT-IR) and *in situ* FT-IR were both recorded using a Bruker VERTEX 70. X-ray diffraction (XRD) was performed using a Bruker D8 Advance. Nitrogen adsorption/desorption isotherms were performed using a Micromeritics ASAP 2460. Inductively coupled plasma optical emission spectrometry (ICP-OES) was tested using an Agilent ICP-OES 730. Scanning electron microscopy (SEM) was performed using an FEI Quanta 200F. Energy-dispersive Xray in the transmission electron microscopy (EDX-TEM) and high-angle annular dark-field scanning TEM (HAADF-STEM) were taken using an FEI F20. Thermogravimetric (TG) analysis was performed using a TGA/DSC 3+. In situ TEM spectroscopy was recorded on a JEM-2100F (JEOL Inc.) and an in situ heating TEM holder (model 652, Gatan Inc.) was used to control the temperature. Samples were heated for 5 min at a rate of 20 K min⁻¹ and temperature was recorded in 100 K increments. Thermal conductivity was tested using a NETZSCH 447. A VarioCAM HD research 880 was employed for infrared thermal imaging. Details about hydrogen-oxygen titration are shown in the Supplementary information (Fig. S1).

RESULTS AND DISCUSSION

The sintering of metal NPs may occur following two different mechanisms, namely, Ostwald ripening (OR) and PMC. OR causes large particles to grow at the expense of smaller particles due to the migration of single metal atoms on the support [30]. Metal NPs can migrate and coalesce to form larger particles in the PMC sintering process [31], which is a crucial method of achieving NP growth. In this paper, MD simulation was performed to study Pt NP sintering on y-Al₂O₃ through a PMC sintering mechanism. y-Al₂O₃ was selected based on the fact that it is widely used as the support in heterogeneous catalysis due to its versatile physical-chemical properties [32]. The PMC sintering evolution of Pt NPs on the γ -Al₂O₃ (010) surface was evaluated. We observed that Pt NPs merge easily on γ -Al₂O₃ (010) at 1000 K (Fig. 1a) and that Pt sintering accelerates as the temperature increases (Fig. S2).

In this paper, we focus on 2D materials, which have attracted considerable attention due to their extraordinary physical and chemical properties, such as high charge-carrier mobility, high thermal conductivity, high optical activity, and high mechanical strength [33–40]. 2D materials are widely and commonly used as supports to disperse single noble metal atoms and NPs [41–44]. However, it is still unknown whether and which 2D materials can act as effective supports to achieve antisintering of Pt NPs. Pt NP sintering behaviors present in the three types of 2D materials (i.e., h-BN, graphene, and h-BAs) were systematically studied. 2D h-BN, graphene,

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Figure 1 MD simulations and phonon DOS. Vector field distribution for NPs merging on (a) γ -Al₂O₃, (b) graphene, (c) h-BN, and (d) h-BAs supports predicted using MD simulations and following NP migration coalescence sintering mechanism. The 2D material supports are not shown to highlight Pt NP merging behaviors. (e) The phonon DOS of Pt, γ -Al₂O₃, and h-BN obtained using DFT calculation. (f) Relative sintered density of different model systems at the end of sintering process.

and h-BAs materials are selected here because they have higher thermal conductivities than γ -Al₂O₃ by one or two orders (Table S2).

New Pt-Pt bond formation is accompanied by heat release during Pt NP sintering due to PMC [45]. However, heat cannot dissipate effectively from y-Al₂O₃, which has low thermal conductivity. Compared with Pt/ y-Al₂O₃, Pt NP sintering due to PMC decelerates on h-BAs, graphene, and h-BN supports that have higher thermal conductivities than γ -Al₂O₃ (Fig. 1a–d). Heat released from Pt NP merging can facilitate fast heat dissipation on the 2D materials, preventing build-up of hot spots on Pt NPs. Pt/graphene displays the optimized performance for Pt NP anti-sintering, followed by h-BN and h-BAs (Fig. 1b-d), which can be attributed to the higher thermal conductivity of graphene than h-BN and h-BAs. Nevertheless, the structure collapse of graphene occurs at high temperatures and is likely to be removed during catalyst regeneration [46]. Therefore, we adopt h-BN as an optimal choice in this anti-sintering study by also considering its strong chemical inertness, thermal conductivity, superior temperature stability, acid-base resistance, and low cost [47,48].

An h-BN support can inhibit Pt NP sintering. However, the migration of Pt NPs occurs frequently on the highly crystalline surface of h-BN and few Pt NPs can anchor onto an h-BN surface due to the weak interactions between h-BN and Pt NPs. Synthesizing a low crystallized h-BN support to maintain the high dispersion of Pt NPs is a possible solution [49]. However, this will lower the thermal conductivity of the h-BN support that accelerates Pt NP sintering. We have thereby resorted to other approaches to decelerate the sintering of Pt NPs with a high dispersion. The y-Al₂O₃ support binds Pt NPs more strongly in comparison with h-BN [50], and therefore, Pt NPs prefer to anchor onto the surface of γ -Al₂O₃ in the presence of both y-Al₂O₃ and h-BN supports. This finding was corroborated by our STEM characterization (Fig. S3). Hence, we propose a new strategy to relieve sintering of Pt NPs by combining y-Al₂O₃ and h-BN to produce a composite support. First, h-BN can prevent Pt NP sintering through the PMC mechanism. The heat released by Pt NPs that are growing and merging can dissipate quickly through h-BN with high thermal conductivity. Second, sintering via OR predicts that large metal-support interactions results in a high rate of sintering due to the large migration of atoms along the support. The weak interaction between single Pt atoms and h-BN [51] inhibits Pt NP sintering via the OR mechanism. Third, highly dispersed Pt NPs can be deposited on γ -Al₂O₃.

To prove our hypothesis, we resort to phonon DOS calculations. We found that the phonons of γ -Al₂O₃ are

primarily distributed between 0–25 THz (Fig. 1e). The phonon DOS of h-BN shows obvious peaks at ~9, 18 and 38 THz. However, for Pt NPs, the overwhelming majority of phonons have frequencies <7 THz (Fig. 1e). This could be attributed to the heavier atomic mass and weaker inter-atomic force of the Pt NPs than the h-BN samples. In general, a stronger mismatch in the phonon DOS distributions will result in higher interfacial thermal resistance on the interface between materials [52], which will retard heat dissipation across the interfaces. Therefore, judging by the mismatch in phonon DOS distributions among Pt, γ -Al₂O₃, and h-BN, the Pt/ γ -Al₂O₃-h-BN is an optimal configuration for decelerating Pt NP sintering. A schematic diagram of two different configurations is shown in Fig. S4.

To verify the design strategy, we adopted an MD approach to simulate the sintering procedure when three 2D materials with high thermal conductivity (h-BN, h-BAs, and graphene) were introduced into Pt/γ -Al₂O₃ systems (Fig. 1e). The results show that the Pt/γ -Al₂O₃ system has the highest relative sintered density, which indicates the least anti-sintering performance. Combined with a series of high thermal conductivity 2D composites, the relative sintered densities of Pt NPs decease in different grades (Fig. 1f). Moreover, among all the systems, the "Pt/ γ -Al₂O₃-2D-material" configurations demonstrate better anti-sintering performances than their counterparts. This confirmed that, as we proposed, Pt/y-Al₂O₃-h-BN is an optimal material for decelerating Pt sintering. The phonon DOS distributions of h-BN, h-BAs [53], and graphene [54] demonstrate a stronger mismatch with Pt NPs than with γ -Al₂O₃ and this can be explained by the analysis of phonon DOS distributions previously discussed. Placing y-Al₂O₃ between Pt NPs and the high thermal conductive components may be an optimal strategy.

To confirm our theoretical predictions, Pt/γ -Al₂O₃ and Pt/γ -Al₂O₃-h-BN samples were successfully synthesized to understand their sintering behaviors. First, the surface properties, crystallinity, specific surface area, and textural structure of the four samples, γ -Al₂O₃, γ -Al₂O₃-h-BN, Pt/ γ -Al₂O₃, and Pt/ γ -Al₂O₃-h-BN, were characterized using FT-IR, XRD, and N₂ adsorption and desorption isotherm characterization techniques (Figs S5, S6). Two typical FT-IR absorption bands at 1378 and 816 cm⁻¹ are identified for the high-purity commercial h-BN [55]. XRD characterization confirmed the existence of a hexagonal crystal structure of boron nitride and alumina is present in the gamma phase. Both γ -Al₂O₃ and h-BN retain their original phases after the introduction of Pt NPs and

during the heating process (Fig. S6).

N₂-sorption isotherms were obtained to reveal the textural structure of Pt/γ -Al₂O₃ and Pt/γ -Al₂O₃-h-BN samples calcined at different temperatures (Fig. S5b and Table S3). Compared with Pt/γ -Al₂O₃, the Barrett-Joyner-Halenda pore size of Pt/γ -Al₂O₃-h-BN is slightly smaller (Fig. S5b inset), which can be explained by the low specific surface area of pristine commercial h-BN (Table S3). Sintering of γ -Al₂O₃ and γ -Al₂O₃-h-BN substrates is not observed by raising the temperature from 773 to 973 K due to the high Tammann temperature of alumina (1500 K) and high thermal stability of h-BN [56]. Therefore, a minor fluctuation of the Brunauer-Emmett-Teller (BET) surface area of Pt/γ -Al₂O₃ and Pt/γ -Al₂O₃-h-BN with variation in temperature exists even up to 973 K.

The initial mass fraction and dispersion of Pt NPs in the Pt/y-Al₂O₃ and Pt/y-Al₂O₃-h-BN samples were measured using ICP-OES and hydrogen-oxygen titration, respectively (Table S4). A lower platinum dispersion was observed in Pt/γ -Al₂O₃-h-BN than in Pt/γ -Al₂O₃, which corresponds to the inhibited sintering behavior of Pt/γ -Al₂O₃-h-BN. The high temperature sintering process was examined for the Pt/y-Al₂O₃ and Pt/y-Al₂O₃-h-BN samples using in situ TEM (Fig. 2). Pt NPs initially have the same size distribution of 2.6±0.4 nm on both y-Al₂O₃ and y-Al₂O₃-h-BN supports. Pt NPs are predominantly deposited on the surface of the γ -Al₂O₃ support (length of alumina nanotube is ~20 nm) for the Pt/γ -Al₂O₃, whereas for Pt/y-Al₂O₃-h-BN, h-BN (width of h-BN wafer is ~13 μ m) blends with γ -Al₂O₃ (Fig. S7). Using EDX in conjunction with TEM characterization, we found that Pt NPs are predominantly deposited on γ -Al₂O₃ in the Pt/ γ -Al₂O₃-h-BN sample (Fig. S3).

Sintering can occur at elevated temperatures, namely, Pt NPs supported on γ -Al₂O₃ grow larger with the increase of temperature from 300 to 1000 K (Fig. 2a-h). Pt NPs are supported on γ -Al₂O₃ sinter via both OR and PMC mechanisms. At 800 K, Pt NPs on γ-Al₂O₃ begin to coalesce into a single particle as they meet in regime I. OR occurs when larger Pt NPs grow at the expense of smaller particles in regime II after increasing the temperature to 800 K. For the Pt/y-Al₂O₃-h-BN sample, no obvious aggregation of Pt NPs occurs below 800 K (Fig. 2i-p). Pt NP sintering becomes increasingly evident on Pt/y-Al₂O₃-h-BN when the temperature increases to >900 K due to PMC and OR. Pt NPs always have a smaller size when supported on γ -Al₂O₃-h-BN than when on γ -Al₂O₃ from 300 to 1000 K (Fig. 3a). The experimental findings are corroborated with our theoretical predictions that the addition of h-BN to y-Al2O3 would hinder Pt NP sin-



Figure 2 *In situ* TEM characterization of sintering of Pt/γ -Al₂O₃ and Pt/γ -Al₂O₃-h-BN. TEM images of Pt/γ -Al₂O₃ at temperatures of (a) 300 K, (b) 400 K, (c) 500 K, (d) 600 K, (e) 700 K, (f) 800 K, (g) 900 K, and (h) 1000 K. TEM images of Pt/γ -Al₂O₃-h-BN at temperatures of (i) 300 K, (j) 400 K, (k) 500 K, (l) 600 K, (m) 700 K, (n) 800 K, (o) 900 K, and (p) 1000 K.

tering. The better anti-sintering ability of Pt/ γ -Al₂O₃-h-BN can be attributed to two primary causes. When the Pt NPs were loaded on the h-BN in the Pt/ γ -Al₂O₃-h-BN sample, weak metal-support between single Pt atoms and h-BN inhibits OR sintering and high thermal conductivity of h-BN hinders sintering due to PMC. When the Pt NPs were loaded on the γ -Al₂O₃ in the Pt/ γ -Al₂O₃-h-BN sample, Pt NP sintering due to OR and PMC mechanisms decelerates because of the high thermal conductivity of h-BN.

HAADF-STEM characterizations were further performed to identify Pt NP sintering during a long-term heating process with an elevated temperature rate of 1.58 K min^{-1} (Fig. 3a, b and Figs S8–S10). Pt NP sintering on γ -Al₂O₃ can be typically divided into three phases. In phase I at temperatures below 773 K, Pt NPs on γ -Al₂O₃ are a relatively uniform size of <5 nm. The Pt NP sintering rate is slow at low temperatures in phase I. In phase II, the temperature rises from 773 to 873 K and OR and PMC are responsible for the rapid Pt NP growth. The particle size of Pt NPs supported on γ -Al₂O₃ grows from 11.3±4.1 nm to 13.5±3.4 nm during phase III when temperatures increase from 873 to 973 K. However, the particle size of Pt NPs supported on γ -Al₂O₃-h-BN grows from 6.8±2.0 nm to 9.2±2.1 nm during phase III. Although Pt/ γ -Al₂O₃-h-BN has a similar sintering behavior as Pt/ γ -Al₂O₃ does, Pt NPs have a lower growth rate on γ -Al₂O₃-h-BN than on γ -Al₂O₃ below 973 K (Fig. 3b).

Consistent with *in situ* TEM characterizations, sintering of Pt NPs is inhibited during the three phases by introducing h-BN in Pt/ γ -Al₂O₃-h-BN through HAADF-STEM analysis (Fig. 3a, b). Because sintering is a thermodriven process, the Pt NPs supported on the substrate migrate from a place of high temperature to one of low temperature as driven by the temperature gradient [57– 59]. The thermal gradient driving force for grain



Figure 3 Particle-size distribution and thermal properties. (a) Particle-size distribution of Pt/γ -Al₂O₃ and Pt/γ -Al₂O₃-h-BN under *in situ* TEM. Particle-size distribution of (b) Pt/γ -Al₂O₃ and Pt/γ -Al₂O₃-h-BN and (c) Pt/TiO_2 and Pt/TiO_2 -h-BN in aberration-corrected HAADF-STEM images. (d) Thermal conductivities of Pt/γ -Al₂O₃ and Pt/γ -Al₂O₃-h-BN obtained using a laser flash apparatus.

boundary migration is proportional to the thermal gradient [57]. Infrared thermal imaging camera results show a more uniform temperature field distribution after introduction of h-BN in Pt/γ -Al₂O₃ (Fig. 4a-d). A gentler temperature distribution trend for Pt/y-Al₂O₃-h-BN than for Pt/γ -Al₂O₃ is shown in Fig. 4a-d and Fig. S11. The thermal gradient ratio of Pt/y-Al₂O₃ and Pt/y-Al₂O₃-h-BN is 2, indicating that a stronger driving force exists for Pt NP sintering in $Pt/\gamma-Al_2O_3$ than for $Pt/\gamma-Al_2O_3$ -h-BN. The thermal conductivity of Pt/y-Al₂O₃-h-BN is four times that of Pt/γ -Al₂O₃ (Fig. 3d). The high in-plane thermal conductivity of h-BN [60], which facilitates heat transformation, makes a large contribution to a lower thermal gradient in Pt/y-Al₂O₃-h-BN. As a result, the more uniform temperature field distribution decreases the thermal gradient-driven force for Pt NP sintering at a macroscale in Pt/y-Al₂O₃-h-BN. In other words, thermal interface resistance between Pt NPs and substrates is reduced and the excess heat for Pt NPs can be transported quickly with the help of h-BN-inhibited sintering of Pt NPs in Pt/γ -Al₂O₃-h-BN.

In this paper, we proposed an efficient strategy to antisintering Pt NPs by introducing h-BN, a material with high thermal conductivity, into γ -Al₂O₃. Our strategy for anti-sintering metal NPs by means of thermal management is different from previous approaches, namely, by strengthening the metal-support interaction effect [4-12], which enhances OR sintering and hinders PMC sintering. The integration of h-BN to the support not only enhances heat transfer in the system but also changes the electrical and chemical environments of the active centers. Zhu et al. [44] indicated that Pt NPs are more negatively charged on vacancy-abundant BN nanosheets than on SiO₂. Liu et al. [49] revealed that Pt NPs stabilized at the grain boundary of BN could be more easily reduced in a propane combustion reaction as compared with those on the surface of BN, and thereby are more active, suggesting different reaction pathways for these catalysts and the possible participation of the grain boundary of the BN support in the reaction. Cao et al. [61] indicated that defects of the Ni/h-BNNS catalyst can strongly influence metal-support interaction due to electron donor/acceptor mechanisms and favor the adsorption and catalytic activation of CH₄ and CO₂.

As shown in Scheme 1, Pt NP sintering due to OR and PMC mechanisms decelerates under high temperatures in the Pt/γ -Al₂O₃-h-BN system. h-BN is an optimal 2D material for anti-sintering Pt NPs because of its high



Figure 4 Temperature field distribution of (a, b) Pt/γ-Al₂O₃ and (c, d) Pt/γ-Al₂O₃-h-BN tested using an infrared thermal imaging camera.



Scheme 1 Schematic of the anti-sintering strategy during the high temperature sintering process.

thermal conductivity. Thermal conductivity is higher and thermal interfacial resistance is lower when h-BN is introduced into Pt/γ -Al₂O₃, and thereby a large amount of heat can be transported quickly from the surface of Pt NPs to substrates to inhibit sintering due to PMC and OR mechanisms. The advantage of the present strategy lies in its simplicity and effectiveness as well as in the adaptability to complex environments, such as during realistic chemical reaction conditions. We have extended this to the reducible Pt/TiO₂ system where the introduction of h-BN into Pt/TiO₂ can inhibit Pt NP sintering (Fig. 3c and Figs S12, S13).

CONCLUSION

A universal anti-sintering strategy was developed using a combination of theoretical prediction and experimental validation. The ultrahigh anti-sintering performance of Pt NPs at high temperatures was demonstrated by introducing high-thermal-conductivity h-BN material into Pt/γ - Al_2O_3 material. This strategy can be extended to other oxide-supported TM NPs. Our work demonstrates a method for controlling the sintering process and provides insight into the development of novel anti-sintering materials and structures.

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Supplementary information Experimental and theoretical details and supporting data are available in the online version of the paper.





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基于热管理策略实现负载型铂纳米颗粒的抗烧结

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摘要 抑制催化剂在高温条件下的烧结仍是目前多相催化领域的 一个巨大挑战.本文报道了高热导率六方氮化硼可作为γ-Al₂O₃负 载型铂纳米粒子优异的抗烧结材料.在升温条件下,六方氮化硼的 高热导率能够确保铂纳米粒子到γ-Al₂O₃的有效散热,从而实现铂 纳米粒子Ostwald熟化烧结和颗粒碰撞烧结均被抑制.TiO₂负载的 铂纳米粒子在引入六方氮化硼后,铂纳米粒子的烧结同样被抑制. 本工作提出了一种基于热管理实现抗烧结的通用策略,为在多相 催化中广泛应用的抗烧结材料和其结构设计提供了新的思路.