

Aggregate stability of a crusted soil: differences between crust and sub-crust material, and consequences for interrill erodibility assessment. An example from the Loess Plateau of China

Baptiste Algayer, Bin Wang, Hocine Bourennane, Fenli Zheng, Odile Duval, Guifang Li, Yves Le Bissonnais, Frédéric Darboux

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sub-crust material, and consequences for interrill erodibility 2 assessment. An example from the Loess Plateau of China 3 4 B. ALGAYER^a, B. WANG^b, H. BOURENNANE^a, F. ZHENG^{b, c}, O. DUVAL^a, 5 G. LI^c, Y. LE BISSONNAIS^d, & F. DARBOUX^a 7 8 9 ^aInstitut National de la Recherche Agronomique (Inra), UR0272, Science du sol, 10 Centre de recherche Val de Loire, CS 40001, F-45075 Orléans Cedex 2, France, 11 ^bCollege of Resources and Environment (Northwest A&F University), No. 3 Taicheng 12 Road, 712100, Yangling, Shaanxi, China, ^cInstitute of Soil and Water Conservation 13 (CAS), NO.26 Xinong Road, 712100, Yangling, Shaanxi, China, and dINRA, UMR 14 LISAH (INRA-IRD-SupAgro), F-34060 Montpellier, France. 15 16 Correspondence: B. Algayer. Email: Baptiste.Algayer@orleans.inra.fr 17 18 19 20 21 Running title: Aggregate stability of a crusted soil 22

Aggregate stability of a crusted soil: differences between crust and

23 Summary

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Soil interrill erodibility is a key component of soil erosion models. However, when using aggregate stability to assess soil erodibility, samples are usually collected from the plough layer, while soil erosion occurs at the soil surface. Hence, the potential changes in erodibility caused by crusting are ignored. Moreover, soil interrill erodibility is still difficult to predict accurately. This lack of prediction means that current erosion models use a constant erodibility value for a given soil, and thus do not consider potential heterogeneity of erodibility. This study was conducted (i) to assess the heterogeneity of aggregate stability for a crusted soil and (ii) to relate this heterogeneity to the aggregate stability of the underlying material (sub-crust) and to standard soil properties. A field study was conducted in a small area of the Loess Plateau in China in which the crust and the sub-crust were sampled. Standard soil properties (organic matter content, sand content, silt content, clay content, cationexchange capacity, pH in water, and water content at the time of sampling) were measured as potential explanatory factors of aggregate stability. The results showed a large heterogeneity in aggregate stability among the sites, even though the sites had the same soil type. The mean weight diameter (MWD) of the crust varied between 0.33 and 2.04 mm while the MWD of the sub-crust varied between 0.23 and 1.42 mm. Soil texture and pH were very homogeneous among the sampling sites, whereas water content, organic matter content and CEC varied more. Even though some correlations existed (for example r = 0.57 between the MWD for slow wetting test and organic matter content), none of the standard soil properties was able to predict aggregate stability accurately. The aggregate stability of the crust was significantly greater than that of the sub-crust. The large differences in aggregate stability imply large

differences in soil interrill erodibility. Because a single soil type was investigated, this
finding proves that erodibility can vary greatly in space even for a given soil type.

Soil interrill erodibility should be estimated from the exact material actually exposed
to erosive forces, the soil surface material. Using the sub-crust would have led to
greatly over-estimated erodibility and thus to a marked bias in erosion model
predictions.

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Résumé

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L'érodabilité inter-rigole est un paramètre clef des modèles d'érosion du sol. 57 Cependant, lorsque des tests de stabilité structurale sont utilisés pour évaluer 58 59 l'érodabilité, les mesures sont habituellement réalisées sur des échantillons prélevés 60 dans l'horizon labouré alors que l'érosion a lieu à la surface du sol. Ainsi, les changements potentiels d'érodabilité causés par la formation de croûte sont ignorés. 61 62 De plus, l'érodabilité inter-rigole reste encore difficile à prédire avec précision. Ces difficultés conduisent les modèles d'érosion à utiliser une érodabilité constante pour 63 un type de sol donné, et donc à ne pas considérer l'hétérogénéité potentielle de 64 l'érodabilité. Cette étude a été conduite pour (i) évaluer l'hétérogénéité de la stabilité 65 66 structurale pour un sol encroûté et (ii) relier cette hétérogénéité à la stabilité 67 structurale du matériau sous-jacent (sous-croûte) et aux propriétés standards du sol. Une étude de terrain a été réalisée sur un secteur de surface limitée du Plateau de 68 Lœss (Chine). Des échantillons provenant de la croûte et de la sous-croûte ont été 69 70 collectés. Les propriétés standards (teneur en carbone organique, teneurs en sable, limon et argile, CEC, pH, et teneur en eau au prélèvement), ont été mesurées en tant 71 que facteurs explicatifs potentiels de la stabilité structurale. Les résultats ont montré 72

une grande hétérogénéité de la stabilité structurale entre les différents sites alors que ces derniers présentaient le même type de sol. Le MWD de la croûte variait entre 0,33 et 2,04 mm tandis que le MWD de la sous-croûte variait entre 0,23 et 1,42 mm. La texture du sol et le pH étaient très homogènes entre les sites étudiés, tandis que la teneur en eau, la teneur en matière organique et la CEC variaient plus fortement. Bien que certaines corrélations aient été identifiées (par exemple r=0.57 entre le MWD du test à l'humectation lente et la teneur en carbone organique), aucune de ces propriétés n'a permis de prédire précisément la stabilité structurale. La stabilité structurale de la croûte était significativement supérieure à celle de la sous-croûte. Les grandes différences de stabilité structurale mesurées impliquent des érodabilités très contrastées. Comme un seul type de sol a été étudié, ce résultat prouve que l'érodabilité peut être très variable spatialement pour un type de sol donné. L'érodabilité inter-rigole du sol devrait être mesurée sur le matériau exact qui subit l'érosion, c'est-à-dire le matériau de surface. L'utilisation du matériau sous-jacent aurait engendré une forte surestimation de l'érodabilité et donc un biais important dans les prédictions d'un modèle d'érosion.

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Introduction

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In the context of soil erosion by water, interrill erodibility corresponds to the sensitivity of the surface material to detachment and transport by raindrop impacts and by sheet flow. Accordingly, interrill erodibility is a key component in erosion models (Gumiere et al., 2009; Wang et al., 2013). Currently, there is no unified definition of erodibility and those proposed are qualitative: there is thus a need for quantitative methods (Wang et al., 2013).

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Interrill erodibility can be estimated from standard soil properties such as soil texture or carbon content and using statistical functions (Alberts et al., 1995; Renard et al., 1997). Although such estimations are easy to carry out once the statistical function has been established, they postulate that samples with similar standard soil properties have similar erodibilities. Moreover, the ranges of validity of the statistical functions (the textures and carbon contents for which these functions can be used) are often limited and poorly known. Finally, erosion models typically use a single erodibility value for a given soil, hence postulating a small spatial heterogeneity of the erodibility (Renard et al., 1997; Jetten et al., 2003). Another approach to characterize soil interrill erodibility is to measure aggregate stability in the laboratory (Le Bissonnais, 1996; Barthès & Roose, 2002). Aggregate stability corresponds to the ability of an aggregate not to break up into smaller fragments. A large aggregate stability of the top-soil induces a strong resistance of the surface aggregates against breakdown, and thus induces less particle detachment and transport by raindrop impacts and by sheet flow (Le Bissonnais, 1996; Bajracharya & Lal, 1998). Hence, even though a few models use this soil property currently (LISEM, De Roo et al., 1996), aggregate stability is considered as a proxy of soil interrill erodibility, with a poor aggregate stability corresponding to a large potential erodibility and vice versa (Barthès & Roose, 2002; Gumiere et al., 2009). The properties of a given soil may change over a period of a few weeks or months because of crust development (Poesen, 1981; Bryan et al., 1989). In an agricultural context, the soil surface evolves from a seedbed (loose surface layer composed of clods and macro-aggregates) to successive stages of crusting that correspond to different types of crust (Bresson & Boiffin, 1990). The structural crust corresponds to

a thin surface layer where the micro-aggregates resulting from the breakdown of

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surface clods are sealed together, and the sedimentary crust corresponds to a compact surface layer where the surface pores and micro-depressions are filled by small fragments resulting from the erosion and sedimentation processes. The presence of a crust can induce marked differences between the properties of the plough-layer and the soil surface. Numerous studies show that the infiltration capacities can be very different between the crust and the underlying material (e.g. Morin & Van Winkel, 1996). However, only a few studies have addressed the effect of a crust on erodibility (McIntyre, 1958; Poesen, 1981; Darboux & Le Bissonnais, 2007). Most of the studies using aggregate stability to assess erodibility are made with samples collected within the plough layer (Bullock et al., 1988; Bajracharya & Lal, 1998; Barthès & Roose, 2002; Legout et al., 2005), notwithstanding that interrill erosion occurs at the soil surface and thus depends directly on the erodibility of the crust and not on the erodibility of the plough layer material. For a clay loam soil, Darboux & Le Bissonnais (2007) did not find significant differences in aggregate stability between a structural crust and the seedbed material (without crust); but there were notable differences in aggregate stability between a sedimentary crust and the seedbed material (without crust). This finding led these researchers to conclude that estimations of erodibility for material collected from the plough layer may be invalid for the crust, resulting in a potential bias in the estimated erodibility. However, the results of this laboratory experiment had limited application, and did not attempt to assess the factors responsible for differences in aggregate stability, even though numerous factors have previously been identified (Amézketa, 1999). In the present work, a field study was conducted in a small area (7.5 km radius) of the Loess Plateau of China. The crust and the underlying materials were sampled in areas designated for different land uses. Aggregate stability was measured as a proxy of soil erodibility, along with standard soil properties known to be related to aggregate stability. We wished to test the hypotheses that crusts developed from a given soil type show different aggregate stabilities depending on the aggregate stability of the underlying material and on the standard soil properties. The research objectives were (i) to assess the heterogeneity of aggregate stability of crusted Luvisols within an area presenting a small spatial extent and (ii) to relate this heterogeneity to the aggregate stability of the underlying material and to the standard soil properties. The consequences for erodibility assessment and erosion modeling are discussed.

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Materials and methods

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159 Sampling sites

> The Chinese Loess Plateau (northwest China) is recognized as the largest deposit of loess in the world. Silt particles resulting from wind erosion at the Tibetan Plateau and the Gobi desert have accumulated to an average thickness of 150 m. The silt loam soils that developed on this substrate are very homogeneous in both texture and chemical properties and are recognized to be very sensitive to erosion (Zheng, 2005). The experimental area was located in the Ziwuling area, in the hilly-gully region of the Loess Plateau (Figure 1). Altitude of the sampling sites varied between 1100 and 1300 m with an average annual temperature of 9° C and average annual precipitation of 577 mm. Soil samples were collected on seven field sites, selected in order to present the same soil type (silt loam Luvisols, WRB, developed on loessial material) but with different land uses, erosion conditions and environmental conditions such as altitude, slope position and orientation (Table 1). The sites (A, B, C and D) were geographically close together (located within a 7.5 km radius) (Figure 1). There were

four sub-sites at D (D1, D2, D3 and D4) which were located along a 200-m long eroded hill slope. Table 1 provides details of the various land uses and locations.

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Sampling method

Sampling was performed in September 2009 over a period of three consecutive days, beginning four days after the last previous rain event. For each site (A, B, C, D1, D2, D3 and D4), five plots (one square meter each) were defined to collect samples in order to take into account the spatial heterogeneity within each site. Prior to sampling, the soil surface was described, and the crust type was identified (Bresson & Boiffin, 1990; Belnap et al., 2008). The soil surfaces had no obvious mosses or lichens and had a light colour, indicating little cyanobacterial development (Belnap et al., 2008). Paired samples (crust and underlying material) were collected from each plot at each site so that the crust was collected separately from the underlying material (hereafter referred to as 'sub-crust'). All of the sites had a structural crust, but only site C had both structural and sedimentary crust. Therefore, only structural crust is considered hereafter. Because the lower depth of the structural crust was indistinct, a thickness of approximately 5 mm was considered to be the limit. The sub-crust was defined as the soil material between -1 and -5 cm from the soil surface. In all cases, three-to-five cm samples were collected using a sharp knife to cut through the material without affecting its structure. Soil samples from the crust and sub-crust were divided into five sub-samples in order to measure aggregate stability, organic matter content, CEC, pH and soil texture.

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Measurements

Aggregate stability Samples were oven-dried at 40° C over two days and stored in a 197 cold room at 4° C for fifteen days before measurements. Aggregate stability was 198 measured using a slightly modified version of Le Bissonnais' method (Le Bissonnais, 199 200 1996; ISO/DIS 10930, 2012), where air-dried samples from both crust and sub-crust 201 were cut into 2–5 mm fragments with a sharp knife. 202 The three stability tests of Le Bissonnais (1996) (fast wetting, slow wetting and 203 stirring) were designed to reproduce the processes involved in crust formation and interrill erosion (slaking, differential clay swelling and mechanical breakdown). 204 205 Results of each test can be investigated separately to analyse the resistance of the 206 material against each process. Because the three processes occur often 207 simultaneously: the three MWD resulting from the three tests are commonly 208 averaged. Five-g sub-samples were dried at 40° C for 24 hours before the application of a 209 test, and each test was replicated twice (instead of three times as in the original 210 211 method). After the tests, the resulting fragments were sieved in ethanol. The results are presented using the mean weighted diameter (MWD). Each MWD corresponds to 212 one of five classes of stability: MWD >2 mm corresponds to very stable material 213 (very weak erodibility), between 2 and 1.3 mm corresponds to stable material (weak 214 215 erodibility), between 1.3 and 0.8 mm corresponds to median stability (median 216 erodibility), between 0.8 and 0.4 mm corresponds to unstable material (strong erodibility), and <0.4 mm corresponds to very weak stability (very strong erodibility) 217 218 (Le Bissonnais, 1996). 219 Standard soil properties Standard soil properties were measured to explain 220

differences in aggregate stability between the sites and between the crust and sub-

222 crust. These were gravimetric water content, organic matter content, clay content, silt 223 content, sand content, CEC and pH. Relationships between these variables and aggregate stability have frequently been reported in the literature (Wischmeier & 224 225 Mannering, 1969; Tisdall & Oades, 1982; Amézketa, 1999; Zhang & Horn, 2001). 226 Hence, these variables could be assumed to be suitable explanatory factors for the differences in aggregate stability between the crust and sub-crust materials of a given 227 228 site and also between sites. Clay, silt and sand contents were measured by laser diffraction granulometry, 229 230 (Loizeau et al., 1994), with a Mastersizer 2000 (Malvern Instruments Ltd, Malvern, 231 UK). Soil organic matter content was measured with the Walkey & Black (1934) method, cation-exchange capacity (CEC) with the ammonium rapid method 232 233 (Mackenzie, 1951), and pH with a 1:2.5 soil:water ratio and a pH meter. Gravimetric

water content was measured at the time of sampling: 10-g sub-samples were dried at

105° C over 48 hours. Measurements were performed on soil bulk samples for both

crust and sub-crust materials. Each measurement was replicated twice.

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Statistical analyses

Statistical analyses were performed using version 2.9.2 of software R (R Development Core Team, 2011). To avoid the assumption of normality of samples required for the use of parametric tests, a non-parametric test (Wilcoxon test) was used to compare the MWD and the standard soil properties of crust and sub-crust samples. We considered a significant threshold of 5%. The heterogeneity (dispersion) of the soil properties was quantified using the coefficient of variation, which is a normalized measure of dispersion. Linear correlation analyses (Pearson's coefficient) were performed to quantify the relationships between the standard soil properties and aggregate stability.

247 To model MWD according to the soil properties, in other words to quantify the proportion of MWD (dependent variable) variability which is explained by 248 249 independent variables, multiple regression analyses were conducted.

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Results

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253 Heterogeneity of the aggregate stability For all the sampling sites, and for both crust and sub-crust, MWD was the largest for the slow wetting test (1.47 and 0.97 mm for 254 255 the crust and sub-crust, respectively) and the least for the fast wetting test (0.98 and 0.36 mm for the crust and sub-crust, respectively) (Table 2). 256 When the mean of the three stability tests is considered, the MWD of the crust varied 257 258 among the sites between 0.33 and 2.04 mm, with a coefficient of variation of 0.37 259 (Table 2). For crust material and for each stability tests, sites A (cultivated maize 260 field) and D1 (Ziwuling experimental station, interrill area) had the largest MWD 261 while site C (cultivated radish) had the smallest (Figure 2). 262 With the sub-crust, and again considering the mean of the three stability tests, the MWD varied between 0.23 and 1.42 mm, with a coefficient of variation of 0.47 263 264 (Table 2). For all the stability tests on these samples, site D1 had the largest MWD and site C had the smallest (Figure 2). Among the sites, the coefficients of variations 265 266 were larger for the sub-crust samples than for the crust samples, except for the stirring 267 test which had the same coefficient of variation (Table 2). For each site, samples were 268 collected from five plots to consider intra-site heterogeneity. Considering the mean of 269 the three stability tests, the intra-site coefficient of variations for the five plots taken at 270 each site were larger for the sub-crust than for the corresponding crust samples for

sites A, D1, D2, D3 and D4.

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Comparison of aggregate stability for paired crust and sub-crust samples

The aggregate stability of the crust was significantly different from that of the underlying material ($P = 2.10^{-10}$ for the mean of the three stability tests). For most of the paired samples, the aggregate stability of the crust was greater than that of the corresponding sub-crust, and the sub-crust samples were never more stable than their corresponding crust (Figure 2). The difference in aggregate stability between crust and sub-crust varied with the stability test. The fast wetting test had the the largest differences in MWD between crust and sub-crust (0.62 mm, Table 3). In order to study the relationships between the MWD of the crust and the MWD of the sub-crust material, a correlation analysis was undertaken for each aggregate stability test and for the mean of the three tests. The largest correlation coefficient (r = 0.69, $P = 5.10^{-6}$ significant) was found between the MWD of the crust and that of the sub-crust for the slow wetting test. The correlation coefficients were 0.43 for the fast wetting test (P =0.009, significant), 0.48 for the stirring test (P = 0.003, significant) and 0.59 for the mean of the three tests ($P = 2.10^{-4}$, significant). However, these correlation coefficients were greatly influenced by the very small MWD of site C. Without site C, the correlation coefficients were only 0.52 for the slow wetting (P = 0.003,significant), 0.20 for the fast wetting (P = 0.30), -0.06 for the stirring test (P = 0.75)and 0.28 for the mean of the three tests (P = 0.14). The difference in aggregate stability between a crust and its sub-crust showed the crust was always more stable. The amplitude of this difference varied greatly both for a given site and among the sites (Table 3). For example, for the mean of the three tests, the inter-site coefficient of variation was 0.60 (Table 3a), whereas it ranged from 0.16 (site D4) to 0.90 (site D1) (Table 3b).

298	Variability of standard soil properties
299	All samples had silt content between 65.5 and 73.1% and clay content between 10.0
300	and 14.4% (Figure 3) and thus belonged to the silt loam texture class (Soil Survey
301	Division Staff, 1993). Clay content had little variability between the sampling sites
302	Silt content and sand content presented larger differences between sites, but their
303	inter-site variability was small.
304	There were large differences in gravimetric water contents between crust and sub-
305	crust. The water content of sub-crust was larger than that of crust whatever the site.
306	Crust water content varied between 0.8% (site C) and 11.7% (site D4) while sub-crust
307	water content varied between 10.8% (site D2) and 14.9% (site D4) (Figure 4d). Crust
308	water content varied significantly between sites while sub-crust water content did not
309	differ significantly among the sites (Figure 4d).
310	The organic matter content varied between 0.7% (site D4) and 1.9% (site B)
311	(Figure 4a). The CEC varied between 16.6 cmol kg ⁻¹ (site C) and 27.5 cmol kg ⁻¹
312	(site A) (Figure 4b). The organic matter content and CEC varied significantly between
313	sites. The pH, which ranged between 8.3 and 8.6, did not differ significantly between
314	the sites (Figure 4c).
315	At both intra- and inter-site scales, the percentages of clay, silt and sand
316	(Figure 3), organic matter content, CEC and pH (Figure 4) did not differ significantly
317	between a crust and its corresponding sub-crust.
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319	Relationship between standard soil properties and aggregate stability
320	A correlation analysis was performed between the aggregate stability (MWD) and the
321	soil properties assumed to be potential explanatory factors (Table 4). This analysis

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tests.

322 was performed for the crust (Table 4a) and sub-crust (Table 4b) separately. In both cases, the largest correlation coefficients were found between the MWD of the slow 323 wetting test (0.57, $P = 3.10^{-4}$, significant) and the organic matter content (0.56, P =324 4.10⁻⁴, significant). 325 Clay, silt and sand contents were not significantly correlated with any of the 326 MWD values, either for the crust and sub-crust samples. For the crust, water content, 327 organic matter content and CEC were significantly correlated with the MWD 328 whatever the stability test (Table 4a). For the sub-crust, organic matter content, CEC 329 330 and pH correlated significantly with MWD, except that organic matter content did not correlate significantly with MWD for the stirring test, and pH did not correlate with 331 332 MWD for slow wetting test (Table 4b). 333 A multiple regression analysis was performed using the soil properties (organic 334 matter content, CEC, water content and pH) wich were significantly correlated to aggregate stability. For the crust, among all the combinations tested the best 335 336 regression was found for the mean MWD of the three tests as the dependent variable 337 and the organic carbon content and CEC as explanatory variables: $MWD_{mean}(mm) = 0.39 \ (\pm 0.15) \times SOM \ (\%) + 0.06 \ (\pm 0.02) \times CEC \ (cmol.kg^{-1}) -$ 338 $0.66 (\pm 0.47)$. (1) 339 340 (the number in parenthesis is the standard error). 341 The coefficient of determination (R^2) was 0.38. The residual standard error for the estimated MWD was 0.36 mm at the 95% confidence interval. However, because 342 organic matter content and CEC are significantly correlated, the relevance of the 343 344 proposed relationship is questionable. When CEC is removed from the relationship,

the model explained only 25% of the variance of the MWD for the mean of the three

347	For the sub-crust, among all the tested combinations, the most statistically
348	meaningful regression was found between MWD of the slow wetting test and organic
349	matter content and pH:
350	$MWD_{SW}(mm) = 0.69 \ (\pm 0.17) \times SOM \ (\%) + 1.15 \ (\pm 0.44) \times pH - 9.62 \ (\pm 3.70). \ \ (2)$
351	(the number in parenthesis is the standard error). The coefficient of determination (R^2)
352	was 0.40. The residual standard error for the estimated MWD was 0.43 mm at the
353	95% confidence interval.
354	In order to link the differences in MWD between the crust and the sub-crust
355	materials to the soil properties further, linear correlation analysis was performed
356	(Table 5). Potential explanatory factors were the soil properties as before but also the
357	difference between the crust and the sub-crust for a given soil property.
358	Generally, the differences in stability between the crust and the sub-crust materials
359	were positively correlated with (i) the crust organic matter content and the difference
360	in carbon content between crust and sub-crust, (ii) the crust and sub-crust CEC and
361	(iii) the crust water content. In addition, the differences in stability between the crust
362	and the sub-crust materials were generally negatively correlated with the crust silt
363	content. A multiple regression analysis was performed using the difference in
364	aggregate stability between the crust and sub-crust materials as dependent variable
365	and the soil properties and the differences between each property for the crust and
366	sub-crust as explanatory variables. No statistically meaningful relationship was found.
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Discussion

370 The aggregate stability of a crust is different from the aggregate stability of its

371 *sub-crust*

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To the best of our knowledge, no study has investigated differences in aggregate stability between crust and its underlying material. However, differences in aggregate stability as a function of the crusting stage were investigated by McIntyre (1958) and more recently by Darboux & Le Bissonnais (2007). Using simulated rainfall in the field, McIntyre (1958) showed that crusting decreased the splash rate on sandy loams, concluding that the crust formation processes increased the resistance of soil surface against the breakdown induced by the raindrop impacts. This observation concurs with the results of the stirring test in the present study, where crust had larger MWD than its underlying material for most of the sites (Figure 2c). The same observations were found for the other stability tests (Figure 2b, 2c). Darboux & Le Bissonnais (2007) showed different results in a laboratory experiment. They measured the aggregate stability of a seedbed (non-crusted, initial material), a structural crust and a sedimentary crust, and showed that the stability of structural crust was similar to that of the seedbed. In the present study, the aggregate stability of the structural crust was usually very different from the aggregate stability of the sub-crust irrespective of the sampling site and the stability test. The differences between the results of these two studies may lie in the experimental conditions. Darboux & Le Bissonnais experiment (2007) used a soil with a different texture (11% clay, 58% silt and 31% sand) and well-controlled experimental conditions in a laboratory. The structural crust was formed very rapidly: starting from a seedbed (non-crusted material), they applied a single and intense simulated rain (30 mm.h⁻¹), and obtained a structural crust after only six minutes of rain. Moreover, samples were collected quickly after the rain ended. In our field conditions, crust formation was probably a more gradual and discontinuous process, depending on the duration and intensity of successive rainfalls.

The present crust samples must therefore have gone through numerous cycles of wetting and drying that could lead to additional consolidation.

The amplitude of the difference in aggregate stability between crust and sub-crust varied according to the stability test (Table 3a). The fast wetting test was designed to reproduce the processes of slaking: during rapid wetting, the compression of air entrapped inside the aggregate ruptures the inter-particle bonds within the aggregate and producing small fragments leading to a small MWD (Le Bissonnais, 1996). Sub-crust material was very sensitive to slaking, leading to the smallest MWD, and to the largest differences in MWD between crust and sub-crust (Figure 2a). The amplitudes of difference were least for the differential swelling process involved in the slow wetting test and for the kinetic energy involved in the stirring test (Table 3a, Figure 2). Thus, the fast wetting test was the best discriminator between the crust and sub-crust MWD.

For a given site, water content at the time of sampling was the only variable showing significative differences between crust and sub-crust (Figure 4). However, none of the measured standard soil properties was able to explain the differences in aggregate stability between crust and sub-crust. The crust is directly exposed to atmospheric conditions and may be submitted to a larger amplitude of wetting and drying cycles than the sub-crust. As wetting and drying cycles are an important factor of aggregate stability variation (Cosentino *et al.*, 2006), we can hypothesize that difference in hydric history between crust and sub-crust may explain some of the difference in aggregate stability between these materials. Water content at the time of sampling did not give information about the hydric history of the soil, and thus, could not explain the differences in aggregate stability between crust and sub-crust. The differences may be explained by other variables. Because the crust and sub-crust

originated from the same initial material (a seedbed for the cultivated fields), the differences in stability result necessarily from the crust formation processes. In addition, the presence of carbonates and their crystallization through wetting and drying cycles may also play a role in the crust reinforcement (Fernandez-Ugalde et al., 2011). Those possibilities indicate a need for a time-monitoring of aggregate stability and other variables in both the crust and sub-crust.

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Aggregate stability varied greatly even for sites located on the same soil type within a

429 small area

> In the present study, standard soil properties were not dominant factors controlling aggregate stability. Water content, organic matter content and CEC varied significantly among the sites (Figure 4). Because these variables are known to be related to aggregate stability (Wischmeier & Mannering, 1969; Tisdall & Oades, 1982; Amézketa, 1999; Zhang & Horn, 2001), it might have been expected that the variability in aggregate stability could be explained by these properties. None of these variables (or their combination) was able to satisfactorily predict the aggregate stability of the crust or sub-crust. At best, only 40% of the variability could be explained and this had a residual standard error of approximately 0.4 mm. Hence, the predicted MWD could be wrong by as much as two stability classes (out of five stability classes) (Figure 2). Consequently, these relationships have no practical use for prediction, and their use would probably lead to large flaws in the interpretations.

> Land use and site environmental conditions may have caused the differences in stability among the sites without affecting the standard soil properties. Variables known to affect aggregate stability, but not commonly noted, include tillage, crop management or mulching through their effect on microbial activity and soil water

content (Amézketa, 1999). Altitude, slope position and orientation influence local climate which can affect aggregate stability through soil hydric history (Amézketa, 1999; Cosentino *et al.*, 2006). The current experimental design did not allow us to study precisely the influence of topography or location. However, we can note that sites A and D1 that had the largest MWD for both crust and sub-crust were located on the lowest slopes. Even more than hydric history, topography can affect flow and transport history of the material which in return affects aggregate stability (Amézkéta, 1999). In future studies, variables such as the organic matter quality, microbial activity, wetting-drying cycles and topography may need to be considered.

The heterogeneity of the aggregate stability measured in the crust samples was less than that measured in the sub-crust samples. This finding was consistent in the inter-site comparison and often observed in the intra-site comparison. The crust had larger MWD on average and larger standard deviation than the sub-crust (Table 2). As the observed aggregate system is physically constrained by full dispersion of the particles (the MWD of a fully dispersed loamy soil may be around 0.2 mm), it may have been expected that CV values would decrease with increasing MWD. However, our analysis did not identify correlations between the standard deviation and the mean MWD, nor negative correlations between the mean MWD and the CV. Hence, the smaller heterogeneity of crust aggregate stability than of that of the sub-crust may not be related to the CV calculation. The development of the crust could have decreased the spatial heterogeneity of aggregate stability. This assumption has to be examined in future studies.

Consequences for erodibility assessment and erosion modelling

When used for erodibility assessment, aggregate stability is usually measured in the sub-crust material (Bullock *et al.*, 1988; Bajracharya & Lal, 1998; Barthès & Roose, 2002; Legout *et al.*, 2005). The finding that the crust is generally less erodible than the sub-crust strongly suggests that erodibility should be assessed on the material actually exposed to erosive forces: the soil surface. The common practice of using the underlying material, instead of the crust, would cause an over-estimate by at least one erodibility class in 60% of cases and by at least two erodibility classes in 30% of cases of our soil (Figure 2).

In erosion models, erodibility can be assessed with soil standard properties such as soil texture and organic matter content through statistical functions (Alberts *et al.*, 1995; Renard *et al.*, 1997). Such an approach assumes that samples collected from the same soil type have similar erodibilities (Gumiere *et al.*, 2009). Because a single soil type was investigated in the present study, a similar erodibility would have been expected. This was clearly not the case. This finding underlines the large uncertainty in the prediction of erodibility when assessed using standard soil properties. Currently, parameterization of erosion models sets a single erodibility value for a given soil and thus does not consider the variability of erodibility within a given soil. This oversimplification could explain part of the large inaccuracy in the predicted results of erosion models (Jetten *et al.*, 2003). Comparisons between the seven sites showed that the heterogeneity of the crust was less than that of the sub-crust. Using crust samples for erodibility assessment, would decrease the heterogeneity of the mapped erodibility (although this heterogeneity would remain large).

Conclusions

Crust showed a greater aggregate stability than its underlying material. This finding emphasizes the importance of estimating soil interrill erodibility on the soil surface material. On a crusted soil, the use of material collected from the plough layer may lead to greatly over-estimated erodibility and thus bias the results of the erosion models. The large heterogeneity in aggregate stability among sites proves that erodibility can greatly vary in space, even when considering a small test area and a single soil type. From the present study, we conclude that interrill erodibility assessment should ideally be performed with a large sampling density, which could be impractical, leaving the construction of a sound erodibility map currently unattainable. The fact that standard soil properties were not able to accurately predict the observed differences in aggregate stability lead us to suggest investigating other variables such as (i) the soil hydric history linked to local climatic conditions, (ii) environmental factors such as topography and (iii) the physical processes involved in crust formation. Factors that affect the erodibility of the soil surface should be better understood so that reliable erodibility maps can be produced from a reasonably small set of measurements.

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deforestation on the Loess Plateau. Pedosphere, 15, 707-715.

602 **Table 1** Site locations and land uses

Site	Geographic location	Land use and slope position	Altitude / m	Orientation	Slope gradient
	(latitude; longitude)				(field scale)
A	36°03.888' N; 109°12.621' E	Cultivated maize field, upslope	1053	Е	5° - 10°
В	36°03.874′ N; 109°12.675′ E	Apple orchard, shoulder of a terrace	1118	SW	5° - 30°
C	36°04.227' N; 109°11.226' E	Cultivated radish crop, middle slope, sampling in ridges and furrows	1206	SE	5° - 13°
D1	36°05.149' N; 109°8.958' E	Ziwuling experimental station, bare soil, upslope, interrill area	1270	SW	5° - 10°
D2	36°05.431' N; 109°8.951' E	Ziwuling experimental station, bare soil, mid-slope, rill area	1245	SW	30° - 35°
D3	36°05.450' N; 109°8.947' E	Ziwuling experimental station, bare soil, 20 m from foot slope, ephemeral gully area	1180	SW	25° - 35°
D4	36°05.460' N; 109°8.884' E	Ziwuling experimental station, bare soil, 10 m from foot slope, gully area	1154	SW	35° - 40°

Table 2 Heterogeneity of the mean weighted diameter among the sampling sites (inter-site heterogeneity) for the fast wetting test, the slow wetting test, the stirring test and the mean of the three tests. Mean of the MWD corresponds to the mean of five

		MW	D of the cr							
Stability test	Min.	Max.	Mean	σ^{a}	CV ^b	Min.	Max.	Mean	σ	CV
	/mm	/ mm	/ mm	/ m)		/ mm	/ mm	/ mm	/ mm	
Fast wetting	0.20	1.62	0.98	0.41	0.42	0.13	0.95	0.36	0.18	0.51
Slow wetting	0.41	2.22	1.47	0.52	0.36	0.22	1.93	0.97	0.52	0.54
Stirring	0.29	1.77	1.14	0.41	0.39	0.23	1.23	0.69	0.27	0.39
Mean of the 3 tests	e 3 tests 0.33 2.04 1.20 0.44 0.37						1.42	0.68	0.32	0.47

plots with two replicates each, n=10.

^aσ: standard deviation; ^bCV: coefficient of variation. 603

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Table 3 Heterogeneity of the difference in mean weighted diameter between crust and sub-crust (a) among the sampling sites (inter-site heterogeneity) for all stability tests, and (b) for each site (intra-site heterogeneity) for the mean of the three stability tests. Mean of the MWD corresponds to the mean of five plots with two replicates each, n=10.

(a) 609

Difference in MWD	between cri	ust and sub-crust
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Stability test	Min.	Max.	Mean	σ	CV
	/ mm	/ mm	/ mm	/ mm	
Fast wetting	0.10	1.04	0.62	0.35	0.56
Slow wetting	0.24	1.03	0.50	0.30	0.60
Stirring	0.00	0.81	0.45	0.32	0.71
Mean of the 3 tests	0.16	0.93	0.46	0.28	0.60

^aσ: standard deviation; ^bCV: coefficient of variation.

(b) 611

Difference in MWD between crust and sub-crust

Site	Min.	Max.	Mean	σ	CV
	/ mm	/ mm	/ mm	/ mm	
\mathbf{A}	0.61	0.90	0.80	0.12	0.22
В	0.44	1.24	0.77	0.30	0.39
\mathbf{C}	0.09	0.27	0.16	0.07	0.45
D1	0.08	1.25	0.52	0.47	0.90
D2	0.08	0.59	0.31	0.27	0.87
D3	0.05	0.40	0.18	0.14	0.76
D4	0.83	1.13	0.93	0.15	0.16

^aσ: standard deviation; ^bCV: coefficient of variation.

Table 4 Correlations (Pearson's coefficient) between aggregate stability and standard

soil properties (a) for the crust and (b) for the sub-crust. 614

615 (a)

MWD	Water content	Organic matter	CEC	pН	Clay content	Silt content	Sand content
Fast wetting	0.35	0.50	0.50	0.11	0.08	-0.31	0.21
Slow wetting	0.32	0.57	0.46	0.22	0.09	-0.18	0.11
Stirring	0.45	0.42	0.56	0.20	0.14	-0.16	0.06
Mean of the three tests	0.36	0.52	0.52	0.18	-0.10	-0.22	0.13

616 n=35; $\alpha=5\%$: r=0.32

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bold = significant at the 5% level 617

618 (b)

MWD	Water content	Organic matter	CEC	pН	Clay content	Silt content	Sand content
Fast wetting	-0.11	0.51	0.44	0.19	0.12	0.09	-0.07
Slow wetting	-0.17	0.56	0.44	0.41	0.04	-0.12	0.11
Stirring	-0.05	0.22	0.46	0.47	0.28	0.29	-0.29
Mean of the three tests	-0.13	0.49	0.48	0.41	0.13	0.03	-0.04

N = 35; $\alpha = 5\%$: r = 0.32619

bold = significant at the 5% level

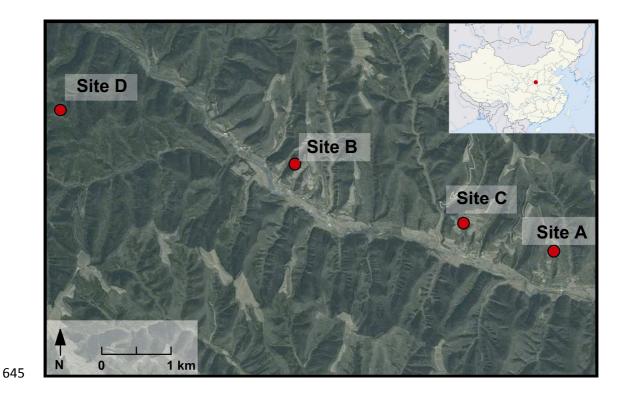
Table 5 Correlations (Pearson's coefficient) between the differences in aggregate stability between crust and sub-crust and the standard soil properties. 621

Difference in	V	Vater cont	content Organic matter CEC			pH Clay content					S	ilt Cont	ent	Sand content							
MWD	C	U	C-U	C	U	C-U	C	U	C-U	C	U	C-U	C	U	C-U	C	U	C-U	C	U	C-U
Fast wetting	0.40	0.29	0.30	0.40	0.27	0.29	0.45	0.45	-0.16	0.04	0.16	0.09	-0.07	0.20	-0.21	-0.46	-0.26	-0.23	0.37	0.16	0.23
Slow wetting	0.32	0.42	0.09	0.18	-0.01	0.42	0.12	0.15	-0.10	-0.19	-0.07	-0.11	-0.21	0.25	-0.35	-0.22	-0.04	-0.25	0.23	-0.06	0.36
Stirring	0.40	0.26	0.32	0.40	0.29	0.29	0.35	0.33	-0.07	-0.01	-0.28	-0.06	-0.19	0.09	-0.21	-0.48	-0.32	-0.16	0.42	0.23	0.19
Mean of the 3tests	0.36	0.30	0.26	0.34	0.19	0.37	0.33	0.33	-0.12	-0.06	0.05	-0.10	-0.17	0.20	-0.28	-0.41	0.22	-0.23	0.36	0.11	0.28

C=crust; U=sub-crust; C-U=difference in soil property value between the crust and the sub-crust. N = 35; α = 5%: \underline{r} = 0.32

Bold = significant at the 5%. 624

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646 **Figure 1** Location of the study sites.

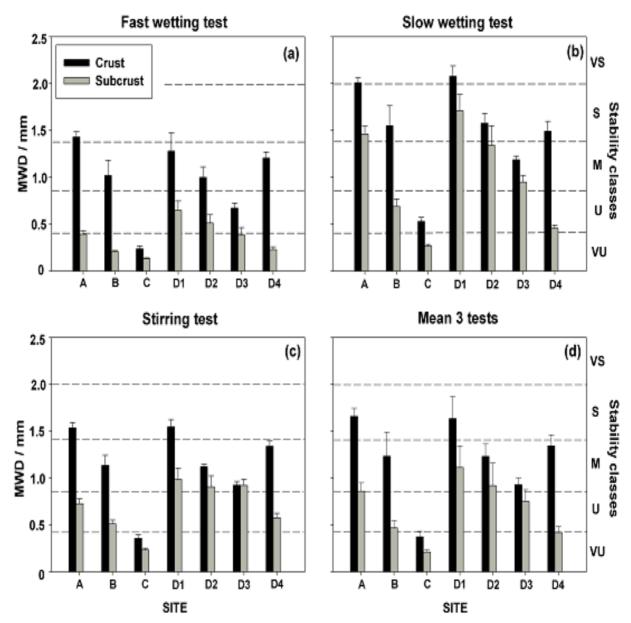


Figure 2 Aggregate stability of crust and sub-crust for (a) fast wetting, (b) slow wetting, (c) stirring tests and (d) the mean of the three tests for all sites. Each MWD corresponds to the mean of five plots with two replicates each, n=10. Bars represent

standard errors.

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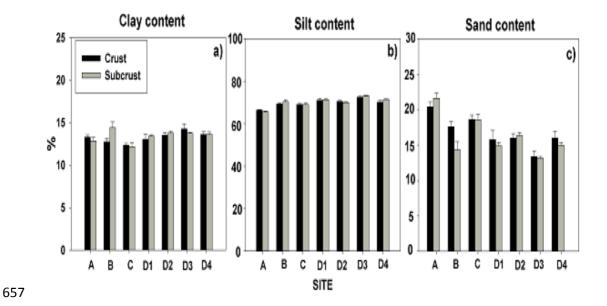


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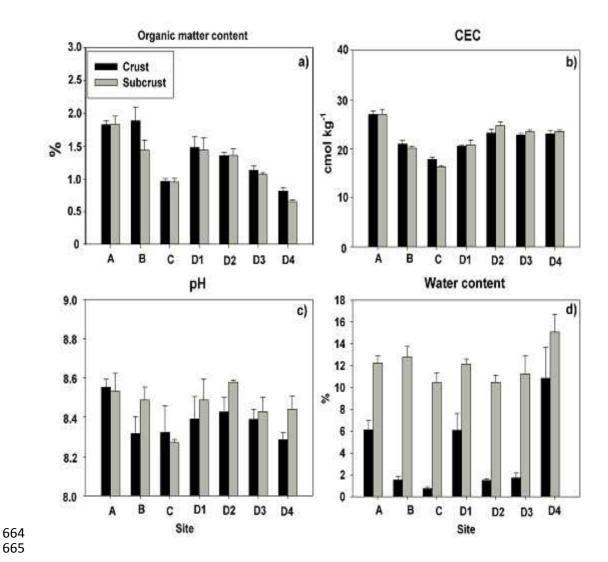


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