

Briefs

An Improved Forward I - V Method for Nonideal Schottky Diodes with High Series Resistance

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Abstract—Two methods are described to obtain the value of the series resistance (R) of a Schottky diode from its forward I - V characteristic. The value of R is then used to plot the curve $\ln(I)$ versus $V_D (=V - IR)$ which becomes a straight line even if $\ln(I)$ versus V does not. The ideality factor n and the Schottky-barrier height ϕ_{B0} of the diode then follow from the standard procedure. The main advantages of the methods are: 1) a linear regression can be used to calculate the value of R , 2) many data points are used over the whole data range which raises the accuracy of the results, and 3) the validity of constant R assumption can be checked by the linearity of the $\ln(I)$ versus V_D curve. The methods are illustrated on the experimental data of a real diode.

I. INTRODUCTION

For a real Schottky diode, the I - V characteristic (see, e.g., Fig. 1) is often approximated by

$$I = I_s \left(\exp\left(\frac{\beta V_D}{n}\right) - 1 \right) \approx I_s \exp\left(\frac{\beta V_D}{n}\right) \quad (1)$$

(for $\beta V_D \gg 1$),¹ where n is the ideality factor, V_D is the voltage across the diode, $\beta = q/kT$, and

$$I_s = AA^{**} T^2 \exp(-\beta \phi_{B0}) = I_0 \exp(-\beta \phi_{B0})$$

and the applied voltage V is assumed to differ from V_D by a value IR (i.e., $V_D = V - IR$), where R is defined as the series resistance of the diode. A well-established method of determining the barrier height ϕ_{B0} and the ideality factor n is to make a $\ln(I)$ versus V plot. For voltages larger than several kT/q and small R , this plot will be a straight line whose slope and extrapolated intercept with the zero voltage axis can be used to calculate the ideality factor and the barrier height (standard I - V method).

As the series resistance increases, the linear region in the $\ln(I)$ versus V plot shrinks resulting in an inaccurate measurement of n and ϕ_{B0} . To remedy this difficulty, Norde [1] has proposed a modified method for the case of a Schottky diode with $n = 1$ by finding the minimum of the function

$$F(V) = 0.5 V - \frac{1}{\beta} \ln\left(\frac{I(V)}{I_0}\right).$$

The disadvantages of the Norde method are that 1) the ideality factor is assumed to be unity, which is not always true for a real diode, and 2) a few data points near the minimum of $F(V)$ are actually used to calculate the barrier height. This latter fact tends to increase the statistical error of the result.

Here we suggest two methods to obtain the value of R and

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¹See, e.g., S. M. Sze, *Physics of Semiconductor Devices*, 2nd ed. New York: Wiley, 1982.

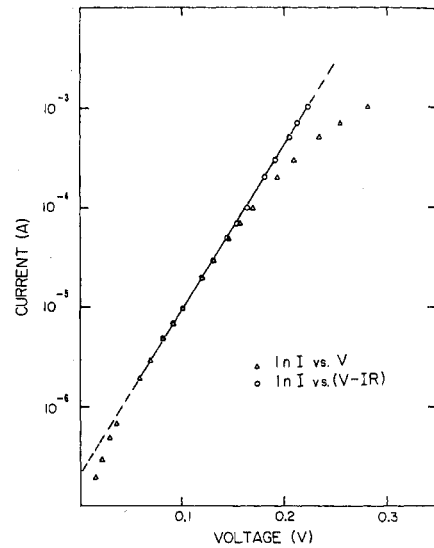


Fig. 1. Experimental data of $\ln(I)$ versus V (triangles) for a $\text{Ni}_{36}\text{W}_{64}/\text{Si}$ Schottky diode on an n-type (100) Si. $T = 20^\circ\text{C}$, $A^{**} = 112 \text{ A} \cdot \text{K}^{-1} \cdot \text{cm}^{-2}$, and $A = 1.97 \times 10^{-3} \text{ cm}^2$ are used here. Using $R = 58.3 \Omega$, we have plotted the $\ln(I)$ versus $V_D (=V - IR)$ (circles) curve which yields $n = 1.05$, and $\phi_{B0} = 0.63 \text{ V}$.

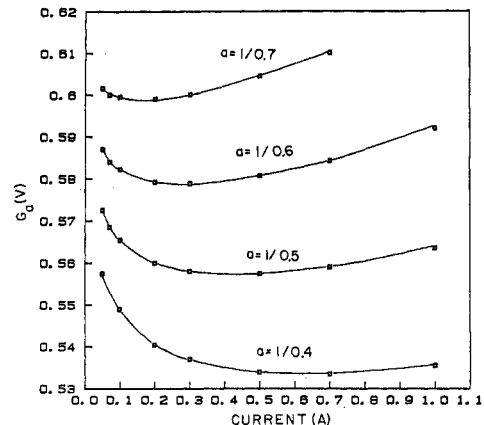


Fig. 2. $G_a(I)$, calculated from the I - V data shown in Fig. 1, are plotted against I for several a 's. For each a , $G_a(I)$ has a minimum at $I = I_a$.

to use this R to plot the $\ln(I)$ versus V_D curve. The standard I - V method is then used to obtain the values of n and ϕ_{B0} .

II. METHOD

The first method used to obtain the series resistance by plotting several Norde-type functions

$$F_a(V) = V/a - \frac{1}{\beta} \ln\left(\frac{I(V)}{I_0}\right) \quad (2)$$

versus I (for $\beta V_D \gg 1$) and finding the minimum point of each F_a for several a 's, given ranges from n (ideality factor) to ∞ (see e.g., Fig. 2). Since V is a strictly monotonic function of I , F_a can also be viewed as a function of I , viz., $G_a(I) = F_a(V)$.

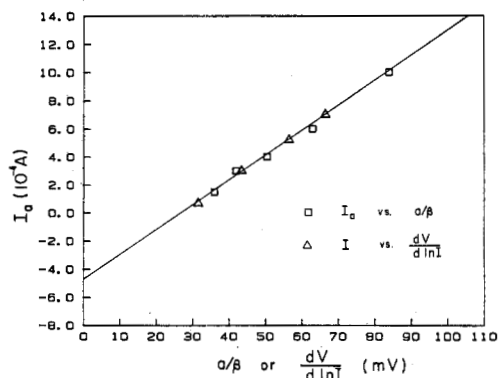


Fig. 3. I_a , obtained from Fig. 2, are plotted against a/β (squares). The triangles are the data calculated from the second method as discussed in the text, i.e., I versus $dV/d \ln(I)$. The calculated resistance value R is equal to 58.3Ω .

It turns out to be convenient to consider $G_a(I)$ rather than $F_a(V)$ because (4) contains I , not V . $G_a(I)$ has a minimum that (for each a ranging from n to ∞) occurs when $dG_a(I)/dI = 0$, (assuming this occurred at $I = I_a$), i.e.,

$$\frac{dG_a(I_a)}{dI_a} = \frac{1}{a} \frac{dV_a}{dI_a} - \frac{1}{\beta I_a} = 0. \quad (3)$$

This equation together with (1) results in

$$I_a = \frac{1}{R\beta} a - \frac{n}{R\beta}. \quad (4)$$

This equation shows that a plot of I_a versus a is a straight line (see e.g., Fig. 3) whose slope can be used to determine the value of R and whose extrapolated intercept is at $I_a = 0$ given n . The advantage of using a set of different values of a , rather than only one, resides in the fact that such a plot makes use of an extended range of data points of the I - V characteristic. This plot also tests the assumption that the real diode can be modeled as a purely exponential characteristic diode in series with a constant resistance. In practice, if a linear relationship between I_a and a is observed, this plot is best used to obtain the value R ; n is more accurately determined subsequently from the corrected I - V characteristic.

The second method is based on (3), which states that $a^{-1} = (1/\beta)d \ln(I)/dV$ at $I = I_a$. This means that the parameter a can be obtained for any given current $I = I_a$ by taking the derivatives of the measured I - V characteristic at this point. That procedure is easy to carry out on computerized I - V plotters or with computer fitting of experimental data. An explicit evaluation of G_a or F_a as it is required in the Norde method is thus bypassed. With the parameter a known for any value of I_a , the method again allows one to plot the relationship of (4) and derive the value of R . Obviously, mathematically the second method should yield the same I_a versus a plot as the first method.

Once the value of R has been established by either method, its contribution to the experimental data points can be subtracted. After this subtraction, within experimental uncertainties, the characteristic should yield the straight line predicted by (1). This outcome means that the model of a purely exponential characteristic diode in series with a constant resistance is consistent with the data. Accurate values of Φ_{B0} and n can then be determined from this corrected characteristic.

As an example, Fig. 1 shows an experimental I - V characteristic (triangles) of a Schottky diode plotted semi-logarithmi-

cally. There is no linear region in this plot to allow for a reliable barrier height and ideality factor determination. Fig. 2 shows $G_a(I)$ versus I curves for various a . The values of I at the minimum points of G_a , defined as I_a , are then plotted against a/β as shown in Fig. 3 (squares). The triangles shown in Fig. 3 are calculated by the second method, i.e., I versus $dV/d \ln(I)$. The data derived from both methods agree very well. The fitted value of R is 58.3Ω . Using this value of R , we have plotted the $\ln(I)$ versus $V_D (=V - IR)$ data (circles) shown in Fig. 1. The ideality factor and barrier height are then determined by the standard method, which yields $n = 1.05$ and $\phi_{B0} = 0.63$ V. The linearity of the plots in Figs. 1 and 3 shows that the assumption of a constant series resistance and a purely exponential characteristic diode is good over the range of operating points considered.

III. CONCLUSION

We have proposed an improved forward I - V method to calculate the series resistance, ideality factor, and barrier height of a Schottky diode. Applying this method to experimental data of a real diode, we obtain quite a good result.

ACKNOWLEDGMENT

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Temperature Dependence of the Nonideal Component of Base Current in Micropower n-p-n Transistors

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Abstract—The low-temperature dependence of the nonideal base current component has been studied in low-concentration emitter n-p-n Si transistors. Under forward bias, below a certain temperature, ideality factors greater than 2 have been found and h_{FE} roll-off characteristics deviate from a S-R-H recombination model.

INTRODUCTION

The behavior of n-p-n BJT's at very low currents is of great interest concerning micropower applications, bipolar VLSI devices, and parasitic effects modeling. The nonideal component of base current sets the limit for transistor operation at very low currents, and its origin is still under controversy. Most of the published works refer to room-temperature measurements and they treat forward and reverse B - E junction behavior separately. There is general agreement that reverse I_B - V_{BE} characteristics diverge from ideal Shockley theory due to metallic precipitates that cause a field-dependent generation-recombination mechanism [1], [2]. However, for

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