

Analysis of the Effect of Clock Drifts on Frequency Regulation and Power Sharing in Inverter-based Islanded Microgrids

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Abstract—Local hardware clocks in physically distributed computation devices hardly ever agree because clocks drift apart and the drift can be different for each device. This paper analyses the effect that local clock drifts have in the parallel operation of voltage source inverters (VSIs) in islanded microgrids (MG). The state-of-the-art control policies for frequency regulation and active power sharing in VSIs-based MGs are reviewed and selected prototype policies are then re-formulated in terms of clock drifts. Next, steady-state properties for these policies are analyzed. For each of the policies, analytical expressions are developed to provide an exact quantification of the impact that drifts have on frequency and active power equilibrium points. In addition, a closed-loop model that accommodates all the policies is derived, and the stability of the equilibrium points is characterized in terms of the clock drifts. Finally, the implementation of the analyzed policies in a laboratory MG provides experimental results that confirm the theoretical analysis.

Index Terms—Microgrids, islanded mode, distributed control, frequency regulation, active power sharing, clock drifts, performance evaluation

I. INTRODUCTION

Computation devices are equipped with hardware clocks which run at a not necessarily identical speed. As a consequence, clocks of distributed devices may differ [1]. This situation leads to inaccurate and inefficient performance of many applications and protocols in distributed systems [2].

Microgrids (MGs), that are composed by distributed generation units, loads and storage systems [3] operated with digital computation and communication technology [4]–[7], may also suffer from drifting clocks. This paper investigates the effect of local clock drifts on the parallel operation of voltage source inverters (VSIs) in islanded MGs, with emphasis on frequency regulation and active power sharing. The accomplishment of these two control goals can be achieved following different strategies [8]–[10]. Among them, several approaches follow a standard hierarchical control architecture [11], [12] where primary control applies the well-known droop method [13]–[15] to achieve active power sharing while secondary control (in different forms, see e.g. [16]–[24]) corrects the steady-state

frequency deviation introduced by the droop using an integral-like control. Alternatively, recent approaches have considered different strategies where the hierarchical approach is avoided, e.g. [25], [26].

The impact of clocks drifts in frequency control and power sharing in MG has been recently investigated in [27]–[32]. The work in [27] shows that droop-controlled VSI-based MG are robust to clock drifts, although small steady-state deviations in active power sharing are observed. An extension providing a deeper modeling, analysis and experimental validation is presented in [29]. In [28] it is shown that local clock drifts in local integral controllers designed for frequency regulation make the MG unstable, results that are illustrated with simulations. The work by [30] provides an steady-state analysis of several distributed secondary frequency control strategies with consideration to clock drifts, illustrated with simulation results. In [31], and focusing in angle droop control, stabilizing controllers based in consensus are derived to remove the negative effects that drifts have on frequency control and power sharing. Simulation results are also used to corroborate the control proposal. Finally, [32] analyses the impact of clock drifts on local secondary control schemes that do not exchange control data.

The contribution of this paper is to provide a theoretical and experimental analysis of state-of-the-art control policies for parallel operation of VSIs in islanded MG. The analysis focuses on steady-state properties of the frequency control and active power sharing, as well as on stability properties considering clock drifts. It covers the results presented in [27]–[30], and extends them with additional policies, with steady-state expressions of the equilibrium points, with a robust stability characterization of the equilibrium points, and/or with experimental validation. In addition, it complements the analysis of local policies given in [32] because the focus of this paper is mainly on control schemes that exchange control data to accomplish the frequency control. Note however that the specific effect that communications have in the performance of the analyzed polices has not characterized. The performance evaluation paper [33] focuses on this topic.

The paper is structured as follows. The problem formulation is given in Section II. A set of representative prototype policies for frequency restoration and active power sharing are selected in Section III. The MG steady-state equilibrium points in the presence of drifts are analyzed in Section IV and analytical expressions that relate the steady-state frequency

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and active power of each policy as a function of the VSI local clock drifts are provided. Section V presents the closed-loop modeling approach and stability analysis considering clock drifts. Experimental results on a laboratory MG reported in Section VI illustrate the operation of the reviewed policies, corroborating the theoretical analysis. Conclusions are summarized in Section VII.

II. PROBLEM FORMULATION

The MG system considered in this paper is a power network that gathers distributed generation (DG) units, inverters, loads and storage elements that can operate in grid-connected or islanded mode. The analysis of MG system can be made using the standard power flow equations for n inverters given by [34]

$$P_i(t) = G_{ii}V_i^{*2}(t) - \sum_{j=1}^n (G_{ij} \cos(\Phi_i(t) - \Phi_j(t)) + B_{ij} \sin(\Phi_i(t) - \Phi_j(t))) V_j^*(t) V_i^*(t) \quad (1)$$

$$Q_i(t) = -B_{ii}V_i^{*2}(t) - \sum_{j=1}^n (B_{ij} \cos(\Phi_i(t) - \Phi_j(t)) - G_{ij} \sin(\Phi_i(t) - \Phi_j(t))) V_j^*(t) V_i^*(t) \quad (2)$$

where $P_i(t)$ and $Q_i(t)$ are the active and reactive power injections of the i^{th} inverter, G_{ii} and B_{ii} are the real and imaginary parts of the local admittance, G_{ij} and B_{ij} are the real and imaginary parts of the line admittance, $V_i^*(t)$ is the inverter computed set-point voltage amplitude, and Φ_i is the inverter voltage phase given by

$$\Phi_i(t) = \int \omega_i^*(t) dt \quad (3)$$

where $\omega_i^*(t)$ is each inverter computed set-point voltage frequency. Figure 1 provides a conceptual block diagram of the MG where the plant, named H , is modeled using (1)-(2), having as inputs the set of set-point frequencies and amplitudes, $\omega_i^*(t)$ and $V_i^*(t)$ respectively, and the active and reactive power as outputs, P_i and Q_i respectively. Henceforth, the paper focuses on frequency regulation and active power sharing in islanded MGs while voltage amplitude and reactive power control is deliberately omitted because no standard policy has been recognized to be the best and required practice, as it can be concluded from [10].

Figure 2 illustrates the type of MG adopted in this paper, highlighting the main parts being considered like buses (thick lines), interconnection between them (thin lines), loads (arrows) and inverter-based DGs (dashed boxes). The figure highlights the fact that each inverter, and more specifically, each micro-processor is driven by a local clock.

In each i^{th} inverter, $\omega_i^*(t)$ is calculated by the micro-processor with local measures (and possibly data received from other VSIs) in local time coordinates t_i given by local clocks. Let the time progression at each VSI be defined as a function of the global time. Specifically, let $t_i \in \mathbb{R}^+$ denote the local times at each inverter and let $t \in \mathbb{R}^+$ denote the global time. Hence, VSIs local times can be described by

$$t_i = d_i t \quad (4)$$

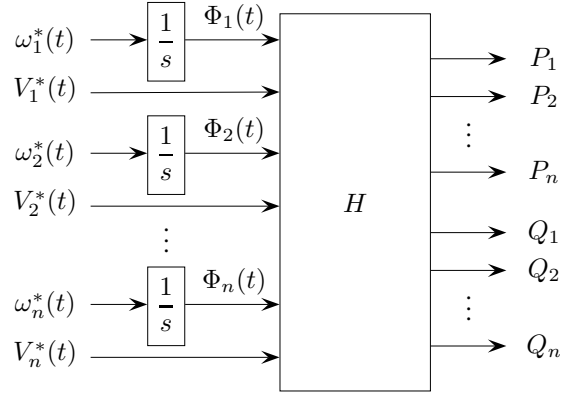


Fig. 1: Block diagram of the plant

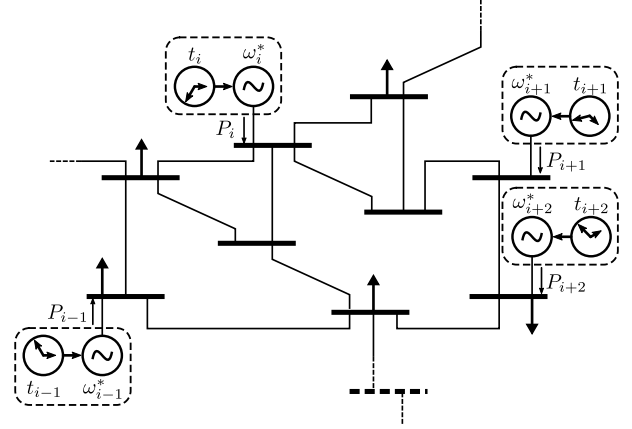


Fig. 2: Scheme of the inverter-based islanded microgrid

where d_i is the drift rate of the i^{th} VSI local clock and it denotes the rate (frequency) of the clock. Note that in the local time definition (4), the clock offset is explicitly omitted. The offset is the difference in value from local time t_i to global time t . This is done on purpose because although not all clocks are initially synchronized, i.e. $t_{0,i}$ is not the same for all VSI, local clocks are occasionally synchronized due to the phase-locked loop connection of each VSI.

In the absence of global time, the set-point frequencies $\omega_i^*(t)$ generated by the digital controllers differ between them [29]. Applying different set-point frequencies to the standard power flow equation of the active power (1) it can be observed that the P_i steady-state values deviate. Consider the standard approximation that assumes that when phases $\Phi_i(t)$ are similar, then

$$\begin{cases} \cos(\Phi_i(t) - \Phi_j(t)) \simeq \cos(0) = 1 \\ \sin(\Phi_i(t) - \Phi_j(t)) \simeq \Phi_i(t) - \Phi_j(t) \end{cases}$$

Then the active power (1) (and considering (3)) evolves to

$$P_i(t) = G_{ii}V_i^{*2}(t) - \sum_{j=1}^n (G_{ij} + B_{ij} \int \omega_i^*(t) - \omega_j^*(t) dt) V_j^*(t) V_i^*(t) \quad (5)$$

That is, P_i values at each inverter will not settle if the set-point frequencies $\omega_i^*(t)$ and $\omega_j^*(t)$ are different. The integral

will increase (or decrease) infinitely, that is, no equilibrium point exists due to local clock drifts in open-loop operation.

The problem to be solved is to analyze if existing control strategies for frequency regulation and active power sharing are able to cope with this undesired unstable scenario and quantify their performance as a function of clock drifts.

III. FREQUENCY CONTROL AND POWER SHARING

A. Selected policies

The most common approach to the regulation of voltage frequency and amplitude in the parallel operation of VSIs is achieved by computing the set-point frequency $\omega_i^*(t)$ and amplitude $V^*(t)$ for the inverter current and voltage internal control loops. For power sharing, the droop method [13] is commonly applied, which is given by

$$\omega_i^*(t) = \omega_0 - m_p P_i(t) \quad (6)$$

$$V_i^*(t) = V_0 - n_q Q_i(t) \quad (7)$$

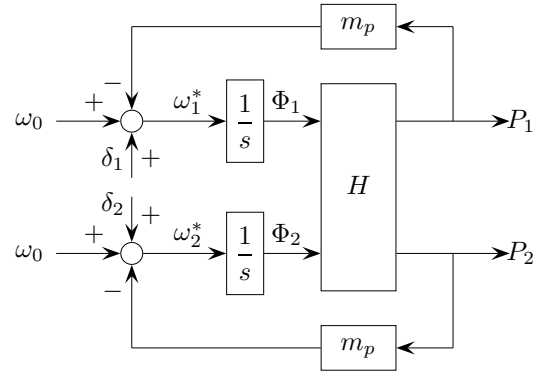
where ω_0 and V_0 are the nominal voltage frequency and amplitude, $P_i(t)$ and $Q_i(t)$ are the inverter output active and reactive power, m_p and n_q are the proportional control gains, and equation (6) is called frequency droop control and equation (7) is called voltage droop control. In the standard definition of droop, which corresponds to (6) and (7), control actions are done relative to a desired active and reactive power set-point, P_{0i} and Q_{0i} respectively [13], which is determined by long-term objectives (e.g. tertiary control). In (6)-(7) these set-points have been omitted but their inclusion does not alter the paper results. In addition, the measured rather than the normalized values for active and reactive power are used because working with dimensionless values could hide the real impact of clock drifts. Hence, without losing generality, all inverters are assumed to have the same nominal power. Both droop methods (6) and (7) introduce deviations in the frequency and amplitude, to be corrected by the secondary control. Since the paper restricts the focus on frequency regulation and active power sharing, the considered droop control is (6). It will be further complemented with a corrective term for frequency restoration, thus leading to different secondary control policies. The standard voltage droop control (7) will not be further complemented. By fixing this policy, a common comparison framework is established for performance evaluation.

The analyzed policies that apply together with the droop method (6), namely droop-based policies, will be based on

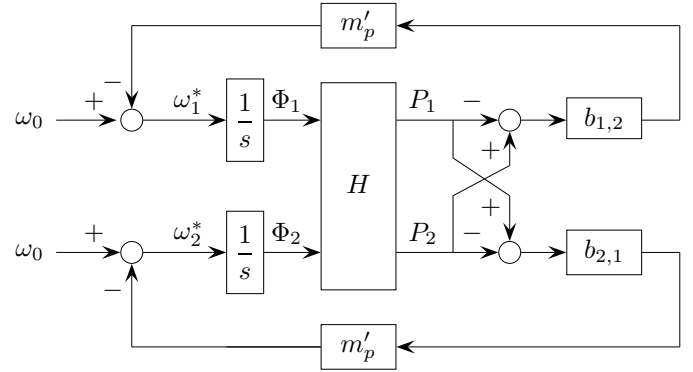
$$\omega_i^*(t) = \omega_0 - m_p P_i(t) + \delta_i(t) \quad (8)$$

where $\delta_i(t)$ is a corrective term that operates as an integral-like control of the frequency error, and it determines the features of the complete control scheme. For completeness, the analysis also considers a recent alternative approach for frequency regulation and power sharing named droop-free [25], where the nominal frequency is modified by a proportional function of the inverter output active power $P_i(t)$ and the rest of $n-1$ MG inverters active power $P_j(t)$, provided that communications are available. It has the form

$$\omega_i^*(t) = \omega_0 + m'_p \sum_{j=1}^n b_{i,j} (P_j(t) - P_i(t)) \quad (9)$$



(a) Droop-based policies (8)



(b) Droop-free policy (9)

Fig. 3: Block diagram for the droop-based and droop-free policies for the case of two inverters.

where m'_p is the control gain and $b_{i,j}$ are communication weights that are also design parameters that specify the connectivity structure of the MG. Both droop-based (8) and droop-free (9) policies are illustrated as block diagrams in Figure 3 for the case of two inverters. For each policy, the top loop corresponds to one inverter and the bottom loop corresponds to the other inverter. It can be observed that in the droop-based policies the corrective terms δ_1 and δ_2 have not been specified yet. For the droop-free policy, it can be observed the exchange of active power P_1 and P_2 that takes place among the two inverters.

Table I summarizes the evaluated policies that are introduced next, being some of them also illustrated as block diagrams in Figure 4 for the case of two inverters. The first policy, termed as *Droop-only* control, is the standard droop method locally implemented at each inverter (with $\delta_i(t) = 0$ in (8), sub-figure 3a). Although for this policy the effects of drifts were analyzed in [27], it is included in the analysis to serve as a baseline policy for comparative purposes. The next policy termed *Local-integrals* is the straightforward extension of the *Droop-only* to secondary control because each corrective term given in (12) is an integral controller of the local frequency error locally computed at each VSI (sub-figure 4a).

TABLE I: MG control policies under evaluation

Policy	Control	Correction term ($\delta_i(t) =$)
Droop-only	(8)	0
Local-integrals	(8)	$k_{II} \int_0^t (\omega_0 - \omega_i^*(t)) dt$ (12)
Centralized	(8)	$k_{IC} \int_0^t (\omega_0 - \omega_m^*(t)) dt$ (13)
Decentralized	(8)	$k_{Id} \int_0^t (\omega_0 - \omega_m^*(t)) dt$ (14)
Averaging	(8)	$k_{Ia} \int_0^t (\omega_0 - \omega_a^*(t)) dt$ (15)
Consensus	(8)	$k_c \int_0^t (\omega_0 - \omega_i^*(t) + \alpha (\delta_a(t) - \delta_i(t))) dt$ (16)
Droop-free	(9)	0

A preliminary drift analysis for this policy is in [28].

The next four policies implement different secondary control policies with specific local integral controls ((13)-(16) in Table I) with a common denominator: they rely on a communication infrastructure linking VSI for the exchange of control data (the communication paths are marked with dashed blue lines in Sub-figures 4b-4e). In the policy termed as *Centralized* the corrective term (13) that is used at each VSI, namely $\delta_m(t)$, is again an integral controller of the frequency error computed in a central control unit, often called MGCC (MG central controller) [11], using its set-point frequency $\omega_m^*(t)$. The $\delta_m(t)$ term is then sent to each VSI for droop control (8) (sub-figure 4b) In the *Decentralized* control policy (see the overview given e.g. in [18]) the frequency error in (14) is calculated at each VSI using the received set-point frequency computed and sent by the MGCC, $\omega_m^*(t)$ (sub-figure 4c). In the *Averaging* control policy (see [24] or [19] for DC MG) the corrective term (15) is calculated at each VSI using the averaged set-point frequency computed as

$$\omega_a^*(t) = \frac{1}{n} \sum_{j=1}^n \omega_j^*(t) \quad (10)$$

where $n - 1$ frequencies have been received from the others MG VSIs (sub-figure 4d). The *Consensus* control policy (see for example [20], sub-figure 4e) is characterized by a correction term (16) that considers two errors, the frequency one, $\omega_0 - \omega_i^*(t)$, and the error on the correction term, $\delta_a(t) - \delta_i(t)$, where

$$\delta_a(t) = \frac{1}{n} \sum_{j=1}^n \delta_j(t) \quad (11)$$

The last policy listed in Table I, termed using the original name [25], *Droop-free*, does not rely on the droop method and its operation specified in (9) directly ensures frequency regulation and power sharing. Its application requires communications because all VSI must send their measured $P_i(t)$ (sub-figure 3b).

B. MG control policies in terms of local times

Table II summarizes each MG control policy previously given in Table I when they are expressed in local time

coordinates. For the *Droop-only* policy given in (8) and the *Local-integrals* policy given by (8) and (12), their expression in terms of each VSI local time t_i is straightforward and is given in (17) and (18), respectively.

For the *Centralized* policy specified by (8) and (13), only the MGCC controller computes the integral term. Therefore, its set-point frequency $\omega_m^*(t_m)$ will be computed depending only on its local time t_m , as indicated in (19). For the rest of VSIs, the computation of $\omega_i^*(t_i)$ will depend only on local times t_i because the integral term is just a "quantity" received from the MGCC, as indicated in (20).

The *Decentralized* policy given in (8) and (14) differs from the *Centralized* in the fact that integrals are computed locally in terms of local times t_i , with a measure given by the MGCC in terms of its own time, t_m . Therefore, the MGCC set-point frequency $\omega_m^*(t_m)$ is computed like in the previous policy, as indicated in (21). For the rest of VSIs, the computation of the local frequency set-points $\omega_i^*(t_i)$ will depend on local times t_i and on the MGCC measure expressed in terms of t_m . But knowing the relation of t_m and t_i with the global time t given in (4), it is possible to express t_m in terms of t_i as in

$$t_i = d_i t, \quad t_m = d_m t \quad \rightarrow \quad t_m = \frac{d_m}{d_i} t_i \quad (26)$$

and therefore the computation of $\omega_i^*(t_i)$ can be expressed only in terms of local times t_i as indicated in (22) in Table II.

In the *Averaging* policy given in (8) and (15) the set-point frequency $\omega_i^*(t_i)$ calculation depends on the averaged frequencies (10) computed at the i^{th} VSI using the received set-point frequencies $\omega_j^*(t_j)$ sent by the others j^{th} VSIs (and computed with their local times t_j). Using the same procedure than in the previous case, the others j^{th} VSIs local times t_j can be written in terms of the local time t_i as

$$\left. \begin{aligned} \omega_a^*(t_i) &= \frac{1}{n} \sum_{j=1}^n \omega_j^*(t_j) \\ t_i = d_i t, \quad t_j = d_j t \end{aligned} \right\} \rightarrow \omega_a^*(t_i) = \frac{1}{n} \sum_{j=1}^n \omega_j^* \left(\frac{d_j}{d_i} t_i \right) \quad (27)$$

and the computation of $\omega_i^*(t_i)$ can be expressed only in terms of local times t_i as indicated in (23).

For the *Consensus* policy given in (8) and (16) the set-point frequency $\omega_i^*(t_i)$ calculation depends on the averaged correction terms (11) computed at the i^{th} VSI using the received correction terms $\delta_j(t_j)$ sent by the others j^{th} VSIs (and computed with their local times t_j). Similar as before, the others j^{th} VSIs local times t_j can be written in terms of the local time t_i as

$$\left. \begin{aligned} \delta_a(t_i) &= \frac{1}{n} \sum_{j=1}^n \delta_j(t_j) \\ t_i = d_i t, \quad t_j = d_j t \end{aligned} \right\} \rightarrow \delta_a(t_i) = \frac{1}{n} \sum_{j=1}^n \delta_j \left(\frac{d_j}{d_i} t_i \right) \quad (28)$$

and the computation of $\omega_i^*(t_i)$ can be expressed only in terms of local times t_i as indicated in (24).

Note that in (26), (27) and (28) the same global time t is assumed for t_m , t_i and/or t_j . Hence, it is implicitly assumed that the data transfer via the communication network is instantaneous (zero latency) and deterministic (no jitter).

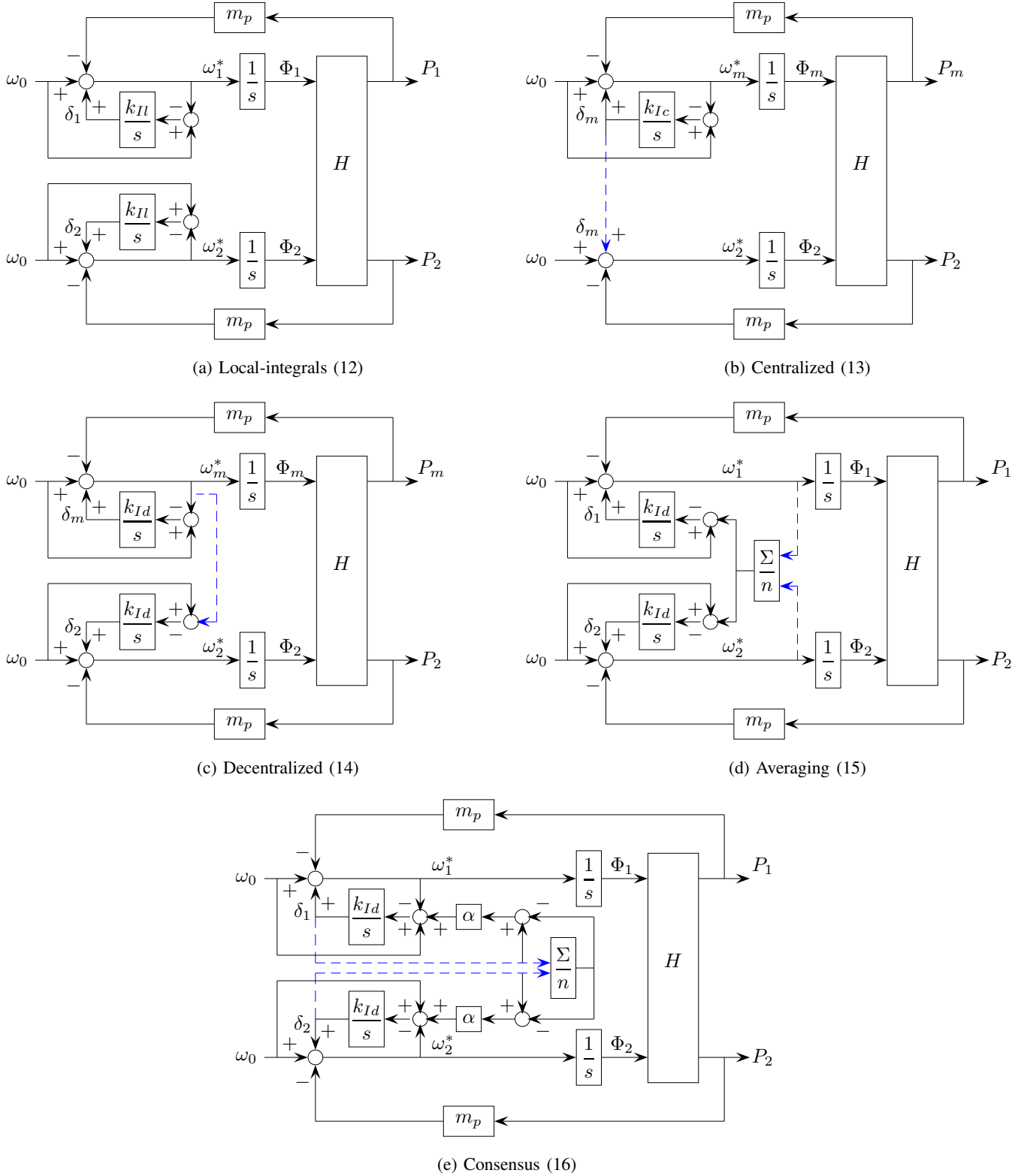


Fig. 4: Block diagram for the diverse droop-based policies for the case of two inverters.

For the *Droop-free* policy given in (9), the expression in terms of local times is obtained straightforward by replacing t by t_i , which leads to the specification given in (25). Note that for this policy, numerical integration is not required and the received active power values are just "quantities". Hence

the only clock that matters at each VSI is the local one that generates t_i .

The influence of drifts can not be explicitly observed in some of the expressions of the policies shown in Table II. However, since they are expressed in terms of local times,

TABLE II: MG control policies in terms of local times

Policy	Control formulation
Droop-only	$\omega_i^*(t_i) = \omega_0 - m_p P_i(t_i)$ (17)
Local-integrals	$\omega_i^*(t_i) = \omega_0 - m_p P_i(t_i) + k_{IL} \int_0^{t_i} (\omega_0 - \omega_i^*(t_i)) dt_i$ (18)
Centralized	$\omega_m^*(t_m) = \omega_0 - m_p P_i(t_m) + k_{Ic} \int_0^{t_m} (\omega_0 - \omega_m^*(t_m)) dt_m$ (19)
	$\forall i \neq \text{MGCC}, \omega_i^*(t_i) = \omega_0 - m_p P_i(t_i) + k_{Ic} \int_0^{t_m} (\omega_0 - \omega_m^*(t_m)) dt_m$ (20)
Decentralized	$\omega_m^*(t_m) = \omega_0 - m_p P_i(t_m) + k_{Id} \int_0^{t_m} (\omega_0 - \omega_m^*(t_m)) dt_m$ (21)
	$\forall i \neq \text{MGCC}, \omega_i^*(t_i) = \omega_0 - m_p P_i(t_i) + k_{Id} \int_0^{t_i} \left(\omega_0 - \omega_m^* \left(\frac{d_m}{d_i} t_i \right) \right) dt_i$ (22)
Averaging	$\omega_i^*(t_i) = \omega_0 - m_p P_i(t_i) + k_{Ia} \int_0^{t_i} \left(\omega_0 - \frac{1}{n} \sum_{j=1}^n \omega_j^* \left(\frac{d_j}{d_i} t_i \right) \right) dt_i$ (23)
Consensus	$\omega_i^*(t_i) = \omega_0 - m_p P_i(t_i) + k_c \int_0^{t_i} \left(\omega_0 - \omega_i^*(t_i) + \alpha \left(\frac{1}{n} \sum_{j=1}^n \delta_j \left(\frac{d_j}{d_i} t_i \right) - \delta_i(t_i) \right) \right) dt_i$ (24)
Droop-free	$\omega_i^*(t_i) = \omega_0 + m'_p \sum_{j=1}^n b_{i,j} (P_j(t_i) - P_i(t_i))$ (25)

using the local time definition (4), it is straightforward to make drifts d_i to explicitly appear in those expressions. This could help understanding the part of each policy that would be affected by the clock drift. However, it would not reveal the impact of drifts in each policy steady-state performance, which is presented next.

IV. IMPACT OF CLOCK DRIFTS: STEADY-STATE ANALYSIS

In the previous section, the MG control policies for frequency regulation and active power sharing were characterized in terms of VSI local times. The question that arises is to assess whether both control goals can still be accomplished in the presence of divergent clocks. This section gives the answer.

A. MG steady-state behavior under clock drifts

The analyzed MG control policies were designed to reach an equilibrium frequency. Next theorem states that for droop-based policies subject to clock drifts a MG equilibrium frequency exists if local set-point frequencies are constrained by a given form, named *local equilibrium frequencies*.

Theorem 1. *Let t and t_i be global and local times coordinates, respectively, defined by (4). For droop-based controlled VSI (6), the local set-point frequencies at each VSI must have the following form*

$$\omega_i^*(t_i) = \frac{C_{i,1}}{t_i} + C_{i,2} \quad (29)$$

in order to ensure an equilibrium frequency $\omega(t)$ in the MG, with $C_{i,1}, C_{i,2} \in \mathbb{R}$

Proof. Let $\omega(t)$ denote the MG frequency in terms of the global time t . This frequency will stabilize if

$$\frac{d\omega(t)}{dt} = 0 \quad (30)$$

and $\omega(t)$ is obtained from (3) as

$$\omega(t) = \frac{d\Phi(t)}{dt} \quad (31)$$

Additionally, each VSI generates a local set-point frequency $\omega_i^*(t_i)$ in local time coordinates (see eq. (17) to (24)) that originates from the droop control (8). And with this frequency a local phase $\Phi_i(t_i)$ is generated at each VSI that should obey (3). However, considering that standard implementations of the droop method in (8) assume that the variation in active power is slow enough to consider the active power constant, the generated local phase is

$$\Phi_i(t) = \int (\omega_0 - m_p P_i(t)) dt \simeq (\omega_0 - m_p P_i(t))t = \omega_i^*(t)t \quad (32)$$

In order to obtain the MG frequency (31) in global time coordinates as a function of local times, the variation of a local phase with respect to global time can be expressed as

$$\omega(t) = \frac{d\Phi_i(t_i)}{dt} \quad (33)$$

By deriving the local time t_i , defined in (4), with respect to the global time t , it is obtained

$$\frac{dt_i}{dt} = d_i \frac{dt}{dt} \rightarrow dt = \frac{dt_i}{d_i} \quad (34)$$

that introduced in (33) gives

$$\omega(t) = \frac{d\Phi_i(t_i)}{dt_i} d_i \quad (35)$$

Then, by replacing the droop phase (32) into (35), the MG frequency in global time coordinates as a function of local times t_i is written as

$$\omega(t) = \frac{d(\omega_i^*(t_i)t_i)}{dt_i} d_i = \left[\frac{d\omega_i^*(t_i)}{dt_i} t_i + \omega_i^*(t_i) \right] d_i \quad (36)$$

The condition (30) for the equilibrium frequency using (36) can be rewritten as

$$\left[\frac{d^2 \omega_i^*(t_i)}{dt_i^2} t_i + 2 \frac{d\omega_i^*(t_i)}{dt_i} \right] d_i^2 = 0 \quad (37)$$

which is a linear homogeneous ordinary differential equation with variable coefficients known as the Cauchy-Euler equation with solution given by (29). \square

It is interesting to note that when time progresses, the local equilibrium frequencies given by (29) evolve to

$$\lim_{t_i \rightarrow +\infty} \omega_i^*(t_i) = \lim_{t_i \rightarrow +\infty} \left(\frac{C_{i,1}}{t_i} + C_{i,2} \right) = C_{i,2} \quad (38)$$

The subsequent corollary summarizes this result.

Corollary 1. *An equilibrium frequency in the MG exists if each local set-point frequency settles to a constant value when time tends to infinity.*

It is interesting to observe two properties of the local equilibrium frequencies (29). First, their derivative is zero when time tends to infinity. This can be observed from their definition in (29) or from (38), and it is summarized next.

Property 1. *For the local equilibrium frequencies given in (29) it holds that*

$$\lim_{t_i \rightarrow +\infty} \frac{d\omega_i^*(t_i)}{dt_i} = 0 \quad (39)$$

The second property states that when time tends to infinity, the MG frequency in global time coordinates $\omega(\infty)$ can be directly expressed as a function of the local set-point equilibrium frequency $\omega_i^*(\infty)$ and drift rate d_i . Applying limits at the two sides of eq. (36), and using Property 1, it holds that

$$\begin{aligned} \omega(\infty) &= \lim_{t \rightarrow +\infty} \omega(t) = \lim_{t_i \rightarrow +\infty} \left[\frac{d\omega_i^*(t_i)}{dt_i} t_i + \omega_i^*(t_i) \right] d_i \\ &= \omega_i^*(\infty) d_i \end{aligned} \quad (40)$$

and the following property can be announced

Property 2. *For the equilibrium MG frequency expressed in global time coordinates $\omega(t)$ and the local equilibrium frequencies $\omega_i^*(t_i)$ given in (29) expressed in local time coordinates, when time tends toward infinity, they are related by*

$$\omega(\infty) = \omega_i^*(\infty) d_i \quad (41)$$

where d_i is the local drift rate (4).

Two more properties are announced. The first one follows from Property 2 and the second one is the power balance equation assuming negligible power losses.

Property 3. *If a MG equilibrium frequency $\omega(\infty)$ exists, then local equilibrium frequencies for two VSI are related by*

$$\omega_i^*(\infty) d_i = \omega_j^*(\infty) d_j \quad (42)$$

where d_i and d_j are local drift rates (4).

Property 4. *The steady-state active power $P_i(\infty)$ delivered by all inverters meets the MG load demand, i.e.*

$$\sum_{i=1}^n P_i(\infty) = P_T \quad (43)$$

where P_T is the power demanded by the MG load at $\omega(\infty)$.

Theorem 1 affirms that drifts do not affect the stability of the MG frequency in the sense that frequency equilibrium points still exist. The challenge that arises now is to determine them.

B. Frequency and active power equilibrium points

This section presents the expressions of the local equilibrium frequencies (29) and the steady-state active powers for droop-based policies (17)-(24) using the properties 1, 2, 3, and 4 that they exhibit. For the droop-free policy (25), the derivation of the steady-state properties follows a similar procedure. All results are summarized in Table III. Appendix A provides the details for deriving all the expressions shown in the table.

The steady-state values for frequencies and active powers shown in Table III analytically reveal the impact that clock drifts have in the accomplishment of the frequency regulation and power sharing control goals. The first observation refers to the existence of solutions. For all policies an equilibrium frequency exists, eqs. (45), (47), (49), (51), (53), (55), and (57), while it does not always exist an equilibrium point for the active power. In the *Local-integrals* policy the active power does not settle (46) and the system becomes unstable. For the rest of policies equations (44), (48), (50), (52), (54), and (56) give the active power equilibrium points.

Looking at the active power (middle column of Table III), and except for the *Local-integrals*, the rest of policies can be classified into two categories according to the impact of the underlying communication paradigm that they use. For those using a master/slave scheme (*Centralized* and *Decentralized*), the steady-state power value computation is different for the master ($d_i = d_m$) and for the slaves ($d_i \neq d_m$). This asymmetry disappears for the case of the *Droop-only* because it does not use communications, and for the *Averaging*, *Consensus*, and *Droop-free* policies that use a multi-master (assumed to be an all-to-all) communication scheme. Regarding to the size of the steady-state power sharing error, it can be observed that avoiding large errors in power sharing requires setting a high value for the droop gain m_p (or droop-free gain m'_p). This poses a conflict with the well accepted design paradigm that establishes that m_p cannot be chosen arbitrarily large because the primary droop control may become unstable [26].

Looking at the equilibrium frequencies (right column of Table III), none of the policies is able to achieve a local set-point frequency $\omega_i^*(\infty)$ matching the desired one ω_0 due to the presence of clock drifts. Except for the *Droop-only*, that does not regulate frequency, in the rest of policies, the size of the frequency deviation will depend on the drift rates coefficients, which in general can be considered very closed to 1 and similar between them. Therefore, the frequency deviations given in (47)-(57) are expected to be very small.

TABLE III: Steady-state active power and frequencies

Policy	$P_i(\infty)$	$\omega_i^*(\infty)$
Droop-only	$\frac{P_T}{\sum_{j=1}^n \frac{d_i}{d_j}} + \frac{\omega_0}{m_p} \left(1 - \frac{n}{\sum_{j=1}^n \frac{d_i}{d_j}} \right) \quad (44)$	$\omega_0 - m_p \left(\frac{P_T}{\sum_{j=1}^n \frac{d_i}{d_j}} + \frac{\omega_0}{m_p} \left(1 - \frac{n}{\sum_{j=1}^n \frac{d_i}{d_j}} \right) \right) \quad (45)$
Local-integrals	$\pm\infty \quad (46)$	$\frac{n\omega_0}{\sum_{j=1}^n \frac{d_i}{d_j}} \quad (47)$
Centralized	$\frac{P_T}{n} + \frac{\omega_0 d_m}{m_p} \left(1 - \frac{\sum_{j=1}^n \frac{d_j}{d_m}}{n} \right) - \frac{\omega_0 (d_m - d_i)}{m_p d_i} \quad (48)$	$\frac{\omega_0}{\frac{d_i}{d_m}} \quad (49)$
Decentralized	$\frac{P_T}{n} + \frac{\omega_0 d_m}{m_p} \left(1 - \frac{\sum_{j=1}^n \frac{d_j}{d_m}}{n} \right) - \frac{\omega_0 (d_m - d_i)}{m_p d_i} \quad (50)$	$\frac{\omega_0}{\frac{d_i}{d_m}} \quad (51)$
Averaging	$\frac{P_T}{n} + \frac{\omega_0}{m_p} \left(1 - \frac{n}{\sum_{j=1}^n \frac{d_i}{d_j}} \right) \quad (52)$	$\frac{n\omega_0}{\sum_{j=1}^n \frac{d_i}{d_j}} \quad (53)$
Consensus	$\frac{P_T}{n} + \frac{\omega_0(\alpha + 1)}{\alpha m_p} \left(1 - \frac{n}{\sum_{j=1}^n \frac{d_i}{d_j}} \right) \quad (54)$	$\frac{n\omega_0}{\sum_{j=1}^n \frac{d_i}{d_j}} \quad (55)$
Droop-free	$\frac{P_T}{n} + \frac{\omega_0}{m_p'} \left(1 - \frac{n}{\sum_{j=1}^n \frac{d_i}{d_j}} \right) \quad (56)$	$\frac{n\omega_0}{\sum_{j=1}^n \frac{d_i}{d_j}} \quad (57)$

V. IMPACT OF CLOCK DRIFTS: STABILITY ANALYSIS

The stability analysis is built upon the power flow expressions of the power exchanged among two consecutive inverters given by

$$P_{ij}(t) = V_i^2(t)G_{ij} - V_i(t)V_j(t)G_{ij} \cos(\Phi_i(t) - \Phi_j(t)) + V_i(t)V_j(t)B_{ij} \sin(\Phi_i(t) - \Phi_j(t)) \quad (58)$$

where the admittance between the two nodes in terms of the line resistance R_{ij} and inductance X_{ij} is

$$G_{ij} + B_{ij}j = \frac{1}{R_{ij} + X_{ij}j} \quad (59)$$

Lines are considered to be mainly inductive, that is

$$R_{ij} \ll X_{ij} \rightarrow B_{ij} \approx \frac{1}{X_{ij}}. \quad (60)$$

In addition, it is made explicit that each inverter voltage phase (3) is computed in terms of the drifting local time (4), that in Laplace notation can be expressed as

$$\Phi_i(s) = d_i \frac{\omega_i^*(s)}{s}. \quad (61)$$

Then, being $\hat{P}_{ij}(t)$ and $\hat{\omega}_i^*(t)$ small displacements from the equilibrium points of the exchanged power equation (58), the

Laplace small-signal model for $\hat{P}_{ij}(s)$ considering (59), (60) and (61) is given by

$$\hat{P}_{ij}(s) = \frac{V_i(s)V_j(s)}{sX_{ij}}(d_i\hat{\omega}_i^*(s) - d_j\hat{\omega}_j^*(s)) \quad (78)$$

By observing that

$$\hat{P}_i(s) = \sum_{j=1, j \neq i}^n \hat{P}_{ij}(s) \quad (79)$$

the exchanged power (78) can be written in matrix form as

$$\hat{P}(s) = G(s)D\hat{\Omega}^*(s) \quad (80)$$

where each power $\hat{P}_i(s)$ is expressed in terms of each frequency $\hat{\omega}_i^*(s)$, where

$$G_{ij}(s) = \begin{cases} \sum_{j=1, j \neq i}^n \frac{V_i(s)V_j(s)}{sX_{ij}} & i = j \\ -\frac{V_i(s)V_j(s)}{sX_{ij}} & i \neq j \end{cases} \quad (81)$$

and where D is a matrix with the drift rates in its diagonal. It is assumed that (80) already includes the Kron reduction that eliminates the nodes that do not produce power.

By making explicit that the nominal voltage frequency ω_0 is local to each inverter time (4), and by applying the change of

TABLE IV: Laplace transform of the MG control policies

Policy	For the i^{th} inverter	For all inverters (with $\hat{\Omega}_0[z] = \omega_0 \left(\frac{s}{d_i} \right)$)
Droop-only	$\hat{\omega}_i^*(s) = \frac{1}{d_i} \hat{\omega}_0 \left(\frac{s}{d_i} \right) - m_p \hat{P}_i(s)$ (62)	$\hat{\Omega}^*(s) = D^{-1} \hat{\Omega}_0(s) - m_p \hat{P}(s)$ (63)
Local-integrals	$\hat{\omega}_i^*(s) = \frac{1}{d_i} \hat{\omega}_0 \left(\frac{s}{d_i} \right) - m_p \hat{P}_i(s) + d_i k_{II} \frac{\frac{1}{d_i} \hat{\omega}_0 \left(\frac{s}{d_i} \right) - \hat{\omega}_i^*(s)}{s}$ (64)	$\hat{\Omega}^*(s) = D^{-1} \hat{\Omega}_0(s) - m_p \hat{P}(s) + D k_{II} \frac{D^{-1} \hat{\Omega}_0(s) - \hat{\Omega}^*(s)}{s}$ (65)
Centralized	$\hat{\omega}_m^*(s) = \frac{1}{d_m} \hat{\omega}_0 \left(\frac{s}{d_m} \right) - m_p \hat{P}_m(s) + d_m k_{IC} \frac{\frac{1}{d_m} \hat{\omega}_0 \left(\frac{s}{d_m} \right) - \hat{\omega}_m^*(s)}{s}$ (66)	$\hat{\Omega}^*(s) = D^{-1} \hat{\Omega}_0(s) - m_p \hat{P}(s) + D k_{IC} \mathbb{M}_n \frac{D^{-1} \hat{\Omega}_0(s) - \hat{\Omega}^*(s)}{s}$ (68)
	$\hat{\omega}_i^*(s) = \frac{1}{d_i} \hat{\omega}_0 \left(\frac{s}{d_i} \right) - m_p \hat{P}_i(s) + d_m k_{IC} \frac{\frac{1}{d_m} \hat{\omega}_0 \left(\frac{s}{d_m} \right) - \hat{\omega}_m^*(s)}{s}$ (67)	
Decentralized	$\hat{\omega}_m^*(s) = \frac{1}{d_m} \hat{\omega}_0 \left(\frac{s}{d_m} \right) - m_p \hat{P}_m(s) + d_m k_{Id} \frac{\frac{1}{d_m} \hat{\omega}_0 \left(\frac{s}{d_m} \right) - \hat{\omega}_m^*(s)}{s}$ (69)	$\hat{\Omega}^*(s) = D^{-1} \hat{\Omega}_0(s) - m_p \hat{P}(s) + D k_{Id} \frac{D^{-1} \hat{\Omega}_0(s) - \mathbb{M}_n \hat{\Omega}^*(s)}{s}$ (71)
	$\hat{\omega}_i^*(s) = \frac{1}{d_i} \hat{\omega}_0 \left(\frac{s}{d_i} \right) - m_p \hat{P}_i(s) + d_m k_{Id} \frac{\frac{1}{d_m} \hat{\omega}_0 \left(\frac{s}{d_m} \right) - \hat{\omega}_m^*(s)}{s}$ (70)	
Averaging	$\hat{\omega}_i^*(s) = \frac{1}{d_i} \hat{\omega}_0 \left(\frac{s}{d_i} \right) - m_p \hat{P}_i(s) + d_i k_{Ia} \frac{\frac{1}{d_i} \hat{\omega}_0 \left(\frac{s}{d_i} \right) - \hat{\omega}_i^*(s)}{s}$ (72)	$\hat{\Omega}^*(s) = D^{-1} \hat{\Omega}_0(s) - m_p \hat{P}(s) + D k_{Ia} \frac{D^{-1} \hat{\Omega}_0(s) - \frac{1}{n} \mathbb{1}_n \hat{\Omega}^*(s)}{s}$ (73)
Consensus	$\hat{\omega}_i^*(s) = \frac{1}{d_i} \hat{\omega}_0 \left(\frac{s}{d_i} \right) - m_p \hat{P}_i(s) + d_i k_c \frac{\frac{1}{d_i} \hat{\omega}_0 \left(\frac{s}{d_i} \right) - \hat{\omega}_i^*(s) + \alpha (\hat{\delta}_a(s) - \hat{\delta}_i(s))}{s}$ (74)	$\hat{\Omega}^*(s) = D^{-1} \hat{\Omega}_0(s) - m_p \hat{P}(s) + k_c \left[(D^{-1} s + \alpha) I - \frac{\alpha}{n} \mathbb{1}_n \right]^{-1} \left[D^{-1} \hat{\Omega}_0(s) - \hat{\Omega}^*(s) \right]$ (75)
Droop-free	$\hat{\omega}_i^*(s) = \frac{1}{d_i} \hat{\omega}_0 \left(\frac{s}{d_i} \right) + m'_p \sum_{j=1}^n b_{i,j} (\hat{P}_j(s) - \hat{P}_i(s))$ (76)	$\hat{\Omega}_i^*(s) = D^{-1} \hat{\Omega}_0(s) + m'_p \mathcal{L}_b \hat{P}(s)$ (77)

scale property of the Laplace transform that allows expressing a function of drifted time as a scaled function of the scaled complex variable s , the Laplace transform of each policy in Table I is given in Table IV for each inverter (second column) and in compact form for all inverters (third column). In (68) and (71), matrix \mathbb{M}_n denotes a $n \times n$ square matrix with all its entries being 0 except for one column of 1s in the m position, in (73) and (75) matrix $\mathbb{1}_n$ denotes a $n \times n$ square matrix with all its entries being 1, and in (77) matrix \mathcal{L}_b is the Laplacian associated to the communication graph. Moreover, policies of Table IV are expressed in Table V (second column) according to the following structural pattern

$$\hat{\Omega}^*(s) = H_1(s) \hat{\Omega}_0(s) - H_2(s) \hat{P}(s) \quad (95)$$

Given the exchanged power (80), and using the structural pattern (95), the closed-loop MG model for all policies can be

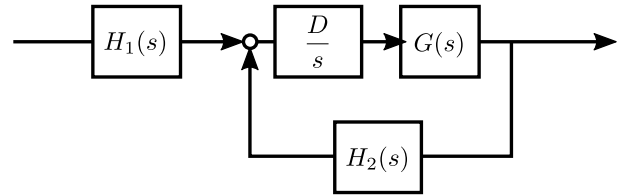


Fig. 5: Closed-loop diagram

expressed by

$$\begin{aligned} \hat{P}(s) &= G(s) \hat{\Omega}^*(s) \\ &= G(s) \left[H_1(s) \hat{\Omega}_0 - H_2(s) \hat{P}(s) \right] \\ &= [I + G(s) H_2(s)]^{-1} G(s) H_1(s) \hat{\Omega}_0 \end{aligned} \quad (96)$$

and schematically drawn in Figure 5.

TABLE V: $H_1(s)$ and $H_2(s)$ for the structural pattern (95), and stability condition

Policy	$H_1(s)$ and $H_2(s)$	Stability condition
Droop-only	$H_1(s) = D^{-1}, H_2(s) = m_p I$ (82)	$\bar{\sigma} \left(r [I + s^{-1} G m_p]^{-1} [-s^{-1} G m_p] \right) < 1$ (83)
Local-integrals	$H_1(s) = D^{-1}, H_2(s) = m_p s [sI + Dk_{II}]^{-1}$ (84)	(It does not apply)
Centralized	$H_1(s) = D^{-1}, H_2(s) = m_p s [sI + Dk_{Ic} \mathbb{M}_n]^{-1}$ (85)	$\bar{\sigma} \left(p [s(I + G m_p) + K_{Ic} \mathbb{M}_n]^{-1} [-K_{Ic} \mathbb{M}_n - G m_p] \right) < 1$ (86)
Decentralized	$H_1(s) = [sI + Dk_{Id} \mathbb{M}_n]^{-1} [sI + Dk_{Id} I] D^{-1},$ $H_2(s) = m_p s [sI + Dk_{Id} \mathbb{M}_n]^{-1}$ (87)	$\bar{\sigma} \left(p [s(I + G m_p) + K_{Id} \mathbb{M}_n]^{-1} [-K_{Id} \mathbb{M}_n - G m_p] \right) < 1$ (88)
Averaging	$H_1(s) = [sI + Dk_{Ia} \mathbb{1}_n]^{-1} [sI + Dk_{Ia} I] D^{-1},$ $H_2(s) = m_p s [sI + Dk_{Ia} \mathbb{1}_n]^{-1}$ (89)	$\bar{\sigma} \left(p [s(I + G m_p) + K_{Ia} \mathbb{1}_n]^{-1} [-K_{Ia} \mathbb{1}_n - G m_p] \right) < 1$ (90)
Consensus	$H_1(s) = D^{-1},$ $H_2(s) = m_p \left[I + k_c \left[(D^{-1} s + \alpha) I - \frac{\alpha}{n} \mathbb{1}_n \right]^{-1} \right]^{-1}$ (91)	$\bar{\sigma} \left(r s^{-1} \left(\alpha - \frac{\alpha}{n} \right) \mathbb{1}_n \left[I + K_c [s + s G m_p]^{-1} [I + \left(\alpha - \frac{\alpha}{n} \right) \mathbb{1}_n]^{-1} \right]^{-1} \right. \\ \left. [I + \left(\alpha - \frac{\alpha}{n} \right) \mathbb{1}_n]^{-1} \right) < 1$ (92)
Droop-free	$H_1(s) = D^{-1}, H_2(s) = m'_p \mathcal{L}_b$ (93)	$\bar{\sigma} (r [s + G m_p \mathcal{L}_b]^{-1} [-G m_p \mathcal{L}_b]) < 1$ (94)

The closed-loop system (96) is analyzed using robust control techniques to assess the stability of the equilibrium points considering clock drifts. In particular the MG is treated as an uncertain system where the uncertainty is given by each drift d_i (gathered in D). The structure of the uncertainty for each policy is given by the feedback path characterized by $H_2(s)$ and it can be modeled using an additive structured uncertainty $D = I + r\Delta$, where I is the identity matrix, r is the scalar value given by the drifts upper bound, and Δ is a diagonal matrix such that $\bar{\sigma}(\Delta) < 1$. For convenience, D^{-1} is similarly defined as $D^{-1} = I + p\Delta$, where p is the scalar value which represents the maximum value of the entries of $p\Delta$. Table V (third column) shows the application of the small gain theorem for MIMO (multiple-input/multiple-output) systems that allows characterizing the stable equilibrium points of each policy as a function of the clock drifts that are encoded in terms of the uncertainty upper bounds r or p .

The following observations can be made by looking at the stability conditions given in Table V. First of all, the stability condition for the *Local-integrals* policy is missing because no stable equilibrium point for the active power exists as indicated in Table III and therefore it can not be characterized the impact of the drift in the equilibrium point. Second, for the rest of policies it is expected that if the closed-loop system was designed to be stable, small deviations caused by clock drifts should not alter the stability nature of the equilibrium points. Third, the *Droop-only* and the *Droop-free* policies do not include in their formulations (17) and (25) the integral of the frequency error, which avoids the impact that drifts have in the integral terms, thus leading to closed-loop formulations where drifts do not appear in the feedback path (in $H_2(s)$).

VI. EXPERIMENTAL RESULTS

The laboratory MG follows the scheme shown in Figure 6, which is explained in detail in [35] (chapter 14). The MG is

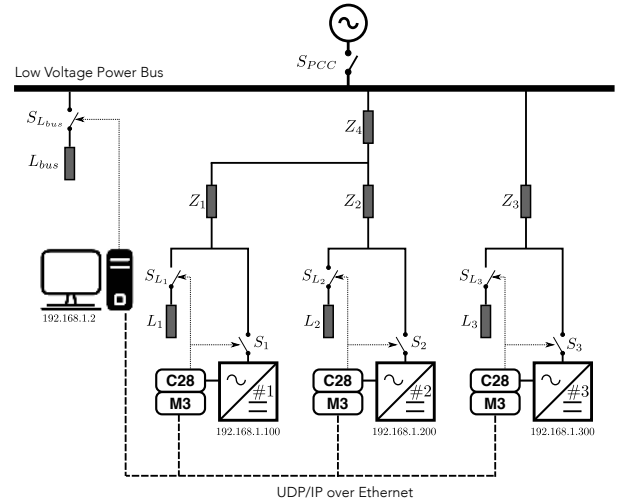


Fig. 6: Scheme for the laboratory microgrid.

composed by three VSI nodes feeding a global load, named L_{bus} whose power demand is $P_{L,bus} = 1.5\text{kW}$, that may be connected or disconnected. In all the experiments presented next, this load is permanently connected. Each power converter is driven by a dual core platform to program the control strategies shown in Table I. The chosen control platform for each VSI is a 32-bit Concerto-F28M36P63C board, composed by a C28 DSP core for power control purposes and a Cortex-M3 ARM core for communications. The MG uses the User Datagram Protocol (UDP)/Internet protocol (IP) protocol over an Ethernet link to allow communication among the three inverters, and with the supervisory Personal Computer (PC), where MG data is gathered for monitoring purposes. The diagram also includes line impedances modeling the parasitic elements of the cables and power transformers connected at the output of each inverter. The nominal values of the

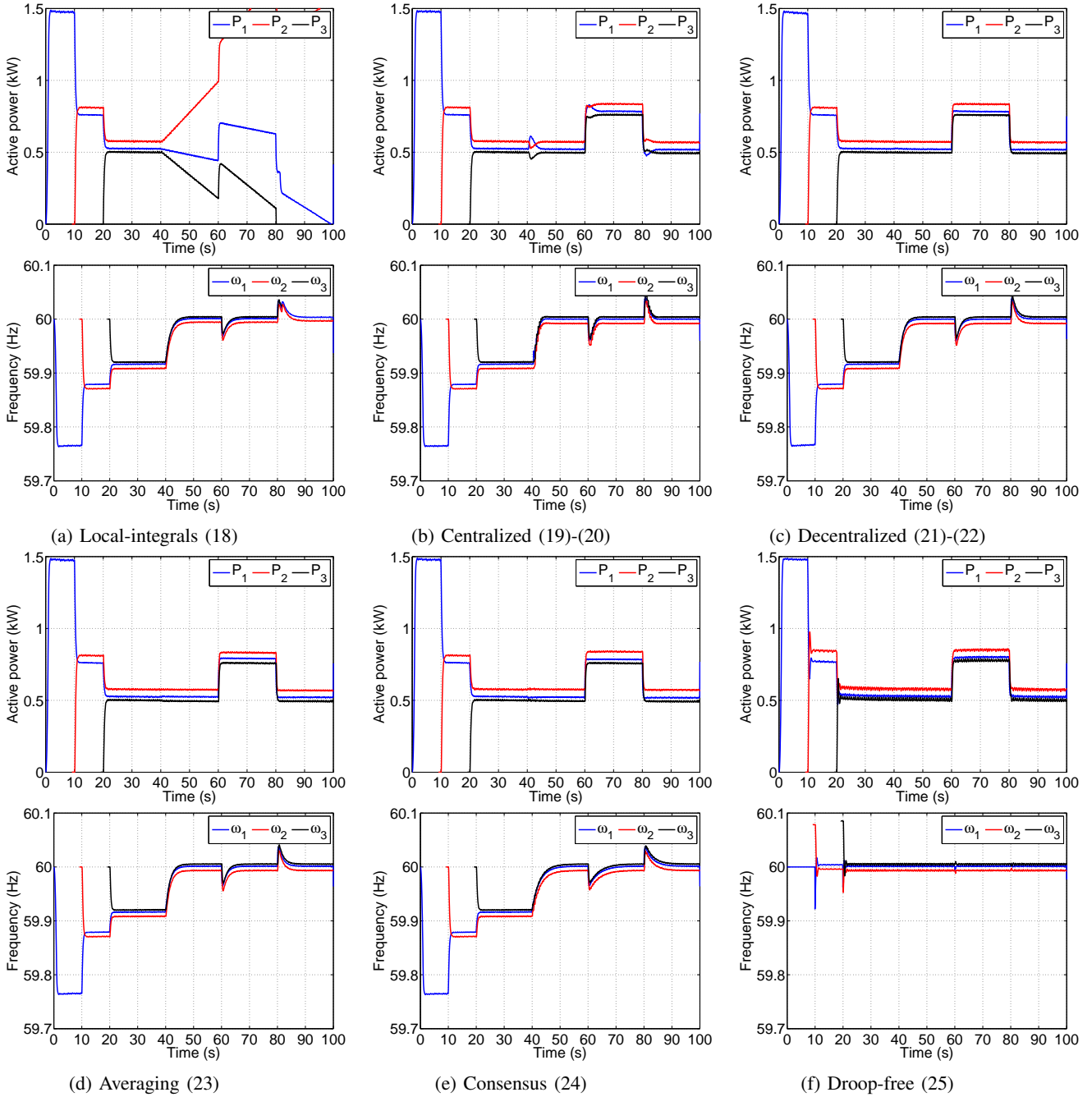


Fig. 7: Active power and frequency for the 3-nodes MG under different control policies

MG components are listed in Table VI. Each inverter has a local load L_i with a power demand of $P_{L,i} = 0.75\text{kW}$ that allows playing with different scenarios. For the experiments presented next, L_1 has been used. The other local load remain disconnected.

The control parameters of each policy, also shown in Table VI, are kept constant whenever possible or have been defined to obtain similar dynamics among the evaluated policies. In addition, clocks drift rates have been often artificially magnified to better illustrate its effects in the steady-state values for each of the policies. The three Concerto clocks have a drift rate upper bounded by 1.00002 [37], that is, the clocks

accuracy error is lower than ± 20 parts per million (ppm). The magnified drift rates used in some of the experiments are 5 times higher, that is, with an error of 100 ppm. Note that this is however a standard number for some of the nowadays micro-controllers crystal oscillators, like those used for Ethernet communication [36]. The experiments with non-magnified (default) drifts permit a more realistic sizing of the impact that the three Concerto clocks have on the performance of the laboratory MG. The last two parameters of Table VI refer to the transmission frequency that data is exchanged between inverters. In particular, T_r (or T_r^l) is the time interval elapsed between two consecutive messages, i.e. transmission

TABLE VI: Nominal values of the laboratory MG components

Symbol	Description	nominal value
n	Number of inverters	3
V_i	Inverter output voltage (rms line-to-line)	$\sqrt{3}$ 110 V
ω_0	Angular frequency at no load	$2\pi 60 \text{ rad/s}$
Z_1	Line impedance 1	1.24Ω (0.0512p.u.), 66.15°
Z_2	Line impedance 2	0.63Ω (0.0260p.u.), 37.02°
Z_3	Line impedance 3	1.15Ω (0.0475p.u.), 11.32°
Z_4	Line impedance 4	0.30Ω (0.0124p.u.), 90°
$P_{L, bus}$	Bus load power	1.5 kW
$P_{L, i}$	Local load power	0.75 kW
m_p	Gain of the frequency droop	1 mrad/(W/s)
n_q	Gain of the voltage droop	0.5 mV/(VAr)
L_V	Virtual impedance	10 mH
k_{Px}	Integral gains for policies (12)-(15)	0.6 rad/s
α	Proportional gain of consensus	5
k_c	Integral gain of consensus	4 rad/s
m'_p	Proportional gain of droop-free	0.33 mrad/W
d_1	Clock drift rate of digital processor 1	1.0000
d_2	Clock drift rate of digital processor 2	1.0001
d_3	Clock drift rate of digital processor 3	0.9999
T_s	Sampling period	$100\mu\text{s}$
T_r	Transmission period for policies (19)-(24)	0.5 s
T'_r	Transmission period for policy (25)	0.015 s

period, that is used for sending data in policies (19)-(24) (or policy (25)).

A. General overview

Figure 7 shows the laboratory experiments corresponding to policies (18)-(25) with magnified drift rates. For each policy, top and bottom sub-figures show the active power $P_i(t)$ and frequency $\omega_i^*(t)$ for the three VSI during an experiment of 100s. The experiment has the following pattern. Looking at generators, at time $t = 0, 10$ and 20 s the first, second and third inverter are activated, respectively. The first generator starts and fixes a MG frequency and voltage while starting to feed the bus load (L_{bus}). The activation of the second and third inverter is done by means of a phase-locked loop for synchronizing them to the MG frequency, and also start feeding the load. Looking at the control strategy, two scenarios apply. For droop-based policies (18)-(24), sub-figures 7a to 7e, up to time $t = 40$ s, only droop control applies, and from $t = 40$ s to the end, the complete policy applies. The droop-free policy (25), sub-figure 7f, is always active. The first inverter adopts the master role whenever required by the policy. In addition, for all cases, at time $t = 60$ s load L_1 is connected, and it is disconnected again at time $t = 80$ s.

Figure 7 does not explicitly shows the *Droop-only* policy (17) because it is already included in the five first policies up to time $t = 40$ s. As it can be observed in sub-figures 7a to 7e the local set-point frequencies (bottom sub-figures) stabilize to different values that produce small error in power sharing (top sub-figures). In fact, repeating the experiment with real drifts, that is without magnified drifts, it is observed that the power sharing errors can not be appreciated

TABLE VII: Theoretical vs measured magnified drifts

	Magnified drifts	Clock drift	Real magnified drifts d_i
VSI ₁	1.0000	$-3.4535 \cdot 10^{-5}$	0.999965464
VSI ₂	1.0001	$3.4185 \cdot 10^{-7}$	1.000100341
VSI ₃	0.9999	$6.8259 \cdot 10^{-7}$	0.999900682

and can be considered negligible, as further analyzed in sub-section VI-C, thus experimentally corroborating the claim in [27] that the droop method is robust to clock drifts.

Still looking at sub-figures 7a to 7e that correspond to the droop-based policies, a dramatic difference exists between sub-figure 7a that corresponds to *Local-integrals* and the rest of policies. As announced in [28], the (small) divergence in the local set-point frequencies provokes instability in the delivered active powers. Note that the same occurs for real drifts (as it will be shown in sub-section VI-C). For the rest of droop-based policies, sub-figures 7b to 7e, the divergency in the steady state frequencies theoretically announced in the previous section does not have a critical impact on the delivered active powers. In fact, for these policies, the dynamics of $P_i(t)$ slightly differ but the steady-state power sharing error is similar to the case of the droop-only scenario, which permits concluding that the performance delivered by these policies is not significantly affected by clock drifts.

The *Droop-free* policy shown in sub-figure 7f presents a different profile in active power and frequency because the policy is always active. However, similar properties with respect to the rest of policies can be observed. That is, small differences in frequency leads to small power sharing errors for the scenario of magnified drifts. Hence, the policy also performs well even in the presence of local clock drifts.

In terms of numbers, for all policies shown in Figure 7 all equilibrium frequencies lie in $60 \pm 0.01\text{Hz}$, and all power sharing steady state values present a deviation bounded by $\pm 50\text{W}$. Remind that this numbers are obtained for magnified drifts. Sub-section VI-C complements these numbers in the case of not-magnified drifts.

B. Theoretical results versus experimental results

This section assesses the correctness of the theoretical results for the steady-state values of frequencies and active powers with respect those obtained in the experiments. The evaluation is based on the same experimental set-up used in the previous section, with magnified drifts. It is important to highlight that on top of the magnified drifts, the real clock drifts also appear. Therefore, for an accurate assessment of the theoretical vs. the experimental results, the altered magnified drifts have been used. They have been obtained through measures. Table VII shows the theoretical magnified drifts, the clock measured ones, and the resulting drift d_i that applies.

The assessment is shown in Table III, and the values correspond the time $t = 70$ s of each experiment. In particular, it shows, for each policy, the percentage error of each theoretical frequency $\omega_i^*(\infty)$ (equations (45), (47), (49), (51), (53), (55),

TABLE VIII: Percentage errors for frequency and active power

Policy	Frequency error % ($\times 10^{-3}$)		
	$e_{\omega,1}$	$e_{\omega,2}$	$e_{\omega,3}$
Droop-only	0.0033	-0.0160	0.0120
Local-integrals	-3.5000	-5.7000	1.7000
Centralized	6.8000	6.8000	6.9000
Decentralized	7.0000	7.0000	7.0000
Averaging	0.0170	0.0089	0.0580
Consensus	1.3000	1.3000	1.4000
Droop-free	-0.0690	-0.0780	0.1500

Policy	Power error %		
	$e_{P,1}$	$e_{P,2}$	$e_{P,3}$
Droop-only	-0.0023	0.0100	-0.0096
Local-integrals	-	-	-
Centralized	0.0078	0.0150	-0.0270
Decentralized	-0.0054	-0.0210	0.0280
Averaging	-0.4900	-0.1800	0.7200
Consensus	0.0052	-0.1000	0.1200
Droop-free	0.0600	0.0340	-0.1000

and (57)) with respect to the experimental one $\omega_{i,m}^*(\infty)$, defined as

$$e_{\omega,i} = 100 \frac{\omega_i^*(\infty) - \omega_{i,m}^*(\infty)}{\omega_{i,m}^*(\infty)} \quad (97)$$

and the percentage error of each theoretical active power $P_i(\infty)$ (equations (44), (46), (48), (50), (52), (54), and (56)) with respect to the experimental one $P_{i,m}(\infty)$, defined as

$$e_{P,i} = 100 \frac{P_i(\infty) - P_{i,m}(\infty)}{P_{i,m}(\infty)} \quad (98)$$

From Table VIII it can be stated that there is a very good agreement between theoretical and experimental results.

C. Important aspects

This section complements the previous results by placing the attention to two important aspects.

First of all, the previous experimental results shown in Figure 7 were obtained with magnified drifts. By removing the artificial drifts, the deviations in frequency and power sharing due to the inherent (real) drifts still exist, as announced by the theoretical results summarized in Table III. But their effect is much smaller, and deviations are virtually inexistent for all the policies except for the *Local-integrals* that still exhibit the unstable behavior. Just for illustrative purposes, Figure 8 shows the case of the *Averaging* policy (to be compared with sub-figure 7d). The deviations in frequency and active power can be considered negligible.

Second, the last set of conducted experiments studies whether the availability of a clock synchronization protocol would significantly alter the obtained results when VSI are driven by drifting clocks that periodically synchronize. For this purpose, the IEEE 1588 precision time protocol (PTP) [38] has been implemented. The protocol synchronizes slave clocks to a master clock ensuring that events and time-stamps in all devices use the same time base. Rather than using specific hardware support for the PTP implementation (such as message detectors and time stamps units), the prototype implementation here applied is based on software interrupts, being the first inverter the master providing the source of time and the two other inverters the slaves synchronizing their clocks. The

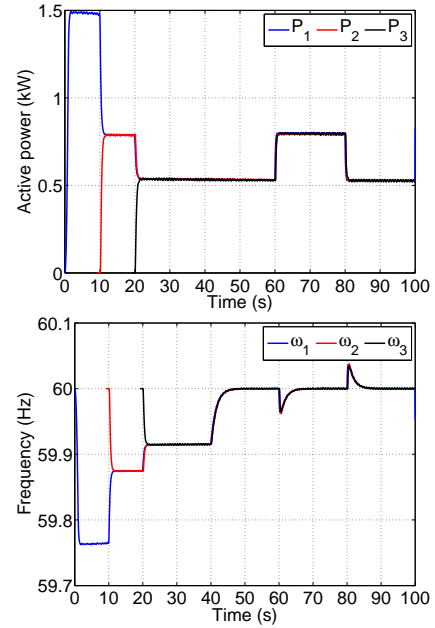
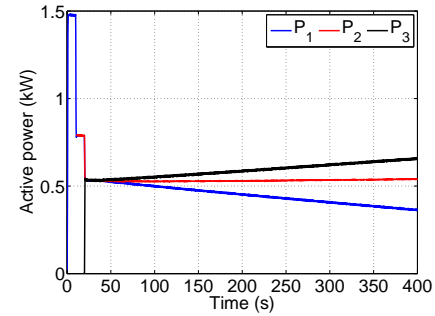
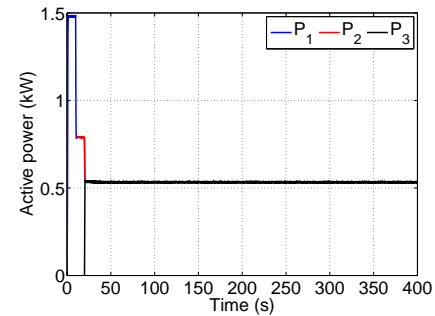


Fig. 8: The case of not-magnified clock drifts (eg. *Averaging*)



(a) *Local-Integrals*



(b) *Averaging*

Fig. 9: The case of real drifting clocks with the IEEE1588 Precision Time Protocol for *Local-integrals* and *Averaging* policies.

execution run follows the same start-up sequence than the other experiments, but the experiment is longer and runs for 400s. The experiment is based on real default drifts, that is, no magnified drifts are artificially applied. Figure 9 summarizes the main results. Sub-figure 9a shows the active power for the case of the *Local-integrals* policy. As it can be observed, the application of the clock synchronization protocol does not mitigate the problem caused by clock drifts: active powers de-

viate. Although clocks are periodically synchronized, between clock synchronization instants, the three clocks deviate again, causing a permanent local frequency error that is different in each node. Their integration in the control algorithm (18) does not stop, and as a consequence, active powers increase or decrease permanently. Sub-figure 9b corresponds to the *Averaging* policy (taken as example within policies (19)-(25) that provide exactly the same type of results). The application of the clock synchronization protocol does not remove the announced active power steady-state deviations for these policies. But as it can be observed in the sub-figure, deviations can not be distinguished and they can be considered negligible. In summary, the application of a clock synchronization protocol does not alter the obtained results. Hence, a research challenge is the design of local control policies for frequency regulation and active power sharing being robust to clock drifts and without requiring communications for control data exchange nor for clock synchronization.

VII. CONCLUSION

This paper has analyzed the impact that local drifting clocks have in the performance of control policies targeting frequency regulation and power sharing in VSIs-based islanded MGs. The state-of-the-art that applies has been divided into two different type of policies depending on whether they rely on the droop method. Knowing that the droop method is robust to clock drifts, the paper has analyzed the effect that local clock drifts have in the steady-state performance of those policies built on top of the droop method and those policies that do not rely on the droop method. The theoretical analysis and the experimental evidences have revealed that all the analyzed policies suffer negligible degradation due to nowadays clock drifts, except for one that makes the MG unstable.

APPENDIX

This appendix provides the theoretical derivation of the steady-state expressions for frequencies and active powers shown in Table III for each of the policies being analyzed.

1) *Droop only*: By using the policy definition (17) when time tends to infinity, it holds that

$$\omega_i^*(\infty) = \omega_0 - m_p P_i(\infty) \quad (99)$$

Considering Properties 3 and 4 and (99) a system of equations is obtained whose solution is given in (44) and (45).

2) *Local-integrals*: The solution to the equation obtained by applying Property 1 the policy (18) is

$$P_i(\infty) = \lim_{t_i \rightarrow +\infty} \frac{k_{II} (\omega_0 - \omega_i^*(\infty))}{m_p} t_i \quad (100)$$

Properties 2, 4 and (100) form a system of equations whose solution is the local equilibrium frequency given in (47). Since in general $\omega_i^*(\infty)$ are different than ω_0 , from (100) it holds that $P_i(\infty)$ will always increase or decrease, as indicated in (47).

3) *Centralized*: The solution to the equation obtained by applying Property 1 to the master policy (19) is

$$P_m(\infty) = \lim_{t_m \rightarrow +\infty} \frac{k_{Ic} (\omega_0 - \omega_m^*(\infty))}{m_p} t_m \quad (101)$$

By applying Property 1 to the rest of VSIs (20) (and considering (26) and (101)) the resulting equation solves to

$$P_i(\infty) = \frac{d_m}{d_i} P_m(\infty) \quad (102)$$

Using Property 4 and (102) the steady-state active power given in (48) is obtained. Since $P_i(\infty)$ are constant, from Property 1 applied to either master or slave, it is obtained that

$$\omega_m^*(\infty) = \omega_0 \quad (103)$$

The application of Property 2 and 3 to (103) permits deriving the local set-point frequency for any inverter, as in (49).

4) *Decentralized*: For this case characterized ((21) or (22)), the result for the equilibrium frequencies and active powers is the same as in the case of the *centralized* policy. Therefore, the mathematical derivation is omitted, but the results are given in (50) and (51). The only difference is the transient dynamics of each $\omega_i^*(t)$ because the integration term of each policy is different and is characterized by the local clock drift rate.

5) *Averaging*: The solution to the equation obtained by applying Property 1 to policy (23) is

$$P_i(\infty) = \lim_{t_i \rightarrow +\infty} \frac{k_{Ia} \left(\omega_0 - \frac{1}{n} \sum_{j=1}^n \omega_j(\infty) \right)}{m_p} t_i \quad (104)$$

Considering Properties 3, 4 and (104) a system of equations is obtained whose solution is given in (53). For this case, the steady-state active power stabilizes to a given value that depends on the local integral of each corrective term in (23). Assuming the same integral value for all of them, the steady-state power stabilize in (52).

6) *Consensus*: The solution to the equation obtained by applying Property 1 to policy (24) is

$$P_i(\infty) = \lim_{t_i \rightarrow +\infty} \frac{k_c \left(\omega_0 - \omega_i(\infty) + \frac{\alpha}{n} \sum_{j=1}^n \delta_j(\infty) - \alpha \delta_i(\infty) \right)}{m_p} t_i \quad (105)$$

Considering Properties 3 and 4 and (105), and assuming that the corrective term in (24) stabilizes, i.e. $\dot{\delta}(\infty) = 0$, a system of equations is obtained whose solution is given in (54) and (55).

7) *Droop-free*: This policy (25) does not rely on the droop method and Theorem 1 and the derived properties can not be directly applied. The phase of this policy, that applying (3) is given by

$$\Phi_i(t) = \omega_0 t + m'_p \int \sum_{j=1}^n b_{i,j} (P_j(t) - P_i(t)) dt \quad (106)$$

can be written in terms of local time coordinates t_i using the time transformation given in (26) with t_j instead of t_m as

$$\Phi_i(t) = \omega_0 t + \varphi_i(t) \quad (107)$$

with

$$\varphi_i(t_i) = m'_p \int_0^{t_i} \sum_{j=1}^n b_{i,j} \left(P_j \left(\frac{d_j}{d_i} t \right) - P_i(t) \right) dt \quad (108)$$

By multiplying and dividing $\varphi_i(t)$ by t_i in (107) and rearranging, the phase becomes

$$\Phi(t_i) = \left(\omega_0 + \frac{\varphi_i(t_i)}{t_i} \right) t_i \quad (109)$$

which can be seen as a droop-based policy (recall (8)) with $m_p = 0$ and a frequency correction, with set-point frequency

$$\omega_i^*(t_i) = \omega_0 + \frac{\varphi_i(t_i)}{t_i} \quad (110)$$

The application of Property 1 to (110) simplifies to

$$\lim_{t_i \rightarrow +\infty} \left[\frac{d^2 \varphi_i(t_i)}{dt_i^2} \right] = 0 \quad (111)$$

which alerts that the equilibrium frequency implies that

$$\varphi_i(t_i) = \rho_i t_i \quad (112)$$

with $\rho_i \in \mathbb{R}$ being a constant. That is, the phase (107) must always increase (or decrease) in order to have an local equilibrium set-point frequency.

Knowing that the limit as time tends to infinity of the derivative of (108) must be a constant, ρ_i , using Properties 3 and 4, and the set-point frequency definition (110), the following system of equation can be formulated

$$\sum_{j=1}^n b_{i,j} (P_j(\infty) - P_i(\infty)) = \frac{\rho_i}{m'_p} \quad (113)$$

$$\omega_i(\infty) d_i - \omega_j(\infty) d_j = 0 \quad (114)$$

$$\omega_i(\infty) - \omega_0 = \rho_i \quad (115)$$

$$\sum_{j=1}^n P_j(\infty) = P_T \quad (116)$$

whose solutions when $\forall i, j \ b_{i,j} = 1$ (when data exchange occurs between all the nodes and with the same weight) are (56) and (57). The solutions for the case of arbitrary weights are matrix-based algebraic expressions that deserve a deeper analysis and are out of the scope of the analysis presented in the paper.

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