Assessment of Aircraft Noise Emissions at International Eskisehir Hasan Polatkan Airport with Multiple Approach Model

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ABSTRACT

Aircraft noise emissions are a problem that negatively affects human health, directly or indirectly. For this reason, examining and managing the noise effects caused by aircrafts at the airports is important for the sustainable development of aviation. In the present study, a noise management model based on the multiapproach method, including some actions related to aircraft noise, has been created. The model was applied to the International Eskisehir Hasan Polatkan Airport (LTBY). Within the scope of the model, in the first stage, in 365 days, day, evening and night noise levels around the airport were simulated using IMMI software under the European noise directive and European Civil Aviation Conference (ECAC) doc 29-interim was also used to measure aircraft noise. In the second stage, the noise generated by the Cessna 172-S aircraft under different operating conditions experimentally measured was carried out. After the model had been applied to LTBY, improvement opportunities for aircraft noise were evaluated. It is thought that the study and its results will help other civil airports on the issue of noise problem at airports.

Keywords: Aircraft noise; Noise measuring; Noise management; Aviation acoustics; Aviation management; European noise directive.

INTRODUCTION

Aircraft noise emissions from the past have become one of the important research topics in environmental management in aviation. An aircraft has components that generate noise, such as the engine, main gear brake system, nose gear brake system and airframe system (Isermann and Bertsch 2019; Bertsch *et al.* 2019). In addition, aircraft landing detail and aircraft wheel configuration are effective parameters in noise production (Shafabakhsh *et al.* 2018). With technological advances, these components are more efficient in terms of reducing noise generation. Also, it is observed that aircraft and engine manufacturers made significant improvements in noise in the production of new generation aircraft engines to prevent noise emission caused by aircraft. Especially in areas close to airports, people are disturbed by the noise generated by aircrafts during landing, takeoff and ground operations. It is observed that many of the existing airports in the world are mostly located near city centers and dense settlements (AIRBUS 2016).

Worldwide, both planned passenger traffic and air cargo traffic are projected to exceed 4% annual growth over the next 20 years, which means doubling global air traffic (EUROCONTROL 2013). Thus, noise emissions will affect people living near airports more.

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The fact is that the airport positions remained in the city with the development of the cities brought with its alteration of the percentage of inhabitants exposed to noise each day. The negative consequences of noise effects around airports and settlements on people, directly or indirectly, are sleep disturbance, lack of concentration, anxiety, and high blood pressure heart problems (WHO 2009).

Modeling the noise effects of Heathrow and Gatwick airports in the UK were carried out. It is stated that the noise generated by aircraft at the two airports affects 255,800 people, causing 54 myocardial infarctions, resulting in 17 early deaths each year (Wolfe et al. 2017).

The EU Environmental Noise Directive 2002/49/EC mandates that the noise level in settlers with more than 100,000 settlers be calculated and displayed on tactical noise maps that are assessed and updated every 5 years, if necessary. Noise mapping involves presenting data using a noise predictor on an actual or expected noise situation. These maps are created using specific methods and strategies aimed for public exposure assessment in residential zones. For the most part, noise maps are generated by predictions depending on both known and assessed metrics, including a description of the digital territories in 3D and aircraft GPS data (EC 2002; Ozkurt *et al.* 2015; Sari *et al.* 2014; Vogiatzis 2012).

In this study, a model was designed for sustainable noise management at airports. In the model, both noise estimation with simulations and noise measurements were made with a measuring device.

METHODOLOGY

Airports have various managerial mechanisms, but the key criteria in distinguishing these mechanisms are directly related to the size and capacity of airports. Another factor concerning the mechanism of managing is the various types of management. While the airports that also adopted the centrally controlled management strategy prefer formal organizational structures, a limited organizational structure for the airports with a versatile management approach is favored. For airports that have a versatile management strategy, management rates are seen to be less and less plain. Even so, there are airports with combined organizational mechanisms (Akyuz *et al.* 2019; Paşaoğlu *et al.* 2013; Sengur 2016).

It is determined that the noise management unit must be included in the mixed organizational mechanism at the airports. Depending on the capacity and a variety of activities, the number of noise management units and the number of staff in the team may vary. To establish and maintain the noise management unit in an airport, the upper units to which the unit is connected and the airport senior management to which it is naturally connected must be defined. In this context, the position of a sustainability manager at the airport under the top management unit and the environmental sustainability manager position as its subunit are defined, as shown in Fig. 1 (Akyuz *et al.* 2019).

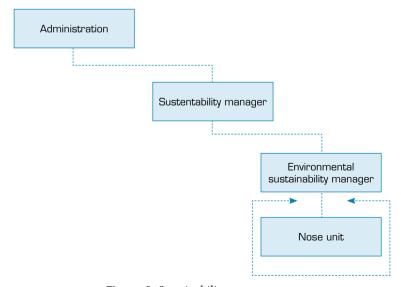


Figure 1. Sustainability management.

The sustainability manager in the organizational structure is linked to the airport top management and sets sustainability policies for the airport in economic, environmental and social areas. The environmental sustainability manager makes evaluations on environmental issues at the airport (Akyuz *et al.* 2019).

At the airports, the noise management unit is one of the units under the airport top management and under the sustainability manager.

The methodology of the model

The balanced approach concept of the International Civil Aviation Organization (ICAO) should be considered as the main policy to prevent noise arising from aircraft and to struggle noise problems (ICAO 2005).

Balanced approach covers the following four basic parameters:

- Reduction of noise from its source.
- Planning and management of land use.
- Noise reduction in operational procedures.
- Operating restrictions on aircraft.

In this context, a detailed infrastructure has been developed. For this reason, a building model is shown in Fig. 2.

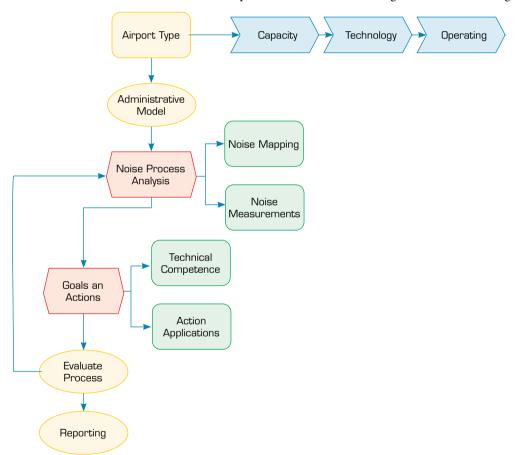


Figure 2. Noise management action plan.

When the aircraft is close to the ground, aircraft-induced noise has been evaluated under four main headings (Basner *et al.* 2017; Franssen *et al.* 2004; Klæboe *et al.* 2006; Viswanathan 2018):

- Taxiway and apron noise;
- Takeoff noise;
- Landing noise (especially due to reverse thrust);
- The noise generated during maintenance of the aircraft on the ground.

In the created model, these four basic approaches are also considered. The information, including the multiple approach tasks, is visualized in Fig. 3.

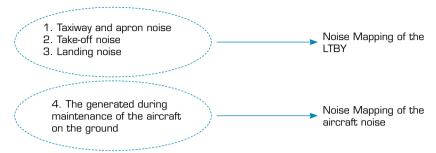


Figure 3. Summary of multiapproach tasks.

For the airport, the implementation process of this work depending on the model is shown in Fig. 4.

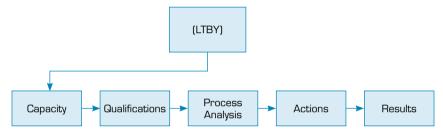


Figure 4. Model-based working process for LTBY.

To evaluate the mapping of the aircraft noise, aircraft noise map of the airport was modelled for the year of 2018 using IMMI software. The aircraft types and classes, maximum takeoff weights and their compatibility with the ICAO annex 16 guide chapters (ICAO 2005; ICAO 2015) were analyzed for each of the 5100 aircraft at the airport in one year.

To examine noise generated during maintenance of the aircraft on the ground, the Cessna 172-S aircraft has been identified, because Cessna 172-S aircraft, Faculty of Aeronautics, Department of Astronautics Piloting, performs approximately 55% of all aircraft operations per year within the scope of training flight activity. The measurements were made in line with ISO 3744, ISO 3746 and ISO 3740 standards (ISO 2010a; b; 2019).

Model stage 1: aircraft noise mapping of LTBY

International Eskisehir Hasan Polatkan Airport (LTBY) is located within the boundaries of the Tepebasi district of Eskisehir province and opened to traffic in March 1989. The coordinates of Eskisehir Hasan Polatkan Airport are 39°48'36"N; 30°31'10"E and its altitude is 2589 m. There is one terminal station inside the airport, an Air Traffic Control (ATC) center, two maintenance hangars, a firehouse, and a meteorological unit (HPH 2020). The satellite image of the airport is shown in Fig. 5 (Google 2018).



Figure 5. International Eskisehir Hasan Polatkan Airport (LTBY). Retrieved from Google Earth (2018) Eskişehir Hasan Polatkan. Image © 2018 Maxar Technologies.

The runway operating within the airport is the runway named 09/27. The coordinates of the reference point of Eskisehir Hasan Polatkan Airport are defined as $39^{\circ}48'47"N$, $30^{\circ}30'45"E$. There is a runway of 3000×45 m in the airport (HPH, 2020).

The statistical flight data and aircraft classes are related to the AzB standard *Instructions on the Calculation of Noise Protection Areas* (AzB 2007) and aircraft types and classes, maximum takeoff weights and compatibility of ICAO annex 16 guide chapters of aircraft operating in the airport were studied and classified parallel to the AzB and are given in Tables 1 and 2.

Table 1. Matching 5100 flight operations to AzB standard.

Aircraft type	AzB group number	Aircraft type	AzB group number	Aircraft type	AzB group number
A319	S5.2	B734	S1.1	C25A	S1.O
A320	S5.2	B738	S1.1	C56X	\$1.0
A321	S5.2	B763	S6.1	C650	S1.O
AS32	H2	BE40	P2.1	C680	S1.O
B350	P2.2	C160	S1.2	CL6O	S1.O
B38M	S1.1	C172	P1.3	CRJ2	S1.O
B429	H2	C208	P1.4	E35L	S1.O
F2TH	S1.O	J328	S1.O	E545	S1.1
FA7X	S1.O	LJ35	S1.O	EC35	H1
GLF4	S1.O	LJ40	S1.O	P46T	P1.4
H25B	S1.O	LJ45	S1.0	PA32	P1.4
H60	H2	LJ60	S1.O	PAY3	P1.4
HA4T	S1.O	MD82	S1.1	S76B	H2
TB20	P1.3	BE9L	P1.4		

Table 2. Distribution of the flight operations based on period.

AzB	Landing operations (%)			Takeoff operations (%)		
Category	Day (07:00 – 19:00 h)	Evening (19:00 - 23:00 h)	Night (23:00 – 07:00 h)	Day (07:00 - 19:00 h)	Evening (19:00 - 23:00 h)	Night (23:00 - 07:00 h)
S5.2	4.29	16.00	68.16	4.97	17.53	21.08
H2	0.13	0.00	0.00	1.32	0.00	0.00
P2.2	0.13	0.00	0.00	0.16	0.00	0.00
P2.1	0.09	0.00	0.00	0.11	0.00	0.00
S6.1	0.04	0.00	0.00	0.05	0.00	0.00
P1.3	76.89	38.67	17.32	73.60	21.65	70.91
H1	0.09	0.00	0.56	0.11	0.00	0.17
S1.2	0.04	0.00	0.00	0.05	0.00	0.00
P1.4	9.58	1.33	1.12	10.48	0.00	4.18
S1.0	3.85	6.67	3.91	3.70	17.53	2.26
S1.1	4.86	37.33	8.94	5.45	43.30	1.39

Noise levels were simulated in terms of L_{den} (L_{day} , L_{evening} , L_{night}) unit at a height of 4 m from the ground for 5100 aircraft that operated and landed at the airport in 2018. Calculated noise level values were obtained as 55–59, 60–64, 65–69, 70–74 and > 75 dB (A) and noise maps were created as grids with a range of 50 m (Ozkurt *et al.* 2015; Sari *et al.* 2014).

Model stage 2: experimental measurement of the aircraft noise

Cessna 172-S is the most operated aircraft in the LTBY annually and this aircraft has been selected within the model. The aircraft has one staff and three passenger capacity, with a curb weight of 736 kg and takeoff weight of 1113 kg. It has a power of 180 HP (134 kW), and Lycoming IO-360-L2A boxer type of engine (Cessna 2020). Eskisehir Technical University, Faculty of Aeronautics and Astronautics is used within the scope of training flight activity. Following ISO 3740, ISO 3744, ISO 3746 standards of the Cessna 172-S aircraft, acoustic noise measurement and analysis were performed, and the following operations were applied respectively.

The Cessna was placed on a flat concrete floor in a way that coincides with the center of the hemisphere with a 15 m radius. The aircraft was operated for 15 min at 725 rpm to heat the engine and reach the full rpm in the second condition.

The measurement group was carried out on the test environment, outdoors, single reflective surface and concrete ground. The noise level measurement device calibration process was performed before the measurement.

The reference box definition, which is a prismatic rectangular prism covering the components where the source emits sound, is shown in Fig. 6 and ends on the reflective plane/planes on which the noise source is located (ISO 2010a).

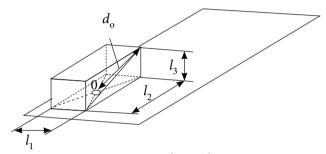


Figure 6. Reference box.

The characteristic source size of the reference box on a reflecting plane was calculated as in Eq. 1. The measuring radius was determined as 15 m.

$$d_0 = \sqrt{\left(\frac{l_1}{2}\right)^2 + \left(\frac{l_2}{2}\right)^2 + (l_3)^2} \tag{1}$$

where, $l_1 = 11 \text{ m}$, $l_2 = 8.28 \text{ m}$, $l_3 = 2.72 \text{ m}$, and $d_0 = 7.4 \text{ m}$.

TESTO 815 type-2 sound level meter (SLM) was used for the measurements. The SLM that appropriates the requirements of IEC 61672-1: 2002 for measurements of the noise (IEC 2002). The measurements were made with the aircraft in no-load mode (IDLE) and full load (full thrust).

The SLM had been calibrated before starting each measurement group. The background noise level measured at every point was determined before the aircraft was operated. It was determined that the background noise was at least 15 dB less than the measurement values taken from the points. Measurements were made under conditions where the wind speed was lower than 5 m/s and there was no precipitation in the air (ISO 2010b). Microphone positions are shown in Fig. 7.

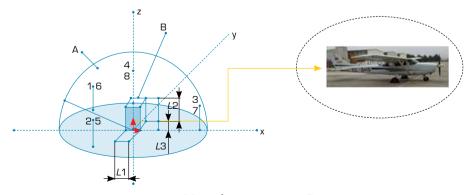


Figure 7. Microphone positions, 3D view.

where, A: measuring surface, B: reference box, L_1 : length of reference box, L_2 : width of reference box, L_3 : height of the reference box, r: radius of the measuring surface

RESULTS AND DISCUSSION

In line with the European Directive 2002/49/EC, and Turkish Regulation on Assessment and Management of Environmental Noise (RAMEN), the maximum allowable limit for noise is $L_{\rm den}$ = 63 dB (A) (Turkey 2010; EC 2002; Ozkurt et. al 2014; Keskin 2014). The noise mapping results of LTBY as $L_{\rm den}$ are shown in Fig. 8.

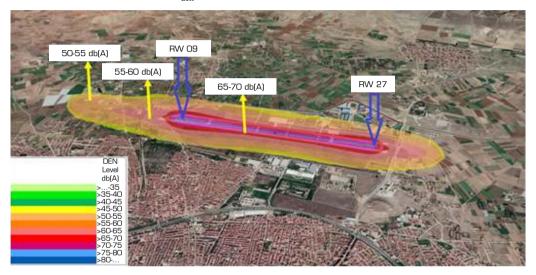


Figure 8. Noise mapping of LTBY, L_{den} .

When the noise mapping results were evaluated, it was observed that the noise level, which would adversely affect human health, was not exceeded.

However, the dominant wind direction in the airport region has an impact on the noise generated at the airport and the propagation of noise emission around the airport. Propagating the sound in the direction of the wind will slightly increase its effect (Keskin 2014).

Therefore, aircraft noise has been associated with the prevailing wind direction at the airport and around it. Winds prevail in the direction of east to west in the winter and northwest in the first months of spring. At the end of spring, winds from the southwest, west and northwest can be seen (GDM 2019). In this context, when 09/27 runway at LTBY is examined and evaluated in terms of the prevailing wind direction and its surroundings during the year, the use of runway 09 during the months of winter and spring, and runway 27 during the remaining months of the year, due to the departure operations of the aircraft from the airport, will affect the noise emission. Therefore, it is recommended to pay attention to the use of runways in parallel with these arguments stated in-flight operation plans.

One of the tasks in the developed model was noise measurement. The measurement results under ISO 3746 for Cessna 172-S are given in Tables 3 and 4.

When the results of the experimental measurements were evaluated, it was observed that the values were exceeding the lowest exposure limit of 80 dB (A) (Nazlioğlu 2014).

In this context, preventive measures were studied, and the identified improvement opportunities were presented.

Under ideal conditions, spreading of sound waves and a decrease in sound pressure levels due to distance are observed. Accordingly, due to the noise generated by the noise source during the aircraft engine tests, hydraulic and pneumatic tests in the maintenance hangar area or the front of the hangar, the safe contour zones are created because the distance data will decrease by approximately $1 \, \text{r}^{-2}$ from the source. The safe contour zones are shown in Fig. 9.

Table 3. Experimental measurement results and calculations of the operation condition: IDLE.

Source	Cessna 172-S 180 HP, 134 kW				
Source location	Single reflective surface, concrete/asphalt ground				
Ambience	Outdoor environment (negligible K ₂)				
Operation condition		725 rpi	725 rpm (IDLE)		
Source dimensions		8.28, 11, 2.72 m			
Microphone positions	Eight positions				
Background noise	level correction	n value, K _{1A}			
Background noise level, L_{Pa}	ound noise level, L _{Pa} 56 dB(A)				
$\Delta L_{ m pA}$ Correction value $K_{ m 1A}$	15 dB(A) O dB(A)				
Measuren	nents results di	B(A)			
Point 1	81.7	81.7	81.7		
Point 2	79.6	79.6	79.6		
Point 3	79.5	79.5	79.5		
Point 4	81.7	81.8	81.7		
Point 5	79.8	79.8	79.8		
Point 6	81.8	81.8	81.8		
Point 7	79.2	79.2	79.2		
Point 8	81.7	81.8	81.8		
A weighted average sound pressure level, $\bar{L}_{\rho \mathrm{A^{-}}}\mathrm{dB}$ (A)	80.76	80.78	80.77		
$10 \log \left(\frac{S}{S_0} \right)$ S = hemispherical measuring surface area (m²)	31.50	31.50	31.50		
A weighted sound power level - dB (A)	112.26	112.28	112.27		
Measureme	ent uncertainty	value			
Standard deviation, σ_{omc} , dB (A) (resulting from operation conditions)		2			
Standard compliance deviation of the method, $\sigma_{RO^{\rm t}}$ dB (A)		3			
Total standard deviation, σ_{tot} , dB (A)		3.6			
Extended uncertainty value, U , dB(A) coverage	Extended uncertainty value, U , dB(A) coverage factor k		2		

Table 4. Experimental measurement results and calculations of the operation condition: full thrust.

Source		Cessna 172-S 1	80 HP, 134 kW	
Source location		Single reflective surface, concrete/ asphalt ground		
Ambience		Outdoor environment (negligible K ₂)		
Operation condition		2350 rpm	2350 rpm (full thrust)	
Source dimensions		8.28, 11, 2.72 m		
Microphone positions	Eight positions			
Background noise leve	el correction valu	ie, K _{1A}		
Background noise level, L_{Pa} ΔL_{pA} $\mathrm{Correction\ value,\ }K_{\mathrm{1A}}$	56 dB (A) 15 dB (A) O dB (A)			
	results, dB (A)			
Point 1	83.9	83.7	83.8	
Point 2	81.3	81.4	81.3	
Point 3	81.2	81.2	81.2	
Point 4	83.3	83.4	83.3	
Point 5	81.8	81.8	81.8	
Point 6	83.9	83.9	83.8	
Point 7	83.2	83.2	83.2	
Point 8	83.3	83.4	83.3	
A weighted average sound pressure level, $\bar{L}_{pA^-}\mathrm{dB}$ (A)	82.85	82.86	82.85	
$10 \log \left(\frac{S}{S_0} \right)$ S = hemispherical measuring surface area (m²)	31.50	31.50	31.50	
A weighted sound power level - dB (A)	114.35	114.36	114.35	
Measurement u	ıncertainty value			
Standard deviation, σ_{omc} , dB (A) (resulting from operation conditions)		2		
Standard compliance deviation of the method, σ_{RO} , dB(A)		3	3	
Total standard deviation, σ_{tot} , dBA		3.	6	
Extended uncertainty value, $\it U$, dB(A) coverage fac	ctor k	2	2	

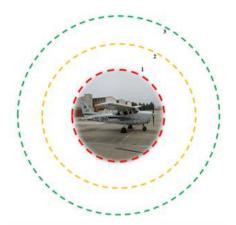


Figure 9. Safe contour zones for Cessna 172-S.

The first contour zone is the minimum diameter distance surrounding all components of the aircraft and will vary depending on the aircraft in maintenance. The second contour zone will end at 4 r from the center. The third contour area will end at 9 r from the center. The specified distances can be implemented in a very practical way, and it is recommended that these distances be maintained.

CONCLUSION

In this study, a noise management model based on the multiapproach method, including some actions related to aircraft noise, has been created. The model was applied to the LTBY.

Within the scope of the model, in the first stage, day, evening and night noise levels around LTBY were simulated using IMMI software under the European noise directive and the ECAC Doc 29-Interim was also used to measure aircraft noise.

According to results of the aircraft noise mapping, it was observed that the noise level, which would adversely affect human health, was not exceeded. However, these values are valid for the year of 2018; it is recommended to update aircraft noise mapping periodically to ensure sustainability. In the study, the use of the runway was evaluated in terms of the prevailing wind direction in the year around the runway. It was suggested to use runway 09 in the months of winter and spring and runway 27 in the rest of the year, due to the departure operations of the aircraft in the analyzed airport.

In the second stage, the noise generated by the Cessna 172-S aircraft, which has a piston-prop engine type, the mostly operated at the LTBY, under different operating conditions, experimentally measured was carried out. According to the noise measuring results, it was observed that the values were exceeding the lowest exposure limit of 80 dB (A). Therefore, preventive measures were examined and opportunities for improvement identified. Safe contour zones were determined for the Cessna 172-S aircraft during maintenance. Furthermore, it was emphasized that protective equipment should be used for the technicians during the maintenance of the aircraft.

After the model had been applied to LTBY, improvement opportunities for aircraft noise were evaluated. Finally, considering that there are not very common studies on the management of aircraft noise in the literature, it is thought that this study will help with the management and evaluation of aircraft noise at other civil airports.

AUTHORS' CONTRIBUTION

Conceptualization: Sogut MZ and Turan O; Methodology: Akdeniz HY, Sogut MZ and Turan O; Investigation: Akdeniz HY; Writing – Original Draft: Akdeniz HY; Writing – Review & Editing: Akdeniz HY, Sogut MZ and Turan O; Supervision: Sogut MZ and Turan O.

DATA AVAILABILITY STATEMENT

The data will be available upon request.

FUNDING

Not applicable.

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