

Research Article

Batch Sorption Experiments: Langmuir and Freundlich Isotherm Studies for the Adsorption of Textile Metal Ions onto Teff Straw (*Eragrostis tef*) Agricultural Waste

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Adsorption of heavy metals (Cr, Cd, Pb, Ni, and Cu) onto Activated Teff Straw (ATS) has been studied using batch-adsorption techniques. This study was carried out to examine the adsorption capacity of the low-cost adsorbent ATS for the removal of heavy metals from textile effluents. The influence of contact time, pH, Temperature, and adsorbent dose on the adsorption process was also studied. Results revealed that adsorption rate initially increased rapidly, and the optimal removal efficiency was reached within about 1 hour. Further increase in contact time did not show significant change in equilibrium concentration; that is, the adsorption phase reached equilibrium. The adsorption isotherms could be fitted well by the Langmuir model. The R_L value in the present investigation was less than one, indicating that the adsorption of the metal ion onto ATS is favorable. After treatment with ATS the levels of heavy metals were observed to decrease by 88% (Ni), 82.9% (Cd), 81.5% (Cu), 74.5% (Cr), and 68.9% (Pb). Results indicate that the freely abundant, locally available, low-cost adsorbent, Teff straw can be treated as economically viable for the removal of metal ions from textile effluents.

1. Introduction

Demands of clothing and apparel increase with the improving sense of fashion and lifestyle; thus textiles are manufactured to meet the growing demands. In developing countries such as Ethiopia, textile production becomes their source of income that contributes to their gross domestic product (GDP). However, this has brought both consequences to such countries either in a positive way which is an improvement of economy or in a negative way which led to an increased anthropogenic impact on the biosphere.

Heavy metals, particularly, Pb, Cr, Cd, and Cu are widely used for the production of color pigments of textile dyes. These heavy metals which have transferred to the environment are highly toxic and can bioaccumulate in the human body aquatic life and natural water bodies and also possibly get trapped in the soil [1]. These toxic heavy metals entering in the aquatic environment are adsorbed onto particulate matter, although they can form free metal ions and

soluble complexes that are available for uptake by biological organisms [2].

Various methods of treating effluents containing heavy metals have been developed over years, such as chemical precipitation, chemical oxidation or reduction, electrochemical treatment, ion exchange, reverse osmosis, filtration, evaporation recovery, and electrocoagulation [3–11]. These methods have significant disadvantages, including high energy requirements, inefficient metal removal, generation of toxic sludge, and expensive equipment. Therefore, there is a need to develop an efficient, rapid, cost-effectively and environment friendly method for the removal of heavy metals from effluents. Adsorption of heavy metals is a new technology for treatment of textile effluents containing different types of heavy metals. Adsorption is the adhesion of a chemical substance (adsorbate) onto the surface of a solid (adsorbent). The most widely used adsorbent is activated carbon [12]. The adsorption process is being widely used by various researchers for the removal of heavy metals [13–18] from



FIGURE 1: Teff straw before treatment (a) and after treatment (b).

waste streams, and activated carbon has been frequently used as an adsorbent.

Adsorption isotherm is an empirical relationship used to predict how much solute can be adsorbed by activated carbon [19]. Adsorption isotherm is defined as a graphical representation showing the relationship between the amount adsorbed by a unit weight of adsorbent (e.g., activated carbon) and the amount of adsorbate remaining in a test medium at equilibrium, and it shows the distribution of adsorbable solute between the liquid and solid phases at various equilibrium concentrations [20]. The three well-known isotherms are (a) Freundlich, (b) Langmuir, and (c) BET adsorption isotherm [19].

In this study a new, environment friendly, cost-effective, and locally available agrowaste *Eragrostis tef* adsorbent was investigated for the adsorption of heavy metals (Cr, Cd, Pb, Ni, and Cu) from textile effluents. The effects of different parameters such as the pH, the initial metal concentration, the dose of the adsorption, the contact time, and temperature were studied.

2. Materials and Methods

2.1. Description of the Study Area. The study was carried at the MAA Garment and Textile Factory built near Alula Abanega airport, due southeast of Mekelle city, Tigray, Northern Ethiopia. The study area lies between latitudes $13^{\circ}28'56''N$ longitudes $39^{\circ}31'59''E$. The factory is owned by Kebire Enterprises Plc. and is fully equipped with state-of-art production facilities acquired from the most reputable manufacturers of the world with over 825 sewing machines. The industrial area is spread over $210,000\text{ m}^2$ of land and it utilizes about $24,000\text{ m}^3/\text{day}$ fresh water. The effluent discharge amounts to about $13,050\text{ m}^3/\text{day}$, that is, 54.4% of the total industrial effluents.

2.2. Adsorbent. Teff straw was used as biomass sample in this study for adsorption of heavy metals from textile effluents. Teff (*Eragrostis tef*) is obviously one of Ethiopia's most important cereal crops. It is indigenous to the country, and it is a fundamental part of the culture, tradition, and food. Recently, the taxonomy of Teff has been clarified by numerical taxonomy techniques, cytology, and biochemistry, including

leaf flavonoids and seed protein electrophoretic patterns [21–23]. The Teff straw was provided by Mekelle University College of Agriculture and treated in the Physical Chemistry laboratory. Figure 1 shows some samples of Teff straw before treatment and after treatment.

2.3. Sorbent Preparation. Teff straw was washed several times with double-distilled water to remove all dirt in its original particle size followed by filtration and was dried at 100°C . The cleaned and dried Teff straw was oven-dried at 400°C for three hours to form carbonized Teff straw (CTS). The CTS was treated with 1 M sulfuric acid at room temperature. Acidified Teff Straw was dried overnight at 70°C and the dried Teff straw was heated to 120°C . The reacted product was washed repeatedly with distilled water. Finally the cleaned Teff straw was oven-dried overnight at 100°C and packed for utilization.

2.4. Sorption Studies

2.4.1. Batch Experiments and Adsorption Isotherms. Sorption studies were conducted by the batch technique and column test using wastewater from MAA Garment. Batch experiments were carried out to determine the adsorption isotherms of metal ions onto the adsorbents in 250 mL glass flask. The flasks were shaken at a constant rate, allowing sufficient time for adsorption equilibrium. It was assumed that the applied shaking speed allows all the surface area to come in contact with heavy metal ions over the course of the experiments. The study was performed at room temperature to be representative of environmentally relevant condition. All experiments were carried out in duplicate and the average value was used for further calculation. The pH of the solution was measured with a HACH-pH meter. The flasks were plugged and kept closed to avoid the fluctuation of pH due to the exchange of gases during the experiment. The effects of various parameters on the rate of adsorption process were observed by varying contact time, adsorbent concentration, temperature, and pH of the solution. The solution volume (V) was kept constant. The amount of metal adsorbed per unit mass is calculated as

$$Q_e = \frac{(C_i - C_e)V}{m}, \quad (1)$$

TABLE 1: Mean concentration (mg/L) with St. dev. of HMs in MAA Garment and Textile Factory effluents.

Sample	Parameters	Ni	Cu	Cd	Cr	Pb
Untreated	Mean \pm St. dev.	3.53 ± 0.33	2.54 ± 0.74	1.23 ± 0.22	0.98 ± 0.07	0.12 ± 0.02
Treated	Mean \pm St. dev.	0.43 ± 0.19	0.47 ± 0.12	0.02 ± 0.01	0.25 ± 0.05	0.04 ± 0.01
	Percentage removed	88%	81.5%	82.9%	74.5%	68.9%

where C_i and C_e are the initial and equilibrium concentration (mg/L), m is the mass of the adsorbent (g) and V is the volume of the solution (mL). Percent metal ion removal (%MR) was calculated using the equation

$$\%MR = \frac{(C_i - C_e)}{C_i} * 100. \quad (2)$$

2.4.2. Column Test. The adsorption experiments were carried out in columns that were equipped with a stopper for controlling the column flow rate. This experiment is useful in understanding and predicting the behavior of the process. The sample solution was passed through the adsorption column with a known amount of ATS at a flow rate of 6 mL/min by gravity. The flow rate was kept constant by controlling the stopper valve.

The concentration of residual individual heavy metal in the sorption medium was determined using fully automated PC-controlled true double-beam AAS with fast sequential operation (Varian AA50 FS, Australia) for fast multielement flame AA determinations with features 4 lamp positions and automatic lamp selection. Statistical analysis was performed using the statistical software packages. Detection limits for each metal on the instrument are: Cr: 0.006 mg/Kg, Cd: 0.002 mg/Kg, Pb: 0.010 mg/Kg, Ni: 0.010 mg/Kg, and Cu: 0.003 mg/Kg.

3. Results and Discussion

3.1. Adsorption of the Tested Heavy Metals onto ATS. Concentrations of heavy metals of the factory's effluent are presented in Table 1. Nickel concentration in the wastewater sample constituted the major portion of the total metal ions determined (3.53) followed by Cu (2.54) and Cd (1.23), while Cr (0.98) and Pb (0.12) concentrations were the lowest. The concentration of nickel in untreated effluent was found to be 3.53 ± 0.33 and in treated sample was 0.43 ± 0.19 ; it was 88% less as compared to untreated effluent (Table 1). The level of copper was 2.54 ± 0.74 in untreated samples and 0.47 ± 0.12 in treated samples which means 81.5% less in treated sample. And the concentrations of cadmium before and after treatment were found to be 1.23 ± 0.22 and 0.02 ± 0.01 respectively, while the levels of the concentration of Pb, 0.12 ± 0.02 and 0.04 ± 0.01 . The obtained results revealed that ATS has good adsorption capacity and is effective for the removal of heavy metals from textile effluent.

3.2. Effect of Adsorbent Dose on Adsorption. The effect of adsorbent dose on the adsorption of the heavy metals onto ATS was investigated. The concentration of heavy metals in

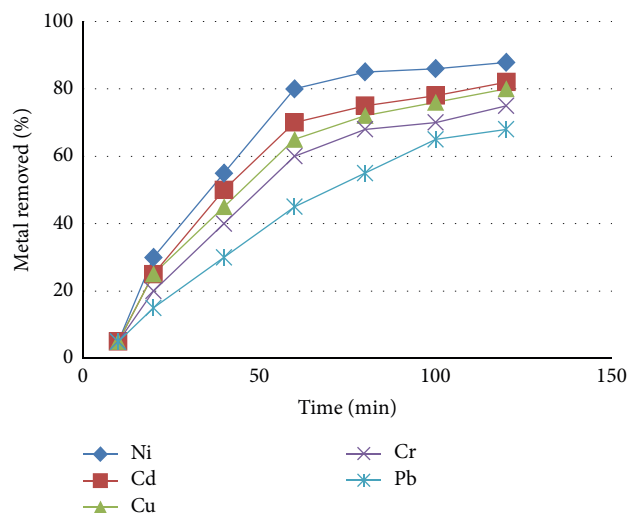


FIGURE 2: Effect of contact time on adsorption efficiency.

the textile effluent was reduced by 88% (Ni), 82.9% (Cd), 81.5% (Cu), 74.5% (Cr), and 68.9% (Pb) after treatment. Metals adsorption efficiency was increased with increase in adsorbent dose. This revealed that the adsorption sites remain unsaturated during the adsorption reaction whereas the number of sites available for adsorption site increases by increasing the adsorbent dose.

3.3. Effect of Contact Time on Adsorption. The effect of contact time on the adsorption of metal was investigated. Figure 2 shows the percent metal ion removal with respect to time. Contact time is one of the most effective factors in batch adsorption process. Adsorption rate initially increased rapidly, and the optimal removal efficiency was reached within about 60 min. Further increase in contact time did not show significant change in equilibrium concentration; that is, the adsorption phase reached equilibrium.

3.4. Effect of Temperature on Adsorption. Effect of temperature on adsorption of the heavy metals onto ATS was studied by conducting different sets of experiments at different temperatures, that is, 298, 308, 318, 328, and 343°K. It was observed that adsorption of metal ions increases with the increase in the temperature.

3.5. Effect of pH on Adsorption. The pH of a solution is an important parameter in the adsorption process. During this study, results revealed that the removal of metal ions was strongly dependent on the pH of the solution. The effect of pH on adsorption of metal ions onto ATS was studied at

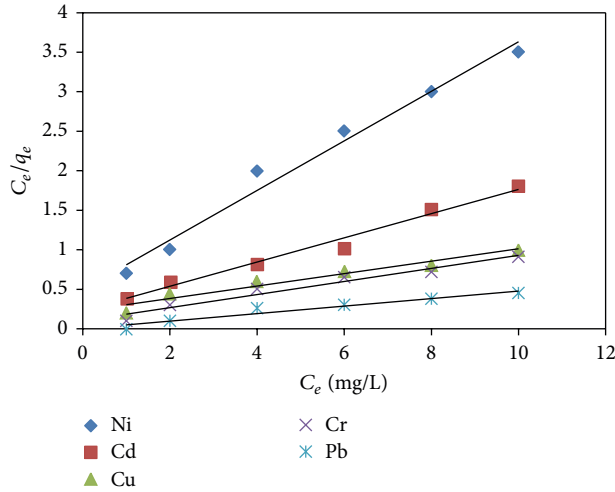


FIGURE 3: Langmuir isotherm showing the variation of adsorption (C_e/q_e) against the equilibrium concentration (C_e) for adsorption of metal ions onto ATS.

TABLE 2: Isotherm parameters for adsorption of metal ions onto ATS.

Isotherm model	Metal ion	Estimated isotherm parameters		
		q_{\max} (mg/g)	b (L/mg)	R^2
Langmuir	Ni	41.2	0.189	0.998
	Cu	34	0.173	0.982
	Cd	27.2	1.908	0.940
	Cr	21.3	0.143	0.962
	Pb	17.5	0.114	0.945
Freundlich	Metal ion	n	K_f	R^2
	Ni	1.10	1.24	0.748
	Cd	2.11	3.52	0.977
	Cu	1.53	2.01	0.967
	Cr	1.50	1.77	0.939
	Pb	1.51	1.82	0.957

pH 1.0–11.0, and the maximum removal capacity of ATS was found to be at pH 6.5. Percent metal ions removal increased rapidly with the increase in pH of the solution initially, and the optimal pH was observed at pH 6.5. Further increase in pH causes a drastic decrease in the adsorption percentage. This might be due to the weakening of electrostatic force of attraction between the oppositely charged adsorbate and adsorbent which ultimately leads to the reduction in sorption capacity [24].

3.6. Adsorption Isotherm. Adsorption is usually described through isotherms, that is, functions which connect the amount of adsorbate on the adsorbent. Distribution of metal ions between the liquid phase and the solid phase can be described by several isotherm models such as Langmuir and Freundlich. The Langmuir isotherm assumes monolayer adsorption onto a surface containing a finite number of adsorption sites of uniform strategies with no transmigration

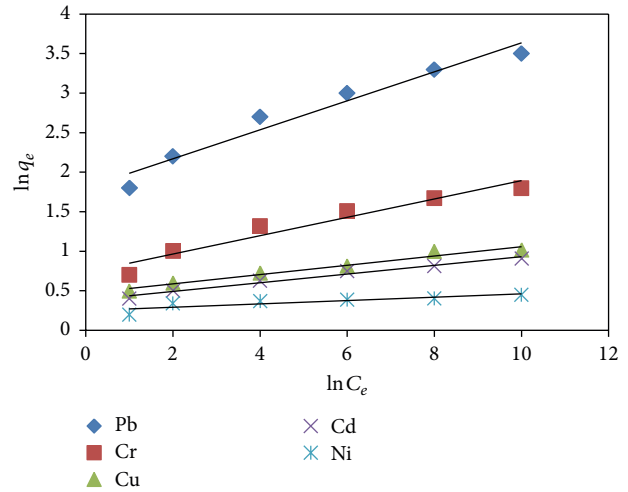


FIGURE 4: Freundlich isotherm representing variation of $\ln(q_e)$ with respect to $\ln(C_e)$ for adsorption of metal ions onto ATS.

of adsorbate in the plane surface [25]. Once a site is filled, no further sorption can take place at that site. This indicates that the surface reaches a saturation point where the maximum adsorption of the surface will be achieved. The isotherm is represented by

$$\frac{C_e}{q_e} = \frac{1}{bq_{\max}} + \frac{C_e}{q_{\max}}. \quad (3)$$

The linear plot of specific adsorption (C_e/q_e) against the equilibrium concentration (C_e) (Figure 3) shows that the adsorption obeys the Langmuir model. The constants b and q_{\max} relate to the energy of adsorption and maximum adsorption capacity, and their values are obtained from the slope and interception of the plot and are presented in Table 2.

The Freundlich isotherm is introduced as an empirical model, where q_e represents the amount adsorbed per amount of adsorbent at the equilibrium (mg/g), C_e represents the equilibrium concentration (mg/L), and K_f and n are parameters that depend on the adsorbate and adsorbent.

Consider

$$q_e = K_f C_e^{1/n}. \quad (4)$$

The equation can be linearized and the temperature dependent constants K_f and $1/n$ found by linear regression:

$$\ln q_e = \ln K_f - \frac{1}{n} \ln C_e, \quad (5)$$

where K_f and n are Freundlich constants which correspond to adsorption capacity and adsorption intensity, respectively. Freundlich equilibrium constants were determined from the plot of $\ln q_e$ versus $\ln C_e$ from Figure 4, on the basis of the linear form of Freundlich equation. The n value indicates the degree of nonlinearity between solution concentration and adsorption as follows: if $n = 1$, then adsorption is linear; if $n < 1$, then adsorption is a chemical process; if $n > 1$, then adsorption is a physical process. The n value in Freundlich

equation was found to be 1.10–2.11, (Table 2). The situation $n > 1$ is most common and may be due to a distribution of surface sites or any factor that causes a decrease in adsorbent-adsorbate interaction with increasing surface density [26] and the values of n within the range of 1–10 represent good adsorption [27, 28]. In the present study, since n lies between 1 and 10 it indicates the physical adsorption of metal ions onto ATS.

In both cases, linear plots were obtained, which reveal the applicability of these isotherms on the ongoing adsorption process. Figures 3 and 4 exhibit Langmuir and Freundlich plots, respectively, for the adsorption of metal ions onto ATS, and different Langmuir and Freundlich constants derived from these plots are presented in Table 2. Nearly similar results have been reported in the literature [29–31] for Langmuir and Freundlich models.

Langmuir and Freundlich adsorption constants and correlation coefficients (R^2) are presented in Table 2. To find the most appropriate model for the metal ions adsorption; data were fitted to Langmuir and Freundlich isotherm models. Results revealed that Langmuir adsorption isotherm was the best model for the metal ions adsorption onto ATS with R^2 of 0.998. The essential features of Langmuir adsorption isotherm parameter can be used to predict the affinity between the sorbate and sorbent using a dimensionless constant called separation factor or equilibrium parameter (R_L), which is expressed by the following relationship [32, 33]:

$$R_L = \frac{1}{(1 + bC_i)}, \quad (6)$$

where b is the Langmuir constant and C_i is the initial concentration. The value of R_L indicated the type of Langmuir isotherm to be irreversible ($R_L = 0$), linear ($R_L = 1$), unfavorable ($R_L > 1$), or favorable ($0 < R_L < 1$) [34]. The R_L values between 0 and 1 indicate favorable adsorption. The R_L value in the present investigation was found to be 0.298–0.986, indicating that the adsorption of the metal ion onto ATS is favorable.

4. Conclusions

Teff (*Eragrostis tef*) straw is environment friendly, cost-effective, and locally available agrowaste adsorbent for the adsorption of metal ions from textile effluents. Results from this study showed that adsorption of heavy metals onto ATS increases with the amount of adsorbent. This may be explained because of the fact that adsorption is a surface phenomenon where adsorbate molecules occupy specific sites on the adsorbent. These sites are commonly known as active centers. The concentration of these active centers on the surface is further related to the pore size and pore volume available after impregnation. This explains why increasing the quantity of adsorbent results in increased adsorption. Results revealed that initially the % removal increase, rapidly; however, after some times the rate becomes almost constant. This is because all the available active centers on the adsorbent have been occupied and there are no further sites and hence no further adsorption is possible. The time when this

phenomenon occurs, therefore, may be termed optimum time.

The adsorption isotherms could well be fitted by the Langmuir model. The R_L value in the present investigation was less than one, indicating that the adsorption of the metal ion onto ATS is favorable. In treatment with ATS, the removal of metal ions from textile wastewater sample is high whereby the percentage of removal is more than 80 percent of the initial concentration. Since Teff Straw is freely abundant, locally available, low-cost adsorbent and has a considerable high adsorption capacity, it may be treated as economically viable for removal of metal ions from textile effluents.

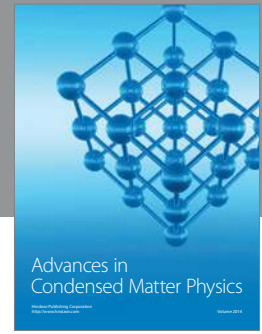
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