BEHAVIOUR OF MINE WASTE AS REINFORCED SOIL

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Abstract

Mining in Goa is done by open cast method, which gives rise to huge quantity of mining waste that occupies space and forms a source for series of problems. The enomerous amount of mine waste dumped around the regions of mining activity need to be reused constructively. Hence, if the mine waste is studied for its use as a reinforced soil, then burning issue of environmental pollution caused by mining dumps lying unprotected and unstabilized can be tackled to a certain extent. Also, it will be a step towards finding an alternative material for cohesionless soil in reinforced soil construction. In this study an attempt is made to check the suitability of soil from one of the mining dumps in Goa to be used as reinforced soil. The mine waste soil samples are studied for its compressive strength and shear strength behaviour by conducting two types of tests, unconfined compressive strength test and triaxial tests on unreinforced and reinforced soil samples. The reinforcement used in the form of a grid made from natural material bamboo. The bamboo grid reinforcement is placed in one, two and three layers, for studying the effect of reinforcement on compressive strength, shear strength parameters, stiffness and modes of failure of mining waste soil. The results of the tests on mining waste show improvement in strength as a reinforced soil mass.

Index Terms: Mine waste, bamboo reinforcement, unconfined compression strength and triaxial tests

1 INTRODUCTION

Mine waste dumps have caused severe damage to the ecology and hydrology of the tiny state of Goa. As per the report of Goa State Pollution Control Board [10] there are 316 mining dumps spread across the mining active regions of the state, resulting in accidents such as slipping into and destroying paddy fields, silting up rivers including those supplying drinking water. Agriculture and horticulture all over the mining belt in the state has been severely hit by mining dumps. Due to decades of extraction of minerals, many mines are unable to store dumps within their mining lease, due to huge collection of substandard ore, rejects and overburden [8]. There is a need to put the mine waste to constructive use. Many researchers have attempted to study the stress-strain behaviour of cohesionless soil using triaxial tests [5], [15], [17]. Cohesive soil has also been considered for reinforced soil construction [11], [13]. However very limited research work is available on mine waste as an alternative material for reinforced soil construction. Cohesive soils with appropriate compaction also behave as good as granular soil with reinforcement and they can be used as an alternative material for soil wall construction [3]. Over the years strengthening of soil is done with variety of reinforcements which include natural geosynthetics made from jute, coir, bamboo in consolidation of soil [4], improving bearing capacity of soft soils, [15], as general soil reinforcement material [7].

The present study uses the combination of mine waste and bamboo grid as reinforcement to study the shear strength behaviour of soil under unconfined compression and triaxial loading conditions, so as to explore the use of mine waste from one particular region of Goa as alternative material for reinforced soil construction.

2 CHARACTERIZATION OF MATERIALS

2.1 Mine Waste

Mine waste soil obtained from the mining dumps at Advalpal village in Goa is considered for use as reinforced soil. The physical properties of the mine waste soil samples obtained from mining dumps are given in Table-1. The electrochemical property pH of mining waste is determined to be 5.48. Representative sample of mine waste soil is shown in Fig-1

Table -1: Physical properties of mine waste soil

Property	Value
Specific gravity, G	2.625
Liquid Limit, W _L (%)	37.80
Plastic Limit, $W_P(\%)$	32.36
Plasticity Index, I _P (%)	5.44
Effective particle size, D ₁₀ (mm)	0.0017
D _{30 (} mm)	0.042
D _{60 (} mm)	0.52
Uniformity Coefficient, C _u	305.88
Coefficient of curvature, C _c	1.995
Maximum dry unit weight, γ_{dmax} (kN/m ³)	20.1
Optimum moisture content, OMC (%)	11.17%
Coefficient of permeability, k (m/sec)	2.46 x 10 ⁻⁰⁶



Fig-1: Mining waste soil sample

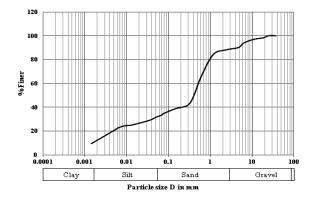


Fig -2 shows the grain size distribution curve for the soil. According to IS: 1498, 1970 [12], the mine waste soil is classified as silty sand.

Fig-2: Particle size distribution curve for mine waste soil

2.1.1 Chemical Composition Of Soil

The mine waste soil was tested for its chemical composition at the the Sophisticated Analytical Instrument Facility (SAIF), I.I.T., Bombay. X-Ray fluorescence test was performed by using a spectrometer (Philips PW 2404). The chemical composition of mining waste soil is given in Table-2.

Chemical composition of mi	
Chemical Name	Value (%)
SiO ₂	27.782
Al ₂ O ₃	10.441
Fe ₂ O ₃	10.748
CaO	0.004
K ₂ O	0.501
MnO	0.052
P_2O_5	0.018
SrO (ppm)	15.384
TiO	1 449

 Table -2:
 Chemical composition of mine waste

2.2 Reinforcement

Natural material bamboo is used as reinforcement. Bamboo strips are arranged to form a bamboo grid (BG), the grid is circular in shape with diameter 55 mm and aperture size 10 mm x 10 mm as shown in

Fig-3.



Fig-3: Bamboo grid

2.2.1 Tensile Strength of Bamboo Grid

The tensile strength of bamboo grid is evaluated by conducting wide width tension test. The test is performed as per ASTM D4595 [1]. Fig-4(a) (b) shows the bamboo grid in wide width tension test before and after failure respectively. Bamboo grid sample of size 200 mm wide x 100 mm gauge length was subjected to tensile pull. Fig-5 shows the load-strain curve of bamboo grid tension test. Table-3 gives the properties of bamboo used in the present study.

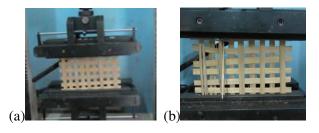


Fig-4: Bamboo grid in tension test (a) before failure, (b) after failure

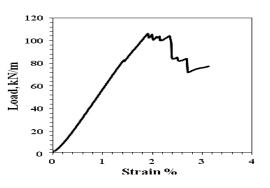


Fig-5: Load versus strain curve for bamboo grid sample Table -3: Properties of bamboo

Property	Value
Mass per unit area (gm/m ²)	512.5
Tensile Strength (kN/m)	106.37
Maximum elongation	1.9 %
Initial tangent modulus (kN/m)	7142.85

3 EXPERIMENTAL WORK

3.1Tests Conducted

The mining waste soil is subjected to following types of tests to check the strength in unreinforced and reinforced case.

- 1) Unconfined Compression Strength (UCS) tests
- 2) Triaxial Tests (Unconsolidated Undrained, UU)

3.1.1Preparation Of Specimen

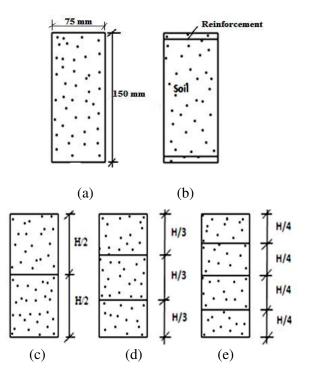
Remoulded specimens are prepared in the laboratory depending on the proctors data at the required moulding water content. The sample size used was 75 mm diameter and 150 mm height, prepared in a split mould. The dry weight of soil (Wdsoil) required to prepare the specimen was calculated based on, Wdsoil = γ dmax × volume of the triaxial mould. The amount of water to be added was calculated by Wwater= Wdsoil × OMC. The dry soil and water is then mixed into a homogeneous mass.

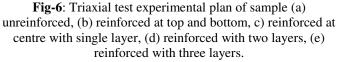
For unreinforced sample the measured quantity of soil is put in the mould in layers and 25 blows are applied to each layer. Care is taken to obtain uniform degree of compaction. For the reinforced sample preparation the measured quantity of soil required to fill the triaxial mould was divided into equal portions based on the number of layers of reinforcement. The level of reinforcement position is marked on the mould and accordingly the soil is compacted up to the marking, then the compacted soil surface is scratched with the help of a pointed tool and the reinforcement is placed. Five types of samples were tested,

- i. Unreinforced soil sample
- ii. Reinforced soil sample with reinforcement at top and bottom
- iii. Reinforced soil sample with reinforcement at the mid height of sample
- iv. Reinforced soil sample with reinforcement at each 1/3rd of sample height and
- v. Reinforced soil sample with reinforcement at each 1/4th

of sample height.

The soil density in each test was maintained constant. Confining pressures used were 50 kPa, 100 kPa and 150 kPa, so as to obtain the shear strength parameters and to simulate the different loading conditions in the field. Fig-6(a) to (e) shows the five soil samples considered in experimental plan.





3.1.2 Test Procedure

The UCS test is conducted by placing the unreinforced or reinforced soil sample in the Perspex cell, without water in the cell, hence confining pressure on the soil sample is zero and the soil is made to fail under increasing normal pressure. The sample is sheared under constant volume.

The Unconsolidated Undrained (UU) triaxial tests were conducted as per Indian Standard IS 2720(part 11) - 1993 [12]. Fig-7 shows the triaxial test apparatus used for conducting the tests. The specimen was carefully extruded, weighed to check the desired density of compacted sample being attained, and immediately set up in the triaxial cell. The hydraulic confining pressure system was used to apply confining pressure simulating the effect of surrounding soil at that depth. A load cell and LVDT (Linear Variable Differential Transformer) is used to measure the deviator load and vertical displacement respectively through an electronic display system. The load

cell and LVDT are calibrated before use. The strain rate was kept at constant rate of 1.2 mm/minute during testing.

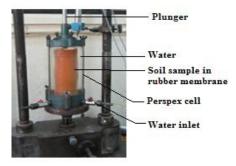


Fig-7: Triaxial test apparatus

The test is stopped when the deformation of the sample increases without any considerable increase in load. All the tests were conducted up to maximum axial strain of 20% to permit evaluation of the post peak stress-strain behaviour. However all samples failed prior to reaching 20% strain. The test was conducted to investigate the strength contribution made by bamboo reinforcement and the soil behaviour as reinforced soil under triaxial loading.

4 RESULTS AND DISCUSSIONS

4.1 Unconfined Compressive Strength Test

4.1.1 Modes Of Failure

Fig-8(a) to (e) shows the modes of failure of soil samples tested under unconfined compression. The failed samples show fine cracks on the sample surface inclined at approximate values of $45 + \phi/2$. Samples with two and three layers of reinforcement show longer cracks on the surface along with some amount of bulging.

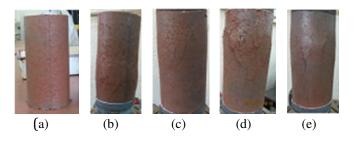


Fig-8: Modes of failure of soil sample: Unreinforced soil sample (a) before failure (b) after failure (c) Soil sample with reinforcement at centre (d) Reinforcement at each 1/3rd height of sample(two layers) and (e) Reinforcement at each 1/4th height of sample (three layers)

4.1.2 Stress Strain Behaviour

The stress-strain curves are shown in

Fig-9. The stress - strain curves show a well defined peak stress at failure and there is loss in post-peak stress values. Unreinforced soil samples reaches the peak stress value at axial strain of 2.26%, whereas, the reinforced soil samples attain the peak shear strength value at axial strain of 2%, hence reinforcement increases the stiffness of soil samples. The soil deformation mobilizes the shear strength in soil and peak strength of the soil increases with deformation until a peak shear stress value is attained. The peak shear stress value increases as the number of layers of reinforcement are increased from no reinforcement to three layers of reinforcement. Table-4 gives the UCS and strain % values corresponding to unreinforced and reinforced mine waste soil specimen.

Table-4: Unconfined compressive strength and strain values

Type of specimen	UCS (kPa)	strain %
Unreinforced soil	298.67	2.26
Reinforced with BG, 1 layer	366.97	2.00
Reinforced with BG, 2 layers	430.34	2.00
Reinforced with BG, 3 layers	488.01	2.00

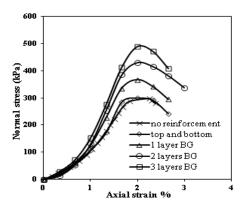


Fig-9: Stress-strain curves corresponding to unreinforced soil sample and samples reinforced at top and bottom, at centre, at 1/3rd height and at 1/4th height of soil specimen

4.2 Tri axial Test

4.2.1 Modes Of Failure

The modes of failure of triaxial test specimen are shown in Fig-10(a), (b), (c). In case of unreinforced soil failed samples fine cracks were observed on the surface, whereas the reinforced soil samples failed by bulging. Bulging is more towards the central and bottom portion of the reinforced soil samples. Bulging of specimen indicates deformation of the soil and deformation mobilizes the shear strength of soil. Bulging is noticed to be more prominent for soil samples reinforced with three layers of bamboo grid.

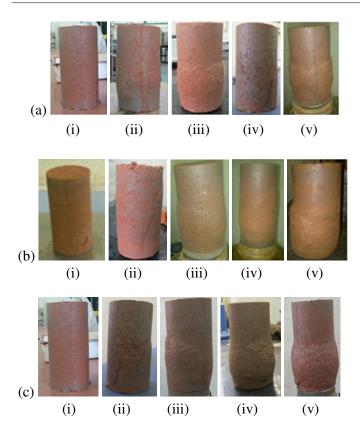


Fig-10: Modes of failure of soil sample at confining pressure
(a) 50 kPa (b) 100kPa and (c) 150 kPa for soil as i)
Unreinforced soil sample before failure ii) after failure iii)
reinforced sample after failure with reinforcement at centre iv)
at each 1/3rd height of sample (two layers) and v) at each
1/4th height of sample (three layers)

4.2.2 Stress Strain Behaviour

The stress strain curves are shown in Fig-11(a), (b), (c). The unreinforced sample has the least deviator stress at failure and the sample with reinforcement at top and bottom shows a similar behaviour, the reinforced samples exhibit higher values of peak deviator stress and the deviator stress increases with the number of layers of reinforcement, the highest being for the sample with three layers of reinforcement.

The loss in post peak deviator stress is less in the triaxial tested samples as compared with the samples in unconfined compression strength tests. In triaxial test soil can sustain larger deformations due to confinement. It is noticed that after attaining maximum value of deviator stress there is not much change in the stress value. As seen in stress-strain curves of triaxial tests, axial strain % corresponding to peak deviator of reinforced soil sample is lower than the axial strain % corresponding to peak deviator stress of unreinforced soil; this indicates the stiffness of reinforced soil samples in triaxial tests.

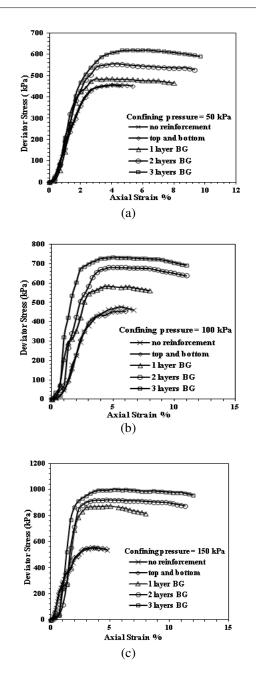


Fig-11: Deviator stress-strain relationship for unreinforced and reinforced soil samples at confining pressures of (a) 50 kPa (b) 100 kPa (c) 150 kPa

4.2.3 P-Q Diagrams And Shear Strength Parameters

Fig-12 show the p-q diagram corresponding to unreinforced sample and samples reinforced with one, two and three layers of reinforcement.

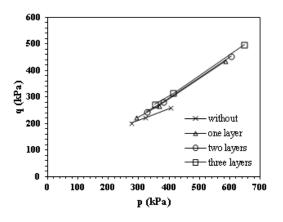


Fig-12: p-q diagram for the unreinforced and reinforced Samples

Table-5 lists the values of shear strength parameters of the unreinforced and reinforced soil samples based on the p-q diagram.

Table-5: Shear strength parameters of unreinforced andreinforced soil samples with triaxial tests at confining pressuresof 50 kPa, 100 kPa and 150 kPa

Soil sample	C or C _a (kPa)	φ or δ (°)
Unreinforced soil	51.5	32
Reinforced with BG, 1 layer	17.5	53
Reinforced with BG, 2 layers	32.5	52
Reinforced with BG, 3 layers	45	51
 C Cohesion for unreinforced case C_a Adhesion for reinforced case \$		
δ Friction angle for reinforced case		

The shear strength parameter values indicate slippage failure of the bamboo reinforced mining waste, as the adhesion is decreasing and the interface friction angle is increasing as compared to the cohesion and friction angle of unreinforced soil mass.

4.2.4 Effect Of Number Of Reinforcement Layers On

Peak Deviator Stress

Effect of number of layers of reinforcement is shown in Fig-13. Bamboo grid inclusion increases the peak deviator strength of mine waste significantly. Unreinforced sample has the least peak deviator stress. For reinforced sample with one layer at centre, the peak deviator stress increases by 5%, with two

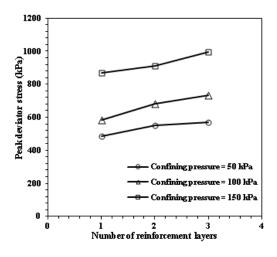


Fig-13: Effect of number of layers of reinforcement (bamboo grid) on the peak deviator stress

layers it increases by 19.4% and with three layers of reinforcement the peak deviator stress increases by 22.9% as compared to the peak deviator stress of unreinforced soil sample at a confining pressure of 50 kPa. For applied confining pressure of 150 kPa the peak strength increases by 57.6%, 64.5% and 80.2% as the number of reinforcement layers increase from one to three. Increase in peak shear strength is more pronounced for greater number of reinforcement layers. This indicates that the reinforcement improves the lateral confinement of the soil sample. The peak deviator stress values corresponding to all the test cases is given in Table-6.

Table-6: Peak deviator stress for unreinforced and reinforced soil samples with one, two and three layers of bamboo grid reinforcement.

Type of soil	Peak deviator stress values		
sample	50 (kPa)	100 (kPa)	150 (kPa)
Unreinforced	462.75	476.89	552.68
Reinforced with BG, 1 layer	486.02	582.80	870.94
Reinforced with BG, 2 layers	552.53	682.27	908.96
Reinforced with BG, 3 layers	608.25	734.72	995.81

4.2.5 Effect of Confining Pressure On The Peak Deviator Stress

The applied confining pressure improves the peak deviator stress, which is depicted in the Fig-14. The peak deviator stress of unreinforced sample increases as the applied confining pressure is increased from 50 kPa to 150 kPa. The sample reinforced with one layer of bamboo grid at centre shows an increase of 5.03%, 22.2 % and 57.58% in peak deviator stress at the confining pressure of 50, 100 and 150 kPa respectively. The inclusion of bamboo grid in mine waste soil shows an impact on improving the strength of the mining waste soil in conjunction with confining pressure.Table-7 brings out the comparison of the mine waste with the FHWA (2001) recommendations [9].

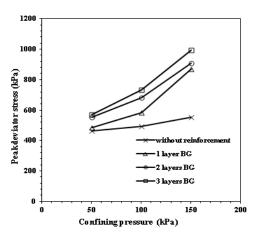


Fig-14: Effect of confining pressure on the peak deviator stress of unreinforced and soil sample reinforced with one, two and three layers of bamboo grid reinforcement

Property of soil	FHWA recommendation	Present study result
Plasticity Index, Ip	Shall not exceed 6	5.44
Angle of internal friction, φ	Lower bound value 28°	32°
Cohesion (kPa)	Cohesionless	51.5
pH value	> 3< 9	5.48
% passing 0.075 mm	0-15	21.67

 Table-7: Comparison of mine waste properties with FHWA (2001) recommendations

CONCLUSIONS

The mine waste soil is tested for its strength improvement as reinforced mass by using bamboo reinforcement. Based on the experimental findings, following conclusions are drawn,

- 1. The evaluated unconfined compressive strength of the bamboo reinforced mine waste soil was more as compared to the unreinforced sample and increases as the number of layers of reinforcement increased.
- 2. The peak stress value in UCS test for unreinforced case is reached at a strain value of 2.26%, whereas for the

reinforced case the peak deviator stress is reached at a strain of 2%. Hence reinforced mine waste soil behaves stiffer than the unreinforced soil mass.

- 3. The UCS for unreinforced case was 298.67 kPa and it increases to 366.97, 430.34, 488.01 kPa for mine waste reinforced with one layer, two layers and three layers of reinforcement respectively.
- 4. Triaxial test results indicate shear strength improvement of mine waste soil with reinforcement as well as with confining pressure. The maximum strength improvement was with three layers of reinforcement at an applied confining pressure of 150 kPa.
- 5. The adhesion value of each of the reinforced case is less than the cohesion value of unreinforced case, whereas the angle of internal friction is increased by an average amount of 62.49% as compared to the unreinforced case.
- 6. The reinforcement enhances the confinement of the sample over and above the applied confining pressure, hence for a particular confining pressure the percentage increase in peak deviator stress is more with increasing confining pressure as compared to the percentage increase in peak deviator stress with number of layers of reinforcement at same confining pressure.
- 7. The grid structure of reinforcement being open structure allows strength mobilization at low stresses and further enhances the friction at the soil-reinforcement interface thereby increasing the shear strength of soil.
- 8. Hence, the abundant soil available as mine waste dumps at Advalpal village in Goa can be considered for its use as reinforced soil along with bamboo reinforcement.

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