

CERN/PS/BR 77-6
16.5.1977

[REDACTED]
CERN LIBRARIES, GENEVA



CM-P00059343

BUNCH LENGTHENING AND MICROWAVE INSTABILITY

(Part 2)

F.J. Sacherer

This is a continuation of CERN/PS/BR 77-5 (Part 1)

CONTENTS

1. Derivation of the mode-coupling matrix
2. Adjoint modes
3. Resonator
4. Coasting-beam stability criterion

References

1. DERIVATION OF THE MODE-COUPLING MATRIX

The equations of motion for a single particle are

$$\frac{d\Delta E}{dt} = \frac{e\omega_0}{2\pi} [V_{rf} \sin \phi + \text{induced voltage}] \quad (14)$$

$$\frac{d\phi}{dt} = \eta h \omega_0 \frac{\Delta E}{p} = \frac{\eta h \omega_0}{\beta^2} \frac{\Delta E}{E} \quad (15)$$

where ΔE and ϕ are energy and phase (RF radians) deviations from the synchronous values, V_{rf} is the peak RF voltage per turn, and $\eta = 1/\gamma_T^2 - 1/\gamma^2$. The additional voltage due to the coupling impedance $Z(\omega)$ has a stationary part $V_0(\phi)$ induced by the stationary line density $\lambda_0(t)$ and an oscillating part $V_m(\phi, t)$ due to the perturbation $\lambda_m(\phi, t)$. In the following, we set $h = 1$ and $V_{rf} \sin \phi + V_0(\phi) = V_T \phi$ to simplify the derivation. Then (14) and (15) become

$$\ddot{\phi} + \omega_s^2 \phi = -\omega_{so}^2 \frac{V_m(\phi, t)}{V_{rf}} = -\omega_s^2 \frac{V_m(\phi, t)}{V_T} \quad (16)$$

where ω_{so} is the synchrotron frequency (rad/sec) corresponding to the voltage V_{rf} and ω_s is the single-particle or incoherent frequency corresponding to the total voltage V_T .

For the stationary distribution, the particle orbits are circles in the normalized phase plane (Fig. 8), and the stationary distribution $\psi_0(r)$

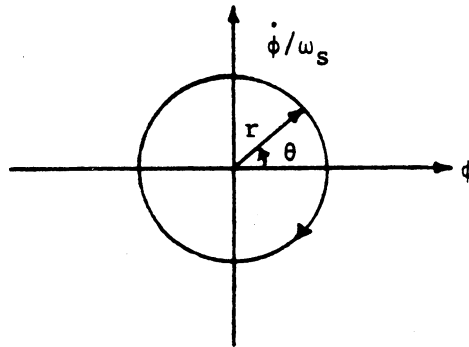


FIG. 8

depends only on the amplitude r and not on the synchrotron phase θ . For small oscillations about the stationary distribution

$$\psi = \psi_0(r) + \psi_m(r, \theta)e^{j\omega t} \quad (17)$$

where ψ_m satisfies the usual linearized Vlasov equation

$$j\omega\psi_m - \omega_s \frac{\partial \psi_m}{\partial \theta} - \omega_s \frac{V_m(\phi)}{V_T} \frac{d\psi_0}{dr} \sin \theta = 0. \quad (18)$$

Normalize ψ ,

$$\int \psi d\phi d\dot{\phi} = \int \psi \omega_s r dr d\theta = 1, \quad (19)$$

and introduce the line density

$$\lambda(\phi) = \int \psi d\dot{\phi}. \quad (20)$$

For N particles/bunch, $eN\lambda(\phi)$ = charge/radian, $eN\omega_0\lambda(\phi)$ = charge/sec, and

$$V_m(\phi) = -eN\omega_0 \sum_p Z(p) \tilde{\lambda}_m(p) e^{jp\phi} \quad (21)$$

where

$$\lambda(\phi) = \sum_p \tilde{\lambda}(p) e^{jp\phi}. \quad (22)$$

In the limit of zero intensity, $V_m = 0$, and the solutions of (18) are

$$\psi_m = R_m(r) e^{jm\theta} \quad (23)$$

$$\omega = m\omega_s$$

where $R_m(r)$ is any function of r . For the general solution, write

$$\psi = \sum_m R_m(r) e^{jm\theta} \quad (24)$$

and substitute into (18) to find the equations

$$j(\omega - m\omega_s) R_m(r) \delta_{mk} = \frac{eN\omega_0 \omega_s}{V_T} \frac{d\psi_0}{dr} \sum_{p,k} j^m \frac{m}{pr} J_m(pr) \tilde{\lambda}_k(p) Z(p) \quad (25)$$

where δ_{mk} is the kronecker delta. The relation

$$\frac{1}{2\pi} \int_0^{2\pi} e^{jpr \cos\theta - jm\theta} \sin\theta d\theta = -j^m \frac{m}{pr} J_m(pr) \quad (26)$$

has been used where J_m is a Bessel function. Since

$$\begin{aligned} \tilde{\lambda}_k(p) &= \frac{1}{2\pi} \int_0^{2\pi} e^{-jp\phi} \lambda_k(\phi) d\phi \\ &= (-j)^k \int_0^\infty J_k(pr) R_k(r) \omega_s r dr, \end{aligned} \quad (27)$$

equation (25) can be written as

$$j(\omega - m\omega_s) R_m(r) \delta_{mk} = \frac{m\omega_s}{V_T} eN\omega_0 \frac{1}{r} \frac{d\psi_0}{dr} j^m \sum_{p,k} (-j)^k \frac{Z(p)}{p} J_m(pr) \int_0^\infty J_k(pr') R_k(r') \omega_s r' dr'. \quad (28)$$

For low intensities, only the diagonal $m=k$ term need be retained, and (28) reduces to an integral equation for the radial mode pattern $R_m(r)$ and eigenfrequency ω .

It is shown in the next section that the adjoint function $R_m^+(r)$ defined by

$$R_m(r) = \frac{1}{r} \frac{d\psi_0}{dr} R_m^+(r) \quad (29)$$

is orthogonal to $R_m(r)$. Multiply (28) by $R_m^+(r)$ and integrate over $\omega_s r dr$ to find the equations

$$j(\omega - m\omega_s) \int_0^\infty R_m^+ R_m \omega_s r dr \delta_{mk} = \frac{m\omega_s}{V_T} e N \omega_0 \sum_{p,k} \frac{Z(p)}{p} \tilde{\lambda}_m^*(p) \tilde{\lambda}_k(p) \quad (30)$$

The LHS of (30) can be expressed in terms of the line density rather than $R(r)$. Consider the sum

$$\begin{aligned} \sum_{p=0}^{\infty} p \tilde{\lambda}_k^*(p) \tilde{\lambda}_k(p) &= \sum_{p=0}^{\infty} p \int_0^\infty \int_0^\infty J_k(pr) R_k(r) \omega_s r dr J_k(pr') R_k(r') \omega_s r' dr' \\ &= \omega_s^2 \int_0^\infty R_k^2(r) r dr \end{aligned} \quad (31)$$

since

$$\begin{aligned} \sum_{p=0}^{\infty} p J_k(pr) J_k(pr') &= \int_0^\infty x J_k(xr) J_k(xr') dx \\ &= \frac{1}{r} \delta(r' - r). \end{aligned} \quad (32)$$

For the parabolic distribution

$$\psi_0(r) = \frac{2}{\pi \omega_s \phi_0^2} (\phi_0^2 - r^2), \quad (33)$$

$$\frac{1}{r} \frac{d\psi_0}{dr} = - \frac{4}{\pi \omega_s \phi_0^4} \quad (34)$$

and (31) becomes

$$\begin{aligned} \int_0^\infty R_k^+(r) R_k(r) \omega_s r dr &= -\frac{1}{4} \pi \phi_0^4 \sum_{p=0}^\infty p \tilde{\lambda}_k^*(p) \tilde{\lambda}_k(p) \\ &\approx -\frac{1}{8} \pi \phi_0^4 \bar{p} \sum_{p=-\infty}^\infty \tilde{\lambda}_k^*(p) \tilde{\lambda}_k(p), \end{aligned} \quad (35)$$

where \bar{p} is the central line in the mode spectrum $\tilde{\lambda}_k(p)$. For the sinusoidal modes of figures 2 and 3,

$$\bar{p} f_0 = \frac{k+1}{2\tau_L}, \quad (36)$$

so $\bar{p} = (k+1)/2B_0$. Thus (30) reduces to (3),

$$|\omega - m\omega_s - M_{mk}| = 0 \quad (37)$$

where the matrix M_{mk} is given by (5). The relations $\phi_0 = \pi B_0$ and $I_0 = eN\omega_0/2\pi$ have been used.

The main approximation in the derivation of (37) is the relation (36) for the central frequency $\bar{p} f_0$ of the mode spectrum. Somewhat smaller values have been measured experimentally⁴ and are likely to occur for Gaussian bunches also. In any event, the correct value of \bar{p} can be used in (37) if desired.

2. ADJOINT MODES

The diagonal $m = k$ term of equation (28) has the form

$$(\omega - m\omega_s) R_m(r) = \frac{1}{r} \frac{d\psi_0}{dr} \int_0^\infty G_m(r, r') R_m(r') r' dr' \quad (38)$$

where

$$G_m(r, r') = -j \frac{m\omega_s^2}{V_T} eN\omega_0 \sum_p \frac{Z(p)}{p} J_m(pr) J_m(pr') = G_m(r', r) \quad (39)$$

is a symmetric kernel. In general, the integral equation (38) has an infinite number of solutions for each azimuthal mode number m . These can be labelled by the index q which specifies the number of nodes in the radial mode pattern $R_{mq}(r)$ (see Fig. 9).

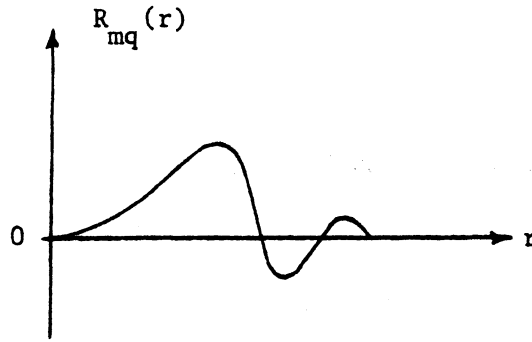


FIG. 9 : The radial mode pattern for $q = 2$.

For each mode, there is an adjoint mode, which satisfies the orthogonality relation

$$\int_0^{\infty} R_{mq}^+(r) R_{ml}(r) r dr = 0 \quad \text{unless } q = l. \quad (40)$$

This can be shown as follows. By definition, the adjoint mode is the solution of the adjoint equation

$$\Delta \omega_q^+ R_q^+(r) = \int_0^{\infty} G_m(r, r') \frac{d\psi_0}{dr'} R_q^+(r') dr' \quad (41)$$

where the index m of R_{mq}^+ is dropped, and $\Delta\omega_q^+ \equiv \omega_q^+ - m\omega_s$. Multiply (41) by $R_1(r)$, equation (40) by $R_q^+(r)$, integrate and subtract to find

$$(\Delta\omega_q^+ - \Delta\omega_1) \int_0^\infty R_q^+(r) R_1(r) r dr = 0. \quad (42)$$

By comparing (38) and (41), it is clear that

$$R_q(r) = \frac{1}{r} \frac{d\psi_0}{dr} R_q^+(r) \quad (43)$$

$$\Delta\omega_q = \Delta\omega_q^+$$

and therefore (42) reduces to (40).

In part 1, only one radial mode ($q=0$) is kept for each azimuthal mode number m , and the second index on $R_{mq}(r)$ is dropped. The neglected higher-order radial modes are assumed to describe the single-particle incoherent motion. A different approach that includes some of the higher-order radial modes is given in reference 7.

3. RESONATOR

A parallel LCR circuit is assumed with impedance

$$Z(\omega) = -jR\sigma \frac{\omega}{\omega_r} \left[\frac{1}{\omega - \omega_r - j\sigma} - \frac{1}{\omega + \omega_r - j\sigma} \right] \quad (44)$$

where

$$\omega_r = \frac{1}{\sqrt{LC}}, \quad (45)$$

$$\sigma = \frac{1}{2RC}.$$

The form factor in equation 7 is

$$F_{mk} = \Delta_{mk} \frac{2}{\pi^2} |S_m S_k|$$

where

$$\Delta_{mk} = \begin{cases} 1 & m-k \text{ even} \\ -j(-1)^m & m-k \text{ odd,} \end{cases} \quad (46)$$

$$S_m = \frac{\sin \frac{\pi}{2} [y-(m+1)]}{y-(m+1)} + (-1)^m \frac{\sin \frac{\pi}{2} [y+(m+1)]}{y+(m+1)}, \quad (47)$$

and $y = \omega\tau_L/\pi = 2f\tau_L$. The second index on F_{mk} has been dropped in Part 1 for the $m=k$ diagonal term. This is plotted in Fig. 5.

For the impedance (44), the matrix elements (5) become

$$M_{mk} = 0.27 \epsilon M B_0 \frac{m\omega}{m+1} \sum_{p=0}^{\infty} S_m(p) S_k(p) \frac{\sigma}{(\omega_p - \omega_r)^2 + \sigma^2} \times$$

$$\times \begin{cases} (-1)^m \sigma & m-k \text{ odd} \\ (\omega_p - \omega_r) & m-k \text{ even} \end{cases} \quad (48)$$

where the summation is over the frequencies (1) or (2). The eigenvalues of the matrix $[m\omega_s + M_{mk}]$ were found by computer for different values of the intensity parameter ϵ and resonator bandwidth $\Delta f = 2\pi\sigma$. The threshold for instability is plotted in Fig. 7.

If only the three central diagonals are retained in the matrix, the results change by less than 5%, and the continued fraction

$$|A| = A_{11} - \frac{A_{12} A_{21}}{A_{22} - \frac{A_{23} A_{32}}{A_{33} - \dots}} \quad (49)$$

can be used for evaluating the determinant.

For small bandwidths, coupled-bunch modes are unstable. The threshold is given by

$$|\Delta\omega_m| = \frac{1}{2} \frac{m}{m+1} S \quad (50)$$

where S is the synchrotron frequency spread between bunch center and bunch edge and $\Delta\omega_m$ is the coherent frequency shift

$$|\Delta\omega_m| = \frac{1}{3} \epsilon MB_0 D \frac{m\omega_s}{m+1} \quad (51)$$

obtained from (7) and (8) with $F_{mm} = \frac{1}{2}$ and $D = \alpha/\sinh \alpha$ where $\alpha = 2\pi\Delta f T/M$ and T is the revolution period. The spread S is approximately

$$S = \frac{2}{3} \omega_s \frac{1+\Gamma^2}{1-\Gamma^2} (hB_0)^2 \quad (52)$$

where $\Gamma = \sin \phi_s$. Thus (50) becomes

$$\epsilon MB_0 \leq \frac{1+\Gamma^2}{1-\Gamma^2} \frac{\sinh \alpha}{\alpha} (hB_0)^2, \quad (53)$$

which is shown in Fig. 7 for stationary buckets ($\Gamma=0$), with every third bucket filled ($h=3M$), and a bunch length $\frac{1}{10}$ of the bucket length ($hB_0 = 0.1$).

4. COASTING-BEAM STABILITY CRITERION

The usual Keil-Schnell criterion³⁾ is

$$\left| \frac{Z}{n} \right| \leq \frac{0.7\pi}{2} \beta^2 \frac{\gamma E_0 |Q|}{e \hat{I}} \left(\frac{\Delta p}{P} \right)_{FWHH}^2. \quad (54)$$

The bunch half-length ϕ_0 in RF radians and half-height Δp_0 are related by

$$\left(\frac{\Delta p}{p}\right)_0 = \frac{\omega_s}{h\omega_0 |\eta|} \phi_0 . \quad (55)$$

For a parabolic distribution with

$$F(\Delta p) = \Delta p_0^2 - \Delta p^2 , \quad (56)$$

$$\left(\frac{\Delta p}{p}\right)_{FWHH}^2 = 2 \left(\frac{\Delta p}{p}\right)_0^2 \quad (57)$$

so

$$\left(\frac{\Delta p}{p}\right)_{FWHH}^2 = \frac{eV_T |\cos \phi_s|}{\pi \gamma E_0 \beta^2 h |\eta|} \phi_0^2 \quad (58)$$

and (54) becomes

$$\left|\frac{Z}{n}\right| \leq \frac{.7}{2} \frac{V_T |\cos \phi_s|}{h \hat{I}} \phi_0^2 \quad (59)$$

where ϕ_0 is related to the bunching factor B_0 by $\phi_0 = \pi h B_0$. The current is

$$\begin{aligned} \hat{I} &= 1.5 I_0 / B_0 && \text{peak current} \\ &= h I_0 && \text{average current} \end{aligned}$$

and (59) reduces to (9) and (10).

1. D. Boussard, CERN Int. Rep., Lab. II/RF/Int. 75-2 (1975), and also these proceedings.
2. S. Hansen and A. Hofmann, ISR Performance Report, CERN Int. Rep. ISR-GS/RF-AH/amb (1976).
3. E. Keil and W. Schnell, CERN Int. Rep. CERN-TH-RF/69-48 (1969).
4. F. Sacherer, Proc. 5th US Particle Accelerator Conf., San Francisco, 1973, IEEE Trans. Nuclear Sci. NS-20, 825 (1973), and also F. Pedersen and F. Sacherer, these proceedings.
5. H.G. Hereward, Proc. 1975 Isabelle Summer Study, Brookhaven BNL 20550, p. 555.
6. F. Sacherer, CERN Int. Rep. CERN/PS/BR 77-6 (1977).
7. A. Renieri, Frascati Rep., LNF-76/11(R) (1976).
8. E. Messerschmid and M. Month, Nuclear Instrum. Methods 136, 1 (1976), and also these proceedings.
9. P. Channell and A. Sessler, Nuclear Instrum. Methods 136, 473 (1976).
10. A. Chao and J. Gareyte, SPEAR-197, PEP-224 (1976), and also these proceedings.
11. H.G. Hereward, Rutherford Lab. Rep. EPIC/MC/70 (1975).