

# Cleaning and Heat-Treatment Effects on Unalloyed Titanium Implant Surfaces

Deepak V. Kilpadi, PhD<sup>1</sup>/Jack E. Lemons, PhD<sup>2</sup>/Jun Liu, PhD<sup>3</sup>/Ganesh N. Raikar, PhD<sup>4</sup>/  
Jeffrey J. Weimer, PhD<sup>5</sup>/Yogesh Vohra, PhD<sup>6</sup>

*This study tested the following hypotheses: (1) acid-cleaned and passivated unalloyed titanium implants have higher surface energies (which are considered desirable for bone implants) than ethanol-cleaned titanium; (2) higher temperatures of heat treatment of unalloyed titanium result in higher surface energies; and (3) these changes can be related to changes in surface composition and roughness. Thus, unalloyed titanium specimens were either acid-cleaned and passivated (CP) or ethanol-cleaned (Et). Each set was then divided into 3 groups and heat-treated for 1 hour at 316°C (600°F), 427°C (800°F), and 538°C (1,000°F), respectively. Surface roughness values for each of these groups were determined using atomic force microscopy, while surface compositions were determined using Auger electron, x-ray photoelectron, and Raman spectroscopic techniques. Surface energies were estimated using a 2-liquid geometric mean technique and correlated with surface roughness, elemental composition, and elemental thickness. The CP surfaces were slightly rougher than the Et specimens, which had greater oxide thickness and hydrocarbon presence. The surface oxides were composed of TiO<sub>2</sub>, Ti<sub>2</sub>O<sub>3</sub>, and possibly titanium peroxide; those heat-treated at 427°C or above were crystalline. The CP specimens had carbonaceous coverage that was of a different composition from that on Et specimens. The CP specimens had significantly higher surface energies, which showed statistically significant correlations with oxide thickness and carbonaceous presence. In conclusion, ethanol cleaning of unalloyed titanium dental implants may not provide optimal surface properties when compared to cleaning with phosphoric acid followed by nitric acid passivation. (INT J ORAL MAXILLOFAC IMPLANTS 2000;15:219–230)*

**Key words:** ethanol, passivation, surface characterization, temperature, titanium

<sup>1</sup>Adjunct Research Assistant Professor, Joint Materials Science PhD Program of The University of Alabama System; and Department of Biomaterials, University of Alabama at Birmingham.

<sup>2</sup>Professor, Joint Materials Science PhD Program of The University of Alabama System; and Department of Biomaterials, University of Alabama at Birmingham.

<sup>3</sup>Researcher, Department of Physics, University of Alabama at Birmingham.

<sup>4</sup>Manager, Surface Analysis and Optical Spectroscopy Laboratory, University of Utah, Salt Lake City, Utah.

<sup>5</sup>Associate Professor, Joint Materials Science PhD Program of The University of Alabama System; and Department of Chemistry and Departments of Chemical and Materials Engineering, University of Alabama at Huntsville.

<sup>6</sup>Professor, Joint Materials Science PhD Program of The University of Alabama System; and Department of Physics, University of Alabama at Birmingham.

**Reprint requests:** Dr D.V. Kilpadi, Department of Biomedical Engineering, University of Alabama at Birmingham, 370 Hoehn, 1075 13th Street South, Birmingham, AL 35294. Fax: (205) 975-4919. E-mail: dkilpadi@uab.edu

The use of metallic implants for dental applications has been increasing, partly because of the possibility of close bone apposition.<sup>1</sup> Increased bone contiguity has been shown to provide characteristics for enhancing long-term implant viability. From a biomaterials perspective, surface roughness, composition, and energy can influence biologic responses and, hence, clinical function.<sup>2,3</sup> For example, osteoblasts have been shown to proliferate on rougher surfaces.<sup>3</sup> Also, surface composition and roughness can affect surface energy. Surfaces with higher surface energies exhibit enhanced wetting behavior, which is thought to result in better interactions with the moieties that are important for osteal responses.

National and international standards on the properties of metallic biomaterials for surgical implants are fairly broad, allowing for several possible procedures prior to implantation—cleaning, passivation, and sterilization—that may include exposure to

**Table 1 Surface Roughness Parameters Examined with Atomic Force Microscopy**

Parameter	Description
Z-range	Distance between the highest and lowest points within a given area
R <sub>q</sub>	Standard deviation of height measurements relative to the mean height within a given area
R <sub>a</sub>	Mean value of the surface relative to the center plane (the center plane is flat and divides the enclosed volume of the image surface into 2 equal parts)
R <sub>max</sub>	Difference in height between the highest and lowest points relative to the mean plane (the mean plane is determined from a first-order least-squares-fit of height data, thereby minimizing variance of image data about this plane)
Surface area difference	Percentage increase of 3-dimensional area relative to 2-dimensional image area (14 μm × 14 μm)

elevated temperatures.<sup>1,4</sup> Previous studies show that the combination of passivation and dry-heat sterilization at 205°C, after cleaning in phosphoric acid, increases surface energy of titanium, while the absence of passivation affects subsequent oxide growth.<sup>5,6</sup> Also, coating techniques such as ion beam sputtering or plasma spraying include heat treatments in the range of about 500°C to 600°C of the coated implant to optimize coating properties.<sup>7</sup> These presurgical procedures can alter the surface characteristics considered critical to biocompatibility. The current study investigated the influence of higher temperatures of heat treatments on the surface energy, roughness, and composition of unalloyed titanium specimens that were either previously acid-cleaned and passivated or ethanol-cleaned.

## MATERIALS AND METHODS

Unalloyed grade 2 titanium was wet-ground using 320- through 600-grit silicon carbide papers. Specimens were then either ethanol-cleaned (Et)—ultrasonically cleaned in 95% ethanol for 10 minutes and allowed to air-dry—or acid-cleaned and passivated (CP)—cleaned in 50% (volume) phosphoric acid for 30 minutes, ultrasonically cleaned in deionized water for 10 minutes, passivated in 30% (volume) nitric acid at room temperature for 20 minutes, ultrasonically cleaned again in deionized water for 10 minutes, and finally air-dried. Each sample

was divided into 3 groups and heated independently in air for 1 hour at temperatures of 316°C (600°F), 427°C (800°F), and 538°C (1,000°F), respectively, and then allowed to cool to room temperature. All specimens were then stored in a desiccator until analyzed.

### Atomic Force Microscopy

Surfaces were examined for microtopographic characteristics with atomic force microscopy (AFM) (Nanoscope III, Digital Instruments, Santa Barbara, CA) using SiN cantilever probes with a constant force of 0.58 N/m and a scan rate of 4 Hz. The tips had a nominal radius of 20 to 40 nm. Roughness was quantified through multiple analyses of 14 × 14 μm<sup>2</sup> area scans (Table 1). Five regions per sample type were examined within a 4-hour period at similar room temperature and humidity. No image processing was done.

### Solid Surface Tension

Values for solid surface tension ( $\gamma_s$ ) were determined using contact angles of drops of ultrapure diiodomethane and distilled water on specimen surfaces that were measured using a goniometer setup (NRL-100, Ramé-Hart, Mountain Lakes, NJ). At least 8 measurements per liquid and surface type were made to provide data for statistical analysis. Surface energy was determined 1 to 4 days after specimen preparation. Previous studies on the influence of storage time showed that time-dependent variance of  $\gamma_s$ , if any, occurred within the first 24 hours of storage; the  $\gamma_s$ s of dry heat-sterilized specimens did not change substantially with dry storage.<sup>8</sup> To minimize effects of alterations caused by the environment at room temperature and humidity, all surfaces were examined within a few hours of each other at room temperature (23°C to 24°C).

The total surface tensions ( $\gamma_t$ ) of the test liquids (distilled water = 72.8 dyne cm<sup>-1</sup> and diiodomethane = 50.8 dyn cm<sup>-1</sup>) were measured using the De Nöuy technique (DCA-312, Cahn Instruments Inc, Cerritos, CA) and were found to be similar to values cited in the literature.<sup>9</sup> The polar ( $\gamma_p$ ) and dispersive ( $\gamma_d$ ) components (water  $\gamma_p$  = 50.3 dyne cm<sup>-1</sup>; water  $\gamma_d$  = 22.5 dyn cm<sup>-1</sup>; diiodomethane  $\gamma_p$  = 2.3 dyne cm<sup>-1</sup>; diiodomethane  $\gamma_d$  = 48.5 dyne cm<sup>-1</sup>) were taken to be the same as values in the literature.<sup>9</sup> The 2-liquid geometric mean equation, recommended for examining high-surface energy surfaces, was used to determine  $\gamma_d$ ,  $\gamma_p$ , and  $\gamma_t$  of the titanium surfaces.<sup>10</sup> Acid-cleaned polytetrafluoroethylene (PTFE) was examined for calibration and as a check of methodology.<sup>9</sup>

### Auger Electron Spectroscopy

Auger electron spectroscopic (AES) analyses were done to determine surface elemental composition of the samples. This was done using a JAMP-30 Auger system (JEOL, Tokyo, Japan) at a base pressure of  $2 \times 10^{-7}$  to  $3 \times 10^{-7}$  Pa. The electron beam current was maintained at about  $3.5 \times 10^{-7}$  A, with an accelerating voltage of 10 kV. All results were obtained at a beam take-off angle of 30 degrees. A modulation potential of 5 V peak-to-peak was used to obtain the data in the differentiated form.

Survey scans (0 to 2,000 eV) were taken both prior to and after depth profiling. Surface layers were sputtered away in 1-second cycles, using a 3 kV, 30 mA argon ion beam at a pressure of 7 mPa. The difference between maximum and minimum intensity of chosen peaks was plotted for after each sputtering cycle. The sputter rate was calibrated using a 1,000 Å Ta<sub>2</sub>O<sub>5</sub> oxide layer on a Ta substrate. Oxide depth was estimated by measuring the number of cycles for the oxygen peak to reach half the maximum concentration.<sup>11</sup> Depths for other elements were determined by the number of cycles taken for the concentration to drop to half the difference between maximum and minimum values. Five spots per surface type were examined.

### X-ray Photoelectron Spectroscopy

X-ray photoelectron spectroscopy (XPS) was used to elicit surface elemental and chemical information. The XPS analyses (Perkin-Elmer ESCA 5400, Norwalk, CT) were conducted at a take-off angle of 45 degrees with a base main chamber pressure of less than  $7 \times 10^{-8}$  Pa. The source was MgK- $\alpha$  radiation at 15 kV and 300 W. Survey scans were done at a pass energy of 89.54 eV and a range of 0 to 1,100 eV. Atomic concentrations were determined from subsequent multiplex spectral scans at a pass energy of 17.9 eV. Two regions per surface type were examined, and quantitative data were obtained from one of these regions. High-resolution scans at a pass energy of 8.95 eV were used to examine elements with an atomic percentage greater than 3%; peak fitting for the C 1s, O 1s, and Ti 2p peaks was done to determine peak separations and full-width half-maximum (FWHM) values, using software on the XPS system.

### Raman Spectroscopy

Raman spectroscopy was used to obtain surface chemical and structural information. Replicate specimens were examined using a micro-Raman spectroscopy system (Dilor, Lille, France). A tunable argon laser (Coherent Innova 70, Santa Clara, CA) with a wavelength of 514.6 nm was used. Two spots

per surface type were examined at a laser power of 20 mW with a collection time of 200 seconds.

### Statistical Procedures

Two-way analysis of variance was used to determine whether effects of surface treatment, temperature of heat treatment, and interaction between surface treatment and temperature were present (interaction alludes to the dependence of the effect of one factor on the other). If differences were present, means were ranked using the Newman-Keuls technique. When comparing surface energy data, 2-way analysis of variance (ANOVA) was done using no replication (ie, only the means for each of the 6 samples were used), unlike other 2-way ANOVA comparisons, where all of the data were used. Differences and ranking among the surface energy data were determined using the Bonferroni *t* test.

Correlation coefficients were used to relate surface roughness, composition, and elemental depths to surface energy. The coefficients were initially tested for significance (ie, whether they were different from 0) and then compared using the Fisher *z*-test.

## RESULTS AND DISCUSSION

### Atomic Force Microscopy

Roughness values for the surfaces are given in Table 2. The temperature of heat treatment did not alter surface roughness in either CP or Et specimens. However, CP specimens had higher  $R_q$  values when compared to the Et samples ( $P = .03$ ). These findings support previous findings where acid-cleaned, passivated, and dry heat-sterilized specimens were rougher than those that were not passivated.<sup>6</sup> With more specimens, it is possible that *Z*-range ( $P = .08$ ) and  $R_a$  values ( $P = .06$ ) also may have been significantly higher for CP specimens. No differences were noted for  $R_{max}$  and surface area difference parameters.

Dissimilar surface profiles can have the same roughness parameter value.<sup>12</sup> Thus, a number of roughness parameters were examined in this study. The *Z*-range parameter, and to a slightly lesser extent,  $R_{max}$ , are sensitive to high peaks and deep valleys. The  $R_a$  and  $R_q$  parameters measure average deviation from a reference plane. The  $R_q$  parameter is more sensitive than  $R_a$  to occasional peaks or valleys and tends to be greater than the corresponding  $R_a$  values for a given surface. This was consistent in the present study: *Z*-range >  $R_q$  >  $R_a$  for all surfaces.

Increased surface roughness has been associated with greater osteoblastic activity.<sup>2</sup> Although the critical level of difference of roughness magnitudes

**Table 2 Surface Roughness**

Parameter	Temperature of heat treatment						2-way ANOVA <i>P</i> values		
	316°C		428°C		538°C		CP vs Et	Temperature effect	Interaction
	CP	Et	CP	Et	CP	Et			
Z-range (nm)	880 ± 10	770 ± 10	850 ± 10	660 ± 10	850 ± 10	770 ± 10	.08	.68	.79
R <sub>q</sub> (nm)	180 ± 30	130 ± 20	160 ± 30	110 ± 10	160 ± 30	130 ± 10	.03	.59	.94
R <sub>a</sub> (nm)	140 ± 20	110 ± 20	120 ± 20	90 ± 10	130 ± 30	110 ± 10	.06	.49	.95
R <sub>max</sub> (nm)	870 ± 70	760 ± 100	790 ± 50	640 ± 60	830 ± 130	760 ± 70	.12	.47	.88
Surface area difference (%)	4.1 ± 0.5	5.1 ± 0.9	4.3 ± 0.3	2.7 ± 0.2	4.5 ± 1.0	4.9 ± 0.7	.92	.15	.17

CP = cleaned in phosphoric acid and passivated in nitric acid; Et = cleaned in ethanol.

**Table 3 Surface Energy Estimation**

Samples	Temperature (°C)	Solid surface tension, dyn/cm		
		γ <sub>p</sub>	γ <sub>d</sub>	γ <sub>t</sub>
CP samples	316	22.9 ± 0.2	23.6 ± 0.2	46.5 ± 0.3
	427	26.8 ± 0.2	28.8 ± 0.6	55.6 ± 0.6
	538	26.6 ± 0.1	24.3 ± 0.1	50.9 ± 0.1
Et samples	316	12.3 ± 0.2	28.2 ± 0.3	40.5 ± 0.4
	427	18.9 ± 0.1	24.7 ± 0.1	43.6 ± 0.2
	538	21.1 ± 0.2	23.3 ± 0.2	44.4 ± 0.2
<i>P</i> , CP versus Et		.03	.95	< .05
<i>P</i> , temperature effects		.13	.68	.20

CP = cleaned in phosphoric acid and passivated in nitric acid; Et = cleaned in ethanol;

γ<sub>p</sub> = polar solid surface tension; γ<sub>d</sub> = dispersive solid surface tension; γ<sub>t</sub> = total solid surface tension.

that influence biologic response has not as yet been established, cells tend to respond most actively to structures that approach their size.<sup>13</sup> The scan lengths used in this study, along with the resolution afforded by AFM, allowed for the study of surface roughness because of structures that were of the same order of magnitude as cells.

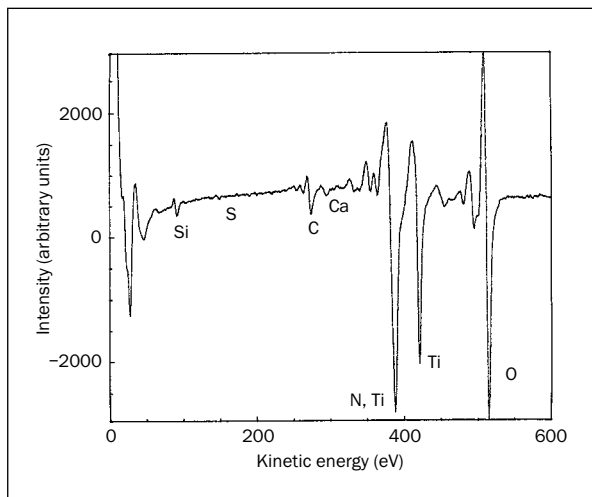
### Solid Surface Tension

Table 3 shows the γ<sub>s</sub> for the sample surfaces. Although estimation of surface energy can be affected by surface roughness,<sup>14,15</sup> no statistically significant correlations between surface roughness parameters and surface energy were detected in this study. Therefore, surface energies were not corrected for surface roughness.

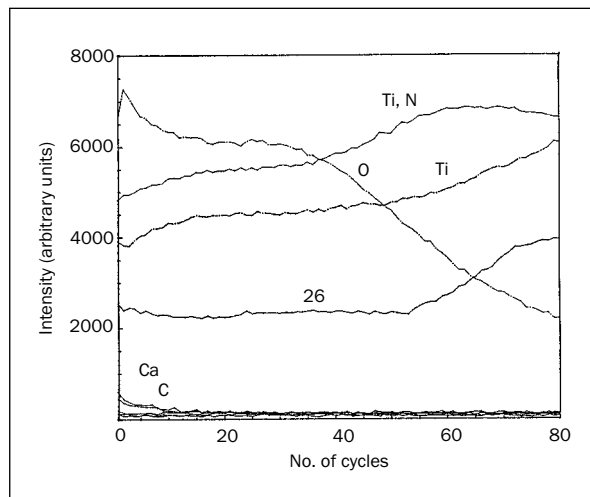
Dispersive solid surface tension was not affected by temperature or surface treatment. Grain structure and mechanical strain, which can be altered with exposure to elevated temperature, are thought not to affect the dispersive component of surface energy.<sup>16</sup> The CP specimens had consistently higher γ<sub>p</sub>, and hence γ<sub>t</sub> (the sum of γ<sub>p</sub> and γ<sub>d</sub>), values than the corresponding Et specimens. In fact, even the

CP specimens with the lowest γ<sub>p</sub> had a value greater than the Et sample with the largest polar component. Although effects of exposures at various temperatures were not statistically significant, possibly because of similar γ<sub>p</sub> values for CP specimens heat-treated at 538°C (538CP) and 427°C (427CP), higher temperatures resulted in higher mean γ<sub>p</sub> for both groups of surface treatment (although there appeared to be an upper limit, as shown by the comparable 427CP and 538CP values). Similarly, CP surfaces had higher total solid surface tension values (γ<sub>t</sub>) than Et samples. These findings corroborated results from a previous study on cleaned, passivated, and dry heat-sterilized specimens where γ<sub>p</sub> was correlated with total solid surface tension.<sup>6</sup>

The surface energy parameter has been shown to be a useful indicator for predicting biologic response.<sup>2,3</sup> However, surface energies are not unique; that is, different surface compositions may result in a similar surface energy value. In addition to modulating biologic response indirectly by altering surface wettability, surface composition can affect biologic response directly through specific interactions with the biologic milieu.



**Fig 1** Representative pre-sputter Auger spectrum (538CP).



**Fig 2** Representative depth profile of 538CP specimens. The profile marked 26 corresponds to a minor titanium peak at about 26 eV.

### Auger Electron Spectroscopy

Surface composition analysis using Auger spectroscopy showed the presence of oxygen, titanium, and carbon (Fig 1). There were also trace levels of silicon, sulfur, calcium, and phosphorus on some of the specimens. Removal of adsorbed oxygen, water, and oxygen-containing carbonaceous species in the initial stages of vacuum exposure and sputtering caused the oxygen profile to decrease, as seen in Fig 2. It reached a plateau, indicating the presence of a subsurface zone of stoichiometric oxide. Further sputtering lead to a gradual drop in the oxygen intensity in the profile. This probably indicates that the oxide boundary is not abrupt, unlike the  $Ta_2O_5$ -Ta boundary (recall  $Ta_2O_5$  was used to estimate the sputtering rate). Differences in the sputtering rates of the oxides and metallic titanium, along with crater effects, may have contributed to the broadening of the depth profile. Other possible contributions may have been the result of differences in the readsorption of sputtered moieties, ionic implantation and atomic mixing, and shadowing related to asperities/surface roughness.<sup>17</sup>

Depth profiling results are provided in Table 4. Oxide thickness increased, as expected, with temperature of exposure for both CP and Et specimens. Two-way ANOVA confirmed that no interaction effects were present and that the oxide thicknesses measured using the half-maximum method were affected by temperature as well as surface treatment. The Et samples had thicker oxide layers than the CP ones. This agrees with previous studies in which unpassivated but dry heat-sterilized (at 205°C) sam-

ples had smoother and thicker oxide layers than those that had also undergone the passivation process.<sup>5,6</sup>

Specimens that were heat-treated (both CP and Et) at 316°C did not show a visual color change; that is, the surface before and after heat treatment retained the original metallic gray color. The specimens heated to 427°C had a uniform golden color, and surfaces that were heat-treated at 538°C were blue, with areas of varying shades of purple and some white. These colors are a result of the interference of incident white light and can be related to the relative thickness of crystalline surface oxide layers.<sup>18</sup> A previous study by Fukuzuka et al using ellipsometry data indicated that the surface oxide layer on titanium was colorless when its thickness was below 100 Å, yellow between 100 and 250 Å, blue between 250 and 700 Å, blue-green between 700 and 1,700 Å, and white when the oxide was thicker than 1,700 Å.<sup>18</sup> The variation in color, from blue to white, of specimens heated at 538°C was probably the result of differing local oxide thickness that was attributed to varying heating/cooling rates, which are thought to be dependent on local thermal gradients. Also, a previous corrosion study had shown that titanium specimens that were heat-treated at 538°C were more likely to corrode than those exposed to lower temperatures.<sup>19</sup> It is possible that microcracks at the oxide-metal interface, caused by stresses from differential thermal expansion, may have facilitated the increase in the equilibrium corrosion potential ( $E_{corr}$ ). These microcracks may also have facilitated differential oxide growth, resulting in a surface oxide layer of varying thickness and, hence, varying shades

**Table 4 Auger Depth Profile Results**

Element	Temperature of heat treatment						2-way ANOVA <i>P</i> values		
	316°C		427°C		538°C		Temperature effects	CP vs Et	Interaction
	CP	Et	CP	Et	CP	Et			
Oxygen	69.4 ± 7.8	109.8 ± 22.1	93.2 ± 11.6	172.6 ± 7.3	116.8 ± 17.2	231.4 ± 56.6	< .01	< .01	> .1
Oxygen plateau	17.0 ± 17.0	69.7 ± 25.5	42.5 ± 6.8	98.6 ± 11.9	66.3 ± 15.3	68.0 ± 34	.34	.02	.42
Carbon	7.7 ± 2.2	16.8 ± 8.7	4.6 ± 0.5	9.2 ± 1.9	5.8 ± 1.9	9.0 ± 1.2	.33	.03	.93

Values are shown as mean ± standard error in Å.

**Table 5 Auger Elemental Thickness Profile and Surface Energy**

Series	Surface tension type	Correlation coefficient ( <i>r</i> )	
		Oxide thickness	Carbon
CP only	$\gamma_d$	—	—
	$\gamma_p$	p	—
	$\gamma_t$	—	n
Et only	$\gamma_d$	n	—
	$\gamma_p$	p	—
	$\gamma_t$	p	—
All	$\gamma_d$	—	—
	$\gamma_p$	—	n
	$\gamma_t$	—	n

CP = cleaned in phosphoric acid and passivated in nitric acid; Et = cleaned in ethanol;  $\gamma_d$  = dispersive solid surface tension;  $\gamma_p$  = polar solid surface tension;  $\gamma_t$  = total solid surface tension; p = positive correlation; n = negative correlation.

of color. As it was not possible to isolate regions of different colors using the black-and-white video output that is inherent with electron microscopic imaging, multiple random sites were examined on a given surface. It was not possible to discern nano- or microcracks, if any, that may have propagated and manifested at the specimen surfaces with either AFM or SEM because of the relative roughness of all the surfaces and the relatively long AFM scan lengths used in this study.

Similarities in color (indicative of similar oxide thicknesses) of CP and Et specimens treated at similar temperatures could have been attributed to the thickness range (about 150 to about 450 Å) that can result in a similar reflected light interference (Table 4).<sup>18</sup> Also, relative differences in surface roughness and composition may have altered relative sputtering rates and contributed to differences in estimated oxide thickness.

There was a slight variance from the results presented by Fukuzuka in that these particular colors

and the measured oxide thicknesses did not fully agree with the Fukuzuka model. This difference may be the result of the Auger depth profile being calibrated using standard tantalum oxide specimens, which may not have fully represented the actual sputtering rate of the titanium surfaces. However, while quantitative comparisons were not possible with other studies per se, the trends were comparable. The Newman-Keuls test for multiple comparisons showed that 538Et and 427Et had the thickest oxide layers. Despite obvious thickness differences between the oxide layers of these surfaces, as substantiated by color differences, the large standard error for 538Et prevented determination of any statistical difference. The magnitude of this variation was in agreement with the different color shadings on the surface. No other statistically significant differences in depth profiles were noted, although color differences were clearly present. Although this study illustrated limitations in discerning oxide thickness differences via depth profiling, statistically significant differences, when present, corresponded well with color/thickness correlations.

The thickness of the carbonaceous layers along the surface was not affected by the temperature of heat treatment. However, the CP surfaces had a thinner carbon layer, which reflects the higher  $\gamma_p$  values. Calcium, silicon, and sulfur thicknesses were minimal—these moieties were sputtered off within the first 2 sputtering cycles (about 3.4 Å). Unlike calcium and silicon, sulfur was present only on the Et surfaces; sulfur may have contributed to the lower surface energy values of Et specimens and may have contributed to the thickening of the surface oxide layer, broadening of the depth profile, or both.

Correlation coefficients, when significantly different from zero, were of similar magnitudes. Thus, only signs, ie, positive, negative, or no correlations, were examined, using CP only, Et only, and all specimens (Table 5). Although some significant correlations present in one of these groups were not

statistically significant with another, the signs were consistent when correlation coefficients were statistically significant for more than 1 group, eg,  $\gamma_p$  increased with oxide thickness for both CP-only and Et-only groups. Differences between the groups may be attributed to the difference in the number of specimens and the dependency of the correlation analysis on the range of the data examined (recall that the lowest of the  $\gamma_p$  values associated with the CP surface was higher than the largest value associated with the Et surfaces).

Although statistical correlation indicates association and not necessarily causation, the results suggest that polar forces at the specimen surface were dependent on the presence of the polar oxide present and any other polar moieties (such as adsorbed water) (see XPS section). Increased oxide thickness increased  $\gamma_p$ , but only to a point. Beyond a critical thickness,  $\gamma_p$  did not increase— $\gamma_p$  values for 538CP and 427CP were similar. Polar forces are characteristic of moieties with fixed dipole moments and are inversely proportional to the fourth power of the distance—thus, polar forces act over a limited distance.<sup>20,21</sup> Hydrocarbons are ubiquitous; hence, despite the most stringent of cleaning procedures, carbonaceous layers are always present on surfaces, although the amount and composition of these layers are dependent on the specific cleaning protocols. Carbonaceous overlayers consisted predominantly of non-polar components (see XPS section below) that masked the polar forces from the underlying oxide layer. Non-polar (dispersive) forces tend to be more localized—they are inversely proportional to the seventh power of the distance from the source and are effective over a distance more limited than for polar forces.<sup>20,21</sup>

### X-ray Photoelectron Spectroscopy

The survey and utility scans showed a comparable presence of titanium ( $19.8 \pm 0.3\%$ ) and sodium ( $4.2 \pm 1.0\%$ ) on all CP and Et surfaces. No temperature effects were seen on the relative percentages for any of the detected elements. Trace amounts of chlorine, nitrogen, calcium, phosphorus, and silicon were also observed. Differences in elements detected using Auger spectroscopy may be the result of different mean free paths of the respective characteristic electrons.<sup>11</sup>

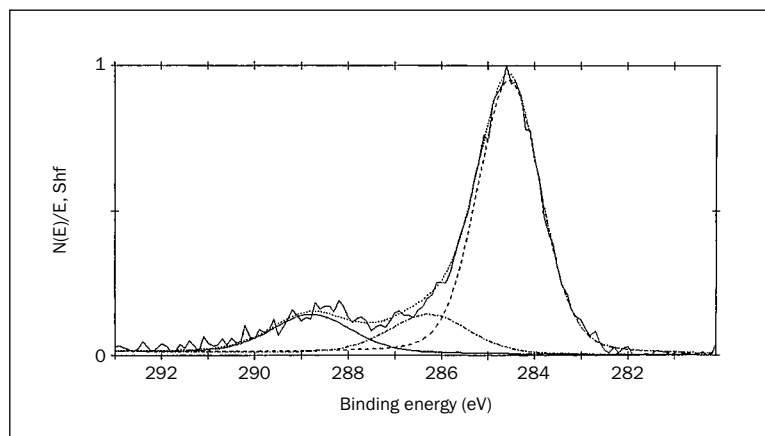
The Et specimens showed a higher carbon and a lower oxygen content (Et: carbon =  $25.4 \pm 1.7\%$ ; oxygen =  $51.0 \pm 0.9\%$ ; CP: carbon =  $19.0 \pm 1.0\%$ ; oxygen =  $54.4 \pm 0.4\%$ ). This corroborates a previous study in which surfaces treated with ethanol were found to have a slightly, but statistically significantly, higher carbon content than untreated surfaces.<sup>22</sup> The amount of carbon in the samples from the cur-

rent study was significantly lower than any of the surfaces examined previously, while the oxygen concentrations were significantly higher.<sup>5</sup> The titanium/oxygen ratios were  $> 2.0$  for samples in this study and  $> 2.0$  for samples in the previous study. This could have been caused by several factors, as follows: (1) the increased temperatures used in this study may have depleted the surface carbon layer; or (2) the thinner oxide layers in the previous study resulted in the spectra including a contribution from the underlying metallic titanium substrate, thereby increasing apparent titanium concentration and, as a consequence, decreased apparent oxygen content.

Because of the limited number of specimens, correlation coefficients determined using data from CP specimens only or Et specimens only were not significantly different from 0. When data from both groups were used,  $\gamma_p$  decreased with increasing surface concentration of carbon (ie, correlated negatively), as was the case with the combined Auger carbon depth profiles. The surface concentration of oxygen correlated positively with  $\gamma_t$ , ie,  $\gamma_t$  increased with increasing oxygen presence at the surface. This was consistent with Auger oxide thickness measurements, which correlated positively with  $\gamma_p$  and  $\gamma_t$  when only Et data were considered. Differences from Auger correlation analyses can be attributed to differences in sensitivity to specific elements, electron escape depths, possible sputtering artifacts, and characteristics used—that is, Auger correlations dealt with depth of elemental presence only and did not specifically consider concentration.

A sample high-resolution spectrum for the carbon 1s region is shown in Fig 3. Peak fitting showed 3 component peaks; there were no statistically significant differences in the corresponding peak positions between CP and Et surfaces (Table 6). The relative percentages of the peaks associated with the carbon subspecies were different for CP and Et surfaces. Peaks at  $\sim 289$  eV and  $\sim 286$  eV are associated with C=O (carbonyl) and C-O bonds, respectively. Peaks at  $\sim 285$  eV are characteristic of aliphatic C-C, C-H bonds.<sup>11,23</sup> The amount of aliphatic C-C and C-H was the same for the Et and CP specimens. The CP specimens had a significantly greater amount of C-O species; this may be one reason for the higher  $\gamma_p$  values for the CP samples. Also, the shape of the  $\sim 286$  eV peak for CP surfaces was broader, as determined by the FWHM parameter. Although a high FWHM can be indicative of lack of long-range order, the specific implication in this case is not clear.

The oxygen 1s envelope was fitted by 2 constitutive peaks; a representative plot is shown in Fig 4. All the samples had comparable sub-peak compositions: the 531.4 eV peak constituted  $17 \pm 1\%$  and the 529.6



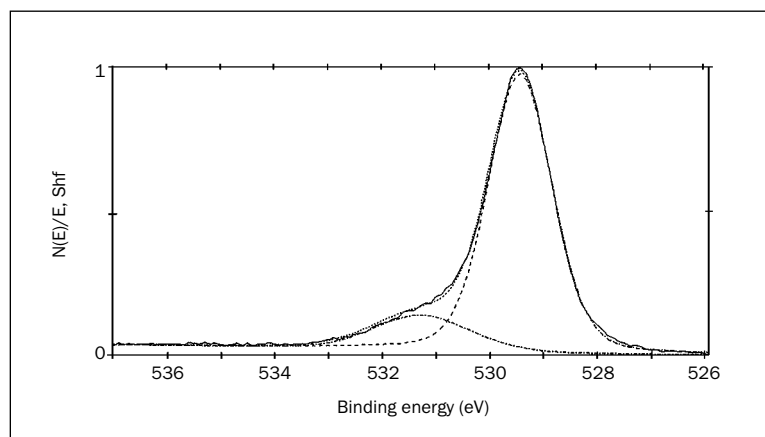
**Fig 3** Deconvolution of XPS carbon envelope for 538CP specimens.

**Table 6** Deconvoluted Carbon 1s Envelopes

Specimen	Peak I (eV)	FWHM		Peak II (eV)	FWHM		Peak III (eV)	FWHM	
		eV	%		eV	%		eV	%
CP	288.8 ± 0.2	2.0 ± 0.0	13 ± 1	286.3 ± 0.3	2.0 ± 0.0*	13 ± 1*	284.6 ± 0.0	1.6 ± 0.1	74 ± 0
Et	288.4 ± 0.1	2.3 ± 0.2	16 ± 2	286.3 ± 0.0	1.4 ± 0.0*	8 ± 1*	284.6 ± 0.0	1.6 ± 0.0	75 ± 1

\*Significant difference between mean CP and mean Et.

FWHM = full-width half-maximum; CP = cleaned in phosphoric acid and passivated in nitric acid; Et = cleaned in ethanol.

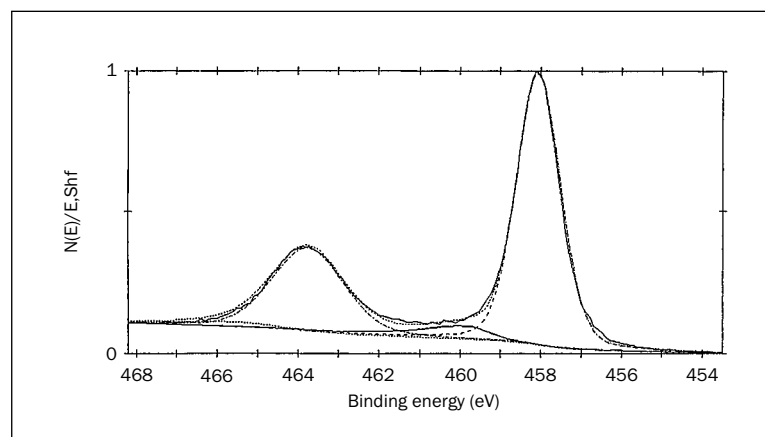


**Fig 4** Deconvolution of XPS oxygen envelope of 538CP specimens.

eV made up  $83 \pm 1\%$  of the oxygen envelope. The peak at the higher binding energy is characteristic of physisorbed water and the other of titanium dioxide.<sup>24–29</sup> There was no indication of peaks characteristic of chemisorbed OH peak at  $\sim 533$  eV.<sup>26</sup> This was in contrast to specimens, examined in a previous study, that were not heat-treated or were heat-treated at a lower temperature than those studied in this

investigation.<sup>5</sup> Desorption of undissociated chemisorbed water occurs at 380 K ( $107^\circ\text{C}/225^\circ\text{F}$ ) and that of dissociated chemisorbed water occurs at 520 K ( $247^\circ\text{C}/447^\circ\text{F}$ ), temperatures that were encountered in this study.<sup>30</sup> However, on cooling to room temperature, the environmental humidity may have resulted in readsorption of water. There are some concerns, however, that the ultra-high vacuum





**Fig 5** Deconvolution of XPS titanium doublet ( $Ti2p_{3/2}$  and  $Ti2p_{1/2}$ ) for 538CP specimens.

associated with XPS may rid the surface of physisorbed water. The oxygen peak at  $\sim 531.4$  eV may also have been caused by carbonaceous material containing oxygen (C-OH and C=O)—corroborating the information from the high resolution carbon peaks or related to titanium sub-oxides.<sup>11,25</sup> All of the surfaces had similar oxide compositions.

High-resolution spectra of titanium peaks showed that the doublet peaks had a binding energy difference range of 5.7 to 5.9, further corroborating the presence of titanium dioxide (Fig 5).<sup>31</sup> There were no differences among the specimens. Also, peak fitting of the Ti  $2p_{3/2}$  peak revealed only the peak at  $\sim 458.5$  eV, which is characteristic of titanium oxide, unlike a previous study of CP specimens incubated at temperatures of  $205^{\circ}\text{C}$  or less, which detected the presence of  $Ti_2O_3$  ( $\sim 457$  eV), and titanium metal ( $\sim 454$  eV).<sup>32</sup> This indicates that the oxide thicknesses of all the samples examined in this study were greater than the escape depth of photoelectrons from the underlying titanium substrate (and also from the intermediate  $Ti_2O_3$  layer—see Raman spectroscopy section below).

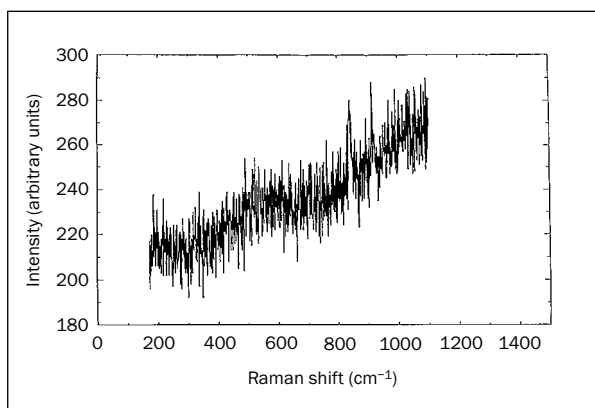
### Raman Spectroscopy

Raman scattering was observed for all of the surfaces heat-treated at  $427^{\circ}\text{C}$  and  $538^{\circ}\text{C}$ . Some of the specimens that were heat-treated at  $316^{\circ}\text{C}$  had broad peaks around 600, 840, and  $914\text{ cm}^{-1}$ , as shown in Fig 6a. Absence of peaks at some sites suggested that surface oxide layer thickness was inadequate in certain areas for Raman signal detection. Raman spectroscopy examines a much greater depth than either XPS or AES, and the spectrum can be dominated by non-Raman signals from the metallic substrate.

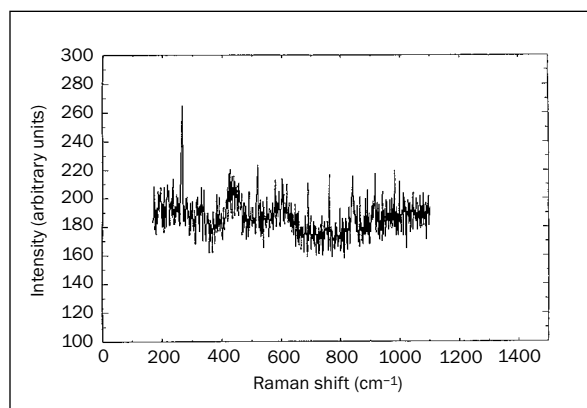
The CP and Et surfaces heated to  $427^{\circ}\text{C}$  and  $538^{\circ}\text{C}$  were primarily rutile, with strong peaks at  $\sim 440\text{ cm}^{-1}$  and  $\sim 600\text{ cm}^{-1}$  and a smaller peak at  $\sim 840\text{ cm}^{-1}$  (Figs 6b and 6c).<sup>33</sup> Weaker peaks at  $\sim 250\text{ cm}^{-1}$  and  $\sim 330\text{ cm}^{-1}$  were attributed to  $Ti_2O_3$ ; the literature cites values of  $\sim 254$  to  $271\text{ cm}^{-1}$  and  $\sim 332$  to  $347\text{ cm}^{-1}$  for these peaks.<sup>34-37</sup> These peaks do not indicate the presence of anatase because of the absence of characteristic Raman peaks at  $\sim 400\text{ cm}^{-1}$  and  $\sim 515\text{ cm}^{-1}$  for the 2 dominant anatase Raman peaks in the backscattering mode used in the current study.<sup>38,39</sup> Detector orientation was critical, as peaks at  $\sim 144\text{ cm}^{-1}$ ,  $\sim 640\text{ cm}^{-1}$ , and  $200\text{ cm}^{-1}$  are the dominant anatase peaks for perpendicular instrument detection geometries.<sup>37-39</sup> Peaks were not observed at these positions. Because XPS analysis is extremely surface-sensitive and did not detect any  $Ti_2O_3$ , the  $Ti_2O_3$  detected with Raman spectroscopy was probably present below an outer titanium dioxide layer.

Titanium peroxide may have been present on all of the specimens, because all of the specimens showed a relatively prominent characteristic peak at  $\sim 914\text{ cm}^{-1}$ .<sup>40</sup> The supporting characteristic peak at  $270\text{ cm}^{-1}$  may also have contributed to the  $\sim 250\text{ cm}^{-1}$  peak observed on all specimens. A peak at  $\sim 525\text{ cm}^{-1}$ , also characteristic of titanium peroxide, was observed with the CP specimens that were heat-treated for 30 minutes at  $427^{\circ}\text{C}$ . This peak was not observed on the other specimens because it may have overlapped with one of the rutile peaks (the one at  $\sim 600\text{ cm}^{-1}$ ).

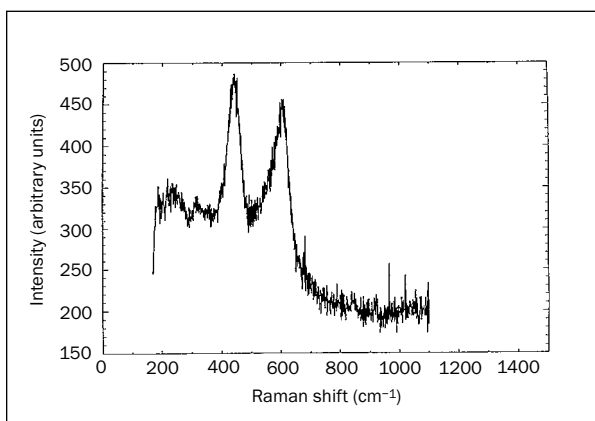
For specimens heat-treated at  $427^{\circ}\text{C}$  ( $800^{\circ}\text{F}$ ) and  $538^{\circ}\text{C}$  ( $1,000^{\circ}\text{F}$ ), the FWHM of the all peaks, except for at  $\sim 250\text{ cm}^{-1}$ , were less than  $80\text{ cm}^{-1}$ .



**Fig 6a** Representative Raman spectrum for surfaces heat-treated at 316°C.



**Fig 6b** Representative Raman spectrum for surfaces heat-treated at 427°C.



**Fig 6c** Representative Raman spectrum for surfaces heat-treated at 538°C.

This suggested that the titanium dioxide and  $\text{Ti}_2\text{O}_3$  were both crystalline. Other investigators have ascribed absence of long-range order in titanium dioxide to FWHMs of  $\sim 180\text{ cm}^{-1}$  for the  $\sim 440\text{ cm}^{-1}$  peak and  $\sim 120\text{ cm}^{-1}$  for the  $\sim 600\text{ cm}^{-1}$  peak.<sup>41</sup> The width of the  $\sim 250\text{ cm}^{-1}$  peak could have been the result of an overlap of the rutile peak at  $\sim 240\text{ cm}^{-1}$  and the  $\text{Ti}_2\text{O}_3$  or titanium peroxide peak at  $\sim 270\text{ cm}^{-1}$ .<sup>33,40</sup>

The characteristic peaks for rutile ( $\sim 440$  and  $\sim 600\text{ cm}^{-1}$ ) were further examined for variations in specific peak positions. Analysis of variance, as well as correlation coefficients, showed that none of the variables (temperature or surface treatment) affected peak positions. Full-width half-maximums of the  $\sim 600\text{ cm}^{-1}$  peak, too, were not affected by

these variables ( $65 \pm 6\text{ cm}^{-1}$  at  $427^\circ\text{C}$  and  $59 \pm 6\text{ cm}^{-1}$  at  $538^\circ\text{C}$ ). However, the FWHMs of the  $\sim 440\text{ cm}^{-1}$  peak, although not affected by surface treatment, decreased with increased heat-treatment temperature, from  $68 \pm 2\text{ cm}^{-1}$  at  $427^\circ\text{C}$  to  $54 \pm 2\text{ cm}^{-1}$  at  $538^\circ\text{C}$ . The FWHM is an indicator of grain size and structural defects; as calibration specific to the structural aspects of titanium oxides was not done, absolute grain sizes could not be determined. Heat treatment at  $538^\circ\text{C}$  would result in grains that were significantly larger than those resulting from heat treatment at  $427^\circ\text{C}$ .<sup>41</sup> Although increased temperatures resulted in higher surface energy, the concomitant increase in oxide crystallinity or oxide grain size may affect corrosion resistance.<sup>19</sup> Corrosion studies are currently underway to examine and optimize heat treatment protocols.

The results of this study indicate that there can be significant differences in surface energy based on the surface cleaning process—up to  $10\text{ dyn/cm}$ —depending on whether a titanium surface was ethanol-cleaned or acid-cleaned and that these changes can be related to surface compositional changes. Clinicians sometimes resort to using ethanol as a quick sterilization process; this study shows that if so, significant implant surface changes may occur as a result. Previous studies have shown that in general for bone/dental implant success, higher surface energy surfaces are preferred.<sup>42,43</sup> For example, fibronectin reorganization and integrin binding of cells are associated with higher energy surfaces.<sup>44</sup> The specific in vivo outcomes for the processes examined in this investigation remain to be studied.

## SUMMARY AND CONCLUSIONS

Implant-grade titanium specimens that were cleaned and passivated were rougher than the ethanol-cleaned surfaces. Analyses of solid surface tensions showed similar trends for polar and total solid surface tension values, which were significantly greater for the cleaned and passivated specimens; dispersive solid surface tension was not affected by the cleaning procedure or the temperature of heat treatment.

Spectroscopic analyses suggested that all of the surfaces had an outer oxide layer of TiO<sub>2</sub>, an inner layer of Ti<sub>2</sub>O<sub>3</sub>, and possibly titanium peroxide. Variations of solid surface tension were related to differences in oxide thickness and crystallinity and in the area, thickness, and composition of carbonaceous presence within the surface zone. Although oxide thickness increased, as expected, with increasing heat treatment temperature, the cleaned and passivated samples had a thinner oxide and carbon depth measurement than the ethanol-cleaned specimens. The ethanol-cleaned specimens also had higher overall surface carbon concentrations. The carbonaceous layers on ethanol-cleaned specimens consisted of a chemical composition different from those on cleaned and passivated specimens. Thus, the various surface and heat treatments altered surface characteristics—surface compositions, surface roughness, and surface energies—and may have implications in clinical application. Studies are currently being conducted to further examine the effect of these differences on biologic interactions.

## ACKNOWLEDGMENTS

This investigation was supported by NIDR Grant No. DE-08917. The AFM instrumentation was supported under Alabama EPSCOR Phase II. We thank Dr Edwin Bradley for his advice with the statistics; Mr Mark Koopman, Ms Cheri Moss, and Dr Robin Griffin for their help in the Auger laboratory; Dr Linda Lucas for the use of the Cahn dynamic contact angle analyzer; Mr Paul Lemons and Ms Krista Speer for their assistance with the logistics; and Dr John C. Gregory for his help.

## REFERENCES

- Albrektsson T, Jacobsson M. Bone-metal interface in osseointegration. *J Prosthet Dent* 1987;57:597–607.
- Walivaara B, Aronsson B-O, Rodahl M, Lausmaa J, Tengvall P. Titanium with different oxides: *In vitro* studies of protein adsorption and contact activation. *Biomaterials* 1994;15(10):827–834.
- Den Braber ET, de Ruijter JE, Smits HTJ, Ginsel LA, von Recum AF, Jansen JA. Effect of parallel surface microgrooves and surface energy on cell growth. *J Biomed Mater Res* 1995;29:511–518.
- ASTM. F86-91: Standard recommended practice for the preparation and marking of surgical implants. Volume 13, Section 13.01. Philadelphia: American Society for Testing and Biomaterials, 1995.
- Kilpadi DV, Raikar GN, Liu J, Lemons JE, Vohra Y, Gregory JC. Effect of surface treatment on unalloyed titanium implants: Spectroscopic analyses. *J Biomed Mater Res* 1998;40(4):646–659.
- Kilpadi DV, Weimer JJ, Lemons JE. Effect of passivation and dry heat-sterilization surface energy and topography of unalloyed titanium implants. *Colloids and Surfaces A: Physicochemical and Engineering Aspects* 1998;135:89–101.
- Ong JL, Lucas LC. Post-deposition heat treatments for ion beam sputter-deposited calcium phosphate coatings. *Biomaterials* 1994;15(5):337–341.
- Kilpadi DV, Lemons JE. The effect of time on surface energy of unalloyed titanium implants. In: *Proceedings of the Ninth Annual Alabama Materials Research Conference*. Birmingham, AL: Alabama Materials Research Society, 1995.
- Dalal EN. Calculation of solid surface tensions. *Langmuir* 1987;3:109–1015.
- Wu S. *Polymer Interface and Adhesion*. New York: Marcel Dekker, 1982.
- Lausmaa J, Kawemo B, Mattsson H. Surface spectroscopic characterization of titanium implant materials. *Appl Surf Sci* 1990;44:133–146.
- Arnell RD, Davies PB, Halling J, Whomes TL. *Tribology: Principles and Design Applications*. London: MacMillan, 1991.
- Black J. *Biological Performance of Materials. Fundamentals of Biocompatibility*, ed 2. New York: Marcel Dekker, 1992.
- Wenzel RN. Resistance of solid surfaces to wetting by water. *Ind Eng Chem* 1936;28:988–994.
- Kilpadi DV, Lemons JE. Surface energy characterization of unalloyed titanium implants. *J Biomed Mater Res* 1994;28:1419–1425.
- Fowkes FM. Determination of interfacial tensions, contact angles, and dispersion forces in surfaces by assuming additivity of intermolecular interactions in surface. *J Phys Chem* 1962;66:382.
- Hofmann S. Depth profiling. In: Briggs D, Seah MP (eds). *Practical Surface Analysis by Auger and X-ray Photoelectron Spectroscopy*. New York: John Wiley & Sons Inc, 1983: 141–179.
- Fukuzuka T, Shimogori K, Hiroshi S, Kamikubo F. On the beneficial effect of the titanium oxide film formed by thermal oxidation. In: Kimura H, Izumi O (eds). *Titanium '80—Science and Technology Proceedings of the Fourth International Conference on Titanium*. Warrendale, PA: Metallurgical Society of AIME, 1980:2783–2792.
- Kilpadi DV, Lemons JE. The effect of surface and heat treatments on corrosion of unalloyed titanium implants. *Proceedings of the 16th Southern Biomedical Engineering Conference*. Biloxi, MS: 16th Southern Biomedical Engineering Conference, 1997.
- Zisman WA. Relation of the equilibrium contact angle to liquid and solid constitution. In: Gould R (ed). *Contact Angle, Wettability and Adhesion*. Washington, DC: American Chemical Society, 1964:1–51.

21. Whitten KW, Gailey KD, Davis RE. *General Chemistry with Qualitative Analysis*. Philadelphia, PA: Saunders, 1988: 301–302.
22. Kilpadi DV. *Surface Characterization of Unalloyed Titanium Implants* [thesis]. Birmingham, AL: Univ of Alabama, 1996.
23. Ameen AP, Short RD, Johns R, Schwach G. The surface analysis of implant materials. 1. The surface composition of a titanium dental implant material. *Clin Oral Implants Res* 1993;4:144–150.
24. Ong JL, Lucas LC, Raikar GN, Connatser R, Gregory JC. Spectroscopic characterization of passivated titanium in a physiologic solution. *J Mater Sci Mater Med* 1995;6:113–119.
25. Kuznetsov MV, Zhuravlev JF, Zhilyaev VA, Gubanoz VA. XPS study of the nitrides, oxides, and oxynitrides of titania. *J Electron Spectrosc Rel Phenomena* 1992;58:1–9.
26. Healy KE, Ducheyne P. Oxidation kinetics of titanium thin films in model physiologic environments. *J Colloid Interface Sci* 1992;150(2):404–417.
27. Shirkhanzadeh M. XRD and XPS characterization of superplastic TiO<sub>2</sub> coatings prepared on Ti6Al4V surgical alloy by an electrochemical method. *J Mater Sci Mater* 1995;6: 206–210.
28. Olejford I, Hansson S. Surface analysis of four dental implant systems. *Int J Oral Maxillofac Implants* 1993;8:32–40.
29. Sayer CN, Armstrong NR. X-ray photoelectron spectroscopy of TiO<sub>2</sub> and other titanate electrodes and various standard titanium oxide materials: Surface compositional changes of the TiO<sub>2</sub> electrode during photoelectrolysis. *Surf Sci* 1978;77:301–320.
30. Jobin M, Taborelli M, Emech R, Zenhausern F, Descouts P. Hydroxylation and crystallization of electropolished titanium surface. *Ultramicroscopy* 1992;42–44:637–643.
31. Hernández de Gatica NL, Jones GL, Gardella JA Jr. Surface characterization of titanium alloys sterilized for biomedical applications. *Appl Surf Sci* 1993;68:107–121.
32. Simon D, Devillers B, Bardeolle J. Study of the oxidation of titanium by microgravimetry and electron spectroscopy (ESCA) at elevated temperatures and low pressures. In: Kimura H, Izumi O (eds). *Titanium '80—Science and Technology Proceedings of the Fourth International Conference on Titanium*. Warrendale, PA: Metallurgical Society of AIME, 1980:2859–2866.
33. Pankuch M, Bell R, Melendres CA. Composition and structure of an anodic films on titanium in aqueous solutions. *Electrochimica Acta* 1993;38(18):2777–2779.
34. Mooradian A, Raccach PM. Raman study of the semiconductor-metal transition in Ti<sub>2</sub>O<sub>3</sub>. *Phys Rev Bull* 1971;3(12): 4253–4256.
35. Shin SH, Aggarwal RL, Lax B, Honig JM. Raman scattering in Ti<sub>2</sub>O<sub>3</sub>-V<sub>2</sub>O<sub>3</sub> alloys. *Phys Rev Bull* 1974;9(2):583–590.
36. Fujii T, Sakata N, Takada J, Miura Y, Daitoh Y, Takano M. Characteristics of titanium oxide films deposited by an activated reactive evaporation technique method. *J Mater Res* 1994;9(6):1468–1473.
37. Franck M, Celis J-P, Roos JR. Microprobe Raman spectroscopy of TiN coatings oxidized by solar beam heat treatment. *J Mater Res* 1995;10(1):119–125.
38. Pawlewicz WT, Exarhos GJ, Conaway WE. Structural characterization of TiO<sub>2</sub> optical coatings by Raman spectroscopy. *Appl Optics* 1983;22(12):1837–1840.
39. Berger H, Tang H, Lévy F. Growth and Raman spectroscopic characterization of TiO<sub>2</sub> anatase single crystals. *J Crystal Growth* 1993;130:108–112.
40. Tengvall P, Vikinge TP, Lundström I, Liedburg B. FT-Raman spectroscopic studies of the degradation of titanium peroxy gels made from metallic titanium and hydrogen peroxide. *J Colloid Interf Sci* 1993;160:10–15.
41. Exarhos GJ. Molecular characterization of dielectric films by laser Raman spectroscopy. In: McGuire GE (ed). *Characterization of Semiconductor Materials*. Park Ridge, NJ: Noyes Publications, 1989:242–288.
42. Baier RE, Meyer AE, Natiella JR, Natiella RR, Carter JM. Surface properties determine bio-adhesive outcomes: Methods and results. *J Biomed Mater Res* 1984;18:337–355.
43. Uyen HM, van Dijk LJ, Busscher HJ. Adhesion of stainable, calcium-rich deposits on substrata with different surface-free energies. An in vivo study in beagle dogs. *J Clin Periodontol* 1989;16:393–397.
44. Altankov G, Grinnell F, Groth T. Studies on the biocompatibility of materials: Fibroblast reorganization of substratum-bound fibronectin on surfaces varying in wettability. *J Biomed Mater Res* 1996;30:385–391.