

Computational Analysis of Porous Channel Flow with Cross-Diffusion

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Abstract We investigate the heat and mass transfer in a variable-viscosity channel flow simultaneously accounting for viscous dissipation, external pollutant injection and Soret-Dufour effects. By adopting the Boussinesq approximation and assuming a fully developed uni-direction flow, the set of governing equations are presented. We formulate a finite difference scheme which decouples the system and is amenable to parallel computing. Gauss-Seidel solver is adopted for the resulting linear systems. The numerical results show that the thermal and solutal Grashof numbers, the viscosity parameter and the Darcy number all increase the flow velocity, while the magnetic field and the Prandtl number decrease the flow. It is also observed that the concentration and temperature are opposing each other; an increase in one causes a decrease in the other. Hence, we concluded that a strategy to mitigate pollution in the considered fluid system is to increase the fluid's temperature.

Keywords Porous channel flow, Finite difference scheme, Temperature-dependent viscosity, Soret effect, Dufour effects, Viscous dissipation

1. Introduction

Flows through porous media have many applications such as in catalytic converters, fischer-tropsch synthesis, oil reservoirs and bioheat [1-4]. For instance, ground flows have many applications like in oil recovery and energy conversion [5]. Other application areas include packed-bed chemical reactors, gas turbines and material processing facilities [6].

These applications have led to enormous research in the flow and transport phenomena taking place in porous materials. Studies have been conducted on automobile exhaust systems [7], Fischer-Tropsch synthesis [3], in transpiration cooling [8], and in human tissues [9]. Heat transfer in porous ground is investigated in [10], see also [11,12] for coupled transport studies in porous media. Bhargava et al. [13] investigated combined heat and mass transfer in a porous medium, taking into account mass fluxes due to temperature gradients (known as Soret effect) and also heat fluxes due to concentration gradients (known as Dufour effect). Here, we use the term cross-diffusion to refer to the combined presence of both Soret and Dufour effects, see also page 62 in [14].

Mehmood and Ali [15] investigated slip condition effects

on a viscous channel flow, and the study is extended to the combined effects of both heat injection and suction in [16]. The results show that the flow velocity is enhanced by increase in both the Darcy number and thermal Grashof's number. Also, the oscillatory flow of a temperature-dependent viscosity Jeffrey fluid in a porous channel is investigated in [17]. They assumed no-slip conditions, incorporated Soret-Dufour effects, an analytical solution is obtained using the homotopy perturbation method. Their results show that the magnetic field decreases the fluid velocity. Two points to note about their work are (i) a time and space dependent problem, as posed by them, requires both boundary and initial conditions. But their initial conditions were not stated, and (ii) they represented the viscous term in the velocity equation as a product of the variable viscosity and the second derivative of the velocity. This is obviously faulty and can only be true if the viscosity were to be a constant. The variable viscosity should appear under the derivative, see [18,6,19,20] for example.

In [21], the steady heat and mass transfer in a Casson fluid flow over a porous sheet is considered with cross-diffusion. They observed that the Casson parameter decreases skin friction. In an earlier study, Makinde and Mhone [22] considered the magnetohydrodynamic flow and heat transfer in a channel filled with porous material, see also [23] for a steady flow. Seth and collaborators [24] investigated the effects of Joule heating, viscous dissipation, Newtonian heating and thermo-diffusion on the MHD flow of a Casson fluid through a porous medium, see also [25]. The numerical challenges encountered in the presence of an exponentially

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time-dependent suction have been investigated in [26,27].

Finite volume analysis of heat transfer in the flow of an electrically conducting fluid in a cylindrical domain is studied in [28], see also [29] for investigations in cylindrical annulus. In [30] the channel flow of copper-kerosene nanofluid with magnetic field and stretching wall effects is investigated. Natural convection heat transfer with heat sources in a cylindrical annulus is considered in [31] while the homotopy analysis of MHD flow between two porous plates intersecting at an angle is studied in [32]. In another study, the Maxwell convective heat transfer model is coupled with the Navier-Stokes fluid model to investigate the flow and thermal characteristics of Titania nanofluids using different base fluids [33]. This set of studies which were conducted by Mebarek-Oudina and collaborators did not consider mass transfer.

In another series of investigations, Makinde and collaborators [34,35] have investigated either heat transfer or mass transfer, but not both, in different geometries; Kumaresan and co-authors [36] considered the combined effects of heat and mass transfer in a Newtonian fluid, and derived an exact solution using Laplace transform approach, for constant-velocity fluids in porous media. Then, Nwaigwe [20] extended the study to incorporate combined heat and mass transfer in a concentration-dependent viscosity flow with concentration-dependent diffusivity. One of the cardinal points in [20] was how to correctly solve the posed problem, hence a sequential implicit scheme was formulated and compared with a Matlab subroutine.

Prasad and collaborators [37] investigated the heat transfer and porous media flow of a Casson fluid with temperature-dependent thermal conductivity. The steady flow and mass transfer in a porous solid is considered in [38], and extended to the unsteady case in [6] without heat transfer; then to the unsteady, temperature-dependent viscosity, non-isothermal case is considered in [19] without mass transfer. Sharma and coworkers in recent study [39] further extended these studies to investigate the influence of both heat and mass transfer in the porous media flow of a Newtonian fluid incorporating Soret effects.

From the above account, it becomes obvious that a full incorporation of heat and mass transfer of variable viscosity fluids with Soret-Dufour effects and pollutant injection is still not complete. In particular, as stated above, the very much commendable work of Selvi and Muthuraji [17] is incomplete because of the formulation of the viscous term and non specification of initial flow fields; their problem is thus not closed. Moreover, the study did not consider pollutant injection. Secondly, the other impressive work of Sharma and colleagues [39] only considered constant viscosity fluids, yet Dufour effects are neglected. Moreover, both of these studies adopted analytical methods of solution - the Homotopy perturbation and the Laplace transform methods - which are limited in terms of re-usability and extendability, unlike numerical methods. In this study, we extend the work of [39] by incorporating variable viscosity

and Soret-Dufour effects, while we improve some aspects of the work of Selvi and Muthuraji [17] by correctly representing the viscous term, incorporating pollutant injection and posing a correct set of initial flow fields consistent with the prescribed boundary conditions. In addition, we propose a numerical scheme which can be easily extended to-and be re-used for other complicated problems.

The remainder of the paper is organized as follows: we present the model equations, including the non-dimensional forms, in section 2. The numerical scheme is formulated in section 3. The numerical results are presented and discussed in section 4 and the paper is concluded in section 5.

2. Formulation of the Mathematical Problem

We consider a vertical channel filled with a saturated porous material and bounded by two impermeable walls separated by a distance h , see figure 1. The \bar{x} and \bar{y} axis are as indicated in the figure. We then consider a flow strictly along the channel axis, fully developed and driven by constant pressure gradient and gravitational and magnetic body forces. The two channel walls are immovable and the fluid is incompressible with temperature-dependent viscosity. A uniform magnetic field is applied perpendicular to the walls and viscous dissipation is incorporated.

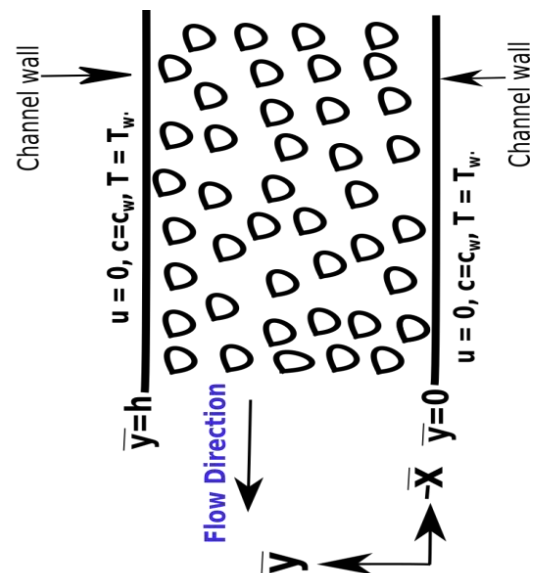


Figure 1. Physical set-up of flow in a saturated vertical porous channel

Further, we assume that the fluid is non-isothermal and some substance is being introduced into the fluid at the rate of $e^{b(c-c_0)}$ per unit volume of the fluid, where $c = c(\bar{y}, \bar{t})$, c_0 and b are, respectively, the substance's concentration at point \bar{y} and at time, \bar{t} ; a reference concentration; and a constant. We also incorporate

cross-diffusion effects, meaning that combined temperature variations due to mass diffusion and concentration variations due to heat diffusion - the Soret-Dufour effects. Bousinesq's approximation is adopted for the fluid body forces due to solutal and thermal variations.

On the channel wall boundaries, the no-slip condition apply, and the temperature and concentration are kept constant at T_w and c_w respectively. At initial time, the fluid velocity has a parabolic profile with maximum value at the channel center and vanishes at the walls in line with the no-slip conditions. Both the temperature and concentration

are initially zero within the fluid except at the walls where the constant values are maintained.

Denoting by $u(\bar{y}, \bar{t}), c(\bar{y}, \bar{t})$ and $T(\bar{y}, \bar{t})$ the velocity, concentration and temperature, respectively, at point \bar{y} and time \bar{t} ; and defining $\Omega_{\bar{t}} = (0, h) \times (0, T_f) \subset \mathbb{R} \times \mathbb{R}^+$. Then, the problem is governed by the following system [18,6,19,20]:

$$\left. \begin{aligned} \rho \frac{\partial u(\bar{y}, t)}{\partial \bar{t}} &= \frac{\partial}{\partial \bar{y}} \left(\mu(T) \frac{\partial u(\bar{y}, t)}{\partial \bar{y}} \right) - \frac{\partial P}{\partial \bar{x}} - \frac{\mu(T)}{K} u(\bar{y}, t) \\ &\quad - \sigma B_0^2 u(\bar{y}, t) + g \rho \beta_T (T - T_0) + g \rho \beta_c (c - c_0), \\ \frac{\partial c(\bar{y}, t)}{\partial \bar{t}} &= \frac{\partial}{\partial \bar{y}} \left(D_0 \frac{\partial c(\bar{y}, t)}{\partial \bar{y}} + \kappa_T \frac{D_0}{T_m} \frac{\partial T(\bar{y}, \bar{t})}{\partial \bar{y}} \right) + S_0 e^{b_2(c-c_0)}, \\ \rho c_p \frac{\partial T(\bar{y}, \bar{t})}{\partial \bar{t}} &= \frac{\partial}{\partial \bar{y}} \left(\kappa_0 \frac{\partial T(\bar{y}, t)}{\partial \bar{y}} + \rho \kappa_T \frac{D_0}{c_s} \frac{\partial c(\bar{y}, \bar{t})}{\partial \bar{y}} \right) + \mu(T) \left(\frac{\partial u(\bar{y}, t)}{\partial \bar{y}} \right)^2 \end{aligned} \right\} \text{ in } \Omega_{\bar{t}} \quad (1)$$

$$u(\bar{y}, 0) = m_0(h - \bar{y})\bar{y}, \forall \bar{y} \in [0, h], \quad c(\bar{y}, 0) = \begin{cases} c_w, & \text{if } y \in \{0, h\}, \\ 0, & \text{else,} \end{cases} \quad (2)$$

$$T(\bar{y}, 0) = \begin{cases} T_w, & \text{if } y \in \{0, h\}, \\ 0, & \text{else,} \end{cases}$$

$$\left. \begin{aligned} u(0, \bar{t}) = u(h, \bar{t}) = 0, \quad c(0, \bar{t}) = c(h, \bar{t}) = c_w, \\ T(0, \bar{t}) = T(h, \bar{t}) = T_w, \end{aligned} \right\} \forall t \in [0, T], \quad (3)$$

where

$$\mu(T) = \mu_0 e^{-b_1(T-T_0)}, \quad S_0 = \frac{(c_w - c_0)\mu_0}{h^2 \rho}. \quad (4)$$

Here, ρ = fluid density, $\mu(T)$ = temperature-dependent fluid viscosity, P = fluid pressure, K = permeability of porous medium, σ = electrical conductivity, B_0 = uniform magnetic field intensity, g = acceleration due to gravity, β_T = temperature expansion coefficient, β_c = concentration expansion coefficient, T_0 = reference temperature, D_0 = diffusion coefficient, κ_0 = thermal conductivity, c_p = specific heat capacity, κ_T = thermal diffusion ratio, m_0 = a constant, T_m = mean fluid temperature, c_s = the concentration susceptibility, while b_1 and b_2 are constants.

2.1. Non-dimensional Formulation

We define the following dimensionless quantities [18,20,6,19]:

$$\begin{aligned}
y &= \frac{\bar{y}}{h}, x = \frac{\bar{x}}{h}, t = \frac{\mu_0 \bar{t}}{\rho h^2}, q_0 = m_0 h^2 \frac{\rho h}{\mu_0}, L = -\frac{\rho h^2}{\mu_0^2} \frac{\partial \bar{P}}{\partial x}, \\
w &= \frac{h u \rho}{\mu_0}, \phi = \frac{c - c_0}{c_w - c_0}, \theta = \frac{T - T_0}{T_w - T_0}, D_u = \frac{\kappa_T D_0 (c_w - c_0)}{c_s c_p (T_w - T_0)}, \\
D_a &= \frac{K}{h^2}, P_r = \frac{\mu_0 c_p}{\kappa_0}, B_r = \frac{\mu_0^3}{\kappa_0 h^2 \rho^2 (T_w - T_0)}, \alpha = b_1 (T_w - T_0), \\
\beta &= b_2 (c_w - c_0), S_c = \frac{\mu_0}{D_0 \rho}, M = \frac{\sigma B_0^2 h^2}{\mu_0}, S_r = \frac{\kappa_T D_0 \rho (T_w - T_0)}{T_m \mu_0 (c_w - c_0)}, \\
G_T &= \frac{\rho^2 g \beta_T h^3}{\mu_0^2} (T_w - T_0), G_c = \frac{\rho^2 g \beta_c h^3}{\mu_0^2} (c_w - c_0).
\end{aligned} \tag{5}$$

Substituting the nondimensional parameters and variables in (5) into (1)-(4), we obtain the following non-dimensional equations:

$$\left. \begin{aligned}
\frac{\partial w}{\partial t} &= L + \frac{\partial}{\partial y} \left(e^{-\alpha \theta} \frac{\partial w}{\partial y} \right) - \left(M + \frac{e^{-\alpha \theta}}{D_a} \right) w + G_T \theta + G_c \phi, \\
\frac{\partial \phi}{\partial t} &= \frac{1}{S_c} \frac{\partial^2 \phi}{\partial y^2} + S_r \frac{\partial^2 \theta}{\partial y^2} + e^{\beta \phi}, \\
\frac{\partial \theta}{\partial t} &= \frac{1}{P_r} \frac{\partial^2 \theta}{\partial y^2} + D_u \frac{\partial^2 \phi}{\partial y^2} + \frac{B_r}{P_r} e^{-\alpha \theta} \left(\frac{\partial w}{\partial y} \right)^2,
\end{aligned} \right\} \text{ in } \Omega_t. \tag{6}$$

subject to

$$\left. \begin{aligned}
w(y, 0) &= q_0 (1 - y) y, \quad \forall y \in [0, 1], \\
\phi(y, 0) &= \theta(y, 0) = \begin{cases} 1, & \text{if } y \in \{1, 0\}, \\ 0, & 0 < y < 1. \end{cases}
\end{aligned} \right\} \tag{7}$$

$$\left. \begin{aligned}
w(0, t) &= w(1, t) = 0, \phi(0, t) = \phi(1, t) = 1, \\
\theta(0, t) &= \theta(1, t) = 1,
\end{aligned} \right\} \forall t \geq 0, \tag{8}$$

where L = pressure-gradient parameter, α = viscosity parameter, M = magnetic field parameter, D_a = Darcy number, G_T = Thermal Grashofs number, G_c = solutal Grashofs number, S_c = Schmidt number, S_r = Soret coefficient, β = injection paramter, P_r = Prandtl number, D_u = Dufour coefficient, B_r = Brinkman number and q_0 is a constant [18,6,19].

3. Sem-Implicit Numerical Scheme

Let $Q \geq 1$ be an integer and Δt be given. Define $\Delta y := \frac{1}{Q}$; $y_i = i \Delta y$ for $i = 0, 1, 2, \dots, Q$; $t^n = n \Delta t$ for $n = 0, 1, 2, \dots$; and

$$w_i^n \approx w(x_i, t^n), \quad \phi_i^n \approx \phi(x_i, t^n), \quad \theta_i^n \approx \theta(x_i, t^n).$$

Also, define $\bar{\mu}_i^n := e^{-\alpha \theta_i^n}$, and $\bar{\mu}_{i \pm 1/2}^n := \frac{\bar{\mu}_i^n + \bar{\mu}_{i \pm 1}^n}{2}$. We propose to discretize the coupling and nonlinear source terms explicitly, while the variable-coefficient viscous terms are treated in conservative form. This leads to the following semi-implicit scheme [40,41] see also [20]:

$$\frac{w_i^{n+1} - w_i^n}{\Delta t} = L + \frac{\bar{\mu}_{i-1/2}^n}{(\Delta y)^2} (w_{i-1}^{n+1} - w_i^{n+1}) + \frac{\bar{\mu}_{i+1/2}^n}{(\Delta y)^2} (w_{i+1}^{n+1} - w_i^{n+1}) - \left(M + \frac{\bar{\mu}_i^n}{D_a} \right) w_i^{n+1} + G_r \theta_i^n + G_c \phi_i^n, \tag{9}$$

$$\frac{\phi_i^{n+1} - \phi_i^n}{\Delta t} = \frac{1}{S_c} \frac{\phi_{i+1}^{n+1} - 2\phi_i^{n+1} + \phi_{i-1}^{n+1}}{(\Delta y)^2} + S_r \frac{\theta_{i+1}^n - 2\theta_i^n + \theta_{i-1}^n}{(\Delta y)^2} + e^{\beta \phi_i^n}, \tag{10}$$

$$\frac{\theta_i^{n+1} - \theta_i^n}{\Delta t} = \frac{1}{P_r} \frac{\theta_{i+1}^{n+1} - 2\theta_i^{n+1} + \theta_{i-1}^{n+1}}{(\Delta y)^2} + D_u \frac{\phi_{i+1}^n - 2\phi_i^n + \phi_{i-1}^n}{(\Delta y)^2} + \frac{B_r}{P_r} \bar{\mu}_i^n \left(\frac{w_{i+1}^n - w_{i-1}^n}{2\Delta y} \right)^2, \tag{11}$$

$$w_0^{n+1} = w_Q^{n+1} = 0, \phi_0^{n+1} = \phi_Q^{n+1} = \theta_0^{n+1} = \theta_Q^{n+1} = 1 \quad \forall n, \\ w_i^0 = q_0(1 - y_i)y_i, \phi_i^0 = \theta_i^0 = \begin{cases} 1, & \text{if } i = 0, Q, \\ 0, & \text{otherwise,} \end{cases} \quad \forall i. \tag{12}$$

Treating the variable coefficient viscous term in this manner allows to avoid derivatives, which may actually not exist; it also reduce the computational cost. The resulting scheme is decoupled and the solution of each state variable can be computed independently, which in turn allows to leverage parallel computing architectures.

4. Numerical Experiments and Results

The numerical results are now presented and discussed. The numerical scheme, (9) - (12), is implemented in an in-house C++ code developed by the first author. We use the following data for all the computations, except when otherwise stated: $L = 1.0, \alpha = 0.1, M = 0.3, D_a = 0.1, G_r = 0.1, G_c = 0.1, S_c = 0.24, S_r = 0.6, \beta = 0.1, P_r = 0.75, D_u = 0.03, B_r = 0.1, \Delta t = 0.005, q_0 = 0.5$ and the total duration of simulation is $T = 0.5$ seconds. The variation of the velocity, concentration and temperature with the flow parameters are

considered. The discussion starts with the viscosity parameter α and end with the magnetic field parameter M .

The variation of flow fields with the viscosity parameter α , is shown in figure 2. It is observed that increasing α , which signifies decreasing the fluid viscosity, leads to increase in the flow velocity. The parameter has no effect on the temperature or the concentration.

The effects of the injection parameter β is displayed in figure 3. We can see that increase in β causes an increase in the concentration and a decrease in the temperature. This is obvious because increase in β means addition of the pollutant into the system which should naturally increase the concentration. In this study we observed that increase in concentration is associated with a decrease in the temperature and vice-versa. This is due to cross-diffusion between the concentration and temperature - where one quantity contributes to the flux of the other. Hence, an increase of one leads to non-increase of the other.

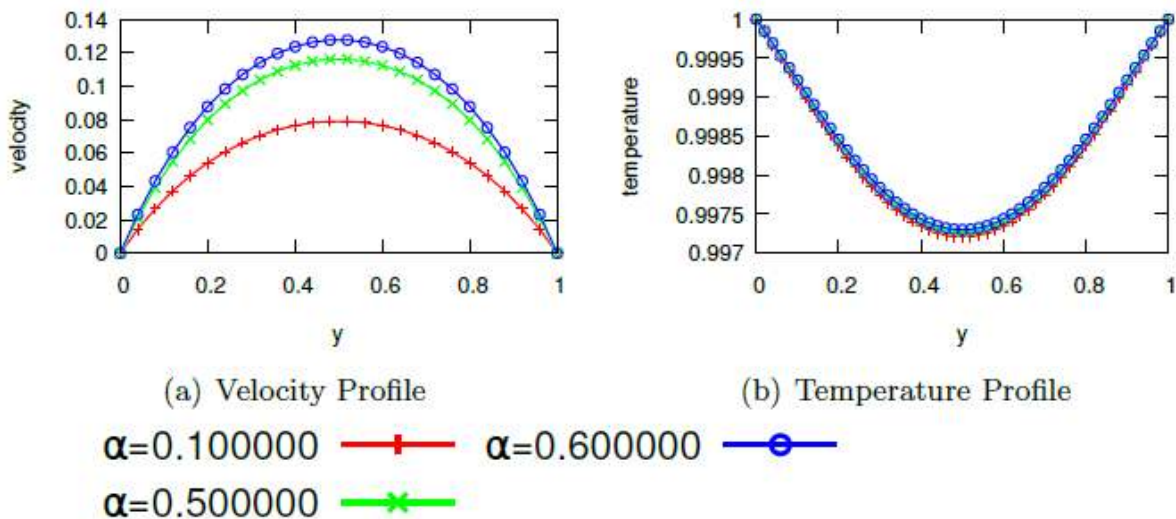


Figure 2. Effect of viscosity parameter α on velocity

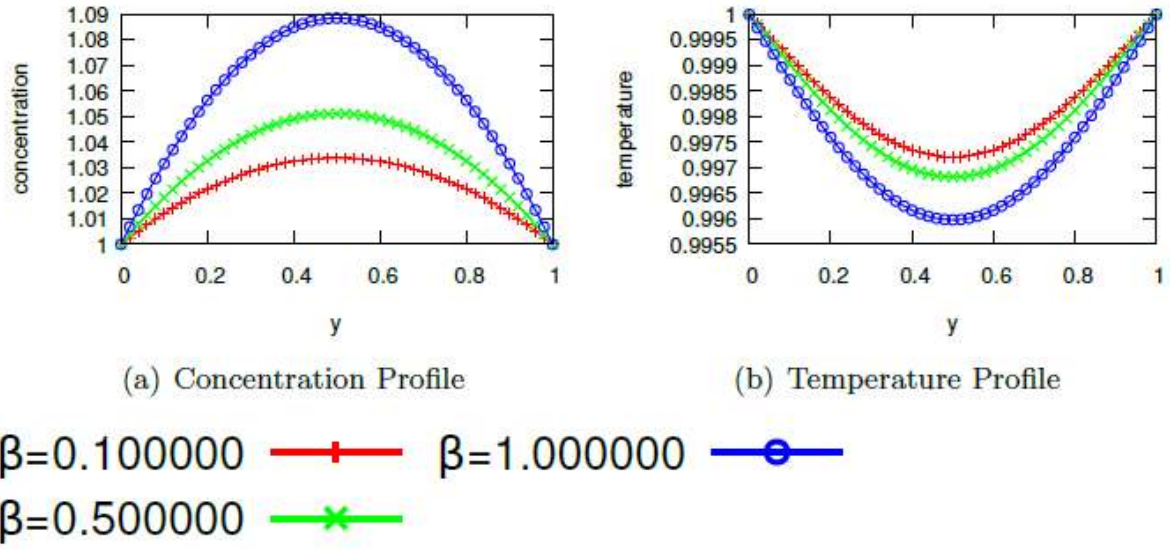


Figure 3. Effect of pollutant injection parameter β on the flow Fields

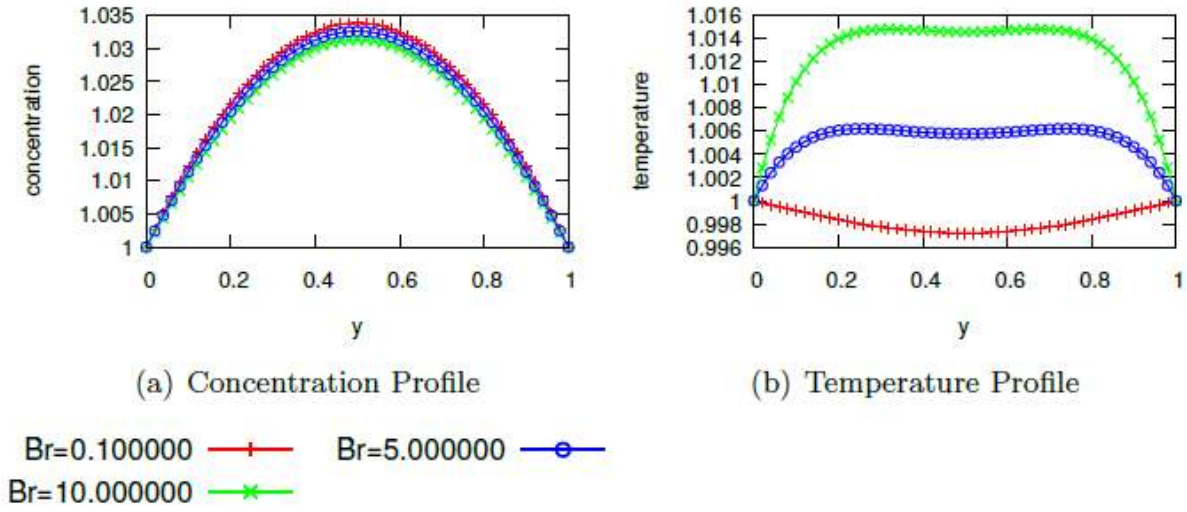


Figure 4. Effect of Brinkman number B_r on the flow fields

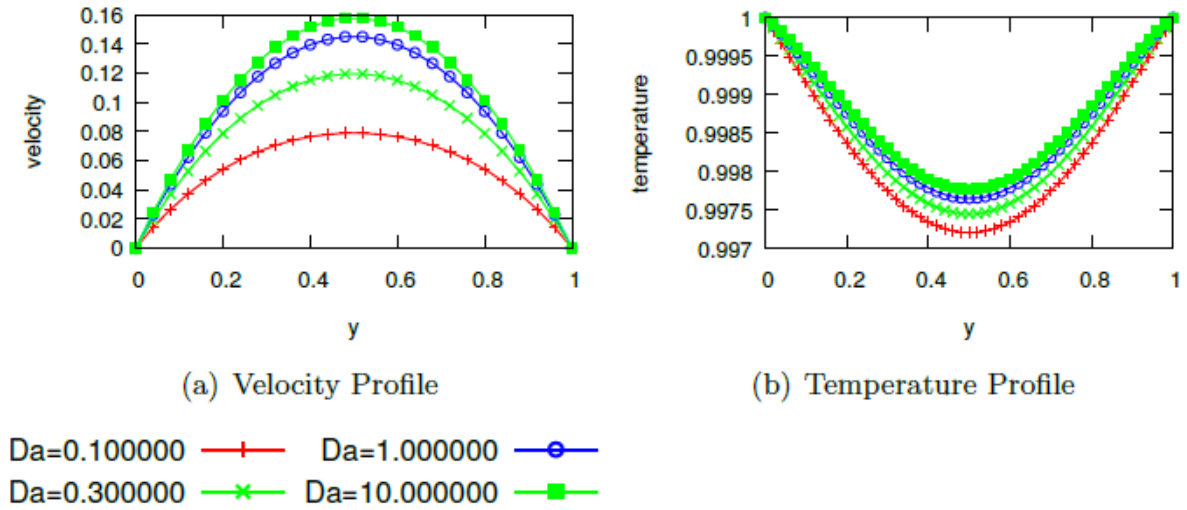


Figure 5. Effect of Darcy number D_a on the flow fields

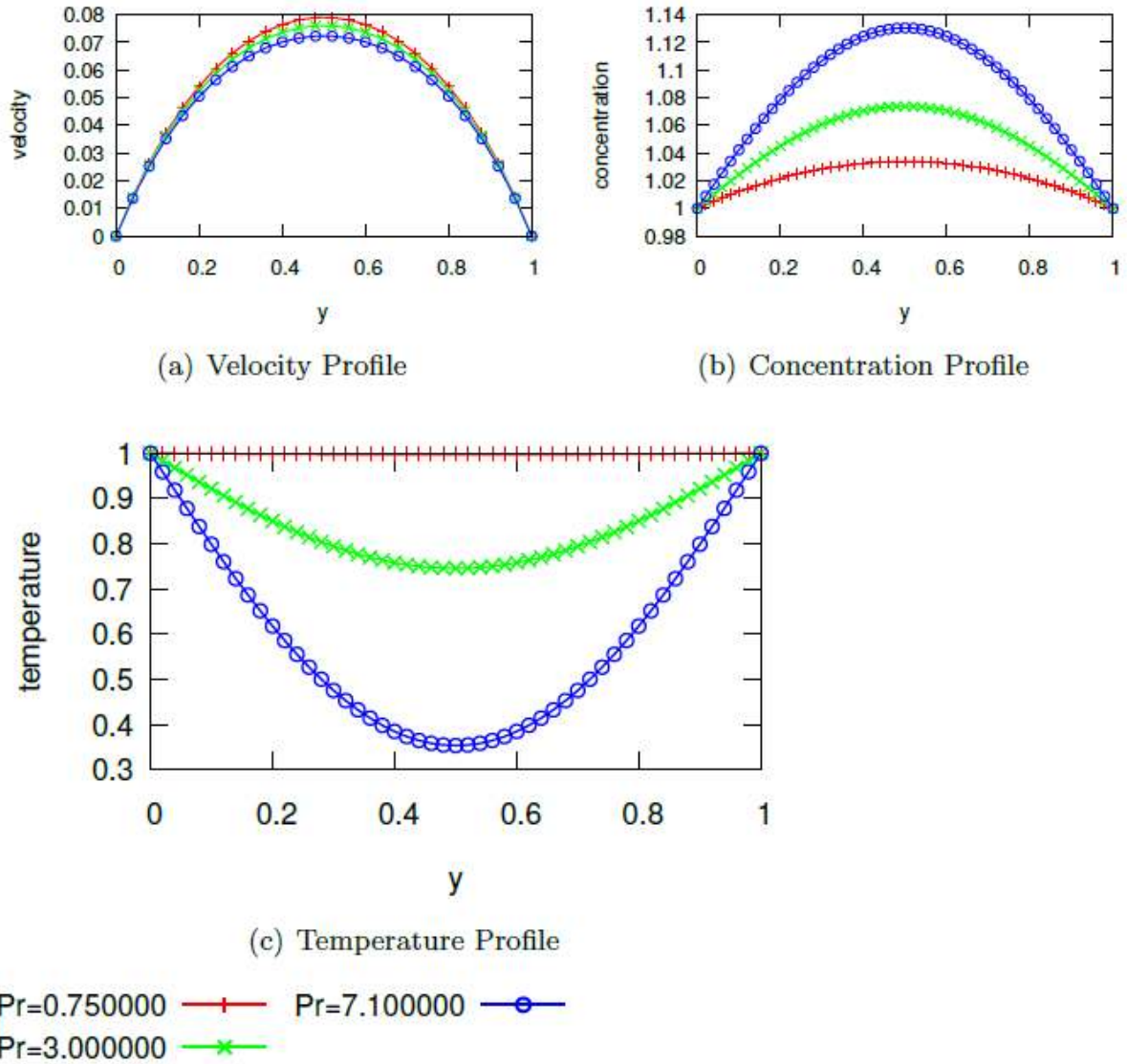


Figure 6. Effect of Prandtl number P_r on the flow fields

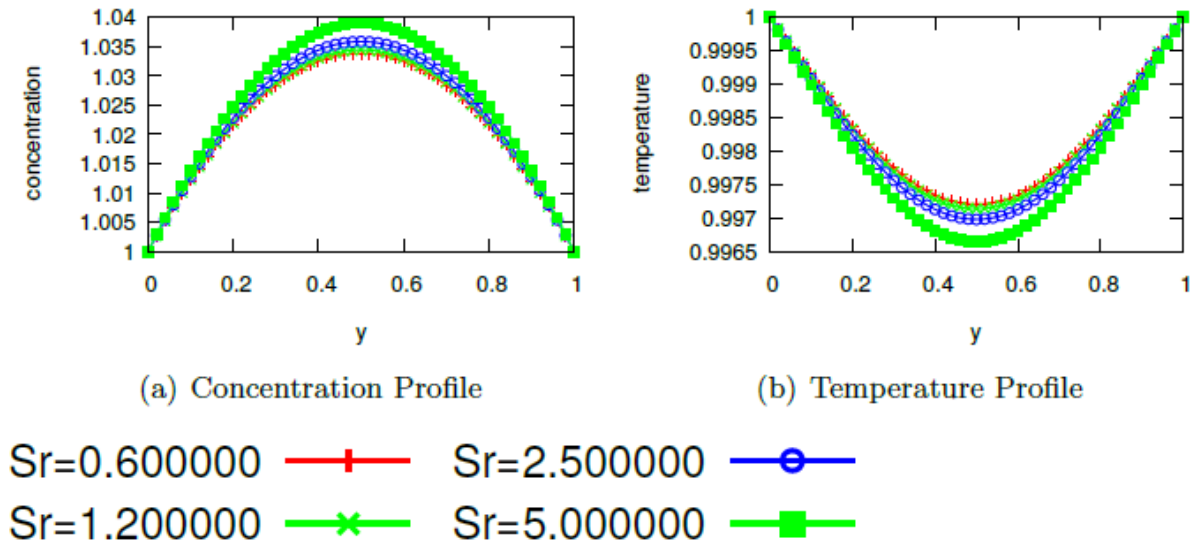
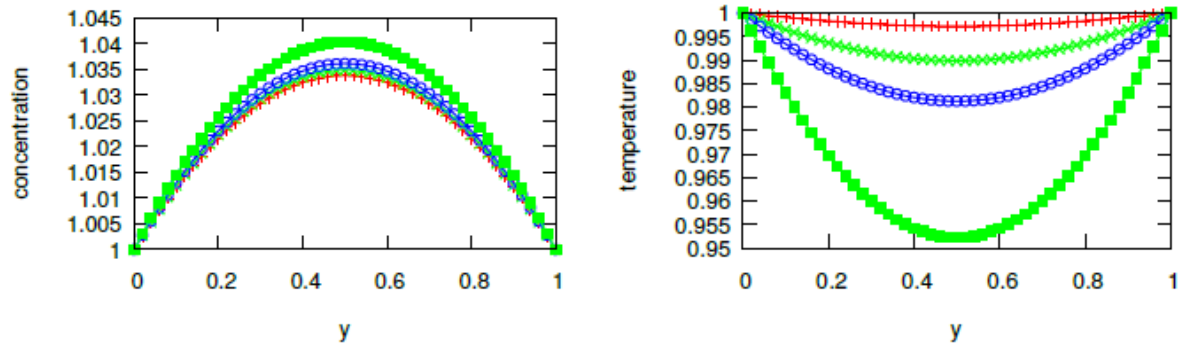


Figure 7. Effect of Soret number S_r on the flow fields

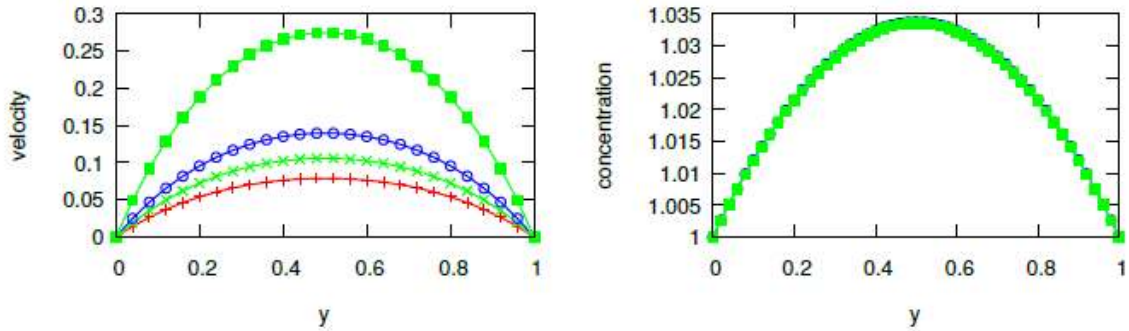


(a) Concentration Profile

(b) Temperature Profile

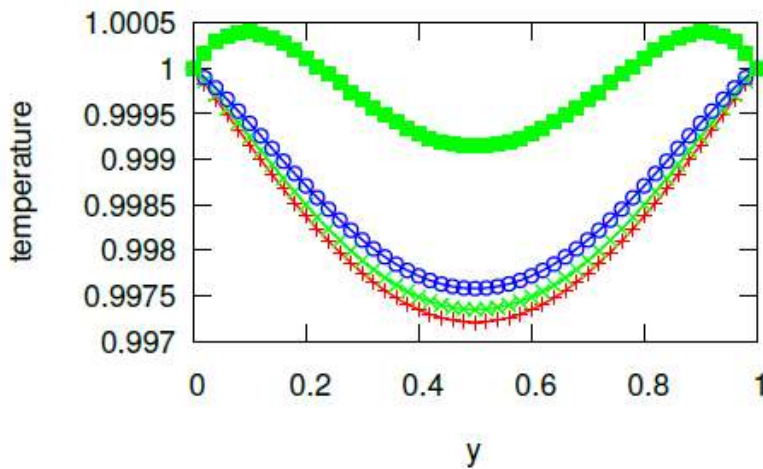
$D_u=0.030000$ —+— $D_u=0.600000$ —○—
 $D_u=0.300000$ —×— $D_u=1.500000$ —■—

Figure 8. Effect of Dufour number D_u on the flow fields



(a) Velocity Profile

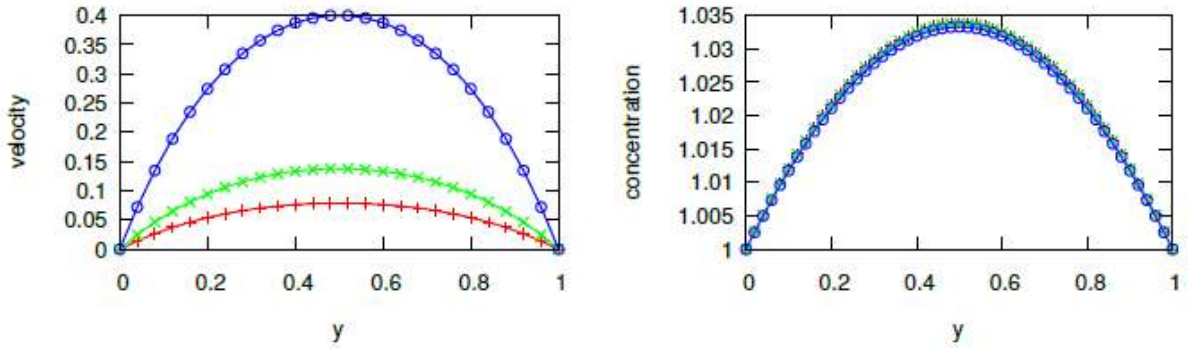
(b) Concentration Profile



(c) Temperature Profile

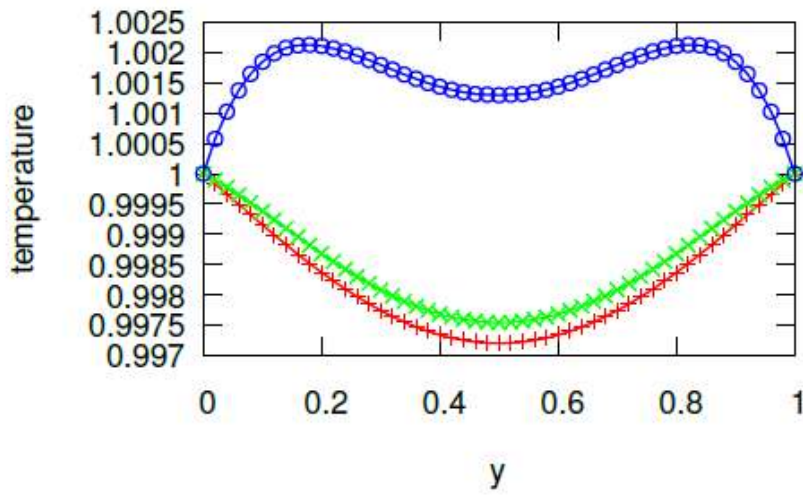
$G_c=0.100000$ —+— $G_c=1.000000$ —○—
 $G_c=0.500000$ —×— $G_c=3.000000$ —■—

Figure 9. Effect of Solutal Grashof number G_c on the flow fields



(a) Velocity Profile

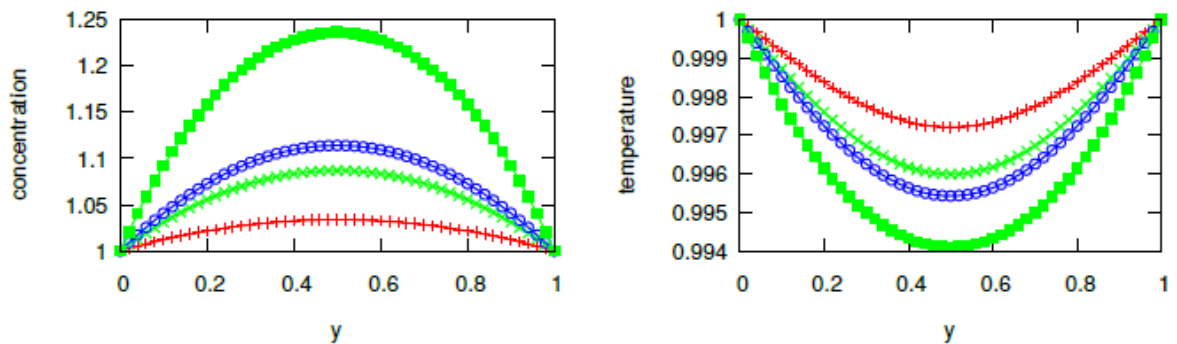
(b) Concentration Profile



(c) Temperature Profile

$G_T=0.100000$ —+— $G_T=5.000000$ —○—
 $G_T=1.000000$ —×—

Figure 10. Effect of Thermal Grashof number G_T on the flow fields



(a) Concentration Profile

(b) Temperature Profile

$Sc=0.240000$ —+— $Sc=0.780000$ —○—
 $Sc=0.600000$ —×— $Sc=2.620000$ —■—

Figure 11. Effect of Schmidt number Sc on the flow fields

An increase in temperature and a slight decrease in concentration are observed in figure 4. This is because an increase in B_r implies an increase in the viscous dissipation. This leads to increased temperature which in turn causes a decrease in the concentration as a result of cross-diffusion. No significant change in velocity is observed and this is due to the opposing effects of the increased temperature and decreased concentration.

The effect of Darcy number are shown in figure 5 which depicts an increase in velocity and temperature. This is because increasing Darcy number implies to increase the porosity of the medium which should naturally increase the flow, hence the observed increase in velocity. Also, since velocity increase results to increase in viscous dissipation which in turn increases the temperature, hence the observed increase in temperature.

The impact of the Prandtl number is displayed in figure 6. As it can be seen, increasing P_r leads to decrease in temperature and velocity but to an increase in concentration. This is because increasing this parameter means to reduce the fluid's thermal conductivity which reduces the rate at which heat is transported from the heated channel walls into the fluid which was initially at zero temperature. The temperature increase then leads to a reduction in the fluid viscosity hence causing a rise in the velocity. The concentration is increased due to the decrease in temperature - the cross-diffusion effect.

The effect of Soret number is shown in figure 7. Increase in S_r decreases the temperature but increases the concentration. The Soret effect acts as a source to the pollutant's concentration leading to increase in the

concentration which in turn reduces the temperature due to cross-diffusion. Exactly the same effect is observed in figure 8 in which the Dufour number enhances the concentration but decreases the temperature. This shows that the Soret-Dufour effects seem to favor the concentration but diminish the temperature. The two parameters, S_r and D_u did not show any influence on the velocity.

The effects of the solutal and thermal Grashof numbers G_c and G_T are displayed in figures 9-10. It is observed that both parameters increase the velocity and temperature. This is expected since an increase in G_c and G_T means increasing the body force on the fluid which enhances the velocity, and this in turn increases the viscous dissipation, hence increasing the temperature. There is also a very small (insignificant) decrease in concentration, and this obviously due to the cross-diffusion effect - the small temperature increase caused the very small decrease in concentration see figures 9(b) and 10(b).

The variations of flow fields with Schmidt number is shown in figure 11. We can see that increasing S_c causes a rise in concentration and a decrease in temperature; no significant change in velocity is observed. This is because, an increase in S_r means to reduce the pollutant diffusivity. Since there is a pollutant injection into the fluid, higher diffusivity will reduce the concentration, while less diffusivity will enhance it. This is why increasing S_r (or reducing diffusivity) increases the concentration. As we noted above, cross-diffusion causes the temperature to decrease. Figure 12 shows that the magnetic field parameter decreases the velocity and have no effect on the concentration or temperature.

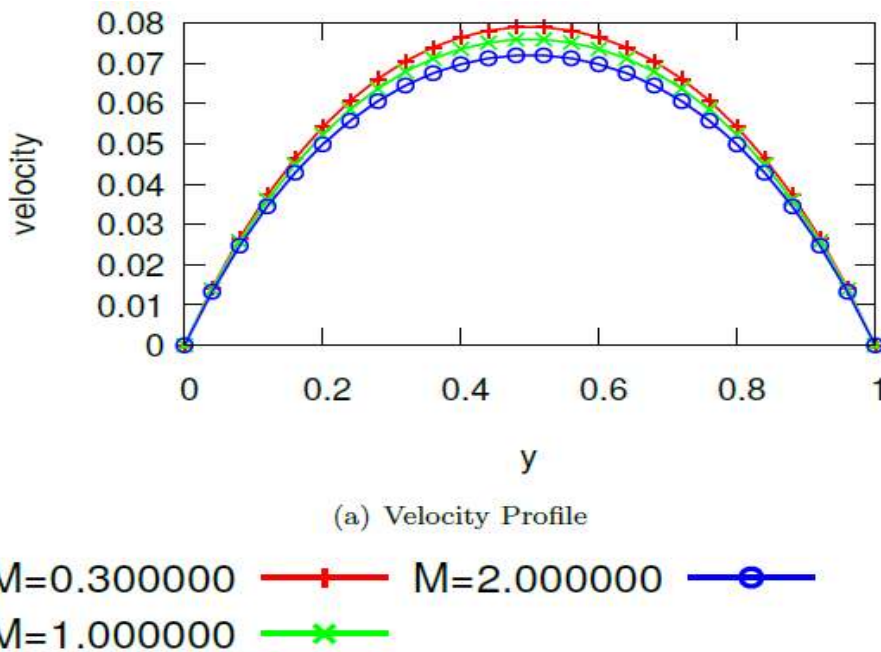
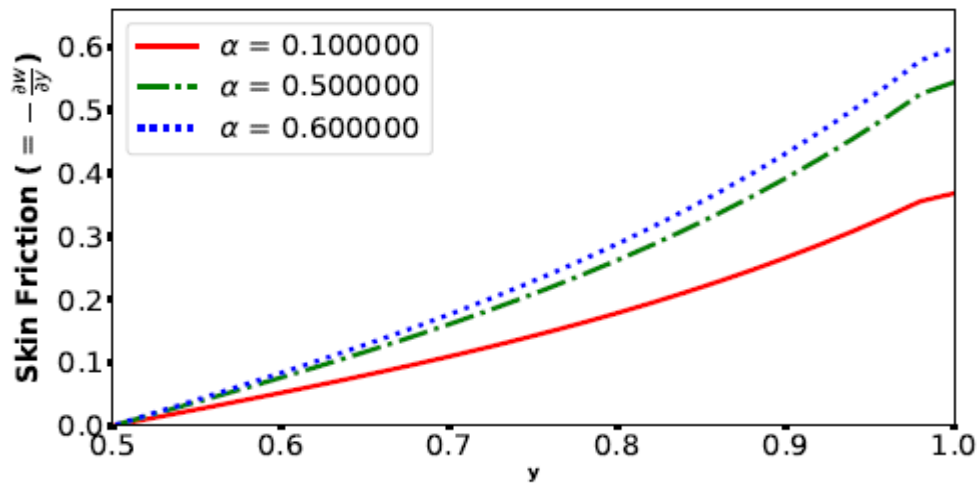
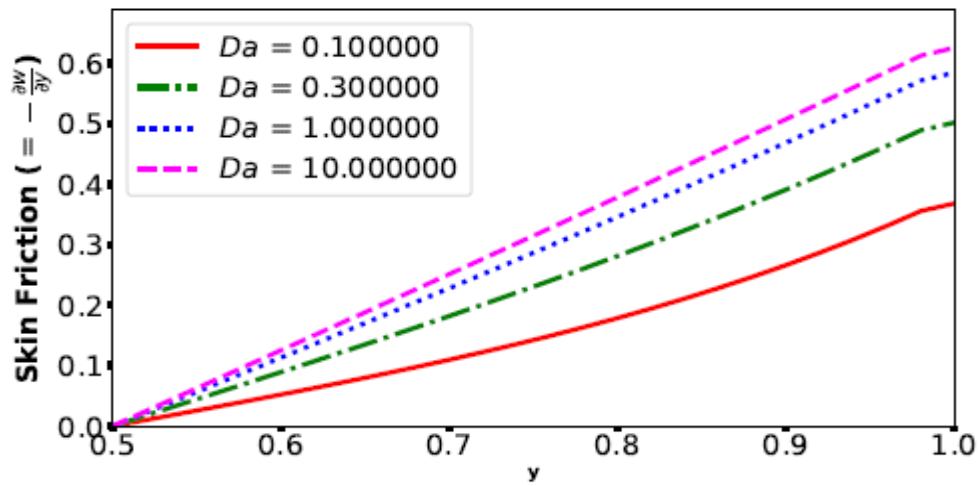


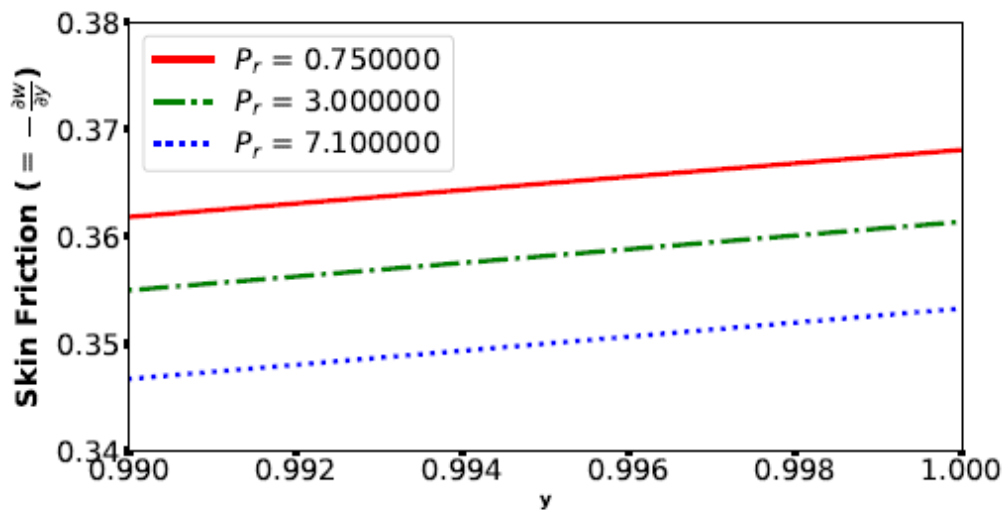
Figure 12. Effect of Magnetic field parameter M on the flow fields



(a) Effect of α on Skin Friction

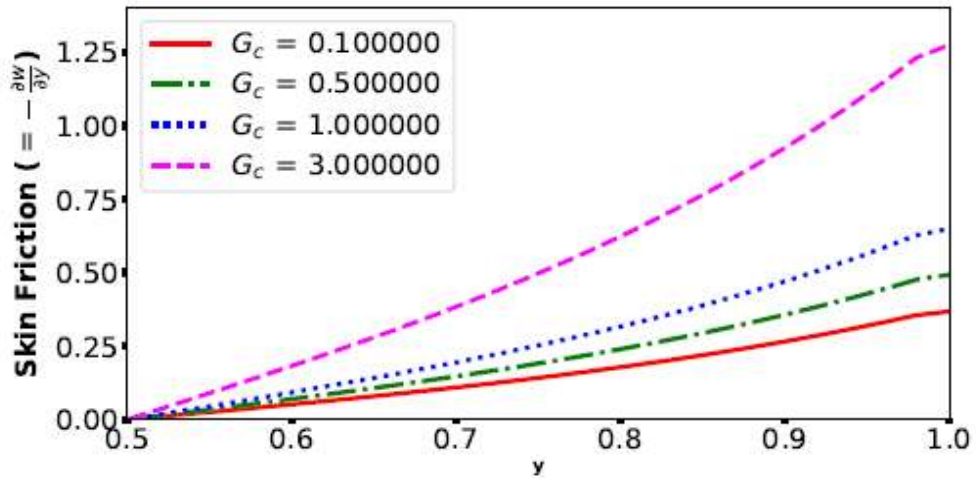


(b) Effect of Da on Skin Friction

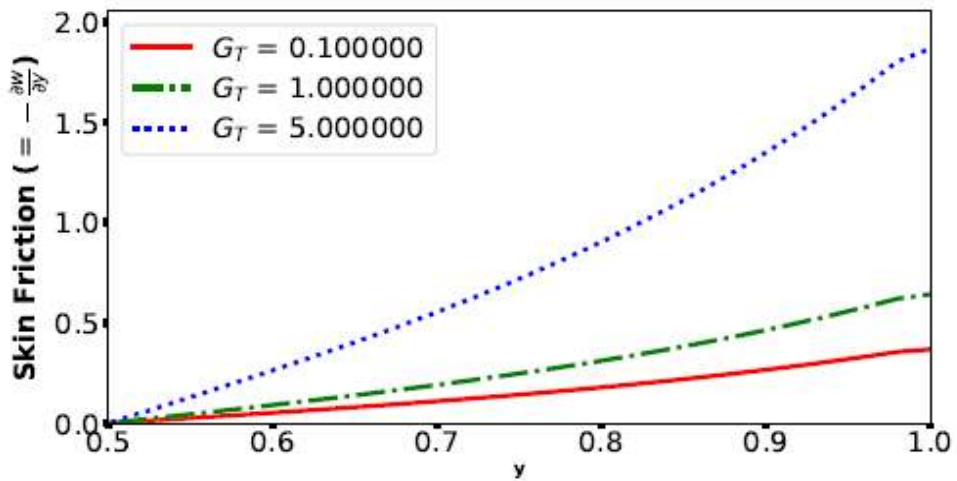


(c) Effect of Pr on Skin Friction

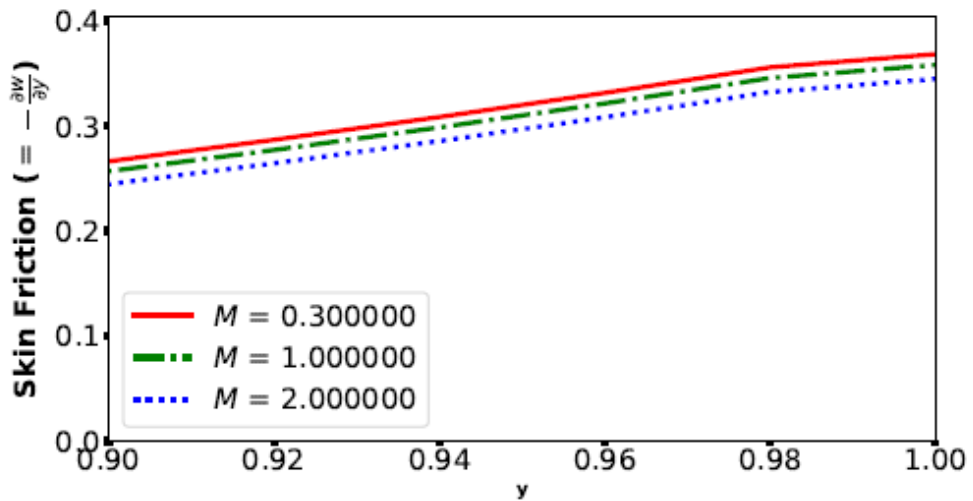
Figure 13. Variation of Skin Friction with α , Da and Pr



(a) Effect of G_c on Skin Friction



(b) Effect of G_T on Skin Friction



(c) Effect of M on Skin Friction

Figure 14. Variation of Skin Friction with G_c , G_T and M

The variations of of the skin friction are displayed in figures 13 and 14. It is shown that the skin friction increases with increase in viscosity parameter α , the Darcy number D_a , the solutal Grashof's number G_c and the thermal Grashof's number G_T . It also shown that the skin friction decreases with increasing magnetic field parameter M and the Prandtl number P_r .

5. Conclusions

This study presented a heat and mass transfer problem in the flow of a temperature dependent viscosity fluid in a saturated porous channel. The effects of dissipation, pollutant injection and cross diffusion are incorporated and the governing equations are solved using a convergent finite difference algorithm. The numerical results show that the flow parameters have opposite effects on the concentration and temperature, meaning that a decrease in one of the two is associated with an increase in the other. We conclude that to eliminate pollutant from the fluid, an increase in temperature might be useful.

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