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Computational Study of MHD Darcy–Forchheimer Hybrid Nanofluid Flow under the Influence of Chemical Reaction and Activation Energy over a Stretching Surface

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Abstract: The energy and mass transition through Newtonian hybrid nanofluid flow comprised of copper Cu and aluminum oxide (Al₂O₃) nanoparticles (nps) over an extended surface has been reported. The thermal and velocity slip conditions are also considered. Such a type of physical problems mostly occurs in symmetrical phenomena and are applicable in physics, engineering, applied mathematics, and computer science. For desired outputs, the fluid flow has been studied under the consequences of the Darcy effect, thermophoresis diffusion and Brownian motion, heat absorption, viscous dissipation, and thermal radiation. An inclined magnetic field is applied to fluid flow to regulate the flow stream. Hybrid nanofluid is created by the dispensation of Cu and Al_2O_3 nps in the base fluid (water). For this purpose, the flow dynamics have been designed as a system of nonlinear PDEs, which are simplified to a system of dimensionless ODEs through resemblance substitution. The parametric continuation method is used to resolve the obtained set of dimensionless differential equations. It has been noticed that the consequences of heat absorption and thermal radiation boost the energy transmission rate; however, the effect of suction constraint and Darcy-Forchhemier significantly diminished the heat transference rate of hybrid nanofluids. Furthermore, the dispersion of Cu and Al_2O_3 nps in the base fluid remarkably magnifies the velocity and energy transmission rate.

Keywords: hybrid nanofluid; slip condition; exponential stretching sheet; MHD; chemical reaction; PCM

1. Introduction

The analysis of the energy and mass communication through hybrid nanoliquid (hnf) across a vertical stretching surface has several implementations in various fields of biomedicine and industries [1]. Hamad et al. [2] used a mathematical approach to investigate the remarkable features of 2D Walters-B nanoliquid flows across a vertically stretching surface in which the substrate contains motile microbes. It was established that the viscoelastic component diminishes the mobility of the nanoliquid flow, but the velocity ratio factor greatly elevates the acceleration of the fluid. Wakif [3] developed a new method for estimating the steady hydromagnetic radiative flows of viscous fluids across a stretchy sheet that is non-uniformly elongating and has a nonhomogeneous thickness. Gangadhar et al. [4] presented a numerical analysis to examine the steady, 2D flow and



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Copyright: © 2022 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). heat transmission over an elongating sheet with varying suction/injection effects in the presence of Newtonian heating and a magnetic field. Algehyne et al. [5] studied the bioconvection that results from the micropolar fluid flow containing movable nanomaterials and microbes along a permeable vertical moving substrate. It was found that the energy transformation curve greatly improves when the Eckert number, Hartmann number, and heat absorption/generation. Gautam et al. [6] scrutinized the effects of binary reaction on the MHD 2D Williamson nano liquid's flow on an extending sheet with varying thickness immersed in a Darcy permeable medium. It was found that the rising trend of reaction rate variables rises the surface heat flux while lessening the mass flux. Rasool et al. [7] performed a numerical evaluation of MHD nanofluid flows in a Darcy permeable medium with a Riga pattern implanted diagonally. It was noted that the frictional component at the stretching sheet is strengthened by Lorentz's forces and Darcy–Forchheimer's. Zaib et al. [8] inspected the effects of entropy formation on Williamson nano liquid's stagnation point flow across a movable sheet. Asjad et al. [9] discussed the continuous flow of a hybrid nanoliquid that conducts an electric effect through a thin, impermeable stretchy sheet. The velocity curve has been found to improve when velocity power index and Hall current are present while decreasing when nanoparticle quantities and sheet thickness are present. Algehyne et al. [10] analyzed a critical viewpoint on the kinematics of water and aluminum based nanofluid across slippery circular geometries (for example, a hemispheric) related to the linear straining movement of the asymmetrical boundaries.

Relative to the traditional fluids employed for energy transference, such as water, ethylene glycol, oil, and nanofluids, hybrid nanocomposites operate well in terms of heat transport. Hybrid nanoliquids are effective at freezing areas with a vast range of temperatures and a variety of thermal activities. Hybrid nanofluids are a novel type of nanomaterials that are often created by disseminating two distinct forms of nps in conventional fluids [11–13]. Applications of hybrid nanocomposites in the fields of refrigeration, ventilation, heating, air conditioning, heat pipes, heat exchangers, coolants in metalworking and production, microelectronics, the auto sector, turbine cooling, transistor cooling, nuclear device, biomedicine, aircraft, and defense are among the foremost domains of study [14–16]. Reddy et al. [17,18] regulated the pulsatile hybrid nanoliquid circulation in a laterally porous irregular tube. It was found that as the ratios of body force variables are increased, the blood flow drops. Additionally, the blood circulation is faster for CuO nanoliquid than hybrid nanoliquid; nevertheless, for a smaller valuation of the frequency factor, the situation is precisely the contrary. Sun et al. [19] have developed the parametric analysis for the flow of the Darcy–Forchheimer CuO hybrid nanoliquid over a porous rotational disc using the parametric continuation method. Hybrid nanoliquid including copper (Cu) and aluminum oxide (Al_2O_3) nano particulates, where the viscosity and thermal conductivity vary non-uniformly with the volume percentage [20], studied the convective flow and energy transmission of various nanofluids. With a rise in Cu nanocomposites, the streams of Cu-C2H6O (copper-ethylene glycol) base nanoliquids showed the best improvement in the heat transference rate. Al-Mubaddel et al. [21] examined a hybrid ferrofluid flow through a heated, irregular, extensible cylinder at a 3D stagnation point with the impact of slip parameters and variable diameter. Alsallami et al. [22] have performed a numerical analysis of the nanoliquid flow under the effects of thermophoresis, Brownian motion, and thermal radiation on a warmed revolving surface. It was thought that the radiation and Prandtl number impact increased the frequency of heat transfer. Shahsavar et al. [23] considered the impact of magnetic flux and the Hall effect on hybrid nanoliquid flow on a gyrating disk's top. Their goal was to upsurge the efficiency of energy transport for use in engineering and industry. Ashraf et al. [24] used the generalized differential quadrature methodology to quantitatively investigate the peristaltic transport of magnetite Fe₃O₄ nanocrystals in blood-based ferrofluid.

The exploration of the electromagnetic characteristics and dynamics of electrically conducting fluids is known as magneto-fluid dynamics (MHD). These magneto fluids, which include plasmas, salt water, liquid metals, and electrolytes, are a few illustrations.

Hannes Alfvén founded the concept of MHD in 1970. The core idea driving MHD is that electromagnets can cause current flow in conducting fluids that are flowing, which polarizes the flow and modifies the magnetic field [25–27]. Ramaiah et al. [28] discussed the consequences of energy exchange in addition to the mass phenomena of an MHD Maxwell fluid in rotating flow across a vertical stretchable sheet. It was found that a solute's percentage in a compound depends on both the rotational constants and the activation energy. Riaz et al. [29] examined the dimensionless model of magnetic properties in a nanoliquid flow using basic symmetry when applied to a movable preheated vertical surface that is either flowing or static with the surface. Zeeshan et al. [30], Chen et al. [31], and Abbas et al. [32] investigated the MHD nanoliquids flow across two simultaneous vertical plates in a permeable media made of carbon nanotubes derived from engine oil. When relative to engine-oil MWCNTs, it is observed that the energy contour of the engine-oil SWCNTs significantly rises.

In the current investigation, we are analyzing the dynamics of Newtonian hybrid nanoliquid containing Cu and Al₂O₃ nanoparticles over an extending vertical surface with thermal and partial slip conditions. No such study and analysis have been found in the literature. The fluid flow has been studied under the consequences of the Darcy effect, thermophoresis diffusion and Brownian motion, heat absorption, viscous dissipation, and thermal radiation. An inclined magnetic field is applied to fluid flow to regulate the flow stream. Hybrid nanofluid is synthesized by the dispensation of Cu and Al₂O₃ nps in the blood. The PCM approach is used to resolve the obtained set of dimensionless differential equations.

2. Mathematical Formulation

The energy and mass transmission through two-dimension electrically conducting Darcy–Forchheimer Newtonian hybrid nanofluid flow across an extending sheet is considered. The consequences of thermal and velocity slip on the hybrid nanoliquid flow are also considered. An inclined magnetic strength B_0 is employed in the flow field as appeared in Figure 1. Here, the non-uniform inertia constraint stated as $F_0 = C_b / \sqrt{K^*}$ is the permeable media. The Cu and Al₂O₃ nps are dispersed into the base fluid for hybrid composition. C_λ and T_λ present the mass and energy of nanofluid, while C_∞ and T_∞ show the surrounding mass and energy. The basic equations are written as [33]:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0, \tag{1}$$

$$u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} = v_{hnf}\frac{\partial^2 u}{\partial y^2} - \frac{\sigma_{hnf}}{\rho_{hnf}}B_0^2 u\operatorname{Sin}^2(\theta) - \frac{v_{hnf}}{K^*}u - \frac{1}{\rho_{hnf}}F_0u^2 + g\left(\frac{(\rho\beta_T)_{hnf}}{\rho_{hnf}}(T - T_\infty)\right),\tag{2}$$

$$u\frac{\partial T}{\partial x} + v\frac{\partial T}{\partial y} = \alpha_{hnf}\frac{\partial^2 T}{\partial y^2} - \frac{1}{(\rho C_p)_{hnf}}\frac{\partial q_r}{\partial y} + \frac{\mu_{hnf}}{(\rho C_p)_{hnf}}\left(\frac{\partial u}{\partial y}\right)^2 - \frac{H_0}{(\rho C_p)_{hnf}}(T - T_\infty) + \frac{\sigma_{hnf}}{(\rho C_p)_{hnf}}$$

$$B_0^2 u^2 \mathrm{Sin}^2(\theta) + \tau \left(D_B\frac{\partial T}{\partial y}\frac{\partial C}{\partial y} + \frac{D_T}{T_\infty}\left(\frac{\partial T}{\partial y}\right)^2\right),$$
(3)

$$u\frac{\partial C}{\partial x} + v\frac{\partial C}{\partial y} = D_B \frac{\partial^2 C}{\partial y^2} + \frac{D_T}{T_{\infty}} \left(\frac{\partial^2 T}{\partial y^2}\right) - k_r^2 (C - C_0) \left(\frac{T}{T_{\infty}}\right)^n \exp\left(-\frac{E_a}{\kappa T}\right).$$
(4)



Figure 1. The hybrid nanoliquid flow over a stretching sheet.

The *u* and *v* are the velocity terms in the *x*, *y* direction. Here, $c = \delta = 0$ is the no-slip conditions, while $\varepsilon_1(x) = \varepsilon_0 e^{x/l}$, $c = c_1/e^{x/2l}$, and $\delta = \delta_1/e^{x/2l}$ are the sheet stretching velocity, velocity slip, and thermal slip, respectively. c_1 and δ_1 signify the initial velocity and thermal slip, and H_0 is the heat absorption constant, while $\varepsilon_2(x) = v_0 e^{x/2l}$ is the suction/injection effect. The term $k_r^2(C - C_0) \left(\frac{T}{T_{\infty}}\right)^n \exp\left(-\frac{E_a}{\kappa T}\right)$ in Equation (4) denotes the modified Arrhenius equation in which *Ea* is the activation energy, k_r^2 is the reaction rate, $\kappa = 8.61 \times 10^{-5} \text{ eV/K}$ is the Boltzmann constant, and *n* is the fitted rate constant, which generally lies in the range -1 < n < 1.

The radiative heat flux is inscribed as [33]:

$$q_r = \frac{-4\sigma^*}{3k^*} \frac{\partial T^4}{\partial y},\tag{5}$$

By executing Taylor's series and disregarding the higher order term:

$$T^4 \cong T^3 (4T - 3T_\infty) \tag{6}$$

By putting Equation (5) in Equation (3), we have:

$$u\frac{\partial T}{\partial x} + v\frac{\partial T}{\partial y} = \left(\alpha_{hnf} + \frac{16T_{\infty}^{3}\sigma^{*}}{3(\rho C_{p})_{hnf}k^{*}}\right)\frac{\partial^{2}T}{\partial y^{2}} + \frac{\mu_{hnf}}{(\rho C_{p})_{hnf}}\left(\frac{\partial u}{\partial y}\right)^{2} - \frac{H_{0}}{(\rho C_{p})_{hnf}}(T - T_{\infty}) + \frac{\sigma_{hnf}}{(\rho C_{p})_{hnf}}B_{0}^{2}u^{2}\operatorname{Sin}^{2}(\theta) + \tau\left(D_{B}\frac{\partial T}{\partial y}\frac{\partial C}{\partial y} + \frac{D_{T}}{T_{\infty}}\left(\frac{\partial T}{\partial y}\right)^{2}\right)$$
(7)

The initial and boundary conditions are [33]:

$$u = \varepsilon_1(x) + c\mu_{hnf} \frac{\partial u}{\partial y}, \quad v = \varepsilon_2(x), \quad C = C_\lambda(x), \quad T = T_\lambda(x) + \delta \frac{\partial T}{\partial y} \right\} \text{ at } y = 0$$
(8)

$$u \to 0, v \to 0, C \to C_{\infty}, T \to T_{\infty} \text{ as } y \to \infty.$$
 (9)

The experimental values of Cu, Al₂O₃, and blood are described in Table 1. In Table 2, the *bf* and *hnf* characterize the base fluid and hybrid nanofluid. $\phi_{Al_2O_3}$ and ϕ_{Cu} represent the nano particulates volume fraction. σ_{hnf} is the electrical conductivity, $(\rho C_p)_{hnf}$ is the heat capacitance, and k_{hnf} is the thermal conductivity of the hybrid nanoliquid.

Table 1. The tentative numerical values of Cu, Al₂O₃, and water [34].

	${oldsymbol ho}({f kg}/{f m}^3)$	$C_p(\mathbf{j/kgK})$	k(W/mK)	σ (S/m)
Water	997.1	4179	0.613	-
Cu	8933	385	401	$59.6 imes 10^6$
Al ₂ O ₃	4907	765	40	$35 imes 10^6$

Table 2. The mathematical model for the hybrid nanoliquid $(\phi_1 = \phi_{Cu}, \phi_2 = \phi_{Al_2O_3})$ [35].

Properties	Models		
Viscosity	$rac{\mu_{hnf}}{\mu_{bf}} = rac{1}{\left(1 - \phi_{Cu} - \phi_{Al_2O_3} ight)^2}$		
Density	$\frac{\rho_{lmf}}{\rho_{bf}} = \phi_{Cu} \left(\frac{\rho_{Cu}}{\rho_{bf}} \right) + \phi_{Al_2O_3} \left(\frac{\rho_{Al_2O_3}}{\rho_{bf}} \right) + \left(1 - \phi_{Cu} - \phi_{Al_2O_3} \right)$		
Thermal Capacity	$\frac{(\rho C_p)_{hnf}}{(\rho C_p)_{bf}} = \phi_{Cu} \left(\frac{(\rho C_p)_{Cu}}{(\rho C_p)_{bf}} \right) + \phi_{Al_2O_3} \left(\frac{(\rho C_p)_{Al_2O_3}}{(\rho C_p)_{bf}} \right) + \left(1 - \phi_{Cu} - \phi_{Al_2O_3} \right)$		
Thermal Expansion	$\frac{(\rho\beta_T)_{lnf}}{(\rho\beta_T)_{bf}} = \phi_{Cu} \left(\frac{(\rho\beta_T)_{Cu}}{(\rho\beta_T)_{bf}} \right) + \phi_{Al_2O_3} \left(\frac{(\rho\beta_T)_{Al_2O_3}}{(\rho\beta_T)_{bf}} \right) + \left(1 - \phi_{Cu} - \phi_{Al_2O_3} \right)$		
Thermal Conductivity	$\frac{k_{lnnf}}{k_{bf}} = \left[\frac{\left(\frac{\phi_{Cu}k_{Cu} + \phi_{Al_2O_3}k_{Al_2O_3}}{\phi_{Cu} + \phi_{Al_2O_3}}\right) + 2k_{bf} + 2(\phi_{Cu}k_{Cu} + \phi_{Al_2O_3}k_{Al_2O_3}) - 2(\phi_{Cu} + \phi_{Al_2O_3})k_{bf}}{\left(\frac{\phi_{Cu}k_{Cu} + \phi_{Al_2O_3}k_{Al_2O_3}}{\phi_{Cu} + \phi_{Al_2O_3}}\right) + 2k_{bf} - 2(k_{Cu}\phi_{Cu} + k_{Al_2O_3}\phi_{Al_2O_3}) + 2(\phi_{Cu} + \phi_{Al_2O_3})k_{bf}}\right]$		
Electrical Conductivity	$\frac{\sigma_{lnnf}}{\sigma_{bf}} = \left[\frac{\left(\frac{\phi_{Cu}\sigma_{Cu}+\sigma_{Al_2O_3}\phi_{Al_2O_3}}{\phi_{CoF_2O_4}+\phi_{Cu}}\right) + 2\sigma_{bf} + 2(\phi_{Cu}\sigma_{Cu}+\phi_{Al_2O_3}\sigma_{Al_2O_3}) - 2(\phi_{Cu}+\phi_{Al_2O_3})\sigma_{bf}}{\left(\frac{\phi_{Cu}\sigma_{Cu}+\phi_{Al_2O_3}\sigma_{Al_2O_3}}{\phi_{Cu}+\phi_{Al_2O_3}}\right) + 2\sigma_{bf} - (\phi_{Cu}\sigma_{Cu}+\phi_{Al_2O_3}\sigma_{Al_2O_3}) + (\phi_{Cu}+\phi_{Al_2O_3})\sigma_{bf}}\right]$		

The similarity variables are [33]:

$$u = \frac{\partial \varphi}{\partial y} = \frac{Re v_f}{l} e^{x/l} f'(\eta), \quad \eta(x,y) = (Re)^{1/2} e^{x/2l} \left(\frac{y}{\sqrt{2l}}\right), \quad v = -\frac{\partial \varphi}{\partial x} = \frac{-v_f (2Re)^{1/2}}{l} (f(\eta) + \eta f'(\eta)) e^{x/2l}, \\ \psi(x,y) = v_f e^{x/2l} (2Re)^{1/2} f(\eta), \quad C(x,y) = C_{\infty} - (C_{\infty} - C_0) e^{bx/2l} \Phi(\eta), \quad T(x,y) = T_{\infty} - (T_{\infty} - T_0) e^{ax/2l} \Theta(\eta). \end{cases}$$
(10)

By putting Equation (10) in Equations (1)–(4):

$$f'''(\eta) + \frac{\rho_{hnf}/\rho_{bf}}{\mu_{hnf}/\mu_{bf}} \left[f''(\eta)f(\eta) - 2f'(\eta)^2 \right] - \frac{1}{\mu_{hnf}/\mu_{bf}} \begin{pmatrix} 2e^{-\chi} \mathrm{Sin}^{2\theta} \frac{\sigma_{hnf}}{\sigma_{bf}} Mf'(\eta) \\ + 2Frf'(\eta)^2 + \frac{(\rho\beta_T)_{hnf}}{(\rho\beta)_{bf}} Gr\Theta(\eta) \end{pmatrix} - 2\xi f'(\eta) = 0,$$

$$(11)$$

$$\frac{1}{Pr} \left(\frac{k_{hnf}}{k_{bf}} + Tb\right) \Theta''(\eta) + \left(\frac{\mu_{hnf}}{\mu_{bf}} e^{\chi} f''(\eta)^2 + \frac{\sigma_{hnf}}{\sigma_{bf}} 2M \mathrm{Sin}^2 \theta f'(\eta)^2 \right) Ece^{(2-a)\chi} + \frac{(\rho C_p)_{hnf}}{(\rho C_p)_{bf}}$$

$$(a\Theta(\eta)f'(\eta) - f(\eta)\Theta'(\eta)) + 2Hae^{-\chi}\Theta(\eta) + Nb\Theta'(\eta)\Phi'(\eta) + Nt\Theta'(\eta)^2 = 0,$$
(12)

$$\Phi''(\eta) + Sc\left(f(\eta)\Phi'(\eta) - bf'(\eta)\Phi(\eta) - Kr(1+\varepsilon\delta)^n\varphi \exp\left(-\frac{E}{1+\varepsilon\delta}\right)\right) + \frac{Nt}{Nb}\Theta''(\eta) = 0$$
(13)

The transmute conditions are:

$$f'(\eta) = L^* f''(\eta) + 1, \ f(\eta) = S, \ \Theta(\eta) = d^* \Theta'(\eta) + 1, \ \Phi(\eta) = 1 \text{ at } \eta = 0$$

$$f'(\eta) \to 0, \ \Theta(\eta) \to 0, \ \Phi(\eta) \to 0 \text{ at } \eta \to \infty$$
(14)

Here, M, χ , Tb, Sc, Nt, K, Re, Ec, Ha, and L is the magnetic term, non-dimensional coordinate, thermal radiation, Schmidt number, chemical reaction, Reynold number, Eckert number, heat source, and velocity slip, respectively, while, Gr, S, ξ , Fr, Pr, Nb, and E are the Grashof number, injection/suction, porosity term, Forchheimer term, Brownian motion, and activation energy, respectively.

$$M = \frac{(B_0 l)^2 \sigma_f}{\mu_{bf} Re}, \quad \chi = \frac{x}{l}, \quad Tb = \frac{16}{3} \frac{T_{\infty}^3 \sigma^*}{k_{bf} k^*}, \quad Sc = \frac{\nu_f}{D_B}, \quad Nt = \frac{(T_0 - T_{\infty})D_T \tau e^{\chi \frac{h}{2}}}{T_{\infty} \nu_{bf}}, \quad K_c = \frac{e^{-\chi} K_0 l^2}{Re \nu_{bf}}, \quad Re = \frac{l\epsilon_0}{\nu_{bf}}, \quad Ec = \frac{\epsilon_0^2}{(C_p)_{bf} (T_0 - T_{\infty})}, \quad Ha = \frac{H_0 l^2}{(\rho C_p)_{bf} \nu_{bf} Re}, \quad L = \frac{\nu_{hnf} c_1}{l} \sqrt{\frac{Re}{2}}, \quad Gr = \frac{(\rho \beta_T)_{bf} (T_0 - T_{\infty}) e^{\chi (\frac{h}{2} - 2)} g l^3}{\mu_{bf} \nu_{bf} Re^2}, \quad D = \frac{\delta_1}{l} \sqrt{\frac{Re}{2}}, \quad S = \frac{l\nu_0}{\nu_{bf}} \sqrt{\frac{2}{Re}}, \quad \xi = \frac{l^2 e^{-\chi}}{Re K^*}, \quad Fr = \frac{F_0 l}{\rho_{bf}}, \quad Pr = \frac{(\rho C_p \nu)_f}{k_{bf}}, \quad Nb = \frac{(C_0 - C_{\infty})D_B \tau e^{\chi \frac{h}{2}}}{\nu_{bf}}, \quad E = \frac{E_a}{\kappa T_{\infty}}.$$

The physical interest quantities are revealed as:

$$Nu_x = \frac{x\tau_w}{k_{bf}(T_\lambda - T_\infty)}, Sf_x = \frac{f_w}{\varepsilon_1^2 \rho_{bf}} \text{ and } Sh_x = \frac{xj_w}{D_{hnf}(C_\lambda - C_\infty)}$$
(16)

where $f_w = \mu_{hnf} \left(\frac{\partial u}{\partial y}\right)_{y=0}$, $\tau_w = -k_{hnf} \left(\frac{\partial T}{\partial y}\right)_{y=0} + (q_r)_{y=0}$, and $j_w = -D_B \left(\frac{\partial C}{\partial y}\right)_{y=0}$ are the surface heat flux, wall shear stress, and wall mass flux.

The non-dimensional form of Equation (16) is:

$$Sf_{x} = \frac{\mu_{hnf}}{\mu_{bf}} \frac{1}{\sqrt{2Re_{x}}} f''(0), \ Nu_{x} = -\left(\frac{k_{hnf}}{k_{bf}} + Tb\right) \sqrt{\frac{\chi Re_{x}}{2}} \Theta'(0), \ Sh_{x} = \Phi'(0).$$
(17)

3. Numerical Solution

The fundamental steps involved in the PCM solution methodology, while dealing with the system of ODEs (11–13), are the following [36,37]:

Step 1: Convert BVP to first order

$$\hbar_1 = f(\eta), \ \hbar_2 = f'(\eta), \ \hbar_3 = f''(\eta), \ \hbar_4 = \Theta(\eta), \ \hbar_5 = \Theta'(\eta), \ \hbar_6 = \Phi(\eta), \ \hbar_7 = \Phi'(\eta).$$
 (18)

By putting (18) in Equations (11)–(14), we obtain:

$$\hbar'_{3} + \frac{\rho_{hnf}/\rho_{f}}{\mu_{hnf}/\mu_{f}} \left(\hbar_{3}\hbar_{1} - 2\hbar_{2}^{2}\right) - \frac{1}{\mu_{hnf}/\mu_{f}} \left(\begin{array}{c} 2e^{-\chi}\mathrm{Sin}^{2}\theta \frac{\partial_{hnf}}{\sigma_{f}}M\hbar_{2}\\ +2Fr\hbar_{3}^{2} + \frac{(\rho\beta_{T})_{hnf}}{(\rho\beta)_{f}}Gr\hbar_{4} \end{array}\right) - 2\xi\hbar_{2} = 0, \quad (19)$$

$$\frac{1}{Pr} \left(\frac{k_{hnf}}{k_f} + Tb\right) \hbar'_5 + \left(\frac{\mu_{hnf}}{\mu_f} e^{\chi} \hbar_3^2 + \frac{\sigma_{hnf}}{\sigma_f} 2M \text{Sin}^2 \theta \hbar_2^2\right) Ec \, e^{(2-a)\chi} + \frac{(\rho C_p)_{hnf}}{(\rho C_p)_f} \tag{20}$$

$$(a\hbar_4\hbar_2 - \hbar_1\hbar_5) + 2Hae^{-\chi}\hbar_4 + Nb\hbar_5\hbar_7 + Nt\hbar_5^2 = 0,$$

$$\hbar'_7 + Sc\left(\hbar_1\hbar_7 - b\hbar_2\hbar_6 - Kr(1+\varepsilon\delta)^n\varphi \exp\left(-\frac{E}{1+\varepsilon\delta}\right)\right) + \frac{Nt}{Nb}\hbar'_5 = 0$$
(21)

The transform conditions are:

$$\begin{split} &\hbar_2 = L^* \hbar_3 + 1, &\hbar_1 = S, \ \hbar_6 = 1 \text{ and } \hbar_4 = d^* \hbar_5 + 1 \ \text{at} \ \eta = 0 \\ &\hbar_2 \to 0, \ \hbar_6 \to 0 \ \text{and} \ \hbar_4 \to 0 \ \text{at} \ \eta \to \infty \end{split}$$
(22)

Step 2: Introducing parameter p:

$$\hbar'_{3} + \frac{\rho_{hnf}/\rho_{f}}{\mu_{hnf}/\mu_{f}} \left((\hbar_{3} - 1)p\hbar_{1} - 2\hbar_{2}^{2} \right) - \frac{1}{\mu_{hnf}/\mu_{f}} \left(\begin{array}{c} 2e^{-\chi} \mathrm{Sin}^{2}\theta \,\frac{\sigma_{hnf}}{\sigma_{f}} \,M\hbar_{2} \\ +2Fr\hbar_{3}^{2} + \frac{(\rho\beta_{T})_{hnf}}{(\rho\beta)_{f}} \,Gr\hbar_{4} \end{array} \right) - 2\xi\hbar_{2} = 0, \tag{23}$$

$$\frac{1}{Pr} \Big(\frac{k_{hnf}}{k_f} + Tb \Big) \hbar'_5 + \Big(\frac{\mu_{hnf}}{\mu_f} e^{\chi} \hbar_3^2 + \frac{\sigma_{hnf}}{\sigma_f} 2M \mathrm{Sin}^2 \theta \hbar_2^2 \Big) Ec \, e^{(2-a)\chi} + \frac{(\rho C_p)_{hnf}}{(\rho C_p)_f}$$
(24)
$$(a\hbar_4\hbar_2 - \hbar_1(\hbar_5 - 1)p) + 2Hae^{-\chi} \hbar_4 + Nb\hbar_5\hbar_7 + Nt\hbar_5^2 = 0,$$

$$\hbar'_7 + Sc\left(\hbar_1(\hbar_7 - 1)p - b\hbar_2\hbar_6 - Kr(1 + \varepsilon\delta)^n\varphi \exp\left(-\frac{E}{1 + \varepsilon\delta}\right)\right) + \frac{Nt}{Nb}\hbar'_5 = 0$$
(25)

Step 3: Apply Cauchy Principal and Discretized Equations (23)-(25).

After discretization, the obtained set of equations is computed through the MATLAB code of PCM.

4. Results and Discussion

This segment assesses the physical scenario behind each table and Figure. The following observations have been noted while keeping all the parameters' values as Fr = 0.2, M = 0.1, $S = \pm 0.1$, Nt = 0.4, Nb = 0.5, Ha = 0.2, Ec = 0.01, d = 0.4, Fr = 0.2, Sc = 0.1, and Kr = 0.3.

Velocity Profile $(f'(\eta))$:

Figure 2a–d revealed the outlines of fluid velocity versus the upshot of Forchhemier number *Fr*, magnetic field *M*, suction effect +*S*, and injection –*S*, respectively. Figure 2a presents the relation of velocity $f'(\eta)$ curve versus the Forchheimer parameter *Fr* for both cases, no-slip (L = 0.5) and slip (L = 0) conditions of the hybrid nanoliquid. The rising values of *Fr* lessen the velocity outline. Physically, the increment of *Fr* produced inertial drag force, which is a barrier to the velocity field $f'(\eta)$; hence as a result, the velocity profile decelerates. Figure 2b expresses the exhibition of velocity contour versus the magnetic constraint *M*. It was noted that with the rising values of *M*, the velocity profile $f'(\eta)$ declines, because the Lorentz force created due to magnetic flux resists the fluid velocity. Figure 2c,d are drafted to indicate the impact of (S > 0) and (S < 0) on the velocity outline. Both illustrate a contradictory performance versus velocity curve. The kinetic viscosity has an inverse relation with the suction/injection parameters, so the rising effect of *S* diminishes the viscosity of the fluid and vice versa. Furthermore, physically the suction effect also resists the fluid field; as a result, such a scenario has been observed in Figure 2c,d.

Energy Profile $\Theta(\eta)$:

Figure 3a-d exemplified the demonstration of energy profile versus the upshot of suction term +S, injection -S, Nt, and Nb, respectively. Figure 3a,b are drawn to display the upshot of suction (S > 0) and injection constraints (S < 0) on the energy profile $\Theta(\eta)$. For mounting values of (S > 0), the energy curve is reduced, while it augments with the effects of the injunction parameter. As discussed earlier, the kinetic viscosity has an inverse relation with the suction/injection parameters, so the rising effect of S diminishes the viscosity of the fluid and vice versa. Furthermore, physically, the suction/injection effect also resists the fluid field, and that fractional force produces an additional heat, which enhances the energy contour as detected in Figure 3a,b. Figure 3c is calculated to observe the nature of *Nt* on the energy $\Theta(\eta)$ profile. It is noted that the energy curve $\Theta(\eta)$ boosts with the flourishing values of Nt. The temperature change occurred due to the upshot of Nt, which causes the reduction in kinetic viscosity of the fluid, and as a result, energy contour augments $\Theta(\eta)$. Figure 3d is drawn to reveal the consequences of Nb versus the temperature outline $\Theta(\eta)$. The molecular diffusion enhances with the rising effect of *Nb*, while the kinetic viscosity of fluid declines with the influence of Brownian motion, as a result, the energy contour augments $\Theta(\eta)$.



Figure 2. Velocity profile versus the upshot of (a) Forchhemier number Fr, (b) magnetic field M, (c) suction effect +*S*, and (d) injection -S.



Figure 3. Energy profile versus the upshot of (a) suction +S, (b) injection -S, (c) thermophoresis Nt, and (d) Brownian motion Nb.

Figure 4a reveals the relation of the magnetic effect *M* versus the energy outline $\Theta(\eta)$. It can be realized that the growing values of *M* augment the $\Theta(\eta)$. Physically, the enhancement of *M* fashions a resistance force (Lorentz Force), which opposes the flow path, and that resistive effect also generates heat; as a result, the energy contour boosts.



Figure 4. Energy profile versus the upshot of (**a**) magnetic field, (**b**) heat source term, (**c**) Eckert number, and (**d**) thermal slip factor *d*.

Figure 4b illustrates the influence of heat source *Ha* on the energy outline $\Theta(\eta)$. It is noticed that the energy contour decreases with the upshot of *Ha*. Physically, the improving worth of *Ha* suggestively rises the heat capacity of the fluid, and thus energy contour drops. Figure 4c shows the relation of energy contour versus *Ec*. It can be perceived that the augmentation in *Ec* drops the $\Theta(\eta)$. Physically, *Ec* is the relation between kinetic energy and enthalpy generation; therefore, the influence of *Ec* diminishes the viscous fluid stresses by decoding kinetic energy to internal energy, as a result, the energy field $\Theta(\eta)$ becomes improved. The upshot of the thermal slip factor *d* versus $\Theta(\eta)$ is presented in Figure 4d.

Concentration Profile:

Figure 5a–e displays the nature of the mass profile versus the upshot of Schmidt number *Sc*, chemical reaction *Kr*, *Nt*, *Nb*, and Arrhenius activation energy *E*, respectively. Figure 5a displays that the growing values of the number *Sc* weakens the concentration field. The molecular diffusion declines, while the kinetic viscosity of fluid augments with the upshot of *Sc*, which results in the diminution of mass profile. Figure 5b represents the nature of concentration gradients as a function versus chemical reaction. It is revealed that the cumulative trend of the chemical reaction factor lessens the concentration contour.

Figure 5c,d are drafted to elaborate on the behavior of Nt and Nb on the mass transmission $\Phi(\eta)$ profile. From Figure 5c,d, it is observed that the mass contour is enhanced due to the rising tendency of Nt, while it decreases with the influence of Nb. Figure 5e reveals that the mass curve significantly boosts with the influence of Arrhenius activation energy.



Figure 5. Mass profile versus the upshot of (**a**) Schmidt number *Sc*, (**b**) chemical reaction *Kr*, (**c**) thermophoresis Nt, (**d**) Brownian motion Nb, and (**e**) activation energy *E*.

Figure 6 expresses the percentage relative valuation between nanoliquid (Cu or Al_2O_3) and hybrid nanoliquid (Cu + Al_2O_3) for both energy and velocity profiles. It can be observed that as compared to nanofluids, the hybrid nanofluid has a remarkable capability of energy transmission.



Figure 6. Percentage comparison between nanoliquid and hybrid nanoliquid.

Tables 3–5 exhibit the relative statistical assessment between hybrid and simple nanoliquid for skin friction Sf_x , Nusselt number Nu_x , and Sherwood number Sh_x , respectively. In both cases, slip L = 0 and non-slip L = 0.4 phenomena have been studied for analysis. It is observed from Figure 3 that the rising credit of magnetic effect and Grashof number enhances the drag force. Figure 4 reports that the flourishing values of Brownian motion and thermophoresis effect diminish the Nusselt number. On other hand, the Sherwood magnifies with the increment of Schmidt number and chemical reaction. Table 5 also presents the comparison of present outcomes with another numerical technique bv4c package for the validity purpose of the results. Both the methods show the best settlement with each other, so it can be perceived that the results are reliable and accurate. Table 6 expressed the comparative analysis of present work with the existing literature. It can be observed that the present outcomes are reliable and accurate.

Param	Parameters		<i>Sf_x</i> for <i>L</i> =0	
М	Gr	$Cu + Al_2O_3$	Cu	$Cu + Al_2O_3$
0.2	0.1	1.136841	1.004931	0.576080
0.4		1.189545	1.048340	0.649375
0.6		1.173506	1.219533	0.714397
0.8		1.395022	1.225452	0.832752
0.2	0.1	1.136841	1.00493	0.576070
	0.5	1.209421	1.135243	0.607352
	0.7	1.298434	1.207564	0.653641
	0.9	1.370320	1.319647	0.787528

Table 3. Numerical outputs of Skin friction Sf_x for slip and no-slip L = 0 conditions.

Parameters		Nu_x for L=0		Nu_x for L=0.4	
Nt	Nb	$Cu + Al_2O_3$	Cu	$Cu + Al_2O_3$	
0.1	0.2	1.358318	1.327615	1.433756	
0.2		1.285501	1.073557	1.386492	
0.3		0.784536	0.574744	0.874617	
0.4		0.567454	0.539545	0.612644	
0.1	0.2	1.358318	1.327615	1.433756	
	0.4	1.164950	1.009444	1.294688	
	0.6	1.068312	1.007518	1.173574	
	0.8	0.863593	0.719485	1.021634	

Table 4. Numerical outputs of Nusselt number Nu_x for slip, L = 0.4, and no-slip, L = 0, conditions.

Table 5. Comparative analysis of Sherwood number (Sh_x) for no-slip (L = 0) conditions between PCM and bvp4c package.

Parameters		bvp4c		РСМ	
Sc	Kr	$Cu + Al_2O_3$	Cu	$Cu + Al_2O_3$	Cu
0.3	0.4	2.596400	2.395722	2.595512	2.396730
0.6		2.638758	2.485473	2.647455	2.486474
0.9		2.784748	2.684288	2.774682	2.685287
1.2		3.052195	2.806367	3.050756	2.807366
0.3	0.4	2.596400	2.395722	2.595512	2.396721
	0.8	2.707473	2.695367	2.735074	2.697366
	1.2	2.875394	2.799536	3.878335	2.887535
	1.6	3.357847	3.064456	3.346754	3.065455

Table 6. Comparative analysis of present work with the existing literature.

Parameters		$-Sf_x$ (Ref. [33])		$-Sf_x$ (Present Work)	
М	θ	L = 0	L = 0.5	L = 0	L = 0.5
0.2	$\pi/3$	0.984548	0.566347	0.984559	0.566368
1.2		1.117289	0.626290	1.117297	0.626381
2.2		1.235613	0.674850	1.235622	0.674862
3.2		1.343110	0.715361	1.343131	0.715373
	$\pi/6$	1.057414	0.599995	1.057437	0.599999
	$\pi/4$	1.150075	0.640188	1.150082	0.640194
	$\pi/3$	1.235613	0.674850	1.235634	0.674861
	$\pi/3$	1.315349	0.705207	1.315357	0.705226

5. Conclusions

The present analysis reported the energy and mass conversion through Newtonian hybrid nanoliquid flow consisting of Cu and Al_2O_3 nps over an extended surface. The thermal and velocity slip conditions are also considered. Hybrid nanofluid is created by the inclusion of Cu and Al_2O_3 nps in the water. The key findings are:

- The velocity contour $f'(\eta)$ of a hybrid nanofluid is diminished by enriching the magnetic field's angle and effect while boosting the energy profile $\Theta(\eta)$.
- The velocity and energy profiles enhance by the intensification of injection constraint, while the Darcy–Forchheimer impact and suction term have an opposite influence on both outlines.
- The thermal profile of hybrid nanofluid increased by rising the thermal effects, heat source, and viscous dissipation, while diminished by varying the thermal slip factor.
- Heat absorption and thermal radiation contributions boost the energy transmission rate, and the thermal slip factor increases the thermal profile.
- The dispersion of Cu and Al₂O₃ nps in the base fluid remarkably magnifies the velocity and energy transmission rate, which is the most tremendous property of Cu and Al₂O₃ nps, used for biomedical and industrial applications.

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Abbreviations

х, у	Cartesian coordinate (m)	и, v	Components of velocity
Т	Temperature (k)	$\varepsilon_1(x)$	Stretching velocity (ms^{-1})
$T_1(x)$	Exponential temperature	θ	Angle (<i>rd</i>)
С	Slip velocity factor	δ	Thermal slip factor
H_0	Heat source (J)	$\varepsilon_2(x)$	Suction velocity
ν	Kinematic viscosity $(m^2 s^{-1})$	μ	Dynamic viscosity $(kgm^{-1}s^{-1})$
ρ	Density (kg/m^3)	σ	Electrical conductivity (S/m^{-1})
B_0	Magnetic field (A/m^{-1})	α	Thermal diffusivity $(m^2 s^{-1})$
(ρc)	Heat capacity $(Jkg^{-1}k^{-1})$	k	Thermal conductivity $(wm^{-1}k^{-1})$
ζ	Porosity parameter	T_{∞}	Ambient temperature (k)
Fr	Forchhemier term	Gr	Grashof number
S	Suction/injection	d	Thermal slip
L	Velocity slip	Ec	Eckert number
Pr	Prandtl number	Re	Reynold number
M	Magnetic factor	Ra	Radiation factor
Ha	Heat absorption	f	Velocity profile

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