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## Contact effects in high performance fully printed p-channel organic thin film transistors

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Contact effects have been investigated in fully printed p-channel organic thin film transistors with field effect mobility up to  $2 \text{ cm}^2/\text{Vs}$ . Electrical characteristics of the organic thin film transistors, with channel length  $<200 \mu\text{m}$ , are seriously influenced by contact effects with an anomalous increase of the contact resistance for increasing source-drain voltage. Assuming that contact effects are negligible in long channel transistors and using gradual channel approximation, we evaluated the current-voltage characteristics of the injection contact, showing that I-V characteristics can be modeled as a reverse biased Schottky diode, including barrier lowering induced by the Schottky effect. © 2011 American Institute of Physics. [doi:10.1063/1.3669701]

The electrical characteristics of organic thin film transistors (OTFTs) are frequently affected by contact effects, which can seriously influence the transistor performance. This is because the “parasitic” voltage drop at the contacts reduces the effective drain-source bias voltage applied to the intrinsic channel of the transistor and, consequently, reduces the device current. Measured contact resistances in OTFTs show a wide range of variation, from few  $\text{k}\Omega\text{cm}$  up to  $10 \text{ M}\Omega\text{cm}$ ,<sup>1–12</sup> depending upon device configuration, metal contacts,<sup>1–3</sup> and the use of self-assembled monolayers<sup>5,6</sup> to control the metal/organic semiconductor work function difference. In particular, contact resistance appears to be strongly influenced by the device architecture, and much higher values are typically observed in coplanar structures (also known as bottom gate bottom contact) than in staggered structures.<sup>3,4,7,8,12</sup> The importance of the contact resistance is more relevant at large carrier mobility and/or small channel length, where its value may become comparable to, or even larger than, the channel resistance. In general, when scaling the channel length, the condition of comparable on-state channel resistance and contact resistance is encountered at a critical channel length,  $L_c$ , and the devices with channel lengths shorter than  $L_c$  can be seriously affected by these contact effects, thus preventing the beneficial aspects of device downscaling on the driven current.

In this work, we have studied contact effects in high performance fully printed p-channel OTFTs, to establish the downscaling limitations as well as to characterize and model the contact resistance in such devices.

P-channel OTFTs, with staggered top-gate configuration, were fabricated at CEA-LITEN, using printing processes<sup>13</sup> on heat stabilized, low roughness polyethylenenaphthalate PEN foils ( $125 \mu\text{m}$  thick). The source and drain gold contacts were defined by laser ablation (minimum channel length  $L = 5 \mu\text{m}$ ). The p-type semiconductor is a solution

processed 6,13-bis(triisopropyl-silylethynyl) pentacene derivative and could be deposited by different techniques such as spin coating or screen printing. The fluoropolymer gate dielectric ( $1.2 \mu\text{m}$  thick) and the Ag gate electrode are both deposited by screen printing. All curing steps are kept below  $100^\circ\text{C}$ , to be compatible with the PEN substrate limitation. After its proper annealing, the small-molecules solution-processed semiconductor is observed to form crystallites, which enhances the carrier mobility. The fabricated OTFTs have a multifinger structure with different channel lengths  $L$  (from  $5$  to  $200 \mu\text{m}$ ) and channel widths  $W$  (from  $100$  to  $2000 \mu\text{m}$ ). From the transfer characteristics measured at low  $V_{ds}$  on long channel devices, as shown in Fig. 1, we deduced typical field effect mobility,  $\mu_{FE}$ , in the range  $1.4$ – $2 \text{ cm}^2/\text{Vs}$ , a threshold voltage,  $V_T$ , between  $-10 \text{ V}$  and  $-15 \text{ V}$  and a subthreshold swing,  $S$ , of  $5$ – $7 \text{ V}/\text{dec}$ . Field effect mobility evaluated from saturated transfer characteristics,  $\mu_{sat}$ , is in the range  $0.9$ – $1.4 \text{ cm}^2/\text{Vs}$ . The output characteristics, reported in Fig. 2, show linear behavior at low  $|V_{ds}|$ , suggesting a low contact resistance, in agreement to what has been already observed in staggered OTFTs.<sup>4</sup> In order to test if the electrical characteristics follow the conventional square-law equation, we have plotted in Fig. 1 the normalized drain current,  $I_d/V_{ds}$ , vs  $V_g - V_{ds}/2$  for transistors with different channel lengths. In the case of a long channel ( $L = 200 \mu\text{m}$ ) device, the normalized transfer characteristics measured at different  $V_{ds}$  are perfectly superposed (see Fig. 1 panel (a)), confirming that the electrical characteristics follow the square-law theory. On the other hand, scaling down the transistor channel length (i.e.,  $L = 10 \mu\text{m}$ ), the normalized drain current shows substantial departure from the expected behavior. We have also tested the applicability of gradual channel approximation (GCA) by comparing the measured output characteristics of devices with different channel lengths, with the following equation:

$$I_d = \frac{W}{L} \int_{V_{gs}-V_{ds}}^{V_{gs}} G(V) dV, \quad (1)$$

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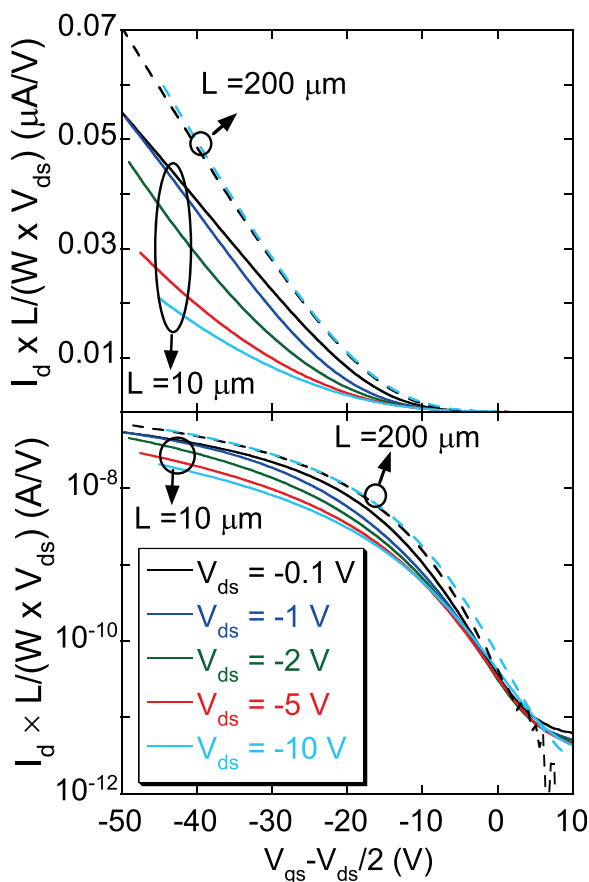


FIG. 1. (Color online) Normalized transfer characteristics of long ( $L = 200 \mu\text{m}$ , dashed lines) and short ( $L = 10 \mu\text{m}$ , solid lines) channel OTFTs measured at different drain voltages.

where  $G(V) = I_d(V_{gs})/V_{ds}$  is the channel conductance determined by the transfer characteristics measured at low  $V_{ds}$  (0.1 V). As it can be seen from Fig. 2, GCA theory reproduces the output characteristics only in the case of long channel devices. Nevertheless, as the channel length is scaled down, GCA progressively fails in reproducing the experimental  $I_d(V_{ds})$  curves, predicting much higher saturation currents. These data clearly suggest the presence of contact effects, which become progressively evident as the channel length is scaled down and as  $V_{ds}$  increases.

The observed increase of the contact effects with  $V_{ds}$  is rather anomalous, if compared with previous observations. In fact, in the case of coplanar structures, the contact effects are more pronounced at low  $V_{ds}$ , resulting in superlinear  $I_d$ - $V_{ds}$  characteristics at low  $V_{ds}$ .<sup>2,4-6</sup> In this case, the contact current shows an exponential increase as a function of the potential drop,  $V_c$ , over the contact region.<sup>4,6</sup> As a consequence of this, the contact resistance substantially decreases for increasing  $V_{ds}$ , often becoming negligible in the saturation regime.<sup>6</sup> For this reason, field effect mobility values in coplanar devices are often extracted from saturated characteristics, as those deduced from the linear regime are much lower and strongly affected by the parasitic resistance effects. In contrast, in our short channel devices, we observed exactly the opposite: the field effect mobility extracted from saturated characteristics is much lower than the one determined from the linear regime (low- $V_{ds}$ ). In the case of staggered OTFTs, contact resistance appears to be

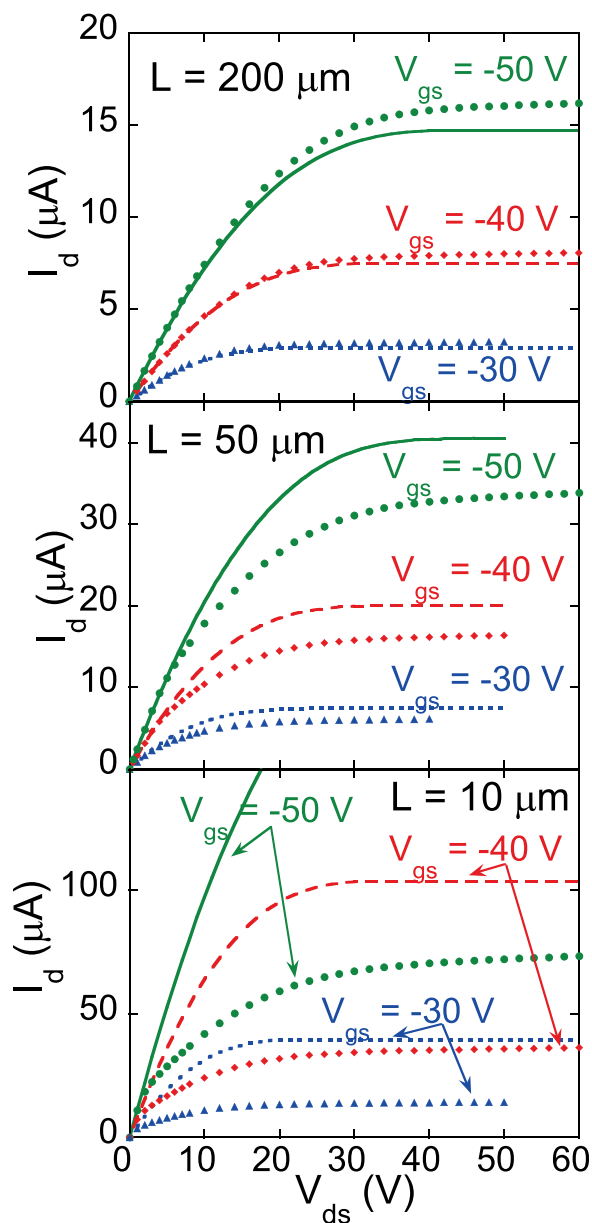


FIG. 2. (Color online) Experimental output characteristics (symbols), measured at different gate voltages, of OTFTs with three different channel lengths. Lines show the theoretical output characteristics calculated by using the gradual channel approximation.

constant with  $V_{ds}$  (ohmic contacts), as determined by the gated four point probe measurements<sup>9</sup> or by measurements on devices with different channel length,  $L$ ,<sup>3</sup> and to decrease with increasing  $V_g$ .<sup>3,9,10</sup> The gate bias dependence has been explained by considering the current crowding effect, which results in an increased contact area as the channel gets more and more accumulated<sup>9,10</sup> and space charge limited current in the bulk of the organic active layer.<sup>10</sup> An alternative approach to explain the gate bias dependence of the contact resistance in polycrystalline organic semiconductors based TFTs has been proposed by Vinciguerra *et al.*,<sup>11</sup> who considered a combination of grain boundary trapping model, including an exponential density of trap states localized at the grain boundaries (Meyer-Neldel model<sup>14</sup>) and Schottky contacts.

In order to evaluate the contact current-voltage characteristics in our devices, we adopted a common approach,<sup>4,6</sup>

splitting the channel into a small contact region at the source electrode, where there is a voltage drop  $V_C$ , and the main channel where the voltage drop is  $V_{DS}-V_C$ . As already shown in Figs. 1 and 2, long channel devices follow closely the GCA, denoting negligible contact effects (channel resistance  $\gg$  contact resistance). Hence, we evaluated the channel conductance  $G(V)$  from the long channel transfer characteristics and we determined the contact potential drop,  $V_C$ , by solving the following equation in the case of short channel devices and for a given set of  $I_d$ ,  $V_{gs}$ , and  $V_{ds}$ :

$$I_d = \frac{W}{L} \int_{V_{gs}-V_{ds}}^{V_{gs}-V_C} G(V) dV. \quad (2)$$

The resulting  $I_d$ - $V_C$  curves deduced for different  $V_{gs}$  and reported in Fig. 3 closely resemble the characteristics of a reverse biased leaky diode. Therefore, we have fitted the  $I_d$ - $V_C$  curves with the following Schottky diode relationship:

$$I_d = -I_0 \exp \left[ \left( \frac{V_C}{V_0} \right)^\alpha \right] \left\{ \exp \left[ - \left( \frac{qV_C}{\eta kT} \right) \right] - 1 \right\}, \quad (3)$$

where  $I_0$  is the reverse current for  $V_{ds} = 0$  V, the second term takes into account the barrier lowering induced by the Schottky effect, which depends on the electric field at the junction,  $E$ , which itself depends upon  $V_C$ , with  $V_0$  and  $\alpha$  as fitting parameters. The third term is the classical diode relationship, with  $\eta$  being the quality factor. It should be pointed out that the Schottky effect has been directly observed in metal/polymer interface by using internal photoemission spectroscopy.<sup>15</sup> A very good reproduction of the  $I_d$ - $V_C$  curves is achieved with the following values of the fitting parameters:  $V_0 = 0.34$  V,  $\alpha = 0.25$  (see Fig. 3). We note that in inorganic semiconductors, the electric field at the Schottky junction is expected to be proportional to  $(V_{bi}-V)^{1/2}$ , where  $V_{bi}$  is the built-in potential, and that the Schottky effect induces a barrier height reduction  $\Delta\Phi = (qE/4\pi\epsilon_s)^{1/2}$  (where  $\epsilon_s$  is the semiconductor permittivity),<sup>16</sup> thus leading to  $\Delta\Phi$  proportional to  $V^{1/4}$ , which is in good agreement with our fitting  $\alpha$ -value. The diode reverse current  $I_0$  is actually found to depend on the gate bias. A plot of such dependence for the three short channel devices is reported in the inset of Fig. 3.

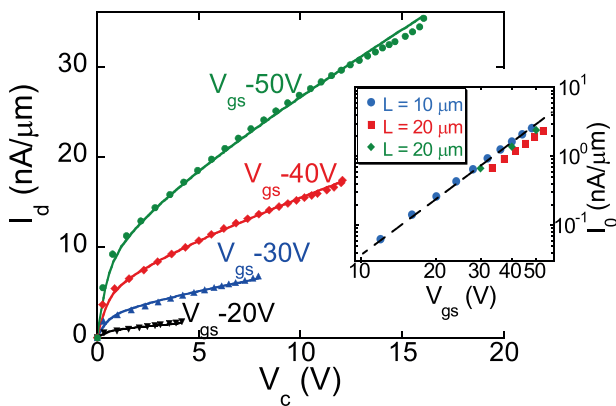


FIG. 3. (Color online) Current voltage characteristics of the source contact, evaluated for different gate voltages, of an OTFT with  $L = 10 \mu\text{m}$  (symbols) and corresponding fits calculated by using Eq. (3) (lines). Inset shows the diode reverse current,  $I_0$ , as a function of gate voltages for devices with different  $L$ .

The three curves follow very closely the same trend and  $I_0$  can be approximated, in the  $V_{gs}$  range considered, as a power law

$$I_0 = I_{00} \left( \frac{V_{gs}}{V_{00}} \right)^\beta, \quad (4)$$

where the constant  $I_{00} = 8 \times 10^{-14}$  A/ $\mu\text{m}$  and the exponent  $\beta = 2.7$ , as extracted from best fitting of the experimental data, while  $V_{00}$  has been introduced to keep the dimensionality of the pre-factor  $I_{00}$  ( $V_{00}$ -value has been arbitrary set to 1). The dependence of  $I_0$  from  $V_g$  could be explained by noting that the source contact is acting as a gated Schottky diode. Indeed, as already suggested by Vinciguerra *et al.*,<sup>11</sup> a contribution to the gate bias dependence of the contact resistance,  $R_s$ , arises from the gate modulation of the Schottky barrier at the source/drain contacts. Consequently, as can be seen in Fig. 4(a), contact resistance decreases with increasing  $V_{gs}$  for fixed  $V_{ds}$ , whereas for a given  $V_{gs}$ ,  $R_s$  increases with increasing  $V_{ds}$  as the voltage drop  $V_C$  at the contact increases. Furthermore, Fig. 4(a) shows that, for  $L = 10 \mu\text{m}$ ,  $R_s$  is comparable or higher than channel resistance even for

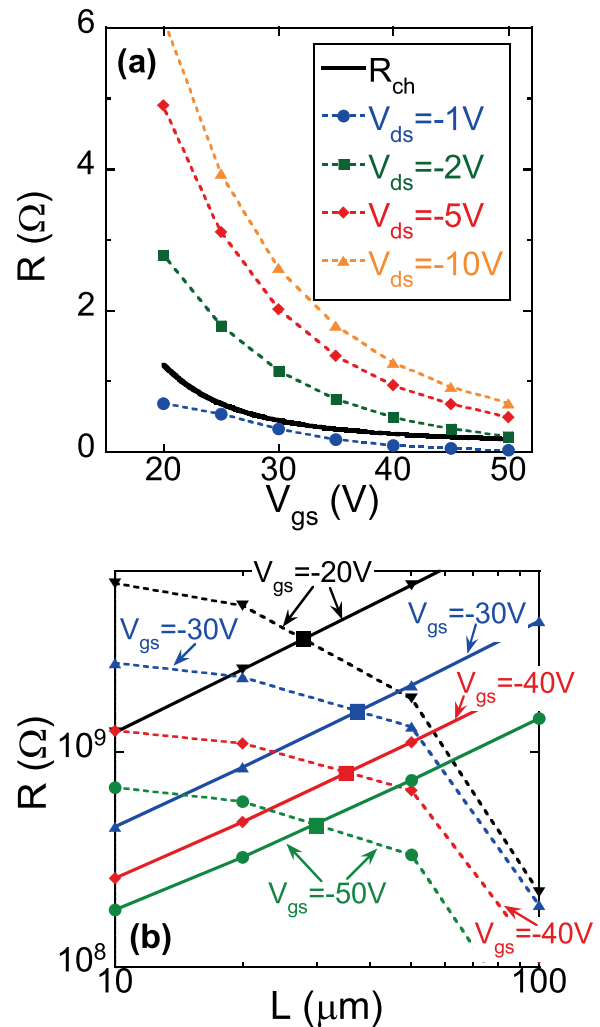


FIG. 4. (Color online) (a) Contact resistance,  $R_s$  (dashed lines), evaluated at different  $V_{ds}$ , and channel resistance,  $R_{ch}$  (solid line), vs gate voltage of an OTFTs with  $L = 10 \mu\text{m}$ . (b) Contact resistance (dashed lines) and channel resistance (solid lines), calculated for a fixed  $V_{ds} (-10$  V) and different  $V_{gs}$ , as a function of  $L$ .

$V_{ds}$  as low as  $-1$  V, then contact resistance becomes dominant in the electrical characteristics of short channel OTFTs. For increasing channel length,  $R_s$  decreases (Fig. 4(b)) showing a similar behavior for all  $V_{gs}$ . This  $R_s$  reduction can be related to the different  $V_{ds}$  partition between the contact and the channel resistances. Indeed, for a given value of  $V_{ds}$ , by increasing  $L$ ,  $R_{ch}$  linearly increases, inducing a larger voltage drop,  $V_d - V_c$ , on  $R_{ch}$ , thus reducing the voltage drop,  $V_c - V_s$ , on  $R_s$ . As a result, considering the  $I_d - V_c$  curves shown in Fig. 3, a lower differential resistance of the diode at the source contact is expected. Fig. 4(b) also shows that, for the bias condition considered,  $R_s$  and  $R_{ch}$  become comparable for OTFTs with  $L$  between 30 and 40  $\mu\text{m}$  suggesting that the critical  $L_c$  value should be placed in this range.

According to the presented analysis, we have then implemented an equivalent circuit of the OTFTs, consisting of a reverse biased diode in series with an “ideal” transistor, i.e., a transistor following GCA and whose  $G(V)$  is extracted from the long channel characteristics. The compact model allows to perfectly reproduce the electrical characteristics of devices with different geometries and it has been implemented in a computer-aided design (CAD) system in order to perform circuit simulations.

In conclusion, contact effects have been investigated in fully printed p-channel organic thin film transistors with field effect mobility up to 2  $\text{cm}^2/\text{Vs}$ . Contact effects seriously influence the electrical characteristics in devices with channel length  $< 200 \mu\text{m}$  and we found a drastic increase of the contact resistance for increasing source/drain voltage. Assuming that contact effects are negligible in long channel devices, as confirmed by the applicability of the gradual channel approximation, we developed a method to extract the current-voltage characteristics of the

source contact. The I-V contact characteristics were modeled as a reverse biased Schottky diode, including barrier lowering induced by this Schottky effect and gate modulation of the reverse current. The developed compact model allows a nice reproducibility of the device characteristics for different geometries and has been applied to circuit simulations.

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