

Design and Analysis of Multiscroll Chaotic Attractors From Saturated Function Series

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Abstract—This paper initiates a saturated function series approach for chaos generation. The systematic saturated function series methodology developed here can create multiscroll chaotic attractors from a three-dimensional (3D) linear autonomous system with a simple saturated function series controller, including one-directional n -scroll, two-directional $n \times m$ -grid scroll, and 3-D $n \times m \times l$ -grid scroll chaotic attractors. The dynamical behaviors and chaos generation mechanism of multiscroll systems are further investigated by analyzing the system trajectories. In particular, a two-dimensional (2D) Poincaré return map is rigorously derived for verifying the chaotic behaviors of the double-scroll chaotic attractor, which is a basic generator of various multiscroll chaotic attractors investigated in the paper.

Index Terms—Chaos generation, multiscroll chaotic attractor, saturated function series, saturated plateau.

I. INTRODUCTION

IT IS WELL KNOWN that chaos is useful and has great potential in many real-world engineering fields such as digital data encryption and secure communications, biomedical engineering, flow dynamics and liquid mixing, power-systems protection, and so on [1], [2].

Currently, generation of multiscroll chaotic attractors has been extensively studied and is no longer a very difficult task [3]–[17]. For example, Suykens *et al.* introduced several methods for generating n -scroll chaotic attractors using simple circuits [3]–[6], [9], [10], including the generalized Chua's circuit [4] and cellular neural network (CNN) [5], [7]. A piecewise-linear (PWL) implementation of n double scrolls [3] was also proposed by Arena *et al.* in [7]. The essence of these methods is to add breakpoints in the PWL characteristic function of the nonlinear resistor in Chua's circuit [18], [19]. Tang *et al.* proposed a sine-function approach for creating n -scroll chaotic attractors, with a systematical circuit realization that can physically produce up to as many as ten scrolls visible on the oscilloscope [8],

[12]. Ozoguz *et al.* presented a nonlinear transconductor method for generating n -scroll attractors [11]. Lü *et al.* introduced a switching manifold approach for creating chaotic attractors with multiple-merged basins of attraction [14]. Yalcin *et al.* proposed a stair function method for generating one-directional (1-D) n -scroll, two-directional (2-D) $n \times m$ -grid scroll, and three-directional (3-D) $n \times m \times l$ -grid scroll chaotic attractors [10]. Hysteresis can also generate chaos [20]–[27]. Elwakil and Kennedy constructed a class of circuit-independent chaotic oscillators [20]. Elwakil *et al.* proposed some hysteresis chaotic oscillators [21]. Recently, Lü *et al.* presented a hysteresis series approach for creating 1-D n -scroll, 2-D $n \times m$ -grid scroll, and 3-D $n \times m \times l$ -grid scroll chaotic attractors [16]. Last but not least, Cafagna and Grassi [17] produced a ring Chua's circuit method for generating 1-D n -scroll and 2-D $n \times m$ -grid scroll chaotic attractors. To this end, it should be noted that stair circuit, hysteresis circuit, and saturated circuit are the three kinds of basic circuits. Since it has been reported that stair circuit and hysteresis circuit can create 3-D multiscroll chaotic attractors [10], [15], [16], it is therefore very interesting to ask whether or not saturated circuit can also generate 3-D multiscroll chaotic attractors. This paper gives a positive answer to this question.

More precisely, this paper proposes a saturated function series approach for generating multiscroll chaotic attractors, including 1-D n -scroll, 2-D $n \times m$ -grid scroll, and 3-D $n \times m \times l$ -grid scroll chaotic attractors. It is noticed that the saturated function series is continuous, yet the stair function and hysteresis series are not continuous at all switching points. The dynamical behaviors and chaos generation mechanism of the multiscroll systems are further investigated by analyzing their trajectories. In particular, a 2-D Poincaré return map is rigorously derived for verifying the chaotic behaviors of the double-scroll chaotic attractor, which is a basic generator of various multiscroll chaotic attractors studied in the paper. In comparison, however, most of the reported multiscroll ($n \geq 3$) chaotic attractors are only verified by using computer simulation and/or electronic circuits, where theoretical analysis and rigorous mathematical proofs are not available.

The rest of this paper is organized as follows. In Section II, the concept of saturated function series is introduced. The saturated function series approach is then introduced in Section III for creating multiscroll chaotic attractors, including 1-D n -scroll, 2-D $n \times m$ -grid scroll, and 3-D $n \times m \times l$ -grid scroll attractors. In Section IV, dynamical behaviors and chaos generation mechanism of the multiscroll systems are further investigated, and a 2D Poincaré return map is rigorously derived for verifying the chaotic behaviors of the double-scroll attractor. Conclusions are finally given in Section V.

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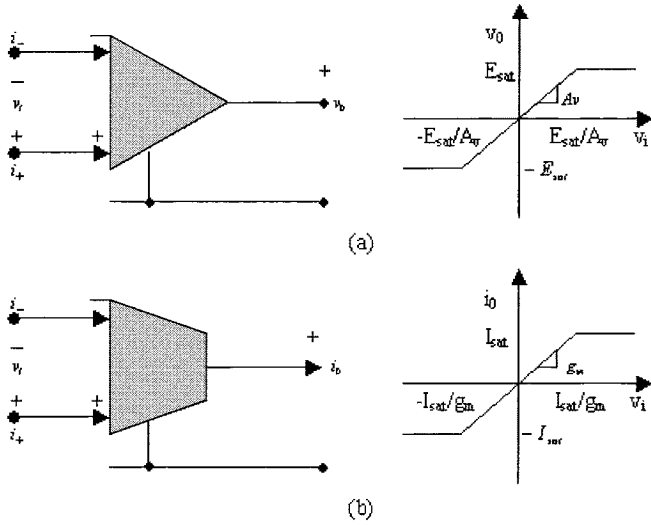


Fig. 1. (a) Opamp and its PWL model. (b) OTA and its PWL model.

II. SATURATED FUNCTION SERIES

This section introduces the saturated function series concept.

A. Saturated Circuit

It is well known that the saturated circuit is one of the basic PWL circuits. The PWL models for operational amplifiers (opamps) and operational transconductance amplifiers (OTAs) can be well characterized by saturated circuit [28]. From Fig. 1, one can see that the PWL approximations for opamps and OTAs are quite accurate [28]. It leads to a simple representation for opamp, which is in the linear region for $-E_{sat} \leq v_o \leq E_{sat}$, with voltage amplification A_v , positive saturation E_{sat} , and negative saturation $-E_{sat}$, as follows:

$$\begin{cases} v_o = \frac{A_v}{2} \left(\left| v_i + \frac{E_{sat}}{A_v} \right| - \left| v_i - \frac{E_{sat}}{A_v} \right| \right) \\ i_- = i_+ = 0. \end{cases} \quad (1)$$

It is called an opamp finite-gain model. In each of the three regions, the opamp can be characterized by a linear circuit.

Similarly, for the OTA, in the linear region $-I_{sat} \leq i_o \leq I_{sat}$, with transconductance gain g_m , positive saturation I_{sat} , and negative saturation $-I_{sat}$, one has

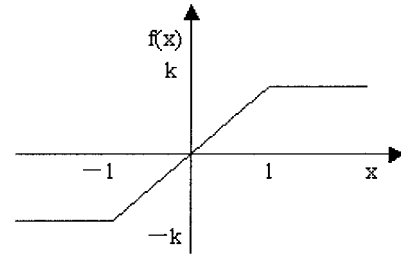
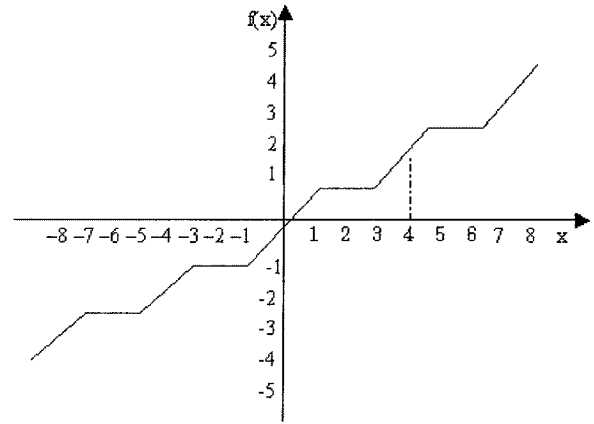
$$\begin{cases} i_o = \frac{g_m}{2} \left(\left| v_i + \frac{I_{sat}}{g_m} \right| - \left| v_i - \frac{I_{sat}}{g_m} \right| \right) \\ i_- = i_+ = 0. \end{cases} \quad (2)$$

B. Saturated Function Series

Consider the following saturated function:

$$f_0(x; k) = \begin{cases} k, & \text{if } x > 1 \\ kx, & \text{if } |x| \leq 1 \\ -k, & \text{if } x < -1 \end{cases} \quad (3)$$

where $k > 0$ is the slope of the middle segment, the upper radial $\{f_0(x; k) = k \mid x \geq 1\}$ and the lower radial $\{f_0(x; k) = -k \mid x \leq -1\}$ are called *saturated plateaus*, and the segment $\{f_0(x; k) = kx \mid |x| \leq 1\}$ between the two *saturated plateaus*

Fig. 2. Saturated function $f_0(x; k)$.Fig. 3. Saturated function series with $k = 1, h = 4$.

is called the *saturated slope*. Fig. 2 shows the phase portrait of the saturated function $f_0(x; k)$.

Definition 1: The following PWL function:

$$f(x; k, h, p, q) = \sum_{i=-p}^q f_i(x; k, h) \quad (4)$$

is called a *saturated function series*, where $k > 0$ is the slope of saturated function series, $h > 2$ is the *saturated delay time* of the saturated function series, p and q are positive integers, and

$$f_i(x; k, h) = \begin{cases} 2k, & \text{if } x > ih + 1 \\ k(x - ih) + k, & \text{if } |x - ih| \leq 1 \\ 0, & \text{if } x < ih - 1 \end{cases}$$

and

$$f_{-i}(x; k, h) = \begin{cases} 0, & \text{if } x > -ih + 1 \\ k(x + ih) - k, & \text{if } |x + ih| \leq 1 \\ -2k, & \text{if } x < -ih - 1. \end{cases}$$

One may recast the saturated function series $f(x; k, h, p, q)$ as follows:

$$f(x; k, h, p, q) = \begin{cases} (2q + 1)k, & \text{if } x > qh + 1 \\ k(x - ih) + 2ik, & \text{if } |x - ih| \leq 1, \quad -p \leq i \leq q \\ (2i + 1)k, & \text{if } ih + 1 < x < (i + 1)h - 1 \\ -(2p + 1)k, & \text{if } x < -ph - 1. \end{cases} \quad (5)$$

Fig. 3 shows the phase portrait of this saturated function series with $k = 1, h = 4$. It is noticed that saturated function series (5) is a PWL continuous function and has better analytical property such as the existence of solution and stability. However, one should notice that the stair function in [10] and the hysteresis series in [15], [16] are not continuous in all switching points.

Consider the following 3-D linear autonomous system:

$$\begin{cases} \dot{x} = y \\ \dot{y} = z \\ \dot{z} = -ax - by - cz \end{cases} \quad (6)$$

where x, y, z are state variables, and a, b, c are positive real constants. To guide the linear system (6) to generate chaotic behavior, it needs to add a nonlinear controller to stretch and fold the trajectories of the system repeatedly. Note that the PWL controller is the simplest nonlinear continuous controller. Here, the saturated function series (5) is used as the controller.

III. DESIGN OF MULTISCROLL CHAOTIC ATTRACTORS FROM SATURATED FUNCTION SERIES

This section introduces a new and systematic method—saturated function series approach—for generating multiscroll chaotic attractors, including 1-D n -scroll, 2-D $n \times m$ -grid scroll, and 3-D $n \times m \times l$ -grid scroll chaotic attractors, from the linear autonomous system (6) by using a PWL controller.

Note that (6) has a unique equilibrium point $(0, 0, 0)$ and its corresponding characteristic equation is

$$\lambda^3 + c\lambda^2 + b\lambda + a = 0. \quad (7)$$

Denote $\hat{p} = b - (1/3)c^2$, $\hat{q} = (2/27)c^3 - (1/3)bc + a$, and $\Delta = (ac^3/27) - (b^2c^2/108) - (abc/6) + (b^3/27) + (a^2/4)$. Solving (7) gives

$$\lambda_1 = -\frac{c}{3} + \sqrt[3]{-\frac{\hat{q}}{2} + \sqrt{\Delta}} + \sqrt[3]{-\frac{\hat{q}}{2} - \sqrt{\Delta}} \quad (8)$$

and

$$\begin{aligned} \lambda_{2,3} &= -\frac{c}{3} - \frac{1}{2} \left(\sqrt[3]{-\frac{\hat{q}}{2} + \sqrt{\Delta}} + \sqrt[3]{-\frac{\hat{q}}{2} - \sqrt{\Delta}} \right) \\ &\quad \pm \frac{\sqrt{3}}{2} i \left(\sqrt[3]{-\frac{\hat{q}}{2} + \sqrt{\Delta}} - \sqrt[3]{-\frac{\hat{q}}{2} - \sqrt{\Delta}} \right) \\ &\equiv \alpha \pm \beta i. \end{aligned} \quad (9)$$

Numerical computations show that the linear system (6) with a saturated function series controller will produce chaotic behavior under the conditions of $\lambda_1 < 0$, $\alpha > 0$, and $\beta \neq 0$. That is, (7) has a negative eigenvalue and one pair of complex conjugate eigenvalues with positive real parts. Moreover, the equilibrium point $(0, 0, 0)$ is a two dimensionally unstable saddle, called a *saddle point of index 2* [17]–[19].

In the following, assume that

$$\begin{aligned} \Delta &= \frac{ac^3}{27} - \frac{b^2c^2}{108} - \frac{abc}{6} + \frac{b^3}{27} + \frac{a^2}{4} > 0, \\ \lambda_1 &= -\frac{c}{3} + \sqrt[3]{-\frac{\hat{q}}{2} + \sqrt{\Delta}} + \sqrt[3]{-\frac{\hat{q}}{2} - \sqrt{\Delta}} < 0, \\ \alpha &= -\frac{c}{3} - \frac{1}{2} \left(\sqrt[3]{-\frac{\hat{q}}{2} + \sqrt{\Delta}} + \sqrt[3]{-\frac{\hat{q}}{2} - \sqrt{\Delta}} \right) > 0. \end{aligned} \quad (10)$$

A. New Double Scroll Chaotic Attractor

Here, the saturated function $f_0(x; k)$ is chosen as a controller to guide system (6) to generate chaos. The controlled system is described by

$$\begin{cases} \dot{x} = y \\ \dot{y} = z \\ \dot{z} = -ax - by - cz + d_1 f_0(x; k) \end{cases} \quad (11)$$

where $f_0(x; k)$ is defined by (3).

When $a = b = c = d_1 = 0.7$, $k = 10$, system (11) has a double-scroll chaotic attractor as shown in Fig. 4(a). Fig. 4(b) shows the x - y plane projection of the double-scroll attractor; Fig. 4(c) shows that the variable $x(t)$ spirals around two values, ± 10 , making random excursions between these two values which correspond to the centers of the two scrolls in the attractor; Fig. 4(d) shows the Poincaré map on section $y = 0$, where it is clear that the trajectories are folded and the corresponding double-scroll map reported in [9] can also be observed.

Obviously, system (11) has three equilibria, $S_{\pm}(\pm 10, 0, 0)$ and $S_0(0, 0, 0)$, which correspond to the three PWL parts of the saturated function $f_0(x; k)$ in Fig. 2, respectively. Equilibria S_{\pm} possess eigenvalues $\lambda_1 = -0.8480$, $\lambda_{2,3} = 0.0740 \pm 0.9055i$, which are called *saddle points of index 2* since the two complex conjugate eigenvalues have positive real parts [17]–[19]. Equilibrium point S_0 has eigenvalues $\lambda_1 = 1.5309$, $\lambda_{2,3} = -1.1154 \pm 1.6944i$, which is called *saddle point of index 1* since the real eigenvalue is positive [17]. It is noticed that the scrolls are generated only around the equilibria of *saddle points of index 2* [17]–[19]. Moreover, equilibria S_{\pm} correspond to the two *saturated plateaus*, which are responsible for generating the two scrolls in the double-scroll attractor. However, the equilibrium point S_0 corresponds to the *saturated slope* and is responsible for connecting these two symmetrical scrolls. The Lyapunov exponent spectrum and Lyapunov dimension can be calculated by using the numerical methods described in [29], yielding $LE_1 = 0.1042$, $LE_2 = 0$, $LE_3 = -0.8043$, and $LD = 2.1297$.

According to the above analysis, this new double-scroll attractor is similar to but different from Chua's double-scroll attractor [18] since Chua's double-scroll attractor is created by using Chua's circuit and the two circuits are not topologically equivalent.

B. 1-D n -Scroll Chaotic Attractors

In the following, to create n -scroll chaotic attractors ($n \geq 3$), a saturated function series controller is added to system (6), leading to

$$\begin{cases} \dot{x} = y \\ \dot{y} = z \\ \dot{z} = -ax - by - cz + d_1 f(x; k_1, h_1, p_1, q_1) \end{cases} \quad (12)$$

where $f(x; k_1, h_1, p_1, q_1)$ is defined by (5), and a, b, c, d_1 are positive constants.

Assume that

$$\begin{aligned} d_1 k_1 &> a \\ 2d_1 k_1 &\geq ah_1 \\ \max\{p_1, q_1\} \frac{|ah_1 - 2k_1 d_1|}{d_1 k_1 - a} &\leq 1 \\ (2d_1 k_1 - ah_1)(q_1 - 1) &< ah_1 - d_1 k_1 - a. \end{aligned} \quad (13)$$

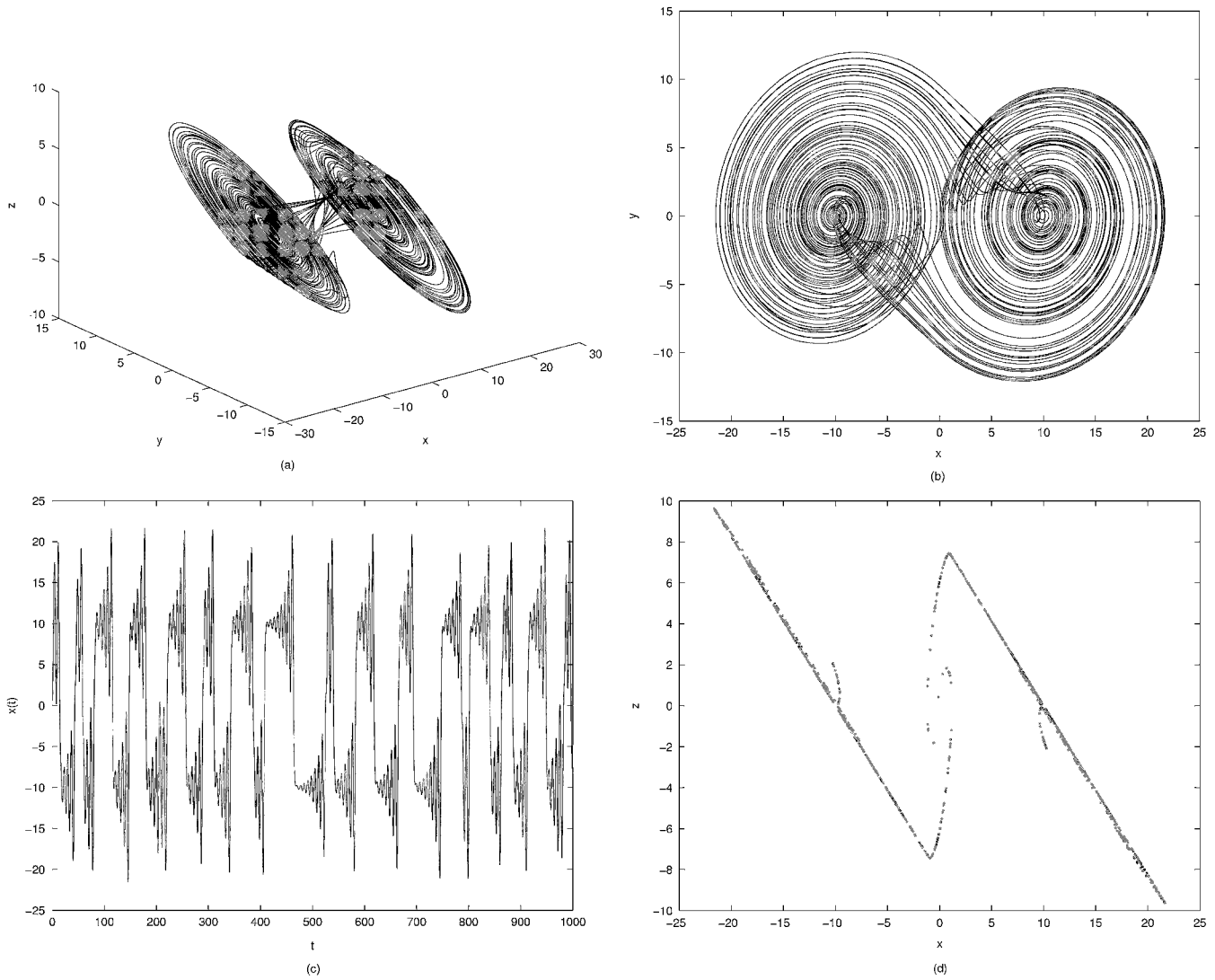


Fig. 4. Double-scroll chaotic attractor. (a) x - y - z space. (b) x - y plane projection. (c) Variable $x(t)$. (d) Poincaré map on section $y = 0$.

Obviously, all $2(p_1 + q_1) + 3$ equilibrium points of system (12) are located along the x -axis, and can be classified into two different sets

$$A_x = \left\{ -\frac{(2p_1 + 1)d_1k_1}{a}, \frac{(-2p_1 + 1)d_1k_1}{a}, \dots, \frac{(2q_1 + 1)d_1k_1}{a} \right\} \quad (14)$$

and

$$B_x = \left\{ -\frac{p_1k_1d_1(h_1 - 2)}{k_1d_1 - a}, \frac{(-p_1 + 1)k_1d_1(h_1 - 2)}{k_1d_1 - a}, \dots, \frac{q_1k_1d_1(h_1 - 2)}{k_1d_1 - a} \right\}. \quad (15)$$

For all equilibria in set A_x , the characteristic equations are (7) and the corresponding eigenvalues satisfy $\lambda_1 < 0$ and $\lambda_{2,3} = \alpha \pm \beta i$ with $\alpha > 0$ and $\beta \neq 0$ from assumption (10). That is, all equilibria in set A_x are *saddle points of index 2*. For all equilibria in set B_x , the corresponding characteristic equations are

$$\lambda^3 + c\lambda^2 + b\lambda + a - d_1k_1 = 0. \quad (16)$$

Since $\lambda_1 + \lambda_2 + \lambda_3 = -c < 0$ and $\lambda_1\lambda_2\lambda_3 = -(a - d_1k_1) > 0$, (16) has one positive eigenvalue and two negative eigenvalues, or one positive eigenvalue and a pair of complex conjugate eigenvalues with negative real parts. To generate chaos from system (12), one may assume that (16) has a positive eigenvalue and a pair of complex eigenvalues with negative real parts. It means that all equilibria in set B_x are *saddle points of index 1*. Since the scrolls are generated only around *saddle points of index 2* [17]–[19], system (12) has the potential to create a maximum of $(p_1 + q_1 + 2)$ -scroll chaotic attractor for some suitable parameters a, b, c, d_1, k_1, h_1 . It should be emphasized that the $p_1 + q_1 + 2$ equilibria in set A_x are responsible for generating $p_1 + q_1 + 2$ scrolls of the attractor. However, the $p_1 + q_1 + 1$ equilibria in set B_x are responsible for connecting these $p_1 + q_1 + 2$ scrolls to form a whole chaotic attractor. Moreover, each equilibrium point in set A_x corresponds to a unique *saturated plateau* of the saturated function series (5) and also corresponds to a unique scroll of the whole attractor. Furthermore, each equilibrium point in set B_x corresponds to a unique *saturated slope* of the saturated function series (5) and also corresponds to a unique connection between two neighboring scrolls.

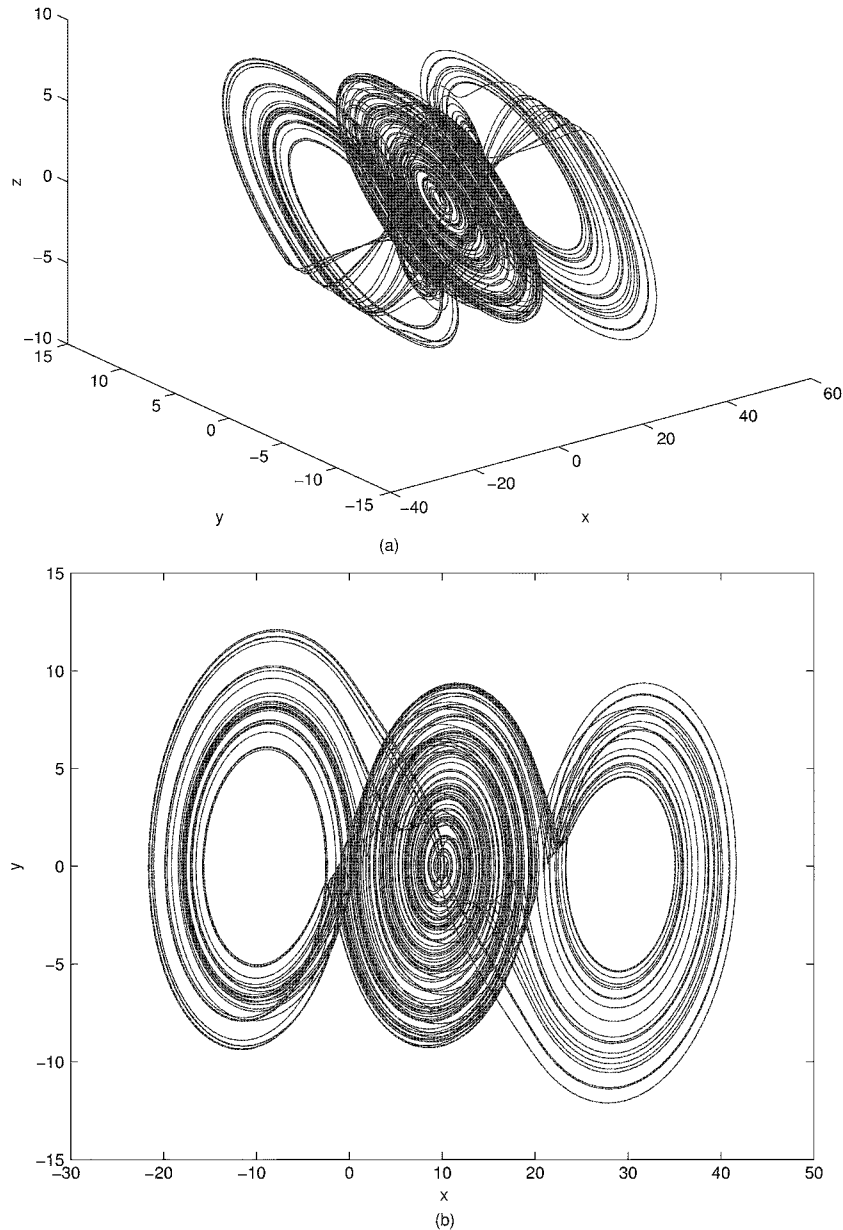


Fig. 5. Three-scroll chaotic attractor. (a) x - y - z space. (b) x - y plane projection.

Fig. 5 shows a 3-scroll chaotic attractor of system (12), where $a = b = c = d_1 = 0.7$, $k_1 = 10$, $h_1 = 20$, $p_1 = 0$, $q_1 = 1$. The Lyapunov exponent spectrum of this 3-scroll chaotic attractor includes $LE_1 = 0.1276$, $LE_2 = 0$, $LE_3 = -0.8258$. Fig. 6 displays a 6-scroll chaotic attractor of system (12), where $a = b = c = d_1 = 0.7$, $k_1 = 9$, $h_1 = 18$, $p_1 = 2$, $q_1 = 2$. The Lyapunov exponent spectrum of this 6-scroll chaotic attractor includes $LE_1 = 0.1486$, $LE_2 = 0$, $LE_3 = -0.8457$.

Remark 1: In fact, system (12) can create an n -scroll chaotic attractor ($n \geq 3$), including odd and even number of scrolls chaotic attractors, by adjusting suitable parameters. There are three basic design strategies to obtain suitable circuit parameters for specified n -scroll chaotic attractors: 1) parameters a, b, c satisfy condition (10); 2) parameters a, d_1, k_1, h_1 satisfy condition (13) where, for simplification, assume that $a = d_1$ and $h_1 = 2k_1$; 3) parameters p_1, q_1 control the number of scrolls in negative and positive x -directions, respectively.

C. 2-D $n \times m$ -Grid Scroll Chaotic Attractors

Here, a saturated function series controller is added to system (6) for generating $n \times m$ -grid scroll chaotic attractors. The controlled system is described by

$$\begin{cases} \dot{x} = y - \frac{d_2}{b} f(y; k_2, h_2, p_2, q_2) \\ \dot{y} = z \\ \dot{z} = -ax - by - cz + d_1 f(x; k_1, h_1, p_1, q_1) \\ \quad + d_2 f(y; k_2, h_2, p_2, q_2) \end{cases} \quad (17)$$

where $f(x; k_1, h_1, p_1, q_1)$ and $f(y; k_2, h_2, p_2, q_2)$ are defined by (5), and a, b, c, d_1, d_2 are positive constants.

Denote, in addition to (14) and (15), the following:

$$A_y = \left\{ -\frac{(2p_2 + 1)d_2 k_2}{b}, \frac{(-2p_2 + 1)d_2 k_2}{b}, \dots, \frac{(2q_2 + 1)d_2 k_2}{b} \right\} \quad (18)$$

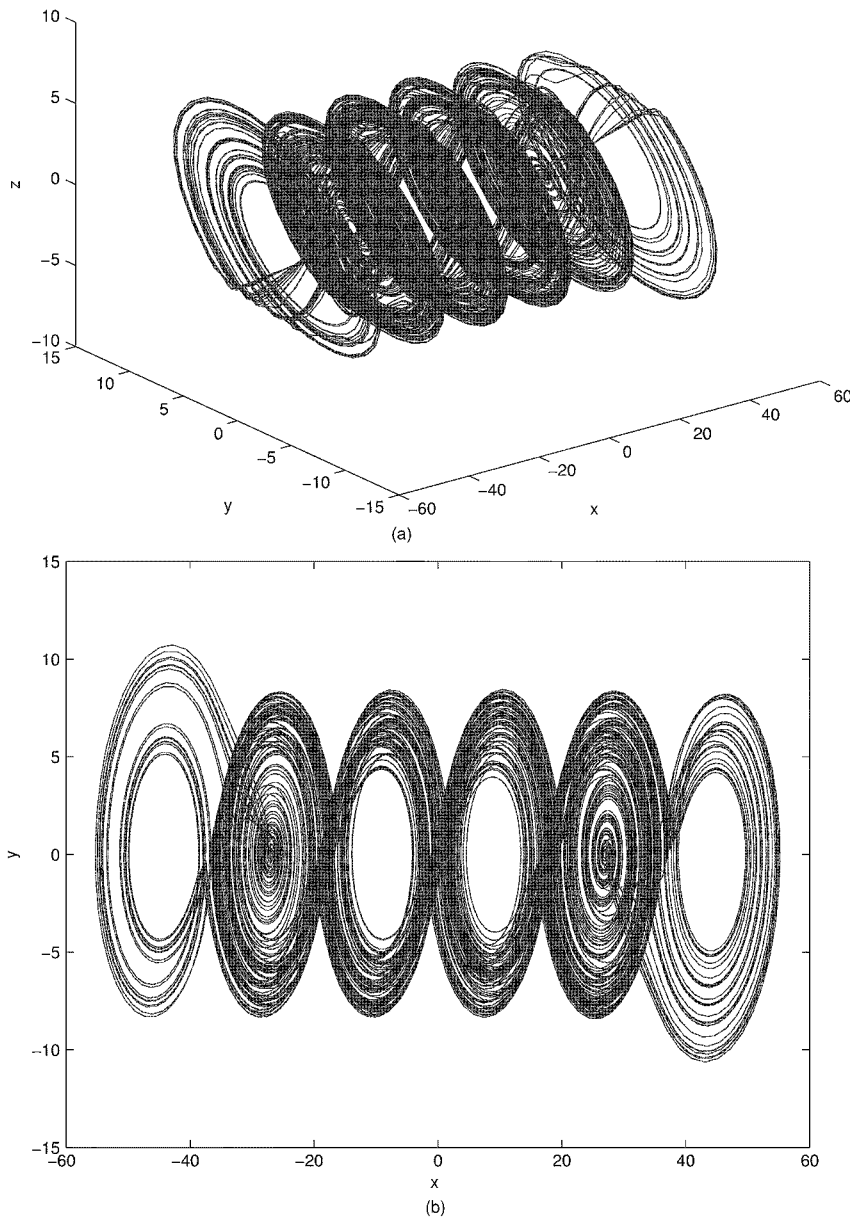


Fig. 6. Six-scroll chaotic attractor. (a) x - y - z space. (b) x - y plane projection.

and

$$B_y = \left\{ -\frac{p_2 k_2 d_2 (h_2 - 2)}{k_2 d_2 - b}, \frac{(-p_2 + 1) k_2 d_2 (h_2 - 2)}{k_2 d_2 - b}, \dots, \frac{q_2 k_2 d_2 (h_2 - 2)}{k_2 d_2 - b} \right\}. \quad (19)$$

Assume that (13) holds and

$$d_2 k_2 > b, 2d_2 k_2 \geq b h_2, \max\{p_2, q_2\} \frac{|b h_2 - 2k_2 d_2|}{d_2 k_2 - b} \leq 1, \\ (2d_2 k_2 - b h_2)(q_2 - 1) < b h_2 - d_2 k_2 - b. \quad (20)$$

Then, (17) has $(2p_1 + 2q_1 + 3) \times (2p_2 + 2q_2 + 3)$ equilibrium points, which are located on the x - y plane and given by

$$O_{xy} = \{(x^*, y^*) \mid x^* \in A_x \cup B_x, y^* \in A_y \cup B_y\}. \quad (21)$$

It is noticed that all equilibria can be classified into four different sets

$$A_1 = \{(x^*, y^*) \mid x^* \in A_x, y^* \in A_y\} \\ A_2 = \{(x^*, y^*) \mid x^* \in A_x, y^* \in B_y\} \\ A_3 = \{(x^*, y^*) \mid x^* \in B_x, y^* \in A_y\} \\ A_4 = \{(x^*, y^*) \mid x^* \in B_x, y^* \in B_y\}.$$

Obviously, the characteristic equations of the linearized system evaluated at the equilibria in set A_1 are (7) and the corresponding eigenvalues satisfy $\lambda_1 < 0$ and $\lambda_{2,3} = \alpha \pm \beta i$ with $\alpha > 0$ and $\beta \neq 0$ by assumption (10). It means that all equilibria in set A_1 are *saddle points of index 2*. For all equilibria in set A_2 , the corresponding characteristic equations are

$$\lambda^3 + c\lambda^2 + (b - k_2 d_2)\lambda + a \left(1 - \frac{k_2 d_2}{b}\right) = 0. \quad (22)$$

Since $\lambda_1 + \lambda_2 + \lambda_3 = -c < 0$ and $\lambda_1\lambda_2\lambda_3 = -a(1 - (k_2d_2/b)) > 0$, (22) has one positive eigenvalue and two negative eigenvalues, or one positive eigenvalue and a pair of complex conjugate eigenvalues with negative real parts. Moreover, all equilibria in A_2 are *saddle points of index 1*. For all equilibria in A_3 , the corresponding characteristic equations are (16) and these equilibria are *saddle points of index 1*. Similarly, for all equilibria in A_4 , the corresponding characteristic equations are

$$\lambda^3 + c\lambda^2 + (b - k_2d_2)\lambda + (a - dk_1) \left(1 - \frac{k_2d_2}{b}\right) = 0. \quad (23)$$

Since $\lambda_1 + \lambda_2 + \lambda_3 = -c < 0$ and $\lambda_1\lambda_2\lambda_3 = -(a - dk_1)(1 - (k_2d_2)/b) < 0$, (23) has one negative eigenvalue and two positive eigenvalues, or three negative eigenvalues, or one negative eigenvalue and a pair of complex conjugate eigenvalues.

To create chaos from system (17), one may assume that (23) has one negative eigenvalue and a pair of complex conjugate eigenvalues with positive real parts. Thus, the equilibria in A_4 are *saddle points of index 2*. Since the scrolls can be generated only around *saddle points of index 2* [17]–[19], the equilibria in A_1 and A_4 may create scrolls. However, numerical simulations show that only the equilibria in A_1 can generate scrolls. In fact, having a *saddle point of index 2* is only a necessary condition, but not a sufficient condition for generating scrolls. According to the Homoclinic Šilnikov Theorem [19], it needs a condition—existence of a homoclinic orbit in the neighboring region of the equilibrium point—for generating scrolls. Therefore, system (17) has the potential to create a maximum of 2-D $(p_1 + q_1 + 2) \times (p_2 + q_2 + 2)$ -grid scroll chaotic attractor, called 2-D $n \times m$ -grid scroll chaotic attractor, for suitable parameters $a, b, c, d_1, d_2, k_1, h_1, k_2, h_2$. Note that each equilibrium point in A_1 corresponds to a unique 2-D *saturated plateau* and also corresponds to a unique scroll in the whole attractor. Moreover, other equilibria in A_2, A_3, A_4 correspond to the *saturated slopes* and are responsible for connecting these $(p_1 + q_1 + 2) \times (p_2 + q_2 + 2)$ scrolls.

Fig. 7 shows a 6×6 -grid scroll chaotic attractor, where $a = b = c = d_1 = d_2 = 0.7, k_1 = k_2 = 50, h_1 = h_2 = 100, p_1 = q_1 = p_2 = q_2 = 2$. Clearly, there are six scrolls in the x -direction and six scrolls in the y -direction, as shown in Fig. 7(b). The Lyapunov exponent spectrum of this 6×6 -grid scroll attractor includes $LE_1 = 0.1599, LE_2 = 0, LE_3 = -0.8622$. Note that these 2-D $n \times m$ -grid scroll chaotic attractors are generated in exactly the same way as the 1-D case discussed in the last subsection, except that the directions of the system trajectories are more vertical here. Similarly, one can design 2-D $n \times m$ -grid scroll attractors in x - z or y - z directions.

Remark 2: There are five fundamental design guidelines for obtaining suitable circuit parameters for specified 2-D $n \times m$ -grid scroll attractors: 1) parameters a, b, c satisfy condition (10); 2) parameters a, d_1, k_1, h_1 satisfy condition (13) where, for simplification, assume that $a = d_1$ and $h_1 = 2k_1$; 3) parameters b, d_2, k_2, h_2 satisfy condition (20) where, for simplification, assume that $b = d_2$ and $h_2 = 2k_2$; 4) parameters p_1, q_1 control the numbers of scrolls in negative and positive x -directions, respectively; 5) parameters p_2, q_2 control the numbers of scrolls in negative and positive y -directions, respectively.

D. 3-D $n \times m \times l$ -Grid Scroll Chaotic Attractors

Here, a saturated function series controller is added to system (6) for creating 3-D $n \times m \times l$ -grid scroll chaotic attractors. The controlled system is

$$\begin{cases} \dot{x} = y - \frac{d_2}{b}f(y; k_2, h_2, p_2, q_2) \\ \dot{y} = z - \frac{d_3}{c}f(z; k_3, h_3, p_3, q_3) \\ \dot{z} = -ax - by - cz + d_1f(x; k_1, h_1, p_1, q_1) \\ \quad + d_2f(y; k_2, h_2, p_2, q_2) + d_3f(z; k_3, h_3, p_3, q_3) \end{cases} \quad (24)$$

with $f(x; k_1, h_1, p_1, q_1), f(y; k_2, h_2, p_2, q_2), f(z; k_3, h_3, p_3, q_3)$ defined by (5), and a, b, c, d_1, d_2, d_3 are positive constants.

In addition to (14), (15), (18), and (19), define

$$A_z = \left\{ -\frac{(2p_3 + 1)d_3k_3}{c}, \frac{(-2p_3 + 1)d_3k_3}{c}, \dots, \frac{(2q_3 + 1)d_3k_3}{c} \right\} \quad (25)$$

and

$$B_z = \left\{ -\frac{p_3k_3d_3(h_3 - 2)}{k_3d_3 - c}, \frac{(-p_3 + 1)k_3d_3(h_3 - 2)}{k_3d_3 - c}, \dots, \frac{q_3k_3d_3(h_3 - 2)}{k_3d_3 - c} \right\}. \quad (26)$$

Assume that (13) and (20) hold and

$$d_3k_3 > c, \quad 2d_3k_3 \geq ch_3, \max\{p_3, q_3\} \frac{|ch_3 - 2k_3d_3|}{d_3k_3 - c} \leq 1, \\ (2d_3k_3 - ch_3)(q_3 - 1) < ch_3 - d_3k_3 - c. \quad (27)$$

Then, (24) has $(2p_1 + 2q_1 + 3) \times (2p_2 + 2q_2 + 3) \times (2p_3 + 2q_3 + 3)$ equilibrium points, given by

$$O_{xyz} = \{(x^*, y^*, z^*) \mid x^* \in A_x \cup B_x, \\ y^* \in A_y \cup B_y, z^* \in A_z \cup B_z\}. \quad (28)$$

Note that all equilibria can be classified into eight different sets:

$$\begin{aligned} \bar{A}_1 &= \{(x^*, y^*, z^*) \mid x^* \in A_x, y^* \in A_y, z^* \in A_z\} \\ \bar{A}_2 &= \{(x^*, y^*, z^*) \mid x^* \in A_x, y^* \in A_y, z^* \in B_z\} \\ \bar{A}_3 &= \{(x^*, y^*, z^*) \mid x^* \in A_x, y^* \in B_y, z^* \in A_z\} \\ \bar{A}_4 &= \{(x^*, y^*, z^*) \mid x^* \in A_x, y^* \in B_y, z^* \in B_z\} \\ \bar{A}_5 &= \{(x^*, y^*, z^*) \mid x^* \in B_x, y^* \in A_y, z^* \in A_z\} \\ \bar{A}_6 &= \{(x^*, y^*, z^*) \mid x^* \in B_x, y^* \in A_y, z^* \in B_z\} \\ \bar{A}_7 &= \{(x^*, y^*, z^*) \mid x^* \in B_x, y^* \in B_y, z^* \in A_z\} \\ \bar{A}_8 &= \{(x^*, y^*, z^*) \mid x^* \in B_x, y^* \in B_y, z^* \in B_z\}. \end{aligned}$$

For all equilibria in \bar{A}_1 , the corresponding characteristic equations are (7). From assumption (10), all equilibria in \bar{A}_1 are *saddle points of index 2*. For the equilibrium points in \bar{A}_2 , the corresponding characteristic equations are

$$\lambda^3 + (c - d_3k_3)\lambda^2 + b \left(1 - \frac{k_3d_3}{c}\right) \lambda + a \left(1 - \frac{k_3d_3}{c}\right) = 0. \quad (29)$$

Since $\lambda_1 + \lambda_2 + \lambda_3 = -(c - d_3k_3) > 0$ and $\lambda_1\lambda_2\lambda_3 = -a(1 - (k_3d_3)/c) > 0$, (29) has three positive eigenvalues, or one positive eigenvalue and two negative eigenvalues, or one positive eigenvalue and a pair of complex conjugate eigenvalues. Based on numerical observations, one may assume that (29)

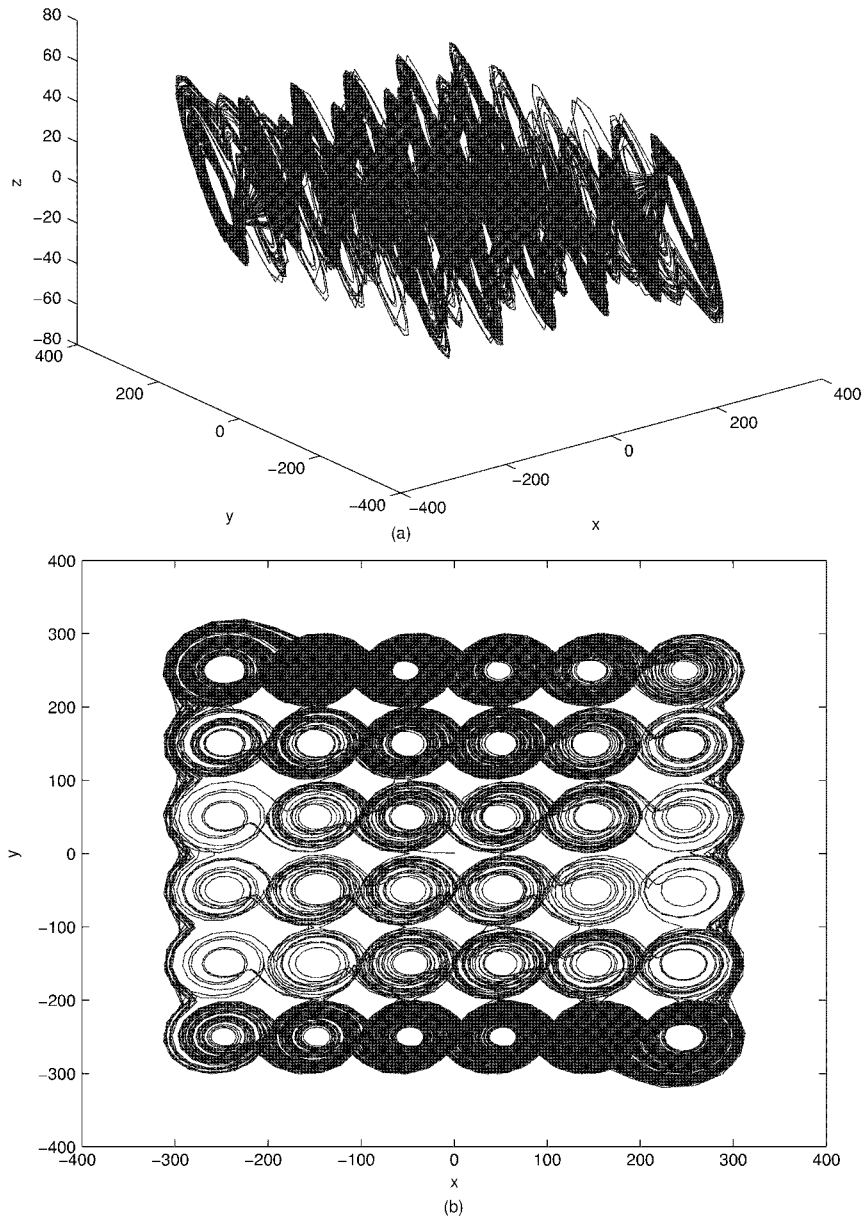


Fig. 7. Two-directional 6×6 -grid scroll chaotic attractors. (a) x - y - z space. (b) x - y plane projection.

has one positive eigenvalue and a pair of complex conjugate eigenvalues with negative real parts. Thus, all equilibria in \bar{A}_2 are *saddle points of index 1*. For all equilibria in \bar{A}_3 , the corresponding characteristic equations are (22).

According to the assumption in the last subsection, the equilibria in \bar{A}_3 are *saddle points of index 1*. For the equilibria in \bar{A}_4 , the corresponding characteristic equations are

$$\lambda^3 + (c - d_3k_3)\lambda^2 + (b - d_2k_2) \left(1 - \frac{k_3d_3}{c}\right) \lambda + a \left(1 - \frac{k_2d_2}{b}\right) \left(1 - \frac{k_3d_3}{c}\right) = 0. \quad (30)$$

Since $\lambda_1 + \lambda_2 + \lambda_3 = -(c - d_3k_3) > 0$ and $\lambda_1\lambda_2\lambda_3 = -a(1 - ((k_2d_2)/(b))(1 - (k_3d_3)/(c))) < 0$, (30) has one negative eigenvalue and two positive eigenvalues, or one negative eigenvalue and a pair of complex conjugate eigenvalues with positive

real parts. Numerical observations show that (30) has one negative eigenvalue and a pair of complex conjugate eigenvalues with positive real parts. Thus, the equilibria in \bar{A}_4 are *saddle points of index 2*. For all equilibria in \bar{A}_5 , the corresponding characteristic equations are (16). According to the assumption in Subsection B, all equilibria in \bar{A}_5 are *saddle points of index 1*. For the equilibria in \bar{A}_6 , the corresponding characteristic equations are

$$\lambda^3 + (c - d_3k_3)\lambda^2 + b \left(1 - \frac{k_3d_3}{c}\right) \lambda + (a - k_1d_1) \left(1 - \frac{k_3d_3}{c}\right) = 0. \quad (31)$$

Since $\lambda_1 + \lambda_2 + \lambda_3 = -(c - d_3k_3) > 0$ and $\lambda_1\lambda_2\lambda_3 = -(a - k_1d_1)(1 - (k_3d_3)/(c)) < 0$, (31) has one negative eigenvalue and two positive eigenvalues, or one negative eigenvalue and a pair of complex conjugate eigenvalues with positive real

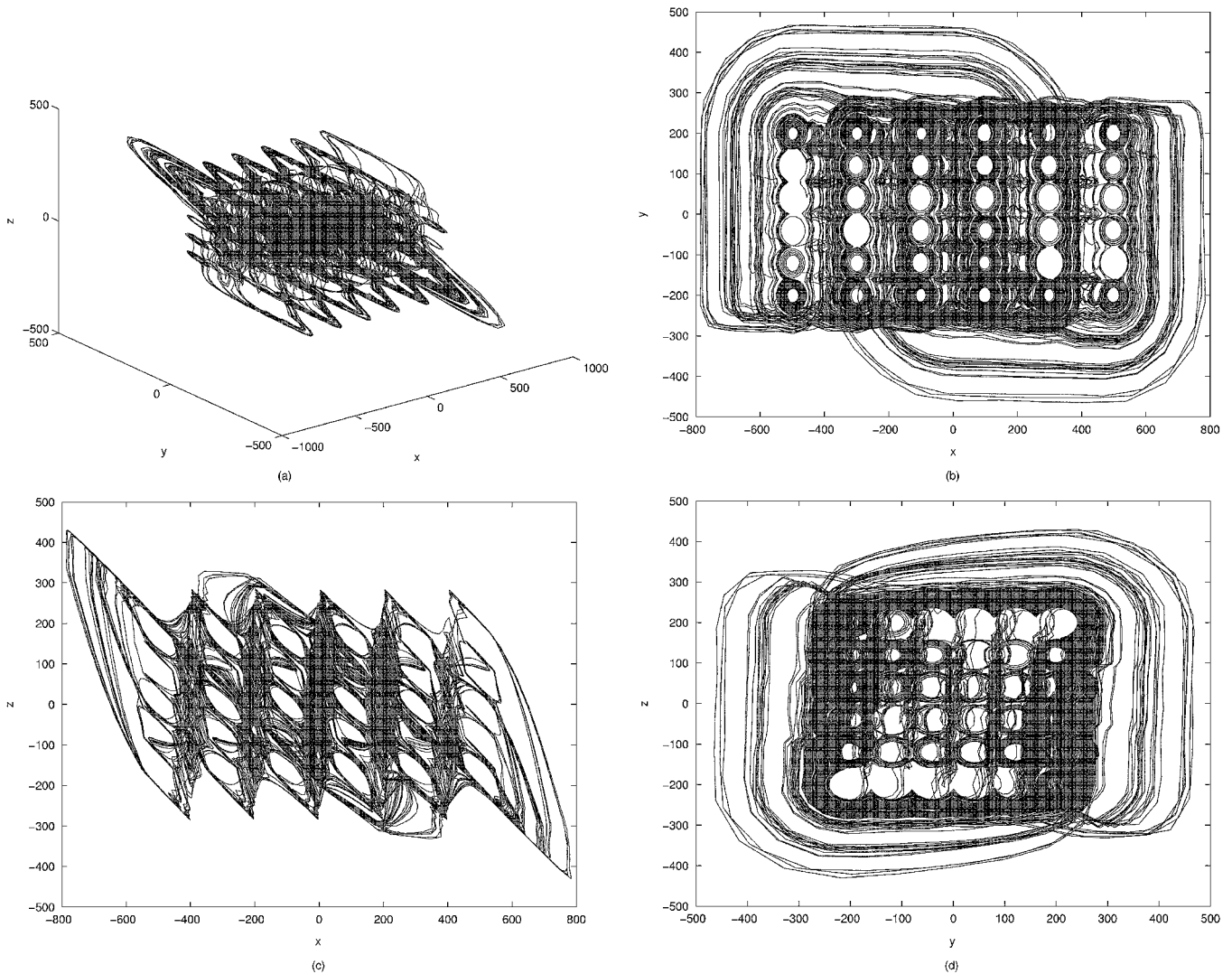


Fig. 8. Three-directional $6 \times 6 \times 6$ -grid scroll chaotic attractors. (a) x - y - z space. (b) x - y plane projection. (c) x - z plane projection. (d) y - z plane projection.

parts. Numerical simulations show that (31) has one negative eigenvalue and two positive eigenvalues. So the equilibria in \bar{A}_6 are *saddle points of index 1*. For all equilibria in \bar{A}_7 , the corresponding characteristic equations are (23). From the assumption in the last subsection, all equilibria in \bar{A}_7 are *saddle points of index 2*. Finally, consider all equilibria in \bar{A}_8 , the corresponding characteristic equations are

$$\lambda^3 + (c - d_3 k_3) \lambda^2 + (b - d_2 k_2) \left(1 - \frac{k_3 d_3}{c}\right) \lambda + (a - k_1 d_1) \left(1 - \frac{k_2 d_2}{b}\right) \left(1 - \frac{k_3 d_3}{c}\right) = 0. \quad (32)$$

Since $\lambda_1 + \lambda_2 + \lambda_3 = -(c - d_3 k_3) > 0$ and $\lambda_1 \lambda_2 \lambda_3 = -(a - k_1 d_1) \left(1 - \frac{k_2 d_2}{b}\right) \left(1 - \frac{k_3 d_3}{c}\right) > 0$, (32) has three positive eigenvalues, or one positive eigenvalue and two negative eigenvalues, or one positive eigenvalue and a pair of complex conjugate eigenvalues. Numerical observations show that (32) has one positive eigenvalue and a pair of complex conjugate eigenvalues with negative real parts. Then, the equilibria in \bar{A}_8 are *saddle points of index 1*.

It should be pointed out that the scrolls can be generated only around *saddle points of index 2* [17]–[19]. Therefore, only the equilibria in \bar{A}_1 , \bar{A}_4 , and \bar{A}_7 may create scrolls. However, numerical observations reveal that only the equilibria in \bar{A}_1 can generate scrolls. In fact, having a *saddle point of index 2* is only a necessary condition, but not a sufficient condition for generating scrolls. That is, system (24) has the potential to create a maximum of 3-D $(p_1 + q_1 + 2) \times (p_2 + q_2 + 2) \times (p_3 + q_3 + 2)$ -grid scroll chaotic attractor, called 3-D $n \times m \times l$ -grid scroll chaotic attractor, for some suitable parameters $a, b, c, d_1, d_2, d_3, k_1, h_1, k_2, h_2, k_3, h_3$. In particular, each equilibrium point in \bar{A}_1 corresponds to a unique 3-D *saturated plateau* and also corresponds to a unique scroll in the whole attractor. Furthermore, other equilibria in \bar{A}_i ($2 \leq i \leq 8$) correspond to the *saturated slopes* and are responsible for connecting the $(p_1 + q_1 + 2) \times (p_2 + q_2 + 2) \times (p_3 + q_3 + 2)$ scrolls.

Fig. 8 shows a $6 \times 6 \times 6$ -grid scroll chaotic attractor, where $a = d_1 = 0.7, b = c = d_2 = d_3 = 0.8, k_1 = 100, h_1 = 200, k_2 = k_3 = 40, h_2 = h_3 = 80, p_1 = p_2 = p_3 = q_1 = q_2 = q_3 = 2$. Obviously, there are six scrolls in each direction of the state space, as shown in Fig. 8(b), (c), and (d), respectively.

The Lyapunov exponent spectrum of this $6 \times 6 \times 6$ -grid scroll attractor includes $LE_1 = 0.0885$, $LE_2 = 0$, $LE_3 = -0.7157$. Note that these 3-D $n \times m \times l$ -grid scroll chaotic attractors are generated in exactly the same way as the 1-D and 2-D cases discussed before, except that the directions of the system trajectories are three here.

Remark 3: There are seven basic design strategies to obtain suitable circuit parameters for specified 3-D $n \times m \times l$ -grid scroll attractors: 1) parameters a, b, c satisfy condition (10); 2) parameters a, d_1, k_1, h_1 satisfy condition (13) where, for simplification, assume that $a = d_1$ and $h_1 = 2k_1$; 3) parameters b, d_2, k_2, h_2 satisfy condition (20) where, for simplification, assume that $b = d_2$ and $h_2 = 2k_2$; 4) parameters c, d_3, k_3, h_3 satisfy condition (27) where, for simplification, assume that $c = d_3$ and $h_3 = 2k_3$; 5) parameters p_1, q_1 control the numbers of scrolls in negative and positive x -directions, respectively; 6) parameters p_2, q_2 control the number of scrolls in negative and positive y -directions, respectively; 7) parameters p_3, q_3 control the number of scrolls in negative and positive z -directions, respectively.

IV. THEORETICAL ANALYSIS FOR MULTISCROLL CHAOTIC ATTRACTORS

A. Dynamical Analysis of Double-Scroll System (11)

Here, the dynamical behaviors of the double-scroll systems (11) are further investigated. In particular, a 2-D Poincaré return map [18], [26] is rigorously derived for verifying the chaotic behaviors of the double-scroll system (11).

Obviously, systems (12), (17), and (24) become system (11) in every corresponding subspace. Therefore, system (11) is the basic generator of the multiscroll chaotic systems (12), (17), and (24) and plays a very important role in chaos generation. When $a = b = c = d_1 = 0.7, k = 10$, system (11) has a double-scroll chaotic attractor as shown in Fig. 4. Obviously, (11) has three different subspaces

$$\begin{aligned} V_1 &= \{\mathbf{X} \mid x \geq 1\} \\ V_2 &= \{\mathbf{X} \mid |x| \leq 1\} \\ V_3 &= \{\mathbf{X} \mid x \leq -1\} \end{aligned}$$

where $\mathbf{X} = (x, y, z)^T$. System (11) has a natural symmetry under the coordinates transform $(x, y, z) \rightarrow (-x, -y, -z)$, which persists for all parameter values. The variation of the volume $V(t)$ of a small element, $\delta V(t) = \delta x \delta y \delta z$, in the state space is determined by the divergence of the flow

$$\nabla V = \frac{\partial \dot{x}}{\partial x} + \frac{\partial \dot{y}}{\partial y} + \frac{\partial \dot{z}}{\partial z} = -c < 0.$$

That is, system (11) is dissipative in each subspace.

For subspaces V_1 and V_3 , the dynamical equations are described by

$$\begin{pmatrix} \dot{\bar{x}} \\ \dot{\bar{y}} \\ \dot{\bar{z}} \end{pmatrix} = \begin{pmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -a & -b & -c \end{pmatrix} \begin{pmatrix} \bar{x} \\ \bar{y} \\ \bar{z} \end{pmatrix}$$

where

$$\begin{aligned} (\bar{x}, \bar{y}, \bar{z})^T &= \left(x - \frac{d_1 k_1}{a}, y, z \right)^T \quad \text{for } \mathbf{X} \in V_1, \\ (\bar{x}, \bar{y}, \bar{z})^T &= \left(x + \frac{d_1 k_1}{a}, y, z \right)^T \quad \text{for } \mathbf{X} \in V_3. \end{aligned}$$

Thus, the exact solution of the above equation is

$$\begin{cases} \bar{x}(t) = A_1 e^{\lambda_1 t} + e^{\alpha t} (A_2 \cos(\beta t) + A_3 \sin(\beta t)) \\ \bar{y}(t) = A_1 \lambda_1 e^{\lambda_1 t} + e^{\alpha t} [(A_2 \alpha + A_3 \beta) \cos(\beta t) \\ \quad + (A_3 \alpha - A_2 \beta) \sin(\beta t)] \\ \bar{z}(t) = A_1 \lambda_1^2 e^{\lambda_1 t} \\ \quad + e^{\alpha t} [(A_2 \alpha^2 + 2A_3 \alpha \beta - A_2 \beta^2) \cos(\beta t) \\ \quad + (A_3 \alpha^2 - 2A_2 \alpha \beta - A_3 \beta^2) \sin(\beta t)] \end{cases} \quad (33)$$

where coefficients are given at the bottom of the page, and λ_1, α, β are defined by (8) and (9). Denote solution (33) as

$$\begin{pmatrix} \bar{x}(t) \\ \bar{y}(t) \\ \bar{z}(t) \end{pmatrix} = \begin{pmatrix} g_1(t) \\ g_2(t) \\ g_3(t) \end{pmatrix} \begin{pmatrix} \bar{x}_0 \\ \bar{y}_0 \\ \bar{z}_0 \end{pmatrix}.$$

For subspace V_3 , the dynamical equation is described by

$$\begin{pmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{pmatrix} = \begin{pmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ d_1 k_1 - a & -b & -c \end{pmatrix} \begin{pmatrix} x \\ y \\ z \end{pmatrix}.$$

Clearly, the exact solution is

$$\begin{cases} x(t) = A'_1 e^{\lambda'_1 t} + e^{\alpha' t} (A'_2 \cos(\beta' t) + A'_3 \sin(\beta' t)) \\ y(t) = A'_1 \lambda'_1 e^{\lambda'_1 t} + e^{\alpha' t} [(A'_2 \alpha' + A'_3 \beta') \cos(\beta' t) \\ \quad + (A'_3 \alpha' - A'_2 \beta') \sin(\beta' t)] \\ z(t) = A'_1 \lambda'^2_1 e^{\lambda'_1 t} + e^{\alpha' t} [(A'_2 \alpha'^2 \\ \quad + 2A'_3 \alpha' \beta' - A'_2 \beta'^2) \cos(\beta' t) \\ \quad + (A'_3 \alpha'^2 - 2A'_2 \alpha' \beta' - A'_3 \beta'^2) \sin(\beta' t)] \end{cases} \quad (34)$$

where coefficients are given at the bottom of the next page, in which λ'_1 is the positive eigenvalue of (16), and α', β' are the real and imaginary parts of the pair of complex conjugate eigenvalues of (16). Denote solution (34) as

$$\begin{pmatrix} x(t) \\ y(t) \\ z(t) \end{pmatrix} = \begin{pmatrix} g'_1(t) \\ g'_2(t) \\ g'_3(t) \end{pmatrix} \begin{pmatrix} x_0 \\ y_0 \\ z_0 \end{pmatrix}.$$

$$\begin{aligned} A_1 &= \frac{(\alpha^2 + \beta^2)\bar{x}(0) - 2\alpha\bar{y}(0) + \bar{z}(0)}{(\lambda_1 - \alpha)^2 + \beta^2} \\ A_2 &= \frac{(\lambda_1^2 - 2\alpha\lambda_1)\bar{x}(0) + 2\alpha\bar{y}(0) - \bar{z}(0)}{(\lambda_1 - \alpha)^2 + \beta^2} \\ A_3 &= \frac{(\lambda_1\alpha^2 - \lambda_1\beta^2 - \lambda_1^2\alpha)\bar{x}(0) - (\beta^2 - \alpha^2 + \lambda_1^2)\bar{y}(0) + (\alpha - \lambda_1)\bar{z}(0)}{\beta[(\lambda_1 - \alpha)^2 + \beta^2]} \end{aligned}$$

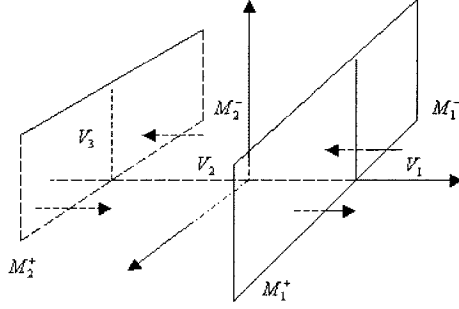


Fig. 9. Trajectory switchings of the double-scroll system (11).

Obviously, system (11) has two symmetrical switching planes: $M_1 \equiv \{\mathbf{X} | x = 1\}$ and $M_2 \equiv \{\mathbf{X} | x = -1\}$. Denote

$$\begin{aligned} M_1^+ &\equiv \{\mathbf{X} | x = 1, y > 0\} & M_1^- &\equiv \{\mathbf{X} | x = 1, y < 0\} \\ M_2^+ &\equiv \{\mathbf{X} | x = -1, y > 0\} & M_2^- &\equiv \{\mathbf{X} | x = -1, y < 0\}. \end{aligned}$$

and the corresponding switching rules are

$$\begin{aligned} \mathbf{X}(t^+) &= (1, y, z)^T \in V_2 & \text{if } \mathbf{X}(t) &= (1, y, z)^T \in M_1^- \\ \mathbf{X}(t^+) &= (-1, y, z)^T \in V_3 & \text{if } \mathbf{X}(t) &= (-1, y, z)^T \in M_2^- \\ \mathbf{X}(t^+) &= (-1, y, z)^T \in V_2 & \text{if } \mathbf{X}(t) &= (-1, y, z)^T \in M_2^+ \\ \mathbf{X}(t^+) &= (1, y, z)^T \in V_1 & \text{if } \mathbf{X}(t) &= (1, y, z)^T \in M_1^+ \end{aligned}$$

where $\mathbf{X} = (x, y, z)^T$.

Fig. 9 shows the trajectory switchings of system (11). Consider switching plane M_1 . If $y > 0, \dot{x} = y > 0$, the trajectories of system (11) will go through switching plane M_1^+ from V_2 to V_1 ; if $y < 0, \dot{x} = y < 0$, the trajectories of system (11) will go through switching plane M_1^- from V_1 to V_2 . For switching plane M_2 , if $y > 0, \dot{x} = y > 0$, the trajectories of system (11) will go through switching plane M_2^+ from V_3 to V_2 ; if $y < 0, \dot{x} = y < 0$, the trajectories of system (11) will go through switching plane M_2^- from V_2 to V_3 . Without loss of generality, assume that the initial point $x_0 \in V_1$. Then, after a long enough time, it will definitely arrive at the switching plane M_1^- . From the switching rules, this trajectory will go through M_1^- from V_1 to V_2 . After a long enough time, it will definitely reach M_1^+ or M_2^- ; if it arrives at M_1^+ , it will go through switching plane M_1^+ from V_2 to V_1 and begin a new cycle; if it reaches M_2^- , according to the switching rules, it will go through switching plane M_2^- from V_2 to V_3 . After a long enough time, this trajectory will definitely arrive at switching plane M_2^+ ; from the switching rules, this trajectory will go through switching plane M_2^+ from

V_3 to V_2 . After some time, it will reach switching plane M_2^- or M_1^+ ; if it arrives at M_2^- , it will repeat the former process; if it reaches M_1^+ , according to the switching rules, it will go through the switching plane M_1^+ from V_2 to V_1 and begin a new cycle. Therefore, the running routes of this trajectory can be classified into three different cases

$$\begin{aligned} V_1 &\rightarrow M_1^- \rightarrow V_2 \rightarrow M_1^+ \rightarrow V_1 \\ V_1 &\rightarrow M_1^- \rightarrow V_2 \rightarrow M_2^- \rightarrow V_3 \\ &\rightarrow M_2^+ \rightarrow V_2 \rightarrow M_1^+ \rightarrow V_1 \\ V_1 &\rightarrow M_1^- \rightarrow V_2 \rightarrow M_2^- \rightarrow V_3 \\ &\rightarrow M_2^+ \rightarrow V_2 \rightarrow M_2^- \\ &\rightarrow \dots \rightarrow V_2 \rightarrow M_1^+ \rightarrow V_1. \end{aligned}$$

In the following, a 2D Poincaré return map is rigorously constructed for verifying the chaotic behaviors of the double-scroll attractor.

Without loss of generality, consider a trajectory started from an initial point $(1, y_0, z_0) \in M_1$ at $t = 0$. If $(1, y_0, z_0) \in M_1 - M_1^-$, according to the exact solution (33), it must reach M_1^- at the positive time t_1 . Let $(1, y_1, z_1) \in M_1^-$ be the hitting point. One can get the arriving time t_1 and the positions y_1 and z_1 by using the solution (33). If $(1, y_0, z_0) \in M_1^-$, according to the solution (34), it must reach M_1 and M_2 at the positive time t_2 and t_3 , respectively, without switchings. Here, t_2 and t_3 are the first arriving time. Let $(1, y_2, z_2) \in M_1$ be the hitting point. One can get the arriving time t_2 and positions y_2 and z_2 by using the solution (34). Similarly, for the hitting point $(1, y_3, z_3) \in M_2$, one can get the arriving time t_3 and positions y_3 and z_3 . Now, one can define a region by

$$\Gamma = \{(1, y, z) \in M_1^- | t_2 < t_3\}.$$

Thus, if $(1, y_0, z_0) \in \Gamma$, this trajectory will arrive at $(1, y_2, z_2) \in M_1^+$ at the positive time t_2 ; if $(1, y_0, z_0) \in M_1^- - \Gamma$, this trajectory will reach $(-1, y_3, z_3) \in M_2^-$ at the positive time t_3 . According to the switching rules, this trajectory will go through switching plane M_2^- at time t_3 from V_2 to V_3 . Due to the symmetry of the vector fields in both V_1 and V_3 , a trajectory started from $(-1, y_3, z_3)$ in V_3 is symmetric to that started from $(1, -y_3, -z_3)$ on M_1^+ in V_1 . Here, one can define a 2D Poincaré return map by

$$\mathbf{F} : M_1 \rightarrow M_1, (y_0, z_0) \rightarrow \begin{cases} (y_1, z_1) & \text{for } (y_0, z_0) \in M_1 - M_1^- \\ (y_2, z_2) & \text{for } (y_0, z_0) \in \Gamma \\ (-y_3, -z_3) & \text{for } (y_0, z_0) \in M_1 - \Gamma. \end{cases} \quad (35)$$

$$A'_1 = \frac{(\alpha'^2 + \beta'^2)x(0) - 2\alpha'y(0) + z(0)}{(\lambda'_1 - \alpha')^2 + \beta'^2}$$

$$A'_2 = \frac{(\lambda'^2_1 - 2\alpha'\lambda'_1)x(0) + 2\alpha'y(0) - z(0)}{(\lambda'_1 - \alpha')^2 + \beta'^2}$$

$$A'_3 = \frac{(\lambda'_1\alpha'^2 - \lambda'_1\beta'^2 - \lambda'^2_1\alpha')x(0) - (\beta'^2 - \alpha'^2 + \lambda'^2_1)y(0) + (\alpha' - \lambda'_1)z(0)}{\beta'[(\lambda'_1 - \alpha')^2 + \beta'^2]}$$

Note that one can write a rigorously mathematical formulation for this map by using the exact solutions (33) and (34), as follows:

$$\begin{pmatrix} 1 - 10 \\ y_1 \\ z_1 \end{pmatrix} = \begin{pmatrix} g_1(t_1) \\ g_2(t_1) \\ g_3(t_1) \end{pmatrix} \begin{pmatrix} 1 - 10 \\ y_0 \\ z_0 \end{pmatrix}$$

$$\begin{pmatrix} 1 \\ y_2 \\ z_2 \end{pmatrix} = \begin{pmatrix} g'_1(t_2) \\ g'_2(t_2) \\ g'_3(t_2) \end{pmatrix} \begin{pmatrix} 1 \\ y_0 \\ z_0 \end{pmatrix}$$

and

$$\begin{pmatrix} -1 \\ y_3 \\ z_3 \end{pmatrix} = \begin{pmatrix} g''_1(t_3) \\ g''_2(t_3) \\ g''_3(t_3) \end{pmatrix} \begin{pmatrix} 1 \\ y_0 \\ z_0 \end{pmatrix}.$$

Moreover, the Jacobian of this map \mathbf{F} is described by

$$D\mathbf{F} = \begin{cases} \begin{pmatrix} \frac{\partial y_1}{\partial y_0} & \frac{\partial y_1}{\partial z_0} \\ \frac{\partial z_1}{\partial y_0} & \frac{\partial z_1}{\partial z_0} \end{pmatrix}, & \text{for } (y_0, z_0) \in M_1 - M_1^- \\ \begin{pmatrix} \frac{\partial y_2}{\partial y_0} & \frac{\partial y_2}{\partial z_0} \\ \frac{\partial z_2}{\partial y_0} & \frac{\partial z_2}{\partial z_0} \end{pmatrix}, & \text{for } (y_0, z_0) \in \Gamma \\ -\begin{pmatrix} \frac{\partial y_3}{\partial y_0} & \frac{\partial y_3}{\partial z_0} \\ \frac{\partial z_3}{\partial y_0} & \frac{\partial z_3}{\partial z_0} \end{pmatrix}, & \text{for } (y_0, z_0) \in M_1 - \Gamma. \end{cases} \quad (36)$$

Therefore, one can get the exact mathematical formulations for the Lyapunov exponents LE_1, LE_2 of the mapping \mathbf{F} from (36). However, the formulations are rather complex. In real calculations, one can use the numerical methods described in [29] to calculate the maximum Lyapunov exponent LE_1 . If $0 < LE_1 < +\infty$, system (11) has a double-scroll chaotic attractor. Fig. 10(a) shows the Poincaré mapping of double-scroll attractor at section M_1 ; Fig. 10(b) displays the Poincaré mapping of the double-scroll attractor at section M_2 . It is clear that these two mappings are symmetric from a theoretical view, but there are some small differences due to calculating errors. Moreover, one can also rigorously prove the chaotic behavior of the double-scroll attractor by using the Homoclinic Šilnikov Theorem in [19]. The detailed proof is similar to the proof of Chua's double-scroll attractor [18] and thus is omitted here.

B. Dynamical Analysis of Multi-Scroll Systems

Here, the dynamical behaviors of multiscroll systems (12), (17), and (24) are briefly discussed.

Note that the multiscroll systems (12), (17), and (24) can be represented by a unified hybrid system, which can be regarded as a linear system with a saturated function series PWL feedback controller. It is described by

$$\dot{\mathbf{X}} = \mathbf{A}\mathbf{X} + \mathbf{B}\varphi(\mathbf{C}\mathbf{X}) \quad (37)$$

where $\mathbf{X} = (x, y, z)^T$ is the state vector, and

$$\mathbf{A} = \begin{pmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -a & -b & -c \end{pmatrix}$$

$$\mathbf{B} = \begin{pmatrix} 0 & -\frac{d_2}{b} & 0 \\ 0 & 0 & -\frac{d_3}{c} \\ d_1 & d_2 & d_3 \end{pmatrix}$$

$$\mathbf{C} = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}.$$

Clearly, it can be classified into three different cases as follows:

a) 1-D n -scroll chaotic attractor: With

$$\varphi(\mathbf{C}\mathbf{X}) = \begin{pmatrix} f(x; k_1, h_1, p_1, q_1) \\ 0 \\ 0 \end{pmatrix}$$

system (37) becomes system (12).

b) 2-D $n \times m$ -grid scroll chaotic attractor: With

$$\varphi(\mathbf{C}\mathbf{X}) = \begin{pmatrix} f(x; k_1, h_1, p_1, q_1) \\ f(y; k_2, h_2, p_2, q_2) \\ 0 \end{pmatrix}$$

system (37) becomes system (17).

c) 3-D $n \times m \times l$ -grid scroll chaotic attractor: With

$$\varphi(\mathbf{C}\mathbf{X}) = \begin{pmatrix} f(x; k_1, h_1, p_1, q_1) \\ f(y; k_2, h_2, p_2, q_2) \\ f(z; k_3, h_3, p_3, q_3) \end{pmatrix}$$

system (37) becomes system (24).

Suykens *et al.* discussed the similar link between the multi-scroll chaotic attractors and the recurrent neural networks in [4]. It should be pointed out that system (37) has some very good analytical properties. This is because system (37) is continuous in \mathbf{R}^3 . However, the corresponding hysteresis multiscroll system in [16] and stair multiscroll systems in [10] are discontinuous in all switching points.

Assume that $a = d_1, b = d_2, c = d_3, h_1 = 2k_1, h_2 = 2k_2, h_3 = 2k_3$. Consider system (12). When $x \in [ih_1 - (h_1/2), ih_1 + (h_1/2)] (p_1 - 1 \leq i \leq q_1 - 1)$, let $x = x' + ih_1, y = y', z = z'$. Then, $f(x; k_1, h_1, p_1, q_1) = f_0(x'; k_1) + 2k_1i$ from (5). Therefore, system (12) becomes

$$\begin{cases} \dot{x}' = y' \\ \dot{y}' = z' \\ \dot{z}' = -ax' - by' - cz' + d_1f_0(x'; k_1) \end{cases}$$

where $x' \in [-(h_1/2), (h_1/2)]$.

It is noticed that this system is the double-scroll system (11) with $x \in [-(h_1/2), (h_1/2)]$. When $x \geq q_1h_1 - (h_1/2)$ (or $x \leq -p_1h_1 + (h_1/2)$), let $x = x' + q_1h_1, y = y', z = z'$ (or $x = x' - p_1h_1, y = y', z = z'$). Then, system (17) is equivalent to the double-scroll system (11) with $x' \geq -(h_1/2)$ (or $x \leq (h_1/2)$). Similarly, for the multiscroll system (17), let $x = x' + ih_1, y = y' + jh_2, z = z'$. Then, system (17) becomes the double-scroll system (11) in the corresponding subspaces. For the multiscroll system (24), let $x = x' + ih_1, y = y' + jh_2, z = z' + kh_3$. Then system (24) is equivalent to the double-scroll system (11) in the corresponding subspaces. That is, in each subspace, system (37) has the same dynamical behaviors as the double-scroll system (11). In essence, system (37) assembles the dynamical behaviors of system (11) with different initial values in different subspaces by its displacements in x, y, z -directions. It is easy to understand why the *saturated plateaus* of system (37) play an important role in the process of multiscroll generation.

According to (5), parameters p_i, q_i ($1 \leq i \leq 3$) determine the number of the *saturated plateaus* in the x, y, z -directions. Moreover, each *saturated plateau* corresponds to a unique scroll and also determines the position of the scroll. In fact, one can arbitrarily design the number and also the position of the scrolls of the multiscroll system (37). One can also rotate the multiscroll chaotic attractors to any desired orientation in the state space.

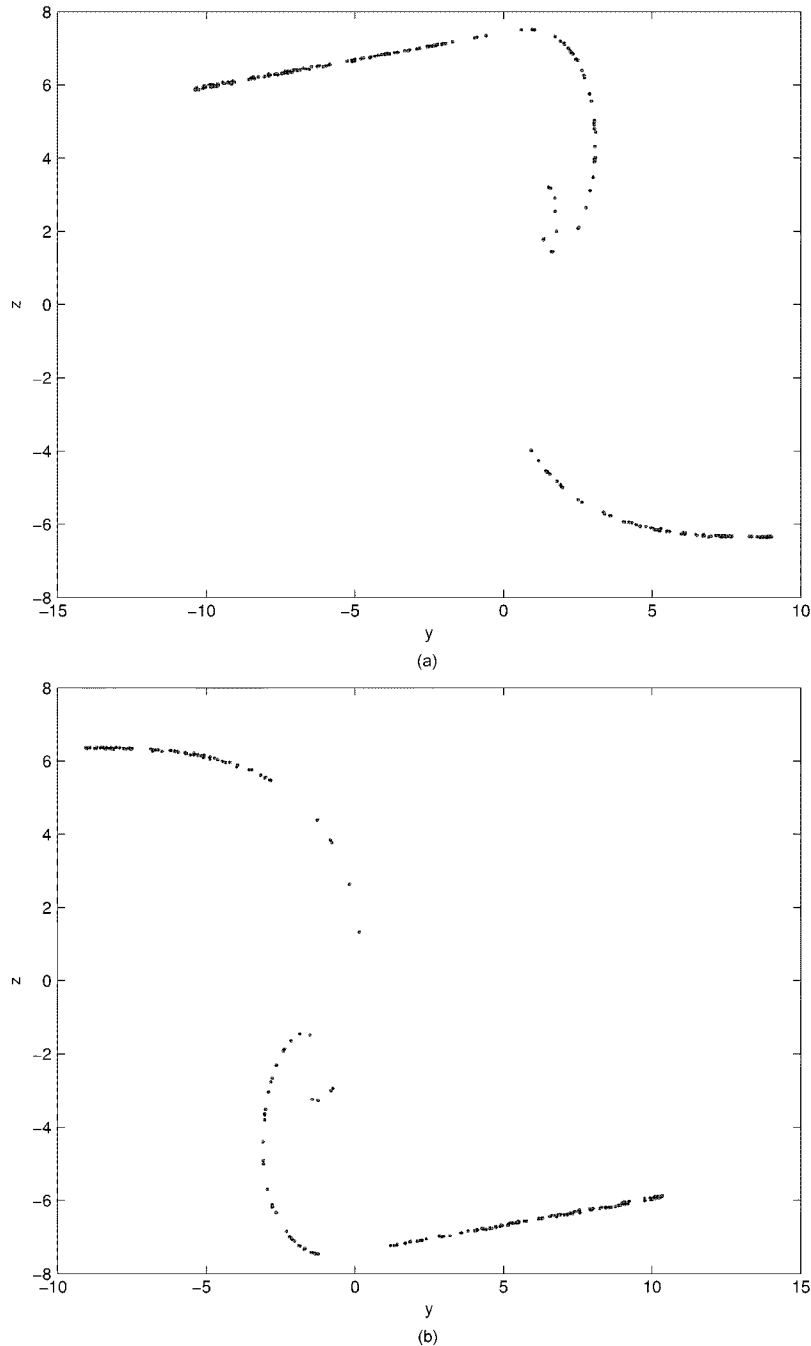


Fig. 10. Poincaré mapping of the double-scroll attractor. (a) Section M_1 . (b) Section M_2 .

Every PWL part has one and only one equilibrium point; however, only the equilibrium points in the *saturated plateaus* can generate scrolls. The trajectories of system (37) are repeatedly stretched and folded in the state space for infinitely many times via saturated function series switchings, leading to the appearance of complex dynamical behaviors. Note that system (37) is PWL and has an exact analytic solution in every subspace. However, the dynamical behaviors of the entire system become rather complex due to the saturated function series switchings.

Consider the 1-D n -scroll system (12). Obviously, system (12) has a 1-D $(p_1 + q_1 + 2)$ -scroll chaotic attractor, which has $2(p_1 + q_1) + 3$ equilibria, located in the x -axis. Note that system (12) has $p_1 + q_1 + 2$ *saturated plateaus*, and each *saturated plateau* corre-

sponds to a unique equilibrium point of index 2. Other $p_1 + q_1 + 1$ equilibria of index 1 correspond to $p_1 + q_1 + 1$ *saturated slopes* between these *saturated plateaus*, respectively. Denote

$$E_{-p_1} = \left(-\infty, -p_1 h_1 + \frac{h_1}{2} \right]$$

$$E_i = \left[i h_1 - \frac{h_1}{2}, i h_1 + \frac{h_1}{2} \right],$$

for $-p_1 + 1 \leq i \leq q_1 - 1$

$$E_{q_1} = \left[q_1 h_1 - \frac{h_1}{2}, +\infty \right).$$

When $h_1 = 2k_1$, for each interval E_i ($-p_1 \leq i \leq q_1$) of variable x , system (12) has the same dynamical behaviors as the double-

scroll system (11), which can be verified by using a displacement transformation $x' = x - ih_1, y' = y, z' = z$ with $-p_1 \leq i \leq q_1$. Thus, one can get the exact solution of system (12) in each subspace. When $p_1 = q_1$, system (12) has a natural symmetry under the coordinates transform $(x, y, z) \rightarrow (-x, -y, -z)$, which persists for all values of the system parameters.

Consider the 2-D $n \times m$ -grid scroll system (17). Clearly, system (17) has a 2-D $(p_1 + q_1 + 2) \times (p_2 + q_2 + 2)$ -grid scroll chaotic attractor, which has $(2p_1 + 2q_1 + 3) \times (2p_2 + 2q_2 + 3)$ equilibria, located in the x - y plane. It is noticed that system (17) has $(p_1 + q_1 + 2) \times (p_2 + q_2 + 2)$ 2-D *saturated plateaus*, and each *saturated plateau* corresponds to a unique equilibrium point of index 2. Other equilibria correspond to the *saturated slopes* between these *saturated plateaus*, respectively.

Denote

$$\begin{aligned} F_{-p_2} &= \left(-\infty, -p_2 h_2 + \frac{h_2}{2} \right) \\ F_j &= \left[j h_2 - \frac{h_2}{2}, j h_2 + \frac{h_2}{2} \right], \\ &\quad \text{for } -p_2 + 1 \leq j \leq q_2 - 1 \\ F_{q_2} &= \left[q_2 h_2 - \frac{h_2}{2}, +\infty \right). \end{aligned}$$

When $h_1 = 2k_1, h_2 = 2k_2$, for each region $\Omega_{ij} = \{(x, y) \mid x \in E_i, y \in F_j\} (-p_1 \leq i \leq q_1; -p_2 \leq j \leq q_2)$, system (17) has the same dynamical behaviors as the double-scroll system (11), which can be verified by using a displacement transformation $x' = x - ih_1, y' = y - jh_2, z' = z$ for $-p_1 \leq i \leq q_1$ and $-p_2 \leq j \leq q_2$. Thus, one can get the exact solution of system (17) in each subspace. When $p_1 = q_1, p_2 = q_2$, system (17) has a natural symmetry under the coordinates transform $(x, y, z) \rightarrow (-x, -y, -z)$, which persists for all values of the system parameters.

Consider the 3-D $n \times m \times l$ -grid scroll system (24). Obviously, system (24) has a 3-D $(p_1 + q_1 + 2) \times (p_2 + q_2 + 2) \times (p_3 + q_3 + 2)$ -grid scroll chaotic attractor, which has $(2p_1 + 2q_1 + 3) \times (2p_2 + 2q_2 + 3) \times (2p_3 + 2q_3 + 3)$ equilibria. Notice that system (24) has $(p_1 + q_1 + 2) \times (p_2 + q_2 + 2) \times (p_3 + q_3 + 2)$ 3-D *saturated plateaus*, and each *saturated plateau* corresponds to a unique equilibrium point of index 2. Other equilibria correspond to the *saturated slopes* between these *saturated plateaus*, respectively.

Denote

$$\begin{aligned} G_{-p_3} &= \left(-\infty, -p_3 h_3 + \frac{h_3}{2} \right) \\ G_k &= \left[k h_3 - \frac{h_3}{2}, k h_3 + \frac{h_3}{2} \right], \\ &\quad \text{for } -p_3 + 1 \leq k \leq q_3 - 1 \\ G_{q_3} &= \left[q_3 h_3 - \frac{h_3}{2}, +\infty \right). \end{aligned}$$

When $h_1 = 2k_1, h_2 = 2k_2, h_3 = 2k_3$, for each subspace $\Gamma_{ijk} = \{(x, y, z) \mid x \in E_i, y \in F_j, z \in G_k\} (-p_1 \leq i \leq q_1; -p_2 \leq j \leq q_2; -p_3 \leq k \leq q_3)$, system (24) has the same dynamical behaviors as the double-scroll system (11), which can be verified by using a displacement transformation $x' = x - ih_1, y' = y - jh_2, z' = z - kh_3$ for $-p_1 \leq i \leq q_1, -p_2 \leq j \leq q_2$, and $-p_3 \leq k \leq q_3$. Then, one can get the exact solution of system (24) in each subspace. When $p_1 = q_1, p_2 = q_2, p_3 = q_3$,

system (24) has a natural symmetry under the coordinates transform $(x, y, z) \rightarrow (-x, -y, -z)$, which persists for all values of the system parameters.

Similarly, the 2D Poincaré return maps can be constructed and used to prove the chaotic behaviors of the multiscroll systems (12), (17), and (24). However, their constructing processes are similar but rather complex, and hence are omitted here.

V. CONCLUSION

This paper has initiated a saturated function series approach for generating multiscroll chaotic attractors, including 1-D n -scroll, 2-D $n \times m$ -grid scroll, and 3-D $n \times m \times l$ -grid scroll attractors, from a given 3D linear autonomous system with a saturated function series as the controller. The dynamical behaviors and chaos generation mechanism of multiscroll systems have been further investigated by analyzing the system trajectories. In particular, a 2D Poincaré return map has been rigorously constructed for verifying the chaotic behaviors of the double-scroll attractor.

It should be pointed out that one can arbitrarily design a desired number of scrolls and their spatial positions and orientations by using this developed systematic methodology. Furthermore, it is relatively easy to design physical electronic circuits to experimentally verify these multiscroll chaotic attractors since the saturated circuit is a basic electrical circuit.

Finally, it can be foreseen that various related bifurcation phenomena in the generated multiscroll chaotic systems deserve further investigation in the near future.

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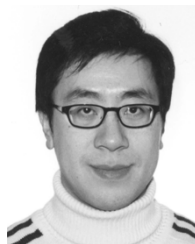
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