

Design of Dual-band Frequency Selective Surface with Miniaturized Elements

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Abstract—A new dual-band frequency selective surface (FSS) is introduced in this paper. By having a miniaturized unit cell size, the proposed FSS transmission response shows minimal sensitivity to the angle of the incident electromagnetic wave. The two passband frequencies of the proposed configuration can be controlled independently by tuning the unit cell geometrical parameters appropriately. An equivalent circuit model analysis is presented to provide an insightful synthesis procedure for the filter. Full-wave numerical electromagnetic simulations are used to confirm the analysis and synthesis method presented based on the circuit model.

Index Terms—Dual-band, Frequency selective surface, periodic structures, spatial filter.

I. INTRODUCTION

Frequency selective surfaces are spatial filters that are widely used in radomes for antennas, microwave absorbers, microwave lenses, reflect array antennas etc. [1]–[6]. A frequency selective surface (FSS) is usually formed by periodic arrays of metallic patterns that are printed on dielectric substrates. The important design specifications in FSSs are the low sensitivity of the transmission response with respect to the oblique angles of the incident electromagnetic wave, the low-order harmonic contents of the response, and the ability to operate in close proximity to the radiation source [1].

In advanced microwave systems, e.g. used in aircraft and shipping, multiband FSSs are needed to cover different operational frequency bands [7]. Different schemes are proposed so far for designing multiband FSSs such as: using fractal metallic arrays [8], [9], perturbation techniques [10] and genetic algorithms [11], [12]. In most of the presented structures, the unit cell size or element spacing is comparable to the resonance wavelength and this makes them sensitive to the incident angle of the electromagnetic wave and causes undesirable low-order harmonics in the frequency response. Recently, new types of dual-band frequency selective surfaces have been introduced in [7], [13], [14] that make use of non-resonant elements in their structures. These recent designs show a lower dependency to oblique angles of the incident wave. However, the element sizes are not small enough (around $\lambda_0/6$) for the applications where the FSS should be used in very close proximity to the radiation source.

In this paper, a dual-band FSS is designed with the unit cell size as small as $\lambda_0/10$. The proposed FSS is composed of an inductive wire grid and an array of square-loop cells that are printed on the two sides of a thin dielectric substrate. The new

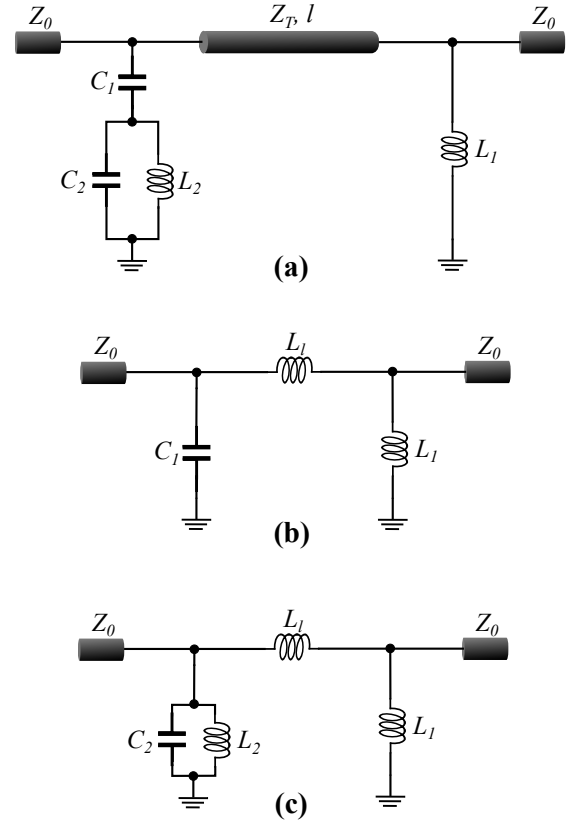


Fig. 1. (a) Equivalent circuit model of the dual-band filter. (b) Simplified circuit model for the first operational passband. (c) Simplified circuit model for the second operational passband.

design provides the advantage of controlling the two passband frequencies independently by varying the physical parameters of the unit cells. The synthesis method and design procedure of the proposed FSS will be presented in the next sections.

II. THE DESIGN PRINCIPLE

Fig. 1.(a) shows the basic circuit model of the dual-band microwave filters that forms the foundation of the proposed FSS. The filter is composed of a hybrid resonator separated from an inductor through a short piece of transmission line. The hybrid resonator is composed of a parallel LC resonance circuit of L_2 , C_2 that is in series with the capacitor C_1 . The transmission line has the length l and the characteristic impedance of Z_l . The frequency of the first passband is mainly

determined by L_1 , C_1 and the length of the transmission line l . On the other hand, the second passband frequency is dominated by L_2 , C_2 . Fig. 1.(b) shows the equivalent circuit model of the filter for the first passband. In this model, it is assumed that the two passbands frequencies are sufficiently separated so that, L_2C_2 possesses a low impedance and can be ignored. The transmission line ($l \ll \lambda$) is replaced with L_1 inductor. Therefore, by using a simple circuit analysis, the frequency of the first passband can be found as

$$f_1 \approx \frac{1}{2\pi\sqrt{C_1(L_1 + L_l)}}. \quad (1)$$

If the relative permeability of the transmission line is considered to be μ_r , L_l can be calculated as [1]

$$L_l = \mu_0\mu_rl. \quad (2)$$

So,

$$f_1 \approx \frac{1}{2\pi\sqrt{C_1(L_1 + \mu_0\mu_rl)}}. \quad (3)$$

At the second passband, the parallel L_2C_2 is dominant and the filter can be modelled by the circuit of Fig. 1.(c). For this passband, the effect of C_1 is ignored and the second passband frequency is approximated as

$$f_2 \approx \frac{1}{2\pi}\sqrt{\frac{1}{C_2}\left(\frac{1}{L_2} + \frac{1}{L_1 + L_T}\right)}. \quad (4)$$

The circuit shows a transmission zero that is arisen from the hybrid resonator of C_1 , L_2 and C_2 . This zero notch separates the two passbands and improves the out of band rejection of the filter. From Fig. 1.(a), this zero frequency can be obtained as

$$f_z = \frac{1}{2\pi\sqrt{L_1(C_1 + C_2)}}. \quad (5)$$

From (1) it is found that the first passband frequency (f_1) is independent of C_2 . Also, (4) shows that f_2 is not dependent on C_1 . This allows to control the two passband frequencies independently. This characteristic will be studied in detail in simulations.

III. FSS SYNTHESIS BASED ON THE CIRCUIT MODEL

A dual-band frequency selective surface can be synthesized by using the filter model described in the previous section. A 3-D view of the synthesized FSS is shown in Fig. 2. The structure is composed of two metallic arrays that are separated from each other by a dielectric substrate with a thickness of l . The back layer is composed of a metallic wire grid, which presents the inductor L_1 of the equivalent circuit. By interacting with the normal incident electromagnetic wave, this wire grid shows an inductive behaviour where, increasing w or decreasing D will decrease the inductance of L_1 . The top layer on the other side comprises a square-loop array that presents the hybrid resonator (C_1, L_2, C_2) of the equivalent circuit in Fig. 1. In this pattern, each square-loop cell has a side length of $D - g$ and the adjacent cells are separated from each other

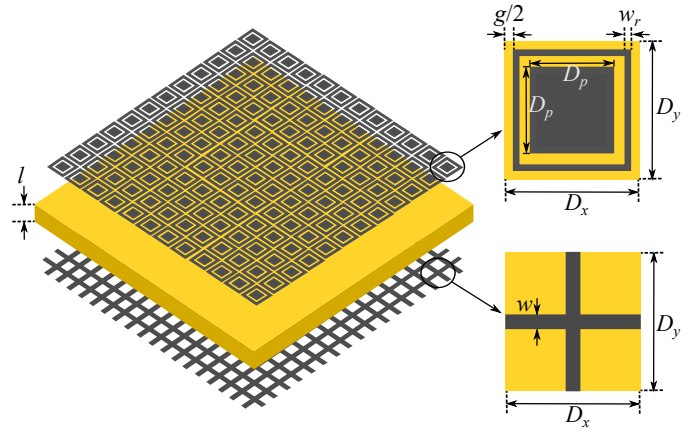


Fig. 2. Topology of the synthesized dual-band FSS. The unit cells of the top and bottom metallic arrays are shown on the right hand side of the figure. The black shading denotes the metal.

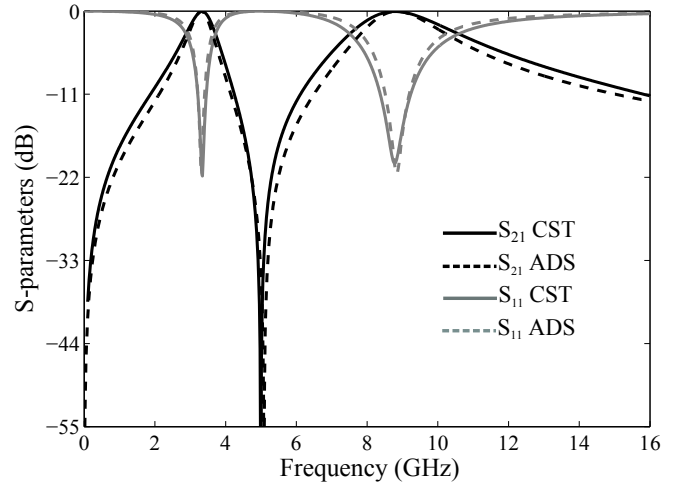


Fig. 3. Free space full wave simulation result of the designed dual-band FSS using periodic boundary condition in CST in comparison with the ADS circuit model simulation results.

by a distance of g . The gap between the unit cells show a capacitive effect to the incident wave. This capacitive effect is denoted by C_1 of the hybrid resonator where, increasing g causes a smaller C_1 . In addition, the loop and square patch in each unit cell provide the parallel L_1C_1 resonance behaviour where L_1 is provided by the inductive effect of the loop sides and C_1 is provided by the capacitive effect between the square patch and the loop sides. In the top pattern, increasing w_r causes a smaller L_2 and decreasing D_P causes a smaller C_2 .

TABLE I
PHYSICAL AND EQUIVALENT CIRCUIT PARAMETERS OF THE DESIGNED DUAL-BAND FSS

Parameter	g	w	w_r	D_x, D_y	D_P
Value	0.1 mm	0.2 mm	0.15 mm	8.8 mm	8 mm
Parameter	L_1	L_2	C_1	C_2	Z_T
Value	2.8 nH	0.98 nH	0.54 pF	0.46 pF	254 Ω

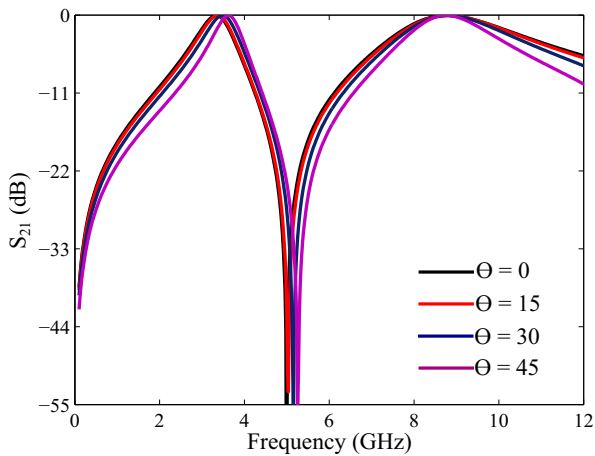


Fig. 4. Full wave simulation results of the transmission coefficient of the designed FSS as function of the electromagnetic wave incident angle.

IV. SIMULATION RESULTS AND DISCUSSIONS

Based on the circuit model and the procedure discussed above, a dual-band FSS with passbands at S- and X-bands with central frequencies of 3.3 and 9.5 GHz has been designed and simulated in CST Microwave Studio full wave simulator. The physical parameters of the designed FSS are listed in Table I together with its equivalent circuit parameters values. The top and bottom metallic layers are patterned on the both sides of 0.254 mm thick Rogers RO5880 dielectric substrate with the relative permittivity of $\epsilon_r = 2.2$ and loss tangent of $\tan\delta = 0.0009$. The full wave simulations are carried out using unit cell boundary condition that simulates an infinite array of unit FSS cells that are exposed to an arbitrary incident angle electromagnetic wave. On the other hand, the equivalent circuit of the FSS (Fig. 1) is simulated in ADS using the parameters listed in Table I. These circuit parameters are optimized by curve fitting using ADS. The full wave simulation results of the FSS are plotted in Fig. 3 together with the results obtained by using ADS. As seen, there is a good agreement between the full wave and circuit model simulations. The passband frequencies of the filter are 3.3 and 8.6 GHz with transmission zero at around 5 GHz that improves the out of band rejection of the FSS.

The scan performance of the designed FSS is shown in Fig. 4 showing a low sensitivity to oblique angle of the incident electromagnetic wave. This low sensitivity arises from the miniaturized unit cell size since the unit cell dimension is as small as $\lambda_0/10$ where, λ_0 is the wavelength at the first operational passband. This feature provides a freedom to use the designed FSS in the applications with non-planar incident phase fronts [13].

As discussed in Section II, the two passband frequencies of the proposed FSS can be controlled independently by controlling C_1 and C_2 element values. The value of the C_1 capacitor can be tuned by varying the gap between adjacent square-loop unit cells (g) where decreasing g increases C_1 and shifts the first passband frequency downward without affecting f_2 . This phenomenon is investigated using the full simulations in CST by changing g and the results are shown in Fig. 5. As

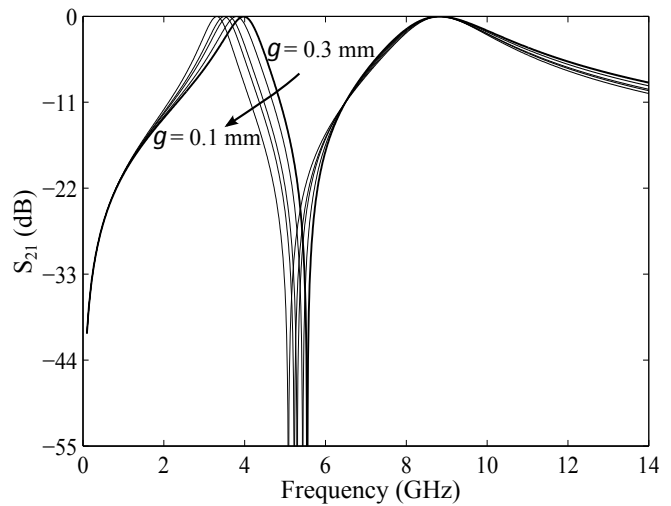


Fig. 5. Full wave simulation of the transmission coefficient of the dual-band FSS as a function of the g . In simulations g is varied from 0.1 mm to 0.3 mm with a step size of 0.05 mm.

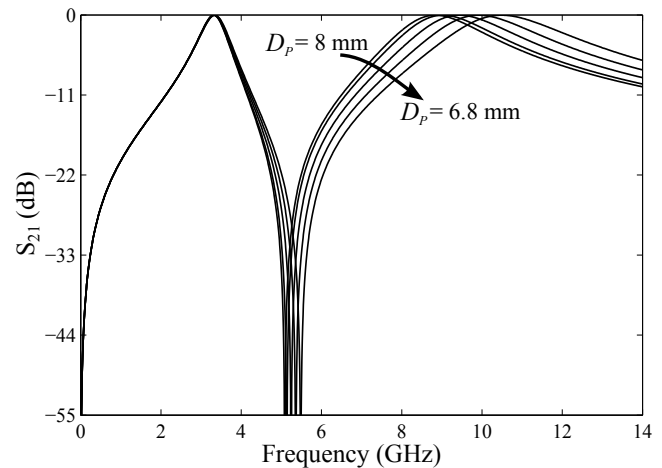


Fig. 6. Full wave simulation of the transmission coefficient of the dual-band FSS as a function of the D_P . In simulations D_P is varied from 8 mm to 6.8 mm with a step size of 0.2 mm.

demonstrated in Fig. 5, the larger value of g causes a lower f_1 without a significant effect on the second passband frequency.

On the other hand, the C_2 capacitor can be tuned by changing the square patch size D_P . A larger D_P causes a larger C_2 which shifts the upper passband frequency downward without sensible change in f_1 . Fig. 6 demonstrates the full wave simulation results of D_P variations effect on the FSS transmission response. As seen, a larger D_P leads to a lower f_2 without significant variation in the lower passband frequency, confirming the analysis presented in Section II.

V. CONCLUSION

A new concept of miniaturized element dual-band frequency selective surface has been presented and analysed by considering its accurate equivalent circuit model. The designed FSS incorporates the unit cells with dimensions as small as $\lambda_0/10$ at the first operational passband providing desired independency of the transmission response with respect to the

angle of the incident wave. In addition, the proposed design approach gives the benefit of independent controllability of the two passband frequencies simply by tuning the unit cell physical parameters.

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