

# Determination of effective temperatures for an extended sample of dwarfs and subdwarfs (F0-K5)<sup>\*</sup>

A. Alonso, S. Arribas and C. Martínez-Roger

Instituto de Astrofísica de Canarias, E-38200 La Laguna (Tenerife), Spain

Electronic mail: aas@ll.iac.es, sam@ll.iac.es and cmr@ll.iac.es

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**Abstract.** — We have applied the InfraRed Flux Method (IRFM) to a sample of 475 dwarfs and subdwarfs in order to derive their effective temperatures with a mean accuracy of about 1.5%. We have used the new homogeneous grid of theoretical model atmosphere flux distributions developed by Kurucz (1991, 1993) for the application of the IRFM. The atmospheric parameters of the stars cover, roughly, the ranges:  $3500 \text{ K} \leq T_{\text{eff}} \leq 8000 \text{ K}$ ;  $-3.5 \leq [\text{Fe}/\text{H}] \leq +0.5$ ;  $3.5 \leq \log(g) \leq 5$ . The monochromatic infrared fluxes at the continuum, and the bolometric fluxes are derived using recent results, which satisfy the accuracy requirements of the work. Photometric calibrations have been revised and applied to estimate metallicities, although direct spectroscopic determinations were preferred when available. The adopted infrared absolute flux calibration, based on direct optical measurements of angular stellar diameters, sets the effective temperatures determined using the IRFM on the same scale than those obtained by direct methods. We derive three temperatures,  $T_J$ ,  $T_H$  and  $T_K$ , for each star using the monochromatic fluxes at different infrared wavelengths in the photometric bands  $J$ ,  $H$ , and  $K$ . They show good consistency over 4000 K, and no trend with wavelength may be appreciated. We provide a detailed description of the steps followed for the application of the IRFM, as well as the sources of the errors associated to the different inputs of the method, and their transmission into the final temperatures. We also provide comparison with previous works.

**Key words:** stars: fundamental parameters — stars: Population II — stars: subdwarfs — stars: general

## 1. Introduction

The stellar effective temperatures might be, in principle, determined following a fundamental or *direct* method based on the combination of the bolometric fluxes and the angular diameter measurements according to the equation:

$$T_{\text{eff}} = \left(\frac{4}{\sigma}\right)^{1/4} \theta^{-1/2} F_{\text{Bol}}^{1/4}, \quad (1)$$

where  $\sigma$  is the Stefan-Boltzmann constant,  $\theta$  is the angular diameter of the star, and  $F_{\text{Bol}}$  is the bolometric flux measured on the surface of the earth.

However, in practice, we need atmosphere models to perform secondary corrections to both the angular diameter measurement (limb darkening) and  $F_{\text{Bol}}$  (interstellar absorption). The Sun is obviously the only exception, since its limb darkening can be empirically determined, and its interstellar absorption is negligible. In any event, the main difficulty affecting the *direct* procedure is the limited number of stars with a reliable measurement of their angular

diameter (see for instance Table 4 from Mozurkewich et al. 1991). This problem is remarkably severe for the low main sequence, as there are no direct measurements of angular diameter for stars later than F5V, with the above mentioned exception of the Sun. For this reason, relatively large uncertainties still remain on the scale of stellar effective temperatures in the low main sequence, especially when the effect of metallicity is considered.

Thus, we are compelled to use *semi-direct* methods, which require, as a basis, atmosphere models in addition to observational information (see the review by Böhm-Vitense 1981). Among the different methods of this type the Infrared Flux Method (hereafter IRFM; Blackwell et al. 1990, and references therein) seems especially adequate to analyse the temperatures of F, G, and K stars. The IRFM has been successfully applied to different samples of population I stars (e.g. Blackwell et al. 1990; Bell & Gustafsson 1989; Saxner & Hammarbäck 1985). However, the works based on the IRFM devoted to metal poor stars (Magain 1987; Arribas & Martínez-Roger 1987, 1989) are restricted to rather limited samples.

The present paper is part of a long term programme aimed to a better definition of the scale of temperatures

Send offprint requests to: A. Alonso

<sup>\*</sup>Table 4 is only available in electronic form at CDS Tables 1-3 are also available via ftp 130.79.128.5

**Table 1.** The calibration of  $q$ - and  $R$ - factors versus metallicity,  $\log(g)$  and effective temperature in  $\lambda_{\text{eff}}=1272.5$  nm (band  $J$ ), computed using models by Kurucz (1991, 1993). The units of  $R$ -factors are (nm)

$T_{\text{eff}}$	$\log(g)$	[Fe/H]=0.50		[Fe/H]=0.00		[Fe/H]=-1.00		[Fe/H]=-2.00		[Fe/H]=-3.00		[Fe/H]=-3.50	
		$q(J)$	$\log(R_J)$	$q(J)$	$\log(R_J)$	$q(J)$	$\log(R_J)$	$q(J)$	$\log(R_J)$	$q(J)$	$\log(R_J)$	$q(J)$	$\log(R_J)$
3500	4.00	1.0106	3.19600	1.0114	3.22780	1.0117	3.23210	1.0088	3.20328	1.0108	3.26472	—	—
3500	5.00	1.0130	3.20760	1.0126	3.23314	1.0113	3.23511	1.0091	3.24874	—	—	—	—
3750	4.00	1.0118	3.22553	1.0104	3.25863	1.0110	3.27501	1.0107	3.28205	1.0107	3.28288	1.0101	3.28121
3750	5.00	1.0138	3.23491	1.0123	3.26000	1.0115	3.27748	1.0105	3.28175	—	—	—	—
4000	4.00	1.0127	3.28154	1.0104	3.28485	1.0098	3.30107	1.0098	3.30538	1.0090	3.30587	1.0100	3.30602
4000	5.00	1.0134	3.28360	1.0118	3.28772	1.0112	3.29982	1.0103	3.30418	—	—	—	—
4250	4.00	1.0140	3.29432	1.0118	3.31003	1.0098	3.32287	1.0090	3.32065	1.0097	3.33102	1.0099	3.33284
4250	5.00	1.0143	3.30337	1.0116	3.31139	1.0100	3.32423	1.0096	3.33045	1.0095	3.33798	—	—
4500	4.00	1.0153	3.32227	1.0127	3.33544	1.0099	3.34908	1.0080	3.35719	1.0090	3.36207	1.0089	3.36350
4500	5.00	1.0154	3.32178	1.0124	3.33548	1.0095	3.34987	1.0083	3.35865	1.0083	3.36555	1.0082	3.36496
4750	4.00	1.0161	3.35022	1.0134	3.36348	1.0100	3.37006	1.0082	3.38977	1.0080	3.39460	1.0082	3.39627
4750	5.00	1.0164	3.35047	1.0131	3.36356	1.0100	3.37815	1.0090	3.38952	1.0087	3.39551	1.0086	3.39743
5000	4.00	1.0163	3.38036	1.0138	3.39394	1.0100	3.41156	1.0083	3.42288	1.0080	3.42804	1.0080	3.43000
5000	5.00	1.0170	3.38078	1.0137	3.39440	1.0101	3.41047	1.0085	3.42258	1.0085	3.42802	1.0079	3.43067
5250	4.00	1.0186	3.41261	1.0147	3.42659	1.0096	3.44817	1.0082	3.45863	1.0077	3.46489	1.0076	3.46608
5250	5.00	1.0174	3.41282	1.0140	3.42685	1.0085	3.44481	1.0081	3.45797	1.0081	3.46427	1.0081	3.46582
5500	4.00	1.0108	3.44008	1.0140	3.46098	1.0094	3.48180	1.0081	3.49427	1.0078	3.50020	1.0077	3.50134
5500	5.00	1.0173	3.44647	1.0139	3.46074	1.0094	3.48067	1.0082	3.49368	1.0079	3.50022	1.0079	3.50120
5750	4.00	1.0108	3.48326	1.0134	3.49037	1.0097	3.51767	1.0084	3.53000	1.0080	3.53513	1.0080	3.53622
5750	5.00	1.0165	3.48180	1.0132	3.49609	1.0096	3.51676	1.0081	3.53009	1.0078	3.53595	1.0077	3.53714
6000	4.00	1.0164	3.51836	1.0134	3.53206	1.0096	3.55044	1.0080	3.56496	1.0083	3.56955	1.0082	3.57004
6000	5.00	1.0167	3.51747	1.0131	3.53169	1.0097	3.55340	1.0084	3.56818	1.0080	3.57110	1.0079	3.57223
6250	4.00	1.0156	3.55598	1.0131	3.56781	1.0098	3.58848	1.0080	3.59884	1.0086	3.60324	1.0088	3.60424
6250	5.00	1.0151	3.55520	1.0131	3.56737	1.0097	3.58842	1.0088	3.60122	1.0084	3.60566	1.0082	3.60701
6500	4.00	1.0156	3.58941	1.0120	3.60338	1.0097	3.62254	1.0092	3.63228	1.0090	3.63817	1.0089	3.63908
6500	5.00	1.0144	3.58912	1.0115	3.60342	1.0096	3.63197	1.0088	3.63570	1.0085	3.64071	1.0087	3.64095
6750	4.00	1.0141	3.62538	1.0111	3.63876	1.0088	3.65605	1.0086	3.66529	1.0082	3.66896	1.0082	3.66976
6750	5.00	1.0136	3.62471	1.0106	3.63812	1.0085	3.65666	1.0080	3.66066	1.0076	3.67372	1.0077	3.67454
7000	4.00	1.0152	3.66083	1.0108	3.67340	1.0076	3.68043	1.0072	3.68820	1.0075	3.70130	1.0073	3.70200
7000	5.00	1.0117	3.66015	1.0096	3.67405	1.0072	3.68368	1.0065	3.70360	1.0059	3.70684	1.0058	3.70762
7250	4.00	1.0123	3.69604	1.0095	3.70831	1.0069	3.72062	1.0058	3.73100	1.0050	3.73384	1.0050	3.73421
7250	5.00	1.0100	3.69541	1.0072	3.70825	1.0061	3.72039	1.0050	3.73376	1.0051	3.73896	1.0047	3.73971
7500	4.00	1.0093	3.73444	1.0063	3.74712	1.0050	3.75713	1.0047	3.76413	1.0044	3.76047	1.0048	3.76070
7500	5.00	1.0075	3.73003	1.0050	3.74321	1.0037	3.75023	1.0034	3.76756	1.0032	3.77082	1.0035	3.77124
7750	4.00	1.0072	3.77085	1.0044	3.78257	1.0022	3.78767	1.0013	3.80445	1.0019	3.80677	1.0016	3.80738
7750	5.00	1.0054	3.77527	1.0035	3.77745	1.0015	3.79300	1.0020	3.79959	1.0014	3.80247	1.0016	3.80281
8000	4.00	1.0058	3.80608	1.0030	3.81709	1.0008	3.83178	1.0004	3.83765	1.0004	3.82083	1.0000	3.84044
8000	5.00	0.9997	3.80371	1.0011	3.81155	1.0000	3.82550	0.9998	3.83155	1.0000	3.83368	0.9995	3.83429
8250	4.00	1.0046	3.84277	1.0021	3.85335	0.9996	3.86076	0.9991	3.87134	0.9991	3.87373	0.9992	3.87400
8250	5.00	0.9965	3.83935	0.9952	3.85113	0.9939	3.86589	0.9932	3.86044	0.9973	3.86587	0.9974	3.86617

for F, G, and K dwarfs and subdwarfs, using the IRFM. This work is relevant to three main topics: (a) analysis of the global behaviour of atmosphere models (e.g., Magain 1987), (b) the correct interpretation of the observed HR diagram (e.g., Arribas & Martínez-Roger 1988, 1989), and (c) fine spectroscopic analysis for abundance determinations of metal poor stars (e.g., King 1994).

The general programme has been focussed on the improvement of the different factors which affect the accuracy in the definition of the temperature scale. Firstly, the sample of selected stars has been substantially enlarged compared to previous works (up to almost 500 stars). This point is particularly important in order to properly sample wide ranges in colour and metallicity. The accurate infrared photometry required for the application of the IRFM was measured for 75% of the stars in the sample (Alonso et al. 1994a, Paper I). Secondly, due to the sensitivity of the IRFM temperatures to the infrared absolute flux calibration considered, this subject was revised in Alonso et al. (1994b, Paper II). There, a new absolute

calibration for the infrared flux of Vega, which scales the IRFM temperatures to those derived by direct methods, is proposed. Thirdly, a method to obtain bolometric fluxes for metal poor stars was devised in Alonso et al. (1995, Paper III). Last, but not least, we have used the improved grid of atmosphere models computed recently by Kurucz (1991, 1993).

This paper provides detailed information on the procedure followed to derive the effective temperatures for the whole sample. The paper is laid out as follows. Section 2 explains the practical implementation of the IRFM. The theoretical and observational inputs of the method, as applied here, have been separated in order to discuss the influence of errors in the derived temperatures. Thus, Sect. 3 analyses the theoretical  $R$ - and  $q$ -factors, and the observational inputs are discussed in Sect. 4. This section also includes a description of the criteria adopted to collect the sample of stars, a revision of photometric calibrations to estimate the metallicity, and the correction of interstellar extinction. The effective temperatures are derived

**Table 2.** The same that Table 1 for  $\lambda_{\text{eff}}=1635.0$  nm (band *H*)

$T_{\text{eff}}$	$\log(g)$	[Fe/H]=0.50		[Fe/H]=0.00		[Fe/H]=-1.0		[Fe/H]=-2.0		[Fe/H]=-3.0		[Fe/H]=-3.5	
		$q(H)$	$\log(R_H)$	$q(H)$	$\log(R_H)$	$q(H)$	$\log(R_H)$	$q(H)$	$\log(R_H)$	$q(H)$	$\log(R_H)$	$q(H)$	$\log(R_H)$
3500	1.00	1.0855	3.22481	1.0710	3.28198	1.0572	3.35350	1.0558	3.40373	1.0522	3.36870	—	—
3500	5.00	1.0577	3.30845	1.0550	3.35420	1.0552	3.35579	1.0502	3.40018	—	—	—	—
3750	1.00	1.0813	3.27000	1.0795	3.30519	1.0578	3.38672	1.0486	3.41153	1.0444	3.41907	1.0418	3.42357
3750	5.00	1.0618	3.33578	1.0536	3.37807	1.0483	3.40675	1.0466	3.41568	—	—	—	—
4000	1.00	1.0725	3.33562	1.0740	3.34383	1.0556	3.39405	1.0483	3.44312	1.0370	3.47083	1.0368	3.48011
4000	5.00	1.0637	3.36533	1.0578	3.40463	1.0459	3.44771	1.0413	3.48288	—	—	—	—
4250	1.00	1.0623	3.40413	1.0629	3.40631	1.0589	3.43010	1.0458	3.47769	1.0338	3.51515	1.0306	3.52893
4250	5.00	1.0589	3.41079	1.0578	3.42979	1.0486	3.47230	1.0384	3.50466	1.0316	3.52532	—	—
4500	1.00	1.0520	3.47101	1.0522	3.47245	1.0485	3.49194	1.0416	3.52341	1.0335	3.55907	1.0318	3.56514
4500	5.00	1.0522	3.46703	1.0517	3.47433	1.0405	3.50464	1.0355	3.54761	1.0278	3.57000	1.0261	3.58300
4750	1.00	1.0426	3.53488	1.0431	3.53646	1.0410	3.55421	1.0368	3.57979	1.0328	3.59017	1.0319	3.60741
4750	5.00	1.0438	3.52861	1.0435	3.53383	1.0407	3.55524	1.0320	3.58400	1.0270	3.61848	1.0262	3.63025
5000	1.00	1.0349	3.59552	1.0348	3.59855	1.0349	3.61329	1.0318	3.63455	1.0267	3.64891	1.0265	3.66187
5000	5.00	1.0361	3.58981	1.0367	3.59330	1.0345	3.61349	1.0298	3.64271	1.0264	3.66031	1.0262	3.67277
5250	1.00	1.0277	3.65441	1.0290	3.65615	1.0303	3.67122	1.0291	3.68812	1.0287	3.69488	1.0287	3.69601
5250	5.00	1.0306	3.64750	1.0300	3.65203	1.0298	3.67091	1.0266	3.69392	1.0255	3.70804	1.0255	3.70556
5500	1.00	1.0225	3.70927	1.0238	3.71246	1.0262	3.72661	1.0261	3.73905	1.0265	3.74330	1.0267	3.74428
5500	5.00	1.0237	3.70350	1.0244	3.70933	1.0254	3.72553	1.0230	3.74356	1.0241	3.74941	1.0238	3.75138
5750	1.00	1.0185	3.78271	1.0200	3.78583	1.0224	3.77988	1.0235	3.78928	1.0240	3.79211	1.0243	3.79275
5750	5.00	1.0190	3.75695	1.0200	3.76171	1.0217	3.77618	1.0218	3.79200	1.0222	3.79566	1.0223	3.79631
6000	1.00	1.0149	3.81351	1.0165	3.81775	1.0191	3.83037	1.0204	3.83758	1.0207	3.84048	1.0208	3.84119
6000	5.00	1.0137	3.80850	1.0160	3.81377	1.0186	3.82919	1.0185	3.83904	1.0199	3.84258	1.0192	3.84330
6250	1.00	1.0125	3.86315	1.0136	3.86848	1.0163	3.87899	1.0172	3.88494	1.0174	3.88762	1.0175	3.88823
6250	5.00	1.0111	3.85858	1.0135	3.86431	1.0156	3.87745	1.0165	3.88548	1.0169	3.88960	1.0170	3.89027
6500	1.00	1.0096	3.91178	1.0108	3.91666	1.0135	3.92616	1.0144	3.93130	1.0147	3.93371	1.0147	3.93425
6500	5.00	1.0079	3.90710	1.0094	3.91263	1.0127	3.92446	1.0150	3.93008	1.0142	3.93370	1.0143	3.93434
6750	1.00	1.0074	3.95819	1.0084	3.96332	1.0111	3.97205	1.0118	3.97671	1.0119	3.97885	1.0120	3.97931
6750	5.00	1.0052	3.95350	1.0065	3.95930	1.0100	3.96970	1.0110	3.97574	1.0112	3.97820	1.0113	3.97871
7000	1.00	1.0050	4.00803	1.0067	4.00827	1.0089	4.01650	1.0092	4.02112	1.0094	4.02274	1.0094	4.02318
7000	5.00	1.0028	3.99828	1.0037	4.00433	1.0070	4.01417	1.0079	4.01958	1.0080	4.02161	1.0081	4.02200
7250	1.00	1.0043	4.04670	1.0048	4.05220	1.0070	4.05990	1.0079	4.06405	1.0074	4.06564	1.0075	4.06594
7250	5.00	1.0009	4.04182	1.0013	4.04810	1.0040	4.05751	1.0049	4.06215	1.0052	4.06412	1.0052	4.06455
7500	1.00	1.0008	4.09372	1.0002	4.09954	1.0051	4.10286	1.0055	4.10620	1.0058	4.10755	1.0058	4.10785
7500	5.00	0.9980	4.08471	0.9984	4.09078	1.0019	4.09945	1.0022	4.10385	1.0024	4.10565	1.0025	4.10597
7750	1.00	0.9991	4.13608	0.9991	4.14254	1.0019	4.15009	1.0020	4.15462	1.0016	4.15643	1.0013	4.15642
7750	5.00	0.9957	4.12825	0.9963	4.13211	0.9980	4.14090	0.9994	4.14475	1.0001	4.14807	0.9999	4.14651
8000	1.00	0.9989	4.17849	0.9974	4.18470	1.0001	4.19202	0.9997	4.19680	1.0000	4.19818	0.9998	4.19821
8000	5.00	0.9974	4.17145	0.9985	4.17332	0.9965	4.18111	0.9967	4.18485	0.9971	4.18813	0.9976	4.18814
8250	1.00	0.9985	4.21874	0.9973	4.22521	0.9980	4.23303	0.9988	4.23779	0.9988	4.24067	0.9983	4.23906
8250	5.00	0.9989	4.21363	0.9971	4.22014	0.9965	4.22567	0.9962	4.22954	0.9964	4.23278	0.9969	4.23581

in Sect. 5, where the internal consistency of the method and the uncertainties affecting  $T_{\text{eff}}$  are assessed. The final temperatures are compared to common determinations of previous works in Sect. 6. Finally, in Sect. 7, the main results are briefly summarized.

In a forthcoming paper, we will provide and discuss the calibrations  $T_{\text{eff}}$ -colours-[Fe/H], as well as the mean intrinsic colours for dwarfs and subdwarfs.

## 2. The implementation of the IRFM

The InfraRed Flux Method (Blackwell et al. 1990) uses the quotient between the bolometric flux ( $F_{\text{Bol}}$ ) and the monochromatic flux at a chosen infrared wavelength of the continuum ( $F(\lambda_{\text{IR}})$ ), both measured at the surface of the earth, as indicator of  $T_{\text{eff}}$ . This quotient is the so-called observational  $R$ -factor ( $R_{\text{obs}}$ ). The theoretical counterpart derived from models,  $R_{\text{theo}}$ , is obtained as the quotient between the integrated flux ( $\sigma T_{\text{eff}}^4$ ) and the monochromatic flux at  $\lambda_{\text{IR}}$  ( $F_{\text{mod}}(\lambda_{\text{IR}})$ ), at the surface of the star. Thus

the basic equation of the IRFM reads:

$$R_{\text{obs}} = \frac{F_{\text{Bol}}}{F(\lambda_{\text{IR}})} = \frac{\sigma T_{\text{eff}}^4}{F_{\text{mod}}(\lambda_{\text{IR}}, T_{\text{eff}}, [\text{Fe}/\text{H}], g)} = R_{\text{theo}}(\lambda_{\text{IR}}, T_{\text{eff}}, [\text{Fe}/\text{H}], g), \quad (2)$$

where the explicit dependence on metallicity, surface gravity, and  $\lambda_{\text{IR}}$  is taken into account. The IRFM only requires from models the correct prediction of the continuum IR fluxes (note that the bolometric flux at the stellar surface is fixed by the value of  $T_{\text{eff}}$ ). This requirement seems relatively easier to fulfill, if compared to those demanded by other *semi-direct* methods. In particular, free-free and bound-free transitions of  $\text{H}^-$  ion, the main source of the continuum opacity in the IR for F, G and K stars, are relatively well understood. Therefore, in principle, the dependence on models is not a critical point to the IRFM, at least for spectral types earlier than late K where the IR opacity due to molecular bands is of minor importance. Another advantage of the IRFM, as explained in Sect. 4.1,

**Table 3.** The same that Table 1 for  $\lambda_{\text{eff}}=2175.0$  nm (band *K*)

$T_{\text{eff}}$	$\log(g)$	[Fe/H]=0.50		[Fe/H]=0.00		[Fe/H]=-1.0		[Fe/H]=-2.0		[Fe/H]=-3.0		[Fe/H]=-3.5	
		$q(K)$	$\log(R_K)$	$q(K)$	$\log(R_K)$	$q(K)$	$\log(R_K)$	$q(K)$	$\log(R_K)$	$q(K)$	$\log(R_K)$	$q(K)$	$\log(R_K)$
3500	4.00	1.0491	3.67077	1.0390	3.67040	1.0340	3.71134	1.0270	3.50720	1.0261	3.72061	—	—
3500	5.00	1.0415	3.67386	1.0352	3.63021	1.0316	3.71324	1.0253	3.79841	—	—	—	—
3750	4.00	1.0442	3.68243	1.0379	3.71302	1.0312	3.76496	1.0260	3.78006	1.0237	3.78449	1.0230	3.78616
3750	5.00	1.0383	3.73570	1.0340	3.75590	1.0283	3.77691	1.0250	3.78110	—	—	—	—
4000	4.00	1.0410	3.75541	1.0362	3.78628	1.0287	3.80118	1.0243	3.82875	1.0226	3.84448	1.0223	3.84980
4000	5.00	1.0302	3.77543	1.0310	3.80467	1.0261	3.83105	1.0233	3.84071	—	—	—	—
4250	4.00	1.0378	3.82777	1.0343	3.83286	1.0275	3.84872	1.0226	3.87759	1.0218	3.89022	1.0217	3.90854
4250	5.00	1.0309	3.83328	1.0293	3.84842	1.0238	3.87605	1.0221	3.88458	1.0217	3.89679	—	—
4500	4.00	1.0345	3.89709	1.0309	3.90121	1.0254	3.91256	1.0217	3.93235	1.0207	3.95498	1.0208	3.95942
4500	5.00	1.0311	3.89437	1.0274	3.90151	1.0225	3.92210	1.0211	3.94782	1.0202	3.96536	1.0211	3.96989
4750	4.00	1.0304	3.96302	1.0279	3.98679	1.0207	3.97732	1.0205	3.99602	1.0200	4.00734	1.0202	4.00900
4750	5.00	1.0277	3.95868	1.0248	3.98410	1.0210	3.97810	1.0204	4.00203	1.0207	4.01704	1.0200	4.02038
5000	4.00	1.0266	4.02373	1.0250	4.02559	1.0216	4.03988	1.0196	4.05472	1.0197	4.06150	1.0198	4.08273
5000	5.00	1.0243	4.02145	1.0225	4.02617	1.0208	4.03902	1.0198	4.05823	1.0202	4.06821	1.0204	4.06975
5250	4.00	1.0230	4.08471	1.0221	4.08505	1.0199	4.10008	1.0194	4.11123	1.0197	4.11577	1.0197	4.11661
5250	5.00	1.0212	4.08121	1.0202	4.08503	1.0197	4.09862	1.0198	4.11303	1.0198	4.11913	1.0198	4.12089
5500	4.00	1.0187	4.14173	1.0190	4.14541	1.0188	4.15745	1.0192	4.16804	1.0192	4.16940	1.0191	4.17154
5500	5.00	1.0170	4.13580	1.0178	4.14344	1.0188	4.15641	1.0196	4.16905	1.0196	4.17137	1.0194	4.17386
5750	4.00	1.0163	4.19648	1.0188	4.20054	1.0181	4.21059	1.0185	4.22184	1.0184	4.23184	1.0182	4.23382
5750	5.00	1.0133	4.19339	1.0154	4.19889	1.0181	4.20925	1.0185	4.21954	1.0185	4.22462	1.0184	4.23194
6000	4.00	1.0134	4.21928	1.0113	4.23444	1.0168	4.24898	1.0173	4.26873	1.0173	4.27404	1.0173	4.27488
6000	5.00	1.0115	4.24731	1.0134	4.25107	1.0165	4.26245	1.0177	4.27046	1.0177	4.27516	1.0179	4.27578
6250	4.00	1.0115	4.29964	1.0130	4.30374	1.0156	4.31339	1.0163	4.32077	1.0164	4.32337	1.0165	4.32378
6250	5.00	1.0092	4.30826	1.0112	4.30184	1.0145	4.31316	1.0155	4.32174	1.0161	4.32444	1.0161	4.32505
6500	4.00	1.0100	4.34713	1.0115	4.35227	1.0130	4.36121	1.0144	4.36897	1.0140	4.37126	1.0140	4.37176
6500	5.00	1.0082	4.34372	1.0092	4.35116	1.0125	4.36224	1.0133	4.37017	1.0136	4.37262	1.0138	4.37311
6750	4.00	1.0083	4.39470	1.0098	4.39997	1.0118	4.40947	1.0126	4.41564	1.0128	4.41770	1.0130	4.41810
6750	5.00	1.0040	4.39287	1.0086	4.39929	1.0103	4.41134	1.0113	4.41888	1.0118	4.41918	1.0119	4.41906
7000	4.00	1.0066	4.44107	1.0077	4.44638	1.0103	4.45648	1.0108	4.46099	1.0108	4.46230	1.0109	4.46289
7000	5.00	1.0012	4.44012	1.0037	4.44576	1.0075	4.45738	1.0087	4.46243	1.0087	4.46391	1.0089	4.46431
7250	4.00	1.0043	4.48559	1.0058	4.49174	1.0078	4.50137	1.0086	4.50523	1.0084	4.50652	1.0085	4.50682
7250	5.00	0.9982	4.48525	1.0004	4.49114	1.0041	4.50223	1.0051	4.50618	1.0053	4.50817	1.0056	4.50840
7500	4.00	0.9985	4.53501	0.9984	4.54125	1.0058	4.54527	1.0055	4.54972	1.0051	4.55019	1.0053	4.55038
7500	5.00	0.9951	4.52939	0.9973	4.53852	1.0007	4.54575	1.0015	4.54937	1.0020	4.55188	1.0021	4.55130
7750	4.00	0.9970	4.58211	0.9973	4.58901	1.0009	4.58797	1.0001	4.60170	1.0003	4.60329	1.0003	4.60361
7750	5.00	0.9918	4.57381	0.9932	4.57984	0.9969	4.58346	0.9978	4.59165	0.9980	4.59335	0.9983	4.59310
8000	4.00	0.9950	4.62493	0.9957	4.63164	0.9985	4.63932	0.9986	4.64381	0.9987	4.64527	0.9987	4.64551
8000	5.00	0.9840	4.62367	0.9883	4.62291	0.9924	4.62901	0.9936	4.63323	0.9940	4.63458	0.9941	4.63472
8250	4.00	0.9954	4.66872	0.9949	4.67282	0.9970	4.68101	0.9978	4.68481	0.9978	4.68615	0.9978	4.68639
8250	5.00	0.9818	4.66525	0.9820	4.67207	0.9851	4.68070	0.9853	4.68246	0.9891	4.67607	0.9894	4.67609

is the large sensitivity of  $R$ -factors to the effective temperature ( $R \sim T_{\text{eff}}^3$ ) and their slight dependence on the secondary atmospheric parameters. Therefore, the uncertainties in the derived effective temperature associated to errors in the gravity and metallicity assignment are small compared to those due to the determination of the bolometric and monochromatic fluxes.

The monochromatic fluxes are obtained by applying the relation

$$F(\lambda_{\text{IR}}) = q(\lambda_{\text{IR}}, T_{\text{eff}}, [\text{Fe}/\text{H}], g) [F_{\text{cal}}(\lambda_{\text{IR}}) 10^{-0.4(m-m_{\text{cal}})}] \quad (3)$$

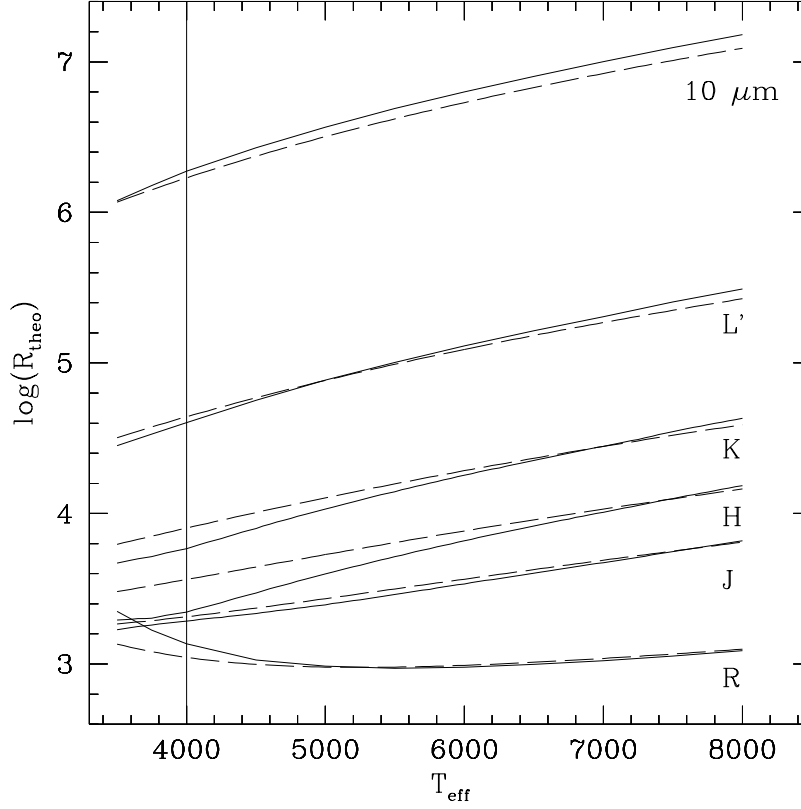
where  $m$  and  $m_{\text{cal}}$  are, respectively, the magnitudes of the problem and standard star,  $\lambda_{\text{IR}}$  is the selected wavelength at the infrared (which should be close to the maximum transmission of the photometric band),  $F_{\text{cal}}(\lambda_{\text{IR}})$  is the absolute flux of the standard star at  $\lambda_{\text{IR}}$ , and  $q(\lambda_{\text{IR}}, T_{\text{eff}}, [\text{Fe}/\text{H}], g)$  is a dimensionless factor which corrects the effect of the different curvature of the flux density distribution, across the filter window, between the stan-

dard and the problem stars (see Sect. 3.2 for further details).

**Table 5.** The influence of the reddening and the uncertainty in the Calibration of the Absolute Flux in the IR (CAFIR) on the temperatures derived using IRFM. The errors induced by the uncertainties on the absolute flux calibration are slightly overestimated, since the change in the bolometric flux has not been taken into account

Input parameter	Error	Error on $T_{\text{eff}}$ (%)					
		3500	4000	5000	6000	7500	
E(B-V)	0.05 mag	2.1	1.6	2.6	3.6	4.5	
CAFIR J [Fe/H]=0.0	3 %	2.75	3	2	1.4	1.2	
CAFIR J [Fe/H]=-3.0	3 %	3.25	2.75	2	1.4	1.2	
CAFIR H [Fe/H]=0.0	4 %	6	1.6	1.4	1.2	1.2	
CAFIR H [Fe/H]=-3.0	4 %	1.75	2	1.75	1.2	1.2	
CAFIR K [Fe/H]=0.0	4 %	2.4	1.4	1.4	1.2	1.2	
CAFIR K [Fe/H]=-3.0	4 %	1.6	1.6	1.4	1.2	1.2	
CAFIR mean	—	2.0	1.7	1.6	1.25	1.2	

The separation of observational inputs and theoretical factors for the implementation of the IRFM is provided



**Fig. 1.**  $R_{\text{theo}}$  factors computed using solar metallicity models developed by Kurucz (1991). The wavelengths considered are  $\lambda_R = 790$  nm,  $\lambda_J = 1272.5$  nm,  $\lambda_H = 1635$  nm,  $\lambda_K = 2175$  nm,  $\lambda_{L'} = 3690$  nm, and a point in the far IR at  $10 \mu\text{m}$ . The dashed lines correspond to  $R_{\text{theo}}$  factors derived from blackbody flux densities. The vertical line ( $T_{\text{eff}} = 4000$  K) shows the lower limit of applicability of IRFM with these models

**Table 6.** Mean accidental errors of the effective temperature derived applying the IRFM in the band K

Input parameter	Error	Error on $T_{\text{eff}}$ (%)				
		3500 K	4000 K	5000 K	6000 K	7500 K
$qR_{\text{theo}}$	5 (%)	3	1.5	1.5	1.5	1.5
$\log(g)$	0.5 dex	2	1.5	0.1	0.1	0.1
$[\text{Fe}/\text{H}]$	0.3 dex	1	0.75	0.15	0.15	0.15
Total		3.3	2	1.5	1.5	1.5

by substituting relation (3) in Eq. (2) as follows,

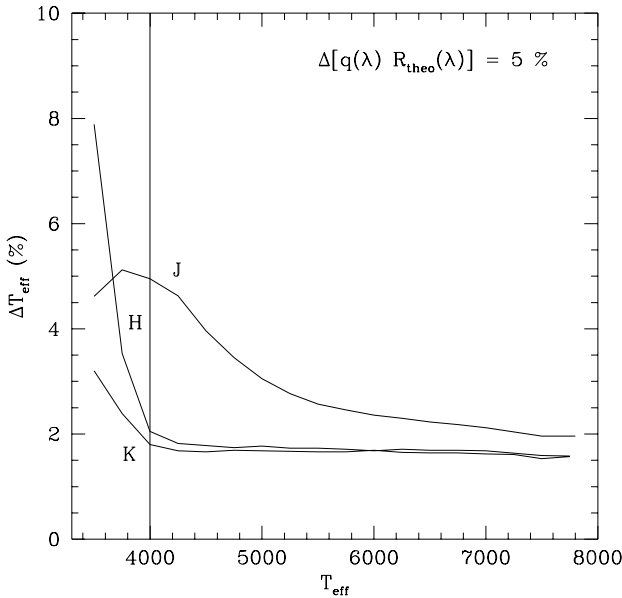
$$\frac{F_{\text{Bol}}}{F_{\text{cal}}(\lambda_{\text{IR}}, T_{\text{eff}}, [\text{Fe}/\text{H}], g) R_{\text{theo}}(\lambda_{\text{IR}}, T_{\text{eff}}, [\text{Fe}/\text{H}], g)} =$$

$$= q(\lambda_{\text{IR}}, T_{\text{eff}}, [\text{Fe}/\text{H}], g) R_{\text{theo}}(\lambda_{\text{IR}}, T_{\text{eff}}, [\text{Fe}/\text{H}], g) \quad (4)$$

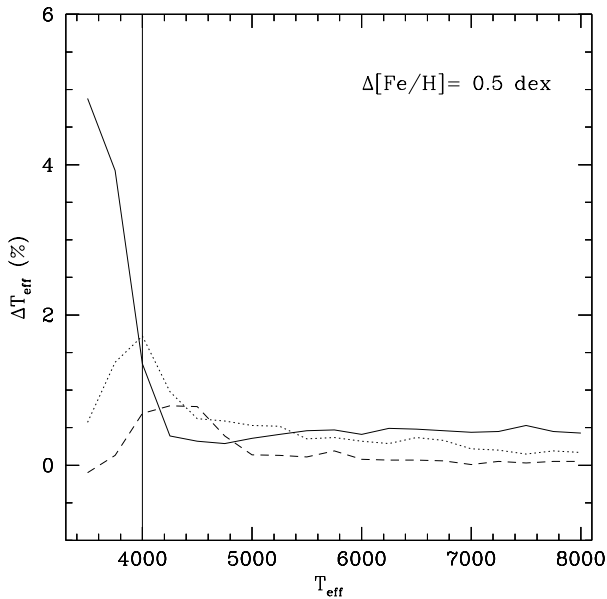
Once  $[\text{Fe}/\text{H}]$  and  $\log(g)$  are known for a certain star, the observational quantities on the left-hand side of Eq. (4) determine the star's effective temperature by comparing to the theoretical information from models on the right-hand side. It is worthy to notice that in a strict sense, models are also needed to obtain the integrated flux in order to

**Table 7.** Comparison between the temperatures derived in the present work (Col. 2) and those derived by Saxner & Hammarbäck (1985) (Col. 3). The mean difference  $T_{\text{IRFM}} - T_{\text{SH85}}$  is  $5 \pm 63$  K

Star	$T_{\text{IRFM}}$ (K)	$T_{\text{SH85}}$ (K)	$\Delta T$	$\Delta T$ (K) (%)
HR0458	6155	6140	15	0.24
HR0483	5874	5810	64	1.09
HR0937	5996	5890	106	1.77
HR1101	5998	5940	58	0.97
HR1543	6482	6470	12	0.19
HR1729	5847	5810	37	0.63
HR1983	6260	6260	0	0.00
HR2085	7013	7160	-147	-2.10
HR2852	7020	7060	-40	-0.57
HR2943	6579	6640	-61	-0.93
HR4540	6095	6120	-25	-0.41
HR4785	5867	5810	57	0.97
HR5447	6770	6760	10	0.15
HR5634	6571	6570	1	0.02
HR5868	5897	5890	7	0.12
HR5914	5774	5870	-96	-1.66
HR5933	6233	6220	13	0.21
HR8905	5954	5870	84	1.41



**Fig. 2.** Uncertainty on the IRFM temperature induced by an error of 5% in the observational quotient  $\frac{F_{\text{Bol}}}{F_{\text{cal}}(\lambda_{\text{IR}})10^{-0.4(m-m_{\text{cal}})}}$



**Fig. 3.** Uncertainty on the IRFM temperature induced by an error of 0.5 dex in [Fe/H]. Solid line: change from [Fe/H]=0 to [Fe/H]=-0.5; dotted line: change from [Fe/H]=-1 to [Fe/H]=-1.5; dashed line: change from [Fe/H]=-2.5 to [Fe/H]=-3

complete the missed flux in the UV and far IR, however, these corrections are small (see for instance Petford et al. (1991) and Paper II).

### 3. Model information: The $R$ - and $q$ -factors

The theoretical flux density distributions used in this work to implement the IRFM were obtained using Kurucz's (1991, 1993) new models. Blackwell and Lynas-Gray (1994) have also used them for the application of the IRFM. These models are widely described in Kurucz (1991). Here we briefly summarize their features concerning the aims of the present programme:

1. The major difference concerning opacities is the use of new iron group atomic lines, which are expected to diminish the problem of the missing opacity in the UV (Magain 1987). The computed opacities consider the effect of 58 million lines both atomic and molecular (which increases in a factor of roughly 30 the number in old models). Diatomic molecules considered include  $\text{H}_2$ ,  $\text{SiO}$ ,  $\text{CH}$ ,  $\text{NH}$ ,  $\text{OH}$ ,  $\text{MgH}$ ,  $\text{SiH}$ ,  $\text{C}_2$ ,  $\text{TiO}$ ,  $\text{CN}$  and  $\text{CO}$ . Regrettably the effects of triatomic molecules, as water vapor, are not considered. In the range 1.75–2.1  $\mu\text{m}$  the contribution to the opacity from water vapour has great influence on the IR flux of cool stars ( $T_{\text{eff}} \leq 4500$  K), specially for solar abundance. This fact sets a lower limit at late K stars for the applicability of the IRFM using these models (see Sect. 5).
2. The physics remains essentially the same that in older Kurucz's models (see Kurucz 1979a, b) since the problem of the opacity has been paid major attention. However, the new models contain slight improvements in the treatment of convection including approximative overshooting. The mixing length to scale height ratio ( $\alpha/H$ ) adopted is 1.25. The solar metal abundances are those derived by Anders & Grevesse (1989). The microturbulent velocity is 2 km/s.
3. From a practical point of view, the new models sample physical parameters in a denser grid: Abundances are sampled in 0.1 dex steps from [Fe/H]=1.00 to [Fe/H]=-0.5, and in 0.5 dex steps from [Fe/H]=-0.5 to [Fe/H]=-4.0. Gravities are sampled in 0.5 dex steps and temperatures in 250 K steps under 8000 K.
4. Model fluxes are sampled in 1221 points covering a wavelength interval from 9 to 160000 nm. The resolution ranges within 1 nm in the UV, 2 nm in the visible and the band J, 5 nm in the band H and 10 nm in the band K. The sampling in the near IR implies a remarkable improvement as far as previous models are concerned, which allows to avoid interpolations.

#### 3.1. $R_{\text{theo}}(\lambda_{\text{IR}})$ factors

The flux density distributions of models described in the previous section have been used to calculate  $R_{\text{theo}}(\lambda_{\text{IR}})$

**Table 8.** Comparison between the temperatures derived in the present work (Col. 2) and those derived by Magain (1987) (Col. 3). The mean difference  $T_{\text{IRFM}} - T_{\text{M87}}$  is  $112 \pm 56$  K

Star	$T_{\text{IRFM}}$ (K)	$T_{\text{M87}}$ (K)	$\Delta T$ (K)	$\Delta T$ (%)
HD19445	6050	5933	117	1.93
HD64000 <sup>(1)</sup>	5441	5370	71	1.36
HD74000	6224	6135	89	1.40
HD84937 <sup>(2)</sup>	6330	6210	120	1.90
HD94028 <sup>(3)</sup>	6001	5777	224	3.73
HD108177	6034	6026	8	0.01
HD132475	5788	5614	174	3.00
HD140283	5691	5607	84	1.47
BD +42 2667 <sup>(4)</sup>	6059	5955	104	1.71
HD201891	5909	5761	148	2.56
HD219617	6012	5918	94	1.56

(1) G090-025

(2) G043-003

(3) G058-025

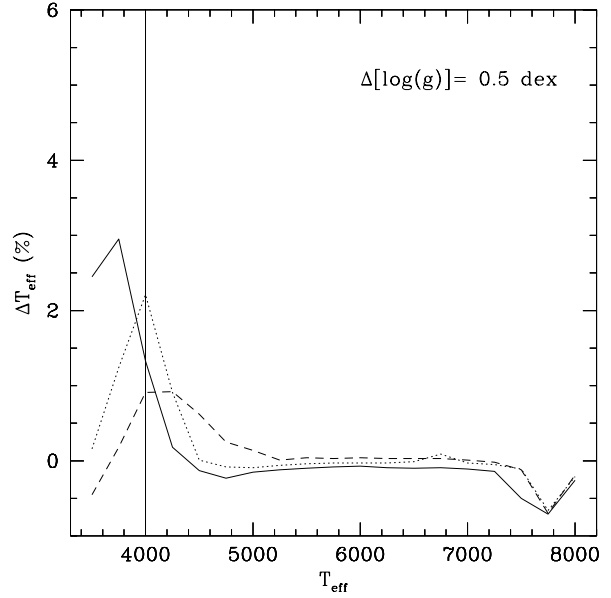
(4) G180-024

**Table 9.** Comparison between the temperatures derived in the present work (Col. 2) and those derived by Bell & Gustafsson (1989) (Col. 3). The mean difference  $T_{\text{IRFM}} - T_{\text{BG89}}$  over 4500 K is  $-49 \pm 75$  K

Star	$T_{\text{IRFM}}$ (K)	$T_{\text{BL94}}$ (K)	$\Delta T$ (K)	$\Delta T$ (%)
HR219	5817	5839	-22	-0.38
HR753	4718	4775	-57	-1.21
HR4785	5867	5861	6	0.10
HR4983	5964	6024	-60	-1.01
HR7503	5763	5826	-63	-1.09
HR7504	5767	5664	103	1.79
HR4496	5342	5552	-210	-3.93
HR7462	5227	5253	-26	-0.50
HR1325	5079	5114	-35	-0.69
HR1084	5076	5156	-80	-1.58
HR8832	4805	4896	-91	-1.89
HR8085	4323	4463	-140	-3.24
HR8086	3865	4252	-387	-10.01

factors, as defined in Eq. (2). The closest wavelengths to the effective wavelengths of the  $J$ ,  $H$ , and  $K$  photometric bands sampled by the models were selected ( $\lambda_J = 1272.5$  nm,  $\lambda_H = 1635.0$  nm and  $\lambda_K = 2175.0$  nm). The effective wavelengths were computed considering the instrumental response of the TCS system (Paper I), and the atmospheric transparency (Manduca & Bell 1979; Glass 1985; Mountain 1983). Tables 1-3 contain the theoretical values of  $\log(R)$  for these three wavelengths. Effective temperatures cover the range 3500–8250 K, surface gravities cover the range  $\log(g)=(3.5, 5.0)$ , and metallicities cover the range  $(0.5, -3.5)$ .

Figure 1 shows the  $\log(R)$  factors for solar metallicity. In addition to  $R$ -factors corresponding to the three wavelengths selected in this work, those corresponding to the  $R$  band (Johnson 1966) at  $\lambda_R = 790$  nm,  $L'$  from TCS system (Paper II) at  $\lambda_{L'} = 3690.0$  nm, and a far



**Fig. 4.** Uncertainty on the IRFM temperature induced by an error of 0.5 dex in  $\log(g)$ . Solid line:  $[\text{Fe}/\text{H}]=0.0$ ; dotted line:  $[\text{Fe}/\text{H}]=-1$ ; dashed line:  $[\text{Fe}/\text{H}]=-2$

IR point at 10004.0 nm have been also plotted to display their overall properties. The correlation of gradient  $\Delta \log(R_{\text{theo}})/\Delta T_{\text{eff}}$  with wavelength may be appreciated in the figure (i.e. the sensitivity of  $R$ -factors to temperature increases with wavelength). The relation  $\log(R_{\text{theo}}) - T_{\text{eff}}$  is double-valued for the band  $R$ , which implies that it is useless to apply the IRFM in the considered  $T_{\text{eff}}$  range.

Among the three wavelengths considered in this work, the  $R_J$  factors are the least sensitive to temperature, especially for  $T_{\text{eff}}$  lower than 5000 K. The sensitivities of the  $R_H$  and  $R_K$  are comparable, although as will be discussed in Sect. 5, temperatures lower than 4000 K derived using  $R_H$  are less reliable, due to the uncertainty associated to the minimum of the  $\text{H}^-$  opacity reached in this band. The variations induced by the change in metallicity or surface gravity are only important for  $T_{\text{eff}}$  lower than 4250 K. In particular, the variation of  $R$ -factors in the range  $\log(g) = 4 - 5$  is almost negligible. For this reason, the assignation of gravity has been done in a somewhat rough fashion, which satisfies nevertheless the accuracy requirements of this work.

### 3.2. $q(\lambda_{\text{IR}})$ factors

The use of broad band photometry to obtain the IR monochromatic fluxes requires the application of the

so-called  $q$ -factors introduced in Eq. (3), and defined as

$$q(\lambda_{\text{IR}}) = \frac{\int_{\lambda_1}^{\lambda_2} K_{\text{cal}}(\lambda, \lambda_{\text{IR}}) T(\lambda) d\lambda}{\int_{\lambda_1}^{\lambda_2} K(\lambda, \lambda_{\text{IR}}) T(\lambda) d\lambda}, \quad (5)$$

where  $T(\lambda)$  is the instrumental transmission of the photometric system, which includes the detector response, the optical system of the telescope and photometer, and the absorption of the atmosphere. The function  $K(\lambda, \lambda_{\text{IR}})$  is the stellar flux density normalized to the value of flux density at  $\lambda_{\text{IR}}$ , and  $(\lambda_1, \lambda_2)$  is the bandpass of the system (see Appendix 1 in Paper II for further details). The  $q$ -factors allow to cope with the problem of deriving the flux in a specific wavelength from the filter-integrated flux in the whole photometric band. An optional approach to this problem is described in Saxner & Hammarbäck (1985).

Ideally,  $q$ -factors should be determined from spectroscopic data, considering a set of stars sampling homogeneously the domain of physical parameters in  $T_{\text{eff}}$ ,  $\log(g)$  and  $[\text{Fe}/\text{H}]$ . Unfortunately the data-base of registered IR spectra is insufficient to make this approach realistic. In practice, we can rely on a grid of models to compute  $q$  factors. Tables 1-3 contain  $q$ -factors for bands  $J$ ,  $H$  and  $K$ , ordered according to temperature, gravity and metallicity. The physical parameters adopted to generate the model for the calibration star (Vega) were  $T_{\text{eff}} = 9610$  K,  $\log(g) = 3.95$ ,  $[\text{Fe}/\text{H}] = -0.25$ . Note that the  $q$ -factors imply secondary corrections in most of the range studied.

### 3.3. Sensitivity of $q \times R$ to the effective temperature

The separation of terms in Eq. (4) (i.e. theoretical elements in the right-handside, and observational data in the left-handside) provides a simple way of analysing the influence of errors on the derived temperatures. Tables 1-3 contain the calibration of  $R$ - and  $q$ -factors generated with Kurucz's new models as a function of temperature, metallicity and surface gravity. These relations allow to determine the errors induced by the different variables on the derived temperatures.

Figure 2 shows the error in temperature induced by a variation of 5% in factor  $q \times R$  (the theoretical counterpart to the quotient  $F_{\text{Bol}}/F(\lambda_{\text{IR}})$ ). As it may be appreciated, the change in temperatures derived using  $R_H$  and  $R_K$  factors is approximately constant over 4000 K: 1.5–2% for  $T_H$  and 1.5% for  $T_K$ . The change of  $T_J$  varies from 5% at 4000 K to 2% at 8000 K. Hence,  $R_J$  is the worse indicator of  $T_{\text{eff}}$  for the application of the IRFM, and will only be used over 5000 K.

Figure 3 shows the influence of an error of 0.5 dex in metallicity on the temperature derived applying the IRFM in the band  $K$ . Over 4200 K the average error is under 0.25%.

Figure 4 shows the influence of an error of 0.5 dex in  $\log(g)$  on the temperature derived in the band  $K$ . The changes in temperature are practically negligible between 4200 K and 7500 K. Between 4000 K and 4200 K the change amounts 1–2%. Over 7500 K the change may amount –0.5%.

## 4. Observational inputs for the IRFM

In the following paragraphs the different observational inputs which enter the application of the IRFM will be commented. First of all, we provide a description of the sample of stars collected for this program.

### 4.1. The selection of the sample

The stars of the sample were extracted mainly from three independent photometric surveys: Sandage & Kowal (1986), Carney & Latham (1987) and Schuster & Nissen (1988). These works are involved with the study of different properties of halo field stars, and provide broad band  $UBV$  and Strömgren photometry. The selected sample of stars covers the entire range of effective temperature and metallicity observed in the main sequence of globular clusters, and intermediate and old disk clusters (i.e. late spectral types of luminosity class V and VI). The stars of the sample range practically  $0.3 < (B - V) < 1.7$ ,  $0.1 < (b - y) < 1.0$ , and  $0.0 < \delta_{0.6}(B - V) < 0.3$ , which roughly implies  $-3.5 < [\text{Fe}/\text{H}] < 0.5$ . After the measurement of IR photometry (Paper I), the stars with  $(V - K) \geq 4.2$  were discarded since the practical limit in temperatures of the models is around this value (equivalent to  $\sim 3500$  K). A subsample containing dwarfs, and all the subdwarfs from the Catalogue of Spectroscopic Abundances (Cayrel de Strobel et al. 1992) with  $[\text{Fe}/\text{H}] < 0$ , observable from the Teide Observatory ( $66^\circ > \delta > -28^\circ$ ) has also been included in order to revise the published relations  $[\text{Fe}/\text{H}] = f((b - y), m_1, c_1, \delta_{0.6}(U - B), (B - V) \dots)$ . The revisions will provide good estimates of the metallicity for the remainder of the stars of the programme (see Sect. 4.5). A number of stars in the sample are in the input catalogue of the Hipparcos mission. The sample also contains a group of metal poor stars whose parallaxes have been accurately determined (Sandage 1983; Laird et al. 1987; Van Altena et al. 1988).

The dwarfs and subdwarfs from Carney (1983a, b) not common to Paper I were incorporated in order to increase the sampling of the metallicity range for types F0-K0. It is noteworthy the good quality of Carney's photometry, and also the close similarity of TCS and CIT infrared systems. The dwarfs contained in the list of calibration stars of the TCS (Kidger 1992) not measured for this programme have also been incorporated into the sample. Some stars contained in the study of M dwarfs by Legget (1992) with  $(V - K) \leq 4.0$  were initially



**Table 10.** Comparison between the temperatures derived in the present work (Col. 2) and those derived by Blackwell & Lynas-Gray (1994) (Col. 3). The mean difference  $T_{\text{IRFM}} - T_{\text{BG89}}$  is  $-31 \pm 58$  K

Star	$T_{\text{IRFM}}$ (K)	$T_{\text{BL94}}$ (K)	$\Delta T$ (%)	$\Delta T$ (K)
HR0509	5388	5316	-1.34	72
HR0219 *	5817	6044	3.90	-227
HR0937	5996	6042	0.77	-46
HR1101	5998	5977	-0.35	21
HR1325	5079	5163	1.65	-84
HR1729	5847	5947	1.71	-100
HR5447	6770	6763	-0.10	7
HR5634	6571	6617	0.70	-46
HR5986	6158	6169	0.18	-11
HR8905	5954	6050	1.61	-96

\* This spectroscopic binary star has been discarded in the computation of the mean difference.

included in the sample, but their cool temperatures (3500–4000 K) are well under limit of validity of the models due to the problems associated to the computation of molecular opacities (Kurucz 1991). Finally, some bright population I stars from Saxner & Hammarbäck (1985) and Bell & Gustafsson (1989), and population II stars from Arribas & Martínez-Roger (1989), who provide temperatures obtained by applying the IRFM, have been included in the sample in order to make comparisons.

In summary, the final sample consists of nearly 500 stars. This number clearly surpasses that of the previous works devoted to the study of the scale of temperatures of low main sequence, especially those which analyse metallicity effects.

#### 4.2. The IR monochromatic fluxes

The determination of monochromatic fluxes at a wavelength of the IR continuum requires, from the observational side, the measurement of IR photometry for the problem stars with respect to a standard whose absolute flux be well determined. By using the results summarised in Sects. 4.2.1 and 4.2.2, we have determined the monochromatic fluxes in  $\lambda_J$ ,  $\lambda_H$  and  $\lambda_K$  for each star in the present sample, which are listed in Table 4.

##### 4.2.1. The IR photometry

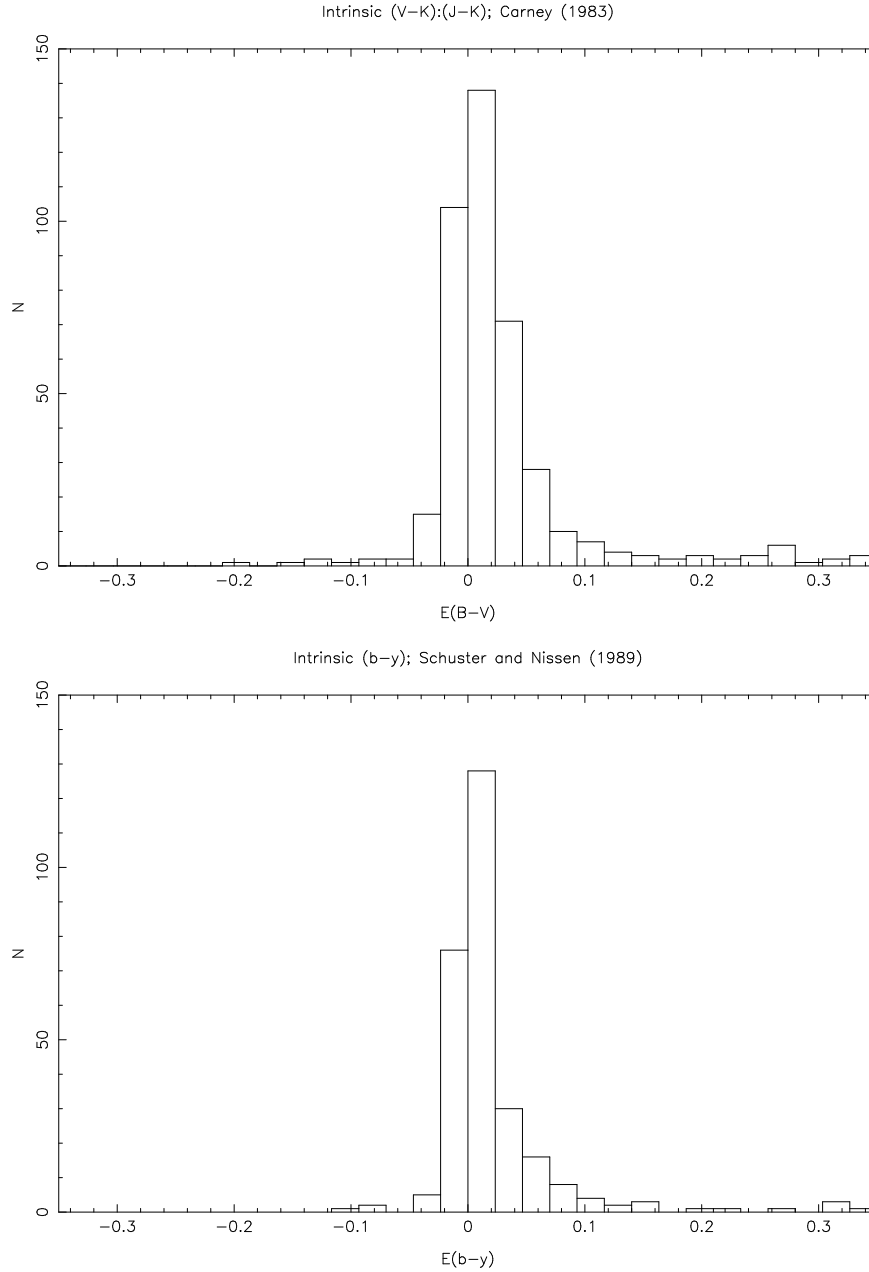
The programme of broad band photometry in the near IR is described in Paper I. There, the photometric system of the TCS was characterized and the transformation equations into/from different photometric systems were established. The  $J$ ,  $H$  and  $K$  magnitudes were measured for 75% of the stars in the sample, with an accuracy in the order of 0.02 mag. For the remainder of the stars, the photometry was obtained from the literature (Carney 1983a, b; Legget 1992; Kidger 1992; Saxner & Hammarbäck 1985; Bell & Gustafsson 1989), after checking that these works had a similar level of accuracy.

The isolated effect of the photometric errors on the  $T_{\text{eff}}$  determination can be inferred from Sect. 3.3, taking into account Eq. (4).

##### 4.2.2. The absolute calibration of the IR flux

In Paper II, a semiempirical method was devised to determine the absolute calibration of the flux of Vega in the near IR (from  $J$  to  $L'$ ). This absolute calibration sets on the same scale the temperatures derived applying the IRFM with new Kurucz's models and the mean direct temperatures derived from angular diameters measurements. When compared to the results of the only so far empirical calibration, summarised by Mountain et al. (1985, M85), a clear trend with wavelength may be appreciated (+0.2% in the band  $J$ , -1.5% in the band  $H$  and -4.5 in the band  $K$ ). This point suggests that the IR fluxes for Vega by M85 are overestimated towards the longest wavelengths. However, it is worth noticing the good agreement (within 1%) with the semiempirical calibration for Vega provided by Walker & Cohen (1992), the theoretical one by Dreiling & Bell (1980) and the 'self-consistent' calibration by Blackwell et al. (1991).

The errors in the absolute IR flux calibration have different effects on the temperatures derived by mean of the IRFM, depending on the photometric band (Table 5). The errors of the absolute IR flux calibration were estimated 3% in the band  $J$ , and 4% in the bands  $H$  and  $K$ . Over 4000 K the effect of these errors is practically a shift in the zero point of the temperatures scale. Considering that the above errors correlate in the three bands, the shift in the zero point of the temperature scale would amount 1.2–1.7% over 4000 K. However if, as it is most likely, the errors in the three bands are uncorrelated, the shift of the zero point is around 0.4–0.9%. Although the indetermination of the zero point of the scale is common to all kind of methods used to derive temperatures, the method adopted in Paper II to fix the absolute calibration of the



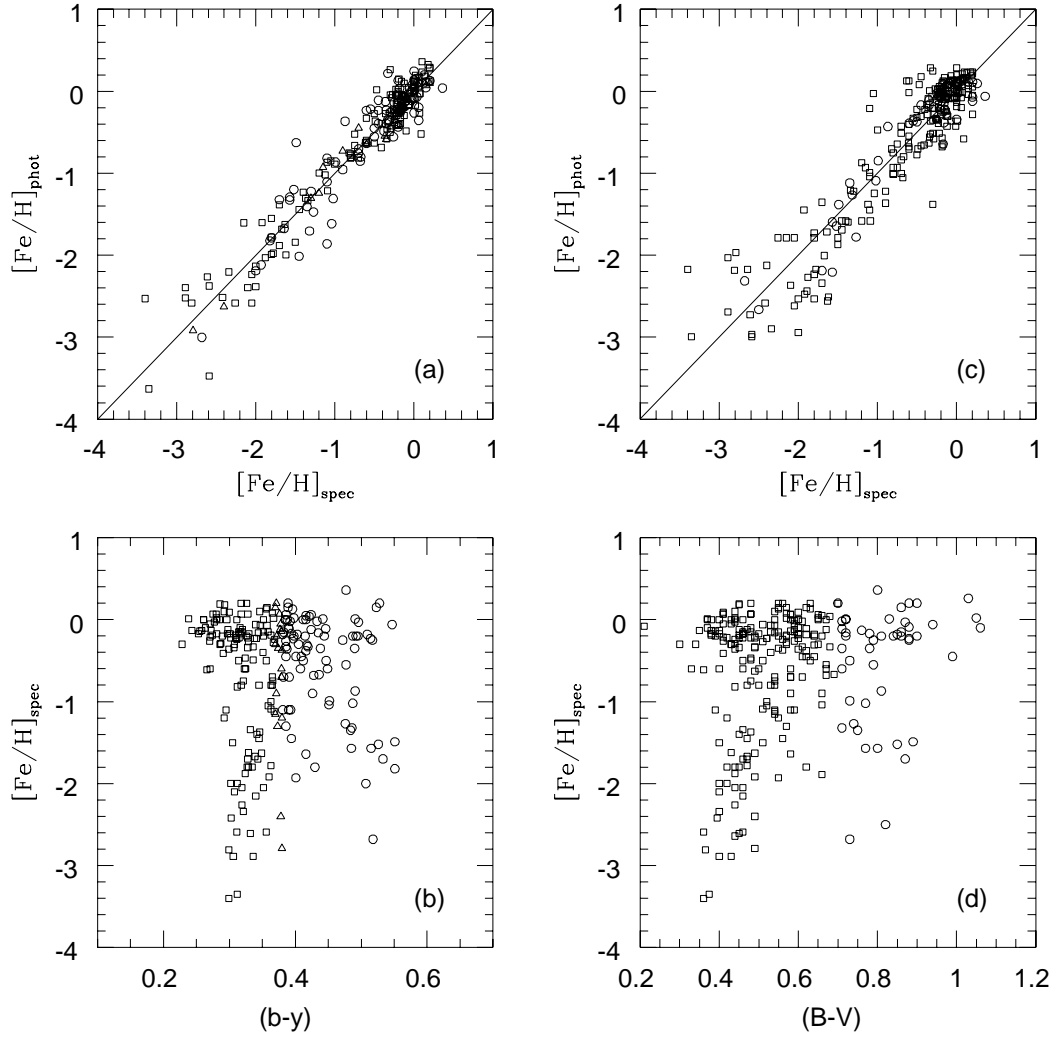
**Fig. 5.** Top: extinction histogram ( $E(B - V)$ ) obtained applying to the stars of the sample the method based on the intrinsic colours  $(V - K):(J - K)$  (Carney 1983). Bottom: extinction histogram ( $E(b - y)$ ) obtained applying to the stars of the sample the method based on the intrinsic relations Strömgren photometry- $\beta$  index (Schuster & Nissen 1989)

flux in the near IR was designed in order to minimise this error.

#### 4.3. The bolometric fluxes

For the spectral types studied in the present work, nearly all the flux arriving at the edge of the earth atmosphere passes through the atmospheric windows. Petford et al. (1988) report an accuracy of the order of 2% when compar-

ing  $F_{\text{bol}}$  derived directly from calibrated spectra to  $F_{\text{Bol}}$  obtained integrating  $UBVRI$  photometry. Therefore, the bolometric flux might be obtained from broad band photometry for each star in the sample. However, photometric calibrations of the type provided by Blackwell & Petford (1991) represent a more practical, and as accurate approach. Unfortunately, this calibrations do not include the effect of the metallicity, being only valid for Population I stars. In order to overcome this difficulty, we provided in

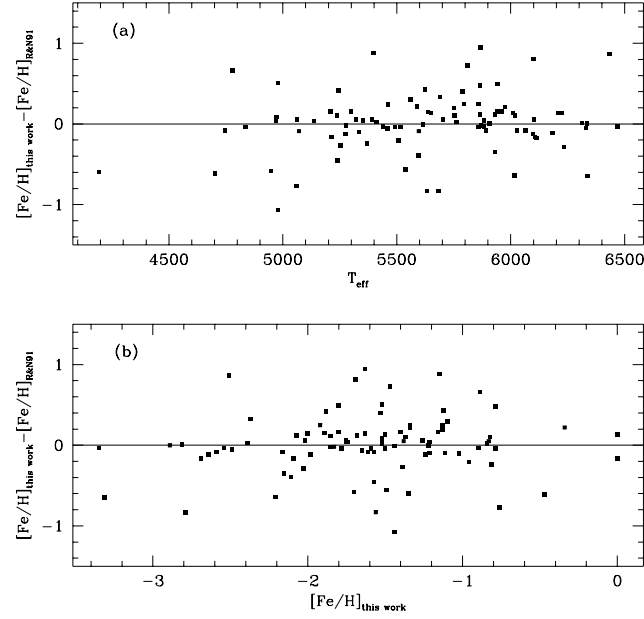


**Fig. 6.** **a)** Comparison between spectroscopic values of the metal abundance (Cayrel de Strobel et al. (1992) and Beers et al. (1991)) and values derived using the calibration by Schuster & Nissen (1989) revised according to expressions (6) and (7). Circles: calibration for F stars, squares: calibration for G stars, triangles: stars in the overlapping range of F and G calibrations. **b)** Range of colour covered by the revised calibration by Schuster & Nissen (1989). **c)** Comparison between spectroscopic values of the metal abundance (Cayrel de Strobel et al. 1992 and Beers et al. 1990) and values derived using the calibration by Carney (1979) revised according to expressions (9) and (10). Squares:  $(B - V) > 0.7$ , circles:  $(B - V) < 0.7$ . **d)** Range of colour covered by the revised calibration by Carney (1979)

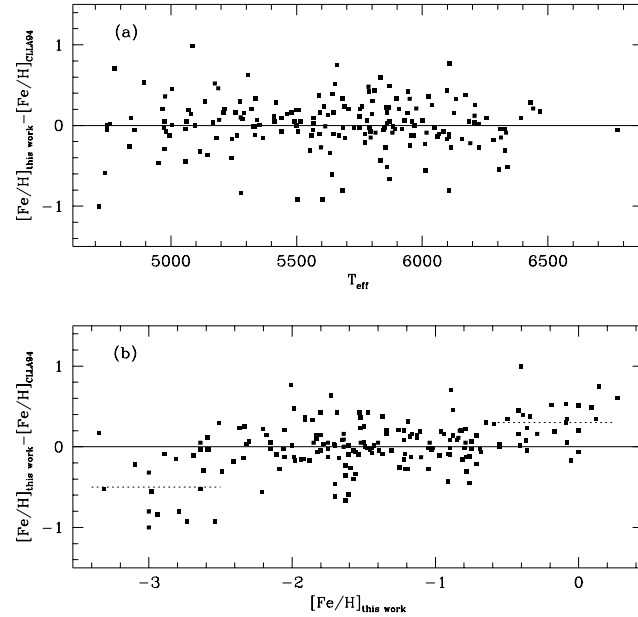
Paper III calibrations of the bolometric flux as a function of  $K$ ,  $(V - K)$  and  $[\text{Fe}/\text{H}]$  for main sequence stars of spectral types F, G and K, which grant the overall level of accuracy expected for the final temperatures derived in this work. It should be noted that these calibrations are ultimately based on the optical absolute flux calibrations of Vega by Hayes & Latham (1975) and Tüg et al. (1977), and the IR absolute flux of Paper II. The bolometric fluxes assigned to the stars in the sample are listed in Table 4.

#### 4.4. The reddening correction

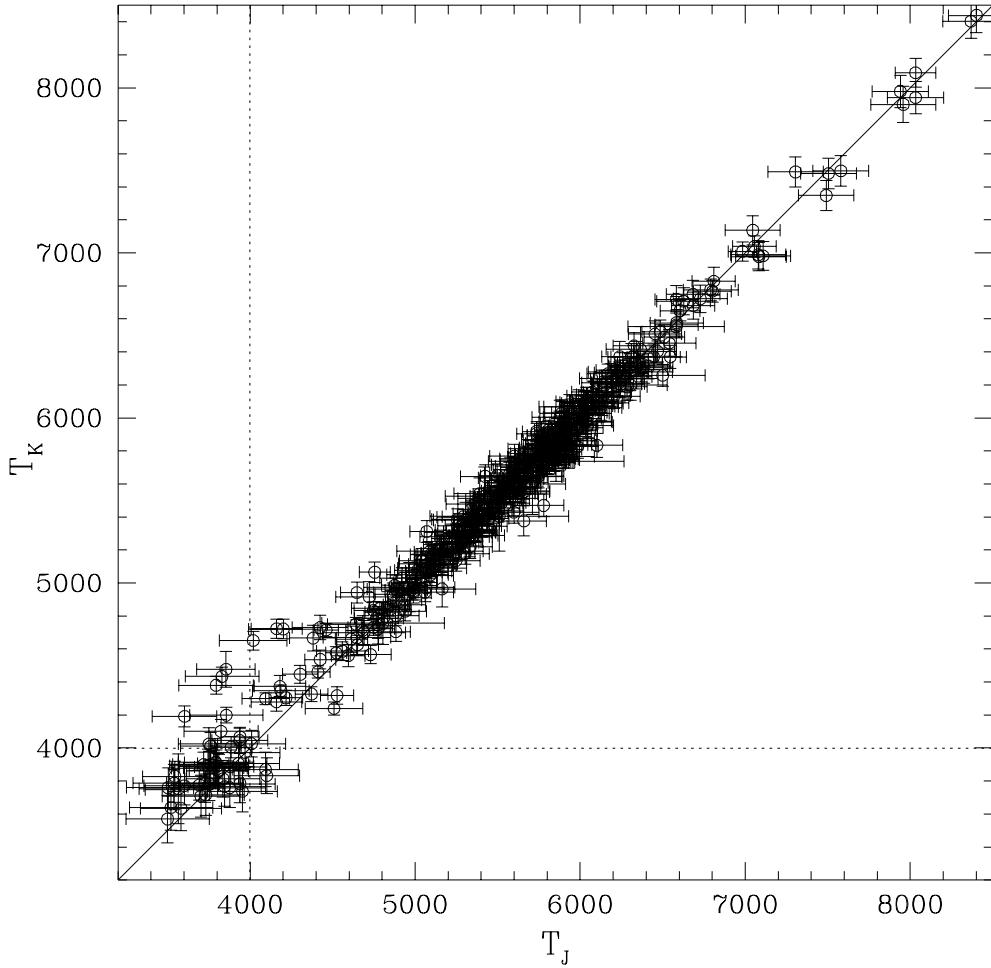
Most of the stars in the sample should not be significantly affected by the interstellar absorption, since are distributed close in the solar neighbourhood. However, in some cases reddening corrections need to be applied. Therefore,  $E(B - V)$  has been estimated for each star in the sample. When these values have been considered significant, the colours have been corrected according to the extinction law ( $A_\lambda = f(A_V, \lambda)$ ) compiled by Landolt-Börnstein (1982c). Two independent methods



**Fig. 7.** **a)** Differences between the metallicities adopted in this work and those derived by Ryan & Norris (1991) versus effective temperature. **b)** The same that in **a)** versus metallicity. The differences show no apparent trends either with temperature or metallicity



**Fig. 8.** **a)** Differences between the metallicities adopted in this work and those derived by Carney et al. (1994) versus effective temperature. **b)** The same that in **a)** versus metallicity. No trend may be appreciated with temperature. However, our  $[\text{Fe}/\text{H}]$  estimate is 0.5 dex higher for  $[\text{Fe}/\text{H}] < -2.5$ , and 0.3 dex lower for  $[\text{Fe}/\text{H}] > -0.5$



**Fig. 9.** Comparison between  $T_J$  and  $T_K$ . The dotted lines mark the lower limit ( $T_{\text{eff}} = 4000$  K) where models begin to falter due to the lacking of molecular opacity sources. It is worth notice the progressive departure of the points from the diagonal towards the cooler stars

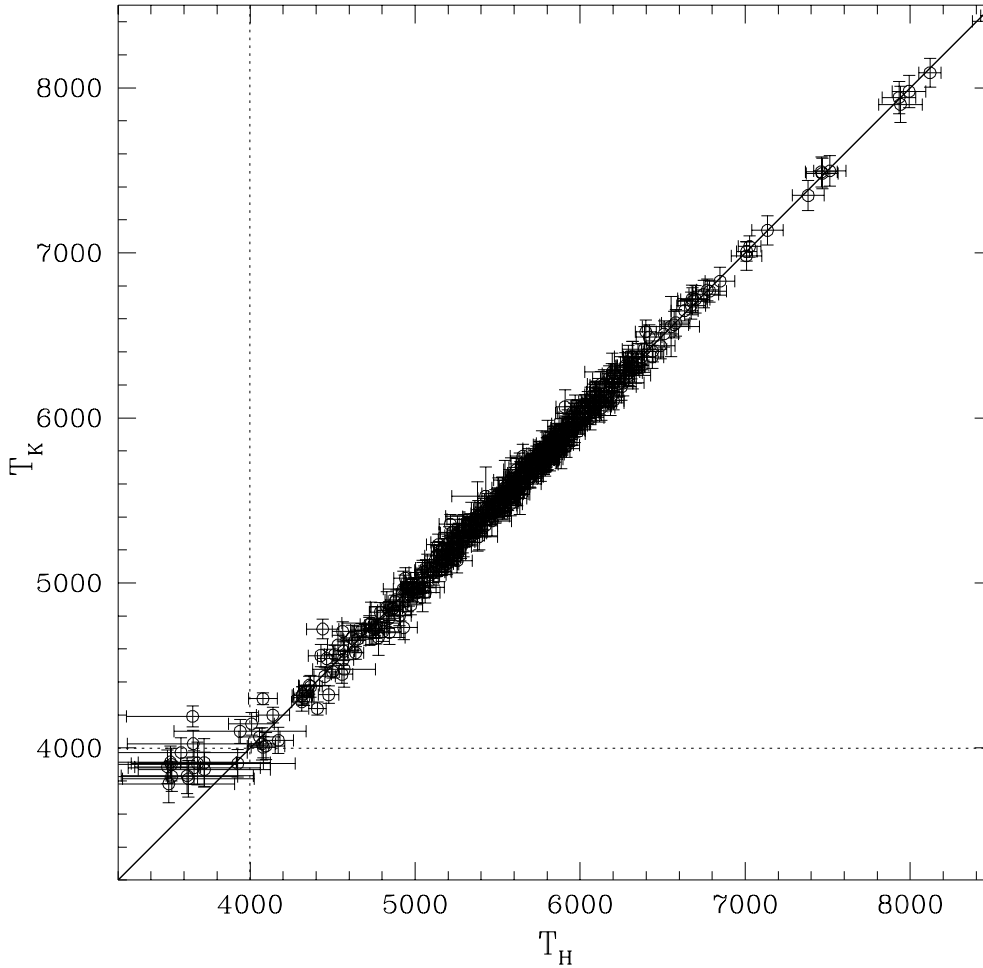
have been considered for determining  $E(B - V)$ . The first one is based on the intrinsic relation  $(V - K):(J - K)$  (Carney 1983a), considering  $E(V - K) = 2.72 E(B - V)$  (Savage & Mathis 1979). The histogram obtained with all the values within the application range is presented in Fig. 5. The second method is based on the  $\beta$  index and Strömgren photometry. Schuster & Nissen (1989) have calibrated  $E(b - y)$  with an accuracy of 0.015 mag. The result of applying this calibration to the stars of the sample is showed in the histogram of Fig. 5.

Moreover a number of stars of the sample have extinction estimations determined by other authors (Laird et al. 1987; Beers et al. 1990) based on reddening maps by Burnstein & Heiles (1982). The correlation between the different methods is acceptable for  $E(B - V) < 0.1$  mag,

over this value it worsens.

When Strömgren and  $\beta$  photometry was available the method by Schuster & Nissen (1989) was preferred, considering  $E(B - V) = 0$  for  $E(b - y) < 0.025$ , and  $E(B - V) = 1.37 E(b - y)$  otherwise (Crawford 1975). The values taken from the literature, and those determined by means of the intrinsic relation  $(V - K):(J - K)$  were considered for the remainder of the stars. Table 4 contains the reddening value assigned to each star in the sample. Note that only a relatively reduced number of stars (about 15 percent) needed reddening correction.

The first line of Table 5 shows the change in temperature induced by  $E(B - V) = 0.05$  mag when applying the IRFM. The effect is stronger for hot stars which emit most of their flux in the visible/UV wavelength range.



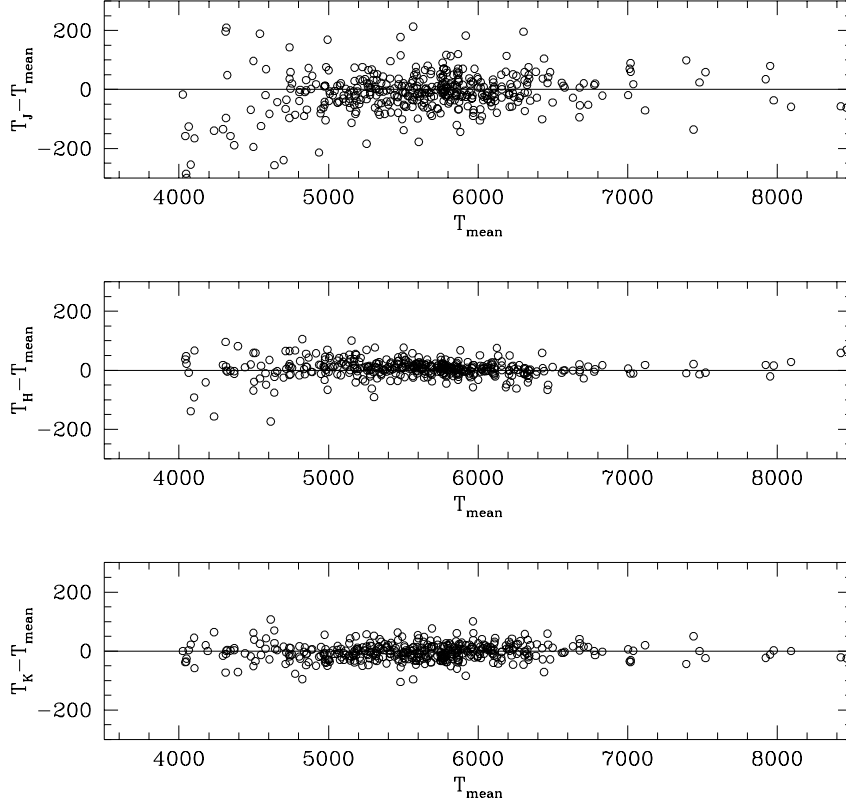
**Fig. 10.** The same that Fig. 9 for  $T_H$  and  $T_K$ . Notice the small dispersion around the diagonal line over 4000 K

#### 4.5. Metallicity and surface gravity

The effective temperature determination by means of Eq. (4) requires an estimation of the star metallicity and surface gravity. These parameters, however, need not to be very accurate as commented in Sect. 3.3. In particular, it may be concluded that 0.5 dex and 0.3 dex uncertainties in  $\log(g)$  and  $[\text{Fe}/\text{H}]$ , respectively, are sufficient to obtain temperatures within an accuracy of 2% (see Table 6). Therefore, regarding the surface gravity, it is enough to consider an average surface gravity  $\log(g)=4.5$  for the subdwarfs. However, taking into account the effect of  $T_{\text{eff}}$  on the stellar radius, we have preferred to assign  $\log(g) = 5$  for the cooler stars, and  $\log(g)=4$  for hottest population I stars. These values are compatible with those provided in the reviews by Popper (1980) and Andersen (1991) for detached binary systems formed by main sequence stars. The gravities adopted for the stars of the sample are listed in Col. 2 of Table 4.

Unfortunately, only a limited number of stars in the sample had their metal abundance determined from fine spectroscopic analysis included in the Catalogue of  $[\text{Fe}/\text{H}]$  determinations by Cayrel de Strobel et al. (1992). Therefore for the remainder of stars, photometric metallicity calibrations based on  $\delta_{0.6}(U - B)$  index (Carney 1979), and on Strömgren photometry (Schuster & Nissen 1989), were adopted.

Instead of apply directly these calibrations, we have checked their validity and accuracy. For this purpose, 252 dwarfs and subdwarfs from Cayrel de Strobel et al. (1992) were considered. For each star we assign an averaged abundance giving preference in the weights to recent data based on solid state detectors. We also included, in that group for checking the photometric calibrations, 45 dwarfs from Beers et al. (1990) common to our sample. We have found slight differences between the photometric calibrations and the spectroscopic values which are



**Fig. 11.** Differences  $T_J - T_{\text{mean}}$  (top),  $T_H - T_{\text{mean}}$  (center) and  $T_K - T_{\text{mean}}$  (bottom) versus effective temperature adopted. No apparent trend may be appreciated

commented below.

(a) *Strömgren photometry calibration.* (Schuster & Nissen 1989): 238 stars with spectroscopic determination of the abundance are within the ranges of the calibrations by Schuster & Nissen (1989). The following corrections were applied:

$$[\text{Fe}/\text{H}]_{\text{phot}}^{\text{F}} = 0.82[\text{Fe}/\text{H}]_{\text{spec}} - 0.08, \quad \sigma = 0.18, \quad \text{dex } n = 150, \quad (6)$$

$$[\text{Fe}/\text{H}]_{\text{phot}}^{\text{G}} = 0.93[\text{Fe}/\text{H}]_{\text{spec}} - 0.01, \quad \sigma = 0.21, \quad \text{dex } n = 105, \quad (7)$$

where the superindex refers to the calibration of type F and G stars. The zero correction is practically negligible, whereas the correction of the slope may imply differences of 0.3–0.5 dex. If we consider both calibrations altogether, the correction should be:

$$[\text{Fe}/\text{H}]_{\text{phot}} = 0.85[\text{Fe}/\text{H}]_{\text{spec}} - 0.04, \quad \sigma = 0.22, \quad \text{dex } n = 238. \quad (8)$$

This result agrees with the conclusion by Schuster & Nissen (1989) that their calibrations should perhaps require a slight correction to adjust the revised spectroscopic

values (they propose a multiplicative factor of correction for their calibration of 1.15 which roughly coincides with our correction).

(b) *Broad band photometry:*  $\delta_{0.6}(U - B)$  (Carney 1979): 259 stars with spectroscopic determinations are within the range of the calibration of  $\delta_{0.6}(U - B)$  index by Carney (1979). This calibration has been extended to the limit permitted by the deblanketing vectors provided by Sandage (1969). Correction differs according to colour.

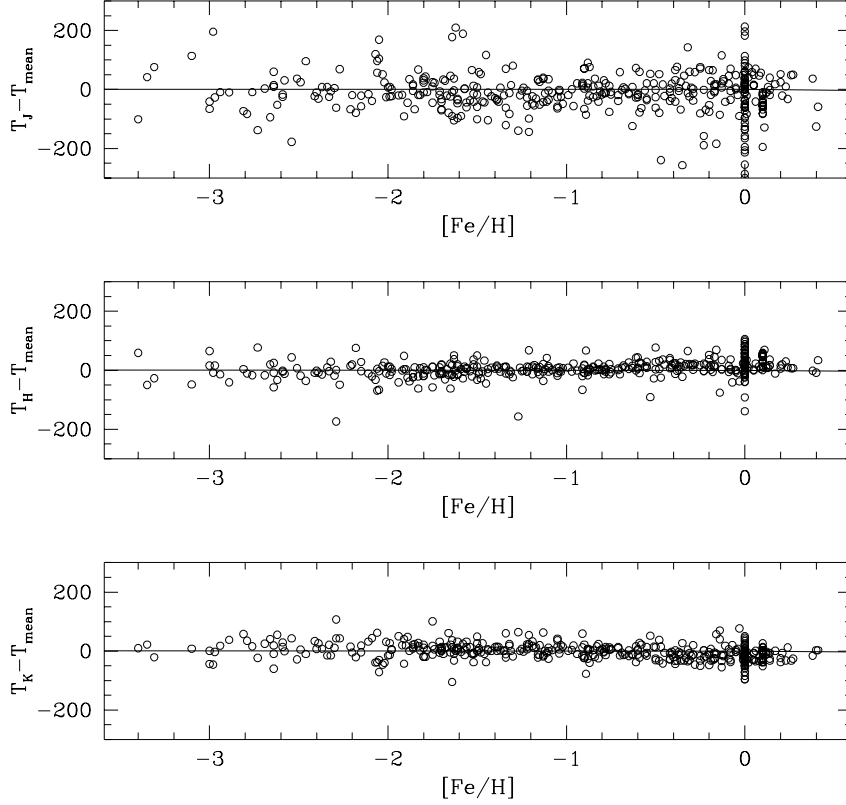
$$[\text{Fe}/\text{H}]_{\text{phot}} = 0.83[\text{Fe}/\text{H}]_{\text{spec}} - 0.02, \quad \sigma = 0.28 \text{ dex}, \quad (9)$$

$$n = 212, \quad (0.35 < (B - V) \leq 0.7),$$

$$[\text{Fe}/\text{H}]_{\text{phot}} = 1.03[\text{Fe}/\text{H}]_{\text{spec}} + 0.10, \quad \sigma = 0.25 \text{ dex}, \quad (10)$$

$$n = 48, \quad (0.7 \geq (B - V) < 1.1),$$

Figure 6 shows the comparison, after corrections, between the spectroscopic and photometric values of the abundance, and the ranges of colour and metallicity covered. Notice the loss of sensitivity, with increasing



**Fig. 12.** The same that Fig. 11 versus  $[\text{Fe}/\text{H}]$

metallicity, in both calibrations.

In summary, the metallicity has been assigned in a twofold way: Firstly, spectroscopic determined  $[\text{Fe}/\text{H}]$  (Cayrel de Strobel et al. 1992), with a mean accuracy within 0.15 dex, have been preferred. Secondly, the revised calibrations by Schuster & Nissen (1989) (accuracy within 0.2 dex) and Carney (1979) (accuracy within 0.3 dex) were applied to the stars lacking fine spectroscopic analysis.

For the M stars extracted from the compilation by Legget (1992), metallicity has been assigned according to their kinematical classification (i.e.  $[\text{Fe}/\text{H}] = 0$  for young disk stars,  $[\text{Fe}/\text{H}] = -1$  for young disk to old disk transition stars, and  $[\text{Fe}/\text{H}] = -1.5$  for old disk stars).

The assigned metallicities are listed in Col. 3 of Table 4.

#### 4.5.1. Comparison to other determinations

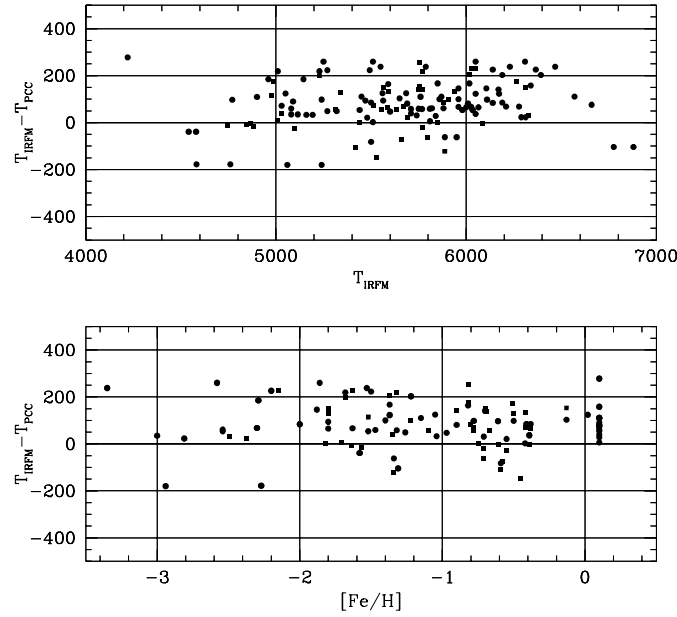
Our work share 92 and 186 stars in common with the extensive surveys of Ryan & Norris (1991; R&N91) and

Carney et al. (1994; CLLA94) respectively. Both works provide a good basis to check the scale of metallicity adopted here.

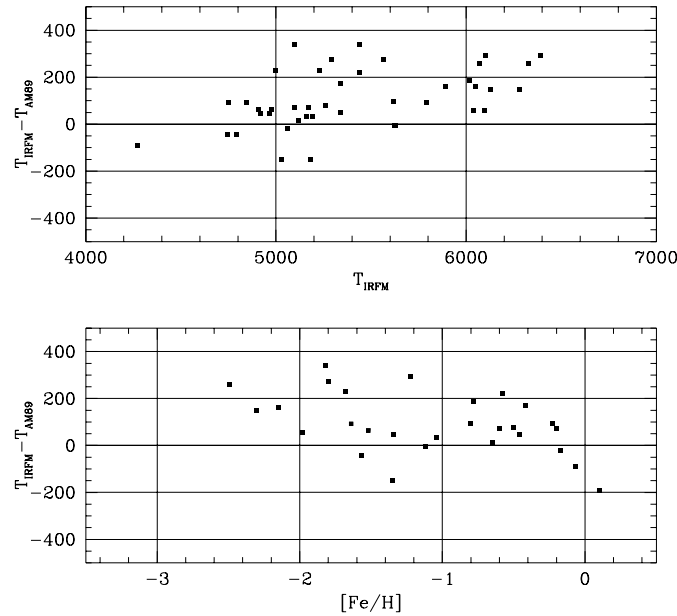
In Fig. 7, we compare our  $[\text{Fe}/\text{H}]$  estimates to the abundances derived by R&N91 based on a calibration of the Ca II H and K line absorption. The mean difference  $[\text{Fe}/\text{H}]_{\text{This work}} - [\text{Fe}/\text{H}]_{\text{R\&N91}}$  is 0.01 dex with  $\sigma = 0.37$  dex. The scatter of the differences is compatible with the internal errors of both works. No trend of the differences may be appreciated either with temperature (Fig. 7a) or with metallicity (Fig. 7b).

The comparison of the abundances adopted by us with those derived by CLLA94, based on the cross correlation of high resolution low  $S/N$  spectra with model templates, shows a fairly good agreement in the range from  $[\text{Fe}/\text{H}] = -2.5$  to  $[\text{Fe}/\text{H}] = -0.75$ . However, noteworthy differences appear for  $[\text{Fe}/\text{H}] < -2.5$  and  $[\text{Fe}/\text{H}] > -0.5$ . The overall mean difference  $[\text{Fe}/\text{H}]_{\text{This work}} - [\text{Fe}/\text{H}]_{\text{CLLA94}}$  is 0.01 dex with  $\sigma = 0.31$  dex. No trend with temperature may be appreciated in the differences (Fig. 8a), however there exists a clear correlation with metallicity (Fig. 8b).





**Fig. 13.** Differences between the temperatures derived in this work ( $T_{\text{IRFM}}$ ) and those derived by Peterson & Carney (1979; Squares), and Carney (1983; Circles).  $T_{\text{PCC}}$  are, in average, 100 K cooler than those derived in the present work. There exists a slight trend with temperature. The differences have a slight slope amounting approximately 100 K between the extreme points of the overlapping range



**Fig. 14.** Differences between the temperatures derived in this work ( $T_{\text{IRFM}}$ ) and those derived by Arribas & Martínez-Roger (1989).  $T_{\text{AM89}}$  are, in average, 150 K cooler than those derived in the present work. There exist clear trends with temperature and metallicity. The differences may be explained taking into account the different models and absolute flux calibration of the IR flux adopted in both work

On the one hand, our  $[\text{Fe}/\text{H}]$  estimate for the most metal deficient stars ( $[\text{Fe}/\text{H}] < -2.5$ ) is 0.5 dex higher in average than  $[\text{Fe}/\text{H}]_{\text{CLLA94}}$ , which implies a difference of  $\pm 0.2\%$  in the temperature derived using the IRFM. On the other, our  $[\text{Fe}/\text{H}]$  estimate for stars with  $[\text{Fe}/\text{H}] > -0.5$  is 0.3 dex lower in average, which implies a difference of  $\pm 0.4\%$  in temperatures derived using the IRFM.

### 5. The temperatures determination

According to the procedure described in previous sections, we have derived three effective temperatures for each sample star by applying the IRFM in the IR wavelengths considered (Eq. 4). The individual values  $T_J$ ,  $T_H$  and  $T_K$ , with their errors are listed in Table 4.

Figures 9 and 10 present the comparison between the temperatures obtained in the three different bands taking  $T_K$  as a reference. The individual errorbars allow to appreciate that the dispersion is compatible with the estimated errors derived from the uncertainties in the input parameters of the IRFM. As expected, the uncertainties are greater for temperatures obtained from  $R_J$  factors, due to the lesser sensitivity of the IRFM in this band, and the greater photometric error in the measurement of  $J$ . The consistency of  $T_J$ ,  $T_H$  and  $T_K$  is good over 4000 K, however under this temperature there exist noteworthy discrepancies due to the fact that  $R_J$ - and  $R_H$ -factors lose their sensitivity to temperature in this range.

The final temperature was derived as the mean of  $T_J$ ,  $T_H$  and  $T_K$  weighted with the inverse of their errors:

$$\overline{T}_{\text{IRFM}} = \frac{\frac{T_J}{(\Delta T_J)} + \frac{T_H}{(\Delta T_H)} + \frac{T_K}{(\Delta T_K)}}{\left[\frac{1}{\Delta T_J} + \frac{1}{\Delta T_H} + \frac{1}{\Delta T_K}\right]}. \quad (11)$$

In order to estimate the error of the mean temperature, a linear transmission of the errors was considered, given that the errors in each band are not totally independent:

$$\Delta T_{\text{IRFM}} = \frac{3}{\left[\frac{1}{\Delta T_J} + \frac{1}{\Delta T_H} + \frac{1}{\Delta T_K}\right]}, \quad (12)$$

where the error in the temperature of each band is defined by

$$\begin{aligned} (\Delta T_i)^2 = & \left[ \frac{\Delta T_i}{\Delta[q(\lambda_i)R(\lambda_i)]} \right]^2 (\Delta[q(\lambda_i)R(\lambda_i)])^2 \\ & + \left[ \frac{\Delta T_i}{\Delta[\text{Fe}/\text{H}]} \right]^2 (\Delta[\text{Fe}/\text{H}])^2 \\ & + \left[ \frac{\Delta T_i}{\Delta \log(g)} \right]^2 (\Delta \log(g))^2 \end{aligned} \quad (13)$$

Over 5000 K, the temperatures in the three bands enter the average with similar weight. In that range, the assignation of weights automatically takes into account the unlike sensitivity of the IRFM in the different bands

and the individual quality of IR photometry. However, under 5000 K only  $T_H$  and  $T_K$  has been considered in the average, since  $R_J$  is a very insensitive indicator of temperature for the cooler stars. Under 4000 K, only  $T_K$  has been considered. This is due to the fact that the coolest models show in the band  $H$  a local maximum of flux which is not observed in IR spectra (Langon & Rocca-Volmerange 1992). The mean error in the final temperatures is around 1–2%. Notice however, that the uncertainties in the temperatures derived under 4000 K are greater than the errors determined from Eq. (12) due to the difficulties of models in this range caused by the absence of important sources of opacity associated to some molecules. Likewise, the IRFM is difficult to apply at temperatures over 8000 K (five stars of the sample have such high temperatures) because as these stars emit a substantial proportion of energy at short wavelengths, the correction for interstellar extinction and the determination of the bolometric flux are rather uncertain. For these reasons, the temperatures outside the range  $4000 \text{ K} < T_{\text{eff}} < 8000 \text{ K}$  have a lower level of accuracy (perhaps a most adequated estimation is the duplication of the size of the errorbars quoted in Table 4 for these temperatures).

We show in Figs. 11 and 12 the differences of  $T_J$ ,  $T_H$  and  $T_K$  from the mean temperature adopted. Over 4000 K they follow approximately a normal distribution both with effective temperature and metallicity.

### 6. Comparison with other determinations

In this section, we provide the comparison of our temperatures with those derived by other authors for common stars of the sample. Furthermore a detailed analysis of the scale of temperatures derived from the present work will be done in a subsequent paper by considering the mean relations  $T_{\text{eff}}: [\text{Fe}/\text{H}]$  and photometric colours  $UBVR IJHK$  and  $uvby-\beta$ .

The Sun and Procyon, the only dwarfs later than F5 whose diameters has been measured by optical methods, are included in the sample. The agreement between their IRFM temperatures and the direct ones is excellent. In fact, the IRFM provides 6579 K for Procyon, close to the direct temperature (6510 K) obtained considering its angular diameter (Hanbury-Brown et al. 1974; Mozurkewich et al. 1991) and its bolometric flux (Code et al. 1976). Regarding the Sun, the value derived from the IRFM determination is 5763 K. This good agreement is a consequence of the procedure followed for scaling the effective temperatures obtained from the IRFM, since the absolute calibration in the near IR was established on the basis of empirical diameters measurements. In addition, it is worthy to notice that the mean temperatures of solar analogue stars (spectral types G0/2V,  $[\text{Fe}/\text{H}] \sim 0$ ,  $(B - V) \sim$

0.63) is close to the solar value ( $5743 \pm 100$  K vs. 5780 K for the Sun), and the same for stars of types F3/5V,  $[\text{Fe}/\text{H}] \sim -0.05$ ,  $(B - V) \sim 0.43$  similar in their features to Procyon ( $6578 \pm 150$  K vs. 6510 K).

The works by Peterson & Carney (1979), and Carney (1983a) (hereafter PCC), based on spectrophotometric analysis, contain respectively 43 and 64 stars common to our sample whose range of temperatures and metallicities is similar to that analysed in the present programme. Figure 13 shows the difference  $T_{\text{IRFM}} - T_{\text{PCC}}$  versus temperature and metallicity. PCC temperatures are, in average, 100 K cooler than those derived in the present work. No significant trend of the differences with metallicity may be appreciated. However there could exist a slight slope along the axis of temperatures amounting approximately 100 K between the extreme points of the overlapping range. This difference is compatible with the uncertainty of the zero point. The different models considered might also explain the observed discrepancies.

There are 18 stars common to the work by Saxner & Hammarbäck (1985, SH85) devoted to F stars and based on the application of the IRFM. The good agreement is noteworthy as can be appreciated from Table 7. The differences are compatible with the errors of both works, and the average residuals only amount  $5 \pm 63$  K ( $T_{\text{SH85}}$  are cooler).

The work by Magain (1987) based on the IRFM presents 11 stars in the metallicity range  $(-1, -3)$ . The mean difference  $T_{\text{IRFM}} - T_{\text{M87}}$  is  $112 \pm 56$  K (Table 8) which implies a shift of 1.9% in the zero point of the temperature scale. This work adopts the IR absolute flux calibration provided by SH85 which is very close to ours ( $+0.3\%$  in  $J$  and  $+1.8\%$  in  $K$ ), so the differences of the models considered in each work should account for the shift of the zero.

There are 28 stars common to the work by Arribas y Martínez-Roger (1989, AM89), based on the application of the IRFM using the empirical absolute flux calibration of the IR flux of Vega derived by Mountain et al. (1985), and models by Kurucz (1979) and Gustafsson et al. (1975). The systematic differences found both with temperature and metallicity (Fig. 14) may be explained taking into account that the models used in the present work include new opacities, and also to the problems of the IR absolute flux calibration derived by Mountain et al. (1985) as described in Paper II.

Bell & Gustafsson (1989, BG89) present 13 dwarfs common to the present sample. BG89 temperatures are based on the IRFM corrected using IR synthetic colours. Over 4500 K the differences listed in Table 9 are compatible with a zero point shift of 56 K ( $T_{\text{BG89}}$  are hotter). For

the coolest stars, where models loses reliability, differences are stronger. The discrepancies are explained taking into account the differences in the bolometric fluxes considered in both works (see Paper III).

Blackwell & Lynas-Gray (1994, BLG94) have recently applied the IRFM using the new Kurucz's models to a sample of Population I stars. Although only 11 dwarfs are common to the present sample and consequently possible systematic differences are difficult to ascertain, that work is a good source for comparison, given that the main difference respect to the present work is the IR absolute flux calibration. BLG94 adopt the theoretical calibration of the IR flux of Vega provided by Dreiling & Bell (1980), which differ less than 1% in all the bands from that adopted here. Table 10 shows the differences. In average,  $T_{\text{BLG94}}$  are 31 K hotter than ours (the spectroscopic binary HR 219 has been discarded in the mean), this shift in temperature ( $\sim 0.6\%$ ) is compatible with the slight difference in the bolometric fluxes (around 1.5%), as analysed in Paper III.

## 7. Summary

The IRFM has been applied to a sample of approximately 500 main sequence stars later than F0, which cover the metallicity range  $(0.5, -3.5)$ . Near IR monochromatic fluxes have been used in order to derive  $T_J$ ,  $T_H$  and  $T_K$  for each star. The uncertainties of the input parameters needed to apply the IRFM and the induced errors on the three temperatures derived have been computed. The consistency of the temperatures derived in the three different bands is fairly good over 4000 K. The final temperature for each star in the sample has been derived considering the mean of  $T_J$ ,  $T_H$  and  $T_K$  weighted with the inverse of their errors. From the analysis of the systematical errors associated to the uncertainty of the absolute flux calibration in the near IR, the expected indetermination of the zero point of the scale of temperatures should be around 1%. However the good agreement between the IRFM and direct temperatures for the Sun and Procyon suggests a lower uncertainty. The mean estimated precision for the final temperatures, considering the effect of both systematical and accidental errors, is around 1.5%. The comparison with other works shows slight discrepancies which may be explained considering the differences induced by the improvements adopted in the application of the IRFM: The new atmosphere models, the absolute IR flux calibration and the determination of the bolometric fluxes.

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**Table 4.** The input parameters needed to the application of the IRFM for each star of the sample. Column 1: Identification, the Giclas number has been preferred when available HD, BD, HR and GJ numbers were used otherwise. The stars are ordered in right ascension. Column 2: Surface gravity. Column 3: Metallicity. Column 4: Bolometric flux in ( $\text{erg cm}^{-2} \text{s}^{-1}$ ). Column 5: Interstellar reddening. Column 6: Monochromatic flux in the band  $J$  in ( $10^2 \text{ erg cm}^{-2} \text{s}^{-1} \text{ nm}^{-1}$ ). Column 7:  $q$ -factor in the band  $J$ . Column 8: Temperature derived in the band  $J$  (units are K). Column 9: Error in  $T_J$  computed considering errors in  $F_{\text{Bol}}$ ,  $F_J$ ,  $\log(g)$  and  $[\text{Fe}/\text{H}]$ . Columns 10-13: The same that Cols. 6-9 for the band  $H$ . Columns 14-17: The same that Cols. 6-9 for the band  $K$ . Column 18: The weighted mean temperature derived from  $T_J$ ,  $T_H$  and  $T_K$ . Temperatures in brackets have not been considered in the mean as explained in Sect. 5. Column 19: Mean error computed considering linear transmission of errors from Cols. 9, 13 and 17. Temperatures under 4000 K are given in parentheses without estimation of the total error because of the uncertainties of the model fluxes in this range

ID	$\log(g)$	$[\text{Fe}/\text{H}]$	$F_{\text{bol}}$	$F_J$	$\Delta F_J$	$F_H$	$\Delta F_H$	$F_K$	$\Delta F_K$	$T_J$	$\Delta T_J$	$T_H$	$\Delta T_H$	$T_K$	$\Delta T_K$	$T_{\text{mean}}$	$\Delta T_{\text{mean}}$
800	4.34	0.00	1.359e-10	4.226e-12	1.011	2.762	135	2.830e-12	1.019	5788	74	5788	74	5788	74	5788	74
HD144013	4.66	0.00	1.359e-10	4.226e-12	1.011	2.762	135	2.830e-12	1.019	5788	74	5788	74	5788	74	5788	74
6171-309	5.00	0.00	1.110e-10	4.384e-12	1.611	7646	166	1.397e-12	1.006	7195	64	7195	64	7195	64	7195	64
HD1139	4.00	0.00	3.342e-10	4.408e-12	1.662	3786	171	1.328e-12	1.057	8444	70	8444	70	8444	70	8444	70
HR66	4.00	0.00	1.416e-10	1.020e-12	1.014	2725	158	1.215e-11	1.020	5599	78	5599	78	5599	78	5599	78
HR76	4.00	0.00	1.071e-10	1.014	1.014	2725	158	1.215e-11	1.020	5599	78	5599	78	5599	78	5599	78
G000-053	4.50	0.00	3.555e-11	1.057e-12	1.011	5794	134	5.934e-13	1.021	5774	73	5774	73	5774	73	5774	73
G031-041	4.50	0.00	3.555e-11	1.057e-12	1.011	5794	134	5.934e-13	1.021	5774	73	5774	73	5774	73	5774	73
G171-047	5.00	0.00	6.451e-10	1.341e-12	1.013	5646	124	1.254e-12	1.021	5814	79	5814	79	5814	79	5814	79
G170-095	4.50	0.00	6.451e-10	1.341e-12	1.013	5646	124	1.254e-12	1.021	5814	79	5814	79	5814	79	5814	79
HD138	4.00	0.00	1.727e-09	6.890e-12	1.015	6047	94	6.599e-13	1.017	6252	83	6252	83	6252	83	6252	83
HR3667	4.20	0.00	3.146e-10	1.076e-12	1.015	5071	102	4.676e-11	1.024	5644	74	5644	74	5644	74	5644	74
G001-009	4.00	0.00	3.146e-10	1.076e-12	1.015	5071	102	4.676e-11	1.024	5644	74	5644	74	5644	74	5644	74
DC +71 31	4.50	0.00	2.243e-11	1.068e-12	1.015	5655	91	2.056e-13	1.021	5668	81	5668	81	5668	81	5668	81
HD4307	4.00	0.00	2.243e-11	1.068e-12	1.015	5655	91	2.056e-13	1.021	5668	81	5668	81	5668	81	5668	81
G005-009	4.00	0.00	2.243e-11	1.068e-12	1.015	5655	91	2.056e-13	1.021	5668	81	5668	81	5668	81	5668	81
HR219	4.50	0.00	1.138e-08	3.365e-12	1.013	5950	155	3.147e-12	1.021	5778	90	5778	90	5778	90	5778	90
G216-117	5.00	0.00	3.555e-11	1.057e-12	1.011	5850	135	1.937e-12	1.021	5850	135	5850	135	5850	135	5850	135
G246-151	5.00	0.00	3.555e-11	1.057e-12	1.011	5850	135	1.937e-12	1.021	5850	135	5850	135	5850	135	5850	135
G243-052	5.00	0.00	3.555e-11	1.057e-12	1.011	5850	135	1.937e-12	1.021	5850	135	5850	135	5850	135	5850	135
HR321	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12	1.012	5317	171	8.270e-11	1.025	5836	83	5836	83	5836	83	5836	83
G246-134	4.00	0.00	2.539e-09	8.391e-12													

Table 4. continued

ID	$\log(T)$	$[Fe/H]$	$P_{\text{rad}}$	$E(B-V)$	$F_V$	$q_V$	$T_V$	$\Delta T_V$	$F_H$	$q_H$	$T_H$	$\Delta T_H$	$F_K$	$q_K$	$T_K$	$\Delta T_K$	$T_{\text{mean}}$	$\Delta T_{\text{mean}}$
G076-042	4.50	-1.66	1.413e-11	0.00	4.420e-13	1.009	5574	131	2.427e-13	1.024	5538	—	8.922e-14	1.019	5066	70	5634	84
HR1081	4.50	0.02	1.008e-08	0.00	3.856e-10	1.014	5089	142	—	—	—	—	9.176e-11	1.023	5046	62	5078	86
HR1101	4.00	-0.12	1.586e-09	0.00	1.476e-10	1.013	6083	137	—	—	—	—	2.914e-11	1.015	5981	74	5998	101
HD22302	4.50	0.00	5.979e-11	0.00	4.452e-12	—	<3500	—	2.058e-12	1.054	4464	57	7.310e-13	1.029	4542	56	4508	56
G080-015	4.00	-0.71	8.898e-10	0.00	1.776e-11	1.011	5779	123	9.657e-12	1.021	5798	—	3.547e-12	1.017	5808	72	5788	87
G006-034	4.50	0.00	1.081e-10	0.00	6.158e-12	1.008	5966	125	5.448e-13	1.022	5834	79	1.965e-12	1.035	5753	211	(3753)	—
HD24289	4.50	-2.07	3.502e-11	0.05	9.459e-13	1.008	5966	125	5.448e-13	1.022	5834	79	2.030e-13	1.018	5827	72	5866	37
HD23329	4.50	-1.64	1.483e-10	0.04	2.077e-12	1.009	5966	125	5.448e-13	1.022	5834	79	1.427e-12	1.021	4854	93	4842	93
HR1325	4.50	-0.17	5.311e-09	0.00	2.077e-12	1.013	5082	94	1.294e-10	1.036	4828	101	4.881e-11	1.024	5030	74	5040	87
G004-016	4.50	-1.61	5.588e-11	0.00	1.519e-12	1.009	5998	94	7.974e-13	1.019	6048	61	2.949e-13	1.017	6044	75	6034	74
VB 17	4.50	0.00	1.145e-10	0.00	2.936e-12	1.015	5502	150	2.112e-12	1.022	5618	77	8.089e-13	1.018	5537	68	5561	87
VA 60	4.50	0.10	1.613e-10	0.00	5.241e-12	1.014	5668	152	2.737e-12	1.019	5764	79	1.026e-12	1.015	5746	71	5749	90
VA 79	4.50	0.00	1.602e-10	0.00	1.773e-11	1.012	5684	163	8.370e-12	1.006	6749	89	3.037e-12	1.006	6750	83	6736	102
VA 215	4.00	0.10	5.826e-10	0.00	1.382e-11	1.012	6627	163	6.590e-12	1.007	6682	80	2.369e-12	1.007	6707	83	6681	102
VB 49	4.50	0.10	1.351e-10	0.00	4.206e-12	1.014	5800	154	2.173e-12	1.017	5800	80	8.056e-13	1.014	5870	72	5868	91
VA 315	4.50	0.10	4.206e-10	0.00	1.057e-11	1.012	6454	161	5.136e-12	1.009	6509	87	1.870e-12	1.009	6509	80	6498	99
VA 548	5.00	0.10	3.241e-11	0.00	1.558e-12	1.013	4303	107	1.558e-12	1.009	4557	64	4.911e-13	1.029	4447	55	4498	59
VA 560	4.50	0.10	6.937e-11	0.00	2.696e-12	1.015	5097	127	1.561e-12	1.030	5235	72	5.941e-13	1.021	5173	64	5180	80
VA 625	4.50	0.10	2.032e-10	0.00	5.859e-12	1.014	6035	157	2.949e-12	1.014	6118	83	1.000e-12	1.012	6093	75	6091	94
VA 682	4.50	0.10	9.660e-11	0.00	3.332e-12	1.015	5485	150	1.848e-12	1.023	5543	76	7.123e-13	1.018	5455	67	5494	86
VA 712	5.00	0.10	3.725e-11	0.00	2.098e-12	1.015	5082	139	1.263e-12	1.032	5147	71	4.860e-13	1.022	5072	63	5102	81
VA 747	5.00	0.10	4.262e-11	0.00	1.713e-12	1.014	4994	136	1.054e-12	1.038	5057	70	4.084e-13	1.023	4973	81	5009	79
VA 748	4.50	0.10	1.781e-10	0.00	5.616e-12	1.014	5760	134	2.536e-12	1.018	5817	79	1.104e-13	1.013	5805	72	5816	91
VA 778	5.00	0.10	3.399e-11	0.00	2.100e-12	1.015	5095	135	1.240e-12	1.031	5193	72	4.770e-13	1.022	5115	63	5140	81
G084-050	4.50	-0.32	1.160e-12	0.00	1.283e-13	1.012	4483	89	8.627e-14	1.041	4895	110	3.494e-14	1.026	4705	60	4740	78
HR1536	4.50	0.13	1.307e-09	0.00	4.031e-11	1.014	5830	148	2.177e-11	1.018	5830	81	8.030e-12	1.015	5812	61	5822	85
HR1543	4.50	0.04	1.374e-08	0.00	3.341e-10	1.012	6541	162	—	—	—	—	6.234e-11	1.011	6404	80	6482	107
G1182	5.00	0.00	6.623e-11	0.00	4.091e-12	—	<3500	—	3.408e-12	—	<3500	—	1.227e-12	1.024	3639	136	(3639)	—
G084-029	4.50	-2.01	3.404e-11	0.00	8.901e-13	1.009	6094	107	4.718e-13	1.019	6099	76	1.704e-13	1.016	6141	78	6110	87
G096-020	4.50	-1.05	3.738e-11	0.00	9.760e-13	1.010	6168	126	5.028e-13	1.012	6208	78	1.798e-13	1.015	6268	58	6222	77
G084-037	4.50	-1.19	3.633e-11	0.02	1.055e-12	1.008	5830	83	5.747e-13	1.021	5840	53	2.079e-13	1.018	5886	62	5852	64
HR1729	4.50	0.00	3.509e-09	0.00	1.050e-10	1.013	5362	155	—	—	—	—	2.112e-11	1.016	5840	72	5817	98
G086-039	4.50	-1.61	8.291e-12	0.03	3.479e-13	1.009	4642	172	2.248e-13	1.038	4723	56	8.501e-14	1.021	4750	40	4739	47
G096-038	4.50	-0.03	5.281e-12	0.03	2.131e-13	1.014	4938	101	1.417e-13	1.039	4886	68	5.231e-14	1.025	4898	60	4892	64
G099-015	5.00	-1.50	7.424e-10	0.00	3.687e-11	1.011	5954	211	3.514e-11	—	<3500	—	1.242e-11	1.027	3737	123	(3737)	—
HR1925	4.00	-0.20	9.735e-10	0.00	2.717e-11	1.013	5110	95	2.163e-11	1.040	5287	47	8.282e-12	1.021	5172	40	5185	53
G102-020	4.50	-1.39	2.479e-11	0.02	8.779e-13	1.009	5221	120	5.150e-13	1.029	5267	125	1.927e-13	1.020	5269	89	5254	109
G191-051	5.00	0.00	7.424e-10	0.00	3.687e-11	1.012	6277	198	3.262e-11	1.054	[3619]	300	1.249e-11	1.032	3832	109	(3832)	—
HR1983	4.00	-0.16	9.574e-09	0.18	2.511e-10	1.012	6277	159	—	—	—	—	4.743e-11	1.014	6251	77	6260	104
LT2437	4.00	0.00	8.301e-09	0.00	1.701e-10	1.013	6101	157	1.308e-14	1.017	5917	80	4.963e-15	1.015	5834	72	5918	92
HR2083	4.00	-1.26	5.712e-11	0.00	1.978e-12	1.009	5289	176	1.158e-12	1.028	5328	92	4.323e-13	1.020	5320	86	5319	113
G103-054	4.50	-1.74	2.601e-11	0.03	8.856e-13	1.008	5375	136	5.129e-13	1.027	5336	68	1.938e-13	1.020	5359	60	5353	77
G102-047	4.50	0.00	5.579e-10	0.00	2.958e-11	1.012	5375	223	2.505e-13	1.038	[3626]	300	9.663e-12	1.019	5400	45	5376	—
G098-056	4.50	-1.32	4.465e-12	0.00	2.934e-13	1.009	5293	162	1.666e-13	1.027	5375	74	6.148e-14	1.019	5400	45	5376	—
G098-058	4.50	-1.86	9.307e-11	0.05	2.939e-12	1.008	5523	184	1.706e-12	1.026	5487	53	6.284e-13	1.019	5523	43	5510	56
G101-033	4.50	-0.37	2.452e-11	0.00	6.795e-13	1.012	5288	161	5.271e-13	1.029	5286	67	1.953e-13	1.020	5281	65	5284	82
G101-034	4.50	-1.83	2.030e-11	0.10	6.771e-13	1.008	5357	133	4.210e-13	1.028	5227	74	1.531e-13	1.020	5305	49	5280	72
HD45281	4.50	0.00	7.200e-11	0.00	2.385e-12	1.014	5187	153	1.247e-12	1.020	5739	79	4.563e-13	1.018	5738	72	5703	91
HR2324	5.00	-1.04	1.875e-10	0.00	6.783e-12	1.010	5187	75	4.116e-12	1.031	5190	72	1.531e-12	1.020	5198	43	5193	59
HR2324	4.00	0.00	1.138e-09	0.00	1.516e-11	1.002	8402	171	6.117e-12	0.997	8334	107	2.253e-12	0.995	8439	103	8464	120
G106-053	4.50	-0.36	3.172e-11	0.00	1.323e-12	1.012	4787	172	8.531e-13	1.039	4806	98	3.212e-13	1.024	4847	40	4855	47
HR2383	4.00	0.00	6.905e-10	0.00	8.216e-12	1.001	8764	171	3.258e-12	0.996	8913	110	1.210e-12	0.995	8786	107	8825	124
G105-049	5.00	-1.60	1.085e-10	0.00	5.952e-12	1.001	<3500	—	5.326e-12	—	<3500	—	1.972e-12	1.028	3586	142	(3586)	—
G103-050	4.50	-1.59	1.140e-11	0.01	4.658e-13	1.009	4747	118	2.903e-13	1.036	4841	69	1.112e-13	1.021	4834	52	4837	59
G103-050	5.00	-3.00	5.458e-12	0.03	2.389e-13	1.013	[4647]	205	1.562e-13	1.042	4778	161	6.189e-14	1.027	4669	108	4713	129
G192-043	4.50	-1.56	2.133e-11	0.00	5.721e-13	1.009	6041	183	2.983e-13	1.018	6093	101	1.697e-13	1.016	6099	85	6085	85
HR2550	4.50	-0.88	1.437e-09	0.03	3.196e-11	1.009	6685	130	1.176e-11	1.011	6673	88	5.757e-12	1.011	6681	82	6679	96
G110-021	5.00	-1.50	2.908e-11	0.00	1.432e-12	1.011	4009	206	1.176e-12	1.050	[2655]	300	4.176e-13	1.024	4026	81	(4026)	—
G088-010	4.50	-2.20	5.230e-12	0.00	1.477e-13	1.008	5487	108	7.972e-14	1.031	5876	80	2.993e-14	1.018	5851	54	5850	74

Table 4. continued

ID	log(g)	[Fe/H]	$F_{\text{Bol}}$	E(B-V)	$F_H$	$F_T$	$\Delta T_1$	$F_H$	$q_H$	$T_H$	$\Delta T_H$	$F_K$	$q_K$	$T_K$	$\Delta T_K$	$T_{\text{mean}}$	$\Delta T_{\text{mean}}$
G087-033	5.00	-1.50	6.77e-11	0.00	3.86e-12	1.011	[3500]	253	3.27e-12	1.033	<3500	1.245e-12	1.029	3570	144	3570	—
G107-063	5.00	0.00	6.27e-11	0.00	3.28e-12	1.012	3779	182	2.89e-12	1.031	[3661]	1.076e-12	1.034	3880	102	3880	—
G089-014	4.50	-1.85	1.99e-11	0.00	5.73e-12	1.008	5804	126	3.04e-13	1.021	5881	1.122e-12	1.018	5885	73	5881	75
G088-027	4.50	-2.21	1.46e-11	0.00	3.99e-13	1.008	5848	162	2.09e-13	1.020	6030	1.723e-14	1.017	6030	84	6015	87
HR2852	4.00	-0.31	5.51e-09	0.00	1.113e-10	1.009	7080	186	—	—	—	1.969e-11	1.009	6989	86	7020	113
G080-003	4.50	-1.89	2.20e-11	0.04	6.41e-13	1.008	5762	199	3.53e-13	1.022	—	1.287e-13	1.018	5813	108	5786	132
G088-032	4.50	-2.59	1.36e-11	0.00	3.43e-13	1.008	6191	86	1.80e-13	1.017	5770	6.583e-14	1.012	6222	65	6208	67
HR2883	4.50	-0.89	1.21e-09	0.00	9.47e-11	1.010	5909	186	1.84e-11	1.019	5937	9.838e-12	1.018	5750	71	5928	101
G088-041	4.00	-0.08	3.12e-10	0.00	9.70e-12	1.013	5776	154	5.20e-12	1.019	5818	1.973e-12	1.016	5750	71	5781	90
G087-047	4.50	-0.88	2.22e-11	0.00	8.17e-13	1.010	5150	262	4.91e-13	1.031	5192	8.183e-13	1.020	5104	72	5188	100
W5058	4.50	-1.15	1.06e-11	0.00	3.643e-13	1.009	5349	118	2.07e-13	1.027	5411	7.703e-14	1.019	5420	67	5400	81
HR2843	4.43	-0.05	1.84e-07	0.00	4.40e-09	1.011	6085	162	2.16e-09	1.009	6579	7.908e-10	1.010	6576	81	6579	100
G112-036	4.50	-0.88	7.53e-11	0.06	2.812e-12	1.010	5103	245	1.782e-12	1.034	5065	6.362e-10	1.021	5090	49	5082	72
G112-038	5.00	-1.50	1.567e-10	0.00	8.307e-12	1.011	[3602]	245	7.86e-12	1.034	<3500	2.569e-12	1.026	3772	118	(3772)	—
G112-043	4.50	-1.61	2.40e-11	0.01	6.448e-13	1.009	6023	110	3.37e-13	1.018	6085	1.252e-12	1.017	6069	66	6065	83
G091-011	5.00	0.00	2.76e-11	0.00	1.620e-12	1.007	3920	—	1.196e-12	1.067	3926	4.708e-13	1.034	3907	84	(3907)	—
HR3029	4.00	0.00	2.09e-10	0.00	3.769e-12	1.007	7491	168	1.764e-12	1.067	7382	6.477e-13	1.003	7348	91	7392	110
HR3064	4.50	0.00	2.32e-09	0.00	7.342e-11	1.014	5738	153	4.001e-11	1.020	5740	1.492e-11	1.017	5711	70	5727	89
G090-025	4.50	-1.82	1.493e-10	0.00	4.831e-12	1.008	5422	101	2.771e-12	1.025	5448	1.049e-12	1.020	5443	69	5441	68
G090-026	4.50	-1.61	2.518e-12	0.00	8.603e-14	1.009	5306	206	4.972e-14	1.037	5341	1.828e-14	1.020	5385	105	5353	142
G112-084	4.50	-0.65	3.291e-10	0.00	1.229e-11	1.011	5118	122	7.449e-12	1.032	5161	2.836e-12	1.021	5117	71	5134	83
HD65583	4.50	-0.60	4.745e-10	0.00	1.720e-11	1.011	5226	79	1.028e-11	1.030	5251	4.930e-12	1.020	5244	55	5242	59
HD68017	4.00	-0.42	5.373e-10	0.00	1.797e-11	1.011	5503	150	1.011e-11	1.024	5547	3.843e-12	1.018	5485	68	5512	87
G194-072	4.50	-1.84	3.33e-11	0.00	9.987e-13	1.009	5877	170	5.195e-13	1.020	5985	1.290e-12	1.017	6004	102	5967	122
HR3176	4.00	0.14	2.038e-11	0.00	6.436e-13	1.014	5762	153	3.425e-13	1.019	5797	1.272e-11	1.016	5775	71	5781	90
G231-034	5.00	-1.73	2.841e-11	0.00	9.877e-13	1.009	5235	80	8.660e-13	1.027	5209	2.111e-13	1.020	5230	74	5208	82
HR3262	4.00	-0.50	2.351e-09	0.00	6.196e-11	1.011	6216	86	3.170e-11	1.014	6245	1.114e-11	1.014	6285	52	6242	70
HD70668	4.50	-0.04	4.004e-11	0.03	1.821e-12	1.013	4560	186	1.311e-12	1.059	4569	4.827e-13	1.028	4587	57	4579	60
G113-040	4.50	-1.13	6.196e-10	0.04	2.960e-11	1.011	[4776]	139	2.007e-11	1.014	4282	7.407e-12	1.013	4273	77	4275	96
HR3427	4.00	0.00	5.794e-10	0.00	7.123e-12	1.011	5857	171	1.872e-12	1.049	4761	1.231e-12	1.022	4722	53	4740	62
G009-014	4.50	-0.76	2.657e-11	0.00	1.003e-12	1.011	5071	127	2.860e-12	0.996	5863	1.021e-12	0.995	5712	107	5763	123
HD74000	4.50	-2.00	3.966e-11	0.00	9.896e-13	1.008	6231	159	5.199e-13	1.031	5046	2.363e-13	1.021	5063	75	5059	91
G009-018	4.50	-1.31	5.078e-11	0.00	1.082e-12	1.008	4883	174	3.356e-13	1.017	6236	1.924e-13	1.011	6209	77	6224	96
G046-005	4.50	-1.70	9.626e-12	0.00	3.755e-13	1.009	4982	96	2.356e-13	1.033	4938	1.937e-13	1.011	6776	67	6776	84
HR3578	4.50	-1.05	1.328e-11	0.00	4.300e-13	1.010	5363	96	2.405e-13	1.024	5361	8.715e-14	1.020	4964	84	4950	61
G114-026	4.50	-1.18	4.757e-12	0.00	3.950e-13	1.009	5663	100	2.138e-13	1.022	5735	7.823e-12	1.018	5572	45	5569	67
G115-049	4.50	-1.47	3.824e-11	0.00	1.157e-12	1.009	5971	187	6.270e-14	1.024	5943	3.076e-14	1.019	5636	97	5625	120
G047-026	4.50	-1.86	6.573e-12	0.00	1.792e-13	1.009	5768	83	6.270e-14	1.022	5805	2.292e-13	1.018	5836	49	5809	86
G116-058	4.50	-1.50	7.438e-11	0.00	4.360e-12	1.009	5967	106	9.852e-14	1.021	5926	3.597e-14	1.017	5958	50	5950	72
G046-031	4.50	-1.65	3.972e-12	0.00	9.700e-14	1.009	6303	255	5.314e-14	1.017	<3500	1.364e-12	1.029	3573	144	(3573)	—
HD80218	4.50	-0.79	1.265e-11	0.00	3.643e-13	1.010	5897	143	2.012e-13	1.020	6195	1.880e-14	1.015	6278	114	6267	160
G041-034	4.50	0.00	5.927e-10	0.00	1.659e-12	1.012	6046	157	8.517e-12	1.016	5853	7.388e-14	1.017	5864	92	5866	93
HR3750	4.00	-0.31	1.964e-09	0.00	1.554e-12	1.014	5180	144	9.118e-13	1.029	5237	3.438e-13	1.022	5182	54	5215	65
HR3775	4.00	-0.01	1.410e-08	0.00	6.419e-11	1.012	6287	82	3.553e-11	1.023	5632	1.324e-11	1.017	5604	59	5611	62
G041-041	5.00	-2.89	1.016e-11	0.00	2.593e-10	1.012	6287	176	1.846e-10	1.011	6339	5.55e-11	1.011	6306	97	6338	88
G193-034	4.50	-2.81	1.894e-11	0.00	1.491e-13	1.008	6328	137	1.289e-13	1.016	6282	4.850e-14	1.015	6371	69	6338	89
G048-029	4.50	-2.81	1.894e-11	0.00	4.671e-13	1.008	6340	240	8.304e-14	1.021	5908	2.292e-13	1.018	6067	103	5966	93
HR3769	4.00	-2.66	2.444e-11	0.01	5.463e-13	1.008	6584	130	2.277e-13	1.016	6317	5.784e-14	1.015	6371	94	6313	80
G045-003	4.50	-2.49	1.363e-10	0.00	3.253e-12	1.008	6355	144	1.719e-12	1.016	6312	8.943e-14	1.013	6335	68	6330	83
BP +44 1910	4.50	-2.97	1.271e-11	0.00	3.247e-13	1.008	6053	157	1.733e-13	1.018	6061	5.265e-14	1.017	6170	75	6063	94
HR286	4.50	-2.97	1.271e-11	0.00	3.247e-13	1.008	6131	110	1.694e-13	1.018	6174	8.474e-14	1.017	6158	74	6158	74
G048-029	4.50	-0.60	2.598e-12	0.00	8.779e-12	1.011	5339	80	4.923e-12	1.025	5300	7.673e-12	1.019	5433	45	5465	63
G161-082	4.50	-1.38	4.747e-12	0.00	1.609e-12	1.009	5248	183	9.218e-14	1.027	5295	2.435e-12	1.020	5241	42	5289	111
HR3740	4.50	-1.68	9.100e-11	0.03	3.161e-12	1.009	5259	108	1.526e-11	1.029	5198	7.133e-13	1.020	5241	42	5289	111
G198-009	5.00	-1.00	1.376e-09	0.00	7.576e-11	1.009	<3500	—	6.458e-11	—	<3500	1.233e-12	1.020	3637	136	(3637)	—
G1378-2	5.00	-1.00	6.944e-11	0.00	4.091e-12	1.009	<3500	—	4.425e-12	—	<3500	1.444e-12	1.020	3580	143	(3580)	—
G1383	5.00	-1.00	7.859e-11	0.00	4.776e-12	1.009	<3500	—	3.777e-12	—	<3500	1.444e-12	1.020	3580	143	(3580)	—

Table 4. continued

ID	log(g)	[Fe/H]	$F_{\text{H}\alpha}$	E(B-V)	$F_T$	$q_1$	$T_F$	$\Delta T$	$F_H$	$q_H$	$T_H$	$\Delta T_H$	$F_K$	$q_K$	$T_K$	$\Delta T_K$	$T_{\text{mean}}$	$\Delta T_{\text{mean}}$
G044-006	4.30	-0.78	2.275e-10	0.00	7.103e-12	1.010	5658	100	3.964e-12	1.023	5684	48	1.453e-12	1.018	5683	70	5683	86
HR4030	4.00	-0.03	1.108e-09	0.00	3.643e-11	1.012	5602	151	1.984e-11	1.022	5654	77	6.004e-12	1.016	5769	71	5692	89
HR4039	4.50	-0.19	1.256e-09	0.00	3.596e-11	1.016	6008	150	1.877e-11	1.016	6028	81	6.891e-12	1.014	6033	74	6020	73
G055-017	4.50	-1.48	1.590e-12	0.00	5.314e-14	1.009	5317	118	3.233e-14	1.028	5297	73	1.199e-14	1.020	5320	66	5325	80
G053-041	4.50	-1.39	1.089e-11	0.00	3.167e-13	1.009	5808	139	1.036e-13	1.021	5860	68	6.328e-14	1.018	5845	65	5844	40
HR4098	4.00	-0.23	3.005e-10	0.00	2.298e-11	1.012	5737	137	1.262e-11	1.021	5727	59	4.725e-12	1.019	5693	58	5715	72
G162-068	4.50	-0.81	1.868e-11	0.00	6.419e-13	1.010	5361	80	3.763e-13	1.028	5370	80	1.396e-13	1.019	5371	45	5368	55
G044-030	4.50	-1.02	8.947e-12	0.00	3.135e-13	1.010	5285	103	6.969e-12	1.023	5341	59	6.729e-14	1.019	5349	45	5334	61
G1400-AB	5.00	-1.50	1.441e-10	0.00	8.461e-12	1.008	5810	139	3.636e-13	1.022	5804	89	2.647e-12	1.029	5870	144	(3570)	—
G119-032	4.50	-1.86	2.297e-11	0.00	6.592e-13	1.009	5412	139	5.924e-13	1.027	5423	58	1.300e-13	1.018	5405	149	5415	119
G058-023	4.50	-1.04	3.046e-11	0.00	1.022e-12	1.009	5412	95	5.924e-13	1.027	5423	58	2.222e-13	1.019	5405	149	5415	64
G196-047	4.50	-1.64	2.752e-12	0.00	8.338e-14	1.009	5659	137	5.118e-14	1.026	5465	119	2.008e-14	1.020	5378	91	5481	112
G058-025	4.50	-1.50	1.438e-10	0.00	3.911e-12	1.009	6008	181	2.132e-12	1.020	5999	117	7.672e-13	1.017	6027	113	6001	131
G055-044	4.50	-0.23	4.919e-11	0.00	2.396e-12	1.011	[4181]	157	1.704e-12	1.037	4367	69	6.591e-13	1.029	4373	66	4370	67
G1410	5.00	-1.00	1.275e-10	0.00	8.838e-12	1.011	[3582]	246	6.005e-12	1.036	3582	300	2.267e-12	1.030	3634	136	(4634)	—
G119-052	5.00	-0.20	1.173e-09	0.00	6.598e-11	1.012	[3544]	195	5.237e-11	1.036	[3525]	300	1.975e-11	1.032	3828	91	(3828)	—
G178-011	5.00	-1.50	3.202e-10	0.00	1.752e-11	1.012	[3500]	—	1.440e-11	—	[3500]	—	5.471e-12	1.027	3696	128	(3696)	—
G119-059	5.00	-1.50	1.320e-10	0.00	6.592e-12	1.011	[3939]	213	5.785e-12	1.035	[3907]	300	2.158e-12	1.026	3743	116	(3743)	—
G010-004	4.50	-2.30	1.026e-11	0.06	3.563e-12	1.008	5174	84	2.151e-13	1.028	5174	57	8.027e-14	1.020	5202	42	5192	56
G056-022	4.30	-0.89	1.278e-12	0.00	5.293e-14	1.010	4691	250	3.296e-14	1.039	4844	63	1.391e-14	1.023	4700	73	4777	88
G119-064	4.30	-1.71	3.507e-11	0.00	8.923e-13	1.009	6388	108	4.698e-12	1.017	6193	71	1.894e-13	1.016	6238	92	6206	88
G1421A	5.00	-1.50	3.965e-11	0.00	3.250e-12	1.010	[3500]	—	2.696e-12	—	[3500]	—	1.005e-12	1.026	3806	113	(3806)	—
G1421B	5.00	-1.50	5.931e-11	0.00	3.403e-12	1.010	[3500]	—	2.859e-12	—	[3500]	—	1.005e-12	1.026	3806	113	(3806)	—
HD77916	4.00	-1.22	5.715e-11	0.00	1.396e-12	1.010	6388	208	7.087e-13	1.015	6388	135	2.556e-13	1.015	6416	139	6393	155
G147-038	4.00	-0.14	5.240e-11	0.00	1.712e-12	1.014	5657	422	9.286e-13	1.020	5653	172	3.513e-13	1.017	5633	142	5659	73
G197-008	4.00	-0.39	4.003e-12	0.00	1.248e-13	1.012	5711	202	7.162e-14	1.023	5653	132	2.646e-12	1.023	5678	144	5678	144
G256-065	5.00	-1.50	1.448e-10	0.00	8.619e-12	1.011	[3456]	227	6.813e-12	—	<3500	—	2.646e-12	1.017	5938	70	5938	93
G056-036	4.50	-1.03	2.780e-11	0.00	7.948e-13	1.010	5993	127	4.289e-13	1.020	5913	90	1.536e-13	1.017	5938	70	5938	93
HR4421	4.50	-0.81	1.231e-09	0.00	2.841e-11	1.009	6606	120	1.397e-11	1.010	6633	81	5.045e-12	1.019	6650	62	6634	82
HD101177	4.00	-0.13	7.558e-10	0.00	2.479e-11	1.013	5599	151	1.485e-11	1.025	5486	75	6.618e-12	1.019	5428	67	5463	86
HR4498	4.50	-0.14	2.099e-09	0.00	7.696e-12	1.013	5256	146	—	—	—	—	1.592e-12	1.020	5362	66	5342	91
HR4501	4.50	-0.82	1.381e-09	0.00	3.576e-11	1.010	6225	127	1.825e-11	1.043	6268	84	6.618e-12	1.014	6290	78	6266	92
G121-012	4.50	-1.17	1.966e-11	0.00	5.538e-13	1.009	5926	109	2.938e-13	1.019	5966	50	1.084e-13	1.017	5970	120	5957	80
HR4533	4.00	0.12	9.014e-10	0.00	2.385e-11	1.013	6300	96	1.195e-11	1.011	6319	55	4.883e-12	1.011	6309	51	6311	62
G176-053	4.50	-1.54	3.136e-11	0.00	9.877e-13	1.009	5556	130	5.096e-13	1.024	5590	57	2.039e-13	1.019	5607	45	5593	64
HR4540	4.00	0.21	9.419e-09	0.00	2.098e-10	1.014	6074	116	1.373e-10	1.014	6115	68	5.076e-11	1.012	6088	70	6095	80
HD103095	4.50	-1.35	8.381e-10	0.00	3.182e-11	1.009	5009	91	1.976e-11	1.038	5040	65	7.413e-12	1.021	5031	50	5029	65
G122-066	4.00	0.00	5.406e-10	0.00	2.919e-11	1.010	[3794]	227	1.976e-11	1.038	4358	63	7.282e-12	1.032	4380	54	4370	58
HD104636	4.00	0.00	1.473e-10	0.00	2.680e-12	1.010	7103	166	1.441e-12	1.007	7008	92	5.309e-13	1.008	6982	86	7019	105
HD104674	4.00	0.00	9.870e-11	0.00	5.270e-12	1.010	[3830]	223	3.415e-12	1.034	4452	64	1.287e-12	1.032	4454	55	4442	59
HR4623	4.00	-0.60	6.467e-09	0.00	1.326e-12	1.008	6903	86	6.286e-11	1.006	7009	62	2.260e-11	1.006	7009	58	7003	67
HD105601	4.00	0.00	9.041e-10	0.00	5.403e-10	1.006	7505	163	2.451e-12	1.001	7487	97	8.785e-13	1.009	7481	92	7481	111
HD105755	4.00	-1.08	1.040e-10	0.00	3.072e-12	1.010	5795	126	1.673e-12	1.022	5807	53	6.196e-13	1.018	5809	48	5806	63
G011-044	4.50	-1.80	1.011e-11	0.00	2.788e-13	1.008	5933	174	1.514e-13	1.020	5925	98	5.521e-14	1.017	5974	45	5943	108
G012-021	4.50	-1.40	2.429e-11	0.00	6.738e-13	1.009	5931	84	3.609e-12	1.020	5966	69	1.330e-13	1.017	5974	50	5960	65
G197-049	5.00	-1.50	8.821e-11	0.00	5.141e-12	1.010	[3500]	—	4.308e-12	—	<3500	—	1.626e-12	1.029	3565	143	(3565)	—
HR4657	4.50	-0.78	9.749e-10	0.00	2.551e-11	1.010	6196	127	1.328e-11	1.016	6209	63	4.837e-12	1.014	6215	77	6208	82
G012-023	4.50	-1.13	1.300e-12	0.00	4.340e-14	1.009	5420	238	2.515e-14	1.027	5427	205	8.807e-13	1.019	5526	176	5463	203
HD106965	4.00	0.00	1.750e-10	0.00	3.325e-12	1.009	7305	167	1.413e-12	1.001	7462	97	5.019e-12	1.010	7431	92	7441	110
HR4688	4.00	0.38	7.545e-10	0.00	1.969e-11	1.015	6380	119	9.922e-12	1.010	6341	64	6.654e-12	1.010	6327	59	6343	73
HD107906	4.00	0.00	8.515e-11	0.00	2.391e-12	1.011	[4019]	205	1.811e-12	1.047	4036	66	6.676e-13	1.029	4051	57	4044	61
HR4689	4.00	0.11	7.021e-09	0.00	9.007e-11	0.993	8961	137	3.574e-11	0.987	8759	109	1.270e-11	0.981	8687	106	8690	116
G337-062	4.00	-0.39	1.862e-10	0.01	6.520e-12	1.012	5365	148	3.877e-12	1.028	5347	74	1.478e-12	1.020	5289	65	5323	84
G059-018	4.50	-1.16	2.949e-11	0.05	1.011e-12	1.009	5381	212	6.102e-13	1.029	5283	113	2.285e-13	1.020	5287	129	5299	141
HD107906	4.00	0.00	7.956e-11	0.00	3.016e-12	1.014	5186	74	1.770e-12	1.029	5234	49	6.639e-13	1.023	5207	43	5205	52
G013-025	4.50	-1.98	3.875e-11	0.00	1.008e-12	1.008	6698	157	5.318e-13	1.018	6082	82	1.975e-13	1.017	6101	75	6097	94
G012-043	4.50	-0.50	7.260e-11	0.00	2.448e-12	1.011	5337	147	1.489e-12	1.028	5366	74	5.665e-13	1.020	5313	66	5338	85
HR4785	4.50	-0.25	5.319e-09	0.00	1.550e-10	1.012	5938	156	—	—	—	—	3.196e-12	1.020	5855	72	5867	99
G012-039	5.00	-1.50	1.002e-10	0.00	5.689e-12	1.008	[3500]	—	4.814e-12	—	<3500	—	1.832e-12	1.029	3576	144	(3576)	—
G059-024	4.50	-2.69	4.653e-12	0.00	1.195e-13	1.008	6111	192	6.424e-14	1.019	6091	53	2.321e-14	1.017	6133	83	6108	83



Table 4. continued

ID	$\log(g)$	$Fe/H$	$F_{Bul}$	$E(B-V)$	$F_I$	$q_I$	$T_I$	$\Delta T_I$	$F_H$	$q_H$	$T_H$	$\Delta T_H$	$F_K$	$q_K$	$T_K$	$\Delta T_K$	$T_{mean}$	$\Delta T_{mean}$
G059-027	4.50	-2.34	1.255e-11	0.00	3.232e-13	1.008	6115	180	1.718e-13	1.018	6117	105	6.303e-14	1.017	6092	117	6107	127
G060-026	4.50	-1.24	3.568e-11	0.00	1.243e-12	1.009	5281	176	7.432e-13	1.029	5274	105	2.780e-13	1.020	5273	42	5275	52
G237-072	4.50	-0.97	5.414e-11	0.00	1.687e-12	1.010	5648	152	9.482e-13	1.022	5643	77	3.502e-13	1.018	5651	70	5647	89
G014-006	4.50	0.10	2.599e-11	0.00	1.505e-11	1.013	[3529]	175	1.322e-11	—	<3500	—	4.626e-12	1.035	5648	121	(3748)	—
HD111980	4.00	-1.12	1.273e-11	0.02	8.987e-12	1.009	5611	148	2.226e-12	1.024	5628	67	8.287e-13	1.018	5625	40	5624	71
G060-048	4.50	-1.92	8.448e-12	0.00	2.452e-12	1.008	5777	92	1.378e-13	1.021	5794	51	4.933e-14	1.018	5815	99	5795	59
HD112758	4.50	-0.29	2.994e-10	0.00	1.134e-11	1.013	5118	119	6.969e-12	1.022	5136	62	2.629e-12	1.022	5103	39	5116	59
G060-057	4.50	0.00	1.520e-12	0.00	7.562e-12	1.012	[4054]	199	6.429e-12	1.054	[3723]	300	2.515e-12	1.032	3870	104	(3870)	—
G014-022	4.50	0.06	7.247e-11	0.00	2.579e-12	1.014	5372	140	8.457e-13	1.025	5436	49	5.429e-13	1.019	5414	50	5413	57
G014-024	4.50	-2.62	2.418e-12	0.01	9.176e-14	1.008	4922	137	5.552e-14	1.030	4941	71	2.063e-14	1.020	5029	64	4974	81
G060-066	4.50	-0.17	2.814e-11	0.00	1.286e-12	1.013	5490	100	7.571e-13	1.024	5511	57	2.731e-13	1.018	5495	63	5500	67
G014-022	4.50	-1.58	1.660e-10	0.00	6.802e-12	1.009	[4730]	124	4.874e-12	1.040	4513	63	1.850e-12	1.021	4596	56	4541	59
G063-005	4.50	-0.34	9.037e-11	0.00	2.861e-12	1.012	5637	179	1.647e-12	1.023	5605	78	6.221e-13	1.018	5558	69	5590	91
G063-006	4.50	0.00	7.138e-12	0.00	2.911e-13	1.012	[3719]	154	3.490e-13	—	<3500	—	1.218e-13	1.034	3900	75	(3900)	—
G061-038	4.50	-0.70	3.204e-11	0.00	1.084e-12	1.010	5804	244	5.080e-13	1.035	5528	148	2.231e-13	1.019	5512	129	5516	161
HR4983	4.50	0.10	3.345e-09	0.00	1.355e-10	1.014	5844	156	8.111e-11	1.016	5877	81	2.897e-11	1.014	5892	74	5864	93
G063-009	4.50	-0.80	3.356e-10	0.00	9.760e-12	1.010	5867	124	5.246e-12	1.020	5884	52	1.851e-12	1.017	5891	53	5884	66
G014-039	4.50	-2.06	2.633e-12	0.00	1.110e-13	1.009	[4595]	101	6.626e-13	1.039	5429	41	2.807e-13	1.021	4360	87	4498	71
G014-045	4.50	-0.22	1.855e-11	0.00	8.579e-13	1.012	[4411]	133	6.206e-13	1.052	4500	75	2.696e-13	1.028	4462	50	5841	70
G062-030	4.50	-0.75	3.606e-11	0.00	1.252e-12	1.011	5533	100	7.408e-13	1.023	5549	76	1.254e-12	1.020	5349	68	5504	79
G164-067	4.50	0.00	1.748e-10	0.00	6.046e-12	1.014	5432	101	3.314e-12	1.023	5459	55	2.042e-14	1.018	5978	63	5970	74
G063-026	4.50	-1.70	3.754e-12	0.00	1.051e-13	1.009	5900	149	5.489e-14	1.020	5988	122	1.108e-14	1.034	4961	108	4994	134
G063-040	4.50	-2.05	1.242e-12	0.00	4.400e-14	1.008	5163	205	2.942e-14	1.032	4928	52	1.904e-12	1.017	5673	47	5882	60
G014-054	4.50	0.12	2.899e-10	0.00	9.407e-12	1.014	5672	103	5.128e-12	1.020	5697	100	1.410e-12	1.032	4199	47	4179	64
HD118100	4.50	-0.07	9.545e-11	0.00	5.029e-12	1.012	[3856]	221	3.834e-12	1.065	4138	49	1.104e-13	1.020	5187	54	5209	63
G062-052	4.50	-1.16	1.351e-11	0.00	4.780e-13	1.009	5243	120	2.913e-13	1.030	<3500	—	2.768e-12	1.028	3658	133	(3658)	—
G165-019	4.50	-1.50	1.588e-10	0.00	8.860e-12	1.009	5510	123	9.599e-14	1.015	6418	77	3.401e-14	1.014	6480	74	6468	87
G064-012	4.50	-3.35	7.998e-12	0.02	1.806e-13	1.009	5682	79	8.552e-13	1.022	5706	52	3.140e-13	1.018	5721	56	5705	60
G063-046	4.50	-0.08	1.359e-10	0.00	1.551e-12	1.010	5682	79	8.552e-13	1.022	5706	52	3.140e-13	1.018	5721	56	5705	60
G062-061	4.50	-0.10	6.926e-11	0.00	4.076e-12	1.013	5968	134	2.329e-12	1.018	5900	88	8.829e-13	1.015	5881	69	5898	82
G062-062	4.50	-1.50	6.926e-11	0.00	3.566e-12	1.011	[3753]	231	3.135e-12	—	<3500	—	1.070e-12	1.025	3878	103	(3878)	—
G165-039	4.50	-2.41	2.726e-11	0.00	6.721e-13	1.009	6259	92	3.300e-13	1.010	6273	37	2.266e-13	1.015	6316	80	6282	72
G064-022	4.50	-1.75	7.656e-12	0.00	2.902e-13	1.009	[4981]	113	1.801e-13	1.032	4862	56	6.935e-14	1.020	4959	63	4971	62
HD128710	4.50	-2.51	1.047e-11	0.01	2.413e-12	1.009	6469	113	1.250e-13	1.015	6439	56	4.634e-14	1.015	6404	63	6432	70
W8296	4.50	-1.32	1.479e-10	0.00	4.400e-12	1.009	5766	153	2.429e-12	1.022	5754	78	8.877e-13	1.018	5786	71	5768	90
G166-022	4.50	-1.65	1.590e-11	0.00	5.203e-13	1.009	5483	77	2.937e-13	1.026	5479	49	1.117e-12	1.019	5452	44	5457	53
G135-042	4.00	-0.36	1.851e-11	0.00	9.546e-12	1.011	[3970]	210	8.064e-12	1.032	[3582]	300	2.837e-12	1.024	3972	89	(3972)	—
G165-047	4.00	-0.29	8.617e-10	0.00	9.191e-13	1.012	5634	91	3.322e-13	1.023	5663	52	1.262e-13	1.018	5575	45	5608	59
G166-027	4.00	-0.38	8.617e-10	0.00	2.776e-11	1.012	5634	124	1.837e-11	1.022	5663	52	5.725e-12	1.017	5634	59	5646	68
G166-028	4.50	-1.50	8.692e-11	0.00	5.483e-12	1.011	<3500	232	4.382e-12	—	<3500	—	1.786e-12	1.028	2383	143	(2383)	—
G166-028	4.50	-1.50	8.692e-11	0.00	5.483e-12	1.011	<3500	232	4.382e-12	—	<3500	—	1.786e-12	1.028	2383	143	(2383)	—
HD128681	4.50	-1.98	5.624e-11	0.00	1.776e-12	1.008	5516	102	9.960e-13	1.025	5546	51	3.758e-13	1.019	5547	46	5541	59
G178-030(3)	4.50	0.00	1.377e-12	0.00	6.389e-14	1.012	[4454]	168	3.612e-14	1.037	4831	83	1.510e-14	1.027	4730	74	4825	78
HR5447	4.00	-0.51	4.328e-09	0.00	9.644e-11	1.009	6728	163	4.824e-11	1.010	6679	88	1.722e-11	1.009	6722	83	6707	102
HR5455	4.00	-0.29	8.736e-10	0.00	2.252e-11	1.011	6311	144	1.129e-11	1.013	6351	89	4.088e-12	1.012	6369	83	6349	99
G201-005	4.50	-2.64	7.370e-12	0.00	1.763e-13	1.008	6343	102	9.249e-14	1.016	6320	97	3.387e-14	1.016	6319	144	6328	111
G066-018	4.50	-0.35	2.088e-12	0.00	6.670e-14	1.011	[4382]	142	6.473e-14	1.048	4617	67	2.352e-14	1.026	4666	79	4639	73
HD128659	4.50	-0.88	6.484e-11	0.05	1.887e-12	1.010	5854	411	1.078e-12	1.022	5762	94	4.028e-13	1.018	5737	122	5763	141
G178-041	4.50	-2.64	2.579e-12	0.00	7.169e-14	1.008	5868	84	3.906e-14	1.022	5884	54	1.508e-14	1.018	5799	107	5859	75
HD129653	4.00	0.00	3.032e-10	0.00	4.684e-12	1.008	7940	170	1.987e-12	1.022	7993	102	7.135e-13	1.021	7979	98	7977	116
G066-022	4.50	-1.11	2.944e-11	0.00	7.752e-13	1.010	5030	135	4.648e-13	1.032	5113	110	1.701e-12	1.027	5085	78	5071	102
G166-045	4.50	-1.00	6.899e-11	0.00	2.583e-12	1.012	[3796]	226	3.686e-12	—	<3500	—	1.931e-13	1.017	3888	101	(3888)	—
G166-045	4.50	-2.33	8.726e-11	0.01	9.941e-13	1.008	6012	108	5.293e-13	1.019	6034	55	1.931e-13	1.017	6058	75	6037	73
G066-030	4.50	-1.30	1.077e-11	0.01	2.768e-13	1.009	6132	126	1.536e-13	1.016	6261	126	5.238e-14	1.016	6211	77	6211	107
HR5534	4.00	0.20	1.204e-09	0.00	3.479e-11	1.014	6044	85	1.826e-11	1.015	6025	69	7.700e-12	1.013	5985	63	6019	71
G151-010	4.50	-0.50	4.609e-11	0.00	1.065e-12	1.012	5249	219	9.375e-13	1.017	5288	111	2.657e-13	1.020	5280	78	5311	114
G200-062	4.50	-0.56	2.352e-10	0.00	8.950e-12	1.012	5067	107	5.441e-12	1.033	5127	71	2.051e-12	1.022	5092	47	5098	67
HR5588	4.50	0.01	1.970e-09	0.00	8.942e-11	1.047	[4522]	63	6.089e-11	1.047	4540	49	2.394e-11	1.027	4577	38	4505	43
HD132476	4.50	-1.53	1.190e-10	0.03	3.393e-12	1.009	5854	127	1.136e-12	1.023	5767	66	7.136e-13	1.018	5779	44	5788	68
G167-011(4)	4.50	-0.14	5.024e-13	0.00	1.826e-14	1.013	(5277)	—	1.626e-14	1.050	4561	63	5.568e-15	1.026	4707	58	4837	60

Table 4. continued

ID	log(g)	[Fe/H]	$F_{\text{bol}}$	$E(B-V)$	$F_U$	$q_U$	$T_U$	$\Delta T_U$	$F_H$	$q_H$	$T_H$	$\Delta T_H$	$F_K$	$q_K$	$T_K$	$\Delta T_K$	$T_{\text{mean}}$	$\Delta T_{\text{mean}}$
HR6634	4.00	0.05	2.75e-09	0.00	6.617e-11	1.012	6554	130	3.267e-11	1.009	6570	87	1.191e-11	1.008	6565	81	6571	95
HD134169	4.00	-1.15	2.380e-10	0.00	6.771e-12	1.010	5896	81	3.735e-12	1.022	5856	81	1.983e-12	1.018	5826	92	5870	84
HD134439	4.50	-1.52	7.690e-11	0.00	2.894e-12	1.009	4932	88	1.785e-12	1.033	4964	59	6.825e-13	1.020	4967	41	4974	48
HD134440	4.50	-1.57	5.600e-11	0.00	2.313e-12	1.009	4749	102	1.515e-12	1.038	4748	42	5.871e-13	1.021	4732	50	4746	40
G015-013	4.50	-1.88	4.471e-12	0.07	1.533e-13	1.008	5279	108	9.339e-14	1.028	5206	111	3.481e-14	1.020	5245	95	5244	104
LT76079	4.50	-1.89	8.181e-12	0.00	2.520e-13	1.008	5594	121	1.410e-13	1.024	5614	77	5.087e-14	1.019	5687	70	5639	84
G015-023	4.50	-1.42	1.276e-11	0.00	4.607e-13	1.009	5152	117	2.755e-13	1.030	5184	46	1.040e-14	1.020	5176	65	5175	62
G015-024	4.50	-1.44	1.769e-12	0.00	2.413e-13	1.009	5604	106	1.305e-13	1.024	5618	48	5.641e-14	1.019	5616	52	5614	87
G152-035	4.00	0.01	6.049e-10	0.00	1.347e-11	1.010	6840	131	6.365e-12	1.005	6848	90	2.327e-12	1.006	6829	84	6831	98
G152-035	4.00	0.00	4.087e-12	0.00	1.394e-13	1.014	5502	90	1.398e-14	1.024	5499	60	2.915e-11	1.019	5478	51	5491	63
HR5830	4.00	-0.13	1.297e-09	0.00	2.815e-11	1.010	6802	118	1.328e-11	1.007	6785	101	5.110e-12	1.008	6768	85	6782	88
HD140283	4.00	-2.37	3.359e-10	0.00	1.141e-11	1.008	5638	146	6.454e-12	1.025	5676	66	2.679e-12	1.015	5689	47	5691	69
HR5868	4.50	0.05	4.514e-09	0.00	1.346e-10	1.014	5913	155	—	—	—	—	2.679e-12	1.015	5889	73	5897	99
G016-013	4.00	-0.86	2.880e-11	0.00	9.573e-13	1.016	5451	118	5.331e-13	1.025	5520	37	1.981e-13	1.019	5526	94	5507	98
HR5901	4.00	0.00	4.061e-09	0.00	1.704e-10	1.014	4810	114	1.115e-10	1.040	4842	68	4.287e-11	1.028	4785	59	4811	63
HR5914	4.00	-0.37	3.900e-09	0.00	1.197e-10	1.012	5769	114	6.530e-11	1.020	5789	69	2.430e-11	1.017	5761	76	5774	82
HR5933	4.00	-0.32	7.590e-09	0.00	2.013e-10	1.012	6221	159	—	—	—	—	3.707e-11	1.014	6238	77	6233	104
G240-023	4.50	-2.78	1.840e-12	0.03	5.052e-14	1.008	5364	177	2.666e-14	1.025	5579	71	1.051e-14	1.020	5479	73	5502	90
G240-002	4.50	-0.78	3.597e-10	0.00	1.155e-11	1.010	5576	151	6.616e-12	1.024	5560	76	2.470e-12	1.018	5541	68	5555	87
HR5968	4.00	-0.17	1.871e-09	0.00	5.752e-11	1.013	5794	117	3.745e-11	1.020	5793	71	1.177e-11	1.016	5753	64	5777	78
HD143921	4.50	-2.48	4.397e-11	0.03	1.565e-12	1.008	5124	135	8.150e-13	1.027	5274	91	3.405e-13	1.020	5229	73	5235	94
HR5986	4.00	0.23	6.497e-09	0.00	1.802e-10	1.014	6168	104	9.167e-11	1.013	6188	62	3.443e-11	1.011	6126	57	6158	69
G016-028	4.50	-1.63	4.580e-12	0.03	1.650e-13	1.009	5143	113	9.772e-14	1.030	5184	72	3.828e-14	1.020	5114	63	5146	78
G180-024	4.50	-1.67	3.248e-11	0.00	8.690e-13	1.009	6038	180	4.597e-12	1.031	6062	119	1.689e-13	1.017	6072	114	6069	128
HD144515	4.50	-0.61	1.645e-10	0.00	6.502e-12	1.011	4940	128	4.273e-12	1.038	4910	88	1.672e-12	1.022	4828	60	4867	64
G225-057	5.00	-1.50	2.405e-10	0.00	1.390e-11	—	<3500	—	1.173e-11	—	<3500	—	4.308e-12	1.029	3578	142	(3578)	—
G184-042	4.50	-1.46	7.903e-12	0.01	2.986e-13	1.009	5015	187	1.783e-13	1.032	5092	95	6.888e-14	1.020	5050	78	5059	105
HR6136	4.50	-2.32	9.273e-09	0.00	2.102e-10	1.012	3804	188	1.924e-10	—	<3500	—	6.795e-14	1.034	3862	105	(3862)	—
G180-058	4.50	-2.32	3.237e-12	0.00	3.102e-13	1.008	5162	99	1.938e-12	1.028	5197	73	7.547e-14	1.020	5153	48	5163	69
G017-021	5.00	-0.75	3.287e-10	0.00	1.001e-11	1.010	5834	99	3.408e-12	1.020	5855	60	1.990e-12	1.017	5857	47	5831	62
HD149144	4.50	-1.79	2.966e-11	0.00	8.456e-13	1.008	5406	149	5.064e-13	1.028	5465	74	1.895e-13	1.020	5444	66	5364	85
G017-025	5.00	-1.34	4.561e-11	0.00	1.784e-12	1.009	4904	186	1.096e-12	1.034	4975	41	4.198e-13	1.021	4855	43	4962	46
HR6189	4.00	-0.63	7.847e-10	0.00	2.159e-11	1.011	6046	129	1.150e-11	1.017	6046	77	4.269e-12	1.016	6028	65	6038	83
HR6228(2)	4.50	0.00	4.097e-09	0.00	1.681e-10	1.014	4878	101	1.400e-10	1.064	4478	62	5.697e-11	1.031	4323	53	4394	57
G017-037(6)	4.50	-2.28	1.278e-12	0.00	5.957e-14	1.010	209	209	3.897e-14	1.036	4440	98	1.283e-14	1.020	4721	60	4614	74
HD152156	4.50	-1.70	5.618e-11	0.13	2.007e-12	1.009	5163	100	1.113e-12	1.027	5229	89	4.173e-13	1.020	5329	63	5289	81
HD153147	4.50	-1.26	5.376e-11	0.07	1.789e-12	1.009	5530	150	9.786e-13	1.024	5614	76	3.535e-13	1.019	5600	48	5622	87
G169-038	5.00	-1.30	1.440e-10	0.00	7.500e-12	1.011	3731	233	6.439e-12	—	<3500	—	2.434e-12	1.027	3717	125	(3717)	—
G019-013	4.50	0.00	2.807e-10	0.00	1.866e-11	1.011	4217	102	1.434e-11	1.059	4327	61	5.442e-12	1.031	4304	45	4314	52
HD156026	5.00	-0.23	1.267e-09	0.00	6.158e-11	1.011	4157	172	4.539e-11	1.057	4343	42	1.709e-11	1.029	4347	36	4345	29
HR6289	4.00	0.00	1.240e-09	0.00	4.167e-11	1.014	5543	150	2.324e-11	1.023	5562	76	8.834e-12	1.019	5508	68	5535	87
HD157089	4.00	-0.58	4.420e-10	0.00	1.417e-11	1.011	5569	82	7.670e-12	1.022	5685	78	2.832e-12	1.018	5684	47	5662	65
G181-043	4.50	-0.84	2.609e-12	0.01	1.269e-13	1.010	5279	120	7.694e-14	1.030	5257	62	2.877e-14	1.020	5248	57	5258	71
G182-007	4.50	-0.19	1.755e-10	0.00	6.508e-12	1.013	5204	108	3.878e-12	1.031	5193	47	1.513e-12	1.022	5143	48	5175	58
G013-024	4.50	0.40	5.758e-10	0.00	3.129e-11	1.012	3939	115	2.905e-11	1.068	4037	124	9.468e-12	1.037	4068	51	4065	72
G019-025	4.50	-1.52	6.878e-12	0.02	2.615e-13	1.009	4900	108	1.612e-13	1.033	5013	71	6.326e-14	1.020	4839	61	4977	75
G181-046	4.50	-0.76	3.851e-11	0.01	1.411e-12	1.011	5268	120	8.047e-13	1.028	5355	52	2.998e-13	1.020	5347	54	5334	65
G181-047	4.50	-0.68	1.115e-10	0.00	3.332e-12	1.011	5801	178	1.818e-12	1.021	5810	93	6.808e-13	1.017	5781	62	5794	93
HR6538	4.00	0.00	6.423e-10	0.00	2.017e-11	1.013	5761	153	1.081e-11	1.019	5788	79	4.036e-12	1.016	5758	71	5770	90
G139-043	5.00	0.00	1.615e-10	0.00	8.852e-12	1.012	3702	235	7.662e-12	—	<3500	—	2.691e-12	1.033	3708	127	(3708)	—
G019-027	4.50	-0.59	1.588e-10	0.00	5.530e-12	1.011	5340	80	3.114e-12	1.028	5444	75	1.150e-12	1.019	5446	45	5418	62
HR6556	4.00	0.00	3.710e-08	0.00	5.736e-10	1.009	7958	197	2.498e-10	0.993	7941	132	9.079e-11	0.993	7900	110	7923	138
G020-008	4.50	-1.25	3.493e-11	0.00	9.733e-13	1.001	5948	81	5.950e-13	1.020	5849	52	1.931e-13	1.017	5960	68	5952	65
G162-019	5.00	-2.59	3.126e-11	0.01	8.688e-13	1.008	5866	83	4.714e-12	1.021	5866	68	1.723e-13	1.018	5820	75	5801	75
G020-015	4.50	-0.71	1.246e-10	0.00	2.815e-12	1.011	5732	133	2.046e-12	1.024	5777	58	1.407e-13	1.013	5717	44	5682	63
G164-021	4.50	-2.79	2.318e-11	0.10	7.038e-13	1.008	5599	136	3.862e-13	1.021	5671	58	3.870e-13	1.020	5168	64	5146	63
HD161903	4.50	-2.29	2.866e-11	0.05	1.769e-12	1.008	5083	89	1.824e-12	1.028	5146	48	6.597e-13	0.999	7497	93	7521	111
HD162208	4.00	0.00	2.306e-10	0.00	8.394e-12	1.006	7380	189	1.624e-12	1.000	7513	97	6.019e-13	0.998	7941	88	7923	115
HR6628	4.00	0.00	2.521e-10	0.00	3.780e-12	1.003	8033	170	1.890e-12	0.988	7832	101	5.161e-12	0.987	8928	107	8794	116
HR6628	4.00	0.00	2.988e-09	0.01	3.780e-11	0.987	8588	137	1.443e-11	0.989	8845	109	6.019e-12	0.987	8928	107	8794	116

Table 4. continued

ID	log(K)	[Fe/H]	$F_{\text{Hd}}$	E(B-V)	$F_{\text{I}}$	$q_{\text{I}}$	$T_{\text{I}}$	$\Delta T_{\text{I}}$	$F_{\text{H}}$	$q_{\text{H}}$	$T_{\text{H}}$	$\Delta T_{\text{H}}$	$F_{\text{K}}$	$q_{\text{K}}$	$T_{\text{K}}$	$\Delta T_{\text{K}}$	$T_{\text{mean}}$	$\Delta T_{\text{mean}}$
G183-011	4.50	-2.05	3.701e-11	0.00	8.834e-13	1.009	6546	97	4.439e-13	1.014	6438	68	1.667e-13	1.015	6370	69	6441	70
G154-054	4.50	0.00	9.956e-12	0.05	3.406e-13	1.019	5486	107	7.342e-14	1.018	5501	75	7.342e-14	1.018	5442	45	5469	66
G154-056	4.50	-1.50	4.119e-11	0.02	1.371e-12	1.009	5392	157	7.458e-13	1.025	5505	100	2.771e-13	1.019	5542	94	5493	111
HR6772	4.50	-0.17	7.908e-09	0.00	3.144e-10	1.013	[4960]	69	1.980e-10	1.056	5023	64	7.623e-11	1.023	4931	41	4978	52
G020-024	4.50	-0.91	1.287e-11	0.12	2.289e-13	1.010	6388	113	7.726e-13	1.014	6388	64	5.971e-14	1.012	6523	70	6404	77
HR6806	4.50	-0.25	8.975e-10	0.00	2.677e-11	1.012	4866	108	2.312e-11	1.037	4964	78	8.719e-12	1.022	4931	70	4947	74
G140-046	4.50	-1.44	2.171e-11	0.00	8.540e-13	1.009	4876	79	5.925e-13	1.034	4972	57	1.964e-12	1.021	4986	42	4980	48
G021-006(7)	4.50	0.00	4.098e-12	0.00	2.020e-13	1.011	[4151]	154	1.196e-13	1.004	4749	67	4.507e-14	1.027	4723	58	4735	62
HR6844	4.50	0.17	5.657e-10	0.00	1.177e-11	1.009	7056	133	3.582e-12	1.004	7037	69	2.003e-12	1.019	7039	65	7038	80
GJ710	5.00	0.00	8.105e-11	0.00	4.241e-12	1.009	[3862]	218	7.860e-12	1.035	[3500]	300	1.381e-12	1.032	3886	102	(3888)	—
HR6847	4.50	0.00	8.240e-10	0.00	1.585e-11	1.012	5697	154	1.363e-11	1.013	5791	73	5.186e-12	1.016	5761	71	5781	90
G184-004	4.50	-0.40	1.565e-12	0.10	6.586e-14	1.012	[4735]	94	3.673e-14	1.053	5110	71	1.899e-14	1.022	5065	63	5086	87
G181-019	4.50	-2.39	2.174e-11	0.06	7.736e-13	1.008	5107	110	4.617e-13	1.028	5130	77	1.738e-12	1.020	5104	64	5138	77
HD171620	4.50	-0.65	2.563e-10	0.00	6.960e-12	1.011	6097	126	3.629e-12	1.016	6113	82	1.366e-12	1.015	6111	68	6109	86
G206-034	5.00	-3.10	8.169e-12	0.04	2.137e-12	1.013	6305	223	1.163e-13	1.014	6143	82	4.158e-14	1.012	6189	92	6191	109
G227-037	4.00	0.27	1.576e-10	0.00	4.802e-12	1.015	5885	124	2.604e-12	1.017	5842	59	8.702e-13	1.015	5869	48	5885	65
BD +20 3876	4.00	-0.45	5.247e-11	0.00	1.750e-12	1.011	5509	150	9.839e-13	1.024	5550	76	3.669e-12	1.018	5525	68	5531	87
G184-020	4.50	-1.63	1.419e-11	0.00	3.865e-13	1.009	5906	180	2.211e-13	1.021	5847	69	8.082e-14	1.018	5876	60	5869	82
G021-022	4.50	-2.11	3.593e-12	0.10	1.108e-13	1.008	5377	124	6.252e-14	1.034	5582	105	2.247e-12	1.025	5915	97	(5915)	—
G184-029	5.00	-1.50	1.602e-10	0.00	8.238e-12	1.011	[3504]	253	6.958e-12	1.035	<3500	—	1.967e-12	1.026	3760	120	(3760)	—
G022-009	4.50	-0.48	2.615e-11	0.00	6.419e-12	1.012	5386	80	5.024e-13	1.025	5497	76	1.847e-13	1.018	5503	68	5485	74
HR7236	4.00	0.00	8.963e-09	0.00	1.083e-10	1.001	8715	171	4.141e-11	1.006	8981	110	1.496e-11	1.009	8927	108	8910	124
HR7260	4.00	0.00	1.031e-09	0.00	3.406e-11	1.014	5591	142	1.875e-11	1.022	5629	67	7.066e-12	1.018	5683	67	5693	81
G022-020	4.50	-1.21	5.932e-11	0.00	1.929e-12	1.003	5498	102	1.045e-12	1.024	5608	52	3.805e-13	1.019	5651	71	5597	70
HD181007	4.50	-2.27	5.022e-11	0.00	2.073e-12	1.009	[4651]	127	1.373e-12	1.033	4633	64	5.220e-13	1.021	4625	57	4582	80
G125-004	4.50	-0.42	9.168e-11	0.00	3.623e-12	1.012	[4665]	276	2.230e-12	1.035	5045	131	8.634e-13	1.023	4975	149	5004	139
G022-024	4.50	-0.47	2.074e-11	0.00	9.407e-13	1.011	[4660]	74	6.184e-13	1.045	4675	66	2.656e-13	1.025	4715	39	4700	49
HR7373	4.00	0.41	2.368e-09	0.00	8.384e-11	1.017	5459	81	4.552e-11	1.023	5552	54	1.698e-11	1.017	5521	68	5518	97
HR7386	4.00	0.24	8.744e-10	0.00	2.544e-11	1.014	6030	125	1.296e-11	1.014	6074	90	4.741e-12	1.013	6074	90	6082	94
G125-012	4.50	-0.87	2.304e-11	0.00	6.678e-13	1.010	5875	170	3.579e-13	1.020	5801	82	1.321e-13	1.017	5801	96	5896	105
G092-008	5.00	-1.50	4.473e-11	0.00	2.553e-12	1.008	<3500	—	2.147e-12	1.020	<3500	—	8.071e-13	1.028	3509	141	(3599)	—
HD338529	4.50	-2.58	5.255e-11	0.00	1.258e-12	1.008	6341	160	6.663e-13	1.016	6298	74	2.427e-13	1.016	6309	58	6310	81
G208-029	4.00	0.00	1.021e-10	0.00	2.445e-12	1.012	6582	292	1.214e-12	1.009	6550	174	4.433e-13	1.010	6553	182	6559	205
HD184499	4.00	-0.69	6.206e-10	0.00	1.891e-11	1.011	5748	116	1.036e-11	1.022	5759	59	9.835e-12	1.018	5745	44	5750	62
G023-005	5.00	-1.50	1.121e-10	0.00	6.130e-12	1.011	<3500	—	5.321e-12	1.022	<3500	—	1.914e-12	1.027	3697	128	(3697)	—
HR7462	4.50	-0.25	4.013e-09	0.00	1.407e-10	1.013	5303	147	—	—	—	—	3.389e-11	1.022	5177	64	5227	89
HR7503	4.50	0.14	1.115e-09	0.00	3.406e-11	1.014	5803	154	1.893e-11	1.019	5780	78	7.122e-12	1.015	5730	71	5763	90
G125-031	5.00	-1.00	1.455e-10	0.00	2.766e-11	1.014	5814	154	1.522e-11	1.019	<3500	—	2.417e-12	1.016	5733	71	(5763)	—
HD188262	4.50	-1.08	8.960e-10	0.00	7.431e-12	1.014	[3846]	222	8.209e-12	1.038	4806	70	3.277e-12	1.026	3766	119	(3766)	—
G023-009	4.00	-1.80	8.512e-11	0.00	2.827e-12	1.008	5596	166	1.526e-12	1.026	5544	78	5.604e-13	1.019	5575	160	5564	121
HD189258	4.00	-1.83	7.181e-12	0.00	2.438e-13	1.008	5260	205	1.470e-13	1.028	5257	112	5.416e-14	1.020	5306	100	5278	126
G022-049	4.00	-1.30	2.306e-10	0.00	6.878e-12	1.009	5744	147	3.983e-12	1.024	5639	52	1.480e-12	1.019	5642	59	5663	87
HR6770	4.00	0.00	5.222e-12	0.00	2.815e-13	1.013	[3554]	177	1.717e-13	1.050	4570	91	6.777e-14	1.030	4477	109	4511	139
G186-011	4.00	0.26	1.431e-09	0.00	4.758e-11	1.015	5621	121	2.705e-11	1.022	5579	76	1.043e-11	1.017	5539	68	5572	83
G024-003	4.50	-1.78	3.929e-10	0.00	1.519e-11	1.013	5666	108	9.926e-12	1.036	4894	69	3.737e-12	1.024	4870	61	5001	75
HD227638	5.00	-0.87	9.290e-11	0.00	5.993e-13	1.008	5850	195	2.932e-12	1.021	5859	66	1.088e-13	1.018	5863	74	5859	89
GJ782	5.00	-1.50	1.477e-10	0.00	3.511e-12	1.011	[3762]	230	2.294e-12	1.035	4986	64	8.780e-13	1.021	4944	58	4984	78
HD345957	4.50	-1.45	8.043e-11	0.00	7.853e-12	1.009	5805	84	1.322e-12	1.022	5743	68	4.901e-13	1.025	3900	99	(3900)	—
GJ784	5.00	-1.50	4.579e-10	0.00	2.673e-11	1.009	<3500	—	2.193e-11	1.022	<3500	—	8.450e-13	1.018	5750	52	5788	65
G024-013	4.50	-1.10	2.534e-11	0.00	8.193e-12	1.009	5523	120	4.581e-13	1.025	5572	51	1.708e-13	1.019	5558	70	5558	71
HD188901	4.50	-1.43	9.745e-11	0.00	2.878e-12	1.010	5790	154	1.618e-12	1.022	5746	78	6.035e-13	1.018	5735	71	5750	90
G186-026	4.50	-3.00	1.401e-11	0.01	3.352e-13	1.008	6327	128	1.638e-13	1.014	6387	87	0.092e-14	1.015	6438	79	6428	94
HD229274	4.50	-2.46	7.292e-11	0.00	2.288e-12	1.008	5510	420	1.384e-12	1.026	5378	193	5.162e-13	1.020	5404	210	5414	243
GJ798	5.00	-1.50	1.732e-10	0.00	9.278e-12	1.011	[3640]	250	7.923e-12	1.021	<3500	—	2.816e-12	1.026	3786	116	(3786)	—
BD +4 4251	4.50	-1.80	4.144e-11	0.00	1.178e-12	1.008	5842	154	6.473e-13	1.021	5829	75	2.453e-13	1.018	5798	72	5819	91
G024-015	4.00	-1.37	1.294e-10	0.00	3.511e-12	1.009	6023	125	1.886e-12	1.019	6012	59	6.945e-13	1.017	6019	74	6017	76
HR7914	4.00	0.00	7.128e-10	0.00	2.215e-11	1.013	5781	154	1.211e-11	1.020	5768	78	4.504e-12	1.017	5745	71	5761	90

Table 4. continued

ID	$\log(g)$	$[Fe/H]$	$F_{B-V}$	$F_J$	$q_I$	$T_I$	$\Delta T_I$	$F_H$	$q_H$	$T_H$	$\Delta T_H$	$F_K$	$q_K$	$T_K$	$\Delta T_K$	$T_{mean}$	$\Delta T_{mean}$
G231-019	5.00	-1.50	3.455e-10	0.00	1.867e-12	35500	126	1.536e-11	1.066	4560	73	6.120e-12	1.028	3630	137	(3630)	—
G209-041	5.00	0.00	6.271e-11	0.00	3.292e-12	[3485]	126	2.098e-11	1.066	4560	73	1.029e-12	1.033	4003	64	4043	81
HR7994	4.00	0.00	2.413e-11	0.00	1.013	5749	153	1.547e-11	1.021	5688	77	5.081e-12	1.015	5839	67	5686	89
G210-048	4.00	0.09	6.305e-10	0.00	1.877e-11	5627	143	1.021e-11	1.018	5872	85	3.810e-12	1.015	5839	67	5870	89
G025-015	4.50	-0.43	3.270e-10	0.00	9.859e-12	5799	102	5.538e-12	1.021	5751	56	2.073e-12	1.017	4327	56	5747	50
HR0882	4.50	-0.03	3.715e-09	0.00	1.740e-10	[4372]	99	1.333e-10	1.056	4319	56	5.042e-11	1.029	4327	46	4323	60
HR0866	5.00	-0.18	2.220e-09	0.00	1.173e-11	[3810]	180	1.073e-10	1.012	<3500	—	6.303e-11	1.032	3865	97	(3865)	—
G067-037	5.00	-1.50	4.091e-10	0.00	2.066e-11	[3876]	219	1.796e-11	—	<3500	—	6.783e-12	1.022	3759	120	(3759)	—
G1820B	5.00	-1.50	2.241e-09	0.00	1.168e-10	[3726]	233	1.168e-10	1.011	<3500	—	6.645e-11	1.026	3786	116	(3786)	—
HD201891	4.50	-1.22	3.162e-10	0.00	8.942e-12	5905	127	4.845e-12	1.020	5905	68	1.780e-12	1.017	5914	49	5909	70
HD201889	4.00	-1.10	1.727e-10	0.00	5.300e-12	5670	137	3.001e-12	1.024	5643	71	1.132e-12	1.019	5609	69	5635	84
GJ285	5.00	-1.50	1.422e-09	0.00	8.148e-11	<3500	—	7.100e-11	—	<3500	—	2.576e-11	1.028	3592	142	(3592)	—
BD +04 4674	4.50	-0.90	1.118e-10	0.00	3.271e-12	5842	154	1.857e-12	1.021	5762	78	6.926e-13	1.018	5747	71	5771	90
G025-029	4.50	-0.80	1.118e-10	0.00	3.271e-12	5842	154	1.857e-12	1.021	5762	78	6.926e-13	1.018	5747	71	5771	90
G026-009	4.50	-1.27	4.843e-11	0.00	2.339e-12	[4095]	143	1.740e-12	1.051	4078	88	3.899e-13	1.024	4288	36	4235	51
G026-012	4.50	-2.64	4.490e-12	0.04	1.107e-13	6245	127	6.107e-14	1.018	6127	82	2.171e-14	1.016	6204	77	6185	91
G026-019	4.50	-0.20	4.728e-11	0.00	1.681e-12	5333	126	1.026e-12	1.029	5277	64	3.915e-13	1.021	5220	72	5267	81
G214-001	4.50	-2.06	4.854e-12	0.04	1.368e-13	5849	124	7.681e-14	1.022	5797	79	9.214e-14	1.018	5754	71	5762	86
G188-029	4.50	-0.05	6.413e-11	0.03	1.756e-12	6160	152	9.254e-13	1.014	6160	99	3.244e-13	1.013	6157	65	6159	94
G215-020	4.50	-1.50	4.695e-11	0.00	2.024e-12	<3500	—	2.024e-12	—	<3500	—	8.204e-13	1.028	3635	136	(3635)	—
G188-030	4.50	-1.99	1.268e-11	0.01	4.340e-13	5273	135	2.582e-13	1.027	5276	55	7.938e-14	1.029	5251	49	5264	65
G018-016	5.00	-1.50	1.605e-10	0.00	9.017e-12	<3500	—	7.809e-13	1.027	<3500	—	2.831e-12	1.029	3580	143	(3580)	—
G018-028	4.50	-0.84	4.468e-11	0.00	1.491e-12	5448	119	8.820e-13	1.031	5413	74	3.301e-13	1.019	5391	67	5411	75
HR8455	4.50	-0.33	9.753e-10	0.00	3.390e-11	5357	118	2.160e-11	1.021	5310	68	7.414e-12	1.020	5356	59	5204	81
G126-062	4.50	-1.80	4.495e-11	0.03	1.277e-12	5979	125	7.017e-13	1.020	5930	100	2.612e-13	1.018	5923	97	5941	106
G126-063(8)	4.50	-1.49	4.005e-12	0.06	1.519e-13	(5003)	104	6.626e-14	1.023	5725	79	2.457e-14	1.018	5738	71	5730	83
HD211476	4.50	0.05	4.137e-10	0.00	1.283e-11	5912	184	6.728e-12	1.018	5864	79	2.566e-12	1.018	5832	49	5862	67
HR3541	4.00	0.00	3.754e-09	0.00	2.668e-11	4633	123	2.824e-11	0.992	8120	67	8.400e-12	0.989	8092	87	8092	92
G016-039	4.50	-1.34	2.000e-11	0.00	3.388e-13	6046	137	2.977e-13	1.020	5965	50	1.106e-13	1.017	5934	73	5976	86
G027-036	5.00	-1.32	1.506e-11	0.00	4.403e-13	5748	123	2.428e-13	1.022	5762	79	1.639e-14	1.018	5752	71	5762	86
HR3885	4.50	-0.09	7.944e-09	0.00	4.280e-12	<3500	—	3.442e-12	—	<3500	—	1.339e-12	1.029	3870	144	(3870)	—
G067-003	4.50	-0.09	4.598e-11	0.00	9.312e-11	4811	171	3.653e-11	0.996	8994	110	1.348e-11	0.995	8878	108	8905	124
G027-044	4.50	-0.90	3.093e-10	0.00	1.665e-12	5293	117	9.947e-13	1.029	5288	73	3.702e-13	1.021	5248	65	5273	80
G156-065	4.50	-0.42	1.703e-10	0.00	5.503e-12	5694	152	5.116e-12	1.022	5746	121	1.849e-12	1.018	5752	73	5730	105
G1884	5.00	-1.50	4.288e-10	0.00	2.309e-11	<3500	—	4.197e-12	1.023	5599	65	1.366e-12	1.018	5585	59	5592	76
G028-043	4.50	-1.75	2.343e-11	0.00	1.255e-12	5016	140	7.513e-13	1.031	5072	76	2.843e-13	1.020	5078	97	5061	98
HR8832	4.50	0.00	2.044e-09	0.00	8.690e-11	[4765]	133	—	—	—	—	2.160e-11	1.028	4785	59	4785	—
G190-015	5.00	-3.00	1.240e-11	0.01	4.481e-13	5074	176	2.602e-13	1.028	5131	73	1.007e-13	1.020	5116	76	5115	82
G216-001	5.00	-1.63	1.537e-10	0.00	4.299e-12	5907	131	2.176e-12	1.019	6063	80	8.277e-13	1.017	6003	74	6012	89
G216-037	5.00	0.00	3.632e-11	0.00	2.002e-12	[3652]	116	1.799e-12	—	<3500	—	6.534e-13	1.032	3775	92	(3775)	—
G029-023	4.50	-2.02	2.387e-11	0.00	6.158e-13	6126	126	3.265e-13	1.013	6129	82	1.241e-13	1.017	6062	75	6102	90
G217-007	5.00	0.00	1.061e-10	0.00	5.513e-12	3830	248	4.814e-12	1.083	[3681]	300	1.807e-12	1.024	3907	130	3980	130
HR8905	4.00	-0.12	4.612e-09	0.00	1.335e-10	5982	156	—	—	—	—	2.637e-11	1.018	5941	73	5954	99
G217-008(9)	4.50	-1.91	1.817e-11	0.01	3.094e-13	(6645)	130	2.432e-13	1.018	6183	82	9.323e-14	1.017	6091	75	6134	70
G273-068	5.00	0.00	1.867e-10	0.00	9.914e-12	[3894]	224	7.452e-12	1.057	[3940]	300	2.799e-12	1.030	4101	72	4101	—
G029-034	5.00	0.00	4.608e-11	0.00	2.497e-12	[3752]	184	1.888e-12	1.066	4090	113	7.527e-13	1.023	4012	83	4048	96
G190-034	4.50	-0.01	7.043e-11	0.00	2.537e-12	5320	147	1.484e-12	1.027	5341	92	5.598e-13	1.021	5301	65	5318	91
G029-047	5.00	0.00	9.468e-11	0.00	5.148e-12	[3754]	180	4.540e-12	—	<3500	—	1.698e-12	1.035	3781	99	(3781)	—
HD221350	4.50	-0.70	1.428e-09	0.00	3.527e-11	5370	160	1.854e-11	1.014	5297	84	6.827e-12	1.014	6296	78	6311	97
HD221389	4.50	0.02	9.686e-11	0.00	3.580e-12	5248	146	2.288e-12	1.022	5181	71	8.440e-13	1.021	5135	63	5174	82
G158-093	4.50	-0.30	2.612e-11	0.00	8.138e-13	5443	119	5.026e-13	1.028	5439	75	1.899e-13	1.010	5422	67	5440	82
G158-020	4.50	-0.59	1.201e-10	0.00	3.465e-12	5919	127	1.926e-12	1.020	5849	67	7.139e-13	1.017	5837	72	5860	83
LT16059	4.00	0.00	7.738e-12	0.00	2.407e-12	[4935]	123	1.474e-13	1.023	5411	76	3.630e-14	1.019	5410	68	5366	84
BD-16 418	4.50	0.00	1.428e-11	0.00	5.777e-13	5255	146	3.684e-13	1.037	4975	69	1.440e-13	1.024	4867	60	4917	64
G251-054	4.50	-1.73	2.841e-11	0.00	9.877e-13	5255	146	5.657e-13	1.027	5309	73	2.115e-13	1.020	5300	86	5308	84

NOTES TO TABLE 4:

- (1) SB501: Wrong  $F_J$ . ( $J=11.22$ ).
- (2) G036-050: The error in  $F_J$  is greater than 10%, hence no  $T_J$  is provided.
- (3) G178-030: Very faint star,  $J=11.63$ ,  $H=11.31$  and  $K=11.127$ .
- (4) G167-011: The error in  $F_J$  is greater than 20%. The faintest star of the sample ( $J=12.99$ ).
- (5) HR8228: Wrong  $F_J$ .
- (6) G017-037: Very faint star,  $J=11.706$ ,  $H=11.300$  and  $K=11.297$ .
- (7) G021-006: Wrong  $F_J$ . ( $J=10.38$ ).
- (8) G126-063: Faint star,  $J=10.69$ ,  $H=10.64$  and  $K=10.59$ .
- (9) G217-008: Wrong  $F_J$ .