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## Development of micropillar array electrodes for highly sensitive detection of biomarkers†

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Micropillar array electrodes ( $\mu$ AEs) have been widely applied in electrochemical detection owing to their advantages of increased mass transport, lower detection limit, and potential to be miniaturized. This paper reports the fabrication, simulation, surface modification, and characterization of PDMS-based  $\mu$ AEs coated with gold films. The  $\mu$ AEs consist of  $9 \times 10$  micropillars with a height of either 100  $\mu\text{m}$ , 300  $\mu\text{m}$ , or 500  $\mu\text{m}$  in a 0.09  $\text{cm}^2$  region. Numerical simulation was employed to study the influence of geometrical parameters on the current density. The  $\mu$ AEs were fabricated by soft lithography and characterized using both SEM and cyclic voltammetry. Experiments revealed that high pillars enabled enhanced voltammetric current density regardless of the scan rates. The platinum–palladium/multi-walled carbon nanotubes (Pt–Pd/MWCNTs) were coated on the  $\mu$ AEs to improve their electrochemical detection capability. The  $\mu$ AEs demonstrated 1.5 times larger sensitivity compared with the planar electrode when hydrogen peroxide was detected. Furthermore,  $\mu$ AE500 with Pt–Pd/MWCNTs was employed to detect sarcosine, a potential biomarker for prostate cancer. The linear range and limit of detection for sarcosine were from 5 to 60  $\mu\text{M}$  and 1.28  $\mu\text{M}$ , respectively. This detection range covers the concentration of sarcosine in human tissues (0–60  $\mu\text{M}$ ). These results suggest that the  $\mu$ AEs have better detection performance in comparison to planar electrodes due to their large surface area and pillar height. This paper provides essential guidelines for the application of  $\mu$ AEs in high sensitivity electrochemical detection of low abundance analytes.

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## Introduction

The detection and identification of biomarkers are important in biological studies and disease diagnosis such as cancers.<sup>1</sup> In the past few decades, a variety of analytical techniques,<sup>2,3</sup> including immunoassay,<sup>4</sup> electrochemistry,<sup>5</sup> and electrochemiluminescence,<sup>6</sup> have been developed for the detection of disease biomarkers. The electrochemical technique is one of the most attractive ways owing to its simplicity, portability, and high sensitivity.<sup>7</sup> Among electrochemical sensors, the amperometric one is reliable and cost-effective and therefore has been broadly implemented to detect a variety of biomarkers,<sup>8</sup> such as glucose,<sup>9</sup> sarcosine<sup>10</sup> and cholesterol.<sup>11</sup>

Compared to the reference and counter electrodes, the working electrode is the most crucial element of the electrochemical sensors and has been attracting plenty of research interest to either increase the sensitivity<sup>12</sup> or reduce the detection limits.<sup>13</sup> According to the geometry, electrodes can be divided into planar and 3D ones. The former ones are the most widely employed electrodes since they are not only cost-effective but easy to fabricate. For example, glassy carbon electrodes, screen-printed electrodes,<sup>14</sup> and conductive films patterned on the substrate<sup>15,16</sup> have been developed. In addition to the planar electrodes, the micropillar array electrodes ( $\mu$ AEs) have attracted research attention as an emerging technology with a better electrical signal due to the increased surface area. The  $\mu$ AEs have been used to detect phenol,<sup>17</sup> biofilm,<sup>18</sup> bone metabolic marker proteins,<sup>19</sup> and metal ions.<sup>20</sup> Compared with the planar electrodes,  $\mu$ AEs significantly enhance the response current and hence provide high sensitivity and low detection limit.<sup>20</sup>

The  $\mu$ AEs are mainly manufactured by complicated techniques involving the LIGA-like process,<sup>17–19</sup> carbonizing the photoresist patterned on a substrate,<sup>21</sup> and homoepitaxially growing.<sup>20</sup> Prehn *et al.* have reported  $\mu$ AEs with 10  $\mu\text{m}$  high pillars fabricated using the photolithography, metallization, and electrodeposition.<sup>22</sup> Sanchez-Molas *et al.* used sputtering

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and deep reactive ion etching (DRIE) to prepare the  $\mu$ AEs with higher micropillar (up to 125  $\mu\text{m}$ ),<sup>23</sup> and this approach showed better definition and reproducibility. The  $\mu$ AEs with high micropillar are attractive in electrochemical applications owing to the larger electrode surface areas. The above studies have successfully demonstrated both the manufacture and the capability of  $\mu$ AEs. However, the fabrication processes are generally not only expensive but time-consuming. Additionally, both the aspect ratio and pillar height are limited by the lithography process.<sup>23</sup> Therefore, the facile preparation of the  $\mu$ AEs with the higher micropillar even 3D profile is of critical significance for the development of low-cost and high-sensitivity microsensors for chemical and biological substances.

The effect of the dimension (*e.g.*, diameter, height, and space) of micropillar array electrodes on the voltammetric response has been studied both numerically<sup>24</sup> and experimentally.<sup>22,23</sup> The voltammetric response of  $\mu$ AEs was related to both the height and the density of micropillar. Sánchez-Molas *et al.* studied the effect both parameters on the current density under different scan rates (0.005–0.2  $\text{V s}^{-1}$ ).<sup>23</sup> They reported that the  $\mu$ AEs with either taller pillars or higher density acquired larger currents.<sup>23</sup> Further, Prehn *et al.* reported the increased pillar height narrowed the potential peak-to-peak separation due to the rapid electrolysis of the material around the cylinder walls.<sup>22</sup>

The above research illustrated the importance of the dimension of  $\mu$ AEs. Therefore, understanding the response current of  $\mu$ AEs under various geometrical parameters is essential to obtain a larger current density. Additionally, for high-density micropillar array, the response current was found to be proportional to the surface area at fast scan rates.<sup>22</sup> However, at low scan rates, there was no significant difference in the response current between the  $\mu$ AEs with low pillars and planar electrodes with the same projection area.<sup>22</sup> Since low scan rates are frequently applied in electrochemical detection of low-concentration analytes, developing  $\mu$ AEs with large response current at low scan rates will benefit their application in electrochemical detection.

Herein, we report the manufacture, simulation, and systematic characterization of micropillar array electrodes to enhance the detection sensitivity. The  $\mu$ AEs was manufactured by sputtering gold on PDMS-based micropillars molded from a 3D-printed master. The platinum-palladium/multi-walled carbon nanotubes (Pt-Pd/MWCNTs) were used to modify the  $\mu$ AEs by simple drop-cast. The electrochemical performance was demonstrated using hydrogen peroxide and sarcosine. The  $\mu$ AEs with high micropillars enabled a larger surface area and current density at low to high scan rates (0.025–1  $\text{V s}^{-1}$ ). The sensitivity of  $\mu$ AEs toward hydrogen peroxide was higher than that of the planar electrode. The linear detection range and LOD of  $\mu$ AEs for sarcosine were 5–60  $\mu\text{M}$  and 17.1  $\mu\text{A mM}^{-1} \text{cm}^{-2}$ , respectively. The paper provided essential guidance for the design and application of  $\mu$ AEs in biomarker detection with high sensitivity.

## Experimental

### Chemicals

The polydimethylsiloxane (PDMS, Sylgard 184) base and curing agent were purchased from Suzhou Research Materials Microtech Co., Ltd. The phosphate buffer solution (PBS, 0.1 M, pH 7.4), 1H,1H,2H,2H-perfluorooctyltrichlorosilane, hydrogen peroxide ( $\text{H}_2\text{O}_2$ ), (3-mercaptopropyl)trimethoxysilane (MPTMS), potassium ferrocyanide and potassium ferricyanide were purchased from Shanghai Macklin Biochemical Co., Ltd. The multi-walled carbon nanotubes (MWCNTs, 10–20 nm in diameter, 0.5–2  $\mu\text{m}$  in length, 95%) were bought from Nanjing XFNANO Materials Tech Co. Potassium chloroplatinate ( $\text{K}_2\text{PtCl}_6$ ), ethyl acetate, sodium tetrachloropalladate ( $\text{Na}_2\text{PdCl}_4$ ), sodium citrate and ethylene glycol (EG) were obtained from Aladdin Industrial Corporation. The Nafion™ 117 solution (5% in a mixture of lower aliphatic alcohols and water) was purchased from Sigma-Aldrich. All chemicals were analytical grade and used without further purifications.

### Instrumentation and measurements

The scanning electron microscopic (SEM) and transmission electron microscopic (TEM) images were captured using a ZEISS SUPRA 55 electron microscope (Carl Zeiss, Germany) and a Tecnai G2 spirit TEM (FEI, USA), respectively. The X-ray photoelectron spectroscopy (XPS) analysis was performed on an X-ray photoelectron spectrometer (PHI5000 Versaprobe II, PHI, Japan). The NanoArch P140 (BMF Precision, Shenzhen, China) was employed to print the polymer masters of micropillar arrays. The oxygen plasma treatment and sputtering were carried out using PDC-002 (Harrick, Japan) and PD-400 (Pudivacuum, China), respectively. The electrochemical measurements (*e.g.* cyclic voltammetry and chronoamperometry) were performed using an electrochemical workstation (CHI 660E, Shanghai Chen Hua Instrument Co. Ltd). All experiments were carried out using three electrodes: working, counter, and reference electrodes. The counter electrode was a platinum wire electrode (0.5 mm in diameter, 63 mm in length), and the reference electrode was Ag/AgCl (3.0 M KCl) electrode (Ag/AgCl wire, 0.5 mm in diameter, 45 mm in length).

### Numerical simulation

A 3D symmetrical model of the pillar and a diffusion domain (Fig. S1†) were generated in COMSOL to simulate the voltammetric response of  $\mu$ AEs with various dimensions. The center-to-center distance between two adjacent micropillars and the height of the diffusion domain varied from 10  $\mu\text{m}$  to 800  $\mu\text{m}$  and 600  $\mu\text{m}$  to 1600  $\mu\text{m}$ , respectively. The radius of the cylindrical diffusion domain was equal to the half of the center-to-center distance between two adjacent micropillars. The pillar height ranged from 100  $\mu\text{m}$  to 1000  $\mu\text{m}$ . While the scan rate was 100  $\text{mV s}^{-1}$  and the height of the diffusion domain was  $6\sqrt{(Dt)}$  higher than the pillar, where  $D$  was the diffusion coefficient of the oxidized species and  $t$  (16 seconds) was the total time for the CV scan.



The diffusional transport of the whole domain was obtained by integration in the radial and axial directions of the domain. The boundary conditions used in the simulations were listed in Table S1.† The diffusional current in a one-electron, fully reversible electrochemical system can be described by:

$$I = 2\pi FD \int_0^{r_{\text{pillar}}} \left( \frac{\partial A}{\partial z} \right)_{z=z_{\text{pillar}}} r dr + \int_0^{z_{\text{pillar}}} \left( \frac{\partial A}{\partial r} \right)_{r=r_{\text{pillar}}} dz + \int_{r_{\text{pillar}}}^{r_{\text{domain}}} \left( \frac{\partial A}{\partial z} \right)_{z=0} r dr,$$

where  $A = 5 \text{ mM}$  is the concentration of the oxidized species;<sup>25</sup>  $F$  is the Faraday constant;  $z$  is the component along the axis of the micropillar;  $r$  is the component along the radial direction of the micropillar;  $r_{\text{pillar}}$  and  $z_{\text{pillar}}$  are the cylinder radius and height; and  $r_{\text{domain}}$  is the radius of the diffusion domain. Since this study only analyzed the data with forwarding scan peak, to simplify the simulation process, it is assumed that both the reduced and the oxidized species have the same diffusion coefficient ( $6.39 \times 10^{-6} \text{ cm}^2 \text{ s}^{-1}$ ).<sup>26</sup>

The grid impedance test was performed to determine the optimal mesh size for acquiring accurate results. Additionally, validation was carried out using a model with the geometry reported in a previous study<sup>22</sup> and boundary conditions which were exactly the same as those employed in this study (Fig. S2†). The difference in the current density between simulations in this study and the previous study<sup>22</sup> was less than 3%.

### Fabrication of micropillar array electrode

Three types of micropillar array electrodes (see Table S2†) containing  $9 \times 10$  truncated cones were designed in a  $0.09 \text{ cm}^2$  region (Fig. 1). The radii of the top and bottom plane of the cones were  $50 \mu\text{m}$  and  $100 \mu\text{m}$ , respectively. The separation of the cone was  $100 \mu\text{m}$ . The height of the pillars was either  $100 \mu\text{m}$  ( $\mu\text{AE}100$ ),  $300 \mu\text{m}$  ( $\mu\text{AE}300$ ) or  $500 \mu\text{m}$  ( $\mu\text{AE}500$ ).

The UV curable polymer was printed on a glass slide using a 3D printer (NanoArch P140) to form the positive masters (see Fig. 1A(a)) of micropillar array. The PDMS-based micropillar

arrays were then manufactured by soft lithography as described elsewhere.<sup>27–30</sup> Briefly, the 3D-printed master was firstly coated with  $1H,1H,2H,2H$ -perfluorooctyltrichlorosilane in a vacuum desiccator. Then the PDMS mixture with the volume ratio of 10 (base) : 1 (curing agent) was cast against the master and degassed for 30 minutes. After baked at  $60 \text{ }^\circ\text{C}$  overnight, the negative PDMS replicas of micropillar arrays were peeled off from the master (Fig. 1A(b)). The negative PDMS replicas were employed as masters to mass-produce the PDMS micropillar arrays using the aforementioned soft lithography technique (Fig. 1A(c) and (d)).

The PDMS micropillar arrays were sputtered with gold to form conduction layers.<sup>31,32</sup> Briefly, the arrays were oxidized for 30 seconds using an oxygen plasma to form hydroxyl groups.<sup>33,34</sup> Afterward, the arrays were placed in a vacuum desiccator with (3-mercaptopropyl) trimethoxysilane for 20 minutes to obtain the thiol groups ( $-\text{SH}$ ). The arrays were then covered using a steel mask (with a  $3 \text{ mm} \times 3 \text{ mm}$  window) and placed in a sputter with the power of 300 W, the Ar flow rate of 50–80 sccm and the pressure of 0.2–0.5 Pa to deposit a gold membrane with a thickness of approximately 250 nm on the pillar arrays. The micropillar arrays with the gold film were referred to as  $\mu\text{AE}$ s without stated otherwise (Fig. 1A(e)).

### Synthesis of Pt–Pd/MWCNTs

The Pt–Pd/MWCNTs nanocomposites were synthesized according to the protocols reported in the literature.<sup>35</sup> Briefly, MWCNTs were immersed in the mixture of concentrated  $\text{HNO}_3$  and  $\text{H}_2\text{SO}_4$  (v/v, 1 : 3) at  $80 \text{ }^\circ\text{C}$  for 8 hours to improve the water solubility. Then, 10 mg MWCNTs were dispersed in 10 mL EG solutions (50% in water) with 30 minute ultrasonication. The MWCNTs suspension was added to an EG solution (30 mL, 50% in water) containing 24.3 mg  $\text{K}_2\text{PtCl}_6$  (50  $\mu\text{mol}$ ), 14.7 mg  $\text{Na}_2\text{-PdCl}_4$  (50  $\mu\text{mol}$ ) and 10 mg trisodium citrate. The pH value of the solution was then adjusted to 10 using NaOH. The mixture solution was deoxygenated by nitrogen for 30 minutes and then incubated at  $100 \text{ }^\circ\text{C}$  for eight hours with continuous stirring. Finally, the reaction products (Pt–Pd/MWCNTs) were filtrated, washed, and vacuum-dried at  $50 \text{ }^\circ\text{C}$  overnight.

### Modification of the micropillar array electrodes

The  $\mu\text{AE}$ s were modified to promote analytical performance further. One  $\mu\text{L}$  Pt–Pd/MWCNTs suspension was pipetted onto the surface of the  $\mu\text{AE}$ s and dried at room temperature. Subsequently, four  $\mu\text{L}$  Nafion (0.05 wt%) was added to the same region of the  $\mu\text{AE}$ s and dried at room temperature, before stored at  $4 \text{ }^\circ\text{C}$  in the phosphate buffer solution (PBS) for the following electrochemical detection. The  $\mu\text{AE}$ s coated with nanomaterials were referred to as Nafion/Pt–Pd/MWCNTs/ $\mu\text{AE}$  in this paper (Fig. 1B).

### Manufacture of sarcosine biosensors

The  $\mu\text{AE}500\text{-Nafion/Pt-Pd/MWCNTs}$  was employed to detect sarcosine. Four  $\mu\text{L}$  sarcosine oxidase solution ( $1 \text{ kU mL}^{-1}$ ) was added to the surface of the electrodes and dried at  $4 \text{ }^\circ\text{C}$ . The electrodes were further coated with four  $\mu\text{L}$  Nafion solution

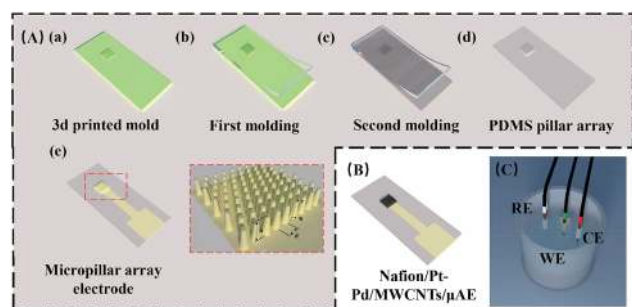


Fig. 1 (A) The schematic diagram showing the fabrication process of the micropillar array electrode using double soft lithography. (a) The positive master from 3D printing of UV curable polymer. (b) The negative mould of the  $\mu\text{AE}$  after the first soft lithography. (c) The second soft lithography and (d) the PDMS-based  $\mu\text{AE}$ . (e) The PDMS-based  $\mu\text{AE}$  sputtered with a gold film. (B) The  $\mu\text{AE}$  coated with Nafion/Pt–Pd/MWCNTs. (C) A typical setup of electrochemical detection using a three-electrode sensor.



(0.05 wt%) and dried at room temperature. The biosensors were finally washed with phosphate buffer (0.1 M, pH 7.4) and stored at 4 °C for further usage.

### Cyclic voltammetry and chronoamperometry measurements

The working, reference, and counter electrodes were directly immersed into a small vial containing the analyte solution to perform electrochemical detection (Fig. 1C). The electrochemically active area of the  $\mu$ AEs was studied using cyclic voltammetry in 5.0 mM  $\text{K}_3[\text{Fe}(\text{CN})_6]/\text{K}_4[\text{Fe}(\text{CN})_6]$  solution containing 0.5 M KCl. As a benchmark, a planar electrode with the same projected area was tested to demonstrate the performance of the  $\mu$ AEs. The hydrogen peroxide and sarcosine were detected using chronoamperometry at a potential of +600 mV for 90 seconds. The current responses were recorded after 80 seconds when the current was steady. All experiments were repeated at least three times.

## Results and discussion

### Numerical evaluation of micropillar array electrodes

The  $\mu$ AEs were developed to obtain the increased electrical signal since they possess the much larger surface area than the planar electrodes with the same projected area ( $A_{\text{pa}}$ ). The dimension (*e.g.*, diameter, height, and separation) of the  $\mu$ AEs significantly influenced their surface area. To this end, understanding the influence of geometrical parameters of the  $\mu$ AEs on the response current is of critical importance for the development of electrochemical biosensors based on  $\mu$ AEs.

The numerical simulation was employed to study the impact of surface area (caused by varying pillar height) as well as the height and separation normalized to the bottom radius of pillars. As shown in Fig. S3,<sup>†</sup> the current density becomes larger as pillar height increased. The increase of the pillar height directly results in an increase of the electrode surface area. Fig. 2A clearly depicts that the current density, *i.e.*, the ratio between the anodic peak current ( $i_{\text{pc}}$ ) and the projection area, is directly proportional to the surface area ( $S$ ) of the  $\mu$ AEs. The relationship can be described by a linear model of:  $i_{\text{pc}}/A_{\text{pa}}$  ( $\text{A m}^{-2}$ ) =  $165.1S$  ( $\text{mm}^2$ ) -  $1.52$  ( $R^2 = 0.99$ ). This linear relationship suggests the planar diffusion dominates the response of the  $\mu$ AEs which is in agreement with the findings by Sánchez-Molas.<sup>23</sup> Additionally, the current density of  $\mu$ AEs with the height of 100, 300, and 500  $\mu\text{m}$  is 0.85, 2.83, and 4.8 times larger than that of the planar electrode, respectively. Therefore,  $\mu$ AEs with a large surface area can be used to obtain electrical signals with increased intensities.

The influence of the dimension, *e.g.*, radius, height, and separation of pillars, on the current density was numerically studied to guide the design of  $\mu$ AEs. The normalized height was  $Z = z_{\text{pillar}}/r_{\text{pillar}}$  and the normalized separation was  $D = r_{\text{domain}}/r_{\text{pillar}}$ . Fig. 2B shows the current density of the  $\mu$ AEs as a function of  $Z$  and  $D$ . For a given micropillar radius and separation, the higher the normalized height ( $Z$ ), the larger the current density. For example, for the model with a 100  $\mu\text{m}$  micropillar radius and  $D$  of 1.5, the current density of the  $\mu$ AE with 800  $\mu\text{m}$  micropillars is 3.08 times of that of the  $\mu$ AE with 200  $\mu\text{m}$  micropillars. This suggests that the height has a significant impact on the response current for any  $\mu$ AEs. In comparison, a much smaller separation is required to achieve a larger surface area. However, a smaller separation might reduce the current density due to the potential overlap of the diffusion layers. For example, when  $Z$  is set to 6, the current density of the  $\mu$ AE with  $D = 1.05$  is 45% of that of the  $\mu$ AE with  $D = 1.25$ . Thus, it is reasonable to employ this model to analyze the maximum response current and the current density of the  $\mu$ AE as long as the normalized height and separation are within the above ranges. Such an analysis may benefit the understanding of the performance of  $\mu$ AEs from the geometry point of view.

### Characterization of micropillar array electrodes

The SEM images of  $\mu$ AE100,  $\mu$ AE300,  $\mu$ AE500, and a planar electrode (PDMS coated with a gold layer) are shown in Fig. 3(a)–(d). The pillars with the truncated-cone shape were successfully manufactured after repeated soft lithography. The height of micropillars on the cross-sectional images of  $\mu$ AE100,  $\mu$ AE300, and  $\mu$ AE500 (Fig. 3(e)–(g)) was measured as  $102.7 \pm 1.4$   $\mu\text{m}$ ,  $311.6 \pm 2.3$   $\mu\text{m}$ , and  $515.4 \pm 3.2$   $\mu\text{m}$ , respectively. The bottom radius of the pillars was approximately 100  $\mu\text{m}$ , while the center-to-center distance of two pillars within the same row or column was around 300  $\mu\text{m}$ . Additionally, there are obvious ripples on the sidewalls of the pillars which were related to the resolution of the layer-to-layer printing. The ripples might be beneficial for raising the surface area to volume ratio of the electrodes. Since the master of  $\mu$ AEs in this study was

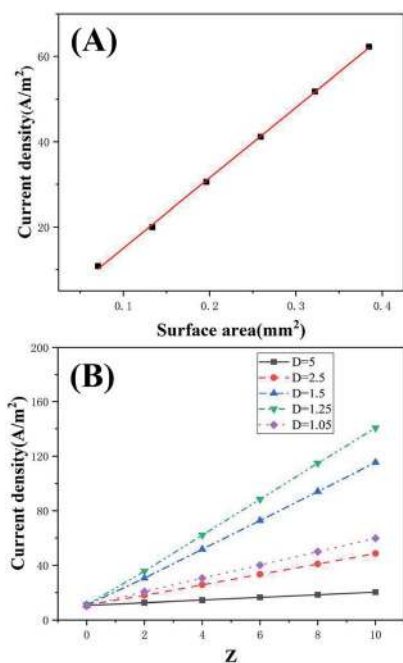


Fig. 2 (A) Variation of current density of the  $\mu$ AEs with surface area when the pillar height varied from 100 to 500  $\mu\text{m}$ . (B) Current density of the  $\mu$ AEs as a function of normalized height ( $Z$ ) at different separations ( $D$ ).



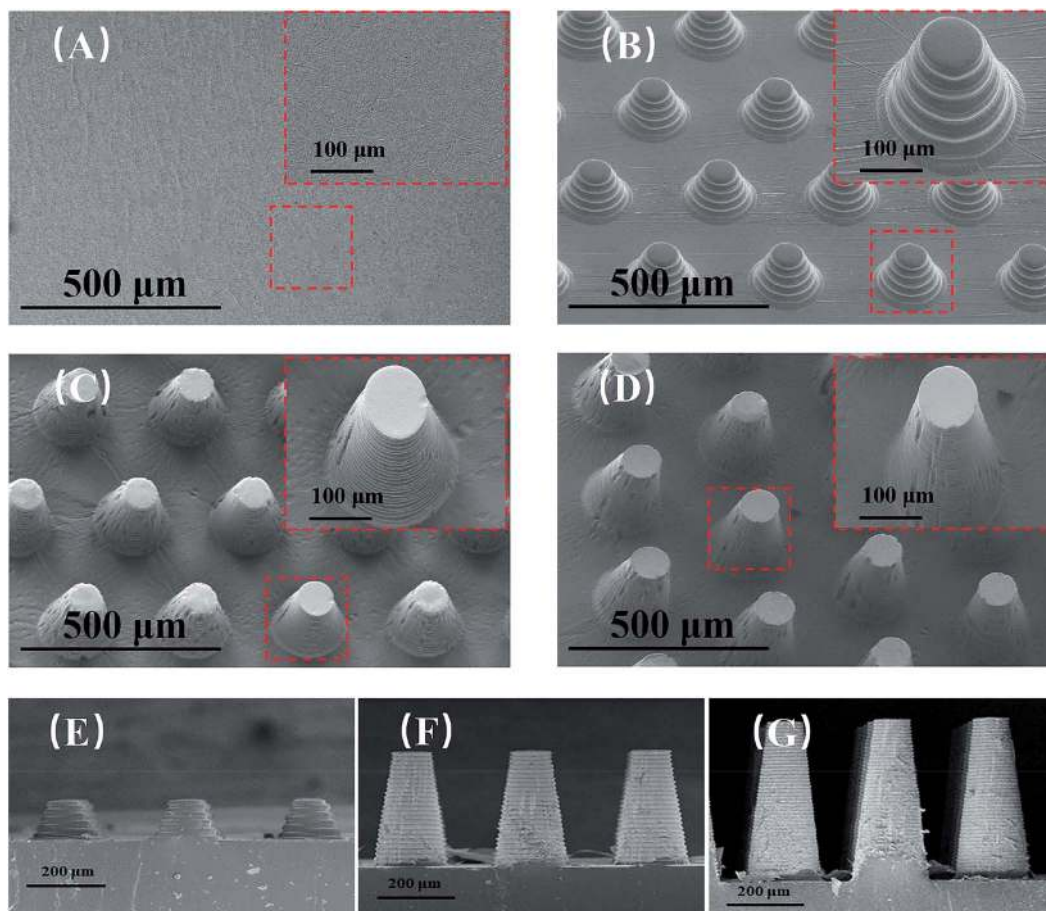


Fig. 3 The SEM images of (A) the planar PDMS electrode, and the PDMS  $\mu$ AEs with (B) 100  $\mu$ m, (C) 300  $\mu$ m and (D) 500  $\mu$ m high pillars. Cross-sectional views of the  $\mu$ AEs with the pillar height of (E) 100  $\mu$ m, (F) 300  $\mu$ m and (G) 500  $\mu$ m.

manufactured by 3D printing, the height of pillars is much higher than those fabricated using MEMS micromachining techniques,<sup>22,23</sup> demonstrating the advantage of the fabrication in this paper.

The cyclic voltammetry (Fig. S4†) was used in a standard redox system of ferrocyanide/ferricyanide with potassium chloride to understand the electrochemical activity of both the planar electrodes and the  $\mu$ AEs with various pillar heights. The CV curves (Fig. 4A) at the scan rate of 100  $\text{mV s}^{-1}$  reveals that the absolute value of both the redox and the anodic peak current increase with the increase of the pillar height. The anodic peak current ( $i_{\text{pa}}$ ) obtained from the curves is proportional to the surface area of the electrodes (inset). For example, the  $i_{\text{pa}}$  and the surface area of  $\mu$ AE500 are approximately 3.3 and 2.13 times higher than those of the planar electrode, respectively. This relationship can be described by a linear model of:  $i_{\text{pa}} (\mu\text{A}) = 26.42 S (\text{mm}^2) - 56.3$  ( $R^2 = 0.99$ ).

The electroactive area ( $A$ ,  $\text{cm}^2$ ) was determined using the Randles-Sevcik equation:<sup>36</sup>  $i_{\text{p}} = (2.69 \times 10^5)n^{3/2}ACD^{1/2}\nu^{1/2}$ , where  $i_{\text{p}}$  is the peak current in amperes,  $n$  is the number of electrons involved in the electrochemical reaction,  $C$  is the concentration of the analyte in  $\text{mol cm}^{-3}$ ,  $D$  is the diffusion coefficient of the species ( $6.39 \times 10^{-6} \text{ cm}^2 \text{ s}^{-1}$ ),<sup>26</sup> and  $\nu$  is the

scan rate in  $\text{V s}^{-1}$ . As shown in Fig. 4B, the electroactive areas of  $\mu$ AE100,  $\mu$ AE300 and  $\mu$ AE500 are 0.67, 1.87 and 3.33 times larger than that of the planar electrode ( $0.15 \pm 0.006 \text{ cm}^2$ ), respectively. This suggests  $\mu$ AEs effectively increase the electroactive area by incorporating micropillars with different heights. Furthermore, the electroactive area is 67–127% larger than the surface area of each electrode, which might be related to the surface roughness as a result of the 3D printing technique (e.g., stepped structure on the side walls).

The relationship (see Fig. 4C) between the scan rates and the redox peak current of  $\mu$ AEs in 5 mM  $\text{K}_3[\text{Fe}(\text{CN})_6]/\text{K}_4[\text{Fe}(\text{CN})_6]$  solution was studied in detail to understand the dynamic behavior of the  $\mu$ AEs. The absolute value of both anode ( $i_{\text{pa}}$ ) and cathodic ( $i_{\text{pc}}$ ) peak current is directly proportional to the square root of the scan rates in the range of 0.14 to 0.5. This relationship can be described by  $i_{\text{pa}} = k\sqrt{\nu} + b$ , where  $k = 251.45$ , 278.36, 524.72, and 752.43 for the planar,  $\mu$ AE100,  $\mu$ AE300 and  $\mu$ AE500, respectively. It is obvious that the slope augmented as an increase in the surface area of the electrodes. Moreover, the linear correlation between redox peak current and the square root of the scan rate indicates that the kinetics of  $\mu$ AEs is diffusion-controlled.<sup>36</sup>



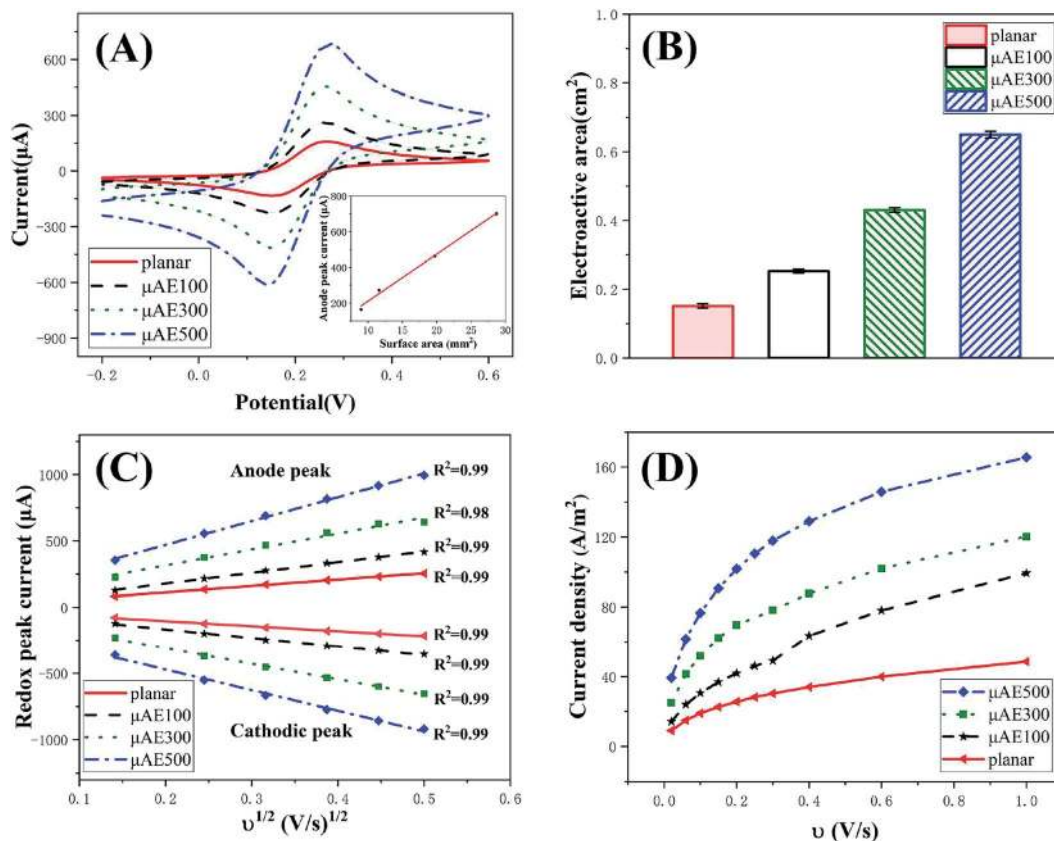


Fig. 4 (A) Cyclic voltammety of the planar electrode,  $\mu$ AE100,  $\mu$ AE300, and  $\mu$ AE500 in the 5 mM  $K_3[Fe(CN)_6]/K_4[Fe(CN)_6]$  solution with 0.5 M KCl. (B) Electroactive area. (C) Anodic and cathodic peak currents as a function of the square root of the scan rates. (D) Variation of current density with scan rate for different electrodes.

The current density of  $\mu$ AEs at distinct scan rates was studied to demonstrate their advantages in improving the detection sensitivity. The relationship between scan rates and the current density is shown in Fig. 4D. The  $\mu$ AEs have higher current densities at any given scan rate in the range of  $0.025\text{--}1\text{ V s}^{-1}$  (ref. 22) in comparison with the planar electrode. For example, when the scan rate is  $20\text{ mV s}^{-1}$ , the current density of the  $\mu$ AE100,  $\mu$ AE300, and  $\mu$ AE500 is 0.56, 1.75 and 3.32 times larger than that of the planar electrode, respectively. According to Prehn *et al.*,<sup>16</sup> when the micropillars are immersed in the diffusion layer, there is no significant difference in the voltammety between  $\mu$ AEs and the planar electrode at a low scan rate ( $0.025\text{ V s}^{-1}$ ). However, our results reveal that higher micropillars achieve higher current density even at low scan rates. This is because the height of the  $\mu$ AEs is sufficient to allow the penetration through the diffusion layer.

#### Characterization of Pt–Pd/MWCNTs

The application of Pt–Pd/MWCNTs was explored in modifying the  $\mu$ AEs. Both TEM and XPS techniques were employed to confirm that the current Pt–Pd/MWCNTs had similar morphology and composition to that in the literature, which indicates the successful synthesis of the nanomaterials. The

TEM photos (Fig. 5A) of the Pt–Pd/MWCNTs indicates that Pt–Pd nanoparticles were deposited on the surface of MWCNTs without visible aggregation. The mean size of Pt–Pd nanoparticles on the TEM photos was measured to be approximately 4 nm. Additionally, the elementary composition of Pt–Pd/MWCNTs was confirmed by XPS. Fig. 5B clearly shows the signal of Pt 4f and Pd 3d in the samples of the Pt–Pd/MWCNTs, while there are no relevant signals in the acid-treated MWCNTs. The core-level spectra of Pt 4f and Pd 3d (Fig. S5A and B<sup>†</sup>) indicates that the intensity peaks of Pt 4f<sub>7/2</sub>, Pt 4f<sub>5/2</sub>, Pd 3d<sub>5/2</sub>, and Pd 3d<sub>3/2</sub> appears when the binding energy was 71.9, 75.2, 336.2, and 341.5 eV, respectively. These results reveal the coexistence of Pt (0) and Pd (0) in Pt–Pd/MWCNTs. In addition to introducing larger surface area using micropillars, nanomaterials,<sup>37,38</sup> *e.g.*, Pt nanoparticles (NPs),<sup>39</sup> bismuth NPs,<sup>18</sup> and gold-black,<sup>19</sup> have been widely employed to modify the surface of  $\mu$ AEs to obtain larger response current. However, most nanomaterials are introduced to the surface by electrodeposition, which not only requires precise control of the current and voltage but is limited for the cases of depositing complex nanomaterials or modification of multiple electrodes simultaneously. The current study employed drop cast of complex nanomaterials, Pt–Pd/MWCNTs, to modify the electrode surface. Such materials were recently developed as a novel nanomaterial to modify



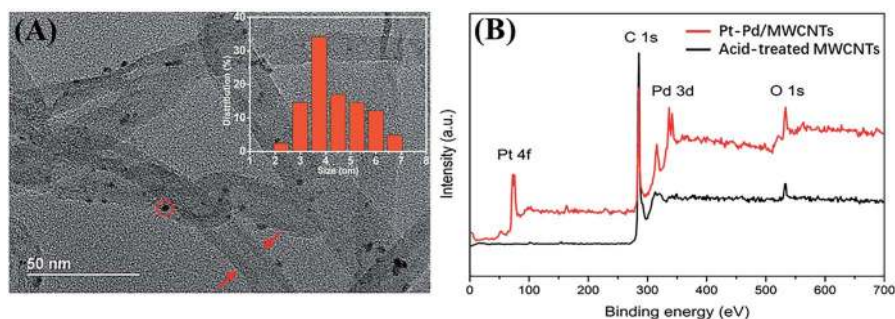


Fig. 5 (A) The TEM photo of Pt–Pd/MWCNTs nanocomposites with the size distribution (inset) of Pt–Pd nanoparticles. (B) The intensity of Pt–Pd/MWCNTs nanocomposites from XPS wide scan.

the glassy carbon electrode for the sensitive detection of hydrogen peroxide.<sup>40</sup> This strategy combines the excellent catalytic ability of platinum–palladium alloy nanoparticles with the outstanding conductivity of carbon nanotubes, enabling a higher detection sensitivity of the sensor.

### Detection of hydrogen peroxide

Many biomarkers such as glucose, sarcosine, and cholesterol can be oxidized to produce  $\text{H}_2\text{O}_2$  which can be quantitatively measured using either electrochemical<sup>40</sup> or colorimetric techniques.<sup>41</sup> The  $\mu\text{AE500}$  modified with Nafion/Pt–Pd/MWCNTs nanocomposites were characterized by assessing their ability in detecting  $\text{H}_2\text{O}_2$  to evaluate the influence of nanocomposite modification on the sensitivity of the detection.

The CV curves of the  $\mu\text{AE500}$ -Nafion/Pt–Pd/MWCNTs are shown in Fig. 6A at different  $\text{H}_2\text{O}_2$  concentrations. The CV curves of the  $\mu\text{AE500}$ -Nafion/Pt–Pd/MWCNTs are shown in Fig. 6A at different  $\text{H}_2\text{O}_2$  concentrations. The  $\mu\text{AE500}$  was modified by  $1 \mu\text{L } 2 \text{ mg mL}^{-1}$  Pt–Pd/MWCNTs nanocomposites. The onset oxidation potential for  $\text{H}_2\text{O}_2$  was about +0.4 V. The oxidation current became maximum at the potential of approximately +0.6 V and maintained an almost constant value when the potential was up to +0.8 V. Therefore, the potential of +0.6 V was chosen as the applied potential in all following experiments. In the absence of  $\text{H}_2\text{O}_2$ , the oxidation current was as low as  $11.5 \mu\text{A}$  (the red solid line). As the concentration of

$\text{H}_2\text{O}_2$  was increased to  $500 \mu\text{M}$  and  $1500 \mu\text{M}$ , the oxidation current increased to about  $18.3 \mu\text{A}$  and  $21.7 \mu\text{A}$ , respectively. This clearly demonstrated the good oxidation ability of the modified electrodes for hydrogen peroxide.

The effect of nanocomposites modification for different electrodes was studied by evaluating the oxidation current in the  $100 \mu\text{M}$   $\text{H}_2\text{O}_2$  solution (Fig. 6B). Regardless of the modification, the oxidation current increased with the increase of the electrode surface area. The oxidation current of modified electrodes was approximately 1.32–2.24 times higher than the same electrode without modification. For example, the response current ( $629.7 \pm 24.9 \text{ nA}$ ) of the modified  $\mu\text{AE500}$  was 2.33 times as big as that ( $270.5 \pm 10.9 \text{ nA}$ ) of the  $\mu\text{AE500}$ . Further, the output current of the modified  $\mu\text{AE500}$  was approximately 8 times that of the planar electrode without modification. Therefore, it can be concluded that both larger surface area enabled by high pillars and the nanocomposite modification contributed to the larger oxidation current.

The influence of the nanocomposite amount ( $1\text{--}8 \text{ mg mL}^{-1}$ ) on detection sensitivity was studied to optimize the electrochemical detection capability of the  $\mu\text{AE500}$ . Fig. S6† depicts the chronoamperometric curves of  $\mu\text{AE500}$ -Nafion/Pt–Pd/MWCNTs and planar electrodes with Nafion/Pt–Pd/MWCNTs in  $\text{H}_2\text{O}_2$  solutions with various concentrations ( $0\text{--}100 \mu\text{M}$ ). A good linear relationship between the current and the  $\text{H}_2\text{O}_2$  concentration was found for all electrodes, regardless of the modification conditions. The slopes of the linear models indicated that the

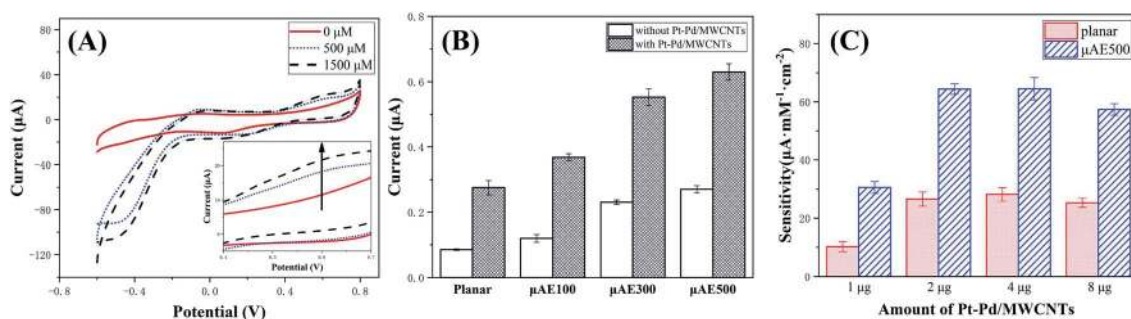


Fig. 6 (A) CV curves of the Nafion/Pt–Pd/MWCNTs/ $\mu\text{AE500}$  electrode in 0, 500, and  $1500 \mu\text{M}$   $\text{H}_2\text{O}_2$  solutions. (B) Oxidation currents of various electrodes with and without modification using Pt–Pd/MWCNTs. (C) Comparison of sensitivity between the planar and  $\mu\text{AE500}$  electrodes coated with 1, 2, 4, or  $8 \mu\text{g}$  Pt–Pd/MWCNTs.



response current of the modified electrodes dramatically increased with the increase of concentration of the nano-materials (in other words, the quantity of nanocomposites coated on the electrodes).

Fig. 6C shows the sensitivity of both the planar and the  $\mu$ AE500. Both the planar and the  $\mu$ AE500 electrodes showed increased sensitivity when the amount of Pt–Pd/MWCNTs coated on the electrodes was increased from 1  $\mu$ g to 4  $\mu$ g. The increase was more pronounced at 1 and 2  $\mu$ g and reached a peak at 4  $\mu$ g. It leveled off from 4  $\mu$ g. At the peak, the sensitivity of the  $\mu$ AE500 is 2.3 times that of the planar electrode. The level-off is related to the agglomeration of the nanomaterial in the small area of the electrode. After agglomeration, the electron transfer process was suppressed due to the reduced contact area,<sup>42</sup> leading to a reduction in the sensitivity. The higher sensitivity of the modified  $\mu$ AE500 is due to the larger surface area of the  $\mu$ AE500, which prevents the agglomeration of the nanomaterial. Additionally, the nanomaterials immobilized on both the top and sidewalls of each pillar probably extend far beyond the diffusion layer of the planar electrode, leading to more and efficient contact with analytes.

Compared to the conventional method of electrodeposition of nanomaterials on the surface of  $\mu$ AEs,<sup>18,19</sup> the drop-cast method to deposit nanomaterials on electrodes was straightforward and flexible. Moreover, the modified  $\mu$ AE500 offered comparable sensitivity ( $64.5 \mu\text{A mM}^{-1} \text{cm}^{-2}$ ) in detecting hydrogen peroxide, compared with the planar electrode modified by the electrodeposition of Ag NPs/GCE<sup>43</sup> ( $32.9 \mu\text{A mM}^{-1} \text{cm}^{-2}$ ), NiHCNFe/ppy/GCE<sup>44</sup> ( $88.33 \mu\text{A mM}^{-1} \text{cm}^{-2}$ ), and Pd NWs/NTs<sup>45</sup> ( $173\text{--}363 \mu\text{A mM}^{-1} \text{cm}^{-2}$ ). These results imply that the  $\mu$ AEs with high micropillars and a large surface area modified by drop-casting nanomaterial have great potential in the development of sensitive and cost-effective electrochemical sensors.

### Detection of sarcosine

The  $\mu$ AE500 modified with Pt–Pd/MWCNTs were employed to detect sarcosine using chronoamperometric (CA) measurement to demonstrate the sensitivity and reliability of the  $\mu$ AEs. The CA measurement was set at a constant potential of 0.6 V (*versus* the reference electrode of AgCl) and the pulse width of 90 s. As

shown in Fig. 7, the absolute value of response current increased proportionally with the increase of sarcosine concentration. The current–concentration curve of sarcosine derived from CA measurements is shown in the inset of Fig. 7. The relationship between current ( $I$ ) and the sarcosine concentration ( $C$ ) can be described by a linear model  $I (\mu\text{A}) = 0.00154 C (\mu\text{M}) + 0.0978$  ( $R^2 = 0.99$ ) when the concentration is in the range of 5–60  $\mu\text{M}$ . The sensitivity was calculated by dividing the slope of the above linear model by the projected area of the electrode. The sensitivity is found to be  $17.1 \mu\text{A mM}^{-1} \text{cm}^{-2}$  with a LOD ( $S/N = 3$ ) of 1.28  $\mu\text{M}$ .

The detection performance of various biosensors for sarcosine is listed in Table S3.† Although different sensors have significantly distinct linear detection ranges and LODs, the  $\mu$ AE in this study has a larger linear range (5–60) but a lower LOD in comparison to the glassy carbon electrodes modified by Pt@ZIF8.<sup>46</sup> Since the current response of  $\mu$ AEs increased with its pillar height/surface area, the  $\mu$ AEs with much higher pillars/surface area will dramatically reduce the LOD.

The sarcosine concentration may vary either from 0 to 5 or from 5 to 60 in different tissues of the healthy and prostate cancer patient, respectively.<sup>47</sup> The concentration of sarcosine higher than 2.67  $\mu\text{M}$  maybe a clear indication of prostate cancer.<sup>48</sup> The LOD (1.28  $\mu\text{M}$ ) of  $\mu$ AE500 for sarcosine detection is much smaller than the cutoff value of  $\mu\text{M}$ . Therefore, the  $\mu$ AE500 in this paper demonstrates its potential in detecting sarcosine from either serum or urine for clinical applications with high sensitivity and reliability.

## Conclusions

This paper reports the facile fabrication, surface modification, and characterization of a PDMS-based micropillar electrode array coated with gold films. The repeated soft lithography of the 3D printed master was employed to manufacture  $\mu$ AEs to dramatically reduce the fabrication cost. Numerical study and experiments showed that the current density of  $\mu$ AEs was proportional to their surface area. Even at a low scan rate,  $\mu$ AEs acquired a much larger current density than the planar electrode. This is favorable for electrochemical detection of low

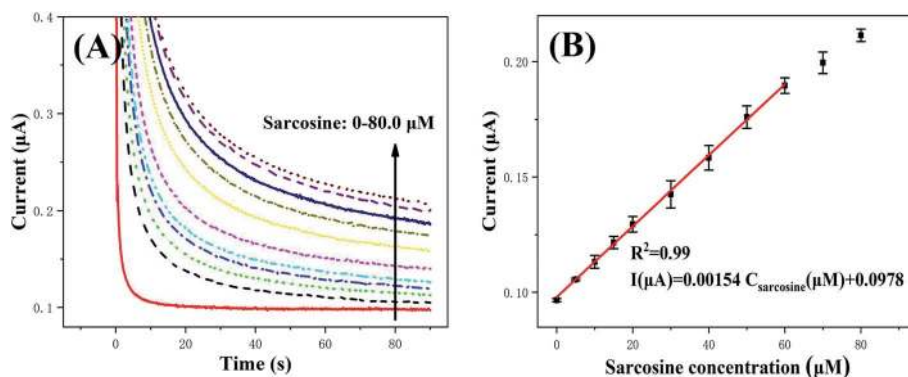


Fig. 7 (A) Chronoamperometric curves of Nafion/SO<sub>x</sub>/Pt–Pd/MWCNTs/ $\mu$ AE500 electrode when the concentration of sarcosine was increased from 0 to 80.0  $\mu\text{M}$  (from bottom to top). (B) Current response at different sarcosine concentrations.





abundance analytes. Moreover,  $\mu$ AEs were coated using home-made platinum–palladium/multi-walled carbon nanotubes (Pt–Pd/MWCNTs) to further enhance detection sensitivity. Hydrogen peroxide and sarcosine were detected to demonstrate the electrochemical performance of Nafion/Pt–Pd/MWCNTs/ $\mu$ AEs. As a result of the larger surface of  $\mu$ AEs and the excellent electrocatalytic performance of the nanocomposite, the output current of the modified  $\mu$ AE500 was approximately 8 times greater than that of the planar electrode without modification. The sensitivity of the Nafion/Pt–Pd/MWCNTs/ $\mu$ AE500 was 1.5 times higher than that of the planar electrode modified at the same condition. The linear detection range, sensitivity and LOD ( $S/N = 3$ ) of the sarcosine biosensors ( $\mu$ AE500) was 5–60  $\mu$ M, 17.1  $\mu$ A  $\text{mM}^{-1} \text{cm}^{-2}$  and 1.28  $\mu$ M, respectively. The outcome of this study is significant for the design and application of the  $\mu$ AEs in electrochemical detection of biomarkers.

## Conflicts of interest

There are no conflicts to declare.

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