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Digital Holographic Multimodal Cross-Sectional Fluorescence and Quantitative Phase Imaging System

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We present a multimodal imaging system based on simple off-axis digital holography, for simultaneous recording and retrieval of cross-sectional fluorescence and quantitative phase imaging of the biological specimen. Synergism in the imaging capabilities can be achieved by incorporating two off-axis digital holographic microscopes integrated to record different information at the same time. The cross-sectional fluorescence imaging is realized by a common-path configuration of the single-shot off-axis incoherent digital holographic system. The quantitative phase imaging, on the other hand, is achieved by another off-axis coherent digital holographic microscopy operating in transmission mode. The fundamental characteristics of the proposed multimodal system are confirmed by performing various experiments on fluorescent beads and fluorescent protein-labeled living cells of the moss *Physcomitrella patens* lying at different axial depth positions. Furthermore, the cross-sectional live fluorescence and phase imaging of the fluorescent beads are demonstrated by the proposed multimodal system. The experimental results presented here corroborate the feasibility of the proposed system and indicate its potential in the applications to analyze the functional and structural behavior of biological cells and tissues.

Over the past decade, multimodal systems based on quantitative phase imaging in combination with fluorescence imaging have been developed considerably due to its several advantages^{1–12}. The phase imaging reveals the structural information by exploiting the optical path-length shifts through the biological specimen, while fluorescence imaging provides functional details of the specific molecules of interest in the biological specimen. Therefore, a hybrid multimodal imaging system comprising both these systems offers to precisely visualize and delineate structural and functional information in the biological specimen on a single platform at the same time.

The quantitative phase imaging technique^{13–16} is an emerging powerful technology of a new paradigm in general imaging and biomedical applications that provides quantitative information including the structure and dynamics of the transparent specimens, which is not easily obtained with the conventional optical imaging techniques. The technique employs the principle of optical interferometry to measure the optical field (i.e. amplitude and phase information). In recent years, quantitative phase imaging has received substantial interest and opened the door for quantifying dynamic structural information of biological cells with nanoscale sensitivity. Popescu *et al.*¹⁷ reported the use of phase imaging for monitoring cell growth, characterizing cellular motility, and investigating the subcellular motions of living cells. The technique has also found applications for various investigations of cells and tissues including measurement of 3D profiling and tracking¹⁵, refractive index¹⁸, spectral dispersion¹⁹, optical path length²⁰, dry mass localization²¹, and optimum focus determinations²², etc.

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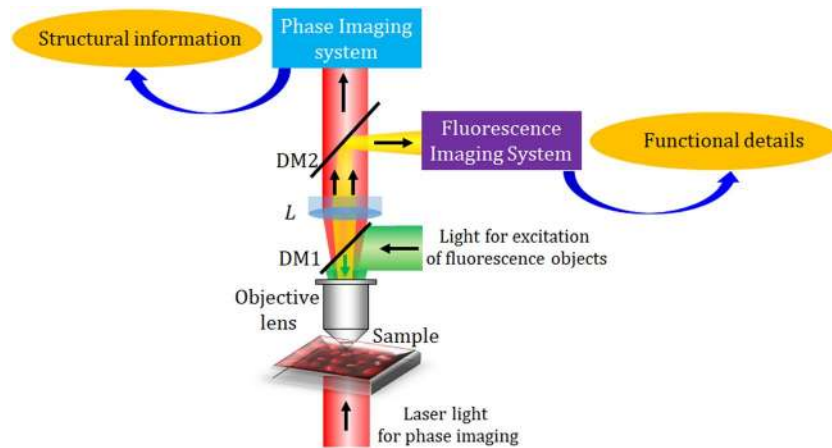


Figure 1. Schematic of the proposed multimodal system for recording off-axis fluorescence and phase digital holography.

In order to study the functional information of a biological sample including cellular and microbiological investigations, fluorescence microscopy is a crucial technique. This technique has been investigated for the study of microbiological processes^{23,24}, cellular and molecular identification^{25–27}, and rapid detection and diagnosis²⁸. Since fluorescence is the most important source of enhancing contrast in biological imaging and the fluorescence images can be acquired from a sample labeled with fluorophores that encode the molecular specificity of the specimen. Most fluorescence imaging techniques involve sectioning, such as laser scanning confocal microscopy^{29,30} or spinning disk confocal microscopy³¹, which are time-consuming processes to obtain images of the 3D field. Further, efforts of adopting digital holography to fluorescence microscopy have been realized. However, these efforts make the system more complicated and the whole process becomes time-consuming^{32,33}. Recently, holographic fluorescence microscopy has been possible due to the advent of Fresnel incoherent correlation holography (FINCH)^{34–37}, as fluorescence light is naturally incoherent³⁸. FINCH is based on the self-interference principle stated that two or more beams originating from the same source point are mutually coherent and interfere to form the in-line digital hologram³⁷. In FINCH, the incident wave originated from each object point is allowed to split into two waves with different curvatures by using an appropriate optical component (say an appropriate pattern, e.g., a grating pattern, displayed on a spatial light modulator) and an interference pattern is produced by the recombination of these waves at an appropriate overlapped region in the image sensor. The continuous progress in the field of FINCH promises new applications. However, FINCH is an inline-holography and thus the phase-shifting method is required to reduce unwanted terms such as DC and conjugated term. In this line of research, we have proposed a single-shot common-path off-axis FINCH system^{39,40} for imaging of biological samples. This configuration of modified FINCH called common-path off-axis incoherent digital holography is accomplished by embedding a focusing lens with a diffraction grating onto a phase-mode spatial light modulator (SLM) to generate two slightly different wavefronts and different propagation directions to form a digital hologram at the image sensor.

A combination of holographic fluorescence microscopy with quantitative phase imaging to obtain the fluorescence and the phase information will open up new possibilities of an exciting frontier to extract more information about the targeted biological specimen. Recently, we have proposed a multimodal imaging system by incorporating the common-path configurations of both the digital holographic microscopes, for simultaneous recording and retrieval of 3D fluorescence and phase imaging of a biological specimen⁴⁰. This system is very stable due to the common-path geometry for both the fluorescence and phase imaging. In the phase imaging, however, it is not easy to control the fringe frequency of the off-axis hologram to create a tilted plane reference wave via the transmittance through a pinhole. The intensity ratio between the object and the reference waves could not be controlled. This degrades the ability of quantitative phase imaging. In this paper, a multimodal digital holographic system is developed by comprising the common-path incoherent digital holographic microscope, for retrieving the 3D fluorescence imaging, with the two-arm off-axis coherent digital holographic microscope, for retrieving the phase imaging. In this configuration, the two-arm off-axis coherent digital holographic microscope implementation is easily installed in the multimodal digital holographic system. This is the first paper, to our best knowledge, that evaluates the quantitative phase accuracy in the multimodal digital holographic microscopes as well as dynamic phase measurement of floating fluorescence beads in the 3D field. The multimodal system could, indeed, have the capability to provide high-contrast functional imaging along with structural details of the biological specimen on a common platform from which it is possible to extract important intrinsic biophysical parameters. The present system has the ability not only to provide the 2D (x, y) information but also depth information (z -direction) of the fluorescent objects in a single-shot without scanning. It should be noted that the incoherent digital holographic system provides good imaging results for sparse objects and the technique is capable of retrieval cross-sectional information for the objects separated by an axial depth of about 250 micrometers.

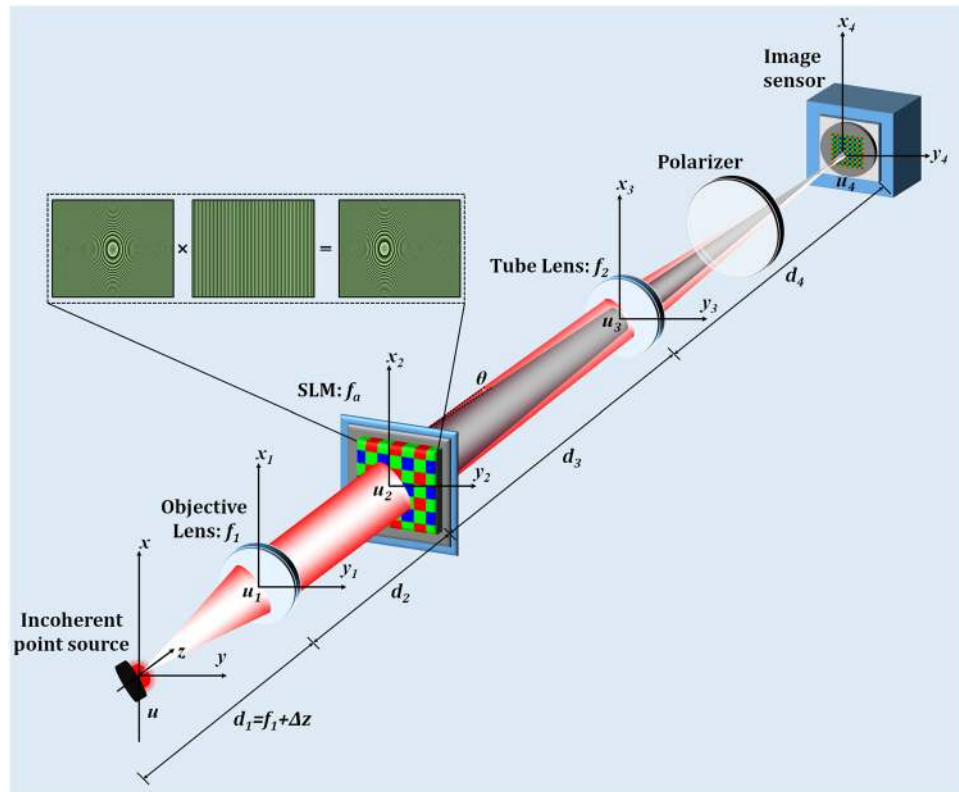


Figure 2. Schematic of the common-path off-axis incoherent digital holographic setup. Top panels indicate the phase pattern displayed on the SLM.

Methodology

In this work, we have presented a common-path off-axis incoherent digital holographic microscope integrated with another off-axis coherent digital holographic microscope for simultaneous measurement of cross-sectional fluorescence imaging and quantitative phase of fluorescent objects. The schematic presentation of the proposed multimodal system is depicted in Fig. 1, where the multimodal system allowing to retrieve simultaneously the structural information by the phase imaging system and the functional details by the fluorescence imaging system of the specimen under study. In the following subsections, the descriptions of both the systems are presented.

Common-path off-axis incoherent digital holography for cross-sectional fluorescence imaging.

Figure 2 shows the schematic of the single-shot common-path off-axis incoherent digital holographic microscope. The system is accomplished by embedding a focusing lens with a diffraction grating onto a phase-mode spatial light modulator (SLM) which splits the incident fluorescent light from the fluorescent object into two light waves with slightly different propagation directions in order to achieve off-axis interference. These two wavefronts interfered at the image sensor plane and form a fluorescent digital hologram.

The mathematical description of the proposed setup, by considering the one-dimensional case, is as follows. Here, we assume that the point source is located at $(x_0, 0, -\Delta z)$. The optical wavefield by a point source $\delta(x-x_0)$ obtained by the Fresnel propagation from x plane to x_1 plane with a distance of $d_1 (=f_1 + \Delta z)$ is described as

$$u_1(x_1) = \int_{-\infty}^{\infty} \delta(x - x_0) \exp\left[i\frac{\pi}{\lambda d_1}(x_1 - x)^2\right] dx = \exp\left[i\frac{\pi}{\lambda d_1}(x_1 - x_0)^2\right] \tag{1}$$

where, δ is the Dirac delta function. Then, a lens function with a focal length of f_1 is multiplied

$$u_{11}(x_1) = \exp\left[i\frac{\pi}{\lambda d_1}(x_1 - x_0)^2\right] \exp\left[-i\frac{\pi}{\lambda f_1}x_1^2\right] = a \exp\left[-i\frac{2\pi}{\lambda d_1}x_0 x_1\right] \exp\left[i\frac{\pi}{\lambda d_{11}}x_1^2\right] \tag{2}$$

where

$$\frac{1}{d_{11}} = \frac{1}{d_1} - \frac{1}{f_1}; \quad a = \exp\left[i\frac{\pi}{\lambda d_1}x_0^2\right] \tag{3}$$

Another Fresnel propagation from x_1 plane to x_2 plane is described as

$$\begin{aligned}
 u_2(x_2) &= a \int_{-\infty}^{\infty} \exp\left(-i\frac{2\pi}{\lambda d_1} x_0 x_1\right) \exp\left(i\frac{\pi}{\lambda d_{11}} x_1^2\right) \exp\left[i\frac{\pi}{\lambda d_2} (x_2 - x_1)^2\right] dx_1 \\
 &= a_1 \exp\left(-i\frac{2\pi}{\lambda} \frac{d_{21}}{d_1 d_2} x_0 x_2\right) \exp\left(i\frac{\pi}{\lambda d_{22}} x_2^2\right)
 \end{aligned} \tag{4}$$

where

$$\begin{aligned}
 \frac{1}{d_{21}} &= \frac{1}{d_{11}} + \frac{1}{d_2}; \quad \frac{1}{d_{22}} = \frac{1}{d_2} - \frac{d_{21}}{d_2^2}; \quad \text{or } d_{22} = d_2 + d_{11}; \\
 a_1 &= \exp\left(i\frac{\pi}{\lambda d_1} x_0^2\right) \exp\left(-i\frac{\pi d_{21}}{\lambda d_1^2} x_0^2\right) = \exp\left[i\frac{\pi}{\lambda} \left(\frac{1}{d_1} - \frac{d_{21}}{d_1^2}\right) x_0^2\right]
 \end{aligned} \tag{5}$$

At SLM (x_2 plane), the object light is multiplied by a diffraction grating and a lens function with a focal length of f_a in a phase-mode SLM.

$$\begin{aligned}
 u_{21}(x_2) &= a_1 \exp\left(-i\frac{2\pi}{\lambda} \frac{d_{21}}{d_1 d_2} x_0 x_2\right) \exp\left(i\frac{\pi}{\lambda d_{22}} x_2^2\right) \exp\left(-i\frac{\pi}{\lambda f_a} x_2^2\right) \exp\left(i\frac{2\pi}{\lambda} \sin\theta x_2\right) \\
 &= a_1 \exp\left[-i\frac{2\pi}{\lambda} \left(\frac{x_0}{d_t} - \sin\theta\right) x_2\right] \exp\left(i\frac{\pi}{\lambda d_{23}} x_2^2\right)
 \end{aligned} \tag{6}$$

where

$$\frac{1}{d_t} = \frac{d_{21}}{d_1 d_2}; \quad \text{or } d_t = \frac{d_1(d_{11} + d_2)}{d_{11}}; \quad \frac{1}{d_{23}} = \frac{1}{d_{22}} - \frac{1}{f_a} \tag{7}$$

Another Fresnel propagation from x_2 plane to x_3 plane is implemented.

$$\begin{aligned}
 u_3(x_3) &= a_1 \int_{-\infty}^{\infty} \exp\left[-i\frac{2\pi}{\lambda} \left(\frac{x_0}{d_t} - \sin\theta\right) x_2\right] \exp\left(i\frac{\pi}{\lambda d_{23}} x_2^2\right) \exp\left[i\frac{\pi}{\lambda d_3} (x_3 - x_2)^2\right] dx_2 \\
 &= a_2 \exp\left(i\frac{\pi}{\lambda d_{32}} x_3^2\right) \exp\left[-i\frac{2\pi}{\lambda d_{t1}} (x_0 - d_t \sin\theta) x_3\right]
 \end{aligned} \tag{8}$$

where

$$\begin{aligned}
 \frac{1}{d_{31}} &= \frac{1}{d_{23}} + \frac{1}{d_3}; \quad \frac{1}{d_{32}} \\
 &= \frac{1}{d_3} - \frac{d_{31}}{d_3^2}; \quad \text{or } d_{32} \\
 &= d_3 + d_{23}; \quad \frac{1}{d_{t1}} \\
 &= \frac{d_{31}}{d_t d_3} \text{ or } d_{t1} \\
 &= \frac{d_1(d_2 + d_{11})(d_3 + d_{23})}{d_{23} d_{11}}; \quad \text{or} \\
 a_2 &= a_1 \exp\left[-i\frac{\pi d_{31}}{\lambda} \left(\frac{x_0}{d_t} - \sin\theta\right)\right]^2 = \exp\left\{i\frac{\pi}{\lambda} \left[\left(\frac{1}{d_1} - \frac{d_{21}}{d_{11}^2}\right) x_0^2 - d_{31} \left(\frac{x_0}{d_t} - \sin\theta\right)\right]^2\right\}
 \end{aligned} \tag{9}$$

The object wave is multiplying by a lens function with a focal length of f_2

$$\begin{aligned}
 u_{31}(x_3) &= a_2 \exp\left(i\frac{\pi}{\lambda d_{32}} x_3^2\right) \exp\left[-i\frac{2\pi}{\lambda d_{t1}} (x_0 - d_t \sin\theta) x_3\right] \exp\left(-i\frac{\pi}{\lambda f_2} x_3^2\right) \\
 &= a_2 \exp\left(i\frac{\pi}{\lambda d_{41}} x_3^2\right) \exp\left[-i\frac{2\pi}{\lambda d_{t1}} (x_0 - d_t \sin\theta) x_3\right]
 \end{aligned} \tag{10}$$

where

$$\frac{1}{d_{41}} = \frac{1}{d_{32}} - \frac{1}{f_2} \quad (11)$$

The Fresnel propagation from x_3 plane to x_4 plane is obtained as

$$\begin{aligned} u(x; \sin \theta, f_a) &= a_2 \int_{-\infty}^{\infty} \exp\left(i \frac{\pi}{\lambda d_{41}} x_3^2\right) \exp\left[-i \frac{2\pi}{\lambda d_{t1}} (x_0 - d_t \sin \theta) x_3\right] \exp \\ &\quad \left[i \frac{\pi}{\lambda d_4} (x_4 - x_3)^2\right] dx_3 \\ &= a_3 \exp\left[-i \frac{2\pi}{\lambda} d_{52} \left(\frac{d_{11}}{d_1} \frac{x_0}{d_2 + d_{11}} - \sin \theta\right) x_4\right] \exp\left(i \frac{\pi}{\lambda d_{51}} x_4^2\right) \end{aligned} \quad (12)$$

where

$$\begin{aligned} \frac{1}{d_{42}} &= \frac{1}{d_{41}} + \frac{1}{d_4}; \quad \frac{1}{d_{51}} = \frac{1}{d_4} - \frac{d_{42}}{d_4^2}; \quad \text{or } d_{51} = d_4 + d_{41} = d_4 + \frac{f_2(d_3 + d_{23})}{f_2 - d_3 - d_{23}} \\ d_{52} &= \frac{d_{42}d_{31}}{d_4d_3} = \frac{d_{23}(d_{51} - d_4)}{d_{51}(d_3 + d_{23})} = \frac{f_2d_{23}}{(f_2 - d_4)(d_{23} + d_3) + d_4f_2}; \quad d_{23} = \frac{(d_2 + d_{11})f_a}{f_a - d_2 - d_{11}} \\ a_3 &= \exp\left\{i \frac{\pi}{\lambda} \left[\left(\frac{1}{d_1} - \frac{d_{21}}{d_1^2}\right) x_0^2 - d_{31} \left(\frac{x_0}{d_t} - \sin \theta\right)^2 - d_{42} \frac{1}{d_{t1}^2} (x_0 - d_t \sin \theta)^2\right]\right\} \end{aligned} \quad (13)$$

Equation (12) represents the modulated light wave obtained by the phase pattern (lens function and grating) displayed on to the SLM. The unmodulated light wave reaching at the image sensor is obtained from Eq. (12), by setting $f_a = \infty$ and $\theta = 0$, as

$$u(x; 0, \infty) = a'_3 \exp\left[-i \frac{2\pi}{\lambda} d'_{52} \left(\frac{d_{11}}{d_1} \frac{x_0}{d_2 + d_{11}}\right) x_4\right] \exp\left(i \frac{\pi}{\lambda d'_{51}} x_4^2\right) \quad (14)$$

where

$$\begin{aligned} a'_3 &= \exp\left[i \frac{\pi}{\lambda} \left(\frac{1}{d_1} - \frac{d_{21}}{d_1^2} - \frac{d'_{31}}{d_t^2} - \frac{d'_{42}}{d_{t1}^2}\right) x_0^2\right] \\ d'_{42} &= \frac{d_4d'_{41}}{d_4 + d'_{41}}; \quad d'_{41} = \frac{f_2d'_{32}}{f_2 - d'_{32}}; \quad d'_{32} = d_3 + d_{22}; \quad d'_{31} = \frac{d_3d_{22}}{d_{22} + d_3}; \quad d'_{t1} = \frac{d_t d_3}{d'_{31}} \end{aligned} \quad (15)$$

The interference of the modulated and unmodulated light waves is carried out at the faceplate of the image sensor with the help of a linear polarizer. The hologram intensity recorded by the image sensor is represented by

$$\begin{aligned} I(x) &= |u(x; 0, \infty) + u(x; \sin \theta, f_a)|^2 \\ &= 2 \\ &\quad + 2 \operatorname{Re} \left\{ a'_3 a_3^* \exp\left[-i \frac{2\pi}{\lambda} \left[\left(d_{52} - d'_{52}\right) \left(\frac{d_{11}}{d_1} \frac{x_0}{d_{22}}\right) - d_{52} \sin \theta\right] x_4\right] \exp \right. \\ &\quad \left. \left[i \frac{\pi}{\lambda} \left(\frac{1}{d_{51}} - \frac{1}{d'_{52}}\right) x_4^2\right]\right\} \end{aligned} \quad (16)$$

where

$$d'_{51} = d_4 + \frac{f_2(d_3 + d_{22})}{f_2 - d_3 - d_{22}}; \quad d'_{52} = \frac{f_2 d_{22}}{(f_2 - d_4)(d_{22} + d_3) + d_4 f_2} \quad (17)$$

When there are numbers of incoherent point sources, the hologram intensity distributions described by Eq. (16) are superimposed. From the recorded hologram, the cross-sectional intensity distribution of the object can be obtained by using the Fresnel propagation algorithm.

Coherent digital holography for cross-sectional quantitative phase imaging. The cross-sectional quantitative phase imaging is accomplished by the off-axis digital holography with a transmission-type

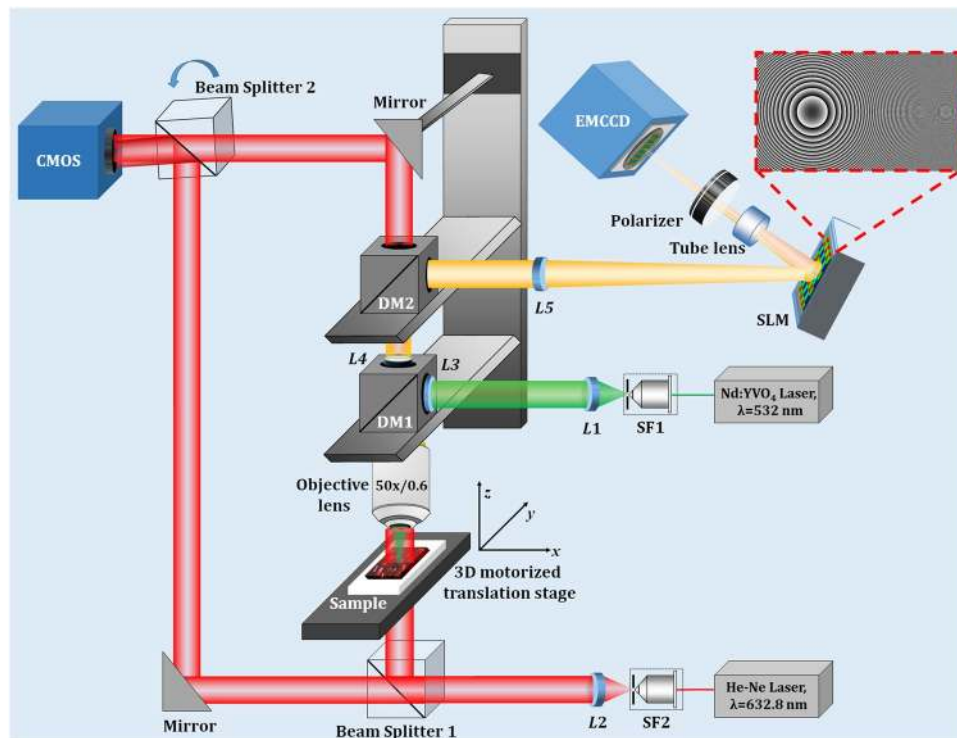


Figure 3. Optical schematic of the proposed multimodal system for the measurement of the cross-sectional fluorescence and the quantitative phase imaging of the specimen.

configuration, which captures the complex wavefront of the targeted sample without disturbing its physiological condition. The detailed description can be obtained in various papers^{4,13–16}. In brief, the off-axis digital holographic microscope is based on the Mach-Zehnder interferometer, in which the coherent laser light source is spatially filtered, collimated, and then divided into the object and reference beams by using a beam splitter. The object beam trans-illuminates the specimen under observation and is collected by the microscope objective, and is magnified by a tube lens. The object beam is allowed to interfere with the reference beam with the use of another beam splitter. The off-axis configuration is created by inducing a small angle between the object wave and the reference plane wave. The phase distribution from the recorded digital hologram is numerically reconstructed after the Fresnel propagation algorithm to the focused plane. Two holograms with and without the specimen are recorded to nullify the aberrations and to obtain the phase distribution of the specimen. This phase distribution corresponding to the specimen is determined by reconstructing both the holograms individually and subtracting their phases.

Experiments and Discussion

Figure 3 shows the schematic of the proposed multimodal system with one incoherent digital holographic microscopy and another coherent digital holographic microscopy, working simultaneously for the measurement of the cross-sectional fluorescence imaging and the quantitative phase imaging, respectively. The incoherent digital holographic microscopy system first uses an Nd:YVO₄ laser (wavelength, $\lambda = 532$ nm) as a light source. The laser beam is expanded and filtered using a spatial filter assembly (SF1) and collimated using a collimator (L1). This collimated beam, after reflected from a dichroic mirror (DM1, Thorlabs, DMLP567R) entered into the microscope objective (Nikon CF160 TU Plan Epi ELWD, $50\times/0.60$). The incident light excites the fluorescent beads of size $\sim 10\text{--}14\ \mu\text{m}$ (mean size = $10.4\ \mu\text{m}$, Spherotech Inc.) in an epi-illumination configuration. The fluorescent beads emit the yellow fluorescence with wavelengths ranging from 550 nm to 600 nm. This fluorescent light travels back through the microscope objective, transmits through DM1 and is reflected from another dichroic mirror, DM2 (Thorlabs, DMLP605R). The Fourier transform of the object beam located at the focused plane of the objective lens is projected onto the plane of the phase-mode SLM (Holoeye Pluto, 1920×1080 pixels, $8\ \mu\text{m}$ pixel pitch, phase-only modulation) by a $4f$ relay system ($L4 \rightarrow L5$). Here, the back focal plane of the objective lens is imaged on the phase-mode SLM. A lens function with focal length, $f_a = 800$ mm and a diffraction grating function with grating period $d_h = 300\ \mu\text{m}$ were displayed onto the SLM which generates two distinct wavefronts at respective angles of the incident beam. These two wavefronts are then imaged by a tube lens and allowed to interfere on to the faceplate of the Electron Multiplying charge-coupled device (EMCCD) sensor (Model-iXon 888, sensor format: 1024×1024 pixels, pixel size of $13\ \mu\text{m}$, sensor diagonal of 18.8 mm) and hence form a fluorescent digital hologram. A linear polarizer is placed before the EMCCD sensor to allow the interference of two beams. A band-pass filter centered at $575\ \text{nm} \pm 12.5\ \text{nm}$ was placed in front of an EMCCD sensor in order to improve the fringe visibility of the holograms.

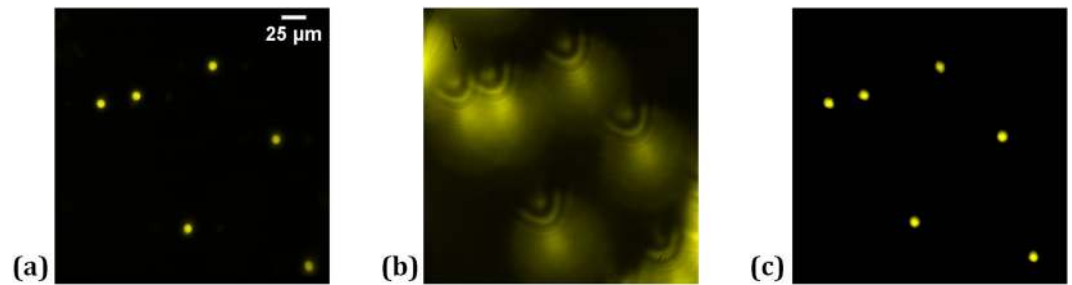


Figure 4. Experimental results of incoherent digital holographic microscopy: (a) original focused image of the fluorescent beads, (b) corresponding digital hologram obtained by moving the beads by $80\ \mu\text{m}$ along the z -direction, and (c) reconstructed image of the fluorescent beads.

The phase imaging is realized by the coherent digital holographic microscopy working in the transmission-type configuration, in which a He-Ne laser ($\lambda = 632.8\ \text{nm}$) is used as an illumination light source. The laser beam is expanded and filtered spatially by a spatial filter (SF2) and collimated by a collimator (L2). The collimated laser beam is divided by a beam splitter into two beams: one is the object beam, which trans-illuminates the specimen under study and another is the reference beam. The object beam, after trans-illuminate the specimen, is collected by the microscope objective and collimated by L4. The DMs are selected in such a way that the object beam passes through both of them. The object and reference beams are combined at the image sensor plane with the help of another beam splitter, tilted slightly to achieve the off-axis configuration. Note that it is not necessary to put the object beam in the image plane of the image sensor because the digital holographic reconstruction can focus on any plane by changing the propagation distance. The interference pattern is recorded by a CMOS camera (Sony Pregius IMX 249, sensor format: 1920×1200 pixels, pixel size of $5.86\ \mu\text{m}$). In this case, two holograms are recorded: one in the presence of the specimen and another without the specimen. This is because the resultant noise caused by the imperfection of the collimated beams and some aberrations of optical elements can be decreased or eliminated.

The performance of the proposed multimodal system was verified by executing various experiments on the fluorescent beads and fluorescent protein-labeled living plant cells. In the first experiment, fluorescent beads, placed on the glass plate mounted on 3D motorized translation stage, are imaged by incoherent digital holographic microscopy, as shown in Fig. 4(a). Afterward, the glass plate is moved in the z -direction by $80\ \mu\text{m}$. A fluorescent digital hologram, as shown in Fig. 4(b), is recorded by projecting a lens function with focal length, $f_a = 800\ \text{mm}$ and a diffraction grating function with grating period $d_h = 300\ \mu\text{m}$ on to the SLM. Pseudocolor according to the central wavelength of the fluorescent light is put on by digital processing. Figure 4(c) shows the reconstructed image of the fluorescent beads retrieved from the recorded digital hologram by the Fresnel propagation algorithm at the reconstruction distance $1020\ \text{mm}$.

At the same time, the phase microscopic system is also working. Figure 5 shows the phase imaging system's capabilities by imaging the same fluorescent beads. In this system, two digital holograms are acquired corresponding to the object and without the object. After processing, the quantitative phase image is reconstructed. Figure 5(a) shows the recorded digital hologram in the presence of the fluorescent beads and the reconstructed wrapped phase image of the fluorescent beads is shown in Fig. 5(b). The unwrapped phase map ($\Delta\varphi$) is obtained by using the PUMA phase unwrapping algorithm⁴¹ and the thickness is measured as, thickness, $h = \frac{\Delta\varphi \times \lambda}{2\pi\Delta n}$, where $\Delta n = n_s - n_m$ with n_s and n_m are the refractive indices of the sample and medium, respectively. Figure 5(c) shows the 2D thickness map of the fluorescent beads and Fig. 5(d) shows the pseudo-3D thickness profile of a selected bead. From Fig. 5(b), we successfully measured the bead size ($\sim 10\ \mu\text{m}$ in diameter) along x -, y -, and z -axes. In Fig. 5(b), five beads are clearly seen. This is the phase imaging results of the same fluorescent beads whose fluorescent imaging results are obtained by the fluorescence digital holography and shown in Figs. 4(a,c).

We experimentally demonstrate the cross-sectional fluorescence and phase imaging capability of the proposed multimodal system on fluorescent protein-labeled living plant cells. In this experiment, we used the protonemata, the hypha-like structure of the moss *Physcomitrella patens* (*Physcomitrella*), a photograph of which is shown in Fig. 6(a). *Physcomitrella* is one of the model organisms for molecular, cellular, and developmental biology, due to its sequenced genome, clear cell identity, and compact body size⁴². We thus chose *Physcomitrella* as the target object of the experiments. We used a transgenic *Physcomitrella*, where the nuclei are labeled with Citrine Yellow fluorescent protein^{40,43}.

A blue laser ($\lambda = 473\ \text{nm}$) is used for excitation of the nuclei labeled with fluorescent proteins. Figure 6(b) shows the fluorescence image of the nuclei of the living plant cells which are distributed in 3D space where nuclei numbered 1–4 are in-focus, nuclei 5 and 6 are out-of-focus by around $10\ \mu\text{m}$ and nucleus 7 is out-of-focus by around $25\ \mu\text{m}$ with respect to the plane of nuclei 1–4, respectively. Figure 6(b) shows the limitation of the conventional full-field fluorescence microscope because it is impossible to obtain all focused images when the plant structure is not flat. By using the proposed common-path off-axis incoherent digital holographic microscope, all focused images to the nuclei can be obtained from one hologram by the numerical wave propagation. Focused position can be determined automatically by evaluating the sharp edge or other criteria. The focused plane corresponding to nuclei 1–4 is moved by $60\ \mu\text{m}$ in the z -direction and a hologram is recorded, as shown in Fig. 6(c), by projecting a lens function (with a focal length of $800\ \text{mm}$) and a diffraction grating function (with a grating

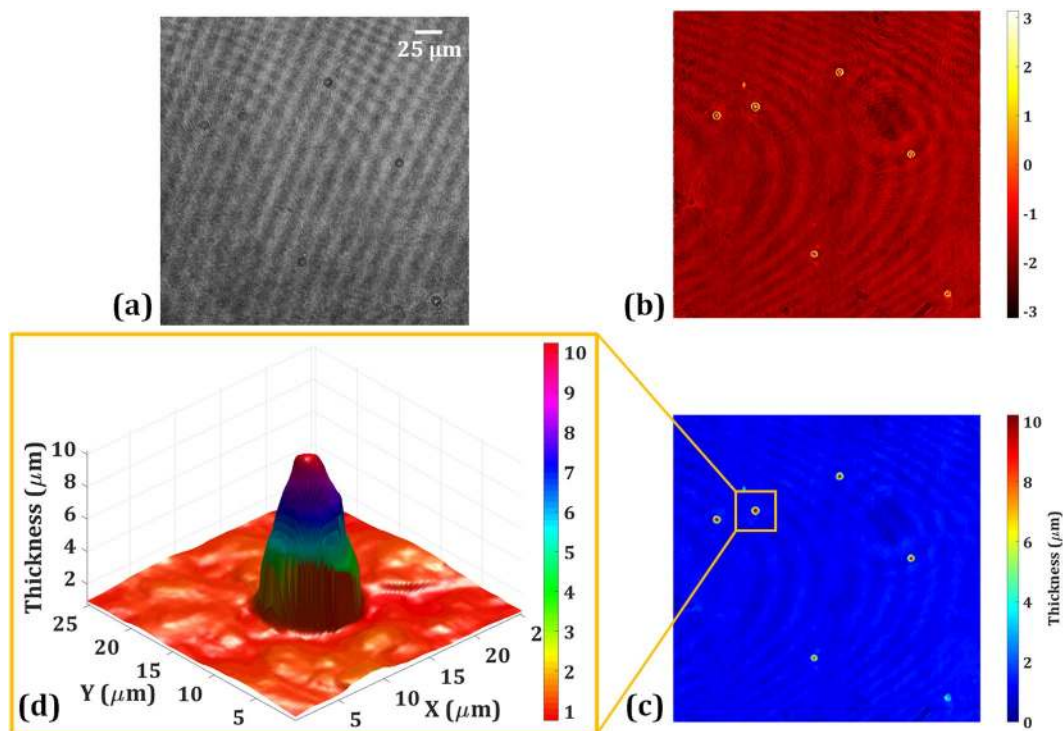


Figure 5. Experimental results of quantitative phase imaging: (a) recorded phase hologram in the presence of the fluorescent beads, (b) the wrapped phase image, (c) thickness map, and (d) pseudo-3D thickness profile of the selected bead.

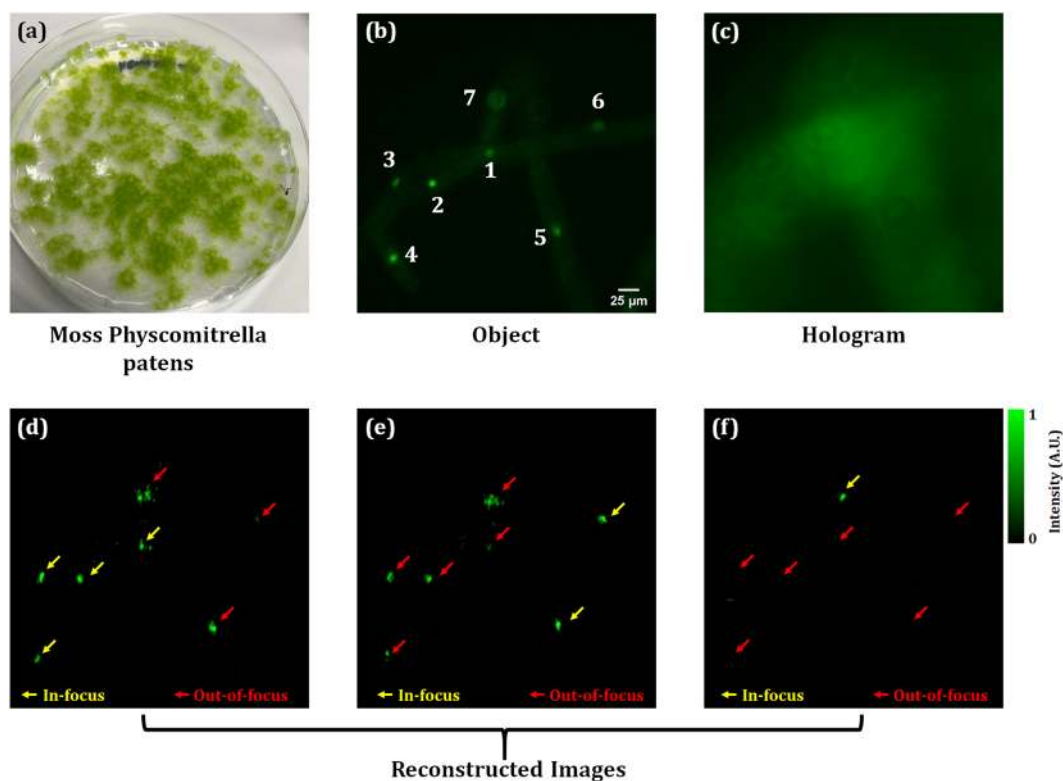
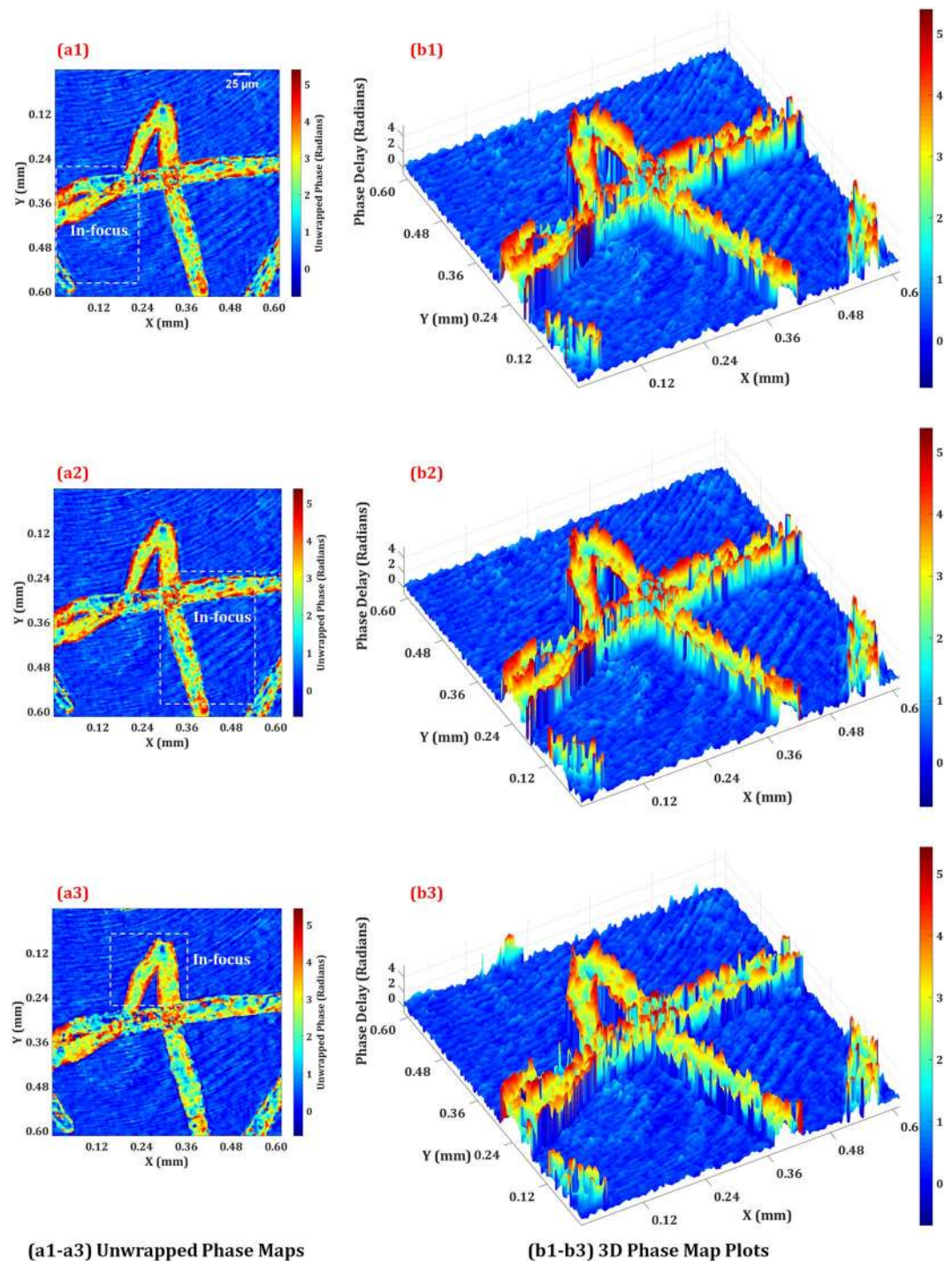


Figure 6. Cross-sectional fluorescence imaging results of living cells of *Physcomitrella*: (a) the photograph of the plant cells, (b) the fluorescent image of fluorescent protein-labeled nuclei, (c) recorded fluorescent hologram, (d–f) the reconstructed images focused on the nuclei in different planes obtained by Fresnel propagation algorithm from the same recorded fluorescent hologram shown in (c). The yellow arrows indicate the in-focus nuclei and the red arrows indicate the out-of-focus nuclei.



(a1-a3) Unwrapped Phase Maps

(b1-b3) 3D Phase Map Plots

Figure 7. Quantitative phase imaging results of the plant cells: the obtained 2D unwrapped phase maps (**a1–a3**) and corresponding 3D phase plots (**b1–b3**) of the plant cells for the three focused planes corresponding to Figs. 6(d–f) obtained by the Fresnel propagation algorithm from the recorded phase hologram. The dotted rectangular in 2D unwrapped phase maps represent the focused regions.

period of $300\ \mu\text{m}$) on to the SLM. Figures 6(d–f) show the reconstructed images focused on each nucleus of the plant cells obtained by Fresnel propagation algorithm (in MatLab 2017Rb) at distances 680 mm, 810 mm, and 1050 mm, which are corresponding to $60\ \mu\text{m}$, $70\ \mu\text{m}$, and $85\ \mu\text{m}$, respectively, in the object space.

Figures 7(a,b) show the quantitative phase imaging results of the same plant cells where Figs. 7(a1–a3) show the unwrapped 2D phase maps of the three focused planes of the plant cells and their corresponding 3D phase map plots are shown in Figs. 7(b1–b3). The dotted rectangular in 2D unwrapped phase maps of Figs. 7(a1–a3) represent the focused regions. The reconstruction distance differences between the three planes along the depth directions are 3.5 mm and 11.6 mm which are equivalent to $10\ \mu\text{m}$ and $25\ \mu\text{m}$, respectively, in the object domain.

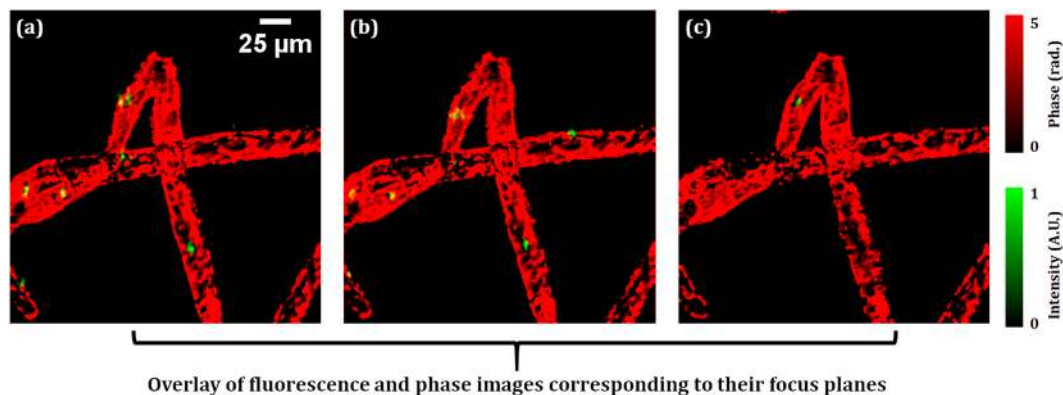


Figure 8. (a–c) the overlay of the focused fluorescence images of Figs. 6 (d–f) and corresponding phase images of Figs. 7(a1–a3).

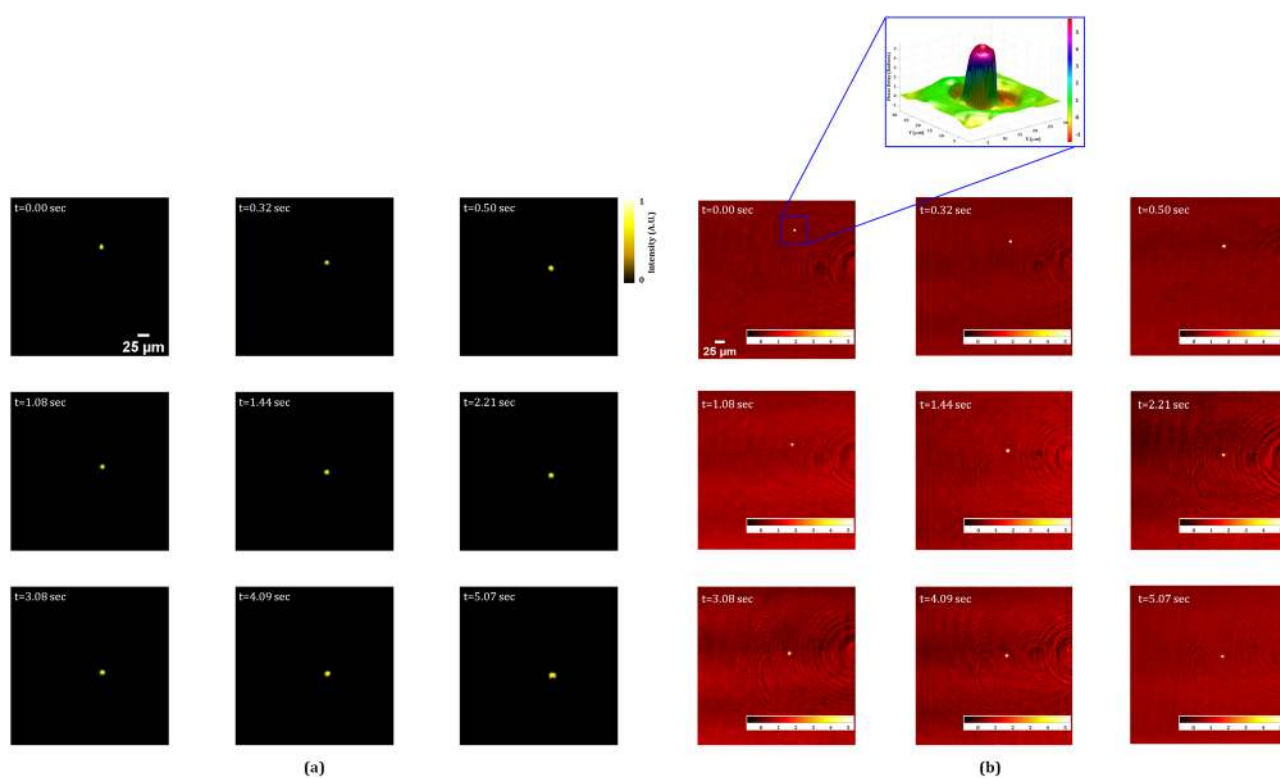


Figure 9. Live fluorescence and phase imaging reconstructions: (a) fluorescence images and (b) phase images, of a fluorescent bead (inset shows the pseudo-3D phase plot of the bead). Also see Visualization 1 (fluorescence hologram), Visualization 2 (reconstructed fluorescence movie), Visualization 3 (phase hologram), and Visualization 4 (reconstructed unwrapped phase map).

The obtained unwrapped phase images show the phase shifts are in a range of 0–5 radians. When we assume that the refractive index of the plant cell is 1.36^{44,45}, the thickness of the cell is about 17 μm. The obtained thickness is in an appropriate range. There are inhomogeneous phase distributions in the plant cell because of the nucleus and many chloroplasts.

Figures 8(a–c) show the overlays of the focused fluorescence images and the corresponding unwrapped phase images of the plant cells. From both observations of the fluorescence and phase, the 3D position of the nucleus with the quantitative phase can be retrieved with a single shot. These results show the high potential of our system to observe the 3D behavior of live cells in a single-shot measurement.

Furthermore, the multimodal system is applied for the live fluorescence and phase imaging of the moving fluorescent bead in a volume. Figure 9(a) shows the reconstructed fluorescence imaging of moving bead, at progressive time intervals, retrieved from the digital fluorescence holograms recorded by the incoherent digital

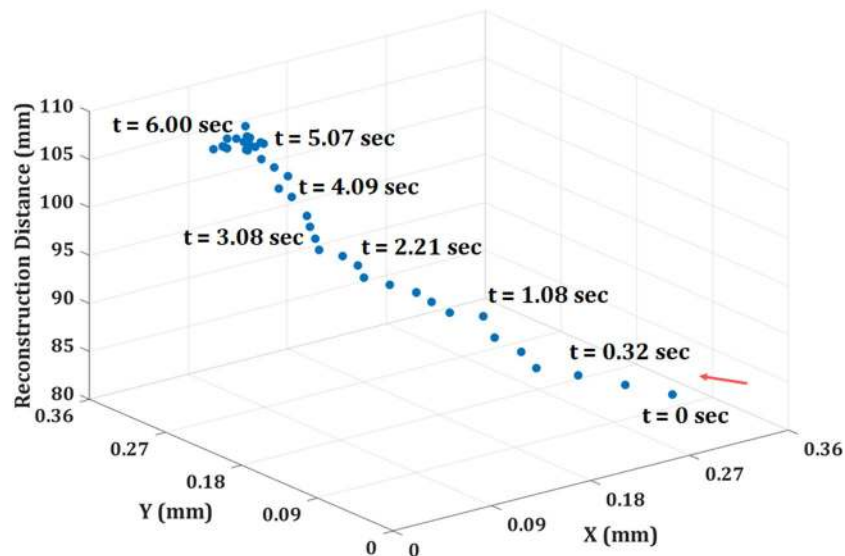


Figure 10. The trajectory of the fluorescence bead.

holographic system. The movie of the holograms of the moving fluorescent bead is shown in Visualization 1. The corresponding movie of the reconstructed fluorescence imaging is shown in Visualization 2. The phase maps of the moving bead, corresponding to Fig. 9(a), are obtained by coherent digital holographic microscopy and are shown in Fig. 9(b) at different time intervals. The movies of the recorded phase holograms and the corresponding reconstructed unwrapped phase maps are shown in Visualizations 3 and 4, respectively. Figure 10 shows the trajectory of the bead. In future work, the time-lapse measurement will be implemented to observe the stem cell formation process in *Physcomitrella*⁴⁶ via 3D visualization of the simultaneous behaviors of the nucleus and cell structures.

Conclusion

A new multimodal system is proposed for simultaneous recording and reconstruction of cross-sectional fluorescence and quantitative phase imaging of fluorescent microsphere beads and successfully implemented for the fluorescence and phase imaging of living plant cells labeled with fluorescent proteins. The system comprises of an off-axis Fresnel incoherent digital holographic microscopy and another off-axis coherent digital holographic microscopy working in transmission-mode for recording and retrieving simultaneously the cross-sectional fluorescence images and the quantitative phase of the fluorescent objects. The experimental results presented here reveal the system's capability for simultaneous investigations of cross-sectional fluorescence and phase information on a single platform. The proposed multimodal system will be the basis for the imaging of rapidly moving vital phenomena in living 3D structures, such as cytoskeleton dynamics⁴⁷, neuronal activation⁴⁸, and morphogenetic flow⁴⁹. Since both the fluorescence and the quantitative phase images of a biological sample can be retrieved from the proposed system, it is possible to extract important biophysical parameters of the sample including its shape and volume, refractive index distribution and the dry mass, etc. Therefore, such multimodality imaging systems could find an immensely beneficial role for improved diagnosis of various diseases. The system could further be upgraded towards a more compact and stable one to provide enhanced image quality and to allow real-time visualization of living biological cells and tissues along with the measurement of various aforesaid intrinsic biophysical parameters.

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Author contributions

O.M. conceived the idea. M.K. and X.Q. fabricated the system. M.K. performed the experiments and wrote the manuscript. M.K., X.Q., O.M., Y.A., and Y.T. analyzed the data. All authors discussed the results and contributed to the manuscript.

Competing interests

The authors declare no competing interests.

Additional information

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