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DISCO: a low-energy multipurpose beamline at synchrotron SOLEIL.

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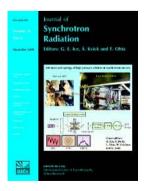
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DISCO: a low-energy multipurpose beamline at synchrotron SOLEIL

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DISCO, a novel low-energy beamline covering the spectrum range from the VUV to the visible, has received its first photons at the French synchrotron SOLEIL. In this article the DISCO design and concept of three experimental stations serving research communities in biology and chemistry are described. Emphasis has been put on high flux generation and preservation of polarization at variable energy resolutions. The three experiments include a completely new approach for microscopy and atmospheric pressure experiments as well as a 'classical' synchrotron radiation circular dichroism station. Preliminary tests of the optical design and technical concept have been made. Theoretical predictions of the beam have been compared with the first images produced by the first photons originating from the large-aperture bending-magnet source. Results are also reported concerning the cold finger used to absorb hard X-ray radiation in the central part of the synchrotron beam and to avoid heavy thermal load on the following optics. Wavelength selection using monochromators with different gratings for each experimental set-up as well as beam propagation and conditioning throughout the optical system are detailed. First photons comply very well with the theoretical calculations.

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Keywords: VUV; beamline; spectroscopy.

1. Introduction

The range from vacuum ultraviolet (VUV) to visible on third-generation synchrotrons is somewhat exotic considering that only a few beamlines working in this domain are under the process of design or already designed. Most of them focus on circular dichroism and spectroscopy between 3 and 7 eV (Sutherland *et al.*, 1980; Gekko *et al.*, 2001; Tao *et al.*, 2001; Clarke & Jones, 2004; Matsuo *et al.*, 2005; Hoffmann *et al.*, 2007).

In the case of the SOLEIL synchrotron radiation facility, a 2.75 GeV storage ring, the DISCO (dichroism, imaging and spectroscopy for biology) beamline will cover the 1–20 eV photon energy range. This paper presents the general concept, implementation and how the issues encountered during the construction of DISCO beamline were solved.

The DISCO beamline possesses three end-stations with different requirements (Figs. 1 and 2). The synchrotron radiation circular dichroism (SRCD) experiment covers the

‡ These authors have contributed equally to the publication of this article.

wavelength range 600-130 nm (2-9.5 eV) (Miron et al., 2005), with maximized conservation of natural polarization from the bending magnet. The spot size at the experimental chamber allows full irradiation of the absorption cell (3 mm in diameter). SRCD shares beam time with a branch line referred to as the atmospheric pressure experiment (APEX). APEX delivers photons windowless in the 300-60 nm range (4.1-20 eV) at atmospheric pressure. A differential pumping stage accommodates for pressure differences between the sample and the beamline. The horizontal focal point position has been chosen in order to have the smallest spot size at the entrance port of the differential pumping. The third endstation, which works in parallel with the two other branch lines, is a microscope using 1000–180 nm (1.2–6.9 eV) fully tunable excitation with special emphasis on the use of the synchrotron radiation time structure for lifetime by phase modulation measurements.

All optical parameters were optimized using *SOLEMIO*, an in-house software that combines ray-tracing calculations and optimization iterations.

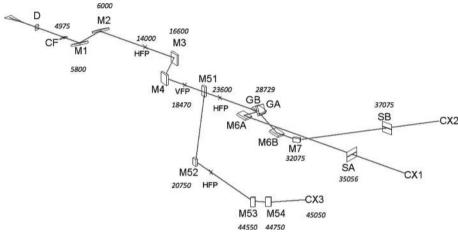


Figure 1Optical layout of the DISCO beamline. D, diaphragm; CF, cold finger; Mx, mirrors (for mirror number refer to Table 1); Gx, gratings (for grating number refer to Table 1); HFP, horizontal focal point; VFP, vertical focal point; CX1, SRCD end-station; CX2, APEX end-station; CX3, microscopy end-station. Distances from the source point are indicated in mm for some elements.

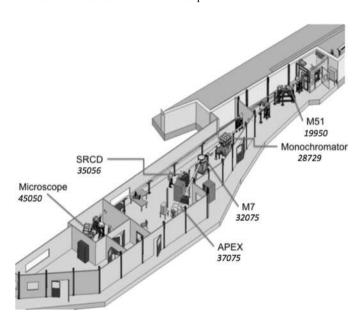


Figure 2
Layout of the DISCO beamline in the experimental hall at SOLEIL.
Distances from the source point are indicated in mm for some elements.

2. Front-end requirements and constraints

2.1. General comments

The beam, extracted from a bending-magnet, D4.1 (1.71 T, bending angle 11.25°), has a 50 mrad \times 10 mrad divergence. It is defined in size by the aperture of a crotch absorber located at 1.5 m from the bending-magnet exit. Vertically the 5 mrad above and under the central emittance allow for the collection of all energies down to 1.2 eV, with a symmetric distribution from the highest to the lowest energies (Fig. 3). The large horizontal extraction of 50 mrad provides the necessary flux.

2.2. Front-end energy selection

As a low-energy beamline, the first point to resolve is the non-standard extraction of the beam. Most of the high ener-

gies are concentrated in the vertical central part of the beam. Therefore, a symmetric extraction of the upper and lower parts implies the exclusion of the central part (Fig. 3). Two possibilities are then opened: either a slotted mirror, as used by the infrared beamlines (Dumas et al., 2006), or a central absorber placed upstream of the first mirror. A slotted mirror implies a very good surface polishing of the slit edges which is not trivial in the proposed energy range. On the other hand, a central absorber may be centred relatively easily on the beam to absorb the energetic photons. It was decided to position a cold finger of thickness 7.5 mm to intercept a vertical angle of 1.5 mrad in the middle of the beam at a distance of 825 mm of the first M1

mirror (Fig. 1). With this design, the cold finger absorbs the entire 3 kW for a 500 mA storage-ring current. This heat load is dissipated by two water circuits with an inlet temperature of 294 K. At 300 mA storage-ring current, the outlet temperature measured was 300 K. The cold finger shape was designed to minimize vertical and horizontal deformation under thermal stress. Moreover, it is made of glidcop owing to the better thermal performances of this material with respect to copper (Troxell, 1989).

At the back of the cold finger a 0.5 mm blade prevents the propagation of diffracted X-rays originating from the front edge of the cold finger further to the first mirror. Hence, the

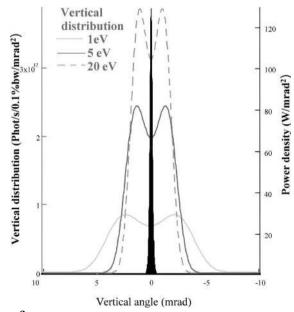


Figure 3 Vertical distribution profiles of the photon fluxes emitted by a dipole for a 50 mrad (V) \times 10 mrad (H) aperture at 1 eV (light gray), 5 eV (dark gray) and 20 eV (dotted line). 99.15% of the total power density (in black, right-hand axis) is concentrated in the central mrad.

 Table 1

 Optical parameters of the mirrors.

R: tangential radius. r: sagittal radius. vls: variable line spacing.

Optical element	Optical property	Distance from source (mm)	Grazing incidence	Material	Radius of curvature
M1	Cylindrical convex	5800	22.5°	Si	r = -75 m
M2	Toroidal	6000	22.5°	Si	R = 21.04 m, r = 2.56 m
M3	Elliptic cylindrical	16600	22.5°	Si	R = 9.93 m
M4	Plane	16800	22.5°	Si	_
M51	Sphere convex	19950	22.5°	Si	R = -35 m
M52	Cylindrical	20750	20.65°	$AlMgF_2$	r = 2 m
M53	Toroidal	44500	22.5	$AlMgF_2$	R = 4.75 m, r = 0.714 m
M54	Toroidal	44750	22.5°	$AlMgF_2$	R = 7.80 m, r = 1.12 m
M6A	Toroidal	28556	75°	Ru	R = 7.87 m, r = 5.56 m
M6B	Spherical	29075	15°	Si	R = 35.4 m
M7	Cylindrical	32075	11°	Si	R = 37.85 m
GA	Plane, 400 lines mm ⁻¹ (vls)	28729	75°	Ru	_
GB	Plane, 250 lines mm ⁻¹ (vls)	28729	15°	Si	-

residual power reaching the first mirror M1 (size 190×260 mm) has been calculated to amount to less than 5 W. This heat is dissipated through a copper braid and a water-cooling circuit at 294 K. Initial tests at a ring current of 300 mA have demonstrated proper cooling of the mirror.

The shadow of the cold finger excludes the central energy towards M1 (Table 1). A second mirror, M2, redirects the beam in the horizontal plane and refocuses it in order to reduce its beam size to 26 mm (horizontal) \times 19 mm (vertical), which is necessary for it to pass through the wall of the storage ring at 14 m from the source.

2.3. Consideration of possible contamination of the first mirrors

Carbon deposition and contamination of the first mirror system has become a major concern at third-generation synchrotron radiation facilities. This pollution arises from photochemical reactions of the background gases with the beam. The main gases emitted while irradiating an ultrahighvacuum chamber with a white beam are H₂, CH₄, CO and CO₂ (Kobari & Halama, 1987). These species could adsorb on the first mirrors M1 and M2, inducing a carbon deposit that would impair reflectivity over time. However, desorption does decrease with dose because of beam cleaning. If the molecular hydrogen contribution remains globally constant with dose, the carbon-containing species do decrease. According to literature data, the desorption level η ranges from 8×10^{-5} molecules photon⁻¹ to 4×10^{-5} molecule photon⁻¹ for H_2 and from 1×10^{-5} molecule photon⁻¹ to 8×10^{-7} molecule photon⁻¹ for CH₄ after a photon dose of 1×10^{21} photon m⁻¹ (Anashin et al., 2004).

Numerous studies have been carried out to elucidate the mechanisms of neutral photodesorption from an illuminated surface (Kobari & Halama, 1987; Gröbner *et al.*, 1989; Kobayashi *et al.*, 1987; Hori *et al.*, 1993; Andritshky *et al.*, 1988). Two phenomena have been proposed: either direct photon desorption or electron-induced desorption, those electrons being emitted by irradiated surfaces. Even if these two phenomena are difficult to distinguish, some evidence is in

favour of photoelectrons. Comparisons between desorption level and photoelectron emission level show behaviour independent of the incident photons' energetic spectrum (Hori et al., 1993). It clearly demonstrates the correlation between desorption and photoelectrons emission. The photodesorption occurs from surfaces close to the illuminated part of the chambers, which are exposed to the emitted photoelectrons. Hence, it has been shown that applying a negative electric field close to those illuminated areas reduces desorption (Kobari et al., 1990).

In order to reduce the risk of carbon deposition on the first optics, it was decided to use specific materials (glidcop) and to set the tooth-like cold finger front-edge facing the beam at a 25° angle. Additionally, a special motorized shutter acting as a screen just before M1 (used during the degassing stage of the cold finger) has been introduced to allow a soft conditioning of the first mirrors. Three large-size diaphragms have been placed upstream of this shutter to prevent scattered light from the cold finger entering the chamber.

2.4. Beam propagation and diagnosis

2.4.1. Ultrahigh vacuum. The beamline is maintained under ultrahigh vacuum (UHV) between a few 10^{-10} and 1 \times 10⁻⁹ mbar. All the mechanical elements have been chosen for UHV compatibility. Each end-station connection to the UHV is treated differently: (i) microscopy through a Suprasil viewport, (ii) SRCD through a CaF₂ viewport and (iii) APEX, windowless, through a differential pumping stage. Indeed, the microscopy line uses photons from 1000 nm up to the Suprasil cut-off at 180 nm, since in this wavelength range atmospheric gases do not absorb and the line is therefore maintained under static primary vacuum for cleanness only. The wavelength range used for SRCD experiments goes down to 130 nm. A calcium fluoride window isolates the branch line from the experimental chamber flushed with nitrogen. The situation is different for the APEX branch line, for which VUV photons down to 60 nm are used. Since there is no material transparent below the LiF cut-off around 105 nm, the branch line is fitted with a differential pumping between the exit slit of the monochromator and the experimental chamber in order to work windowless from the atmosphere on the experimental side. Moreover, since atmospheric gases absorb VUV radiation in this domain, the differential pumping unit works at 1 atm for rare gases (argon or neon) depending on the shorter wavelength to be reached. Interestingly, this differential pumping stage acts as a gas filter preventing higher-order radiation from reaching the experimental areas (Mercier et al., 2000).

2.4.2. Diagnosis. Owing to the relatively complex optical scheme of the beamline, several focal points are found along the beam path (Fig. 1). All the diagnostic chambers are UHV compatible and pumped by ion pumps (StarCell 50, Varian).

The first focal horizontal point appears at 8 m downstream of M2. A diagnostic chamber has been installed at this position inside the synchrotron tunnel. It contains a macor target mounted on a lateral motorized translator, which can be inserted to intercept the beam at 90°. The target itself is oriented at 45° with respect to the beam and faces a camera (SCA640-70gm, Basler Vision Technologies) through a viewport. Therefore, this diagnostic provides an image of the beam and allows for proper tuning of the normal rotation of the M2 mirror.

The first vertical focal point is found 1.67 m downstream of the mirror M4. At this position the beam size is 56 mm horizontally (H) \times 1.2 mm vertically (V). For cluttering reasons, the diagnostic chamber has been placed 170 mm downstream of the focal point. The diagnostic system is composed of three elements: a gold grid, a position-sensitive photodiode (PSD) and a mirror. All of these elements may be inserted and retracted from the beam path.

The gold grid (Precision Eforming, NY, USA) of 70 wires per inch, giving 90% transmission, is used for photon flux measurements upstream of the partial beam withdrawal for the imaging branch.

A plane mirror made of aluminium-coated silica (Optique J. Fichou et Tofico, France) of 90 mm (H) \times 30 mm (V) may be inserted to deflect the beam at 90° through a CaF₂ viewport to a Basler camera. Interferometric filters mounted on the camera allow measurements of the beam shape at different wavelengths in the visible region, as well as fine-tuning of the M3–M4 couple of mirrors.

The PSD measures the position of the photon beam with respect to the theoretical predictions. Because of the large beam size in the horizontal direction, it was not possible to find a commercial PSD allowing measurements in that direction. Hence, we have limited the diagnosis to the vertical direction using a one-dimensional PSD (S3931, Hamamatsu, Japan). A 2.5 optical density filter limits the incident power on the diode.

The second horizontal focal point is found downstream of the M51–M52 mirror system, and 6.8 m from M4. The beam is

 $5~\mathrm{mm} \times 20~\mathrm{mm}$ (H \times V) in size at this position. The diagnostic chamber is placed 500 mm downstream of the focal point and contains the same set of elements as previously, namely a gold grid, a PSD and a mirror. At this particular position the beam size allows us to use a four-quadrants position-sensing photodiode (SXUV600M, International Radiation Detectors, CA, USA). This detector has been aligned precisely to the theoretical position of the beam. Thus, the detector measures the beam position on both the vertical and horizontal axes. A 2.5 optical density filter also protects the photodiode from excessive thermal loading.

Measurements on the gold grid are compared with those made upstream of the M51–M52 couple to monitor the loss of flux owing to the uptake of the M51 mirror for the imaging line

The mirror and the imaging system are of the same type as previously, and provide the opportunity to check the shape of the beam at this vertical focal point.

A horizontal focal point is found on the imaging branch line, located 4.96 m downstream of the M52 mirror. A diagnostic system was placed at this position. It is composed of a macor target oriented at 45° from the beam direction, which faces a Basler camera. The centre of the target is spotted and aligned to the theoretical position of the beam. Therefore, this element permits a precise positioning of the beam. This point is especially important because the next optical elements on this branch line are located 23.8 m downstream of M52 (Table 1).

2.4.3. Stability and alignment. The symmetry of the beam is given by the geometry of the cooled diaphragm, centred on the cold finger. The set constituting the cold finger and the diaphragm was conceived in order to conserve the symmetry during dilatation of the parts under heat deposition by the beam.

The M1–M2 mirror system is placed on an independent mechanical module situated inside the vacuum chamber. This module is mechanically decoupled from the chamber and was positioned on an independent base. The stabilities of the optical module were obtained by binding up efficiently the base pole of the mirrors with the storage-ring floor and by locking all degrees of freedom after adjustments (Fig. 4). The aim was to obtain the highest normal mode of the mirrors' structure, using the high stability of the storage-ring floor and



Figure 4
Layout of the DISCO beamline front-end at SOLEIL. Distances from the source point are indicated in mm for some elements.

the rigid mountings to prevent the propagation or amplification of vibrations coming from the floor or through the vacuum tubes.

The mechanical module with mounted mirrors was prealigned and the optical axes were referenced to external references by relative position measurement, allowing absolute positioning under vacuum. The positions of the mirrors can be directly measured optically. M2 rotation is accessible under vacuum and under beam.

3. Optical design

3.1. General comments

The general optical layout (Fig. 1) has to comply with the energy, polarization and photon flux requirements of the three end-stations as well as with the congestion occurring from the positions of the end-stations themselves (Fig. 2). In order to solve this problem, the DISCO beamline has been designed as a long and narrow beamline implying very large optics.

3.2. Choice of materials

Considering its reflectivity properties over the full energy range of DISCO ($1.1-20~\rm eV$) (Pallick), silicon was selected as the main material for the optics common to the three branches (Table 1). However, the optics used specifically on the two low-energy branches were coated with particular materials for optimal reflectivity in the wavelength of interest and for polarization conservation issues, namely ruthenium for M6A and GA, and AlMgF₂ for M52, M53 and M54.

3.3. Choice of deviation angles

Deviation angles of the mirrors and gratings were chosen to maximize the photon fluxes and to preserve the natural polarization of the synchrotron radiation beam. The first four silicon mirrors are at 22.5° grazing incidence. The vertical pair of mirrors (M1–M2) is followed by another pair of mirrors (M3–M4), which diverts the beam 200 mm horizontally with the same deviation angle (Fig. 1). Hence, transport and translation of the beam from the storage ring through the radiation protection hutch allows preservation of the polarization as well as compliance with the radiation safety rules of SOLEIL. The safety rules require the translation of the synchrotron radiation out of the cone of the *Bremsstrahlung*.

Wavelength selection for the SRCD and APEX endstations is provided by a monochromator containing two separate gratings at different incidence angles (Cinel Company, Italy).

The SRCD branch uses a near normal incidence grating (15° incidence angle) to maintain the polarization of the source, whereas APEX uses a grazing-incidence grating (75° incidence angle) to cover the spectral range up to 20 eV. Both gratings and associated focusing mirrors are controlled by the same mechanism.

3.4. Ray tracing

The parameters of the optics are the result of numerous optimization iterations with the *SOLEMIO* software (Table 1). This in-house software combines ray-tracing calculations with optimization iterations. One chooses any parameters, *e.g.* radius of curvature, distance *etc.*, and sets the minimization criteria, *e.g.* minimization of the vertical image size (horizontal, or a combination of both) at any point of the beamline, or the maximization of the resolving power over a specified spectral range (in this case it is the average of the spectral width on several wavelengths which is minimized).

For the two mirrors M1 and M2, with the combination of the convex radius of M1 and the tangential radius of M2, it is possible to eliminate the curvature of the image (commonly called 'the smile') usually obtained with a single toroidal mirror, to minimize the vertical size of the intermediate image, and to maximize the resolving power. SOLEMIO optimizes simultaneously these two radii of curvature to have the best resolving power for all the spectral range, and then the resulting ray-tracing shows no more curvature at the intermediate image. In the same way, the varied line spacing of the gratings (actually, directly the holographic recording parameters) and the tangential radius of M6 were simultaneously optimized. The varied line spacing is necessary, mostly on the APEX branch, to minimize the defocusing at the exit slit for all the spectral range as well as to maximize the resolving power. The calculated resolving power is between 800 and 3000 for the two branches.

On the SRCD branch the beam diverges vertically by ~ 5 mrad full width at half-maximum (FWHM) from the exit slit of the monochromator, and it is horizontally focused at 0.5 m (by the sagittal radius of M6A). At this experimental point the size of the beam is 1.8 mm (H) \times 2.5 mm (V) FWHM.

On the APEX branch the beam diverges vertically by 2 mrad FWHM from the exit slit of the monochromator and it is horizontally focused at 1.09 m on the last slit of the differential pumping (optimization of the shape of the elliptical mirror M3 and of the curvature of M7). At this point the beam is approximately 1.1 mm (H) \times 2.5 mm (V) FWHM.

On the imaging branch the beam is focused vertically and horizontally onto the entrance slit of the monochromator (iHR 320, Jobin Yvon, France), and its numerical aperture at this point fits with the monochromator. The curvatures of the four mirrors M51, M52, M53, M54 are optimized for this purpose, with the constraint of having a narrow beam on M53 and M54, which are very far from M51/M52 (about 24 m).

The shape of the elliptical mirror M3 was optimized to have the minimum horizontal size on the last slit of the APEX branch.

The bending magnet provides a degree of circular polarization of about 0.74 at 3 mrad from the central axis, and 0.91 at 5 mrad (our maximum acceptance). This distribution is propagated to the circular dichroism branch experimental point, with an angular vertical magnification of about 0.85, and only a very little decrease of the degree of polarization (about

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-0.01), because, from a polarization point of view, M3/M4 compensates M1/M2, and M6A and GA are near normal incidence.

4. Beamline commissioning

4.1. Beam shape and size

From the bending magnet, 2.3° are extracted at 1.7° of the zero tangent. The beam then passes through a crotch absorber at 1.5 m from the source, which defines its dimensions. At 4.13 m a trapezoidal diaphragm reshapes the beam and represents the optical aperture with maximum tolerances accom-

modating beam position shifts while maintaining a constant beam shape (dimensions: length 165.8 mm; inner and outer height of the trapeze shape with respect to the storage ring: 45.1 and 38.2 mm, respectively).

The beam shape close to the first vertical focal point, theoretically calculated by wave propagation calculations using *SRW* (Chubar & Elleaume, 1998), appears to be well balanced between the upper and lower part (Fig. 5). Measurements are in accordance with prediction (Fig. 5).

The *SRW* software predicts the spectral, spatial and polarization properties of the radiation in the near-field and/or far-field approximation produced by a relativistic electron beam travelling through the corresponding bending-magnet field of 1.71 T. The computed wavefront of the radiation can be propagated through drift spaces, lenses (mirror, refractive, Fresnel *etc.*), apertures or arbitrary two-dimensional phase-shifting elements.

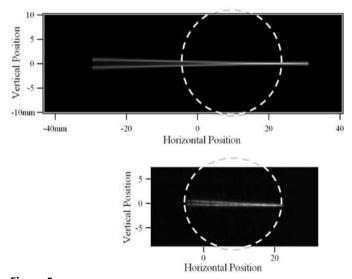


Figure 5 Photon projection recorded (bottom) 0.32 m before the first vertical waist, and simulation with *SRW* (top) of beam shape on the same virtual object plane. Light is filtered using a 633 nm bandpass filter. The dotted circle identifies the region captured by the camera (camera field of view).

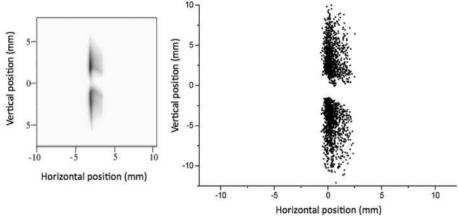


Figure 6Photon projection calculated using *SOLEMIO* ray-tracing (right) at the first horizontal focal point compared with the measurement (left).

In combination with the *SOLEMIO* calculations, these predictions have proven to be very useful in assessing the beam shape at the horizontal focal points.

Initial images at the first horizontal focal point diagnostic, 14 m from the source (Fig. 6), identified a negative tilt of 0.1° of mirror M1 (axis R_n) responsible for the tilted shape of the fan of the focused beam, compared with predictions. These first images, recorded at low storage-ring current of 2 mA, also show an equal proportion of the top and bottom parts of the beam, thereby indicating a very good central alignment of the cold finger (Fig. 6).

At the following vertical horizontal point, 18.5 m from the source, at the exit of the radiation protection hutch a provisional CCD camera with focusing lenses was mounted.

The shape of the horizontal focal point (Fig. 6), taken without objective, demonstrates very well the accordance between measurement and prediction. The difference in height is due to the underestimation of low-intensity regions by the camera.

5. Summary

In this article we have presented the design and the characteristics of the first extracted beam of the DISCO beamline at the SOLEIL synchrotron radiation facility. Front-end energy selection and optical design have been optimized for the three end-stations. Special attention was given to the protection against pollution of the first mirrors and dedicated diagnostics. Ray-tracing calculations using the SOLEMIO inhouse software allowed optimization of the optical parameters. The first experimental measurements of the beam shape and size were in excellent agreement with the wave propagation using SRW and SOLEMIO calculations. The agreements found at various positions along the beam path confirm an excellent alignment of the front-end optical components. The three end-stations of the beamline will be operational in September 2009.

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