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# Dopant-free multilayer back contact silicon solar cells employing $V_2O_x$ /metal/ $V_2O_x$ as an emitter†

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In this study, we present novel multilayer back contact (MLBC) solar cells employing  $V_2O_x$  (8 nm)/metal/ $V_2O_x$  (8 nm) (VMV) multilayers as dopant-free hole-selective contacts deposited using a thermal evaporation process at low temperature. The optimized  $V_2O_x$  films have a high work function and reduced O-deficiency in-gap state energy owing to the introduction of a carefully controlled  $O_2$  partial pressure during the evaporation process. The contact resistivities of VMV (12 nm Ag) and VMV (4 nm Au) contacts with n-Si are  $1.58 \text{ m}\Omega \text{ cm}^2$  and  $0.04 \text{ m}\Omega \text{ cm}^2$ , respectively, which are less than that of a 16 nm  $V_2O_x$ /n-Si contact. Interestingly, VMV (Au)/n-Si MLBC solar cells demonstrate improved charge carrier transport, leading to an induced p–n junction. Moreover, the dominant interfacial charge carrier transport properties of MLBC solar cells with VMV (Ag)/n-Si and VMV (Au)/n-Si contacts correspond with the diffusion–recombination model, whereas, those of MLBC solar cells with  $V_2O_x$ /n-Si and VMV (Ca)/n-Si contacts correspond with the multi-tunneling capture emission model at a high-forward-bias voltage. The use of VMV (4 nm Au) as an emitter achieves an efficiency of 19.02% for this type of MLBC solar cell, which is greater than that of  $V_2O_x$ /n-Si solar cells (17.58%). This work has important implications for enabling the fabrication of low-performance dopant-free back contact solar cells with high stability using a simple fabrication process.

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## 1. Introduction

Interdigitated back contact (IBC) solar cells have achieved high efficiency by completely eliminating metal grid shading at the front surface, and collecting both electrons and holes at the back surface.<sup>1</sup> The solar cell structure requires heavy doping based on B and P diffusion for the efficient transport and collection of charge carriers.<sup>2</sup> These highly doped homo-junctions incur numerous sources of loss such as free carrier absorption (FCA), Auger recombination, Shockley–Read–Hall (SRH) recombination, and other heavy doping effects.<sup>3</sup> The successful development of a heterojunction back contact (HBC) solar cell by Masuko *et al.*<sup>4</sup> has demonstrated that asymmetric carrier-selective heterocontacts are an important step for approaching the efficiency limit of crystalline Si (c-Si) solar cells. However, the present development of HBC solar cells still relies

on the heavily doped amorphous Si (a-Si) layers, which are fabricated using inflammable and explosive precursor gases such as semiconductor-grade silane ( $\text{SiH}_4$ ), phosphine ( $\text{PH}_3$ ), and diborane ( $\text{B}_2\text{H}_6$ ) diluted in  $\text{H}_2$ .<sup>5</sup> Furthermore, while the interfacial defect density increases with increasing dopant concentration, which increases the occurrence of junction recombination and decreases the open circuit voltage ( $V_{\text{OC}}$ ).<sup>6</sup>

Recently, the high efficiency front junction c-Si solar cells have been developed that employ dopant-free asymmetric heterocontacts fabricated using relatively simple techniques such as evaporation, spin coating, and spray pyrolysis, which reduce the cost and complexity of fabrication.<sup>7,8</sup> In principle, the employment of an HBC architecture should further improve the conversion efficiency of dopant-free solar cells, and considerable effort has been devoted to the development of dopant-free HBC solar cells with selective hole and electron contacts. Um *et al.*<sup>5</sup> developed a low-cost, dopant-free HBC solar cell using Molybdenum oxide ( $\text{MoO}_x$ ) and lithium fluoride ( $\text{LiF}_x$ ) contacts on the emitter and back surface field (BSF) region, respectively. Wu *et al.*<sup>9</sup> also employed three transition metal oxides (TMOs;  $\text{WO}_x$ ,  $\text{MoO}_x$ , and  $\text{V}_2\text{O}_x$ ) as hole-selective contacts in the fabrication of HBC solar cells using a simple and low cost self-aligned processing technology *via* metal mask patterning conducted at a low temperature of less than  $40^\circ\text{C}$ .

However, the film bulk resistivity of TMOs is very high, and their sheet resistance is on the order of  $10^9 \Omega \text{ sq}^{-1}$ . Moreover, the low light conditions at the back side of HBC solar cells

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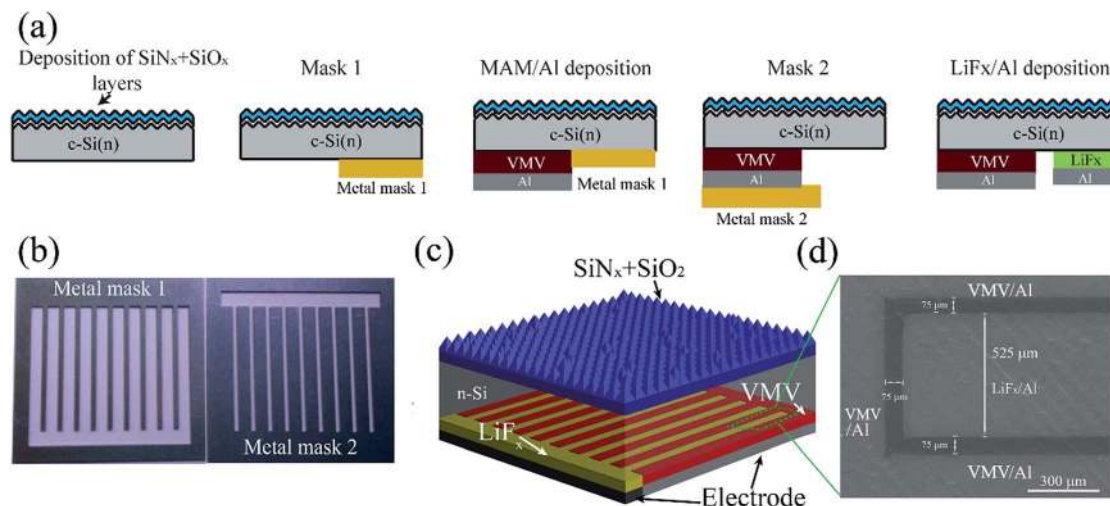


Fig. 1 (a) Schematic illustrating the MLBC solar cell metal patterning fabrication process. (b) The two metal patterning masks. (c) The structure of a completed MLBC solar cell. (d) SEM image of the results of metal mask patterning.

requires that TMO contacts have an enhanced dark conductivity.<sup>10</sup> The gap defect states in the emitter bulk and interface increase with high dopant concentration.<sup>11</sup> In addition, the O vacancies in the bulk of amorphous sub-stoichiometric TMOs lead to a low work function of TMOs, which induces a smaller degree of band bending in the TMO/Si heterojunction and deteriorates the fill factor (FF) and  $V_{OC}$ .<sup>12</sup> Therefore, it is of considerable interest that the work function and charge carrier concentrations and conductivity of oxide/metal/oxide (OMO) multilayer films have been shown to be adjustable in organic optical and electronic devices, which is a property that has been widely developed in transparent and conductive electrodes such as TiO<sub>2</sub>/Ag/TiO<sub>2</sub>,<sup>13</sup> ZnO/Ag/ZnO,<sup>14</sup> InZnO/Ag/InZnO,<sup>15</sup> InZnO/Au/InZnO,<sup>15</sup> ZnMgBeO/Ag/ZnMgBeO,<sup>16</sup> MoO<sub>3</sub>/Ag/MoO<sub>3</sub>,<sup>17,18</sup> WO<sub>3</sub>/Ag/WO<sub>3</sub> (ref. 19 and 20) and V<sub>2</sub>O<sub>5</sub>/Ag/V<sub>2</sub>O<sub>5</sub>.<sup>21</sup>

Inspired by the above advances, we applied V<sub>2</sub>O<sub>x</sub>/metal/V<sub>2</sub>O<sub>x</sub> (VMV) multilayer films fabricated by a thermal evaporation process as the hole-selective contact in dopant-free multilayer back contact (MLBC) silicon solar cells. A carefully controlled O<sub>2</sub> partial pressure introduced during the evaporation process can increase the work function and decrease the gap O-deficiency defect state energy in the band gap of the V<sub>2</sub>O<sub>x</sub> films. The effects of the choice of the intermediate metal, the intermediate metal layer thickness, and the work function on the solar cell performance are evaluated. In addition, we investigate the carrier selectivity of the VMV/n-Si interface using suns- $V_{OC}$  measurements, carrier transport behavior, and the contact resistivity  $\rho_c$ . Employing an optimized emitter structure of V<sub>2</sub>O<sub>x</sub> (8 nm)/Au (4 nm)/V<sub>2</sub>O<sub>x</sub> (8 nm) in the dopant-free MLBC c-Si solar cells achieved an efficiency of up to 19% for a 4 cm<sup>2</sup> Si wafer.

## 2. Experimental

The n-type (100) oriented CZ silicon wafers (2–3 Ω cm, 180 μm) were used for all the device fabrications in this study. The Fig. 1(a) schematically illustrates the simple and low cost self-aligned metal mask patterning process employed in the

present study to fabricate MLBC solar cells featuring emitter-area VMV hole-selective contacts. Rather than photolithographic or screen print masking, the two metal masks (see Fig. S1†) shown in Fig. 1(b) were applied to form the emitter and BSF areas. The V<sub>2</sub>O<sub>x</sub>/metal/V<sub>2</sub>O<sub>x</sub> multilayer films and Al electrodes were applied by thermal evaporation conducted at a low temperature of <40 °C with a deposition rate of about 0.2–0.5 Å s<sup>-1</sup> at a base pressure of 5.0 × 10<sup>-6</sup> Torr. After metal mask application, LiF<sub>x</sub> (2 nm)/Al (500 nm) films were thermally evaporated onto the BSF area. The optimized MLBC solar cells were passivated with a front surface field (FSF; 200 Ω sq<sup>-1</sup>), as shown in Fig. 1(c). The scanning electron microscopy (SEM) image given in Fig. 1(d) demonstrates the high alignment quality obtained by the process, which forms a uniform 75 μm gap between the VMV/Al and LiF<sub>x</sub>/Al contacts, illustrating a BSF region with a uniform 260 μm in half-width, and an emitter region with a uniform 750 μm in half-width (see Fig. S2†). The fabrication process outlined above is very simple compared to the fabrication processes employed for conventional IBC<sup>2</sup> and HBC solar cells.<sup>22</sup>

The cross-section of VMV/n-Si interfaces were obtained by a focused ion beam (FIB) lift-out technique and observed by FEI Tecnai G2 F30 transmission electron microscopy (TEM) operating at 300 kV. The VMV/n-Si samples were covered with Pd in order to protect the films. The Ultraviolet Photoelectron Spectroscopy (UPS) measurements were performed on Thermo Scientific Escalab 250Xi using the monochromated He I radiation (21.2 eV) in an ultra-high vacuum chamber with a base pressure of 2 × 10<sup>-9</sup> mbar. In order to move surface contaminant, the as-deposited sample was sputtered by Ar<sup>+</sup> ions as long as 90 seconds. The UPS spectra were obtained with a sample bias of -5 V in normal emission geometry to obtain secondary electron cutoffs. All spectra were plotted with respect to the Fermi level ( $E_F$ ) determined from the n-Si (100) substrate.

The light  $J$ - $V$  behavior was employed on a NewPort system under standard one sun conditions (100 mW cm<sup>-2</sup>, AM1.5



spectrum, 25 °C) and  $J$ - $V$  curves were recorded by Keithley 2400 with a  $2 \times 2 \text{ cm}^2$  aperture mask using a solar simulator (Class AAA, Oriel Sol3A, Newport), and the dark  $J$ - $V$  behavior was also investigated. The External Quantum Efficiency (EQE) was conducted using a Solar Cell Quantum Efficiency Measurement System (QEX10, PV Measurements). The  $J_{SC}$  of the cell was integrated by the EQE. The injection level dependent open-circuit voltage was measured by transient photo-conductance measurement (WCT-120, Sinton). And the values of contact resistivity  $\rho_c$  for VMV/n-Si contact were respectively measured by the transfer length method (TLM).

### 3. Results and discussions

Because the  $\text{V}_2\text{O}_x$  (16 nm)/n-Si contact has a relatively low contact resistivity (see Fig. S3<sup>†</sup>), the top and bottom  $\text{V}_2\text{O}_x$  layer thicknesses were both fixed at 8 nm to evaluate the effects of the intermediate metal layer in the VMV emitter systematically. The interfacial morphology, work function, and bulk defect states of the carrier-selective contacts with n-Si play an important role in solar cell performance. The cross-sectional TEM image given in Fig. 2(b) indicates that the interface between the  $\text{V}_2\text{O}_x$  and Ag films of the  $\text{V}_2\text{O}_x/\text{Ag}/\text{V}_2\text{O}_x$  multilayer structure is clearly

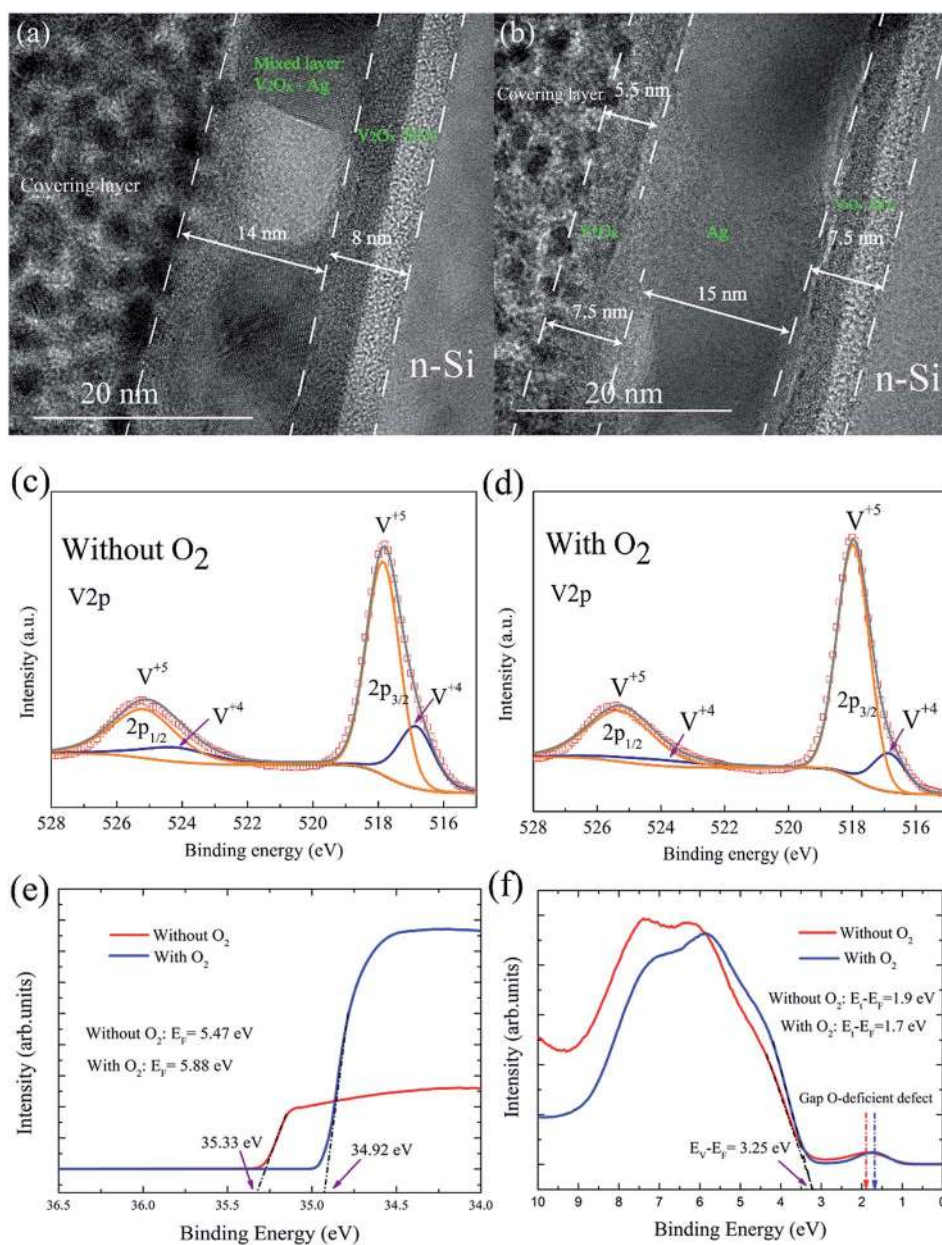


Fig. 2 Cross-sectional TEM micrographs of  $\text{V}_2\text{O}_x$  (8 nm)/Ag ( $x$  nm)/ $\text{V}_2\text{O}_x$  (8 nm) multilayer films with (a)  $x = 4$  nm Ag and (b)  $x = 16$  nm Ag. (c) and (d) XPS spectra of  $\text{V}_2\text{O}_x$  films prepared without and with the introduction of an  $\text{O}_2$  partial pressure into the thermal evaporation process, respectively. The UPS spectra of  $\text{V}_2\text{O}_x$  films: (e) the work function ( $E_f$ ); (f) shows the positions of the O-deficiency in-gap defect states near the Fermi level.



recognizable, with a structure composed of 7.5 nm thick  $V_2O_5$ , 15 nm thick Ag, and 7.5 nm thick reacted layers consisted of  $V_2O_5$  and  $SiO_x$ , respectively, and with an Ag morphology that is clearly identifiable. The interfacial reaction appears during the thermal deposition of  $V_2O_x$  and causes the surface oxidation of silicon.<sup>23</sup> However, when the thickness of the Ag layer is only 4 nm, as shown in Fig. 2(a), some isolated Ag islands are observed to be connected with each other, and the top  $V_2O_x$  film is mixed with the Ag layer, which exhibits a meandering variation.<sup>16</sup> A continuous Ag film can increase the back surface reflectance at long wavelengths, which is beneficial for the performance of MLBC solar cells.

The  $V_2O_x$  films were investigated using X-ray photoelectron spectroscopy (XPS) both with and without introducing an  $O_2$  partial pressure of  $2 \times 10^{-2}$  Pa into the evaporation process. Fig. 2(c) and (d) show the  $2p_{1/2}$  and  $2p_{3/2}$  spectra indicative of the  $V^{5+}$  and  $V^{4+}$  valence states without and with an introduced  $O_2$  partial pressure, respectively. The  $V^{4+}$  valence state, corresponds to an O vacancy at the vertex of an octahedron in the amorphous  $V_2O_x$  network.<sup>24</sup> Based on core level peak areas, the stoichiometry of  $x = 4.89$  and  $x = 4.84$  can be extracted corresponding to  $V_2O_x$  films with and without  $O_2$  partial pressure. It is interesting that the concentration of O vacancies can be reduced when an  $O_2$  partial pressure of  $2 \times 10^{-2}$  Pa is introduced into the evaporation process. The work functions ( $E_F$ ) of

the  $V_2O_x$  films fabricated both with and without introducing an  $O_2$  partial pressure of  $2 \times 10^{-2}$  Pa into the evaporation process were investigated using ultraviolet photoemission spectroscopy (UPS). As shown in Fig. 2(e), the low O vacancy concentrations in the  $V_2O_x$  film owing to the introduction of an  $O_2$  partial pressure leads to a higher work function of 5.88 eV, and also induces greater band bending in the  $V_2O_x/Si$  junction.<sup>12</sup> Furthermore, Fig. 2(f) shows that the energy level ( $E_t$ ) of the O-deficiency in-gap defect state in the bulk of the  $V_2O_x$  film is transferred from a defect levels ( $E_t - E_F = 1.9$  eV) to a shallower defect level ( $E_t - E_F = 1.7$  eV) with the introduction of an  $O_2$  partial pressure, which results in reduced bulk recombination in the  $V_2O_x$  film.<sup>12,25</sup> Therefore, the optimized  $V_2O_x$  films with a high work function and reduced O-deficiency in-gap defect state energy were applied in MLBC solar cells.

Fig. 3 presents the dependence of the characteristic device performance parameters on the thickness of intermediate Ca, Ag, and Au metal layers in VMV multilayer structures, which respectively feature work functions of 2.90 eV,<sup>26</sup> 4.62 eV and 5.40 eV.<sup>27</sup> Fig. 3(a) shows that the average efficiency of MLBC solar cells employing 4 nm Au and 12 nm Ag layers in VMV emitters is improved by 1.20% and 0.78%, respectively. Fig. 3(b) shows that VMV (Ag)-emitter and VMV (Au)-emitter solar cells exhibit only minor differences in the short-circuit current density  $J_{SC}$  regardless of the metal layer thickness, and attain

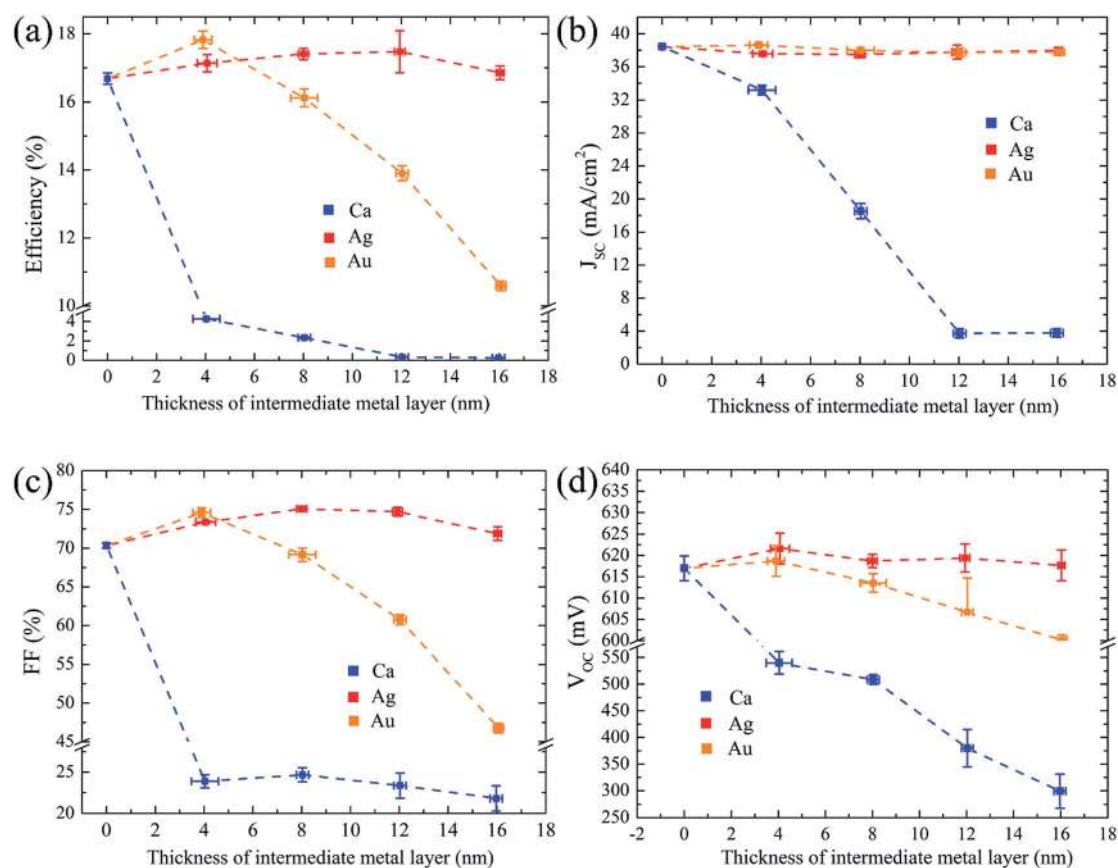


Fig. 3 Characteristic performance parameters (efficiency (a),  $J_{SC}$  (b), FF (c), and  $V_{OC}$  (d)) for the MLBC solar cells fabricated with different intermediate metal layer thicknesses for Ca, Ag, and Au metal layers.



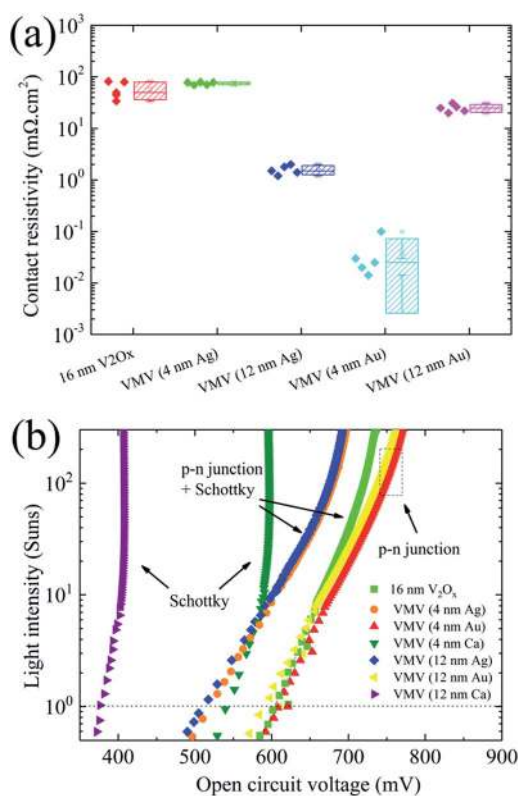


Fig. 4 (a) Contact resistivity for different emitter/n-Si contacts. (b) Suns- $V_{\text{OC}}$  measurement characteristics for MLBC solar cells featuring various emitter structures.

values of  $\sim 38 \text{ mA cm}^{-2}$ , which are greater than those of  $\text{MoO}_x/\text{n-Si}$  front junction solar cells employing excellent interfacial passivation.<sup>28</sup> For MLBC solar cells employing VMV (Ag) and VMV (Au) emitters, the FF increases by  $\sim 5\%$  and the  $V_{\text{OC}}$  values increase by  $\sim 10 \text{ mV}$ , as shown in Fig. 3(c) and (d), respectively. However, both the FF and  $V_{\text{OC}}$  decay for thicker Ag and Au layers. In the case of Au, the FF drastically decreases when thickness of metal increases will be studied in detail below.

It is of interest that MLBC solar cells employing a low work function Ca layer exhibited an S curve (see Fig. S4†), and uniformly demonstrated relatively poor device performance. In general, however, the FF and  $J_{\text{SC}}$  are primarily influenced by the value of series resistance  $R_{\text{S}}$  (see Fig. S4†) and the optical performance for Ca, Ag, and Au layers, which have similar resistivity ( $\sim 10^{-6} \Omega \text{ cm}$  at 300 K)<sup>15</sup> and rear side reflection.<sup>27</sup> This indicates that the ultra-low work function of Ca exerts a negative effect on the interfacial carrier transport and contact resistivity of the VMV (Ca)/n-Si contact.

The electrical contact properties and suns- $V_{\text{OC}}$  measurements of VMV-based hole-selective contacts with n-Si were characterized, and the results are shown in Fig. 4. As shown in Fig. 4(a), VMV/n-Si contacts generally have lower  $\rho_{\text{c}}$  values compared with the (16 nm)  $\text{V}_2\text{O}_x/\text{n-Si}$  contact ( $\rho_{\text{c}} = 42 \text{ m}\Omega \text{ cm}^2$ ) due to the injection of electrons from the metal layer into the  $\text{V}_2\text{O}_x$  layer, which improves its charge carrier concentration. It is worth noting that the averaged  $\rho_{\text{c}}$  values of VMV (12 nm Ag)/n-Si and VMV (4 nm Au)/n-Si are  $\rho_{\text{c}} = 1.58 \text{ m}\Omega \text{ cm}^2$  and  $\rho_{\text{c}} = 0.04 \text{ m}\Omega \text{ cm}^2$ , respectively. In addition, while the  $\rho_{\text{c}}$  value of VMV (12 nm Au)/n-Si is greater than that of VMV (4 nm Au)/n-Si, the FF

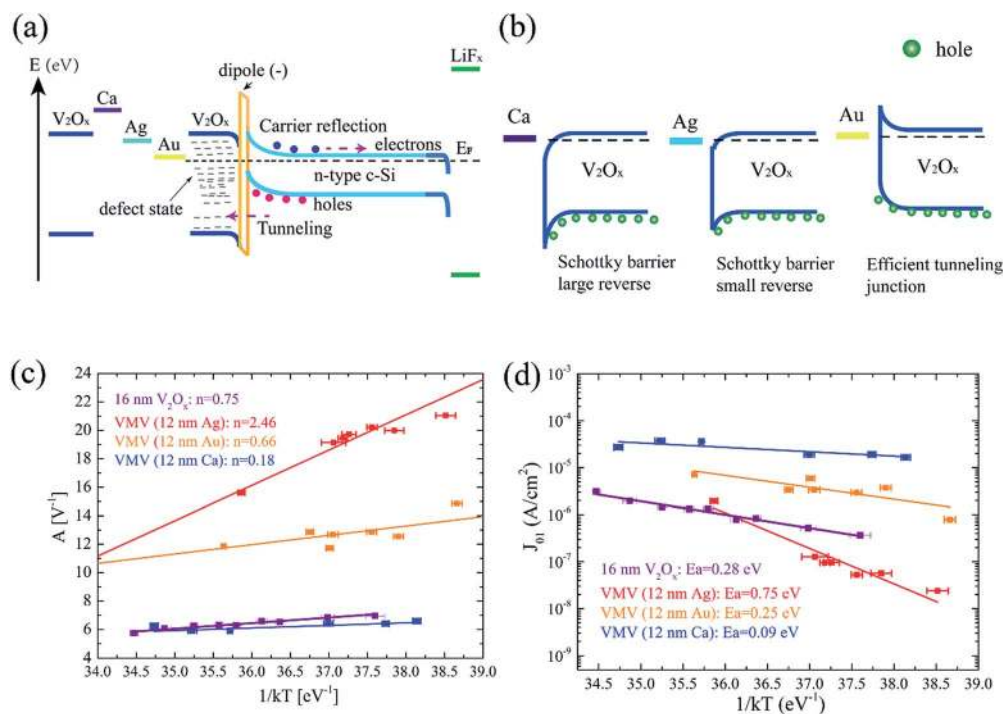


Fig. 5 (a) Band diagram for MLBC solar cells and (b) detailed band structures of  $\text{V}_2\text{O}_x$ /intermediate metal contacts in VMV emitters. (c) The temperature dependence of the exponential factor ( $A$ ) for the MLBC solar cells in a high forward-bias voltage ( $>400 \text{ mV}$ ) condition. (d) The activation energies ( $E_{\text{a}}$ ) for each diode extracted from the Arrhenius plots  $J_{01}$  versus  $1/kT$  in the high forward-bias voltage ( $>400 \text{ mV}$ ) condition.



corresponding to its use in solar cells is also more than 15% less than that of VMV (4 nm Au)/n-Si solar cells (Fig. 3(c)). However, the VMV (Ca)/n-Si contact exhibits a rectifying characteristic (see Fig. S5†). The physical mechanism by which the VMV (Au) and VMV (Ag) stacks reduce the contact resistivity is not yet clear and further research is needed. Interestingly, Fig. 4(b) shows that the VMV (Au)/n-Si solar cell improves the charge carrier transport dramatically, resulting in an induced p–n junction. A Schottky barrier occurs in  $V_2O_x$ /n-Si, VMV (4 nm Ag)/n-Si, and VMV (12 nm Ag)/n-Si solar cells with a lowering of the Schottky barrier. In VMV (Ca)/n-Si solar cells, a strong influence of the Schottky contact on the suns– $V_{OC}$  characteristic is observed in the emitter bulk, and generates a voltage opposite to the induced p–n junction voltage, which leads to a reversal in the suns– $V_{OC}$  curve above 10 suns.<sup>27</sup>

Fig. 5(a) presents an energy band diagram of an MLBC solar cell in equilibrium, which shows large band bending in n-Si for the extraction of holes at the interface between the n-Si absorber and the bottom  $V_2O_x$  layer. For the three intermediate layer metals, the work functions of Ca and Ag are much less than that of  $V_2O_x$ , as shown in Fig. 5(b). The high Schottky barrier and reverse bias of VMV (Ca) interfered with hole transport when used as an emitter for MLBC solar cells, resulting in a low  $J_{SC}$ . Furthermore, the quality of interface passivation mainly impacts the high forward-bias voltage (>400 mV) condition, and thus determines the value of  $V_{OC}$ .<sup>29</sup> Therefore, in this case, we mainly focus on charge carrier transport at the interface under high injection levels, and establish the temperature dependencies of exponential factor  $A$  and recombination current density  $J_{01}$  for MLBC solar cells employing VMV (Ag), VMV (Au), and VMV (Ca) emitters. As can be seen from Fig. 5(c), the diffusion–recombination model is dominant at the interface of VMV (Ag)/n-Si and VMV (Au)/n-Si contacts due to the increase in the exponential factor  $A$  with increasing  $1/kT$ .<sup>29,30</sup> Meanwhile, the multi-tunneling capture emission (MTCE) model determined the charge carrier transport property between  $V_2O_x$ /n-Si and VMV (Ca)/n-Si contacts at a high forward-bias voltage because the  $A$  values remain fairly stable with increasing  $1/kT$ .<sup>31</sup> The MTCE process is more related to the bulk recombination in the emitter than to interface defect states, and, thus, the use of VMV (Ca) as an emitter produces a larger recombination rate and lower  $V_{OC}$ , as shown in Fig. 3(d). Fig. 5(d) shows the influence of Ca, Ag, and Au metal layers on the emitter bulk recombination mechanism at the VMV/n-Si contact interface of MLBC solar cells. The largest activation energy ( $E_a = 0.75$  eV) obtained for an MLBC solar cell employing a VMV (12 nm Ag) emitter is greater than half the energy gap of n-type c-Si (i.e.,  $E_g/2 = 0.56$  eV). Moreover, the value of  $E_a$  for an MLBC solar cell employing a VMV (12 nm Au) emitter is close to that of a cell employing a 12 nm  $V_2O_x$  emitter. Finally, the MLBC solar cell employing a VMV (12 nm Ca) emitter exhibited the lowest value of  $E_a$ , which may be explained by the fact that the increased recombination in the VMV (12 nm Ca) emitter bulk is due to the existence of a large Schottky barrier and reverse bias.<sup>30</sup> Consequently, the use of a VMV (12 nm Ag) as an emitter in an MLBC solar cell can provides the largest value of  $E_a$  ( $E_a = 0.75$  eV) of all

the emitters considered, which is also in good agreement with the increased  $V_{OC}$  shown in Fig. 3(d).<sup>29</sup>

Fig. 6(a) shows the  $J$ – $V$  curve of an optimized VMV (4 nm Au)/n-Si solar cell with  $\sim 200 \Omega \text{ sq}^{-1}$  front surface field passivation (see Fig. S6†), which produce improvement of  $V_{OC}$  by 25 mV. The detailed parameters for this optimized MLBC solar cell are listed in Table 1 along with those of other state of the art back-contact dopant-free solar cells for comparison. The MLBC solar

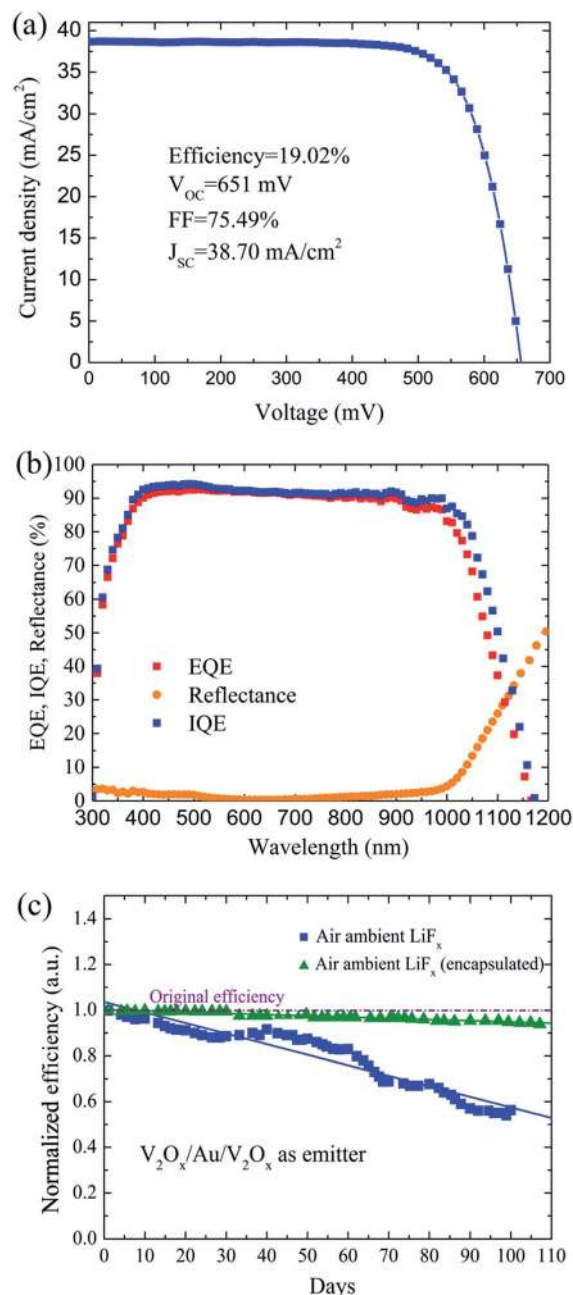


Fig. 6 (a) The average  $J$ – $V$  response of the best MLBC solar cell employing VMV (4 nm Au) as the hole-selective contact (AM1.5G standard illumination). (b) External quantum efficiency (EQE), internal quantum efficiency (IQE), and reflectance responses. (c) The stability of bare and epoxy resin encapsulated MLBC solar cells employing VMV (4 nm Au) emitters in ambient air.



**Table 1** State characteristic parameters for state of the art of dopant-free solar cells measured under standard test conditions (AM1.5G, 100 mW cm<sup>-2</sup>, and 25 °C)

| Structure                 | Emitter                             | BSF                             | V <sub>OC</sub><br>(mV) | J <sub>SC</sub><br>(mA cm <sup>-2</sup> ) | FF<br>(%) | η<br>(%) |
|---------------------------|-------------------------------------|---------------------------------|-------------------------|---|-----------|----------|
| Back contact              | VMV<br>(4 nm Au)                    | LiF <sub>x</sub>                | 651                     | 38.70                                     | 75.49     | 19.02    |
| Back contact              | 20 nm V <sub>2</sub> O <sub>x</sub> | LiF <sub>x</sub>                | 635                     | 38.65                                     | 71.65     | 17.58    |
| Back contact <sup>a</sup> | 15 nm V <sub>2</sub> O <sub>x</sub> | CS <sub>2</sub> CO <sub>3</sub> | 610                     | 38.85                                     | 70.00     | 16.59    |
| Back contact <sup>b</sup> | 10 nm MoO <sub>x</sub>              | LiF <sub>x</sub>                | 561                     | 36.80                                     | 74.60     | 15.40    |

<sup>a</sup> Data taken from ref. 9. <sup>b</sup> Data taken from ref. 5.

cell employing the VMV (4 nm Au) multilayer as the emitter exhibited the highest efficiency of all cells considered, which is 1.44% greater than the efficiency of an optimized MLBC solar cell employing a V<sub>2</sub>O<sub>x</sub> layer as the emitter (with an equivalent FSF). It can be seen from Fig. 6(b) that the IQE is less than 90% for wavelengths greater than 550 nm. This loss is due to electrical shadowing attributed to the recombination of gap and BSF areas, especially, the BSF has a strong impact on the charge collection probability in the base.<sup>32</sup> The gap between the emitter layer and back surface field is without any passivation. The surface recombination velocity of the bare silicon is quite high. It would be better to passivate this region in future. Moreover, the moisture and impurities in the air have a substantial effect on the long-term performance of MLBC solar cells, as shown in Fig. 6(c). Here, we note that the efficiency of the optimized MLBC solar cell decreased nearly continuously over a 100 day period in ambient air because the exposure of V<sub>2</sub>O<sub>x</sub> causes the work function to decrease 1 eV until stabilizing.<sup>10</sup> Hence, the MLBC solar cell is encapsulated by epoxy resin, which demonstrates a high stability when stored in ambient for greater than 3 months.

## 4. Conclusions

We have developed a novel dopant-free V<sub>2</sub>O<sub>x</sub>/metal/V<sub>2</sub>O<sub>x</sub> multilayer-structured hole-selective contact, which is deposited by thermal evaporation at low-temperature for use in MLBC solar cells. The effect of the choice of metal and the thickness of the intermediate metal layer on the performance of an MLBC solar cell is the most important design criterion, and was therefore subjected to systematic investigation. An optimized MLBC solar cell employing VMV (4 nm Au) as an emitter demonstrated an efficiency of 19.02%, which represents an increase of 1.44% compared to an optimized MLBC solar cell employing a V<sub>2</sub>O<sub>x</sub>/n-Si emitter. Furthermore, MLBC solar cells encapsulated by epoxy resin demonstrated high stability when stored in ambient air. The high performance obtained from MLBC solar cells fabricated using low temperature multilayer film deposition and metal patterning techniques together with the simplicity of the solar cells themselves, suggest the great potential for improving back contact heterojunction silicon solar cells using structured and dopant-free emitters.

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