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Dual Heuristic Programming Excitation Neurocontrol for Generators in a Multimachine Power System

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Abstract – The design of optimal neurocontrollers that replace the conventional automatic voltage regulators for excitation control of turbogenerators in a multimachine power system is presented in this paper. The neurocontroller design is based on Dual Heuristic Programming (DHP), a powerful adaptive critic technique. The feedback variables are completely based on local measurements from the generators. Simulations on a three-machine power system demonstrate that DHP based neurocontrol is much more effective than the conventional PID control for improving dynamic performance and stability of the power grid under small and large disturbances. This paper also shows how to design optimal multiple neurocontrollers for nonlinear systems, such as power systems, without having to do continually online training of the neural networks, thus avoiding risks of instability.

Keywords: Multiple Neurocontrollers, Power System Stability, Voltage Regulation, Generators, Multimachine Power Systems, Adaptive Critics, Artificial Neural Networks.

I. INTRODUCTION

Power systems containing turbogenerators are large-scale nonlinear systems. The traditional excitation controllers for the generators are designed by linear control theory based on a single-machine infinite bus (SMIB) power system model. These SMIB power system mathematical models are linearized at specific operating points and then excitation controllers are designed. The machine parameters change with loading in a complex manner, resulting in different behavior at different operating points and the controller which stabilizes the system under specific operating conditions, may no longer yield satisfactory results when there is a drastic change in the power system operating conditions and configurations. Conservative designs are therefore traditionally used, particularly in multimachine systems, to attempt satisfactory control over the entire operating range of the power system.

In recent years, renewed interest has been shown in power systems control using nonlinear control theory, particularly to improve system transient stability [1,2]. Instead of using an approximate linear model, as in the design of the conventional power system stabilizer, nonlinear models are

used and nonlinear feedback linearization techniques are employed for the generator models, thereby alleviating the operating point dependent nature of the linear designs. Using nonlinear controllers, generator transient stability can be improved significantly. However, nonlinear controllers have a more complicated structure and are difficult to implement relative to linear controllers. In addition, feedback linearization methods require exact system parameters to cancel the inherent system nonlinearities, and this contributes further to the complexity of the stability analysis. However, the use of Artificial Neural Networks (ANNs) as neurocontrollers offers a possibility to overcome this problem.

Multilayer perceptron type artificial neural networks are able to identify/model time varying single turbogenerator systems [3] and, with continually online training, these models can track the dynamics of the power system, thus yielding adaptive identification. ANN controllers have been successfully implemented on single turbogenerators using ANN identifiers and indirect feedback control [4]. Adaptive critic design have also been applied to control generators in a SMIB power system successfully [5]. Moreover, ANN identification of turbogenerators in a multi-machine power system has also been reported [6].

The design and performance of nonlinear excitation neurocontrollers based on Dual Heuristic Programming (DHP) theory (a member of the adaptive critics family) for multimachine power systems, to replace the traditional Automatic Voltage Regulators (AVRs) are discussed in this paper. With DHP, optimal neurocontrollers can be designed offline, avoiding the computational load of online learning and the issues of instability. A three-machine power system with DHP excitation neurocontrollers on every machine is presented in this paper. The results show that both voltage regulation and system stability enhancement can be achieved with these proposed neurocontrollers, regardless of the changes in the system operating conditions and configurations. This paper also shows that it is possible to have multiple neurocontrollers controlling multiple generators simultaneously.

II. MULTIMACHINE POWER SYSTEM

The multi-machine laboratory power system in Fig. 1 is modeled in the MATLAB/SIMULINK environment using the Power System Blockset (PSB) [7]. Each machine is represented by a seventh order model. There are three coils on the d-axis and two coils on the q-axis and the stator transient terms are not neglected. A three machine five-bus power system is chosen, to illustrate the effectiveness of the adaptive critic based neurocontrollers. The power system in Fig. 1 consists of two generators and the third machine is the infinite bus.

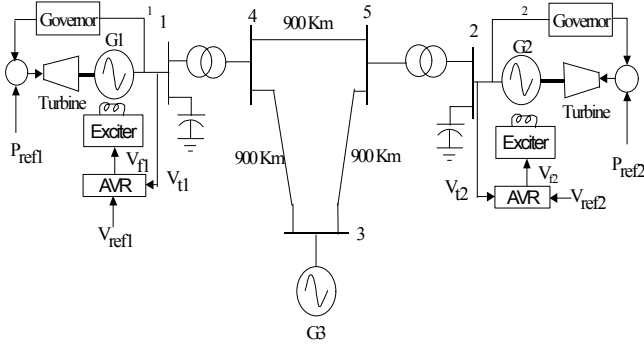


Fig. 1. Three machine five bus power system.

For the purposes of practical implementation studies at the University of Natal's machine research laboratory in South Africa, a simulation study on laboratory power system is carried out first. The laboratory power system consists of two generators, each 3 kW, 220 V, designed to have all their per-unit parameters, except the field winding resistance, the same as those normally expected of a 1000 MW generator. The parameters of the generators, determined by the IEEE standards are given in Table 1 [8]. A time constant regulator is used on each generator to insert negative resistance in series with the field winding circuit, in order to reduce the actual field winding resistance to the correct per-unit value.

The conventional AVR and exciter combination transfer function block diagram is similar for both generators and is shown in Fig. 2 and the time constants are given in Table 2. The exciter saturation factor S_e is given by

$$S_e = 0.6093 \exp(0.2165 V_{fd}) \quad (1)$$

T_{v1} , T_{v2} , T_{v3} and T_{v4} are the time constants of the PID voltage regulator compensator; T_{v5} is the input filter time constant; T_e is the exciter time constant; K_{av} is the AVR gain; V_{fdm} is the exciter ceiling; and, V_{ma} and V_{mi} are the AVR maximum and minimum ceilings.

A separately excited 5.6 kW dc motor is used as a prime mover, called the micro-turbine, to drive each of the generators. The torque-speed characteristic of the dc motor is controlled to follow a family of rectangular hyperbola for

different positions of the steam valve, as would occur in a real typical high pressure (HP) turbine cylinder. The three low pressure (LP) cylinders' inertia are represented by appropriately scaled flywheels. The micro-turbine and the governor transfer function block diagram is shown in Fig. 3, where, P_{ref} is the turbine input power set point value, P_m is the turbine output power, and $\Delta\dot{\omega}$ is the speed deviation. The turbine and governor time constants are given in Table 3.

Table 1. Generator parameters

| | | |
|---------------------|--------------------|---------------|
| $T_{d0}' = 4.50$ s | $X_d' = 0.205$ pu | $R_s = 0.006$ |
| $T_{d0}'' = 33$ ms | $X_d'' = 0.164$ pu | $H = 5.68$ |
| $T_{g0}'' = 0.25$ s | $X_q = 1.98$ pu | $F = 0$ |
| $X_d = 2.09$ pu | $X_q'' = 0.213$ pu | $p = 2$ |

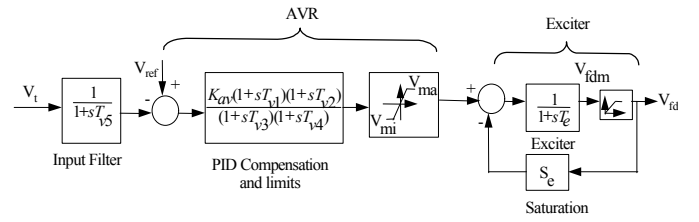


Fig. 2. Block diagram of the AVR and exciter combination.

Table 2. AVR and exciter time constants

| | | | |
|----------|---------|----------|----------|
| T_{v1} | 0.616 s | T_{v4} | 0.039 s |
| T_{v2} | 2.266 s | T_{v5} | 0.0235 s |
| T_{v3} | 0.189 s | T_e | 0.47 s |

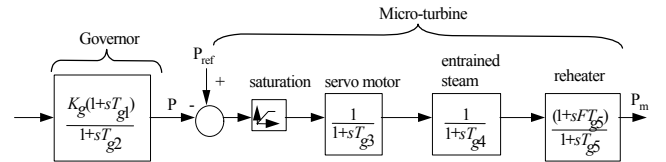


Fig. 3. Block diagram of the micro-turbine and governor combination.

Table 3. Micro-turbine and governor time constants

| | |
|--------------------------------------|--------|
| Phase advance compensation, T_{g1} | 0.264 |
| Phase advance compensation, T_{g2} | 0.0264 |
| Servo time constant, T_{g3} | 0.15 |
| Entrained steam delay, T_{g4} | 0.594 |
| Steam reheat time constant, T_{g5} | 2.662 |
| pu shaft output ahead of reheat, F | 0.322 |

III. DERIVATIVE ADAPTIVE CRITICS' BASED VOLTAGE CONTROLLER

Adaptive Critic Designs (ACDs) are neural network designs capable of optimization over time under conditions of noise and uncertainty. A family of ACDs was proposed by Werbos [9] as a new optimization technique combining concepts of reinforcement learning and approximate dynamic programming. For a given series of control actions, that must

Table 4. Operating points

| | Condition one | | Condition two | |
|------------|---------------|---------|---------------|---------|
| | G1 | G2 | G1 | G2 |
| P_e (pu) | 0.2000 | 0.2000 | 0.3000 | 0.3000 |
| Q (pu) | -0.0200 | -0.0200 | -0.0400 | -0.0400 |
| V_i (pu) | 1 | 1 | 1 | 1 |

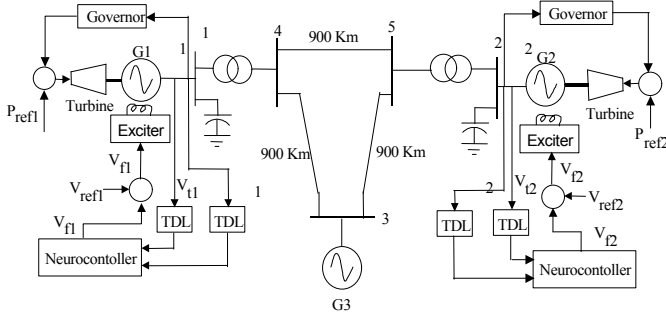


Fig. 6. Multi-machine power system with neurocontrollers on generators G1 and G2.

A. 3% Step change in V_{i1} at First Operating Condition

At the *first* operating condition (Table 4), a 3% step increase occurs in the desired terminal voltage of G1. Figs. 7 and 8 show that the DHP neurocontrollers ensure no overshoot on the terminal voltage and provides superior speed deviation damping unlike with the AVRs.

B. 5% Step Change in V_{i2} at Second Operating Point

At the *second* operating condition (Table 4), a 5% step increase occurs in the desired terminal voltage of G2. Figs. 9 and 10 show that the DHP neurocontrollers again provide the best damping, which prove that the neurocontrollers have learned and adapted themselves to the new operating condition. In fact, Fig. 10 shows signs of an inter-area mode oscillations starting up at about 4.3 seconds, and the neurocontrollers are far more successful in damping this, than the conventional designed AVRs.

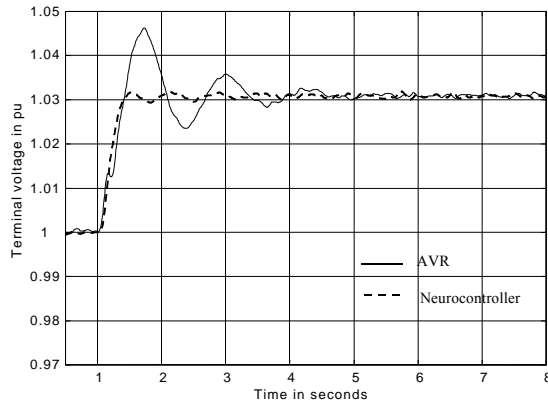


Fig. 7. Terminal voltage of generator G1 for a 3% step change in its desired terminal voltage.

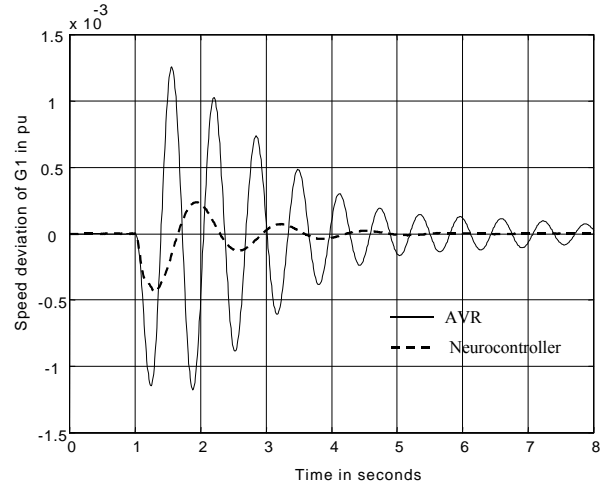


Fig. 8. Speed deviations of generator G1 for a 3% step change in its desired terminal voltage.

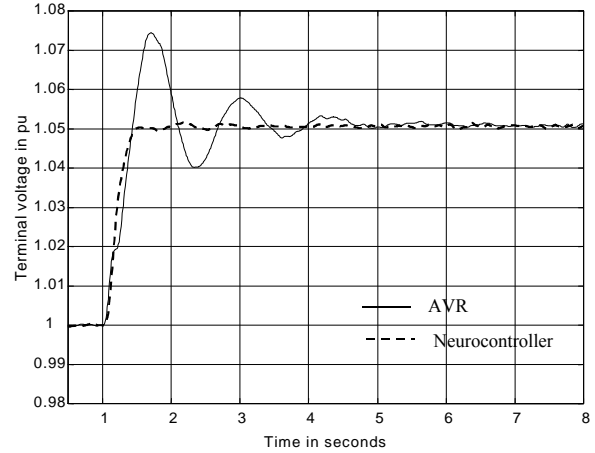


Fig. 9. Terminal voltage of generator G2 for a 5% step change in its desired terminal voltage.

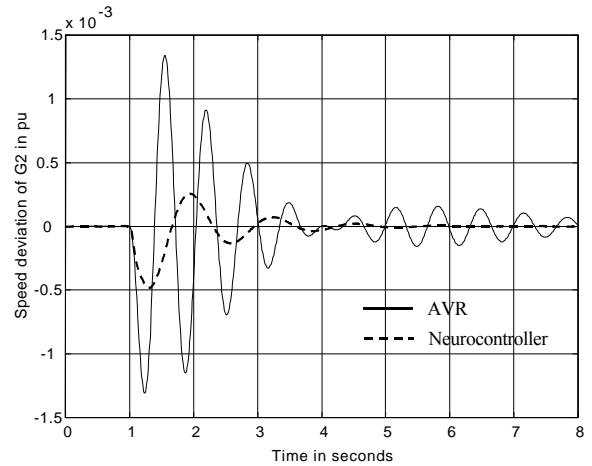


Fig. 10. Speed deviation of generator G2 for a 5% step change in its desired terminal voltage.

C. Three Phase Short Circuit

At the *second* operating condition (Table 4), a 100 ms short circuit occurs halfway between buses 3 and 4 (Fig. 6). Figs. 11 and 12 show that the DHP neurocontrollers again have a better damping on the speed deviation and terminal voltage of G1. Though not shown, this is seen also on the speed deviation and the terminal voltage of G2.

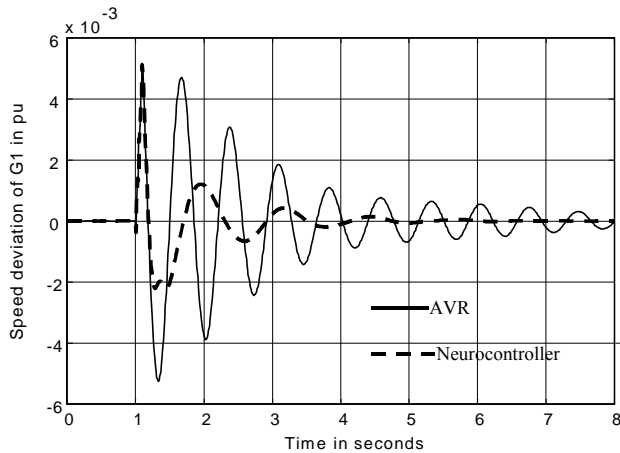


Fig. 11. Speed deviation of generator G1 for a 100 ms 3-phase short circuit between bus 3 and 4.

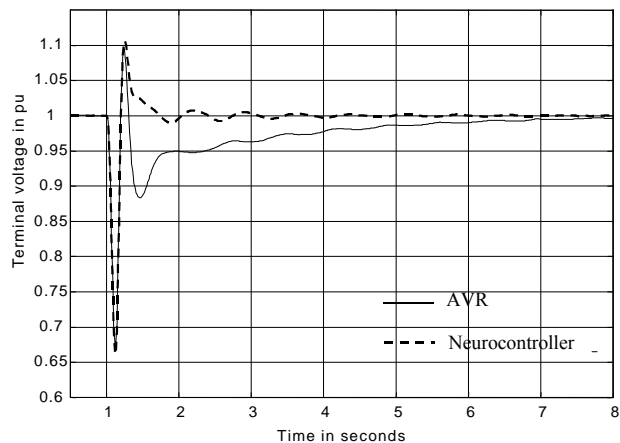


Fig. 12. Terminal voltage of generator G1 for a 100 ms 3-phase short circuit between bus 3 and 4.

All these results show that at operating conditions different from the one at which the AVRs were tuned, their performances have degraded. On the other hand, the DHP neurocontrollers have given excellent performance under all the conditions tested. Many other tests, both small and large disturbances, were carried out at different power levels and power factors to confirm this.

VI. CONCLUSIONS

A new design method based on derivative adaptive critics for voltage/excitation control of generators in a three machine power system have been presented. All control variables are based on local measurements, thus, the control is decentralized. Simulations show that dynamic response of the DHP based neurocontrolled generators are superior to the response of the conventionally controlled generators with AVRs, particularly so when operating conditions change and large disturbances are experienced. Furthermore, it has been shown that it is possible to have multiple optimal neurocontrollers on a power system with no requirement for online training. Thus, avoiding risks of instability with neurocontrol. Practical implementation of these DHP neurocontrollers are currently in progress.

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