MELLENED AN IS MAY 7 1975

SAND-75-0041 Unlimited Distribution

3151

EBW1: A COMPUTER CODE FOR THE PREDICTION OF THE BEHAVIOR OF ELECTRICAL CIRCUITS CONTAINING EXPLODING WIRE ELEMENTS

T. J. Tucker and R. P. Toth

Printed April, 1975

Sandia Laboratories

d Livermore; California 94550 for the United States Atomic mmission under Contract AT-(29-1) 789



1-2900-072-731

DISCLAIMER

This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency Thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.

DISCLAIMER

Portions of this document may be illegible in electronic image products. Images are produced from the best available original document.

Issued by Sandia Laboratories, operated for the United States Energy Research and Development Administration by Sandia Corporation.

NOTICE

This report was prepared as an account of work sponsored by the United States Government. Neither the United States nor the United States Energy Research and Development Administration, nor any of their employees, nor any of their contractors, subcontractors, or their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness or usefulness of any information, apparatus, product or process disclosed, or represents that its use would not infringe privately owned rights.



NOTICE This report was prepared as an account of work sponsored by the United States Government. Neither the United States nor the United States Energy Research and Development Administration, nor any of their employees, nor any of their contractors, subcontractors, or their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness or usefulness of any information, apparatus, product or process disclosed, or represents that its use would not infringe privately owned rights.

EBW1: A COMPUTER CODE FOR THE PREDICTION OF THE BEHAVIOR OF ELECTRICAL CIRCUITS CONTAINING EXPLODING WIRE ELEMENTS*

SAND 75-0041

· ...

T. J. Tucker R. P. Toth Explosives Physics Division 5131

Printed April 1975

ABSTRACT

Resistivity versus specific action data for 23 elemental metals and alloys are combined with a MIMIC language computer program to predict the behavior of electrical circuits containing exploding wire elements.

This document is PUBLICLY RELEASABLE							
Barn	Steels						
Authorizing Official							
Date: 7-	19-07						

l

*This work was supported by the U.S. Energy Research and Development Administration, ERDA.

DISTRIBUTION OF THIS DOCUMENT UNLIMITED

·

This page intentionally left blank.

CONTENTS

Pag	e					
Introduction						
Exploding Wire Behavior						
EBW1: Exploding Wire Circuit Analysis Code	I					
Circuit Definition						
Summary						
References						
Appendix 1 Theoretical Model of Exploding Wire Behavior						
Appendix 2 Metal Resistivity un-cm versus Specific Action (amp ² sec/mm ⁴) and Energy Density (joules/gram)						
Appendix 3 Subroutine SR1 Listing						
Appendix 4 Computer Code EBW1 Listing and Typical Output Results						

This page intentionally left blank.

. 4.

INTRODUCTION

The analysis and prediction of the behavior of electrical circuits containing exploding wire circuit elements, i.e., conductors pulse heated to melt or vaporization temperatures, is of importance in a number of applied situations. Included are such diverse fields as electrical fuse design, EEW detonator studies, and the pulse generation of high magnetic fields. To meet the needs of investigators, particularly those working with EEW detonators, several computer-based circuit-modeling codes have been developed.^{1,2,3,4} The two most widely used of these codes are those of Gold and Heinz (Ref. 2) and Blackburn and Muller (Refs. 3 anf 4). Although extremely useful within their range of applicability, each of these codes is limited by the lack of precise exploding wire resistance data for many metals.

Recently a general study on the behavior of metals at high temperatures using exploding wire techniques has begun to yield relatively accurate resistance profiles for a number of metals. It is the intent of this report to provide these data in a suitable format for use in computer circuit analysis. The form chosen is that of a Fortran subroutine (SRL) requiring only current and time inputs to produce a predicted exploding wire resistance as an output. To provide the greatest flexibility to the user, this subroutine has been combined with a "MIMIC" language main program providing a very simple representation of the electrical circuit differential equations.

EXPLODING WIRE BEHAVIOR

Experimental techniques for the measurement of the transient resistance behavior of exploding wires have been described elsewhere and will not be discussed in detail here.^{1,5,6} Briefly summarized, the resistance data presented were obtained using a high current (8000 A maximum) square wave generator capable of vaporizing a 0.127 mm diameter (.005 in) by 6.0 mm long wire in about 4 microseconds. A simplified diagram of this experimental apparatus is shown in Fig. 1 and an example of a typical output waveform is shown in Fig. 2. It should be noted that wire voltages are determined using a fourterminal technique to minimize effects of contact resistance. To suppress early arc breakdown all tests were performed with the wire covered by a thin covering of common rubber cement.*

It has been previously demonstrated that exploding wire resistivity at fixed current density may be uniquely specified as a function of either of two parameters, energy density, $e = 1/V \int I^2 R dt$, or specific action, $g = 1/A^2 \int I^2 dt$, where V, I, R, A, and t are initial wire volume, current history, resistance history, initial area and time, respectively. From Fig. 2 the relationship between these two parameters is clearly demonstrated in that energy density is simply the resistivity-specific action integral. The concept of action is further discussed in Appendix 1. It is of importance to note that the above representations for e and g are only approximate; because of rate effects, at very high current densities ($j = \sim 10^8 A/cm^2$) wire resistivity appears to decrease and specific action and energy at wire burst appear to increase with increasing j.^{1,6} The codes of Ref. 2 and Ref. 3 attempt to include this dependency, and

 $^{{}^{\}star}$ Best Test paper cement, Union Rubber and Asbestos Company, Trenton, NJ.

it is hoped to ultimately expand this study to include current density effects. At present, however, the data presented here must be considered as those associated with current densities of about 10^7 A/cm^2 and that at higher current densities "anomalous" resistivity effects may occur.⁶ The resistivity versus specific action plot shown in Fig. 2 is typical of that for a number of metals: copper, gold and aluminum, for example. As indicated in the figures, distinct (and some not so distinct) regions can be identified.

By comparison to published thermodynamic data and theoretical models of exploding wire behavior the following regions are evident.⁷

- <u>Solid heating</u> Simple heating of the metal to its melting point. The precise determination of the end of this region is often difficult to estimate from experimental data since no sharp discontinuity associated with the beginning of melting is observed.
- Melting The wire exists as a two-phase material of liquid and solid. The end of this region is generally well defined and may be precisely identified for all metals thus far tested.
- 3. <u>Heating of the liquid</u> Typically a region of little curvature, in which the slope may be relatively large for such metals as gold and copper or approach zero for many refractory metals. Again, the actual transition point from heating of the liquid phase to vaporization is difficult to define and, in fact, evidence exists that superheating of the liquid commonly occurs.
- 4. <u>Vaporization</u> The region is characterized by a very rapid increase of resistance associated with a decrease in wire cross-section. If system voltages are sufficiently high, the resistance rise is terminated by an arc breakdown through the wire vapor;⁶ shunting of the current by this low resistance arc results in a resistance maximum often designated the "spike" or "burst" resistance.

- 5. <u>Arc growth</u> Properties of this region are determined by complex arc breakdown phenomena and have not been studied in detail. The region is characterized by a rapid fall in resistivity associated with the growth of the arc channel; resistivity in this region depends upon both the current profile following burst and upon external confinement.* For the data presented here the current was relatively constant and external confinement was minimal consisting simply of a thin coating of rubber cement over the wire.
- 6. <u>Extrapolated resistance</u> The indicated region is simply a continuation of the arc to times exceeding those normally monitored. In the data reported here extrapolated values of resistivity are generated by the function

$$\rho = \frac{K}{g}$$

where K is a constant selected to maintain continuity in ρ . At present the extrapolation only applies to wire explosions under conditions of continued current flow and moderate confinement.

The effect of confinement is particularly evident with high dielectric strength liquids, such as the 3M Company's Flourinert Electronic Liquids.

EBW1: EXPLODING WIRE CIRCUIT ANALYSIS CODE

Experimentally determined resistivity versus specific action and energy density plots for all metals thus far studied are presented in Appendix 2. It should be noted that phase transition points are also included in the figures. These transition points were obtained by inspection of the data to determine the clearly defined end of melt transition point for each metal. Utilizing the measured energies associated with the identifiable points, the melt transition points were estimated by subtracting handbook values of latent heat. Similarly, the vaporization transition points were estimated by adding the computed energy to heat the wire to vaporization temperature, i.e., e = liquid specific heat times the difference in vaporization and melting temperature. Finally, the arc (burst) transition was found by simple inspection of the data.

The general structure of the computer code EBWl is indicated in Fig. 3. As indicated, all resistivity versus specific action data are contained in subroutine SR1. A complete listing of SR1 is presented in Appendix 3.

By inspection, SRl can be seen to be primarily an array of metal resistivities (micro-ohm cm) versus specific action (amp² sec/mm⁴). Subroutine SRl computes the total specific action input into an exploding wire, based upon current and time input information from the main program, and determines from the tabulated data the associated instantaneous wire resistance to be returned. Since storage requirements for the wire data presently available are not prohibitively large, simple tabulation is possible. For the future, however, it is clear that the data bank could become excessively large, particularly in the case of describing resistivity as a function of both action and current density, and compaction of the data table will be required.

Existing spline fitting routines with knot placement at the transition points seem well suited for this purpose, and will be considered when time permits.

A summary list of all metals tested is presented in Table 1. Included in the table are the transition point values for the exploding wire data, which are compared to literature values of these parameters in Table 2. All metal specifications, i.e., wire diameter and purity, were assumed to be those stated by the supplier; a listing of these parameters is given in Table 3. As can be seen agreement is generally good; however, for a few metals, primarily those with a low melting and vaporization temperature, major differences are indicated. For these low temperature metals heating rate effects appear to be large even at moderate current densities. The majority of metals, however, exhibit burst energies below the handbook value of vaporization energy. This result is to be expected since not all of the wire is vaporized at the time of arc breakdown. It should be noted that tests reported here were done to survey the complete resistance profile, covering a range of several orders of magnitude. Considerably greater resolution is possible if testing is restricted to a more limited range such as early time solid and liquid behavior.

CIRCUIT DEFINITION

Although in principle any main program capable of describing the electric circuit equations and calling subroutine SRl could be utilized to describe exploding wire systems, a "MIMIC" language description has been found to be particularly advantageous.⁸ As an example of the simplicity of programming, consider the case of a capacitor discharge system. For this example the circuit equation is

$$L \frac{dI}{dt} + I(R+R_{W}) + \frac{1}{C} \int Idt = 0$$
 (1)

where, as indicated in Fig. 4, R, L, and C are system resistance, inductance and capacitance, R_{W} and I are instantaneous wire resistance and current, and t is time.

A MIMIC description of this circuit is presented in Appendix 4. Also indicated in the Appendix are the required circuit parameter data cards and the single data input card required by subroutine SRI to identify the exploding wire metal and dimensions. Control cards required to attach subroutines SRI and SR2 (a plotting file) from permanent file are also listed.

Finally, tabular and graphic output resulting from the program for parameter values typical of EBW detonator systems (L = 0.1 μ H, C = 1.0 μ F, R = 0.1 Ω , V_o = 1000 volts, 1.5-mil diameter by 40-mil long gold wire) are shown. The effect of the exploding wire resistance spike upon the normal damped sinusoidal current waveform of a capacitive discharge is clearly indicated.

With regard to EBW detonator studies it should be recalled that the 50% firing threshold can be predicted using the threshold burst current equation^{9,10}

$$I_{bth} = \frac{d}{\sqrt{\ell}} \left[850 + 35.5 \left[\frac{(\ell ds_o^P x 10^{-3} - 120)^2}{(\ell ds_o^P x 10^{-3})^{3/2}} \right] \left[\frac{1}{(1.88 - \delta)^3} \right]$$
(2)

where d and ℓ are wire diemeter and length and S_0^P and δ are explosive specific surface and density. Computer threshold burst currents (I_{bth}) for the actual and the theoretical minimum predicted from Eq. 2 are included in the tabular printout shown in Table 3. By comparison of these threshold values to the predicted burst current, it can be seen that the circuit considered should, as is observed, initiate an EBW detonator.

SUMMARY

It has been the purpose of this report to describe a versatile and flexible computer code developed for analyzing the behavior of electrical circuits containing exploding wire elements. The code presented here (EEWl and subroutine SRl) satisfies this requirement by combining the experimental results contained in an exploding wire study of 23 metals with a MIMIC language electrical circuit description. Although not described here, the code has also been found to be extremely useful in a complementary problem of predicting the transient resistance of metals carrying high surge currents. At present the data reported here cover only one current density, $\sim 10^7 \text{ A/cm}^2$. Some differences in wire behavior may be encountered at current densities greatly in excess to those used. It is to be hoped that future studies will be able to remove this limitation.

- Tucker, T. J., <u>A Survey of EBW System Analysis</u>: Past, Present, and Future, SLA-73-0543, October 1973.
- Gold, S. P. and Heinz, R. O., <u>Scurge: A Fortran X-Unit Simulation</u>, SCL-DR-64-45, August 1964, CRD.
- Blackburn, J. H. and Muller, G. M., <u>Exploding Wire Detonators: Resis-</u> tivity Functions and Initiation Criteria for Circuit Calculations, SC-CR-69-3201, June 1969.
- 4. Blackburn, J. H. and Muller, G. M., <u>Detonator Circuit Calculations</u>: Resistivity Functions, SC-CR-68, May 1968.
- 5. Tucker, T. J., <u>Square Wave Generator for the Study of Exploding Wires</u>, Rev. Sci. Instruments, Vol. 31, No. 2, 165-168, February 1960.
- Tucker, T. J., <u>Behavior of Exploding Gold Wires</u>, J. Appl. Phys., Vol. 32, No. 10, 1894-1900, October 1961.
- 7. Tucker, T. J., <u>A Theoretical Model of the Resistance Behavior of</u> Exploding Wires, SC-RR-71 0739, January 1972.
- 8. Sansom, F. J. and Petersen, H. E., <u>Mimic Programming Manual</u>, Tech. Rep. SEG-TR-67-31, Wright-Patterson Air Force Base, Ohio, July 1967.
- 9. Tucker, T. J., <u>Exploding Wire Detonators: Threshold Burst Current</u> <u>Dependence Upon Detonator and Environmental Parameters</u>, "Exploding Wires," Vol. 4, 211-232, W. G. Chace and H. K. Moore, eds., Plenum Press, New York, 1968.
- Tucker, T. J., <u>Explosive Initiators</u>, "Proceedings Behavior and Utilization of Explosives in Engineering Design, New Mexico Sec. of the ASME,
 L. W. Davison and J. E. Kennedy, eds.

		Melt Beginning		Melting End			Vapor Beginning			Burst			
Metal	ρ* ο	ρ	е	g	ρ	e	g	ρ	е	g	ρ	e	g
·	µΩ-cm	µΩ– cm	J/gm	$\frac{A^2 sec}{4}$ mm	μΩ-cm	J/gm	$\frac{A^2 sec}{4}$ mm	μΩ-cm	J/gm	$\frac{A^2 sec}{4}$ mm	µ∩-cm	J/gm	$\frac{A^2 sec}{4}$ mm
Copper	1.77	9.9	459	80492	18.9	663	94228	26.3	1409	124008	620	5909	173000
Aluminum	2.82	11.2	623	25238	23.1	1021	32035	41.5	2981	48561	393	9782	65776
Gold	2.44	12.1	124	42816	26.0	189	50180	49.3	472	64950	1124	1897	83157
Silver	1.59	8.6	245	61682	15.9	356	71771	27.3	710	90132	859	3425	112290
Platinum	10.0	61.1	235	14701	89.6	347	17979	96.2	656	24979	649	2260	48947
Nickel	7.8	59.2	674	17233	79.6	974	21156	83.4	1812	30173	666	5492	56007
Iron	10.0	119.2	910	12806	123.6	1200	14681	125.8	2295	21568	547	5613	36105
Palladium	11.0	47.0	393	16187	70.8	555	19583	69.8	933	25979	614	3466	51366
Rhodium	4.8	60.4	613	33617	76.1	824	37597	84.4	1384	46139	540	4193	73983
Vanadium	22	116.3	1450	12286	120.9	1777	13971	120.7	2415	17189	428	8715	42786
Tungsten	5.6	90.3	495	24270	116.1	637	27831	123.6	1042	34175	230	3936	75081
Cadmium	7.54	19.6	71	4550	34.1	125	6348	37.5	242	9169	1223	2491	18049
Tin	11.5	27.6	49	1727	50.7	107	2870	100.7	632	8023	1076	2233	12447
Molybdenum	5.7	85.8	1075	30582	93.1	1328	33451	93.6	2281	43350	185	5645	73952
Zirconium	44	147.1	577	3043	158.1	801	3999	159.1	1355	6267	681	4890	16655
Titanium	41	156.0	816	3034	163.5	1218	4163	158	2255	7074	613	7460	19261
Bismuth	120	353.1	40	166	144.9	93	435	196.3	286	1550	1920	760	2654
Scandium	63	325•3	605	685	336.5	977	1020	312.8	1750	1730	790	5074	4194
Lead	22	48.7	37	1283	90.7	60	1674	139.4	254	3587	,1385	1 9 83	5980
Zinc	5.8	16.0	161	11260	31.6	. 263	14484	29.4	497	19990	925	4472	38945
Uranium	28.	96.6	298	6551	. 98.4	351	7582	100.9	681	14011	353	2410	34701
70Au-30Pt	30.8	42.9	187	10387	64.4	265	13391	75.9	561	21572	987	2400	42689

TABLE 1: EXPLODING WIRE DETERMINATION OF METAL PARAMETERS

÷

•

*Handbook of Chemistry and Physics, 48th ed.

×.

.

TABLE 2: COMPARISON OF EXPLODING WIRE TO HANDBOOK PARAMETERS

# <u>78'0'</u> , <u>p 11'</u>	;	Melt Begin		Burst			
Metal	Handbook*	Measured	% Diff	H a ndbook ^{**}	Measured	% Diff	
	J/gm	J/gm		J/gm	J/gm	i	
Copper	463	459	9	5217	5909	+ 13.3	
Aluminum	663	623	- 6.0	10083	9782	- 3.0,	
Gold	147	124	-15.6	1861	1897	+ 1.9	
Silver	245	245	0.	2627	3425	+ 30.4	
Platinum	273	235	-13.9	2601	2260	- 13.1	
Nickel	807	674	-16.5	6762	5492	- 18.8	
Iron	1059	910	-14.1	6844	5613	- 18.0	
Palladium	436	393	- 9.9	3653	3466	- 5. 1	
Rhodium	639	613	- 4.1	5605	4193	- 25.2	
Vanadium	1202	1450	+20.6	9847	8715	- 11.5	
Tungsten	558	445	-20.2	4539	3936	- 13.3	
Cadmium	73	71	- 2.7	947	2491	+163.0	
Tin	51	49	- 3.9	2535	2233	- 11.9	
Molybdenum	850	1075	+27.6	6636	5633	- 15.1	
Zirconium	784	577	-26.4	5728	4890	- 14.6	
Titanium	1147	816	-28.9	9774	7460	- 23.7	
Bismuth	33	41	+24.2	1000	760	- 24.0	
Scandium	753	605	-19.7	8646	5074	- 41.3	
Le a d	41	37	- 9.8	912	1083	+ 18.7	
Zinc	165	161	- 2.4	1925	4472	+132.3	
Uranium	206	298	+44.7		2410		
70Au-30Pt	:	187	· · ·		2400	•	

* Thermophysical Properties of High temperature Solid Materials, Y. S. Touloukin, ed., Macmillan Co., NY (1967).

* Contributions to the Data on Theoretical Metallurgy, X. High-Temperature Heat-Content, Heat-Capacity and Entropy Data for Inorganic Compounds, K. K. Kelley, Bureau of Mines Bulletin 476, 1949.

** Contributions to the Data on Theoretical Metallurgy, III. The Free Energies of Vaporization of Inorganic Substances, K. K. Kelley, Bureau of Mines Bulletin, 383, 1935.

** Introduction to Solid State Physics, 2nd Edition, C. Kittel, p. 99, Table 4.3, Cohesive Energy of Metals, John Wiley and Sons, NY, 1960.

TABLE 3: METALS SPECIFICATIONS

Metal Material	Di a meter Mils	Purity %	Manufacturing Source
Copper	4	99•95	Sigmund Cohn Corp.
Aluminum	5	99.95	Permaluster, Inc.
Gold	5	99.99	Sigmund Cohn Corp.
Silver	5	99.99	Sigmund Cohn Corp.
Platinum	5	99.99	Engelhard Industries
Nickel	5	99.90	Permaluster, Inc.
Iron	6	99.90	Sigmund Cohn Corp.
Palladium	5	99.90	Engelhard Industries
Rhodium	5	99.90	Engelhard Industries
Vanadium	5	99•99	Leico Industries
Tungsten	5	99.90	General Electric
Cadmium	6	99•95	Leico Industries
Tin	7	99.90	Leico Industries
Molybdenum	4	99.90	General Electric
Zirconium	5	99•99	Leico Industries
Titanium	5	99.99	Leico Industries
Bismuth	6	99.90	Engelhard Industries
Scandium	10	99.90	Leico Industries
Lead	10	99.90	Leico Industries
Zinc	8	99.90	Leico Industries
Uranium	5		*
70 Au-30 Pt	5		Sigmund Cohn Corp.

Sigmund Cohn Corp., 121 So. Columbus Ave., Mt. Vernon, NY 10553 Permaluster, Inc., 1844 No. Keystone, Burbank, CA 91504 Engelhard Industries, 113 Astor St., Newark, NJ 07114 Leico Industries, 250 W. 57 St., New York, NY 10019 General Electric Co., 200 W. Broadway, Dover, OH 44622

*Obtained from LASL. Unknown purity and manufacturer.

EXPLODING BRIDGE WIRE STUDIES

using differential input oscilloscope technique







Typical resistivity vs. specific action profile

61

۸.



FIGURE 3.

Computer program EBW1 structure.





LRC circuit

This page intentionally left blank.

APPENDIX 1

Theoretical Model of Exploding Wire Behavior

APPENDIX 1:

Theoretical Model of Exploding Wire Behavior

To illustrate general characteristics of exploding wire resistance behavior consider a simplification of the quasi-static theoretical model developed in Ref. 7. Assume resistance change can be described in terms of two basic processes, heating of a given phase and change of phase.

From conservation of energy the heating process is described by

$$(jA)^2 \frac{\rho \ell}{A} dt = CMd\tau$$
 (1)

where j, A, ρ , ℓ , and t are current density, wire area, resistivity, length, and time and C, M, and τ are wire specific heat, mass and temperature. Rewriting Eq. 1 and integrating

$$g = \int j^2 dt = C\delta \int \frac{d\tau}{\rho}$$
(2)

where δ is the mass density of the metal.

Assume the resistivity is linearly dependent upon temperature, i.e.,

$$\rho = \rho_{i} (1 + \alpha \tau) \tag{3}$$

and thus

$$d\rho = \rho_{a} \alpha d\tau. \tag{4}$$

Substituting Eq. 4 into Eq. 2 and integrating

$$g = \frac{C\delta}{\rho_i \alpha} \ln \frac{\rho}{\rho_i}$$
(5)

and

$$\rho = \rho_{i} e^{\frac{\rho_{i} \alpha}{C \delta} g} .$$
 (6)

Now note the limit of Eq. 5 is

$$g_{\max} = \frac{C\delta}{\rho_{i}\alpha} \ln \frac{\rho_{\max}}{\rho_{i}}$$
(7)

where g_{max} and ρ_{max} are the end points of the heating phase, i.e., the melting or vaporization points. Substitution of Eq. 7 in Eq. 6 yields

$$\rho = \rho_{i}^{e} e^{\int g_{max} \ell n \frac{\rho_{max}}{\rho_{i}}} \quad 0 \le g \le g_{max} \quad (8)$$

To first approximation then, for heating of a single phase, wire resistivity varies exponentially with specific action. The dependence of resistivity upon specific energy $\epsilon = E/V$ follows directly from the relationship

$$\mathbf{e} = \int \rho d\mathbf{g} \quad . \tag{9}$$

From Eq. (5)

$$dg = \frac{C\delta}{\rho_i \alpha} \cdot \frac{d\rho}{\rho} \quad . \tag{10}$$

Substituting Eq. 10 into Eq. 9 and integrating

$$e = \frac{C\delta}{\rho_{i}\alpha} (\rho - \rho_{i})$$
(11)

 \mathbf{or}

$$\rho = \frac{\rho_{i}\alpha}{C\delta} e + \rho_{i} , \qquad (12)$$

and, as might be expected, resistivity varies linearly with specific energy. For phase change processes energy conservation yields

$$G \equiv gA^{2} = \int I^{2} dt = H \int \frac{dM}{R}$$
(13)

where H = latent heat. Assume a radial melting mode so that

$$R = \frac{R_1 R_2}{R_1 + R_2}$$
(14)

where R_1 and R_2 are the resistances of phase 1 and phase 2 material respectively.

From Eq. 14 it follows that

$$R = \frac{\rho_1 \rho_2 \ell}{\rho_1 A_2 + \rho_2 A_1} = \frac{\rho_1 \rho_2 \ell}{\rho_1 A_2 + \rho_2 (A - A_2)}$$
(15)

.

where ρ_1 , ρ_2 and A_1 , A_2 are resistivities and areas of phases 1 and 2 and A is the initial area, i.e., $A = A_1 + A_2$.

By substitution of Eq. 15 into Eq. 13 and simplifying it can be shown that

$$G = \frac{H\delta}{\rho_{1}\rho_{2}} \left[\frac{1}{2R^{2}(\rho_{1}-\rho_{2})} \right] \left[(\rho_{2}\rho_{1}\ell)^{2} - (R\rho_{2}A)^{2} \right]$$
(16)

and

$$G_{\text{max}} = \frac{H\delta}{2\rho_1\rho_2} \left[A^2(\rho_1 + \rho_2) \right]$$
(17)

and thus

$$g_{max} = G_{max} / A^2 = \frac{H\delta}{2\rho_1 \rho_2} (\rho_1 + \rho_2)$$
 (18)

$$R = \frac{\rho_{1}\rho_{2}\ell}{\sqrt{\frac{2(\rho_{1}-\rho_{2})\rho_{1}\rho_{2}G}{W\delta} + \rho_{2}^{2}A^{2}}}$$
(19)

 \mathbf{or}

$$\rho = \frac{\rho_1 \rho_2}{\sqrt{\frac{2(\rho_1 - \rho_2)\rho_1 \rho_2 g}{H\delta} + \rho_2^2}} \quad . \tag{20}$$

Combining Eqs. 18 and 20

$$\rho = \frac{\rho_{1}}{\sqrt{1 - \frac{\rho_{2}^{2} - \rho_{1}^{2}}{\rho_{2}^{2}} \frac{g}{g_{max}}}} \qquad 0 \le g \le g_{max} \qquad (21)$$

For most metals ρ_2 is typically greater than ρ_1 and the ρ vs g curve is concave upwards. If it is assumed that, prior to arcing, the resistivity of the metal vapor is very large, Eq. 21 becomes

$$\rho_{\text{vapor}} = \frac{\rho_{\text{liquid}}}{\sqrt{1 - \frac{g}{g_{\text{max}}}}}$$
(22)

and from the relationship $\epsilon = \int \rho dg$ it follows

$$\rho_{\text{vapor}} = 2 g_{\text{max}} \rho_{\text{liquid}} \left(\sqrt{1 - g/g_{\text{max}}} \right) \qquad (23)$$

For phase change processes the resistivity versus specific energy relationship can be shown to be

$$\rho = \frac{\rho_1}{1 - \left(\frac{\rho_2 - \rho_1}{\rho_2}\right)\frac{\epsilon}{H\delta}}, \qquad (24)$$

again a function concave upwards.

Finally, two additional equations predicting limits for vaporization are of value. From Eq. 22

$$g_{max} = \frac{g - g_v}{1 - (o_\ell / o)^2}$$
(25)

where

$$g_{total} = g_v + g_{max}$$

and from Eq. 23

 $e_{max} = 2 g_{max} \rho_{\ell}$.

(26)

3

. ھ

Thus

 $e_{total} = e_v + e_{max}$.

,

APPENDIX 2

Metal Resistivity $\mu\Omega$ -cm versus Specific Action (amp²sec/mm⁴) and Energy Density (joules/gram)












































This page intentionally left blank.

APPENDIX 3 Subroutine SRL Listing

	SUPPONTINE SPI (C.T. DT. TTOT. DUNI. DUN2. DUN3)
0.0.0.1.1	
000011	
000011	COMMON(TT / 1) = TA(300) = FA(300) = GA(300) = CA(300) = VA(300) = PA(300) = CA(300)
OUDUTÍ	
000011	
000011	
000011	
0.00011	A (1, 1) = 0 = 0 = 0 = 0 = 0 = 0
000012	A = A + A + A + A + A + A + A + A + A +
000017	A(1, 7) = -26765+0584(1, 8) = -339305+0584(1, 9) = -39995+05
000022	$A_{1} = 10 = -439867 + 15584 (1 - 11) = -474077 + 15584 (1 - 12) = -532967 + 105$
000023	A(1, 13) = -613475+058A(1, 14) = -652735+058A(1, 15) = -730275+05
000037	A(1, 15) = .76746F+058A(1, 17) = .80401F+058A(1, 18) = .83011F+05
000000	A(1, 19) = .84924F + 058A(1, 20) = .87296F + 058A(1, 21) = .89258F + 05
000050	A(1, 22) = -911375+058A(1, 23) = -923635+058A(1, 24) = -932825+05
000055	A(1, 25) = $.94256E+05$ (1, 26) = $.95802E+05$ (1, 27) = $.98487E+05$
000061	A(1, 23) = $.10236E+05$ (1, 29) = $.10441E+06$ (1, 30) = $.10787E+06$
000066	A(1, 31) = $.11247F+06$ (1, 32) = $.11637E+06$ (1, 33) = $.11993E+06$
000072	A(1, 34)= $.12421E+06$ (1, 35)= $.12799E+06$ (1, 36)= $.13176E+06$
000077	A(1, 37)= .13552E+06\$A(1, 38)= .13871E+06\$A(1, 39)= .14100E+06
000103	A(1, 40) = $.14345E+06$ (1, 41) = $.14556E+06$ (1, 42) = $.14750E+06$
000110	A(1, 43)= .14971E+058A(1, 44)= .15126E+068A(1, 45)= .15225E+06
000114	A(1, 46) = .15291E+06\$A(1, 47) = .15357E+06\$A(1, 48) = .15493E+06
000121	<u>A(_1, 49)</u> = .15602E+06 3 A(1, 50)= .15726E+06\$A(1, 51)= .15802E+06
000125	A(1, 52)= .15867E+05\$A(1, 53)= .15920E+06\$A(1, 54)= .16043E+05
000132	A(1, 55) = .16155E + 06
000135	A(1, 58) = .16531E+05A(1, 59) = .16625E+06BA(1, 60) = .16632E+05
000143	A(1, 61) = .16745E+065A(1, 62) = .16817E+065A(1, 63) = .16858E+06
000147	A(1, 64) = .15894E + 05 $A(1, 65) = .15893E + 06 $ $A(1, 66) = .16954E + 05$
000154	$A(1, 6) = \cdot 1/180t + 06 A(1, 68) = \cdot 1/180t + 06 A(1, 69) = \cdot 1/180t + 06$
000160	A(1, 73) = -1725000000000000000000000000000000000000
000171	$\frac{A(1_{0},7)}{2} = \frac{1}{2} \frac$
000171	AL 19 701- 17868ELN6\$AL 1, 801- 17020ELN6\$AL 19 701- 17004ELN6 AL 1 701- 17868ELN6\$AL 1, 801- 17020ELN6\$AL 1, 811- 17004ELN6
000170	A(1, R2) = -1R096F + 06TA(1, R3) = -1R202F + 06TA(1, R4) = -1R36RF + 06
000202	A(1, 05) = -1850550057(1, 05) = -1872654058(1, 05) = -188355405
000207	$A(1, AR) = (1.18977 \pm 0.584(1, R9) = (1.91025 \pm 0.684(1, 90) = (1.92535 \pm 0.6)$
000220	A(1, 91) = .19456F+068A(1, 92) = .19813F+068A(1, 93) = .20287F+05
000224	A(1, 94) = .20927E + 06\$A(1, 95) = .21582E + 06\$A(1, 96) = .22355E + 06
000231	B(1, 1) = .18640E+013B(1, 2) = .22838E+018B(1, 3) = .23228E+01
000235	B(1, 4) = .26946E+01\$B(1, 5) = .31062E+01\$B(1, 6) = .30372E+01
000242	B(1, 7) = .35901E+018B(1, 8) = .42167E+018B(1, 9) = .46367E+01
000246	B(1, 1N)= .46405E+01\$B(1, 11)= .52676E+01\$B(1, 12)= .61051E+01
000253	B(1, 13) = .666932 + 018B(1, 14) = .73736E + 018B(1, 15) = .87981E + 01
000257	B(1, 16)= .92178E+01\$B(1, 17)= .99203E+01\$B(1, 18)= .10622E+02
000264	B(1, 19) = .114665+02\$B(1, 20) = .12813E+02\$B(1, 21) = .139515+02
000270	B(1, 22) = .15440E+023B(1, 23) = .17136E+028B(1, 24) = .18129E+02
000275	B(1, 25) = .189122 + 028B(1, 26) = .19280E + 028B(1, 27) = .20077E + 02
000301	B(1, 28) = .205975 + 023B(1, 29) = .21104E + 023B(1, 30) = .21967E + 02
000306	B(1, 31) = .23190E + 028B(1, 32) = .24203E + 028B(1, 33) = .25236E + 02
000312	$B(1, 34) = .26370 \pm 0.25B(1, 35) = .27859E + 0.25B(1, 36) = .29387E +$
000317	$\frac{g(1, 3/1)}{2} + \frac{30855}{2} + \frac{0288}{1} + \frac{381}{2} + \frac{32392E}{2} + \frac{0288}{1} + \frac{391}{2} = -\frac{33993E}{2} + \frac{02}{2} + \frac{02}{$
000323	B(1, 40)= .35529540288(1, 41)= .37205E+0288(1, 42)= .39105E+02
000330	B(<u>1, 43) = .41102t+U28B(1, 44) = .42/99t+U28B(1, 45) = .44409E+02</u>
000754	51 Ig 451= +4795214U2351 Ig 471= +5245314U2351 Ig 481= +521951402
000341	$D_1 + 491 - 673000CTUCDOL + 201 = 67(074CTUCDUL + 211 = 600342CTUCDUL + 020000000000000000000000000000000000$
000347	って エチ ラビノー ものみエのいにていたみかて エチ ラフノー ものだのひとにていとわかて エチ ラタノー ものだうししとやひと

				•				-		•			
						_							
	000352	. В (1.	55) =	•705576	E+023B(1.	56) =_	•74596	E+02\$8(. 1.	57) =	•79169E+02
	000356	B (1,	58)=	.854156	E+02\$8(1,	59)=	•91733	E+02\$B(1,	60)=	10100E+03
	000363	B (1.	61) =	.116056	E+038B(1.	62)=	.13447	E+03\$B(1.	63)=	-16447E+03
	000367	B (1.	64) =	. 18744	+138B(1.	55)=	.19500	F+03\$B(1.	66) =	-25554E+03
	000374	BI	1.	671-	348446	21034B1	1	681-	42703	E + 0 3 4 8 1	1.	691 =	-50000E+03
	0000000		·	701-	590000		·····	741-	62000		. 57 4	721-	54000C+03
	000400	51	1.	707-			1.	(1)-			1.	727-	• J40002+0J
	000405	. В (1.	(3)=	• 49261	+0338(1	(4)=	. 44912	L+U3\$BU(1.	751=	•38618E+U3
	000411	в (1,	75)=	• 315558	E+03\$8(1,	77)=	.25540	E+03\$B(1.	78)=	-22065E+03
	000415	<u>B(</u>	1,	<u>79) =</u>	•194228	+03\$B(1,	80)=	.17841	E+03\$B(1,	81)=	.16198E+03
	000422	В (1,	= (58	.146849	E+03\$8(1.	83)=	.13470	E+03\$B(1,	84)=	12416E+03
	000427	Β(1,	85)=	.116926	E+03\$B(1,	86) =	.11042	E+03\$B(1,	87)=	.10626E+03
	000433	B(1.	88) =	.10354	-+03\$B(1.	89)=	.98870	E+0238(1.	90) =	.92848E+02
	000440	8(11	911=	. 86795	-+ 02\$B(1.	92)=	79929	+128B(1	931 =	.72440E+02
	000440	91	±7. 4	0.1 -	6 7 8 7 9 6		4	951-	55061	5×02401	1	961-	18954E+02
	000444		2		0000390		2	21-				71-	+ E 1 / E E + 0/
	000421	<u>A (</u>	<u> </u>	=	.000006	TUUPAL		2.1 =	+1453	C TUSPAL	<u></u>	· · · · ·	•13143E+04
	000454	A	2,	4]=	•53956t	-+ U4 \$A (2.	5)=	.963851	E+045A6	2,	6)=	+14/541.+02
	000461	A (21	=	19405	=+05\$A(2.	8)=	•21515	E+05\$A(2,	3) =	•24321E+05
	000465	A (2,	10) =	•259368	E+05\$A(2,	11)=	-27307	E+05\$A(2,	12)=	29510E+05
	000472	A.(.	2.	(13) =	.310965	E+05\$A(2.	14)=	.31753	E+05\$A(2,	15)=	.32349E+05
	000476	Α (·	2,	16) =	.331585	E+053A(2,	17)=	.34561	E+05\$A(2,	18) =	.36269E+05
	000503	Α (2.	19) =	. 397448	F+058A(2.	20)=	.42335	E+05\$A(2.	21) =	.45175E+05
	000507	Δ (2.	221 =	. 488956	F+05\$4(2.	231 =	-51291	E+05\$4(2.	241=	-52936E+05
	000514	Δ (2.	251=	.536079		2	261 =	54091	E+0584(2.	27) =	545295+05
	000520		2	291-	E1.97E		2	201-	EE1061		2	30)-	554025405
	000520		<u> </u>	201-	• 540750		29	2 31	• 227 20	CTUSDAL	~ ,	771-	• 99403E+09
	000525	AL	2 1 .	31)=	. 55609	-+U55AL	٢,	321=	.50054	E+053A(۷,	331=	• 70/07 <u>c</u> +07
	000531	A (2,	34) =	•57251	2+U5\$A(2,	351=	•57889	E+05\$A(2,	36)=	·50515E+U5
	000536	<u> </u>	2,	37) =	<u>•59430</u>	+05 BA (2,	38)=	.59987	<u> </u>	21	37) =	.60542E+05
	000542	A (2,	40)=	• 609868	E+05\$A(2,	41)=	•61361	E+05\$A(2,	42) =	•61692E+05
	000547	<u>A (</u>	2,	(43) =	.61955	E+05\$A(2,	44)=	•623261	E+05\$A(2.	45) =	.62759E+05
	000553	A (2,	46) =	·632478	E+05\$A(2,	47) =	.63736	E+05\$A(2,	48)=	.64230E+05
	000560	Α (2,	49) =	.645858	E+05\$A(2,	50)=	.65033	E+05\$A(2.	51) =	.65315E+05
	000564	A (2.	52) =	.653898	E+05\$A(2.	53)=	.65776	E+053A(2.	54) =	.65904E+05
	000571	A	2.	55) =	. 66033F	+05\$A(2.	56)=	.668099	+ 05 \$A (2.	57) =	.67143E+05
	000575	Δ (2.	58) =	. 677146		2.	591=	68197	+ 05 \$ 4 (2.	601=	-68659E+05
	000515		2	611-	630775		2	621-	605760		2	631-	600805+05
	000002			611-	70106			6 5 1 -	71055		2	661-	740605405
	000000		<u> </u>	(7)-	-704205		29	021-	• 7 1 0 2 21	2703DAL	C •	601-	•/194UE+U2
	000613	A (۷.	67)=	•/32135	-+U5\$A(2,	681=	•/45151	-+U5 6A L	2,	691=	·/5350E+05
	000617	A (2.	/0)=	•/50146	+ 05 %A (2.	/1)=	•//49/	2+055A(2,	72)=	·/9165E+U5
	000624	<u>A (</u>	2,	(3) =	. 50694:	+05\$A1	29	741=	•8236UL	+ U5 \$A (29	<u> 75)=</u>	.842042+05
	000630	A (Ζ,	76)=	• 85338E	E+05\$A(2,	77)=	•877471	E+05%A(2,	78)=	•89112E+05
	000635	Α (2,	79) =	•90037E	E+053A (2,	= (08	•92614	E+053A(2.	81)=	•00000E+00
	000640	8(2,	1)=	•30123E	E+01\$B(2,	2)=	• 375 928	E+01\$B(2,	3) =	•40186E+01
	000645	BC	2.	4) =	. 462228	E+0138(2,	51=	.504856	E+01\$8(2,	5) =	.71090E+01
	000651	B (2,	7)=	.83139E	E+01\$B(2,	8) =	.962186	E+01\$B(2,	9) =	11156E+02
	000656	B (2,	10) =	.111705	E+02\$B(2,	11)=	.13033	E+0238(2,	12)=	.16656E+02
	000662	8(2.	13) =	.20703	+0288(2.	14) =	.22564	E+02\$8(2.	15)=	.23663E+02
	000667	8(2.	(6) =	-24656	+02\$8(2	17)=	-26098	F+023B(2.	18)=	-27440F+02
	000673	B(2.	19)=	- 314456	+02\$8(2	2(1) =	.33919	+02180	2.	21)=	-36931E+02
	000700		2.	221-		L02\$8(2	231-	. 451018	E 1 1 2 2 8 1	2.	241-	483256402
	000706		2	261-	1.05075		2	261-	51198		2	271-	62000EL02
	000704	51	29	291-	643237L		29	201-	= 911000 E 0 5 7 70		- - -	201-	+ JE JJJL + UE
	000745		29	211-	7:0073			271=	7=405		29	221-	- JOC DI ETUC
	000/15	80	٢,	511=	• / BUB/2	1702556	٢,	321=	+734050	2402386	٢.	331=	•/02U3E+U2
	000722	8.(2.	34) =	.820415	+02\$8(2,	35)=	. 85589	+U2\$B(<u>, Z</u> •	36)=	.88758E+02
	000726	8(Ζ,	37)=	• 925888	+02\$B(Ζ,	58)=	• 95 32 38	±+02\$8(2,	39)=	•98409E+02
	000733	8(2,	40)=	.10181E	+03\$B(2,	41) =	.10569	E+03\$B1	2,	42) =	11098E+03
	000737	8(2,	43) =	•11991E	E+03\$B(2,	44) =	.127671	E+03\$B(2,	45)=	•14540E+03
	000744	В (2,	46) =	.177278	+03\$B(Ζ,	47) =	.220756	E+03\$B(2,	48)=	·26402E+03
1	000750	31	2.	49)=	.30195F	+03\$B(2.	50)=	.348616	+03\$B(2.	51)=	.36840E+03
		3.	•								· •		

000755	B(2	. 52) = .	38246E+03\$B(2.5	3) =	39327E+0	35B(2.	54) = .37869E+03
000761	B(2	, 55) = .	36605E+03\$B(2, 5	6) = .	35946E+0	3\$8(2,	571= .35335E+03
000766	B1 2	. 58) = .	33447E+03\$B(2. 5	9) = _	30825E+0	3\$B(2.	60) = .27924E+03
000772	B(2	, 61)= .	23599E+03\$B(2, 5	2)= .	19964E+0	3\$B(2,	63)= .17785E+03
000777	B(2	. 64) = .	16309E+03\$B(2. 5	5)=	15352E+0	3\$B(2.	66) = .14411E+03
001003	B(2	, 67)= .	13399E+03\$B(2, 5	8)= .	12605E+0	3\$8(2,	69) = •12175E+03
001010	B(2	. 70) = .	11564E+D3\$B(. 2. 7	1)=	10442E+0	3\$8(2.	72)=95180E+02
001014	8(2)	, 73)= .	87909E+02\$B(2, 7	4)= .	82345E+0	2\$8(2,	75)= •78775E+02
001021	B(2	, 76) = .	<u>74969E+02\$B(</u>	2.7	7) = .	73226E+D	<u>2\$8(2.</u>	<u>78) = .71980E+02</u>
001025	B(2	, 79)= .	69986E+02\$B(2,8	8)= .	62494E+0	2\$81 2,	81) = .00000E+00
001031	A(3	(1) = (1)	<u>00000e+00\$A(</u>	3.	2)=	21933E+0	35A(3.	3) = .18560E+04
001035	A(3	• 4)= •'	96613E+04\$A(3,	5)= •	15023E+0	5\$A(3,	6) = .21214E+05
001041	A1 3	<u>• 7) = </u>	22603E+058A1	3,	8) =	25234E+0	58A(_3.	9) = .28267E+05
001046	A(3	, 10) = .	31076E+05\$A(3, 1	1)= .	33523E+0	5\$A(3,	121 = .36736E+05
001052	A(3	(13) = (13)	39312E+05\$A(3, 1	<u>4) = _</u>	41857E+0	58A(3,	15) = .43775E+05
001057	A (3	, 16) = .	44709E+05\$A(3, 1	7) = •	45784E+0	5\$A(3,	(18) = .46739E+05
001063	<u>A(3</u>	<u>• 19) = •</u>	4788 3E+ U5 \$A (<u> 3. 2</u>	\underline{U} = .	488591+0	<u>554(5</u> ,	211= 49475E+05
001070	A (3	, 22) = .	49900E+05\$A(3, 2	3)= •	50536E+0	5\$A(3,	24)= .51242E+05
001074	<u>A (5</u>	222 = 0	<u>527272+U55A(</u>	316	<u>915.</u>	542546+9	DAL ST	
001101	A ()	251 = -2	534045+05⊅Al 626205×05¢Al	3, 2	9/= • 2)-	5 7 7 4 0 E 7 0	2 DAL 39 6417 2	301 = 00107407
001102		$\frac{311 - 1}{713 - 1}$	5 7 0 0 7 5 4 0 5 4 4 /	<u></u>	<u>61-</u> .	60177EA0	<u>2.841 29</u> 5387 2	361- 704085+05
001112		9 341- AU	0/ 3335403 PA (71 21 75405 8 A (- Je J - 7. 7	$B_{1} = 0$	723235+0	58A1 3.	391 = .73424E + 05
001110	Δ(-3.		742965+15881	<u>9</u> 9 3. 4	(1) = 1	75096E+0	5%A(3.	42) = 104242000
001127	Δ (3)	431 = -1	763095+0534(3.4	(4) = -	76704E+0	58A1 3.	(45) = .77097E+05
001134	A (3	46) =	77336E+05\$A(3.4	7) =	77684E+0	58A(3.	48) = .78094E+05
001140	A(3)	49) =	78566E+05\$A(3.5	0) = .	79099E+0	58A(3.	511= .79563E+05
001145	A(3	· 52)= ·	80081E+05\$A(3, 5	3)= .	80428E+0	5\$A(3,	54) = .80788E+05
001151	A(3	55) =	81082E+05\$A(3, 5	6) = .	81366E+0	5\$A(3,	57) = .81727E+05
001156	A(3,	, 53)= .1	82070E+05\$A(3, 5	9)= .	82340E+0	5\$A(3.	50) = .82559E+05
001162	AL 3	61) = .	82705E+05\$A(3. 5	2)=	82857E+0	5\$A(3.	63) = .82963E+05
001167	A(3,	64) = 1	B3157E+05\$A(3, 6	5) = •	83359E+0	55A(3,	661 = .83510E+05
001173	<u> </u>	67) =	<u>83772E+058A(</u>	3. 6	<u>8) = </u>	84083E+0	55A(691 = .84375E+05
001200	A (3)	, 70) = .0	84741E+U5\$A(5, 7	1) = .	8517UE+U	58A(5,	721= .854326+05
001204	A (3)	$\begin{array}{c} 1 \\ 7 \\ 7 \\ \end{array}$	87/ <u>395</u> +05\$A(3 1	41= . 7\~	80U73E+U	52A1 3.4 Cerki 7	75) = 80453E+U5
001211		70)- •0	0090UETUDDAN 009565+050A/	2 g /	/J- • 0)-	07430240	5 5 4 1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	101 - 002430703
0012222	- <u>- 4.3 2.</u> A (- 3.	1 .[]/─ . 82)= (<u>977996409</u> 841 970165405881	3, 9	$(1 - 1)^{-1}$	10000E+0	2041 39 Nili	841 = 00000000000000000000000000000000000
001222	813	1)= -3	24737E+01\$R(3, 0	2) = -	22726E+0	1 TR (3.	31 = -23813E+01
001232	8(3)	(4) = -1	28962E+01\$B(3.	5) = .	38643E+0	1881 3.	6) = -46355E+01
001236	B(3)	7) =	56057E+01 \$B(3.	8)= .	56034E+0	1\$8(3.	9) = .62753E+01
001243	B(3	. 10) = .	7818E+01\$B(3, 1	1)= .	77884E+0	138(3,	12) = .91000E+01
001247	B(_3	13) = .	103155+02\$81	3, 1	4)= .	11841E+0	2\$B(3,	15) = .12396E+02
001254	3(3,	. 16) = .	L3165E+02\$B(3, 1	7)= .	14491E+0	2\$8(3,	18)= .16016E+02
001260	B(3	19) =	18754E+02\$B1	3.2	0)= .	21295E+0/	288(3.	211= .23961E+D2
001265	B(3	, 22)= .2	25321E+02\$B(3, 2	3)= .	26983E+0	2\$8(3,	24) = .28409E+02
001271	<u>B(</u> 3	25) =	<u>30237E+02\$B(</u>	3, 2	6)= .	32587E+0	238(3,	271= .35202E+02
001276	91 3,	, 28) = .	37257E+02\$B(3, 2	9)= .	39757E+0	2\$8(3,	30) = .42941E+02
001302	<u>B(3</u>	(31) = 0	46466E+02\$B(3, 3	2)= •	50038E+0	2\$8(3,	331 = .53749E+02
001307	B(3,	• 34)= • 9	56947E+023B(3, 3	5)= •	59827E+02	2386 3.	361 = .63374E+02
	<u>B(_3</u> ,	5() = 0	<u> 572545+U258(</u>	3.5	<u>015 </u>	111342+0		341= 10443E+02
001320	B(3)	p 401≓ p(//3>= /	507212+0238(394	17= • 48-	0007EE+0	2301 J. 2301 Z	421= •901996+02 451- 105755107
001324		<u>1.401</u> + 1 . 461-	241202486986	-3 <u>₽</u> 49	77- • 7)=	11311EA0	2481 7	4777 - +107775403 48)= -117655407
001331	0 U D 1	9 401- e. . (131	126615403981	່ງ, 4 ເ, ແ	()- • N)=	135075+0	3881 3.	
001342	RI 3	52)= -1	LA490-+03881	3. 5	(3) = -	189665+0		54)= _21934F+03
001346	B1 3	55)= -2	25305F+03\$B(3. 5	6) = -	30920E+0	3\$8(3-	57)= .39256F+03
001353	B1 3	58)=	54051F+038B(3. 5	<u></u>	70293E+D	3\$B(3	60)= .85794E+03

001761	B(4, 73) = .78126E + 0.28B(4, 74) = .69525E + 0.28B(4, 75) = .60118E + 0.28B(4, 75) = .6018E + 0.28B(4, 75) = .6018E + 0.28B(4, 75) = .6018E + 0
001766	B(4, 76) = .54388E+02\$B(4, 77) = .47471E+02\$B(4, 78) = .00000E+00
001771	A(5, 1) = .00000E + 008A(5, 2) = .34067E + 038A(5, 3) = .14170E + 04
001775	A(5, 4) = .38709E+04 $(5, 5) = .64681E+04$ $(5, 6) = .87878E+04$
002002	A(5, 7) = .11310E + 05SA(5, 8) = .13334E + 05SA(5, 9) = .14868E + 05
002006	A(5, 10) = .15226E+05\$A(5, 11) = .15940E+05\$A(5, 12) = .16839E+05
002013	A(5, 13) = .17544E+053A(5, 14) = .17824E+053A(5, 15) = .16057E+05
002017	A(5, 16) = .18406E+05\$A(5, 17) = .19080E+05\$A(5, 18) = .20171E+05
002024	A(5, 19) = .22072E + 058A(5, 20) = .24178E + 058A(5, 21) = .26926E + 05846E + 05846E + 0586E
002030	A(5, 22) = .29894E+05\$A(5, 23) = .31663E+05\$A(5, 24) = .33406E+05
002035	A(5, 25) = .34504E+05 $(5, 26) = .35350E+05$ $(5, 27) = .36194E+05$
002041	A(5, 28) = .37127E+05 $A(5, 29) = .37740E+05$ $A(5, 30) = .38261E+05$
002046	A(5, 31) = .38781E+05\$A(5, 32) = .39052E+05\$A(5, 33) = .39481E+05
002052	A(5, 34) = .39954E+05\$A(5, 35) = .40628E+05\$A(5, 36) = .41345E+05
002057	A(5, 37) = .41948E+053A(5, 38) = .42594E+053A(5, 39) = .43148E+053A(5, 39) = .43148E+053A(5, 39) = .43148E+053A(5, 38) = .42594E+053A(5, 39) = .43148E+053A(5, 38) = .42594E+053A(5, 38) = .445148E+053A(5, 38) = .42594E+053A(5, 38) = .445148E+053A(5, 38) = .44514E+053A(5, 38) = .44514E+0548E+0548E+0548E+0548E+0548E+0548E+0548E+0548E+0548E+0548E+0548E+0548E+0548E+0548E+0548E+0548E+0548E+058E+058E+058E+0000000000000000000000
002063	A(5, 40) = .43722E+05 $A(5, 41) = .44119E+05$ $BA(5, 42) = .44623E+05$
002070	A(5, 43) = .45103E+05 $BA(5, 44) = .45515E+05$ $BA(5, 45) = .45881E+05$
002074	A(5, 46) = .46350E+05 $BA(5, 47) = .46687E+05$ $BA(5, 48) = .47103E+05$
002101	A(5, 49) = .47307E + 05
002105	A(5, 52) = .48232E+05\$A(5, 53) = .48427E+05\$A(5, 54) = .48616E+05
002112	A(5, 55) = .48947E+05\$A(5, 56) = .49111E+05\$A(5, 57) = .49342E+05
002116	A(5, 58) = .49635E+05\$A(5, 59) = .49926E+05\$A(5, 60) = .50155E+05
002123	A(5, 61) = .50532E + 058A(5, 62) = .50942E + 058A(5, 63) = .51340E + 058A(5, 63) = .5140E + .514
002127	A(5, 64) = .51830E+05\$A(5, 65) = .52328E+05\$A(5, 66) = .52875E+05
002134	A(5, 67) = .53513E+05\$A(5, 68) = .54201E+05\$A(5, 69) = .55095E+05
002140	A(5, 70) = .55928E+05\$A(5, 71) = .57084E+05\$A(5, 72) = .58889E+05
002145	A(5, 73) = .61190E+05\$A(5, 74) = .63982E+05\$A(5, 75) = .66730E+05
002151	A(5, 76)= •70125E+05%A(5, 77)= •74141E+05%A(5, 78)= •74764E+05%
002156	A(5, 79) = .77575E+053A(5, 80) = .79119E+053A(5, 81) = .85778E+05
002162	A(5, 82)= .93000E+05%A(5, 83)= .00000E+00%A(5, 84)= .00000E+00
002165	$\frac{B(5, 1) = .10154E + 025B(5, 2) = .11500E + 025B(5, 3) = .14903E + 02}{247025 + 025B(5, 2) = .14903E + 02}$
002172	B(5) + 4I = -21392E + 025B(5) + 5I = -29762E + 025B(5) + 5I = -30165E + 025B(5) + 30165E + 30165E + 025B(5) + 30165E + 025B(5) + 30165E + 025B(5) + 30165E + 3015E + 30165E + 025B(5) + 30165E + 025B(5) + 30165E + 30165E + 025B(5) + 30165E
002170	$\frac{B(2)}{2} \frac{7}{1} = \frac{479261 + 02381}{2} \frac{2}{2} \frac{612}{2} = \frac{612}{2} \frac{2}{2} \frac{612}{2} \frac{1}{2} $
002203	B(5, 10)= +03502E+029B(5, 11)= +08035E+029B(5, 12)= +75973E+02
002244	$\frac{1}{2} = \frac{1}{2} = \frac{1}$
002214	0(5) 101 = 0.91024E + 0.28E(5) 171 = 0.92002E + 0.28E(5) 101 - 0.94012E + 0.28E(5) = 0.05402E + 0
002220	$\frac{B(2)}{2} \frac{1}{2} \frac$
002231	BL 5, 261- 49/4/254023BL 5, 261- 49010254028BL 5, 271- 4970335402 B/ 5, 261- 1002754034B/ 5, 261- 1017054034B/ 5, 271- 102785403
002231	$\frac{1}{1} = \frac{1}{1} = \frac{1}$
002250	B(5, 31) = .11271F + 038B(5, 32) = .11534F + 038B(5, 33) = .11802F + 03
	B(5, 34) = .11970F + 038B(5, 35) = .12255F + 038B(5, 36) = .12689F + 03
002253	B(5, 37) = .12982E + 038B(5, 38) = .13383E + 038B(5, 39) = .13870E + 03
002260	B(5, 40) = .14323F + 0.3 B(5, 41) = .14796F + 0.3 B(5, 42) = .15464F + 0.3
002264	B(5, 43) = .16251F+03\$B(5, 44) = .17105E+03\$B(5, 45) = .18349E+03
002271	B(5, 46) = .20316F+03\$B(5, 47) = .22853F+03\$B(5, 48) = .25977E+03
002275	B(5, 49) = .29534E+03B(5, 50) = .32193E+03B(5, 51) = .40253E+03
002302	B(5, 52) = .49734E+03\$B(5, 53) = .55196E+03\$B(5, 54) = .60228E+03
002306	B(5, 55) = .64881E+03\$B(5, 56) = .62627E+03\$B(5, 57) = .57600E+03
002313	B(5, 58) = .44761E+03\$B(5, 59) = .34964E+03\$B(5, 60) = .29559E+03
002317	B(5, 61) = .24572E+03B(5, 62) = .20978E+03B(5, 63) = .18891E+03
002324	B(5, 64) = .16904E+03\$B(5, 65) = .14998E+03\$B(5, 66) = .13666E+03
002330	B(5, 67) = .12436E+03\$B(5, 68) = .11167E+03\$B(5, 69) = .10095E+03
002335	B(5, 70)= .89469E+02\$B(5, 71)= .78977E+02\$B(5, 72)= .73308E+02
002341	B(5, 73) = .64967E+02\$B(5, 74) = .57712E+02\$B(5, 75) = .54815E+02
002346	B(5, 76) = .51924E+02\$B(5, 77) = .49565E+02\$B(5, 78) = .45722E+02
002352	B(5, 79) = .43810E+02 $B(5, 80) = .46698E+02$ $B(5, 81) = .45254E+02$
002357	B(5, 82) = .43398E+02\$B(5, 83) = .00000E+00\$B(5, 84) = .00000E+00

002765	B ($6 = 85$ = $-77630E \pm 0288(-6, -86) = -71697E \pm 0288(-6, -87) = -65275E \pm 02$	
002772	8(6, 88) = .62352E+02\$B(6, 89) = .00000E+00\$B(6, 90) = .00000E+00	
002775	AL	7. 1) = .00000E+00\$A(7. 2) = .20482E+03\$A(7. 3) = .48334E+03	
003001	A (7, 4) = .14997E+04\$A(7, 5) = .27984E+04\$A(7, 6) = .37312E+04	
003005	A	$7_{1} = -46741E + 043A(7_{1} = 8) = -52810E + 043A(7_{2} = 9) = -57674E + 04$	
003012	A (7, 10) = .62880E+04\$A(7, 11) = .67244E+04\$A(7, 12) = .71828E+04	
003016	A	7. 13)= .75227E+043A(7. 14)= .79312E+04\$A(7. 15)= .83138E+04	
003023	A (7, 16) = .87624E+04\$A(7, 17) = .92194E+04\$A(7, 18) = .94471E+04	
003027	<u>A (</u>	7, 19) = .96745E+04\$A(7, 20) = .98789E+04\$A(7, 21) = .10072E+05	
003034	Α (7, 22) = .10298E+05\$A(7, 23) = .10491E+05\$A(7, 24) = .10773E+05	
003040	Α (7, 25) = .11056E+05\$A(7, 26) = .11541E+05\$A(7, 27) = .12250E+05	
003045	A (7, 28) = $.13014E+05$ (7, 29) = $.13674E+05$ (7, 30) = $.14681E+05$	
003051	Α (7, 31) = .16009E+05\$A(7, 32) = .18306E+05\$A(7, 33) = .18918E+05	
003056	A (7, 34) = .20676E+05\$A(7, 35) = .21633E+05\$A(7, 36) = .22887E+05	
003062	<u>A (</u>	7, 371 = .23597E + 058A(7, 38) = .24470E + 058A(7, 39) = .24845E + 05	
003067	A (7, 40) = .25463E+05\$A(7, 41) = .25982E+05\$A(7, 42) = .26346E+05	
003073	Α (7, 43)= .26710E+05\$A(7, 44)= .27073E+05\$A(7, 45)= .27456E+05	
003100	Α (7, 46) = .27839E+05\$A(7, 47) = .28187E+05\$A(7, 48) = .28523E+05	
003104	Α (7, 49 = $.29487E + 05$ ($7, 50$) = $.29834E + 05$ ($7, 51$) = $.30266E + 05$	
003111	A (7, 52 = $.30773E+05$ (7, 53) = $.31333E+05$ (7, 54) = $.31804E+05$	
003115	<u>A (</u>	$7 \cdot 551 = \cdot 32178E + 05BA(7 \cdot 56) = \cdot 32498E + 05SA(7 \cdot 57) = \cdot 32870E $	
003122	A (7, 58)= .33145E+05\$A(7, 59)= .33388E+05\$A(7, 60)= .33630E+05	
003126	<u>, A (</u>	7, $611 = .33892E + 058A(7, 62) = .34131E + 058A(7, 63) = .34429E + 05$	
003133	Α (7, $641 = .34722E + 05$ \$A(7, $551 = .35046E + 05$ \$A(7, $661 = .35399E + 05$	
003137	A (7_{2} 67) = $.35488E+058A(7_{2}, 58) = .35723E+058A(7_{2}, 69) = .35933E+05$	
003144	A (7, 70 = .36105E+05 ($7, 71 = .36302E+05$ ($7, 72 = .36509E+05$	
003150	<u>A(</u>	7, 731 = .36948E + 058A(7, 74) = .37336E + 058A(7, 75) = .37640E + 05	
003155	A (7, 76 = $.37932E+05$ (7, 77) = $.38151E+05$ (7, 78) = $.38473E+05$	
003161	A C	(1, 73) = .38861E+05%A(7, 80) = .39212E+05%A(7, 81) = .39756E+05	
003166	A (7, 821 = .40421E+05 ($7, 831 = .41252E+05$ ($7, 841 = .42328E+05$	
003172	AL	7_{1} 8_{2} = 4_{2} 4_{2} 4_{2} 4_{2} 4_{2} 4_{3} 1_{1} 4_{2} 4_{3} 1_{1} 4_{3} 1_{1} 4_{2} 1_{2} $1_$	
003175	86	7_{9} 1)= .11261E+U2\$B(7_{9} 2)= .12642E+U2\$B(7_{9} 3)= .12553E+U2	
003203	<u> </u>	$\frac{1}{1} = \frac{1}{1} + \frac{1}{2} + \frac{1}$	
003207	81	/, //= .269/45+U2\$B(/, 8)= .314965+U2\$B(/, 9)= .394U25+U2 7 40109575.09401 7 44159375.09404 7 491- 515765.09	
003220	5($7_{9} = 101 = -40233E + 029B(-7_{9} = 11) = -49203E + 029B(-7_{9} = 12) = -919(0E + 02)$	
003220	51	$7 + 101 = -700700 \pm 00200 + 7 + 141 = -0030100 \pm 00200 + 7 + 101 = -700700 \pm 00200 \pm 02000 + 020000 + 0200000 + 020000 + 020000 + 0200000 + 020000 + 020000000 + 020000000 + 0200000000$	
003229	51	/9 15/= */90/02+02\$BC /9 1//= *09/19E+02\$BC /9 10/= *92295E+02 7 10/= 10005+02\$BC / 7 20/= 102005+03\$D/ 7 21/= 105805+02	
003236	51	7 221- 10003CTU3DD1 7 201- 11020La03D1 7 211- 11176EL07	
003242	<u>D</u>	$\frac{11}{2} - \frac{11}{2} $	-
003242	B/	7, 231 - 1106651032217, 201 - 1207651032017, 201 - 127565102	
003247	a ($7_{2} = 3125361 + 03561 + 03$	
003233	BI	7_{-} $341 = -126395 + 03887 7_{-}$ $351 = -125795 + 03887 7_{-}$ $361 = -126695 + 03$	
003264	BI	$7_{2} = 37_{2} = -12664F + 0.3 kB(7_{2} = 38) = -12710F + 0.3 kB(7_{2} = 31200 F) + 0.3 kB(7_{2} = 31200 F) + 0.3 kB(7_{2} = 3120 F) + 0.3 kB(7_$	
003204	80	$7_{-40} = 12894F + 0.38B(7_{-41}) = 12956F + 0.38B(7_{-42}) = 1209F + 0.3$	
003271	81	$7_{-43} = -132435 + 0.3 kg (7_{-44}) = -135065 + 0.3 kg (7_{-45}) = -1.39025 + 0.3$	
003302	81	$7_{-46} = .14413F + 0.38B(7_{-47}) = .14907F + 0.38B(7_{-48}) = .15272F + 0.3$	
003306	8(7.49 = .15139E+03\$B(7.50) = .15282E+03\$B(7.51) = .15558E+03	
003313	в.	7. 52 = .159685+038B(7. 53) = .16404E+038B(7. 54) = .16871E+03	
003317	8(7. 55) = .17253E+033B(7. 56) = .17733E+031B(7. 57) = .18349F+03	
003324	8(7. 58 = .18917E+03\$B(7. 59) = .19466E+03\$B(7. 60) = .20310F+03	
003330	8(7, 61)= .21252E+03\$B(7, 62)= .22537E+03\$B(7, 63)= .24769F+03	
003335	B(7, 64 = .29186E+038B(7, 65) = .35915E+038B(7, 66) = .43544E+03	
003341	B (7, 67) = .44781E+03\$B(7, 68) = .50955E+03\$B(7, 69) = .53447E+0.	
003346	B	7, 70 = .54661E+03\$B(7, 71) = .54370E+03\$B(7, 72) = .50766E+03	
003352	8(7, 73) = .44911E+03\$B(7, 74) = .38090E+03\$B(7. 75) = .32042E+03	
003357	8(7, 76) = .27760E+03\$B(7, 77) = .25585E+03\$B(7, 78) = .23083E+03	
003363	8(7, 79) = $.20463E+03$ (7, 80) = $.18489E+03$ (7, 81) = $.16470E+03$	

003370	B(7, 82) = .1	4545E+03\$B(7,	83) = .12636E	+03\$B(7,	84) = .10899E+03
003374	8(7,85)=.9)5996E+02\$B[7,	, 86)= .85410E	+02\$8(7,	87) = .00000E+00
003400	A(8, 1) = .0	10000E+00\$A(8,	2) = .27 71E	+03\$A(81	3) = .13238E+04
003404	A(8, 4) = .5	56688E+04\$A(8,	, 5)= .11254E	+058A(3,	6)= .12485E+U5
003410	A(8, 7) = .1	5345E+05\$A(8)	(8) = (16326E)	+05\$A(8,	9)= .10/50E+05
003415	A(3, 10) = .1	7398E+05%A(8,	(11) = .182/2E	*U53A(0,	127= .19071E+05
003421	A(8, 13) = .1	95856+U5\$A(81	141 = 0199830	+U23A(0)	121 = -21034E + 02
003420	At $0 + 101 = +2$	(33875787 8 41 09 198525485 8 41 8	201- 244625	+050AL 00	211- 361525405
003432	A = 0 + 191 - 0 = 3	TTOELDERAL A	231 = 34402C	+05\$4(8.	24) = -39160E+05
003437 AAZLLZ	A(0) 227 = 03 A(8) 251 = -3	19922F+15\$A(8.	, 26)= .40589F	4058A(8-	27) = .41139E+05
003450	A(8, 28) = -4	1597E+05tA(8.	(29) = .42074F	+05\$41 8.	30 = .42526F+05
003454	$A(B_0, 31) = .4$	3132E+05\$A(8.	32) = .43667E	+05\$A(8.	33) = .44132E+05
003461	A(8, 34) = .4	4839E+05\$A(8.	35)= .45369E	+053A(8.	36) = .46074E+05
003465	A(8, 37) = .4	6948E+05\$A(8.	38) = .47491E	+05\$A(8.	39) = .47921E+05
003472	A(8, 40) = .4	8410E+05\$A(8.	41) = .48891E	+05\$A(8,	42) = .49299E+05
003476	A(8, 43) = .4	9615E+05\$A(8.	44) = .49825E	+05\$A(8,	45) = .50137E+05
003503	4(8, 45)= .5	0397E+05\$A(8,	47)= .50647E	+05\$A(8,	48)= .50869E+05
003507	A(8, 49) = .5	1069E+05\$A(8,	50) = .51366E	+05\$A(8+	51)= .51712E+05
003514	A(8, 52)= .5	2100E+05\$A(8,	53)= .52561E	+05\$A(8,	54)= .53069E+05
003520	A(8, 55) = .5	3523E+05\$A(8,	56) = .53868E	+05\$A(8.	57) = .54325E+05
003525	A(8, 58)= .5	4874E+D5\$A(8,	, 59)= .55431E	+05\$A(8,	60)= •56339E+05
003531	A(8, 61) = .5	57520E+05\$A(8,	62) = .59131E	+05\$A(8,	63) = .61048E+05
003536	A(8, 64) = .6	54467E+05\$A(8,	65) = .68978E	+05\$A(8,	66)= .74585E+05
003542	A(8, 67) = .8	2304E+05\$A(8,	581 = .92741E	+053A(8+	69) = .00000E+00
003546	B(8, 1) = .1	1590E+02\$B(8,	2) = .15029E	+0238(8,	3) = .14483E+02
003553	B(8, 4) = .2	3163E+02\$8(8,	5) = .36044E	+0258(8,	61 = .39343E + 02
003557	B(8, 7) = .4	5010E+02\$8(8,	(8) = .47344E	+02\$8(5,	9) = .49153E+02
007570	$3(8_{1}) = -9$	2891E+U2381 8g	111= ,58993E	+UZ <u>381_01</u>	12)= 00/00E+U2
007575	B(0, 13) = 0/0	'UOD4ETUCDD\ 09 No7005102101 0	+ 147 - +/1/29C	TUCDO1 09	19)- +/1/21C+U2 10)- 605745+02
003575	$D_1 Q_2 + 2J = g_1$	U/09CTUCDD1 09 17392F1028B/ 8	201 = .70881F	<u>▼UZ PDI 09</u> ▲02\$81 8.	101- +077/1E+UC 211= -72361E+02
003606	$B(B_{1}, 22) = .7$	13922402981 89 131255402\$87 8-	207- •700010 231= -74463F	+02\$B(3,	24)= .75593F+02
003612	B(B, 25) = .7	7154E+02\$B(8.	26)= .79057F	+02\$8(8.	27) = .80712F+02
003617	B(8, 28) = .8	2860E+023B(8.	29) = .86499E	+02\$8(8.	30) = .94634E+02
003623	B(8, 31) = .1	05935+03\$B(8.	32) = .12059E	+031B(5.	33) = .12667E+03
003630	B(8, 34) = .1	2837E+03\$B(8.	35) = .13026E	+031B(8,	36) = .13641E+03
003634	B(3, 37)= .1	4474E+03\$B(8,	38)= .1508DE	+0338(8,	39)= .15789E+03
003641	B(8, 40) = .1	6960E+03\$B(8.	411= .19102E	+0338(8.	421= .21683E+03
003645	B(8, 43)= .2	5651E+03\$8(8,	44)= .30653E	+03\$B(8, 1	45)= .36955E+03
003652	B(8, 46) = .4	5374E+03\$B(8,	471 = .52873E	+03\$B(8,	481 = .57262E+03
003656	B(8, 49) = .5	9547E+03\$B(8,	50) = .61412E	+03\$8(8,	51) = .59288E+03
003663	B(8, 52) = .5	1111E+03\$B(8,	53 = 39833E	+03\$8(8,	54) = -31033E+03
003657	B(8, 55) = .2	4181E+03\$8(8,	56)= .20914t	+0358(8,	57)= •17717E+03
003700	B(8, 58) = .1	56135+0358(8,	591 = .14151E	+0358(8,	501 = -12585E+03
007705	B(8, 61) = .1	13472+03386 8,	62)= 10257t	40358(3 ₄)	65)= .00001E+U2
003705	D(0) 041 = 07	14/1CTUCDD(01	6077- 00202C	TUCDD(01	60)- 0000E+02
003711	Δίο ₁ 0/) - •4	2009ET0290(99 10000E10046(9.	21- 545076	▼UZDU 09 - 40798/ 9.	3)- 167475×04
0.037.21	$\frac{\pi \sqrt{2}}{\Delta (9, L)} = -L$	3062F+864A1 0-	5)= 7543076	+84\$A[Q_	5) = 10885F405
003725	A(9, 7) = .1	3398F+05\$&(Q_		+0584(9-	9)= .18754F+05
003732	A(9, 10) = -2	0834E+05\$A(9-	11) = 23052F	+05\$A(9-	12)= .24487F+05
003736	A(9, 13) = -2	6232E+058A(9-	14) = .27775F	+05\$A(9.	15)= .28975E+05
003743	A(9, 16) = .3	1266E+05\$A(9.	17) = .32855E	+05\$A(9.	18)= .33682E+05
003747	A(9, 13) = .3	4720E+05\$A(9.	20)= .35776E	+05\$A(9,	21)= .36733E+05
003754	A(9, 22)= .3	72925+05\$A(9.	23) = .37733E	+05\$A(9,	24) = .38266E+05
003760	A(9, 25) = .3	9376E+05\$A(9,	26)= .42172E	+05\$A(9,	27)= .45378E+05
003765	A(3, 28) = .4	8117E+05\$A(9,	29)= .51240E	+05\$A(9,	30)= .54357E+05

003771	A(9, 31) = .57148E + 058A(9, 32) = .58333E + 055A(9, 33) = .59447E + 05
003776	A(9, 34)= .59945E+05\$A(9, 35)= .60962E+05\$A(9, 36)= .61953E+05
004002	A(9, 37) = .62627E+05\$A(9, 38) = .63165E+05\$A(9, 39) = .64015E+05
004007	A(9, 40)= .649975+05\$A(9, 41)= .65953E+05\$A(9, 42)= .66819E+05
004013	A(9, 43) = .674165+05\$A(9, 44) = .67991E+05\$A(9, 45) = .68541E+05
004020	A(9, 46)= .69068E+05\$A(9, 47)= .69571E+05\$A(9, 48)= .70070E+05
004024	A(<u>9, 49)= .70502E+05\$A(9, 50)= .71015E+05\$A(9, 51)= .71478E+05</u>
004031	A(9, 52)= .71931E+05\$A(9, 53)= .72212E+05\$A(9, 54)= .72486E+05
004035	A(9, 55) = .72525E+05\$A(9, 56) = .72878E+05\$A(9, 57) = .73384E+05
004042	A(9, 58)= .73600E+05\$A(9, 59)= .73983E+05\$A(9, 60)= .74273E+05
004046	A <u>(9, 61)= .74697E+05\$A(9, 62)= .75167E+05\$A(9, 63)=</u> .75767E+05
004053	A(9, 64)= .76553E+05\$A(9, 65)= .77353E+05\$A(9, 66)= .77865E+05
004057	A <u>(9</u> , 67)= .78260E+05\$A(9, 68)= .78891E+05\$A(9, 69)= .79826E+05
004064	A(9, 7))= .81843E+05\$A(9, 71)= .85326E+05\$A(9, 72)= .888895E+05
004070	A(9, 73) = .93013E+05\$A(9, 74) = .00000E+00\$A(9, 75) = .00000E+00
004073	B(9, 1)= .94559E+01\$B(9, 2)= .62532E+01\$B(9, 3)= .62540E+01
004100	B(9, 4) = •74753E+01\$B(9, 5) = •93705E+01\$B(9, 6) = •11730E+02
004104	B(9, 7)= .13986E+D2\$B(9, 8)= .17461E+D2\$B(9, 9)= .20527E+D2
004111	B(3, 10) = .24229E+02\$B(9, 11) = .28474E+02\$B(9, 12) = .31741E+02
004115	B(9, 13)= .35498E+02\$B(9, 14)= .39284E+02\$B(9, 15)= .42847E+02
004122	B(9, 16) = .49225E+02B(9, 17) = .53598E+02B(9, 18) = .56616E+02
004126	B(9, 19)= .60990E+02\$B(9, 20)= .66319E+02\$B(9, 21)= .71770E+02
004133	B(9, 22) = .74742E+02\$B(9, 23) = .76704E+02\$B(3, 24) = .77979E+02
004137	B(3, 25) = .79447E+02\$B(9, 26) = .81739E+02\$B(3, 27) = .83921E+02
004144	B(9, 28) = .857785 + 028B(9, 29) = .87357E + 028B(9, 30) = .89262E + 02
004150	$B(9, 31) = .90421 \pm .028B(9, 32) = .91589E \pm .028B(9, 33) = .94875E \pm .028B(9, 31) = .94875E \pm .028B(9, 32) = .94875E \pm .02886E \pm .028B(9, 32) = .94875E \pm .02885E \pm .02885E \pm .02885E \pm .02875E \pm .02885E \pm .02885E \pm .02875E \pm .028$
004155	B(9, 34) = .97520 + 023B(9, 35) = .99366E + 023B(9, 36) = .10009E + 03
004161	B(9, 37) = .10313E+033B(9, 38) = .10491E+033B(9, 39) = .10697E+03
004165	$B(9, 47) = \cdot 10950 \pm 033B(9, 41) = \cdot 11245 \pm 038B(9, 42) = \cdot 11552 \pm 03$
004172	B(9, 43) = .11915E+035B(9, 44) = .12271E+033B(9, 45) = .12639E+03
004177	$\frac{B(9)}{40} + \frac{1309}{E} + \frac{1309}{E} + \frac{135}{20} = \frac{47}{2} = \frac{13716E}{4035B} + \frac{13716E}{23} = \frac{14378E}{403} = \frac{14378}{403} =$
004203	B(9, 49) = .152155 + 0.35B(9, 50) = .155105 + 0.35B(9, 51) = .188005
004210	$\frac{B(9, 52) = .220142 + 035B(9, 53) = .259492 + 035B(9, 54) = .303132 + 03}{2000354035000}$
004214	51 J, 55)= .30083C+03BB1 Y, 56)= .37818E+03B81 Y, 57)= .48321E+03 R/ 0
004225	$\frac{01}{91} \frac{91}{2} = \frac{01}{2} \frac{91}{2} \frac{91}{2} = \frac{01}{2} \frac{91}{2} \frac{91}{2} = \frac{01}{2} \frac{91}{2} \frac{91}{2} \frac{91}{2} = \frac{01}{2} \frac{91}{2} 91$
004222	$01 \ 9_{1} \ 011 - \ 047944 + + 0.5 B1 \ 9_{1} \ 021 = \ 0.39055 + 0.5 B1 \ 9_{1} \ 0.51 = \ 0.32202 + 0.5$
UU4232	$\frac{0}{9} \frac{9}{9} \frac{0}{2} \frac{0}{1} - \frac{1}{2} \frac{0}{1} \frac{1}{2} $
004230	DI 9, DI/= +10404E+U3DDI 9, 507= +15432E+U3DBI 9, 597= +14298E+U3 DI 0, 701= +3238E+032DI 0, 741= 448EEE+032DI 0, 751= +0688EE+03
004243	$\frac{1}{2} = \frac{1}{2} = \frac{1}$
004247	$\Delta (10, 1) = -00000000000000000000000000000000000$
004256	A(10, 4) = -18332F + 048A(10, 5) = -40771F + 048A(10, 3) = -62389F + 04
004250	$\Delta(10, 7) = -83988F + 048A(10, 8) = -95154F + 048A(10, 0) = -10303F + 06$
004267	A(10, 10) = .11019E+05SA(10, 11) = .11572E+05SA(10, 12) = .12192E+05
004273	A(10, 13) = .130876+058A(10, 14) = .141176+058A(10, 15) = .148046+05
004300	A(10, 16) = .15674E+05\$A(10, 17) = .18166E+05\$A(10, 18) = .19557E+05
004304	A(10, 13) = .22306E+05 $BA(10, 20) = .24842E+05$ $BA(10, 21) = .26513E+05$
004311	A(10, 22) = .27617E+05\$A(10, 23) = .28606E+053A(10, 24) = .29774E+05
004315	A(10, 25) = .30715E+05 $BA(10, 26) = .31901E+05$ $BA(10, 27) = .33038E+05$
004322	A(10, 28) = .33706E+05\$A(10, 29) = .34351E+053A(10, 30) = .35060E+05
004326	A(10, 31) = .35678E+053A(10, 32) = .36447E+053A(10, 33) = .37038F+05
004333	A(10, 34) = .37476E+05 $BA(10, 35) = .37825E+05$ $BA(10, 36) = .38260E+05$
004337	A(10, 37) = .38846E+05 $A(10, 38) = .39492E+05 $ $A(10, 39) = .40088E+05$
004344	A(10, 40) = .40716E+053A(10, 41) = .41246E+053A(10, 42) = .41505E+05
004350	A(10, 43) = .41797E+05BA(10, 44) = .42222E+05BA(10, 45) = .42469E+05
004355	A(10, 46) = .42785E+05\$A(10, 47) = .43044E+05\$A(10, 48) = .43565E+05
004361	A(10, 49) = .44087E+058A(10, 50) = .44629E+058A(10, 51) = .45210E+05
004366	A(10, 52) = .45719E+05\$A(10, 53) = .46256E+05\$A(10, 54) = .46887E+05

.4

004372	A(10, 55)) = .47700E+05\$A(1)), 56) = .43654E+058A(10, 57) = .50355E+05
004377	A(10, 58)) = .52730E + 058A(1)	1, 591 = .56513E + 05\$A(10, 60)= .585036+05
004403	A(10, 61)) = .60266E+058A(1)	52) = 65143E + 058A(10, 631 = .68647E+05
004410	A(10, 64)) = .72973E+05\$A(1)	(-55) = .76406E + 053A(10, 66) = .79542E+05
004414	A(10, 67)) = .85611E + 053A(1)	$1 \cdot 68) = \cdot 92520E + 05$ (10, 69) = .00000E+00
004420	B(10, 1)) = .21000E + 023B(1)	(2) = .29020E + 02\$B(10, 31 = .29028E+02
004425	B(10, 4))= .36538E±0238(10), 5)= .53910E+0238(10, 6) = .72458E+02
004431	B(10, 7))= .91691E+02\$B(10), 8)= .10030E+03\$B(10, 9) = .10601E + 0.3
004436	B(10, 10)) = .11082E + 03\$B(10)	(11) = .11350E + 03B(10, 12) = .11604E+03
004442	B(10, 13)) = .11886E+03\$B(1)), 14)= .12122E+03\$B(10, 15) = .12156E+03
004447	B(10, 16)) = .12080E + 03\$B(1))• 17)= •12061E+03\$B(10, 18) = .12155E+03
004453	8(10, 19)) = .12293E+03	(, 20) = .12413E+03\$B()	10, 21)= .125065+03
004460	B(10, 22))= .12640E+03\$B(10), 23)= .12751E+03\$B(10, 24)= .12965E+D3
004464	8(10, 25))= .13180E+03\$B(10), 26)= .13377E+033B(10, 27)= .13529E+03
004471	8(10, 28)) = .13720E + 03B(1)	1, 29) = .13876E + 033B(10, <u>30)</u> = .141558+03
004475	8(10, 31))= .14423E+03\$B(1(), 32)= .14888E+03\$B(10, 33 = .15303E+03
004502	B(10, 34))= .15770E+03\$B(1)	(35) = .16225E + 03B(10, 36) = .16584E+03
004506	B(10, 37))= .17188E+03\$B(1), 38)= .18222E+03\$B(10, 39) = .19497E+03
004513	B(10, 40)) = .21481E+033B(1)) <u>, 41)</u> = .24070E+03\$B(10, 42)= .27286E+03
004517	B(10, 43))= .30418E+03\$B(10), 44)= .36611E+03\$B(10, 45 = .40656E+03
004524	B(10, 46)	$) = .42772E + 03 \pm B(10)$	1 + 47) = 41786E + 038B(10 + 48 = + 35455E + 03
004530	3(10, 49))= .28931E+035B(10), 50)= .23854E+03\$B(10, 51) = .20101E+03
004535	B(10, 52))= +17505E+03\$B(10), 53)= .15353E+03\$B(10, 54)= .13787E+03
004541	B(10, 55))= .12487E+03\$B(10), 56)= .11410E+03\$B(10, 57 = .10229E+03
004546	B(10, 58)) = .92120E+02\$B(10), 59)= .75386E+02\$8(10, 50) = .77767E+02
004552	B(10, 61))= .73895E+02\$B(10), 52)= .6229EE+02\$B(10, 63 = .62299E+02
004557	B(10, 64)) = .56034E + 023B(10)), 65) = .47817E+02\$B(10, 661 = .49741E + 02
004563	B(10, 67))= .47318E+02\$B(10), 68)= .44959E+02\$B(10, 69) = .00000E+00
004567	A(11, 1)) = .00000E + 00\$A(1)	2)= .60656E+03\$A(11, 3) = .19606E+04
004573	A(11, 4))= .43822E+04\$A(11	• 5)= •70028E+04\$A((11, 6) = .91028E+04
004577	A(11, 7)) = .10899E+05\$A(11		11, 9)= .136415+05
004604	A(11, 10))= .14859E+05\$A(11	., 11) = .16143E+05\$A(11, 12)= .17395E+05
004610	A(11, 13)) = .18641E+05\$A(11	14) = .20236E + 05\$A(11, 15)= .21300E+05
004615	A(11, 16))= .22652E+053A(11	• 17)= •24013E+05\$A((11, 18) = .24914E+05
004521	A(11, 13)) = .26178E+05\$A(11	• 20)= •27181E+05\$A(11, 21) = .279292+05
004626	A(11, 22))= .29013E+05\$A(11	., 23) = .30815E+05\$A(11, 24) = .32639E+05
004632	A(11, 25)) = .32954E+05\$A(11	26) = .35450E+05\$A(11, 27) = .36608E+05
004637	A(11, 28))= .38458E+05\$A(1)	., 29)= .40463E+05\$A(.	(1, 30) = .43431E+05
004643	A(11, 31)) = .45662E+05\$A(11	• 32) = • 48334E+05\$A(<u>1. 33) = .49892E+05</u>
004650	A(11, 34))= .52430E+05\$A(11	., 35)= .54189E+05\$A(:	11, 36 = .56502E + 05
004654	A(11, 37)) = .57812E+05\$A(11	(-38) = -59821E + 05\$A($11, \ 39) = .614235 + 05$
004661	A(11, 40))= .62518E+05\$A(11	(+ 41) = -64245E + 053A(11, 42)= .65985E+05
004665	A(11, 43)) = .67326E+05\$A(11	_•_44)= •68379E+05\$A(11, 45) = .69426E+05
004672	A(11, 46))= .70971E+05\$A(11	., 47)= .72539E+058A((1, 48) = .73572E+05
004676	A(11, 43)	<u>) = .74472E+05\$A(11</u>	• 50) = •75081E+053A(11, 51) = .75609E+05
004703	A(11, 52))= •76545E+05\$A(11	• 53)= •77448E+05\$4(11, 54)= .786765+05
004707	A(11, 55)) = .79734E+05\$A(11	, 56) = .80612E + 05\$A(11, 57) = •81806E+05
004714	A(11, 58))= .83209E+053A(11	., 59)= .84528E+053A(11, 60)= .88548E+05
004720	A(11, 61)) = .94910E + 05 \$A(1)	(262) = .00000E + 00\$A(11, 63) = .0000000 + 00
004723	8(11, 1)) = .12000E+02\$B(11	., 2) = .12300E+02\$B((1, 3) = .12325E+02
004730	B(11, 4)) = .14349E+02\$B(11	<u>, 5)= ,17115E+02\$B(</u>	11, 6) = .20466E + 02
004734	8(11, 7)) = .23951E+02\$B(11	• 8)= •27637E+02\$B((1, 9) = .31456E+02
.004741	B(11, 10)	= -35520E + 023B(11)	+ 11) = -40275E + 028B((1, 12) = .45819E+02
004745	B(11, 13))= .52259E+02\$B(11	• 14)= •60858E+02\$B(11, 15) = •67733E+02
004752	B(11, 16)) = .77030E+02\$B(11	• 17)= •88078E+023B(11, 18) = .95758E+02
004756	8(11, 19)) = •10503E+03\$B(11	• 20)= •11216E+03\$B((1, 21) = .11670E + 03
004763	B(11, 22)) = .12077E+03\$B(11	. 23) = .12424E+03\$B(11, 24) = .12682E+03
004767	B(11, 25))= .12777E+03\$B(11	, 26)= .13218E+033B(11, 27) = .12924E+03

_....

÷

005375	B(12, 67)=	+11198E+03\$B(12+	68) = .10007E+03\$B(12,	69)= .94296E+02
005402	8(12, 70)=	.80105E+02\$B(12,	71)= .69659E+023B(12,	72)= .00000E+00
005405	A(13, 1) =	.00000E+00BA(13,	2) = .40691E + 023A(13)	3) = .39310E+03
005411	A(13, 4) =	.10712E+04\$A(13,	5) = .17243E+04\$A(13,	6) = .19639E+04
005416	A(13, 7)=	.22551E+04\$A(13,	8) = .25065E+04\$A(13,	9)= .26798E+04
005422	A(13, 10)=	.28719E+045A(13.	11) = .31533E + 043A(13)	12) = .38678E+04
005427	A(13, 13) =	.49271E+04\$A(13.	14) = .60479F + 048A(13)	(15) = .70731E+04
005433	A(13, 16) =	-75012E+04\$A(13-	17) = .805931 + 043A(13)	(18) = .85532E + 04
005440	A(13, 19) =	.88856E+04\$4(13.	20) = .91251F + 048A(13)	21) = -93396F + 04
005444	A(13, 22) =	-95229F+14\$A(13-	23) = -96872E + 04 + A(13)	24) = _97721E+04
0.05444	A(13, 25) =	.99837E+0484(13.	261 = -10267E + 058A(13)	27) = .10525E+05
005451	A(13, 28) =	10758E+05\$A(13.	$29) = .10977E + 05 \pm 113$	$301 = -14204E \pm 05$
005455	A(13) 20)-	11/21/05 \$4/13.	$(2) = (1678E + 05 \pm 0.013)$	331~ 117895A05
005462	A(13, 36) =	11012E+05\$A(13.	$351 = .11963E + 05 \pm 0.113$	361 = 1204AF+05
005400	A(13, 37)-	121606405\$8(13)	$397 = 129910 \pm 05000000000000000000000000000000000$	301 - 122005 + 05
005473	A(13, 60) =	-12362E+05\$A/13-	$41) = -12447E + 05 \pm 1/13$	(2) = 12599E + 05
005477	A(13) + 0) = A(13) + 03) =	12778E+05\$A(13,	417 = 12859E + 053A(13)	45)~ 12958E+05
005510	A(13, 45)=	13040E+05\$A(13.	$47) = 13166E + 05 \pm 1/3$	$(43) = (133470 \pm 05)$
005515	A(13, 40) -	13484E+05\$A/13-	501 = .13605E + 05 \$A(13)	51)- 13724FADS
005521	A(13 52)-	1 385 DE+05 \$8 (1 3.	$531 \pm 1308051050000000000000000000000000000000$	
002221	A(13, 55)-	-14374E+05\$A(13-	561 = -14654E + 05\$A(13)	571 - 140000000000000000000000000000000000
0.05570	A(13) 577-	1612754053A/43	501 - 156775 + 0504(13)	(0) = (1 + 2) + (1 + 2) = (1 + 2) + (1 + 2) = (1 + 2) + (1 + 2)
005577	A(13) 201-	1702551053A/13	$577 = -176676 \pm 05071139$	631- 18264EA0E
005537	AILON QL)-	1 2737EAD5 \$8/13	$651 \pm 10156510520(13)$	65)- 10/595105
005543	A(13, 67) =	-10002-+05%A(13-	577 = 171902 + 09 BA(13)	601 - 22327E + 05
005556	A(10) 077-	2/161EA05\$A(13)	711 - 000006 + 0000006 + 0000006 + 00000000	
005557	A(13, 70) = 0.000	- 1 776 7E + 0 2 \$ \$ 1 3 \$	2) = 44000E + 0230(13)	3)- 16000E+00
005557	D(13) 11-	24677640200113	$E_1 = -27601E_102001139$	61- 30738EL02
005570	B(13) + 4/=		$R_{1} = -41359E + 0238(13)$	
005575	D(13) (1) = 0(17)	60602Ex0220113	113 - 536765 + 0230(13)	121- 598905+02
005501	B(13, 10)-	6 JR 05 52 C + 02 DO (1 3)	$1.17 = -700206 \pm 020013$	151- 903605402
005606	B(13 15)-	0/676EA0230(13)	171 - 10123E + 02001130	19)- 108/65+07
005612	B(13, 10)-	11430EAD338(13)	201 = 11968E + 0328(13)	21) = 126045403
005617	B(13, 19/-	4 22505407¢0/4 2	231 - 44426540340443	241 = 147055407
002017	B(13, 26)-	15404EA03\$P(13	251 - 164400 + 0350113	271- 177345402
009023	$\frac{1}{2}(13, 23) =$	+0100F+N3\$P/13	2Q = 21152E + 0360113	
	0113 201-	320026103401134	$277 = 32276 \pm 0.20074.2$	
UU2034 005674	D(13) (31) = 0	-20003-TUSPO(13	321 - 0.02342 + 0.001139	361- 680775407
005645	3(13, 34) =			30/~ .000//LV03
000040	B(13, 40)-	10500540488/13.	(1) = 10761E + 00 pb(13)	42) - 405335404
005656	B(13, 40) =	410505CV04080139	417 - 4107010 + 0400113 + 441 - 402170 + 0400113 + 441 - 402170 + 0400113 + 441 - 4400113 + 44000113 + 44000113 + 44000113 + 44000113 + 440000113 + 440000000000000000000000000000000000	427- 11000000000
005663	B(13, 46)=	9/571E+033P/13	47) - B2455E10348(13)	497- 699723LTUS
005667	B(13, 40)-	57775A0390(13)		511- 30562540Z
005674	B(13, 52) -	- 35330E+0300(1)7	57)	541- 20340EA07
005074	B(13, 55)-	26772511720/17		571- 22044Ex07
005700	$\frac{3(13)}{2(13)}$	21007522+USpB(159	501 - 106185403001139	577 - 5220442703
005705	D(13, 50)-	46102C+0300(13)	521- 15708Ex03001139 521- 15708Ex03001139	631- 15/065×03
	0(13 64)-	4 101 72 YUJ PD (1 3	65)- 13066FAN34D/13	661- 17046E107
005722	B(17 67)-	4242902703901239	681 - 424645A0300(13)	601 - 116865107
	D113+ 0/1-	41021-10210/13 41021-10210/13		72) = 00000000000000000000000000000000000
005720	51159 707- A116. ()-	- 11021CT U3 D01134	2)- 2/525551200001139	767~ 00000000TU0 71~ 046005406
005/31	A(14 4)-	4 0970510434 (14)	$\frac{c_{I}}{c_{I}} = \frac{c_{I}}{c_{I}} \frac{c_{I}}{c$	
005761	A (4)	440070CT04DA1149 - 10672C±050144	シェー ・ロサコエビビサリ分し140 タリー ・1クルウフビエルにビタメイル	0/= +031/0E+U4 0/- +1/202E+0E
005766	A (1)	16377510528/144	07- 01- 01- 01- 02- 02- 02- 02- 02- 02- 02- 02- 02- 02	77- 4142 JOETUD
005752	ALL49 LUJ=	- 1007 JETU2 24 1149 21707E10E4141	1/1/- 0101/4C7UDD4114; 1/1/- 070/EE10E04/4/	151- 354605405 151- 356605405
00772	A116 151-	961191CTU2DA1149	17) - 070608×054144	181- 28676EADE
UU2/2/ NAE767	MILH9 107-	42007/CTU2PA1149 20229510528/44		107- CODJOETUJ 211- 206405100
000700	A(14) = 191 = A(44) = 201 = 0	4 2 7 2 3 0 C T U 7 2 A 1 4 4	271- 222675+05#4(14)	
UUD/(U	A 1 14 0 221 =	• J LO J C C T U D D A 1 L 4 •	CJJ - 03C30/ビサリプあんに140	とりょう ふうとうどうとすりち

005774	A(14, 25) = .33451E+05\$A(14, 26) = .34291E+05\$A(14, 27) = .36392E+05
006001	A(14, 28) = .39638E+05 $A(14, 29) = .41726E+05$ $A(14, 30) = .43602E+05$
006005	A(14, 31) = .45753E+05\$A(14, 32) = .47690E+05\$A(14, 33) = .49485E+05
006012	A(14, 34) = .50587F+05 A(14, 35) = .51617F+05 A(14, 36) = .52542E+05
006015	A(14, 37) = 53259F+058A(14, 38) = 54077F+058A(14, 39) = 55643F+05
006023	A(14, 40) = 572(6+05(A(14, 41)) = 58814(14, 42) = 60277(14, 14) = 60277(14)
006027	$A(1)_{2} = 0$
006034	$\mathbf{A}_{1}\mathbf{A}_{1}\mathbf{A}_{2}\mathbf{A}_{3}\mathbf{A}$
00604	$\mathbf{A}_{114} + \mathbf{A}_{01-} = \mathbf{A}_{20} + \mathbf{A}_{140} + \mathbf{A}_{14} + \mathbf{A}_{14-} = \mathbf{A}_{20} - \mathbf{A}_{140} + \mathbf{A}_{$
000040	$\frac{1}{1} \frac{1}{1} \frac{1}$
006054	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
006051	$\frac{-A(14)}{A(14)} = \frac{-A(14)}{A(14)} = \frac{-A(14)}{A$
000000	A(14, 50) = -7392224038(14, 59) = -7443024058A(14, 50) = -720122405
	$\frac{A(14y \ b1)}{(14y \ b1)} = \frac{A(14y \ b1)}$
006067	A(14, 64) = .77925E+05 A(14, 65) = .78746E+05 A(14, 65) = .79434E+05
006073	A(14, 67) = .80021E+05
006100	A(14, 70) = .82589E+05 $A(14, 71) = .83878E+05$ $A(14, 72) = .85553E+05$
006104	A(14, 73) = .87020E+05\$A(14, 74) = .88070E+05\$A(14, 75) = .88561E+05
006111	A(14, 76)= .89194E+05\$A(14, 77)= .90075E+05\$A(14, 78)= .91277E+05
006115	<u>A(14, 79) = .92765E+05\$A(14, 80) = .94006E+05\$A(14, 81) = .95675E+05</u>
006122	A(14, 82)= .97669E+05\$A(14, 83)= .10017E+06\$A(14, 84)= .10339E+06
006126	A(14, 85) = .10699E+06\$A(14, 86) = .11144E+06\$A(14, 87) = .11564E+06
006133	A(14, 83) = .11988E+06 $(14, 89) = .12516E+06$ $(14, 90) = .13088E+06$
006137	A(14, 91) = .13682E+06\$A(14, 92) = .14320E+06\$A(14, 93) = .00000E+00
006143	B(14, 1) = .92819E+01\$B(14, 2) = .96156E+01\$B(14, 3) = .94188E+01
006150	B(14, 4) = .10394E+02\$B(14, 5) = .12347E+02\$B(14, 6) = .14833E+02
006154	3(14, 7) = .17763E+02 \$B(14, 8) = .21517E+02\$B(14, 9) = .25214E+02
006161	B(14, 10) = .30421F+02 $B(14, 11) = .36388F+02$ $B(14, 12) = .42414F+02$
006165	B(14, 13) = 50906F + 02\$B(14, 14) = 59866F + 02\$B(14, 15) = 67445F + 02
006172	B(14, 16) = .73367F+02\$B(14, 17) = .77997F+02\$B(14, 18) = .80689F+02
006176	B(14, 19) = .82392E+02\$B(14, 20) = .83775E+02\$B(14, 21) = .86025E+02
006203	B(14, 22) = .88885E+02\$B(14, 23) = .91172E+02\$B(14, 24) = .92234E+02
006207	B(14, 25) = .93094E+02\$B(14, 26) = .92681E+02\$B(14, 27) = .92361E+02
006214	B(14, 28) = .92581E+02\$B(14, 29) = .93024E+02\$B(14, 30) = .93641E+02
006220	B(14, 31) = .94541E+02B(14, 32) = .95749E+02B(14, 33) = .97058E+02
006225	B(14, 34) = .98333E+023B(14, 35) = .10039E+033B(14, 36) = .10281E+03
006231	B(14, 37) = .10411F+03BB(14, 38) = .10469F+03BB(14, 39) = .10482F+03
006236	B(14, 40) = .10548F+035B(14, 41) = .10511F+035B(14, 42) = .10730F+03
0.06242	B(14, 43) = 10888F+035B(14, 44) = 11070F+035B(14, 45) = 11334F+03
006247	B(14, 46) = .11722E+03B(14, 47) = .11924E+03B(14, 48) = .12090E+03
006253	B(14, 49) = .12278E+D3\$B(14, 50) = .12545E+D3\$B(14, 51) = .12888E+D3
006260	B(14, 52) = .13330E+03BB(14, 53) = .14006E+03BB(14, 54) = .14776E+03
006264	B(14, 55) = .157105+03\$B(14, 56) = .16787E+03\$B(14, 57) = .17930E+03
006271	B(14, 58) = .18481F+03BB(14, 59) = .18092F+035B(14, 60) = .17208F+03
006275	B(14, 51) = .15641E+03BB(14, 52) = .13896E+03BB(14, 53) = .12605E+03
006302	B(14, 64) = .11404E+03BB(14, 65) = .10543E+03B(14, 66) = .99975E+02
006306	B(14, 67) = .95654E+02\$B(14, 68) = .91874E+02\$B(14, 69) = .88563E+02
006313	B(14, 70) = .85865E+02\$B(14, 71) = .83067E+02\$B(14, 72) = .80392E+02
006317	B(14, 73) = .78191E+023B(14, 74) = .76684E+023B(14, 75) = .75259E+02
006324	B(14, 76) = .72380E+02\$B(14, 77) = .69832E+02\$B(14, 78) = .66975E+02
006330	B(14, 79) = .64695E+02B(14, 80) = .62067E+02B(14, 81) = .59074E+02
006335	B(14, 82) = .56595E + 023B(14, 83) = .53372E + 023B(14, 84) = .50153E + 023E(14, 85) = .5015E(14, 85) = .501E(14, 85) = .501E(15, 85) = .501E(14, 85) = .501E(1
006341	B(14, 85) = .469455+02\$B(14, 36) = .43323E+02\$B(14, 87) = .40671E+02
006346	B(14, 88) = .38283E + 028B(14, 89) = .35896E + 028B(14, 90) = .34039E + 02
006352	B(14, 91) = .32360E+02\$B(14, 92) = .31033E+02\$B(14, 93) = .00000E+00
006356	A(15, 1) = .00000E+008A(15, 2) = .56476E+028A(15, 3) = .28882E+03
006362	$A(15, 4) = .67945 \pm 0.3$ $BA(15, 5) = .99904 \pm 0.3$ $BA(15, 6) = .12137 \pm 0.4$
006366	A(15, 7) = .13721E+048A(15, 8) = .16341E+048A(15, 9) = .17860E+04
006373	A(15, 10) = .19064E+048A(15, 11) = .20028E+048A(15, 12) = .21636E+04
· -	

· · · · · · · · ·

006377	A(15, 13) = -26622E+04\$A(15)	14) = .33499E+D4\$A(15,	15)= .3564DE+04
006404	A(15, 16) = .37618E+04BA(15, 16)	17)= .33930E+04\$A(15,	18)= •42518E+04
006410	A(15, 19) = .53638E+048A(15, 19) = .55636A(15, 19) = .55636E+048A(15, 19) = .5564E+048A(15, 19) = .556E+048A(15, 19) = .556E+00000000000000000000000000000000000	20) = .60321E+04\$A(15.	21) = .655735+04
006415	A(15, 22) = .70503E+04\$A(15,	23) = .78715E+04\$A(15,	24)= .85894E+04
006421	A(15, 25) = .90170E + 04\$A(15, 25) = .90170E + .9	26) = .95208E+04\$A(15,	27)= +10062E+05
006426	A(15, 28)= .10455E+05\$A(15,	29)= .10694E+05\$A(15,	30)= .10840£+05
006432	A(15, 31) = .11034E+058A(15,	32)= .11385E+05\$A(15,	33)= .11738E+05
006437	A(15, 34) = .12136E+05\$A(15,	35) = .12548E+05\$A(15.	36)= .12852E+05
006443	A(15, 37) = .13118E+05\$A(15,	38) = .13376E + 05\$A(15)	39) = .13641E+05
006450	A(15, 40) = .13845E+05\$A(15,	41) = .14032E+05\$A(15,	42)= .14211E+05
006454	A(15, 43) = .14397E+05\$A(15, 143)	44) = .14558E+05\$A(15.	45)= .14718E+05
006461	A(15, 46) = .14890E+05\$A(15,	47)= .15086E+05\$A(15,	48)= .15264E+05
006465	A(15, 49) = .15437E+05\$A(15)	50) = .15630E+05\$A(15,	51)=_+15785E+D5
006472	A(15, 52) = .16052E+05\$A(15,	53)= .16099E+05\$A(15,	54)= .16209E+05
006476	A(15, 55) = .16324E+05\$A(15,	56) = .16448E + 05\$A(15)	571 = .16655E + 05
006503	A(15, 58)= .16812E+05\$A(15,	59)= .17151E+05\$A(15,	60) = .175535+05
016507	A(15, 61) = .17971E+055A(15, 61) = .17971E+0.00000000000000000000000000000000000	62) = .18187E+05\$A(15,	63)= +184025+05
006514	A(15, 64) = .18621E+05\$A(15, 64) = .18621E+05\$A(15, 64) = .08621E+05\$A(15, 65) = .08621E+	65)= .18878E+05\$A(15,	66) = .19232E+05
006520	A(15, 67) = .19820E+05\$A(15,	68)= ,20636E+05\$A(15;	69)= +21625E+05
006525	A(15, 70) = .23110E+05\$A(15,	71)= .24968E+05\$A(15,	72)= .27751E+05
006531	A(15, 73) = .30532E+05\$A(15, 15)	74) = .00000E + 00\$A(15)	75)= .00000E+00
006534	B(15, 4)= .90623E+02\$B(15,	5)= .11522E+03\$B(15,	6)= .13510E+03
006541	B(15, 1) = .050000+03\$B(15, 1)	2) = .053000+03\$B(15,	3) = .66337E+02
006547	B(15, 7) = .14476E+03\$B(15,	8)= .15273E+03\$B(15,	9)= .14902E+03
006554	B(15, 10) = .13914E+03\$B(15, 10) = .13914E+03B(15, 10) = .13914E+00B(15, 10) = .13914E+00B(15, 10) = .13914E+00B(15, 10) = .13	11) = .13481E+03\$B(15,	12) = .13610E+03
006560	B(15, 13) = .14186E+03\$B(15, 13) = .14186E+03\$B(15, 15) = .14186E+03B(15, 15) = .14186E+050B(15, 15) = .14186E+050B(15, 15) = .14186E+050B(15, 15) = .14186E+000B(15, 15) = .14186E+000B(15, 15) = .14186E+000B(15, 15)	14)= .15141E+033B(15,	15)= •15438E+03
006565	B(15, 16) = .15632E+03\$B(15, 156)	17) = .15808E+03\$B(15,	18) = .15832E+03
006571	B(15, 19)= .15856E+03\$B(15,	20)= .15881E+03\$8(15,	21)= .15939E+03
006576	B(15, 22) = .16025E+03\$B(15,	23) = .16063E+03\$B(15,	24) = .16157E + 03
006602	B(15, 25) = .16332E+03\$B(15,	26) = .16396E+03\$B(15,	27)= .16589E+03
006607	B(15, 28) = .16777E+03\$B(15, 28) = .167777E+03\$B(15, 28) = .16777E+03\$B(15, 28) = .16777E	29)= .17017E+03\$B(15,	30)= .17196E+03
006613	B(15, 31) = .17379E+033B(15, 31) = .17379E+030B(15, 31) = .17379E+033B(15, 31) = .17379E+033B(15, 31) = .17379E+033B(15, 31) = .17379E+030B(15, 31) = .17379E+000B(15, 31) = .17379E+	32)= .17429E+03\$B(15,	33)= .17561E+03
006620	$B(15, 34) = .17813 \pm 033B(15, 34)$	35) = .18085E+03\$B(15.	36) = .18314E+03
006624	B(15, 37) = .18600E+033B(15, 37) = .18600E+033B(15, 37)	38)= .18897E+03\$B(15,	39)= .19326E+03
006631	B(15, 40) = .19674E+03\$B(15, 19674E+03)	41) = .20091E+03\$B(15,	42) = .20702E+03
006635	$B(15, 43) = .21360E+03$B(15, -21360E+03$B(15, -21360E+038))}$	44)= .22152E+03\$B(15,	45)= .23290E+03
006642	$B(15, 46) = .24920 \pm 033B(15, -24920 \pm 033B(15, -24920 \pm 033B))$	47)= .27342E+03\$B(15,	48) = .30148E+03
006646	B(15, 49) = .34234E+03\$B(15,	50)= .39686E+03\$B(15,	51)= •44405E+03
006653	B(15, 52) = .55446E+03B(15, 52)	53) = .57554E + 03B(15)	541 = .61501E + 03
006657	B(15, 55) = .64893E+03B(15, 55) = .6489B(15, 55) = .6488B(15, 55) = .6488B(15, 55) = .6488B(15, 55) = .648B(15, 55) = .648B	56) = .66789E+03\$B(15,	57) = .68140E + 03
006664	B(15, 59) = .67130E+033B(15, 59) = .67140E+0500 = .67140E+05000 = .671400E+05000 = .6714000 = .6714000000000000000000000000000000000000	<u>59)</u> = .61306E+03\$B(15,	601 = .52392E + 03
006670	B(15, 61) = .42927E+033B(15, 61) = .42927E+0327E+034200 = .42927E+03400000000000000000000000000000000000	62)= .38334E+03\$B(15,	63) = .35224E+03
006675	B(15, 64) = .32081E+03\$B(15, 64) = .32081E+03881E+03881E+03881E+03881E+038881E+038881E+038881E+038881E+038881E+0	55)= .29605E+03\$B(15,	661 = .27434E+03
006701	B(15, 67) = .24702E+03BB(15, 67) = .24702E+0.24700 = .247000 = .247000 = .247000000000000000000000000000000000000	68) = .21737E + 03 B(15)	69) = .19734E+03
006706	$B(15, 70) = .17979 \pm 038B(15, 17979)$	$71) = .15844E + 03 \pm B(15)$	72) = .12855E+03
006712	$B(15, 73) = .10691E + 03 \beta B(15, -10691E)$	74 = .00000E+00\$B(15,	75) = .00000E+00
006715	A(16, 1) = .00000E+00\$A(16, 1)	2) = .34551E + 02SA(16)	3) = -20231E+03
006721	A(16, 4) = .45475E+03\$A(16, 16)	5) = .81922E + 03 \$A (16,	6) = .11582E+04
006725	A(16, 7) = .14941E+04\$A(16, -16)	8) = .17552E + 048A(16)	9) = .19202E+04
006732	A(16, 10) = .20536E+048A(16, 10) = .20536E+000000000000000000000000000000000000	11) = .22267E + 04\$A(16,	12) = .23844E+04
006736	A(16, 13) = .248725+04\$A(16, 13)	141 = .26773E + 048A(16, 14) = .26773E + .26774E + .267774E + .26774E + .267774E + .26774E + .26774E + .26774E + .26774E + .267774E + .26774E + .267774E + .26774E + .26774E + .26776E + .26774E + .26774E + .267774E + .267774E + .267774E + .267774E + .2677774E + .267774E + .267774E + .26777	15J = .29390E+04
006743	A(16, 16) = .33664E+04\$A(16, 16)	17) = .37374E + 04 (16,	(18) = .41629E+04
006747	A(16, 19) = .46508E+04\$A(16, 16)	201 = .53897E + 048A(16)	21) = .65059E+04
006754	A(16, 22) = .80701E+04\$A(16, 16)	231 = .89719E + 04 \$A (16,	24) = .10479E+05
006760	A(16, 25) = .11227E+053A(16, 16)	26) = .12115E + 053A(16)	271 = .12754E+05
006765	A(16, 28) = .13251E+05\$A(16, 16)	29)= .13926E+05\$A(16,	30) = .14537E+05
006771	A(15, 31) = .15139E+05 $BA(16, 31) = .15139E+05$ $BA(16, 31) = .15139E+05$	32) = .15471E+058A(16,	33)= .15795E+05
006776	A(16, 34) = .16080E+05 $A(16, 34) = .16080E+05$ $A(16, 34) = .16080E+05$	35) = .16372E+05\$A(16,	36)= .16761E+05

007002	A(15 - 37) = -17043E + 058A(16 - 38) = -17277E + 058A(16 - 39) = -1747.9E	105
007007	A(16, 40) = .17642E + 05 $(16, 41) = .17853E + 05 $ $(16, 42) = .18094E +$	05
007013	A(16, 43) = .18360E+05\$A(16, 44) = .18557E+05\$A(16, 45) = .18709E+	05
007020	A(16, 46) = .18924E+05\$A(16, 47) = .18966E+05\$A(16, 48) = .19121E+	105
007024	A(16, 49) = .19261E+05\$A(16, 50) = .19377E+05\$A(16, 51) = .19561E+	05
007031	A(16, 52) = .19907E + 05\$A(16, 53) = .20261E + 05\$A(16, 54) = .20533E + .20532E + .2052E + .20	05
007035	A(16, 55) = .20708E+05\$A(16, 56) = .20940E+05\$A(16, 57) = .21391E+	05
007042	A(16, 58) = .22228E+05\$A(16, 59) = .23407E+05\$A(16, 60) = .25130E+	05
007046	A(16, 61) = .26980F+05\$A(16, 62) = .28988F+05\$A(16, 63) = .30990E+	05
007053	B(16, 1) = .61044E + 02\$B(16, 2) = .57703E + 02\$B(16, 3) = .55127E + .55127E + .5512E	102
007057	B(16, 4) = .65642E+02\$B(16, 5) = .86587E+02\$B(16, 6) = .10961E+	03
007064	B(16, 7) = .13399E+03\$B(16, 8) = .14987E+03\$B(16, 9) = .15872E+	0.3
007070	B(16, 10) = .16274E+03 $B(16, 11) = .16612E+03$ $B(16, 12) = .16175E+$	03
007075	B(16, 13) = .15670E+D3\$B(16, 14) = .15363E+03\$B(16, 15) = .15519E+	03
007101	B(16, 15) = .15903E + 03B(16, 17) = .16206E + 03B(16, 18) = .16349(+)	03
007106	B(16, 19) = .16304E+03\$B(16, 20) = .16117E+03\$B(16, 21) = .15908E+	03
007112	B(16, 22) = .15624E+03B(16, 23) = .15621E+03B(16, 24) = .15480E+	03
007117	B(16, 25) = .15518E+03\$B(16, 26) = .15660E+03\$B(16, 27) = .15801E+	03
007123	B(16, 28) = .16016E + 03\$B(16, 29) = .16195E + 03\$B(16, 30) = .16287E +	03
007130	B(16, 31) = .16287E+03\$B(16, 32) = .16383E+03\$B(16, 33) = .16478E+	03
007133	B(16, 34) = .16790E + 03BB(16, 35) = .17211E + 03BB(16, 36) = .17991E +	03
007140	B(16, 37) = .18661E+03\$B(16, 38) = .19579E+03\$B(16, 39) = .20513E+	03
007144	B(16, 40) = .21981E + 03B(16, 41) = .24929E + 03B(16, 42) = .29485E + .294855E + .29485E + .29485E + .29	03
007151	B(16, 43) = .36318E+03 $B(16, 44) = .42604E+03$ $B(16, 45) = .47047E+$	0.3
007155	B(16, 46) = .54199E+03\$B(16, 47) = .55511E+03\$B(16, 48) = .59348E+	03
007162	B(16, 49) = .61339E+03\$B(16, 50) = .60219E+03\$B(16, 51) = .54714E+	03
007166	B(16, 52) = .44817E+03BB(16, 53) = .36861E+03BB(16, 54) = .31389E+	03
007173	B(16, 55) = .29338E+03\$B(16, 56) = .27216E+03\$B(16, 57) = .25086E+	0.3
007177	B(16, 58) = .22346E + 03B(16, 59) = .19296E + 03B(16, 60) = .15635E +	03
007204	B(16, 61) = .13336E+03 $B(16, 62) = .11235E+03$ $B(16, 63) = .10124E+$	0.3
007210	A(17, 1) = .00000E+008A(17, 2) = .23086E+028A(17, 3) = .25985E+	20
00/214	A(17, 4) = .83673E+028A(17, 5) = .13292E+038A(17, 6) = .17302E+	0.3
007220	$\frac{A(1/2)}{A(1/2)} = \frac{19535 + 038A(1/2)}{A(1/2)} = \frac{22144 + 038A(1/2)}{A(1/2)} = \frac{25228 + 0}{25228 + 0}$	<u>U</u> <u>3</u>
007225	A(1/2, 10) = .30426E+03\$A(1/2, 11) = .34306E+035A(1/2, 12) = .43547E+	05
007276	A(1/2, 1/2) = .000302+032A(1/2, 14) = .915002+032A(1/2, 15) = .133092+	04
007235	A(1/2) = -10454E+04BA(1/2) = -1/402E+04BA(1/2) = -10002E+	04
007242	A(1/2, 1/2) = -3195685 + 0.48A(1/2, 20) = -205095 + 0.48A(1/2, 21) = -2117/5 + A(1/2, 20) = -225085 + 0.48A(1/2, 20) = -225085	04
007247	AVII9 221- +210/05404DAVII9 231- +224225404DAVII9 241- +2209054 A/17, 261- 2303754064A/17, 261- 2365554064A/17, 271- 2378054	04
007250	$\frac{4(17, 28)}{2(10, 20)} = \frac{2(10, 20)}{2(10, 20)} = \frac{2(10, 20)}{2(1$. 12 V . 11 L
007266	A(17, 31) = .25271F + 0.45A(17, 32) = .25691F + 0.45A(17, 33) = .25703F + .2570F + .2570	-04 -04
007271	A(17, 34) = .25711F+048A(17, 35) = .25977F+048A(17, 36) = .26106F+	от П <u>с</u>
007275	A(17, 37) = .26354F+048A(17, 38) = .26535F+048A(17, 39) = .26758F+	14
007302	A(17, 40) = .26920F+047A(17, 41) = .27156F+047A(17, 42) = .27354F+	14
007306	A(17, 43) = .27551E+04\$A(17, 44) = .27878E+04\$A(17, 45) = .28216E+	04
007313	A(17, 46) = .28651E+048A(17, 47) = .29441E+048A(17, 48) = .31042E+	04
007317	A(17, 49) = .34575E+043A(17, 50) = .41063E+048A(17, 51) = .43851E+	04
007324	A(17, 52) = .49851E+043A(17, 53) = .59417E+043A(17, 54) = .68717E+	04
007330	B(17, 1) = .20453E+03B(17, 2) = .18779E+03B(17, 3) = .18783E+	03
007335	B(17, 4) = .21169E+03\$B(17, 5) = .28373E+03\$B(17, 6) = .36784E+	03
007341	B(17, 7) = .23855E+03BB(17, 8) = .22643E+03BB(17, 9) = .17990E+	03
007346	B(17, 10) = .16007E+03B(17, 11) = .15083E+03B(17, 12) = .14491E+	03
007352	B(17, 13) = .15217E+03B(17, 14) = .16593E+03B(17, 15) = .18541E+	03
007357	B(17, 16)= .20096E+03\$B(17, 17)= .20899E+033B(17, 18)= .21721E+	03
007363	B(17, 19) = .22853E+03\$B(17, 20) = .24086E+03\$B(17, 21) = .25095E+	03
007370	B(17, 22) = .26283E+03\$B(17, 23) = .27595E+03\$B(17, 24) = .29140E+	03
007374	B(17, 25) = .31080E+038B(17, 26) = .33445E+038B(17, 27) = .36507E+	03
007401	B(17, 23) = .41062E+03\$B(17, 29) = .48007E+03\$B(17, 30) = .60541E+	03

007405	B(17, 31)=	.772945+035B(17,	32)= +97784E+03\$8(17,	331 = +12741E+04
007412	B(17, 34)=	12848E+04\$B(17,	35) = .15219E + 043B(17)	36) = .17688E+04
007416	B(17, 37) =	.19180E+04\$B(17,	38) = .19195E + 04\$B(17)	39) = •17526E+04
007423	8(17, 40)=	<pre>.15044E+04\$B(17,</pre>	(41) = .10400E + 0488(17)	42)= •71391E+03
007427	B(17, 43) =	.56878E+93\$B(17.	44) = .44182E+03\$B(17)	45)= .366265+03
007434	B(17, 45)=	.30721E+03\$B(17,	47) = .24840E+03\$B(17,	48)= .19339E+03
007440	B(17, 49) =	.14072E+033B(17.	50) = .10033E + 033B(17)	51) = .10033E+03
017444	B(17. 52)=	.90123E+02\$B(17.	53) = .78220E + 023B(17)	54) = .74819E+02
007451	A(13, 1) =	.00000F+005A(19.	2) = .40222E + 023A(19)	31 = .11157F+03
007454	A(19, 4) =	.18363E+038A(19.	$5) = .26773E + 0.3 \pm A(19)$	5) = -33718E+03
007461	$\Delta(19, 7) =$	-39335F+03\$A(19-	8) = -44208E + 0.3 tA (19)	9) = .49658E+0.3
007465	A(19, 10) =	-54946E+0374(19-	111 = -60221E + 033A(13)	12) = -66659E + 03
007402	A(19, 13) =	.72070E+03\$A(19-	141 = .77770E + 0.38A(19)	151 = -83613E + 03
007476	$\Delta(19, 16) =$	-94259E+038A(19-	$171 = .10588E + 0.4 \pm 0.19$	18) = .11661E+04
007475	A(19, 19) =	-125162+0434(19-	20) = -13532E + 048A(19)	21) = .15115E+04
007203	$\Lambda(19, 22) =$	158376+04 \$4 (19.	$231 \pm 18372E + 044A(19)$	
007516	$\lambda(10, 25) =$	22082E+04 \$A(19)	$261 \pm 23880 \pm 0.41414$	271= 256785+04
007514	$\Lambda(10, 28) -$	26077=+04\$A(10-	20)231/35+0/th/(10)	201- 203665404
007920		201205+04#A(10	22)	$307 = -235000 \pm 04$ $331 = -345075 \pm 00$
007525	A1199 311-	2000EE+04PA(10	32)	331- •31347ET04
007531	A(19, 34) =	- 322U9E + U4 DA (19)	- 391 363475+040A1199 - 701 765325+0654443	351 354/4 <u>E</u> +U4
00/516	<u>A (17, 37) =</u>	-34069E+046A119	301 = .34992t+U4DA1191	391= 32009E+04
007542	A(19, 40) =	• 35558E+04 \$A (19,	41)= .36155E+048A(19,	421= .366662+04
007547	A(19, 43) =	- 37446E+04\$A(19;	44)= .3/9/5E+U45A(19)	45) = +384062+04
007553	A(19, 45) =	-3790UE+U4%A(19,	471 = .39404E + 043A(19)	48)= •39786E+04
007560	A(19, 43) =	•400755+04\$A(19)	50)= .40428E+045A(19)	51) = .40741E+04
007564	A(19, 52)=	•41159E+048A(19,	53)= +41943E+U45A(19,	541= .424132+04
00/5/1	A(19, 55) =	-430275+04\$A1199	561 = .437971 + 0434(19)	5/1= •44359E+U4
007575	A(19, 58) =	.44751E+04\$A(19)	59) = .45104E + 048A(19)	60) = -45353E+04
007602	A(19, 61)=	.45720E+04\$A(19,	62) = .46089E + 045A(19)	631 = .46580E+04
007606	A(19, 64) =	.47020E+04\$A(19,	65) = .47544E + 04 \$A (19,	65) = .47909E+04
007613	A(13, 67)=	•48316E+04\$A(19,	68) = .48670E + 04\$A(19)	69) = .49120E+04
007617	<u>A(19, 73) =</u>	-49791E+04\$A(19,	71) = .50737E + 043A(19)	72) = .51712E + 04
007624	A(19, 73)=	.53834E+04\$A(19,	74 = $.55489E + 048A(19)$	75) = .57063E + 04
007630	8(1, 1)=	.16000E+03\$B(19,	21 = .17532E + 0.33B(19)	3) = .19288E+03
007635	B(19, 4)=	.21959E+033B(19,	5) = .24566E + 0.3\$B(19)	6) = .26305E+03
007641	B(19, 7)=	.27661E+03\$B(19,	8) = .28874E + 03\$B(19)	9) = .29881E+03
007646	B(19, 10) =	•30802E+03\$B(19,	(11) = .31581E + 03\$B(19)	121 = .32383E+03
007652	<u> </u>	<u>.32832E+03\$8(19,</u>	141 = .33238E + 035B(19)	151 = .33379E + 03
007657	B(19, 16) =	.33425E+03\$B(19,	17) = .33761E + 033B(19)	181 = .33607E + 03
007663	B(19, 19) =	• 334035+03\$B(19,	201 = .32850E + 0.358(19)	211 = -32099E + 03
007679	B(19, 22)=	•31437E+03\$B(19,	23 = $.30871E + 033B(19)$	$24) = .30318\pm03$
007674	B(19, 25)=	.29921E+03\$B(19,	26) = .29700E + 03\$8(19)	271 = .29567E + 03
007701	B(19, 28)=	.239495+03\$B(19,	291 = .30341E + 03\$8(19)	30) = .31265E+03
007705	B(19, 31) =	<u>.32105E+03\$B(19,</u>	$32) = .32626E + 03 \pm B(19)$	331 = .33590E + 03
007712	B(19, 34)=	.34503E+03\$B(19,	351 = .35432E + 03BB(19)	36)= .36866E+03
007715	B(19, 37) =	.38520E+03\$B(19,	38) = .40088E + 035B(13)	39)= •4199DE+03
007723	B(19, 40)=	•44942E+03\$B(19,	41) = .48173E + 03\$B(13)	42)= •51309E+03
<u>007727</u>	B(19, 43) =	.57367E+03\$B(19,	44) = .60990E + 0358(13)	45)= .63632E+03
007734	B(19, 46)=	•67519E+03\$B(19,	47) = .71443E + 03\$B(19)	48) = .74204E+03
007740	B(19, 49)=	.75854E+03\$B(19,	50) = .77201E + 03	51) = .77574E+03
007745	B(19, 52)=	.78086E+03\$B(19,	53)= .79017E+03\$B(19,	54)= .78645E+03
007751	B(19, 55) =	.77900E+03\$B(19,	56) = .76875E+033B(19,	57) = .76549E + 03
007756	B(19, 53)=	•75944E+03\$B(19,	59) = .75098E+03\$B(19,	60)= .73666E+03
007762	8(19, 61)=	.70427E+03\$B(19,	62) = .68058E+03\$B(19,	63) = .63985E + 03
007767	B(19, 64)=	•59923E+03\$B(19,	65) = .56539E+03\$B(19,	66)= •54188E+03
007773	B(19, 67)=	.51789E+03\$B(19,	68) = .49998E+03\$B(19,	691 = .48629E + 03
010000	B(19, 70) =	.46923E+03\$B(19,	71) = .45237E+03\$B(19,	72) = .43557E+03

010011	A(21, 1) = .00000F+00BA(21, 2) = .83908F+02BA(21, 3) = .22053E+03
010014	A(21, 4) = .566585+03.A(21, 5) = .11515E+04.6A(21, 5) = .12857E+04
010021	A(21, 7) = .13834E+048A(21, 8) = .14619E+048A(21, 9) = .15595E+04
010025	A(21, 10) = .16170E+04BA(21, 11) = .16742E+04BA(21, 12) = .19270E+04
010032	A(21, 13) = .247022+048A(21, 14) = .29879E+048A(21, 15) = .36318E+04
010036	A(21, 15) = .33130E+045A(21, 17) = .40531E+045A(21, 18) = .42759E+04
010043	A(21, 19) = .44873F+04BA(21, 20) = .46396E+04BA(21, 21) = .47533E+04
010047	A(21, 22) = .43551E+04GA(21, 23) = .49451E+04GA(21, 24) = .50305E+04
01 0054	A(21, 25) = .50978t + 045A(21, 26) = .51751t + 045A(21, 27) = .52499t + 04
010050	A(21, 28)= +53390"+04%A(21, 29)= +541541+04%A(21, 30)= +520942+04 A(21, 21)= ==================================
	$\frac{A(21, 31) = .998(1.404)A(21, 30) = .99932240404(21, 30) = .970302404}{A(21, 30) = .586000000000000000000000000000000000000$
010076	$\frac{1}{3} \frac{1}{3} \frac{1}$
010075	A(21, 40) = -50640E + 04EA(21, 41) = -51132E + 04EA(21, 42) = -51610E + 04
010102	$\Delta(21, 43) = -62024(+048\Delta(21, 44) = -6243(+048\Delta(21, 45) = -63040E+04$
010113	A(21, 46) = .63(32) + 046A(21, 47) = .64524(4) + 046A(21, 48) = .65632(2+04)
010121	A(21, 43) = .668155 + 048A(21, 50) = .682935 + 048A(21, 51) = .696255 + 04
010124	A(21, 52) = .70702E+04\$A(21, 53) = .72275E+04\$A(21, 54) = .75316E+04
010131	A(21, 55) = .80560E+04\$A(21, 56) = .85545E+04\$A(21, 57) = .00000E+00
010134	B(21, 1) = .220247+02B(21, 2) = .23609E+02B(21, 3) = .23011E+02
010141	B(21, 4) = .32274E+025B(21, 5) = .44426E+028B(21, 6) = .48748E+02
010145	B(21, 7) = .54846E+025B(21, 8) = .62053E+025B(21, 9) = .77240E+02
010152	B(21, 10) = .84886E+025B(21, 11) = .90748E+025B(21, 12) = .98702E+02
010156	B(21, 13) = .11158E+038B(21, 14) = .12395E+038B(21, 15) = .14061E+03
010163	3(21, 16) = .147647 + 0358(21, 17) = .15473E + 035B(21, 18) = .16401E + 03
010167	B(21, 19) = 17483E+035B(21, 20) = 18418E+035B(21, 21) = 19349E+03
010174	B(21, 22) = .29428E + 0.5BB(21, 25) = .21524E + 0.5BB(21, 24) = .22981E + 0.5BB(21, 25) = .21524E + 0.5BB(21, 24) = .22981E + 0.5BB(21, 25) = .21524E + 0.5BB(21, 24) = .22981E + 0.5BB(21, 25) = .21524E + 0.5BB(21, 24) = .22981E + 0.5BB(21, 25) = .22881E + 0.5BB(21, 25) = .228
	8(21, 29)= +24429t+U3\$8(21, 29)= +20/42t+U3\$8(21, 27)= +303U9t+U3 3/34 - 301= -75325=+07\$8(23, 30)= -40/705+07\$0/21 - 301= -472/75+03
010205	2/21 - 3/2 - 3/22/2 + 0.5 +
010211	R(21, 34) = -931845(+03)R(21, 35) = -10656(+04)R(21, 36) = -11777(+04)
010222	B(21, 37) = .12398F + 045B(21, 38) = .13172F + 045B(21, 39) = .13628F + 04
010227	B(21, 40) = .13845E+045B(21, 41) = .13655E+045B(21, 42) = .13237E+04
010233	B(21, 43) = .119872+045B(21, 44) = .10174E+045B(21, 45) = .86500E+03
010240	B(21, 45) = .73361E+03\$B(21, 47) = .61972E+03\$B(21, 48) = .51148E+03
010244	B(21, 4) = .42951E+03\$B(21, 50) = .3+576F+03\$B(21, 51) = .28612E+03
010251	B(21, 52) = .25159E+03\$B(21, 53) = .22503E+03\$B(21, 54) = .19720E+03
010255	3(21, 55) = .171192+03\$B(21, 56) = .14719E+03\$B(21, 57) = .00000E+00
010261	A(22, 1) = .00030E+00BA(22, 2) = .59070E+03BA(22, 3) = .14883E+04
010265	A(22, 4) = .470545+045A(22, 5) = .637945+045A(22, 6) = .826465+04
	$\frac{A(22, 7) = .90731 \pm 048A(22, 8) = .10765 \pm 058A(22, 9) = .11596 \pm 05}{A(22, 40) = .42260 \pm 0.02}$
	A(22) 10) = +122500±+058A(22) 11) = +13005±+058A(22) 12) = +13700±+05 A(22) 13) = 16686±405±A(22) 16) = 15676±05€A(22) 15) = 18003€±05
010302	$A(22, 15) = .1969666405 \pm 0.022, 17) = .208426 \pm 0.5 \pm 0.022, 18) = .221956 \pm 0.5$
010313	A(22, 13) = -238737 + 055A(22, 20) = -25366F + 058A(22, 21) = -26312F + 05
010320	A(22, 22) = .276457+05 hA(22, 23) = .23551F+05 hA(22, 24) = .29417E+05
010324	A(22, 25) = .30373E+055A(22, 26) = .31225E+05\$A(22, 27) = .31934E+05
010331	A(22, 29) = .324735+05\$A(22, 29) = .32985E+05\$A(22, 30) = .33394E+05
010335	A(22, 31) = .336979+05\$A(22, 32) = .33814E+05\$A(22, 33) = .34004E+05
010342	A(22, 34) = .342375+05\$A(22, 35) = .345095+05\$A(22, 36) = .34722E+05
010345	A(22, 37) = .34834E+05\$A(22, 38) = .35058E+05\$A(22, 39) = .35329E+05
010353	A(22, 49) = .35635E+05\$A(22, 41) = .35818E+05\$A(22, 42) = .35927E+05
010357	A(22, 43) = .351410 + 055A(22, 44) = .363280 + 053A(22, 45) = .364310 + 0554(22, 45) = .365310 + 0554(22, 45) = .365310 + 0554(22, 45) = .365310 + 0554(22, 45) = .365310 + 0554(22, 45) = .365310 + 0554(22, 45) = .365310 + 0554(22, 45) = .365310 + 0554(22, 45) = .365310 + 0554010 + 055400 + 055600 + 055600 + 0556000 + 0556000 + 055600 + 0556000 + 0556000 + 0556000000 + 05560000000000
010364	A(22, 46) = .365312+05BA(22, 47) = .36714E+05BA(22, 48) = .36823E+05
010370	$\frac{4(22, 49) = .37058 \pm 0554(22, 50) = .37269E \pm 0554(22, 51) = .37520E \pm 05}{4(20, 51) = .37520E \pm 05}$
UIU375 010404	A(22) 52)= •)//482+05%A(22) 53)= •380252+05%A(22) 54)= •385322+05 A(22) 55)= 380(55,05*A(22) 56)= 30(575,05*A(22) 57)= 30(555,05*
010401	$\frac{A(22)}{A(22)} = \frac{A(22)}{A(22)} = \frac{A(22)}{A$
010400	м касф - 207 — то 77 зостиран касф - 277 — т4исотстиракс ер - 601 — т 44466+05

r

010412	A(22, 61) = .40634E+058A(22, 61) = .4063AE+058A(22, 61) = .4063AE+058AE+00000000000000000000000000000000000	62)=	•40984E+05\$A(22, 63)= •41191E+05
010417	A(22, 64) = .41435E+058A(22, 64) = .414445E+058A(22, 64) = .41456E+058A(22, 64) = .41456E+000000000000000000000000000000000000	65) =	•41879E+05\$A(22, 66)= •42278E+05
010423	A(22, 67) = .42796E+058A(22,	68)=	•43624E+05\$A(22, 69) = •44834E+05
010430	A(22, 70) = .46263E+058A(22)	71)=	•48335E+05\$A(22. 72)= .50897E+05
010434	B(22, 1) = .63837E+01\$B(22, 1)	2) =	.68273E+013B(22, 3) = .69438E+01
010441	B(22, 4) = .91996E+01\$B(22, 4)	5) =	•10075E+02\$B(22, 6)= •11836E+02
010445	B(22, 7) = .13603E+02\$B(22, 1)	8) =	•14945E+02\$B(22• 9)= •16713E+02
010452	B(22, 10) = .19507E + 02\$B(22, 10) = .19507E + .1	11)=	•22451E+02\$B(22, 12)= •27072E+02
010456	B(22, 13) = .31550E+02\$B(22, 12) = .3150E+02\$B(22, 13) = .31550E+02\$B(22, 13) = .3150E+02\$B(22, 13) =	14)=	.30960E+0288(22, 15)= .30077E+02
010463	B(22, 16) = .29349E + 023B(22, 16) = .29349E + .023B(22, 16) = .29349E + .29349E + .023B(22, 16) = .29349E + .29349E + .023B(22, 16) = .29349E + .29348E + .2938E +	17) =	.29356E+02\$B(22, 18)= .30396E+02
010467	B(22, 19) = .30564E+02\$B(22, 19) = .30564E+02B(22, 19) = .30564E+02B(22, 19) = .30564E+02B(22, 19) = .30564E+02B	20)=	• 31034E+028B(22, 21)= • 31938E+02
010474	B(22, 22) = .32556E + 02\$B(22, 22) = .32556E + .3256E + .32556E + .3256E + .32556E + .3256E + .3256E + .3256E + .3256E + .3256E + .3256E + .32556E + .3256E + .32556E + .3256E + .32556E + .3256E + .32556E + .32556E + .3256E + .32556E + .3256E + .3256E + .32556E + .32556E + .32556E + .32556E + .3256E + .32	23)=	• 33456E+02\$B(22, 24)= • 35232E+02
010500	B(22, 25) = .37452E+02\$B(22.	26)=	•39572E+02\$B(22, 27)= •42600E+02
010505	B(22, 28) = .45629E + 02\$B(22, 28) = .45629E + .45628E + .4568E + .45628E + .4568E + .45628E + .45628E + .4568E + .4568E +	29)=	.49709E+025B(22, 30) = .54246E+02
010511	B(22, 31) = .60446E+02\$B(22, 31) = .6044E+02\$B(22, 31) = .6044B+02\$B(22, 31) = .604B+02\$B(22, 31) = .604B+02\$B(22, 31) = .604B+02B+02B+02B+00B+02B+00B+00B+02B+00B+00	32)=	.68699E+02\$B(22, 33) = .76688E+02
010516	B(22, 34) = .82658E+02\$B(22, 34) = .8268E+02\$B(22, 34) = .82658E+0200000000000000000000000000000000000	35)=	•93736E+02\$B(22, 36)= •11236E+03
010522	B(22, 37) = .13056E+03\$B(22.	38)=	.13989E+035B(22, 39) = .15242E+03
010527	B(22, 40) = .16913E+03\$B(22, 40) = .16913E+03	41)=	-18343E+03\$B(22, 42)= -20906E+03
010533	B(22, 43) = .24498F+03\$B(22, -24498F+03)B(22, -2448F+03)B(22, -2448F+03)B(22, -2448F+03)B(22, -2448F+03)B(22, -2488F+02)B(22, -2488F+03)B(22, -2488F+028F+03)B(22, -2488F+038F+038F+038F+038F+038F+038F+038F+0	44) =	-31029E+03\$B(22, 45) = $-39777E+03$
010540	B(22, 46) = .47004E+03B(22, 46)	47) =	•60745E+03\$B(22• 48)= •64055E+03
010544	B(22, 49) = .68725E+03\$B(22, 49) = .68725E+03\$B(23, 49) = .68725E+030\$B(23, 49) = .68725E+030\$B(23, 49) = .68725E+030\$B(23, 49) = .6872	50) =	.74485E+03\$B(22, 51)= .79282E+03
010551	B(22, 52) = .82934E+03\$B(22.	53)=	.86120E+0338(22, 54)= .90265E+03
010555	B(22, 55) = .92473E+03\$B(22,	56)=	•90539E+03\$B(22, 57)= •86108E+03
010562	B(22, 58) = .73333E+03\$B(22, 58) = .73334E+03\$B(22, 58) = .73334E+03\$B(23, 58) = .73334E+03\$B(22, 58) = .73334E+03\$B(22, 58) = .73334E+03\$B(22, 58) = .73334E+03\$B(22, 58) = .7334E+03\$B(22, 58) = .7344E+03\$B(22, 58) = .7344E+0	59) =	•57169E+03\$B(22, 60) = •53228E+03
010566	B(22, 61) = .47585E+033B(22, 61) = .4758E+0.4758E+0.475E+0.045E+0.475E+0.475E+0.0475E+0.475	62) =	•36975E+03\$B(22, 63)= •33133E+03
010573	B(22, 64) = .30343E+03\$B(22, 64) = .30344B+03\$B(22, 64) = .30344B+03\$B(22, 64) = .30343B+03\$B(22, 64) = .3034B+03\$B(22, 64) = .303B+03\$B(22, 64) = .303B+03B+03B+03B+03B+03B+03B+03B+03B+03B	65)=	•27816E+03\$B(22, 66)= •26287E+03
010577	B(22, 67) = .25223E+03\$B(22, 67) = .25222B+03\$B(22, 67) = .2522B+03\$B(22, 67) = .2522B+03\$B(22, 67) = .252B+03\$B(22, 67) = .252B+03B+03B+03B+03B+03B+03B+03B+03B+03B+03	68) =	•24375E+03\$B(22, 69) = •23523E+03
010504	B(22, 70) = .21459E + 03\$B(22, 10) = .21459E + .21458E	71)=	•19056E+033B(22, 72)= •17018E+03
010610	A(23, 1) = .00000E+005A(23, 1)	2)=	•30148E+03%A(23, 3)= •74571E+03
010614	A(23, 4) = .19055E+04\$A(23, 4) = .1905E+04\$A(23, 4) = .1905E+04\$	<u>5) =</u>	.25017E+04\$A(23, 6) = .28791E+04
010620	A(23, 7) = .33991E+04\$A(23, 7) = .33991E+0	8)=	•37464E+04\$A(23• 9)= •42366E+04
010625	A(23, 10) = .47745E+048A(23, 10) = .47745E+0.488A(23, 10) = .4784A(23, 10) = .478A(23, 10) = .478	11)=	•59754E+04\$A(23, 12)= •66851E+04
010631	A(23, 13) = .75822E+04\$A(23, 13) = .758242E+04\$A(23, 13) = .75824E+04\$A(23, 13) = .75824E+04\$A(23, 13) = .75824E+04\$A(23, 13) = .7582E+04\$A(23, 13) = .7582E+04\$A(23) = .7582E+04\$A(23, 13) = .7582E+04\$A(23, 13) = .7582E+04\$A(14) =	•85569E+04\$A(23, 15)= •99244E+04
010636	A(23, 16) = .11211E+05\$A(23, 16) = .11211E+05\$A(25, 16) = .1121E+05\$A(25, 16) = .1121E+05\$A(25	17)=	•13166E+05\$A(23, 18)= •15923E+05
010642	A(23, 19)= .17165E+058A(23,	20)=	•18542E+05\$A(23, 21)= •20175E+05
010647	A(23, 22) = .21830E+058A(23, 22)	23)=	.23003E+05BA(23, 24)= .23943E+05
010653	A(23, 25)= .24728E+05\$A(23,	26)=	•25569E+05\$A(23, 27)= •26524E+05
0 1066 0	4(23, 28) = .27326E+05\$A(23, 28) = .27326E+	29)=	-28166E+05 (23, 30) = $-28768E+05$
010664	A(23, 31) = .29249E+05\$A(23, 31) = .29249A(23, 31) = .29249A(23, 31) = .29248A(23, 31) = .2924A(23, 31) = .2924A(23, 31) = .2924A(23, 31) = .292A(23, 3	32)=	$\cdot 29713E + 05$ \$A (23, 33) = $\cdot 30045E + 05$
010671	A(23, 34) = .30545E+05\$A(23, 34) = .30545E+05	35)=	.31039E+05 (23, 36) = $.31622E+05$
010675	A(23, 37) = .32140E+055A(23, 37) = .32140E+0555A(23, 37) = .32140E+05055A(23, 37) = .32140E+05055	38) =	$\cdot 32608E + 05$ (23, 39) = $\cdot 33003E + 05$
010702	A(23, 40) = .33264E+05\$A(23, 40) = .33264E+	41) =	-3351DE+055A(23, 42) = -33768E+05
010706	A(23, 43) = .33973E+058A(23, -33973E+058A(23, -33973E+058A))	44) =	$\cdot 34279E + 05$ (23, 45) = $\cdot 34701E + 05$
010713	A(23, 46) = .35021E+05 $A(23, 46) = .35021E+05 $ $A(23, 46) = .35021E+05$	47)=	$\cdot 35394E + 05$ (23, 48) = $\cdot 35808E + 05$
010717	A(23, 49) = .30384E+058A(23, 49) = .30384E+000000000000000000000000000000000000	50)=	-36678E+05 (23, 51) = $-36931E+05$
010724	A(23, 52) = .37226E+053A(23, 52) = .372226E+053A(23, 52) = .37224E+053A(23, 52) = .37224E+0.27224E+0.27224E+0.2724E+0.0724E+0.0724E	53)=	.37436E+05 (23, 54) = $.37631E+05$
010730	A(23, 55) = .38036E+058A(23, 55) = .38036E+0500000000000000000000000000000000000	56) =	.38384E+053A(23, 57) = .38720E+05
010735	A(23, 58) = .39145E+053A(23, 58) = .39145E+05045E+0000000000	59)=	-39690E+058A(23, 60) = -40488E+05
010741	A(23, 61) = .41514E+05\$A(23, 61) = .41514E+05	= (50	•42635E+058A(23+63)= •44135E+05
010746	A(23) $b41 = -460792+058A(23)$	551=	• 490 90t + 45 A (23, 66) = • 53015t + 85
010752	A(23, 67) = .57158[+05\$A(23, 200)]	68)=	• b U 3 3 9 b + U b 3 A (2 3, 69) = • 00000 b + 00
010756	B(23, 1) = 5.0000E+013B(23, 0)	2)=	-65000000000000000000000000000000000000
UI U763	$B(23) = -848082 \pm 0258(23)$	5)=	• 0 9 0 0 Ct + U C \$ B (C) = 0 1 = • 9 2 2 6 9 E + 0 2
UIU/6/	B(25, 7) = -93229t + 028B(23, -9329t + 028B(23, -93289t + 028B(23, -93288t + 028B(23, -93288t + 02888t + 0288t + 02888t + 02888	6)=	• 91014E+U25B123, 9)= • 88939E+02
~ ~ ~ ~ ~ .		11)=	- 94639640288723。 121= .978376482

~

- - - - -----
	B(23, 13) =98355E+U2\$B(23, 14) =96877E+U2\$B(23, 15) =9595UE+U2
011005	B(23, 16) = .97051E+02\$B(23, 17) = .99633E+02\$B(23, 18) = .10377E+03
011011	$B(23, 19) = .10569E + 03 \pm B(23, 20) = .10817E + 03 \pm B(23, 21) = .11109E + 03$
011016	B(23, 22)= .11656E+03\$B(23, 23)= .12060E+03\$B(23, 24)= .12503E+03
011022	B(23, 25) = .12917E+03\$B(23, 26) = .13557E+03\$B(23, 27) = .14356E+03
011027	B(23, 28)= .15144E+03\$B(23, 29)= .15885E+03\$B(23, 30)= .16367F+03
011033	B(23, 31) = .16881E+03\$B(23, 32) = .17539E+03\$B(23, 33) = .18163E+03
011049	B(23, 34) = .193465+03BB(23, 35) = .20923E+03BB(23, 36) = .23066E+03
011044	B(23, 37) = .258095 + 038B(23, 38) = .28171E + 038B(23, 39) = .30647E + 03
011051	3(23, 40) = -321755 + 0358(23, 41) = -332985 + 0358(23, 42) = -342235 + 03
011055	B(23, 43) = -34807F+035B(23, 44) = -35207F+035B(23, 45) = -35366F+03
011052	$B(2)_{2} + 0^{-1} +$
011002	0/23 $+01 = -0.3200000000000000000000000000000000000$
	$\frac{1}{2} \frac{1}{2} \frac{1}$
	$D(23) = 242 - (2423) \pm 0.251 + 0.210 + (2100) \pm 0.251 + 0.200 + 0.251 + 0.200 + 0.251 + 0.25$
	$B(23, 23) = \cdot 1320/2 + 0320/$
011103	$B(23, 58) = .15516\pm 0.038B(23, 59) = .14824E+0.38B(23, 50) = .14081\pm 0.038B(23, 50) = .14081\pm $
011107	B(23, 61) = .13350E+035B(23, 62) = .12665E+035B(23, 63) = .11906E+03
011114	B(23, 64) = .11259E+03\$B(23, 65) = .10272E+03\$B(23, 66) = .94791E+02
011120	<u>B(23, 67) = .88790E+02\$B(23, 68) = .84116E+02\$B(23, 69) = .00000E+00</u>
011124	A(25, 1)= .00000E+00\$A(25, 2)= .62415E+03\$A(25, 3)= .14898E+04
011130	A(25, 4) = .34900E + 048A(25, 5) = .65223E + 048A(25, 6) = .95839E + 04
011134	A(25, 7)= .10405E+05\$A(25, 8)= .10916E+05\$A(25, 9)= .11349E+05
011141	A (25, 10) = .11932E+05\$A(25, 11) = .12664E+05\$A(25, 12) = .13217E+05
011145	A(25, 13) = .13594E+05\$A(25, 14) = .14020E+05\$A(25, 15) = .14771E+05
011152	A(25, 16) = .15522E+058A(25, 17) = .16920E+058A(25, 18) = .19161E+05
011156	A(25, 19) = .20823F + 05\$A(25, 20) = .22407F + 05\$A(25, 21) = .24360F + 05
011163	A(25, 22) = .26110F+058A(25, 23) = .27756F+058A(25, 24) = .29006F+05
D1 1167	A(25, 25) = .3033F+05(A(25, 25)) = .31057F+05(A(25, 27)) = .31084F+05
011174	A(25, 28) = .32901F + 0.5 (A(25, 29) = .33480F + 0.5 (A(25, 30) = .34152F + 0.5)
n • 1 2 n n	A(25, 31) = (346045+0540(25, 32) = (349605+0540(25, 33) = (3543(25)))
011200	A(2) = A(3) = -3 = 0 + 0 + 1 + 0 + 0 + 0 + 0 + 0 + 0 + 0 +
011211	$\frac{1}{10} - \frac{1}{10} $
	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
	$\frac{1}{1} \frac{1}{1} \frac{1}$
011222	A(22), $A(3) = -4U34(2+U2)A(22)$, $A(4) = -4U402(2+U2)A(22)$, $A(2) = -4U314(2+U2)A(2)$
011227	A(22, 40) = .412032+020A(25, 47) = .412002+020A(25, 40) = .417002+02
011233	A(25, 49) = .418/22+05 $A(25, 50) = .420762+05 $ $A(25, 51) = .422772+05$
011240	A (25, 52) = .42689E+05\$A (25, 53) = .43257E+05\$A (25, 54) = .43543E+05
011244	A(25, 55) = .43817E+05 $A(25, 56) = .44168E+05$ $A(25, 57) = .44640E+05$
011251	A(25, 58) = .45210E+05 (25, 59) = .45721E+05 (25, 60) = .46191E+05
011255	A(25, 61) = .46535E+05 $A(25, 62) = .47138E+05$ $A(25, 63) = .47666E+05$
011262	A(25, 64) = .48186E+05\$A(25, 65) = .48691E+05\$A(25, 66) = .49627E+05
011266	A(25, 67)= .50237E+05\$A(25, 68)= .51858E+05\$A(25, 69)= .54468E+05
011273	A(25, 70) = .56637E + 05 $A(25, 71) = .58371E + 05 $ $A(25, 72) = .60632E + 05$
011277	A(25, 73)= .62217E+05\$A(25, 74)= .65644E+05\$A(25, 75)= .69115E+05
011304	A(25, 76) = .73602E+05\$A(25, 77) = .75451E+05\$A(25, 78) = .76988E+05
011310	A (25, 79) = .79533E+05\$A (25, 80) = .81431E+05\$A (25, 81) = .85754E+05
011315	<u>A(25, 82) = .95316E+05\$A(25, 83) = .00000E+00}A(25, 84) = .00000E+00</u>
011320	B(25, 1) = .30801E+02\$B(25, 2) = .31200E+02\$B(25, 3) = .31730E+02
011325	B(25, 4) = .33091E+02\$B(25, 5) = .36715E+02\$B(25, 6) = .41131E+02
011331	B(25, 7) = .429185+02\$B(25, 8) = .44578E+02\$B(25, 9) = .47502E+02
011336	B(25, 10) = .51312E+02\$B(25, 11) = .57365E+02\$B(25, 12) = .63388E+02
011342	B(25, 13) = .65465E+02\$B(25, 14) = .67082E+02\$B(25, 15) = .68606F+02
011347	B(25, 16) = .70345E+02\$B(25, 17) = .72117E+02\$B(25, 18) = .74214F+02
011353	B(25, 19) = .75163E+02\$B(25, 20) = .76814F+02\$B(25, 21) = .78718F+02
011360	B(25, 22) = A0665F+028B(25, 23) = A2830F+028B(25, 24) = B4768F+02
011364	B(25, 25) = B(BR) DE+D2\$B(25, 26) = B(B(56E+D2)B(25, 27) - 02000E+02
011371	R(25, 28) = -95716F+028R(25, 20) = -909090000000000000000000000000000000
011375	$\frac{1}{2} \frac{1}{2} \frac{1}$
011373	01279 311- 0110715403001279 321= 0110215403001279 331= 0121415403

,

011402	B(25, 34) = -12817F+038B	125. 351= 13100F40388125 361- 136255403
011406	B(25, 37) = .14067E+03\$B	(25, 38) = .14859F + 0.3\$B(25, 39) = .16242F + 0.3
011413	B(25, 40) = .18230E+03\$B	(25, 41) = .21445E+03\$B(25, 42) = .25638E+03
011417	B(25, 43) = .30012E+03\$8	(25, 44) = .31297E + 033B(25, 45) = .41475E + 03
011424	B(25, 46) = .58387E+03\$B	(25, 47) = .76577E+03\$B(25, 48) = .88448E+03
011430	B(25, 49) = .93944E+03\$B	(25, 50) = .97118E+03\$B(25, 51) = .98738E+03
011435	B(25, 52) = .98749E+03\$B	(25, 53) = .97813E+03\$B(25, 54) = .96367E+03
011441	B(25, 55)= .94162E+03\$B	(25, 56)= .89267E+03\$B(25, 57)= .79372E+03
011446	B(25, 58) = .65435E + 03\$B	(25, 59) = .51537E + 03 $(25, 60) = .41903E + 03$
011452	B(25, 61) = .35634E+03	(25, 62) = .29047E + 03B(25, 63) = .25657E + 03
011457	B(25, 64) = -22450E+03\$B	(25, 65) = .20641E + 03 (25, 66) = .18133E + 03
011463	B(25, 67) = .17122E+U3\$B	(25, 68) = .15142E + 0.38B(25, 69) = .12847E + 0.3
	B(25, 70) = .11372E+03\$B	(25, 71) = .10394E + 03\$B(25, 72) = .98915E + 02
011474	B(25, 73)= .92563E+U2\$B	(25, 74) = .80834t + 0238(25, 75) = .71252t + 02
011501	$\frac{B(25)}{2} (5) = -650865 + 0238$	(25, 77) = .61772E + 023B(25, 78) = .56112E + 02
011505	B(25, 79) = .55159E+U23B	(25, 80)= .55541E+02\$B(25, 81)= .52812E+02
011512	DI250 027 - 00433270280	(25, 05) = 000000000000000000000000000000000
011516	KEAD IU9SHUI9DAIE9HE69HA W1-W1C/25 444000	G9 HETAL9 HE9 VEN 39 3P
011541	HD=SOPT(4 #HAC/3 14/25 4	##2#1 FA61
011552	10-SQXTX4+**#4075+14725+4	2440,2F10 31
011555		
011556	TTH=TTI=0.	
011561	IF (SP-LE-0-) GO TO 113	
011564	TTH=WD/WL**.5*(850.+35.5	•(WL•WD*SP*.001-120.)**2
	1/(WL*WD*SP*.001)**1.5)/(1.88-DENS) ** 3
011606	TTL=WD/WL**.5*850./(1.88	-DENS) ** 3
011615	113 CONTINUE	
011615	N=JJ=0	
011617	IF (METAL.NE.10HCOPPER)GO TO 1002
011621	M=1 \$NA=96	\$WDEN= 8.96
011626	TR2= 80492. \$TR3= 94228.	\$TR4=124008. \$TR5=173000. \$TR6=223550.
011636	1002 IF (METAL. NE. 10HALUMINUM	<u>) GO TO 1003</u>
011640	M=2 \$NA=80	\$WDEN= 2.699 \$FACT= .5360E+12
011645	1R2= 25238. BIR3= 32035.	\$1R4= 48561. \$1R5= 65776. \$1R6= 92614.
011655	1003 IF (METAL • NE • 10HGOLJ	
01165/		SWUEN=19.32 SFAU1= ./313E+12 STD1= (1000 ETD5=
011004	1005 TEINETAL NE 10051/VED	DIR4- 64950. DIR5= 33157. DIR6= 93014.
011074		PHDEN-10 50 #EACT- 00765412
011703	TP2= 61682, \$TP3- 71771,	\$TPL= 90132 \$TP5-112200 \$TPL-137070
011713	1005 TE (METAL NE. 10 HPLATINUM)60 TO 1006
011715	M=5 \$NA=82	\$WDEN=21.45 \$EACT- 37536+12
011722	TR2 = 14701, $$TR3 = 17979$.	\$TR4= 24979, $$TR5= 48947$, $$TR6= 93000$.
011732	1006 IF (METAL.NE. 10HNTCKEL) GO TO 1007
011734	M=6 \$NA=88	\$WDEN= 8-902 \$FACT= -5266F+12
011741	TR2= 17233. \$TR3= 21156.	\$TR4= 30173. \$TR5= 56007. \$TR6= 91900.
011751	1007 IF (METAL.NE. 10HIRON)GO TO 1008
011753	M=7 \$NA=96	\$WDEN= 7.874
011760	TR2= 12806. \$TR3= 14581.	\$TR4= 21568. \$TR5= 36105. \$TR6= 44837.
011770	1008 IF (METAL.NE. 10HPALLADIUM) GO TO 1009
011772	M=8 \$NA=68	\$WDEN=12.02 \$FACT= .3286E+12
011777	TR2= 16187. \$TR3= 19583.	\$TR4= 25979. \$TR5= 51366. \$TR6= 92741.
012007	1009 IF (METAL.NE.10HRHODIUM)GO TO 1010
012011	M=9 \$NA=73	\$WDEN=12.41 \$FACT= .*017E+12
012015	TR2= 33617• \$TR3= 37597•	\$TR4= 46139. \$TR5= 73983. \$TR6= 93013.
012026	1010 IF (METAL.NE.10HVANADIUM)GO TO 1011
012030	M=10 \$NA=68	\$WDEN= 6.11 SFACT= .3848E+12

								00520
012035		IR2 = 10444 = SIR3 = 1	2232. \$TR4=	15479.	\$TR5= 4	2785	SIR6=	9252 0
012045	1011	IF (METAL.NE. 10HTUNG	STEN JGO TO	1012				
012047		<u>M=11</u> <u>\$NA=61</u>	SWDEN=	19.3	SEACI=		+12	
012054		TR2= 32469. \$TR3= 3	5450 . \$TR4=	42128.	\$TR5= 7	5081. 1	STR6=	94910.
012064	1012	IF (METAL.NE. 10HCAD)	IUM)GO TO	1013				
012066		M=12 \$NA=71	\$WDEN=	8.65	SFACT=	.13738	+12	
012073		TR2= 4550. \$TR3=	6348, <u>\$TR4</u> =	9169.	§TR5= 1	8049-1	STR6=	44400.
012103	1013	IF (METAL.NE.10HTIN)GO TO	1014				
012105		M=13 BNA=70	\$WDEN=	7.31	SFACT=	<u>.0643</u>	+12	
012112		TR2= 1727. \$TR3=	2870. \$TR4=	8023.	\$TR5= 1	2447. 1	STR6=	24151.
012122	1014	IF (METAL.NE. 10HMOL)	BDINUMIGO TO	1015				
012124		M=14 \$NA=92	\$WDEN=	10.22	\$FACT=	•6365E	+12	
012131		TR2= 30097. \$TR3= 3	3005. \$TR4=	42905.	\$TR5 = 7	3952. 1	STR6=1	43200.
012141	1015	IF (METAL.NE. 10HZIRO	ONIUM JGO TO	1016				
012143		M=15 \$NA=73	\$WDEN=	6,53	\$FACT=	.10005	+12	
012150		TR2= 2843. \$TR3=	3812. STR4=	6082.	5TR5= 1	6665. 1	STR6=	30582.
012160	1016	IF (METAL.NE. 10HTITA	NIUM) GO TO	1017	-			
012162		M=16 \$NA=63	\$WDEN=	4.54	SFACT=	.09572	2+12	
012170		TR2= 2864. \$TR3=	4000. STR4=	6906.	STR5 = 1	9261. 1	STR6=	30990.
012200	1017	TE (METAL NE. 10HBIS)	UTH JGO TO	1018				
012202		M=17 \$NA=54	\$WDEN=	9.747	BFACT=	• 35 3 3E	+10	
012207		TR2 = 168.7 TR3 =	440.65TR4=	1553.	185 =	2654 9	TR6=	6872.
012217	1018	CONTINUE						
012217	1019	TE (METAL .NE. 10HSCA)		1020				
012221	1017	M=19 \$NA=75	\$WDEN=	2,992	REACT=	.01258	+12	
012226		TR2 = 684.88TR3 =	1020, STR4=	1730.	ATR5=	4194 1	STR6=	5706.
012236	1020	CONTINUE			•••••			
012236	1021	TE (METAL - NE- 10HI FAT) 60 10	1022				
012240	1961	M=21 \$NA=56	\$WDEN=	11.35	SFACT=	.0155E	+12	
012245		TR2= 1424. 5TR3=	1670. STR4=	2553.	STR5=	6066. 1	STR6=	8556.
012255	1022	TE (METAL - NE - 10HZING		1023	• • • •			
012257	••=-	M=22 \$NA=72	\$WDEN=	7.133	SFACT=	•4403E	+12	
012264		TR2= 12980. \$TR3= 1	4348. STR4=	17067.	3TR5= 3	8945. 1	STRE=	50897.
012274	1023	IF (METAL .NE. 10HURAN	IUM)GO TO	1024				
012276		M=23 \$NA=68	\$WDEN=	18.95	SFACT=	.30636	+12	
012303		TR2= 6090. TT23=	7130. \$TR4=	13575.	STR5= 3	4701. 1	TR6=	60339.
012313	1024	CONTINUE	•••••					
012313	1025	TE (NETAL NE. 10H70AL	INPT IGO TO	9999				
012315	1027	M=25 \$NA=82	SWDEN=	19.9	SFACT=	.45828	+12	
012322		TR2= 10387. \$TR3= 1	3391. \$TR4=	21572.	STR5= 4	2689. 1	STR6=	95316.
012332	3393	CONTINUE			-			
012332		IFLAG=1						
012333		IF (M.NE. 0) GO TO 30						
012334		PRINT 20.METAL						
012342	20	FORMAT (1H1. THE REG	UESTED METAL	-#A10.23	X*IS NO	T ON FI	LE#)	
012346		GO TO 200						
012346	30	CONTINUE						
012346	909	CONTINUE	•		-			
012346	91.3	CONTINUE						
012346		K=NA	• •	-		*		
012350	50	CONTINUE						
012350		IF (M.EQ.0) GO TO 200						
012351		KK=K-1						
012353		IF (T.EQ.D.)GS=CLAST	=TLAST=E=0.			· · ·		
012360		IF (T.EQ.0)=0						
012362		GS=GS+(T-TLAST)/2-	(C++2+CLAST+	+2)/WAC	++2			
012371		DO 60 I=2.K			-			
012372	·,	TF (A (M. I) -1 T-GS) GO	TO 60					
		_	· - · ·					
			and the second					• •

è

.

-

-

012377	GQ. TQ 70
012400	60 CONTINUE
012403	SR1=FACT/GS**2*WLC/WAC *1.E-5
012407	GO TO 107
012410	70 CONTINUE
012410	SR1 = (B(M, T-1) + (B(M, T) - B(M, I-1)) * (GS-A(M, I-1))/
ULLTIG	(A, (M, T) = A, (M, T = 1)) + W = C + MAC + 1 + E = 5
0121.71	
012431	
012431	E = E + (1 - 1LASI)/2 + (U + 2 + SRI+ULASI + 2 + RLASI)
012440	IF (T.EQ.O.) RLASI=SR1
012442	CLAST=C
012443	TLAST=T
012444	RLAST=SR1
012445	G=GS+WAC++?
012447	DUM3=SR1
012450	$I = (I \cap U I - E \cap O I \cap C \cap I \cap C \cap O I \cap O O O I \cap O O O O$
012456	
012494	
012455	
012456	
012460	GA(JJ) = G
012462	CA(JJ) = C
012464	VA(JJ)=C*ST1
012466	RA(JJ)=SP1
012470	R4(1)=B(M,1)*WLC/WAC*1.E-5
012475	PA(JJ)=C**2*SR1
012477	SE(JJ) = E/WAC/WLC/WDEN*1000.
012505	SG(JJ) = G/WAC + 2
012511	$\mathbf{F}(\mathbf{T}_{1} \mathbf{T}_{2} \mathbf{T}_{2} \mathbf{T}_{2}) = \mathbf{G}(\mathbf{T}_{2} \mathbf{G})$
010711	
012517	TELAGED
012917	DENT 400 NEGOT DATE, TTU, TTI, METAL, WAC, WIC, HE, DENS, SP
012520	$r_{\rm T}$ in the state of the
012547	
	ZTWIKC AREA-TE9.3, ZXTMMZTIDX, TLENGIH-TF0.4,
	32X*MM *//12X+EXPLUSIVE*AIU,14X*DENSITT*+1PF6.3,2X+
	4*GM/CM3*17X, *AREA*UPF7.0,2X*CM2/GM*//
	5 11X,*TIME*,8X,*CURRENT*,10X,*VOLTS*,11X,*OHMS*,
	610X,*POWER*,9X,*ENERGY*,9X,*ACTION*,10X,*GDENS*10X*EDENS*/
	71H _6X®MICROSEC#11X#AMPS#36X#KILOWATTS#9X#MILLIJ#7X_
	8*AMP2 SEC*,3X,*AMP2 SEC/MM4*11X*J/GM*/)
012553	DO 240 K=1,JJ
012554	IF(K.EQ.51.0R.K. EQ.101.0R.K.EQ.151.0R.K.EQ.201.0R.
	1K-E0-2511245-250
012576	245 PDINT 255
012010	CTV INTERVIEWS AND
UICOUC	227 FOR AN ADVERSION OF ANY AND ANY ADDENSION ANY ADDENSIONANA ANY ADDENSIANA ANY ANY ADD
	11UX, TUNET, JX, TENERGI J JA, AUTIUN, JUX, GDENS, LUX, EDENS, /
÷	ZIH DATTICKUSECTIATAMPS SOATKIEUWAITS SATHILLIJ 7/AD
	8+AMP2 SEC+,3X,+AMP2 SEC/MM4+11X+J/GM+/)
012506	250 IF (SG(K) .LT. TR2) KEY=3HS
012613	IF (SG(K).GE.TR2)KEY=3HS+L
012621	IF (SG(K).GE.TR3)KEY=3HL
012627	IF (SG(K).GE.TR4)KEY=3HL+V
012635	IF(SG(K).GE.TR5)KEY=3HARC
012643	IF (SG(K).GE.TR6)KEY=3HEXT
012651	PRINT 260-KEY-TA(K)-CA(K)-VA(K)-RA(K)-PA(K)-FA(K)-GA(K)-SG(K)-
012091	ISEIK)
n 1 7 7 1 1	260 ENDNAT (Y A3.60E11.3.00E15.1.E15.1.E15.5.E15.5.20E15.3.20E15.2.00E15.4
UTCI UT	<u>COU FURINALIANAJOFFIINJUFFIDALAFIDALAFIDADATJFIDADAJFIDADAJFIDAAAUPPIDA4</u>
	1617049817053

012705		240 CONT	INUE								
012707		PRIN	T 263								
012713		263 FORM	<u>AT (1H1)</u>								
012717		200 CONT	INUE								
012717		RETU	RN								
012721		END									
			••••••••••••••••••••••••••••••••••••••				• • • • • • •				
SUBPRO 0 45 36 7	GRA	M LENGTH				· · · · ·		· · · · · · · · · · · · · · · · · · ·			
EUNCTI	ON.	ASSIGNMENT	S				· •				
STATEM	ENT	ASSIGNMEN	TS	<u> </u>							
10	-	021165	20	-	021510	30	-	012347	50	-	012351
60		012401	70		012411	100		021523	107	-	012432
113	-	011616	200	-	012720	245	-	012577	250	-	012607
255	-	021615	260		021662	263		021673	909	-	012347
913	-	012347	1002	-	011637	1003	-	011656	1004	-	011675
1005	-	011714	1006	-	011733	1007	-	011752	1008	-	011771
1009		012010	1010		012027	1011		<u> 12046</u>	1012		012065
1013	-	012104	1016	-	012123	1015	-	012142	1016	-	012161
1017		012201	. * 4 * 1 1018		n12220	1010		012220	1020	-	812237
1021	_	012237	1022	-	012256	1022	_	012275	102/-	-	012714
1025		012314	9999	-	012333	TAC3	-	ATCC15	1064	-	01CJT4
BLOCK Shitch Variab	NAM 	ES AND LEN 000011 Assignment	GTHS 	-	005232						
A	-	021721	B.	-	033531	CA	-	001605002	CLAST	-	045357
DATE	-	005216002	DENS	-	005223602	DUNHY	-	000001001	DUN3	-	000000
F	-	045361	FA	-	000455002	FACT	-	045352	G	-	045365
GA	-	001131002	GS	-	045356	HE	-	005222002	Ť	-	045362
TELAG	-	045341	тоит	-	000000000		-	000000000	ĸ	-	045354
KEY	-	045366	KK	_	045355	M	_	045347	METAL	_	095221002
NΔ		045350	NSHOT	-	005215002	PA	-	003411002	RA	-	00273-002
RLAST	-	045364	SE	-	004065602	SG	-	004541002	SHOT	-	045342
SP	-	005224002	SRI		045363	ΤΔ		000001002	TIAST		<u>nus</u> 360
TR2	_	005225002	TR3	-	005226002	TRL	-	005227002	TRS	-	005230002
TR6	-	045353	TTH	-	045345	TTI	-	145346	VA	-	002261002
WAC	_	005220002	wn	_	045346	WDEN	-	045354	4 T	_	066363
WLC	-	005217002	. 7 2		リコンリスサ ー		-	V T J J J J J	A.C.	-	V T J J T J
START	OF	CONSTANTS		<u></u>							
D <u>127</u> 24		· · · · · · · · · · · · · · · · · · ·	=		· -		-				
START 021675	QF.	IEMPORARIE	S								
START	OF	INDIRECTS								· · ~·	- - · · · · · ·
021715		· · ·									
UNUSED	co	MPILER SPA	CE								

This page intentionally left blank.

APPENDIX 4

Computer Code EBWl Listing and Typical Output Results ~ -

- -

EBW1, T20 , CM200000. T.J.TUCKER BOX 102 ACCOUNT, \$509260356, \$5131, \$68702, \$40001020, \$RT, \$KUNC. ATTACH, MIMICB, MIMIC. PREP.MIMICB,MIMIC. ATTACH, USERA, TJ2. ATTACH, USERB, TPT. COLLECT, BINARY, PROGRAM=MIMIC, MIMIC, USERA, USERB, SCORS. RINARY. . (______ C PROGRAM REQUIRES TWO DATA CARDS-0 -----CIRCIUT PARAMETERS-------C С READ IN INDUCTANCE, SOURCE RESISTANCE, CAPACITANCE, VOLTAGE, PRINT OUT С C TIME INCREMENT, AND TOTAL TIME OF RUN. C UNITS ARE HENRIES, OHMS, FARIDS, VOLTS, AND SECUNDS. C USE STANDARD MIMIC 12 COLUMN FORMAT. С C----SECOND DATA CARD-SR1 WIRE DEFINITION------C CARD INCLUDES SHOT NUMBER, DATE, WIRE LENGTH IN MILLIMETERS, WIRE С AREA IN SQUARE MILLIMETERS, AND WIRE METAL. С $\boldsymbol{\mathcal{C}}$ C FORMAT AS 6 FIELDS OF 10 COLUMNS, WIRE METAL LEFT HAND JUSTIFIED. C C IF DETONATOR PREDICTIONS REQUIRED INCLUDE 3 TEN COLUMN FIELDS OF HE TYPE, DENSITY IN GRAMS/CM3, AND SPECIFIC SURFACE IN CM2/GRAM. С PAR(L,R,C,V,DT,TTOT) -v*c QC SR2(TTOT,RW) FLAG1 RW SR1(I,T,DT,TTOT) -1 • / L*(Q/C+1DQ*(RW+R)) 2DQ 100 INT (2DQ,0.) INT(100,00)Q DQ T F INT(I*I*RW,0.) G TNT(T*T,0.)FIN(T,TTOT) FLAG1 END . 1.00E-6 1000. .25F-6 •0020E-6 •100E-6 • 1 1-2-75 1. PETN 2. 1.141E-3GOLD 1. 2000.



1.	L • COOOOE-07	R 1.00000E-0	1	C 1.00000E-06	V 1.00000E+03	0T 2.000001	E-09	TTOT 2.500002-07	
	TEST NO	- 2		DATE 1-2-75		TTHS	374	298 AMPS	· · · · · · · · · · · · · · · · · · ·
	BRIDGEWIRE-	-GOL D		WIRE AREA-1.141E-33	HH2	LENGTH	1.0000	НМ	
	EXPLOSIVE	-PETN		DENSITY 1.000 GM	/CH3	AREA	5000	CH2/GH	
	TIME	CURRENT	VOLTS	OHMS	POWER	ENERGY	ACTION	GDENS	EDENS
MIC	RUSEC	AMPS		<u> </u>	ILUWAITS	MILLIJ	AMP2 SEC	AMP2 SEC7MM4	J/61
<u>s</u>	• 0 2	23.0	. 4	.02168	.009	.00	.0006	1.9173E-01	.000
S	.004	39.9	• 9	.02167	.034	.00	.0000	1.6072E+00	.002
S	.06	59.8	1,3	.02164	.077	.00	.0000	5.4618E+00	.007
S	.008	79.6	1.7	.02158	•137	.03	.0000	1.2962E+01	•017
<u> </u>	.010	93.4	2.1	• 02148	•212	• 00	.0000	2. 33 U 3L+ U1	<u>+ 432</u>
2	+012	119.1	2.5	• 22133	.305	• U U	•8001	4.30/964J1 6.02625404	• 8 2 2
2	-016	150+8	2.9	<u>+ J2112</u>	.40/		.0001		
د د	•ULD . 148	179.0	3.3	• U 2 U D 2	+ 7 C J	• 4 4 4	.0001	1.4669F402	-187
<u>,</u>	. 121	197.5	<u> </u>	. 12817	.782		, 0.0.3	2. 10865+02	
2	. 322	215.9	4.3		.939	.01	.0003	2.6685E+02	. 32 5
<u>s</u>	. 124	236.3	4.7	.01999	1.117	.01	.3005	3.4579E+02	. 419
ŝ	.026	255.7	5.1	. 22035	1.310	• [1	.0306	4.3880E+02	. 52.8
5	.028	275.0	5.5	.)2011	1.520	.01	.0007	5.4699E+02	.657
S	.030	294.2	5.9	.02018	1.747	, 02	.0009	6,7144E+02	.805
S	.032	313.4	6.4	.02026	1.990	.02	.011	8.1326E+02	. 974
S	. 934	332.5	6.8	. 02036	2.250	• 03	.0313	9.7351E+02	1.160
S	• 53E	351.5	7.2	.020+6	2.529	•03	.0015	1.1533E+03	- 1. 38 3
S	.038	370.5	7.6	.02058	2.825	• 64	.0018	1.3535E+03	1.526
s	.340	389.5	8.1	.02071	3.141	• 64	.0021	1.57542+03	1.896
<u>s</u>	.042	468.3	8.5	.02085	3.477	• 05	.0024	<u>1,8139E+03</u>	2.196
5	. 644	427.2	9.0	-02103	3.933	• 65	.0027	2.0881E+03	2.528
<u>></u>		445.4	<u>9.4</u>	• • • • • • • • • • • • • • • • • • • •	4.210		.0031	2.50092403	2:072
2	.048	464.6	A •A	. 02136	4.610	• 17	.3035	2.04475407	3.636
ç	.052	<u>473:2</u> 501.7	10 3	12177			.0040	3. 4169F+03	4.206
2	• 5 5 L	520 2	11 4	- 2233	5 955	. 10	.0056	3. 81812+03	4.725
\$		538.6	12.1	. 02225	<u> </u>	. 12	.0055	4.2487E+03	5.287
ŝ	1058	557.1	12.5	. 02252	6.986	.13	.0061	4.70982+03	5.397
s	. 35 0	575.2	13.1	.02280	7.546	• 14	.0066	5.2021E+03	6.556
\$. 262	F 93.4	13.7	.02311	8.138	.16	.0375	5.72672+03	7.267
S	. 264	611.5	14.3	. [2 3 4 3	8.764	.18	.0082	6+2845E+03	8.034
<u>s</u>	.065	625.6	15.0	.02377	9.424	.20	.0390	6.3762£+03	8.858
\$.068	647.6	15.0	.02414	13.122	• 21	.0098	7.5328E+03	9.745
S	. 278	6F5.5	16.3	. 52452	10.859	• 24	.0106	8.16502+33	10.696
S	. 172	6P3.3	17.2	.02492	11.638	• 26	.0115	8.8539E+03	11.710
S	. 274	731.1	17.8	• 02535	12.459	. 28	.0125	9.60005+03	12.809
2	• J76	713.5	19.1	• J 2651	13.597	• 31	.0135	1.03/4=+04	13.994
<u>></u>	<u></u>	753.5	20.5	+ 1 2783	12. 172		-1146	1-20645+04	15+290
с С	•· CU	15314	22.0	• 32910	10.704	• 37	.0157	1.29365404	18.307
د ۲	+ 1 3 C ^ R /i	788 S	20.0 2012	• U 3 U 2 D 0 7 2 a L	10 221	• • 3	- 0100	1.38682+04	20.03.
5		100.10 807.7	22.03	€ L 3204 	21.802	• • • •	, 1107	1.48645474	21.026
2	• 0 0 0 0 • C 8 8	822.9	28-5	■ U 3 3 2 0 _ 3 3 4 7 A	23.548	• = 0 _ f T	1207	1.5863F+04	23.983
s	.090	839.8	30.2	• 11 0 77 / 12 _ 11 75 11 L	25.34A	• • A	. 122 a	1.69242+04	26.201
<u>š</u>	. 192	856.7	31.8	.03715	27.264		.0235	1.8330F+24	28.586
ŝ	. 194	873.5	37.5	.238.1	29.301	. 69	.0250	1.91792+04	31.151
S	196	892.1	34.3	r_3971	31.464	.75	.0265	2.03742+04	33.907
ŝ	.099	925.7	39.1	.04378	35.414	. 81	.0281	2.1614=+04	36.872
S	.100	923.1	4 F . 4	.04913	41.865	. 69	.0298	2.2900E+04	+1.505
-						• •			

k e

• V

HIGPNSC AMPS KILDAATES HILLU AMP2 SEC MP2 SEC AMP2 SEC AMP2 J/6H S 137 24-2 14-3 14-3 14-3 14-3 14-3 14-3 14-3 14-3 14-3 14-3 14-3 14-3 14-4 14-4 14-3 14-3 14-4 <t< th=""><th></th><th>TIME</th><th>CUPRENT</th><th>VOLTS</th><th>OHMS</th><th>POWER</th><th>ENERGY</th><th>ACTION</th><th>GDENS</th><th>EDENS</th></t<>		TIME	CUPRENT	VOLTS	OHMS	POWER	ENERGY	ACTION	GDENS	EDENS
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		MICROSEC	AMPS			KILOWATTS	MILLIJ	AMP2 SEC	AMP2 SEC/MM4	J/GM
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	s	. 102	934.3	4E.2	.04914	43.364	. 98	. 0 31 5	2.42322+04	44.372
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	S	.104	GEE E	+7.7	.04988	45.541	1.07	.0333	2.5611E+04	48. 376
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	S	.105	971.6	-1.1	.05263	49.677	1.15	.0352	2.7038E+04	52.693
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5	.128	487.4	55.4	.75615	54.747	1.26	.0371	2.85122+04	57.372
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$?	.110	1003.1	63.5	.0€330	63.700	1.38	.0391	3. 22336+04	62.739
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	S	.112	1319.6	59.5	. 36821	72.776	1.52		3.1603E+04	68,935
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5	.114	1033.9	70.6	.06825	72.965	1.66	.0433	3. 3221E+ 04	75.456
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	<u>s</u>	•11F	1042.2	76.7	. 07314	93.211	1.82	.0454	3.4888E+34	A2. 372
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	S	.118	1064.1	84.4	.07925	89.777	1.99	. 3477	3 . 5603E+04	90.091
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	S	.120	1078.9	<u>43.3</u>	. 18550	102.685	2,18	• 6 4 9 9	3.83672+04	98.724
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	S	.122	1093.4	1]3.8	.09496	113.526	2.39	.0523	4.J180£+04	108.395
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	S	.124	1107.6	445+2	+16424	127.874	2,63	.0547	4.20402+04	119,360
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	S+L	• 156	1121.5	123.2	+10989	139.219	2.90	.3572	4 . 3949E+ 04	131.386
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	<u>S+L</u>	.128	1135.1	1+6,0	.12861	165.697	3.20	. 1598	<u>4.5904£+04</u>	145.030
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	S+L	.130	1147.9	139.3	.16.9]	217.291	3.57	• 9624	4 . 7907E+04	161.981
L 134 1179.5 331.3 2275^{5} 332.325 4.7% 0.6677 5.23366.0% 215.207 L 135 1179.5 331.124 5.497 4.2010 L 149 1186.5 351.1 3.375^{5} 429.086 6.31 0.733 5.64374742 248.314 L 149 1185.6 351.1 3.375^{5} 429.086 6.31 0.733 5.64374742 268.819 L 144 1211.0 4.61.2 39655 5.21.658.6 6.20 0.790 6.27115.04 236.849 L 144 1211.0 4.61.2 39655 5.21.658.6 6.20 0.790 6.27115.04 237.807 L 144 1211.0 4.61.2 39655 5.21.658.6 6.20 0.790 6.27115.04 237.80 L 144 1211.0 4.61.2 39655 5.21.658.6 6.20 0.790 6.22515.04 221.558 L 144 1211.0 4.61.2 39655 5.21.658.6 10.53 0.049 6.2235124 242.558 L 144 1211.0 4.61.2 39655 5.21.658.6 10.53 0.049 6.2235124 242.558 L 144 1211.0 4.61.2 39655 5.21.658.6 10.53 0.049 6.225142 318.266 L 147 147 1227.6 5.31.626 11.43 0.909 6.97922.04 603.108 L 1227.6 760.3 62262 311.135 15.17 0.9339 7.2495744 6.633.108 L 1227.6 762.3 62262 311.135 15.17 0.9359 7.44002.04 603.108 L 147 155 1221.2 1.167. $0.67.9$ 1222.098 10.147 0.9959 7.44002.04 603.150 L 147 155 1221.2 1.167. $0.67.9$ 1222.098 10.147 0.9959 7.44002.04 603.150 L 147 156 1211.2 1.144.1 1.167.0 122.037 22.046 1.1627 7.04002.04 0.000.000 L 147 158 1211.2 1.144.1 1.167.0 122.037 22.04 10.000 0.000 0.0000 0.0000 0.00000 0.0000 0.00000 0.00000 0.00000 0.000000	S+L	.132	1159.6	229.1	.22311	299.995	4.08	1650	<u>4.9952£+04</u>	185.277
L 135 1179.3 3115 .2112 .2113 351.224 5.49 1275 5.43775 42 248.314 L 138 1178.5 351.1 .33775 429.086 6.31 .0733 5.631274 248.314 L 149 1135.8 332.4 1274 445.605 7.21 .0762 5.631674. 326.484 L 144 1217.0 445.2 .39655 531.435 9.30 1262 5.6316.744 47.1497 L 144 1217.0 445.2 .39555 531.435 9.30 1262 5.6316.744 47.1497 L 144 1217.0 445.2 .39555 531.435 9.30 1262 5.6316.744 47.1497 L 144 1227.8 733.4 .4575 647.4556 10.53 0899 6.5216.744 47.599 L 1 144 1227.8 733.4 .466.9 72.4674 11.90 .0879 5.7762.04 0391 5.7769.04 0391 5.7979.04 0391 5.7979.04 0391 5.7999.5769.04 0391 5.7999.5769.04 0391 5.7999.5769.04 0391 5.7999.57769.04 0391 5.7999.57769.04 0391 5.775.04 0390.5769.04 0391 5.7979.04 0391 5.7999.57770.7916 5.7120.0990.5769.039770.04 0392.04 0390.5979.04 039	L	.134	1163.9	321+3	.25755	352.525	4.74	.0677	5.2036±+04	215.207
L .118 118.5 151.3 .3.375 429.086 6.31 .073 5.63112.04 286.124 L .142 1193.6 332.4 .32784 463.655 7.21 .0762 5.8496.764 374.807 L .142 120.4 .3 .32784 463.655 7.21 .0762 5.8496.764 374.807 L .142 120.4 .421.54 .39955 581.435 9.30 .0220 6.27162.04 374.807 L .144 121.4 .432.3 .4375 647.455 10.53 .0249 6.52142.44 .477.529 L .444 1222.6 533.4 .4355 647.455 10.53 .0249 6.52142.44 .477.529 L .444 1222.6 .533.4 .4355 647.455 10.53 .0249 6.52142.44 .477.529 L .444 150 1222.5 564.6 .4335 813.266 13.43 .0309 6.37922504 609.10 L .444 150 1222.5 564.6 .42355 813.266 13.43 .0309 6.37922504 609.10 L .444 150 1222.5 564.6 .42355 813.266 13.43 .0309 7.2403544 .477.895 L .44 .150 1222.5 10.67.9 .2232.6 .406.40 .17.15 .03069 7.44002.44 .778.495 L .44 .156 1221.2 .141.2 .1167.4 .17255 10.66.40 .17.15 .03069 7.44002.44 .778.495 L .44 .156 1221.2 .141.2 .1167.4 .172572 22.46 .1026 7.43062404 .003.99 L .44 .156 1221.2 .141.2 .1167.4 .172572 22.46 .1026 7.43062404 .003.99 ARC .156 .0164 .921.7 .3524.5 .374522 .1327.337 .423 .55.76 .1103 .3.32045404 .0103.99 ARC .156 .0164 .921.7 .3545.5 .174522 .3372 .55.76 .1103 .3.32045404 .919.99 ARC .156 .0164 .921.7 .3545.5 .174522 .3372 .55.76 .1103 .3.32045404 .919.99 ARC .156 .0164 .921.7 .3545.5 .374522 .1223.387 .42.30 .1108 .3.32045404 .919.99 ARC .156 .921.7 .1110.2 .1.2433 .991.015 .55.47 .1103 .8.32045404 .974.495 ARC .177 .8.65.7 .1110.2 .1.2433 .991.015 .55.47 .1103 .8.35045404 .974.990 ARC .176 .864.7 .1110.2 .1.2433 .991.015 .55.47 .1103 .8.35045404 .974.192.993 ARC .177 .8.55.7 .1110.2 .912.7 .955.7 .927 .73.65 .1204 .9.299.1127 .70.14 .1209 .932.291.993 ARC .176 .864.7 .110.2 .913.977.7 .73.65 .1204 .9.299.274.137 ARC .176 .844.7 .997.9 .572.8 .73.974.55 .4120 .9.3512.40 .274.290 ARC .176 .844.7 .997.9 .572.8 .73.974.55 .4120 .9.3512.40 .274.290 ARC .176 .844.7 .572.8 .739.455 .500.77.7 .73.65 .1204 .9.2532.40 .274.290 ARC .176 .844.7 .572.8 .739.455 .500.775 .72.6 .1204 .9.2552.40 .334.173 ARC .176 .844.7 .572.8 .739.455 .500.775 .72.6 .1204 .9.2552.40	Ļ	.136	1179.5	331.5	.28133	391.024	5.49		5.4157E+04	248.914
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	L	.138	1188.5	351.J	.30375	429.086	6.31	.0733	5.63112+04	286.119
L .144 1212.4 44.3 $+34.3$.36099 223.586 8.20 .0790 6.0711444 371.807 L .144 1212.4 452.3 39655 581.435 9.10 0242 6.23514.24 421.356 L+V .146 1217.4 572.3 $+3755$ 647.456 10.53 0049 6.52142.44 477.599 L+V .146 1223.5 554.6 $+64.355$ 647.456 10.53 0049 6.52142.44 477.599 L+V .150 1223.5 554.6 $+64.355$ 611.266 13.43 0090 6.97925.04 609.104 L+V .150 1223.5 554.6 $+54.355$ 611.266 13.43 0090 6.97925.04 609.104 L+V .155 1223.4 197.6 $+72.6$.7125 013.5 15.17 0919 7.20355.04 609.105 L+V .156 1224.1 972.6 .7126 1060.404 17.16 0969 7.4005.04 78.495 L+V .156 121.2 1.16.1 197.6 7.67.9 1292.098 19.47 0.9969 7.4005.04 78.495 L+V .156 121.2 1.16.1 1.16.74 1712.572 22.46 1026 7.89665.04 1019.906 L+V .156 121.2 1.16.1 1.16.74 1712.572 22.46 1026 7.89665.04 1019.906 L+V .156 1128.7 255.4 2.404.7 1397.967 24.98 11627 5.1083 5.32045.04 128.998 APC .166 197.6 197.6 19.62.3 9.62222 11225.367 42.30 1083 5.32045.04 1918.993 APC .166 916.6 19.16.7 1952.3 9.62222 1122.367 42.30 1083 5.32045.04 2523.312 APC .166 916.6 19.16.7 1952.3 3.9.6222 1122.367 42.30 1083 5.32045.04 2523.312 APC .166 916.6 19.16.7 1162.4 2.0077.6 1067.602 60.47 1112 8.6075.00 2724.990 APC .166 916.6 19.16.7 1.162.7 1.163 8.6773.02 252.312 APC .166 916.6 19.16.8 2.0137.4 1687.602 60.47 1112 8.6733.460 2.274.290 APC .166 916.6 19.16.4 312.413 13.64.9 1.4625 837.664 57.30 1116 8.47355.04 2272.312 APC .170 887.9 9.31.4 1.1655 837.664 57.30 1165 9.0994.04 3122.497 APC .177 887.9 9.31.4 1.1625 837.664 57.30 1165 9.0994.04 3122.497 APC .176 886.6 713.1 3.64.9 1.46256 837.664 57.30 1165 9.0994.04 3122.497 APC .176 887.9 9.31.4 1.1625 837.664 57.30 1165 9.0994.04 3122.497 APC .176 886.6 713.1 3.7455 584.763 72.5 3.1224.594 3123.245 APC .176 886.6 713.1 4.124.695 5.47 1.137 8.6505.044 3122.477 APC .176 886.6 713.1 4.124.695 5.47 1.126 9.5055.04 1342.177 APC .126 9.5055.04 1342.177 APC .126 9.5055.04 1342.177 APC .126 9.5055.04 1342.177 APC .126 9.6356.04 3122.177 APC .126 9.6356.04 3122.177 APC .126 9.5055.04 363.9 715.5 12.427 APC .126 9	<u> </u>	.149	1195.8		<u>32784</u>	469,605	7.21		5.8495.+64	326.843
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	L	• 142	1204.3	434.9	.36039	523.558	8.20	.3790	6.3711E+04	371.807
L + V . 1447 122+. 346.3	1	.144	1212.4	440.2	.39927	281,430	9.30		<u>6.2951E+84</u>	421. 920
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	L+V	• 145	1215.4	2 52 . 3	+43755	647.456	10.53	.0849	E.5214E+J4	477.599
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	L+V	.145	1223.8	2224	.48639		11.90		<u> </u>	539.625
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		• 15 0	1223.3	504.0	+ 74 3 J 9	612.200	13.43	•0909	5.9/92244	009.103
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $			1222.4	<u> </u>	<u>= 52452</u>	931+332			7.20925704	
L ** . 176 12212 1937		4174	1224+1	3(263	+ 1295 867 0	1000.404	1/.10	• U 70 7	7.44002704	770+493 ##2 450
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		120	4214 2	1.14	1 16764	4743 573	22 / 8	1020	7 99695484	1010 004
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		150	1211+2	2928 /	2	1707 067	26.00	+1420	8 44 008 ASH	1334 980
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	APC	. 162	1069.1	10512.3	<u>€</u> †* <u>9</u> **/. 9. 82322	11228.387	<u> </u>		A. 32045+04	1919.193
ARC 165 916.6 1941.3 2.01374 1667.802 0.047 1123 8.60676+04 2742.990 ARC .168 901.3 1346.0 1.45343 1213.080 63.29 .1137 8.73345+04 2671.137 ARC .170 692.7 1110.2 1.24353 991.018 65.47 .1153 8.6505+04 2970.067 ARC .172 087.9 9.3.4 1.62556 037.564 67.30 .1159 8.7365+04 3052.847 ARC .174 866.1 709.2 .91313 717.071 68.84 .1169 9.1994E+04 3122.913 ARC .174 866.1 713.3 .61416 532.177 70.16 8.84 .1165 9.3237.954 XT .180 .614.4 .534.1 .71576 558.743 .72.53 .1232 9.4528E+04 3237.954 XT .180 .644.4 .534.1 .71576 558.743 .72.53 .1232 9.6532E+04 334.173 XT .180 .644.3 .623.9 .67939 .547.677 <td>APC</td> <td>. 164</td> <td>951.7</td> <td>3364.5</td> <td>1.7652H</td> <td>3392.382</td> <td>55.76</td> <td>.1103</td> <td>8.67355404</td> <td>2529.332</td>	APC	. 164	951.7	3364.5	1.7652H	3392.382	55.76	.1103	8.67355404	2529.332
ARC.1649(1.3 $13+6+3$ 10+63431213.08053.29.1137 3.7334 ± 04 2677.137ARC.170.992.7.1110.21.24363.991.015.65.47.11538.8569E+04.2970.067ARC.172.087.9.93.41.06256.037.564.67.30.11698.37.862+04.3052.847ARC.174.086.6.109.2.91313.717.071.68.84.11859.0994E+04.3122.913ARC.176.086.6.13.3.86416.032.177.70.16.12009.2201E+04.3123.738ARC.176.084.7.53.9.73576.568.743.72.53.12132.9462E+04.3237.954EXT.187.097.5.610.3.71576.568.743.72.55.12489.5853E+04.3341.173EXT.186.97.5.610.3.67979.57.927.73.65.12489.5853E+04.3341.173EXT.186.97.5.610.3.67979.57.927.73.65.1246.9.35652+04.3341.173EXT.186.90.2.572.4.66292.57.966.74.54.1264.9.35652+04.3341.173EXT.186.91.4.344.6.1467.1467.1264.9.35652+04.3341.173EXT.188.91.4.54635.528.589.76.91.1264.9.356544.3488.950EXT.190.90.5.2.572.4.63028.519.668.77.96.1313.10046	APC	. 166	916.6	1941.3	2.00976	1687.802	68.47	.1120	A. 6067E+04	2742.990
ARC.17C $e92.7$ 1110.21.24363991.01565.47.11538.85692.042970.067ARC.172887.9 943.4 1.05256 837.664 67.30 .1169 $8.37862.04$ 3052.847 ARC.174884.1909.2.91313717.07168.84.11859.0994E404 3122.913 ARC.176886.6713.1.81416 $b32.177$ 71.18.1201 $9.2201E404$ 3123.738 EXT.176884.7652.8.73454580.18071.38.1216 $9.3411E404$ 3237.954 EXT.182 894.3 633.9 .7959557.92773.65.1248 $9.5853E404$ 3341.173 EXT.182 894.3 623.9 .59799 547.677 74.76 .1264 $9.5853E404$ 3391.323 EXT.186903.8 597.2 .66292 537.946 75.84.1230 $9.8328E404$ 3440.567 EXT.186901.8 597.2 .66292 537.946 75.84.1230 $9.8328E404$ 3440.567 EXT.190905.2.72.4.663028519.86877.96.13131.0084E405 3569.513 EXT.192.912.2.561.7.61467.511.445.78.93.13291.8211E405 356.513 EXT.192.92.2.560.7.511.445.54.68.1313.0084E405 $356.93.28$ EXT.192.92.2.560.7.61467.511.445 <td< td=""><td>ARC</td><td>.168</td><td>961.3</td><td>13-6-3</td><td>1.49343</td><td>1213.080</td><td>63.29</td><td>.1137</td><td>8.73345+04</td><td>2871.137</td></td<>	ARC	.168	961.3	13-6-3	1.49343	1213.080	63.29	.1137	8.73345+04	2871.137
ARC.172 $0 87,9$ $9 + 3, 4$ 1, 1256 $0 37, 564$ $67, 30$.1169 $8, 37662+04$ $3052, 847$ ARC.174 886.6 713.1.81416 $0 32, 177$ 70.18.1169 $9, 0994E+04$ $3122, 913$ ARC.176 886.6 713.1.81416 $0 32, 177$ 70.18.1200 $9, 2201E+04$ $3122, 913$ ARC.176 886.6 713.1.81416 $0 32, 177$ 70.18.1200 $9, 2201E+04$ $3133, 738$ $2XT$.180 691.4 538.0 .71576 560.743 72.53.1232 $9.4628E+04$ 3290.068 $2XT$.182 694.3 623.9 .71576 560.743 72.53.1248 $9.5053E+04$ 334.173 $2XT$.186 902.8 .623.9.69759 557.927 73.65.1248 $9.5053E+04$ 334.173 $2XT$.186902.8.977.2.6292.577.946.1260 $9.8328E+04$ 3440.567 $2XT$.186902.8.597.2.6292.577.946.1260 $9.8328E+04$ 3440.567 $2XT$.188914.4.534.6.64635.528.68976.91.1296 $9.9579E+04$ 3480.950 $2XT$.190905.7.2.572.4.63028519.86877.96.13131.0084E+05 3356.513 $2XT$.192.1216.916.3.549.3.5495?.503.389 80.311 .13461.0340E+05 3629.328 $2XT$.194	ARC	170	892.7	1110.2	1.24363	991.018	65.47	.1153	8.8569F+04	2970.067
ARC.174886.1109.2.91313717.07168.84.11859.0994E+043122.913ARC.176886.6713.1.8E416 $a32.177$ 70.18.12009.2201E+043143.738 $\pm XT$.178888.7652.8.73454580.18071.38.12169.3411E+043237.954 $\pm XT$.180691.4.638.0.71576568.74372.53.12329.4628E+043341.173 $\pm XT$.182.694.3.613.9.71576.557.92773.65.12489.5853E+043341.173 $\pm XT$.182.694.3.613.9.67939.547.677.74.76.12649.708628E+043340.567 $\pm XT$.186.901.8.547.2.66292.537.946.75.24.12309.8328E+043440.567 $\pm XT$.186.901.4.344.6.14636.1236.9.9575F±04.3440.567 $\pm XT$.186.901.4.344.6.14636.1236.9.9575F±04.3440.567 $\pm XT$.186.901.4.344.6.14636.1236.9.9575F±04.3533.294 $\pm XT$.186.901.4.344.6.1467.11.445.78.39.1329.1.296.9.9575F±04 $\pm XT$.192.912.2.560.7.61467.511.445.78.39.1.329.1.329.1.326.3533.294 $\pm XT$.194.916.3.549.3.5957.503.389.80.01.1.363.0.602±05.3629.328 <tr< td=""><td>ARC</td><td>.172</td><td>887.9</td><td>943.4</td><td>1.06256</td><td>837.664</td><td>67.30</td><td>.1169</td><td>8.97862+04</td><td>3052.847</td></tr<>	ARC	.172	887.9	943.4	1.06256	837.664	67.30	.1169	8.97862+04	3052.847
ARC.176886.6713.1.81416 632.177 70.18.12009.2201E+043183.738 $\pm XT$.178.178.189.178.12169.3411E+043237.954 $\pm XT$.189.091.4.538.0.71576.558.743.72.53.12329.4628E+043290.068 $\pm XT$.182.094.3.623.9.6759.557.927.73.65.12489.5853E+043341.173 $\pm XT$.184.097.5.610.3.67939.547.677.74.76.1264.1264.12009.6328E+043341.173 $\pm XT$.186.001.3.67939.547.677.74.76.1264.12609.6328E+043340.521 $\pm XT$.186.002.8.546.252.57.946.12609.6328E+043340.561 $\pm XT$.186.002.8.546.35.528.689.76.91.12969.6328E+043440.561 $\pm XT$.190.909.2.72.4.63028.519.868.77.96.13131.0084E+053536.513 $\pm XT$.192.912.2.560.7.61467.511.445.78.39.13291.6211E+053583.294 $\pm XT$.194.916.3.549.3.5952.503.389.80.01.1363.0469E+053629.328 $\pm XT$.196.920.7.538.4.54475.495.671.81.00.1363.0469E+053749.279 $\pm XT$.196.920.7.538.4.54475.495.671.81.00.1360.0600E	ARC	.174	886.1	909.2	.91319	717.071	68.84	.1185	9.0994E+04	3122.913
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	ARC	.176	886.6	713.3	.80416	632.177	70.18	.1200	9.2201E+04	3183.738
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	EXT	.178	888.7	652.8	.73454	584.180	71.38	.1216	9.3411E+04	3237.954
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	EXT	.180	891.4	538.0	.71576	568.743	72.53	.1232	9.4628E+04	3290.068
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	EXT	.182	894.3	623.9	. F9759	557.927	73.65	.1248	9.5853E+04	3341.173
FXT .186 903.8 547.2 .66292 537.946 75.84 .1280 9.8328E+04 3440.567 EXT .188 964.4 534.6 .64635 528.589 76.91 .1296 9.9579E+04 3488.950 SXT .190 969.2 572.4 .663028 519.868 77.96 .1313 1.0084E+05 3536.513 SXT .192 912.2 560.7 .61467 511.445 78.99 .1329 1.8211E+05 3583.294 SXT .194 916.3 549.3 .59952 503.389 80.01 .1346 1.0340E+05 3629.328 SXT .196 920.7 538.4 .54475 495.671 81.00 .1363 1.0469E+05 3679.328 SXT .196 920.7 538.4 .54475 495.671 81.00 .1363 1.0469E+05 3679.328 SXT .196 920.7 538.4 .54475 495.671 81.00 .1360 1.060E+05 3779.279 SXT .196 925.2 .527.7 .70.43 488.264	EXT	.184	897.5	610.3	. €7939	547.077	74.76	.1264	9.70862+04	3391.323
EXT .188 9£4.4 34.6 .54635 528.589 76.91 .1296 9.9579E+04 3488.950 5xt .190 96.9.2 572.4 .63028 519.868 77.96 .1313 1.0004E+05 3536.513 5xt .192 912.2 .561.7 .61457 .511.645 78.39 .1329 1.021E+05 3583.294 5xt .194 916.3 .549.3 .599.2 .503.389 80.01 .1346 1.0340E+05 3629.328 5xt .196 920.7 .538.4 .5247.5 .495.671 .61.00 .1363 .0469E+05 3679.646 5xt .196 920.7 .538.4 .5247.5 .495.671 .61.00 .1363 .0469E+05 3679.366 5xt .196 .17.7 .570.43 .488.264 .61.99 .1380 1.060E+05 .3719.279 5xt .200 .22.95 .1397 .0732E+05 .3763.252 .3763.252	Ēxt	•18E	903.8	547.2	.66292	537.946	75.84	.1280	9.8328E+04	3440.567
5xt .190 909.2 572.4 .63028 519.868 77.96 .1313 1.0084E+05 3536.513 5xt .192 912.2 560.7 .61467 511.445 78.99 .1329 1.8211E+05 3583.294 5xt .194 916.3 549.3 .5952 503.389 80.01 .1346 1.0340E+05 3629.328 5xt .196 920.7 538.4 .54475 495.671 81.00 .1363 1.0469E+05 3674.646 5xt .198 925.2 .527.7 .570.43 488.264 81.99 .1380 1.0600E+05 3719.279 5xt .200 923.9 .517.4 .5544 481.142 82.96 .1397 1.0732E+05 3763.252	EXT	.188	964.4	534.6	.64636	528.689	76.91	.1296	9.9579E+04	3488.950
EXT .192 912.2 560.7 .61467 511.445 78.99 .1329 1.0211E+05 3583.294 EXT .194 916.3 549.3 .59952 503.389 80.01 .1346 1.0340E+05 3629.328 EXT .196 920.7 538.4 .56472 495.671 81.00 .1363 1.0469E+05 3674.646 EXT .198 925.2 .27.7 .570.43 488.264 81.99 .1380 1.0600E+05 3719.279 EXT .200 923.9 .517.4 .556.44 481.142 82.96 .1397 1.0732E+05 3763.255	EXT	.190	909.2	572.4	.63028	519.868	77.96	.1313	1.00842+05	3536.513
EXT .194 916.3 549.3 .59952 503.389 80.01 .1346 1.0340E+05 3629.328 EXT .196 920.7 538.4 .58475 495.671 81.00 .1363 1.0469E+05 3674.646 EXT .198 925.2 527.7 .57043 488.264 81.99 .1380 1.0600E+05 3719.279 EXT .200 923.9 .517.4 .556.44 481.142 82.96 .1397 1.0732E+05 3763.252	EXT	.192	912.2	560.7	. 61467	511,445	78.39	.1329	1.8211E+05	3583.294
Image: State stat	EXT	.194	916.3	549.3	• F9953	503.389	80.01	.1346	1.0340E+05	3629.328
EXT 198 925.2 527.7 57043 488.264 81.99 1380 1.0600E+05 3719.279 EXT 220 923.9 517.4 55644 481.142 82.96 1397 1.0732E+05 3763.252	EXT	.196	920.7	536.4		495.671	81.00	.1363	1.04696+45	3674.646
<u></u>	EXT	.198	925.2	52 7. 7	. = 7043	488.264	81.99	.1380	1.0600E+05	3719.279
	<u> </u>	.220	923,9	517.5	155644	481.142	82.95	.1397	1.0732E+05	3763.252

	TIME	CUPRENT	VOLTS	OHMS	POWER	ENERGY	ACTION	GOENS	EDENS
	MICROSEC	AMPS			KILCWATTS	MILLIJ	AMP2 SEC	AMP2 SEC/MH4	J/GM
EVT	202	07/ 7	=	.51283	474.284	83.01	- 1415	1. 18662+05	3805-532
2 1 1	• 2 4 2	93467	· · · · · · · · · · · · · · · · · · ·	52064	447 670	94 35	1632	1 10015405	3859.321
<u>- EXI</u>	• 294	939.7	457.1	54672	407 607 0		1450	4 44 275+05	7031 /63
2.21	.236	944.6	450.2	+10/2	401+201	05.70	+1470 4060	1 4 275 405	3031+400
<u> </u>	• 298	953.1	479.0		455.100		•1400	1.12/3.403	3933.029
EXT	• 210	955.5	4/3+6	• 4 9 1 9 1	449.116	87.63	•1466	1.14152+05	39/4.445
EXT	.212	961.0	461.3	.47998	443.299	89.50	.1504	1.15562+05	4314.527
EXT	.214	966.7	452.7	•46834	437.653	89.38	•1523	1.1698£+35	. 4054.489
EXT	•216	972.5	in to be a to	.45638	432,159	90.25	.1542	1.18432+05	4093.346
EXT	.218	978.3	436.3	. 44591	426.836	91.11	.1561	1.19892+05	· 4132.91J
EXT	. 220	984.3	428.3	• 43511	421.585	91.95	.1580	1.21372+05	4171.395
EXT	.222	990.4	423.5	.42456	416.486	92.79	.1630	1.2287E+05	4209.412
EXT	.224	996.6	412.9	. 41427	411.439	93.62	,1619	1.24382+05	4246.972
EXT	.226	1002.9	+05.4	.46423	406.619	94.44	.1639	1.25922+05	4284. 384
EXT	.229	1009.3	395.1	. 39443	401.935	95.25	.1000	1.2747E+05	4320.758
TX2	.230	1015.3	391.0	.38456	397.143	96.15	.1680	1.29052+05	4357.001
EXT	.232	1022.4	383.9	.37551	392.536	96.84	.1701	1.30642+05	4392.82+
EXT	.234	1029.1	377.0	.36639	388.038	97.62	.1722	1.32262+05	4428.231
EXT	.236	1635.8	370.3	.35749	393.554	98.39	.1743	1.33902+05	4463.232
EXT	.238	1042.c	363.7	.34879	379.158	99.15	.1765	1,35562+03	4497.331
EXT	.240	1049.5	357.2	. 34030	37 + . 8 + 7	99.90	.1787	1.3724E+05	4532.335
EXT	.24?	1056.5	353.8	.332)]	370.587	130.65	.1809	1.38942+05	4565.850
EXT	.244	1053.6	3+4.5	.32390	365.393	101.39	.1831	1.40672+35	4599.282
EXT	.246	1070.7	338.3	.31633	362.233	162.12	.1854	1.42422+05	4632.334
= x T	.248	1077.8	332.3	.30827	359.132	1.2.84	.1877	1.44195+05	4665.012
EXT	.250	1087.1	326.3	.3(373	354.379	103.55	.1901	1.45992+05	4697.320
EXT	.252	1092.4	320.5	.29337	352.370	104.25	.1924	1.+7812+05	4729.262

+

î

r



Distribution:

Los Alamos Scientific Laboratory P.O. Box 1663 Los Alamos, New Mexico 87544 Attn: R. L. Spaulding, GMX-7 W. A. Meyers, GMX-7 University of California Lawrence Laboratory P.O. Box 808 Livermore, California Attn: J. R. Stroud R. C. Weingart 1132 A. B. Church 1535 J. G. Harlan 1540 T. B. Lane 1641 W. J. Halpin 1652 S. D. Spray 2300 L. D. Smith 2310 C. B. McCampbell 2314 J. J. Marron 2315 J. E. Gover 2316 H. M. Barnett 2330 J. P. Shoup 2400 R. S. Claassen 2440 O. M. Stuetzer 2510 D. H. Anderson 2513 D. B. Hayes 2515 E. A. Kjeldgaard 2516 N. E. Brown 5000 A. Narath 5100 J. K. Galt 5110 F. L. Vook 5120 G. J. Simmons 5130 G. A. Samara 5131 L. W. Davison 5131 T. J. Tucker (20) 5131 R. P. Toth 5132 P. M. Richards 5150 J. E. Schirber Attn: R. T. Johnson - 5155 5160 W. Herrmann Attn: B. M. Butcher - 5167 5200 E. H. Beckner Attn: F. Biggs - 5223 5600 A. Y. Pope 5700 J. H. Scott 5718 M. M. Newsom 5800 L. M. Berry Attn: R. L. Schwoebel - 5820 R. W. Rohde - 5832 R. C. Heckman - 5842

8150	D. E. Gregson
5166	J. S. Anderson
8185	C. M. Potthoff
8330	G. W. Anderson
8340	J. L. Wirth
8416	J. A. Mogford
9320	M. Cowan
9350	F. W. Neilson
8266	Library (2)
3151	W. F. Carstens (3)
	for AEC/TIC (Public Release)
3141	Central Tech. Files (5)