

Effect of arc voltage, welding current and welding speed on fatigue life, impact energy and bead penetration of AA6061 joints produced by robotic MIG welding

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Abstract

Aluminum alloys forming to AA6061 have a wide range of desirable properties which are used in different industries such as aircraft industry and other aerospace structures. The effect of process parameters on fatigue life and impact energy of weld metal, and bead penetration in AA6061 joints produced by MIG robotic welding was studied in this paper. Different samples were produced by employing arc voltage of 20, 23, and 26 V, welding current of 110, 130, and 150 A, and welding speed of 50, 60, and 70 cm/min. After welding operations, the mechanical properties of the weld metal were evaluated by fatigue and impact testing at room temperature, and bead penetration was measured for geometrical specimens. Results were clearly illustrated when heat input increases, fatigue life of weld metal decreases whereas impact energy of weld metal increases in first and then drops significantly. A linear increase in bead penetration was observed with increasing welding current and arc voltage. The largest penetration in this study was observed for 60 cm/min welding speed.

Keywords: MIG parameters; fatigue life; impact energy; bead penetration, welding.

1. Introduction

Aluminum and its alloys are used extensively in aerospace and automotive industries because of its low density and high strength to weight ratio (Bakes & Benjamin, 1979). Heat treatable wrought aluminum–magnesium–silicon alloys conforming to AA6061 are of moderate strength and possess excellent welding characteristics over the high strength aluminum alloys (Thomas, 1991). Hence, alloys of this class are extensively employed in marine frames, pipelines, storage tanks and aircraft applications (Dawes, 1995). Fusion welding processes are widely used for fabrications in many engineering applications such as aerospace, automotive, shipbuilding industries (Gourd, 1995; Puchaicela, 1998). These welding processes are routinely used for joining structural aluminum alloys (Elangovan *et al.*, 2009). A Metal Inert Gas (MIG) welding process consists of heating, melting and solidification of parent metals and a filler material in localized fusion zone by a transient heat source to form a joint between the parent metals (Gourd, 1995; Puchaicela, 1998). MIG welding parameters are the most important factors affecting the quality, productivity and cost of welding joint (Kim *et al.*, 2003; Ming *et al.*, 2003).

The present paper aims at the evaluation of fatigue life, impact energy and bead penetration of AA6061 plates obtained by employing different MIG parameters. Extensive studies have been made on fatigue and impact behavior of welded joints. For example, Cavaliere *et al.* (2006) researched on the effect of process parameters on fatigue behavior of AA6056 joints produced by friction stir welding. Also, Cavaliere *et al.* (2008) studied on the effect of friction stir welding parameters on

fatigue properties of AA6082 joints. Large numbers of fatigue testing results of welded joints after ultrasonic peening treatment (UPT) were analyzed by Wang Ting *et al.* (2009). Lee *et al.* (2009) studied on effect of the weld geometry on the fatigue life of non-load-carrying fillet welded cruciform joints. Kolhe & Datta (2007) investigated and correlated the relationship between the various parameters of SA welding and impact energy of single “V” butt joint of mild steel plate. Effect of controlled atmosphere on impact energy of MIG-MAG weldments was described by Kacar & Kökemli (2005). Investigation into the relationship between the welding parameters and bead geometry began in the mid-1900s and regression analysis was applied to welding geometry research by Lee *et al.* (2000) and Raveendra & Parmar (1987). The effect of process parameters on weld penetration in gas metal arc welding processes was studied by Karadeniz *et al.* (2007). However, there exists still little information regarding to the welding researches on fatigue and impact behavior, and bead penetration in AA6061 aluminum alloy welding joints, especially in MIG welding process.

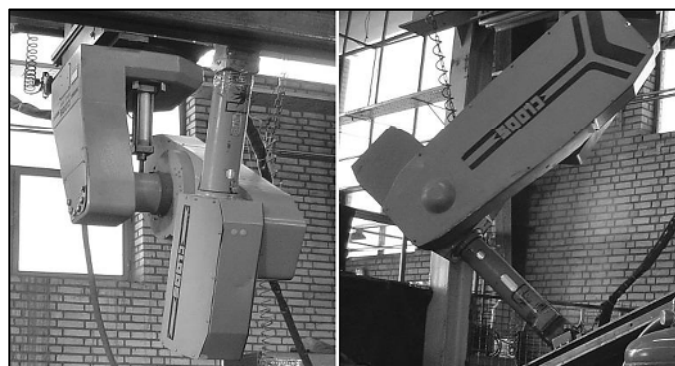
2. Materials and methods

Due to high importance, welding joints were produced from AA6061 aluminum alloy. The ER5356 (AWS A5.10) wire electrode with 1 mm diameter was used as filler metal. In the present study, the consumable wire electrode was selected based on properties and characteristics of the base material, weld dimensions, and existing wire electrode inventory. The chemical composition of filler metal is given in Table 1.

Table 1. Chemical composition of filler metal (ER5356).

Element	Mg	Mn	Si	Fe
Wt. (%)	5.00	0.13	0.25	0.40
Al	Cr	Ti	Zn	Cu
Balance	0.13	0.13	0.10	0.10

100 % argon was used as shielding gas in welding operations. The base materials were supplied in form of plates with ~ 2.35 mm and 10 mm thickness for experimental tests. The plates were cut into coupons with a 30° bevel of each plate to provide 60° groove angle for single-V-groove butt joint configuration. In order to minimize the welding distortion, the plates were located in the fixture jig before welding operations. For each test condition, the seven welding passes were used to join the base metals, and the parameters in welding seven passes in each test condition were same. The MIG welding operations in this study were performed by means of a SOS Model DR Series ARK ROBO 1500 welding robot with a working capacity of 0-600A and 0-50V ranges. The welding robot and its apparatus are shown in Fig. 1.

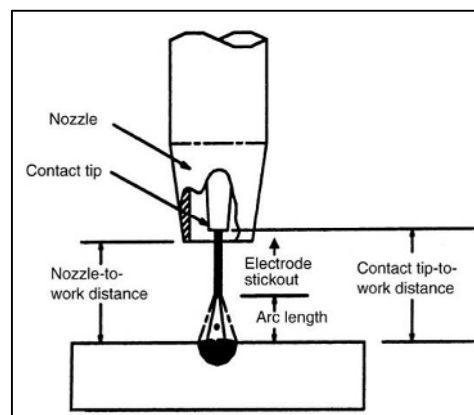
Fig.1. The welding robot and its apparatus used in this study.

The welding characteristics of MIG process were set up according to parameters given in Table 2, and are shown in Fig. 2. The other parameters were fixed.

Table 2. Welding parameters applied in this study.

Cylinder Pressure (bar)	145
Cylinder Outlet Pressure (l/min)	14
Nozzle Opening (mm)	10
Electrode Stick Out (mm)	19.2
Arc Length (mm)	3
Nozzle-to-Work Distance (mm)	20.2
Contact Tip-to-Work Distance (mm)	22.2
Arc Voltage (V)	20, 23, 26
Welding Current (A)	110, 130, 150

Welding Speed (cm/min)	50, 60, 70
Wire Feeding Rate (m/min)	8
Torch Angle (degree)	5
Droplet Transfer	Spray Transfer Mode
Polarity	DCEP

Fig.2. MIG welding parameters (Palani & Murugan, 2006).

The 27 welding conditions with different arc voltage, welding current and welding speed combinations in this study are shown in Table 3. Having finished the welding process, fatigue and impact testing were carried out at room temperature in order to evaluate the fatigue life and impact energy of the weld metals produced in different welding conditions. Fatigue testing on weld metals was performed by using the ZWICK test machine under constant loading control up to 250 Hz sinus wave loading. The low cycle and high cycle fatigue tests were conducted in the axial total stress-amplitude control mode with a stress ratio ($R = \sigma_{Min}/\sigma_{Max}$) equal to 0.1, for all arc voltages, welding currents and welding speeds used in the present study. Fatigue testing specimens of 5 mm middle diameter and 21.27 mm gauge length according to DIN 50113 guidelines were extracted from the welded joints. The fatigue specimens were tested at the 180 MPa stress range only with stress ratio of 0.1 in order to study the effect of the MIG parameters on fatigue life of the weld metals. Impact testing was performed to measure the impact energy of the weld metals. The Standard Charpy V-notch (CVN) specimens were extracted from welded joints according to ASTM E23 standard. It is shown in Fig. 3. The standard impact specimens were 55×10×10 mm³. A standard Charpy V-notch specimen includes a 45° V notch with 2 mm depth, and 0.25 mm root radius. The notch was located in center of impact specimen, and also weld metal. The Dynatup KGH impact tester was used to perform the impact testing. Dynatup is a drop weight impact test tower. Impact testing was carried out with an impact velocity of ~ 5 m/s, and using a tup capacity equal to ~ 44 kN. In order to study the effect of MIG process parameters on bead penetration, the specimens were cut perpendicular to weld line by using a power hacksaw.

Then the cross-sections surfaces were machined, removed from each impurity, polished, and etched using 2% nital for measuring bead penetration. A schematic illustration of bead penetration in welding applications is shown in Fig. 4.

Table 3. The different welding conditions used in this study.

Sample Number	Welding Current (A)	Arc Voltage (V)	Welding Speed (cm/min)
1	110	20	50
2			60
3			70
4		23	50
5			60
6			70
7		26	50
8			60
9			70
10	130	20	50
11			60
12			70
13		23	50
14			60
15			70
16		26	50
17			60
18			70
19	150	20	50
20			60
21			70
22		23	50
23			60
24			70
25		26	50
26			60
27			70

Fig.3. Preparation of fatigue and impact specimens from welding joints

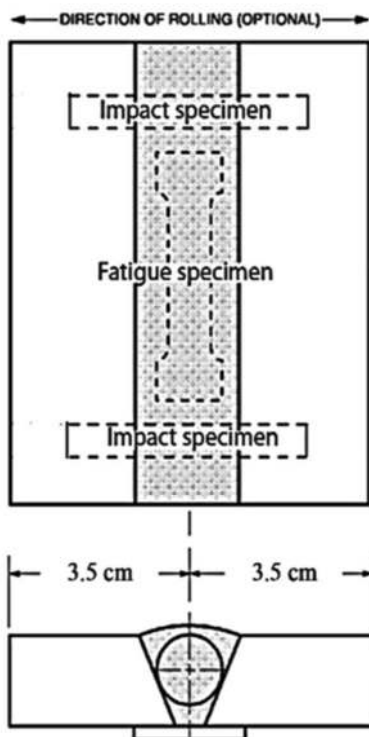
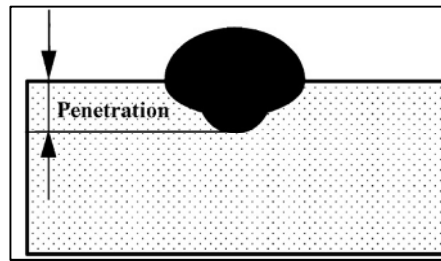


Fig.4. A schematic illustration of bead penetration (Kim et al., 2003)



3. Results and discussion

The 27 welding operations with different welding current, arc voltage and welding speed combinations were performed. The results of this study as a function of the welding parameters are summarized in Table 4.

Table 4. The welding heat input, weld metal mechanical properties, bead penetration for different welding conditions.

Sample Number	Heat Input (J/mm)	Cycles to Failure (Cycles)	Impact Energy (J)	Bead Penetration (mm)
1	264.00	221	83.91	2.411
2	219.96	360	67.37	2.464
3	188.58	476	47.71	2.310
4	303.60	198	91.27	2.571
5	252.96	331	73.75	2.612
6	216.84	463	55.00	2.511
7	343.20	161	91.25	2.599
8	285.96	317	83.93	2.634
9	245.10	429	71.60	2.541
10	312.00	190	94.18	2.781
11	259.98	325	83.01	2.872
12	222.84	439	67.63	2.741
13	358.80	157	81.41	2.860
14	298.98	296	90.55	2.932
15	256.26	408	77.21	2.802
16	405.60	101	63.25	2.941
17	337.98	264	94.32	2.970
18	289.68	372	84.62	2.872
19	360.00	136	77.84	2.983
20	300.00	272	91.01	3.020
21	257.10	390	78.68	2.911
22	414.00	98	61.17	3.078
23	345.00	258	85.65	3.101
24	295.68	366	88.61	3.001
25	468.00	85	58.64	3.150
26	390.00	246	71.91	3.202
27	334.26	353	93.65	3.120

3.1 Effect of welding parameters on fatigue life

The correlations between the welding parameters and fatigue life are shown in Figs. 5-7. From the results, increasing arc voltage from 20 to 26 V, and welding current from 110 to 150 A decreased the fatigue life of weld metal but fatigue life gradually increased with increasing welding speed from 50 to 70 cm/min. In Figs. 5-7, the welding speed was fixed on 50, 60 and 70 cm/min and the maximum values for fatigue life were obtained as 221, 360 and 476 cycles, respectively. The maximum values of fatigue life were obtained in $I=110$ A and $V=20$ V conditions. The changes in fatigue life of weld metal can be due to the microstructural changes in weld zone. According to the following function, the change in welding parameters results in the variation in welding heat input (Funderburk, 1999):

$$H = (60EI)/(1000S) \quad (1)$$

H = Heat Input (kJ/mm)

E = Arc Voltage (V)

I = Welding Current (A)

S = Welding Speed (mm/min)

Fig.5. Fatigue life vs. welding current diagram for 50 cm/min constant welding speed

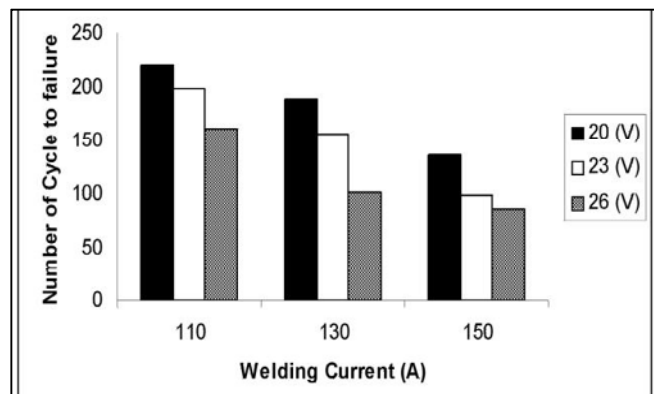


Fig.6. Fatigue life vs. welding current diagram for 60 cm/min constant welding speed

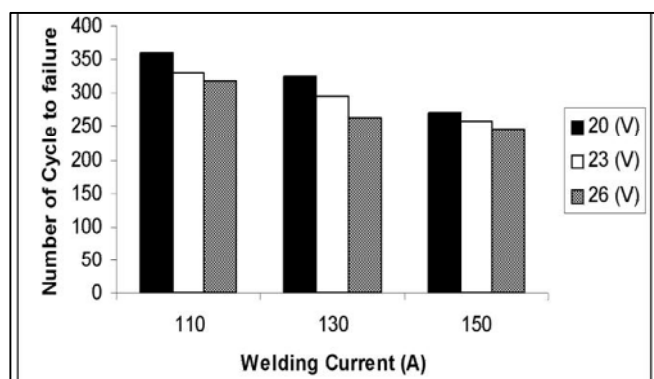
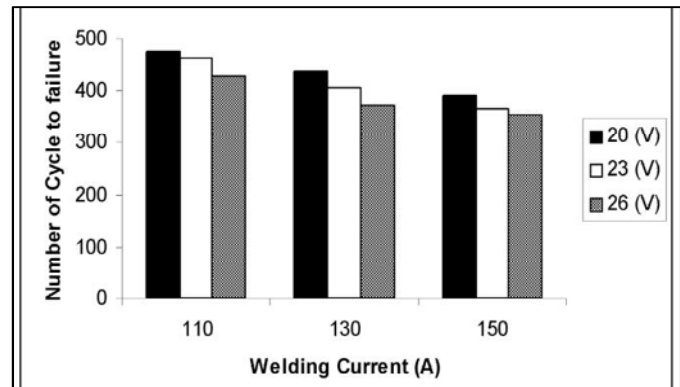


Fig.7. Fatigue life vs. welding current diagram for 70 cm/min constant welding speed



Varying in heat input typically affect the microstructure and mechanical properties of weld. The amount of heat input influences on cooling rate of the weld. The following proportionality function shows the relationship between preheat temperature, heat input and cooling rate of weld. Welding heat input and preheat temperature interact with others such as material thickness, specific heat, density and thermal conductivity to influence the cooling rate (Funderburk, 1999).

$$R \propto 1/(T_0 . H) \quad (2)$$

R = Cooling Rate ($^{\circ}$ C/sec)

T_0 = Preheat Temperature ($^{\circ}$ C)

H = Heat Input (kJ/mm)

The cooling rate is a primary factor that determines the final microstructure and mechanical properties of the weld metal. When the heat input increases, the cooling rate decreases for a given weld metal (Funderburk, 1999) and increases the coarsening of the microstructure of weld. It is shown in Fig. 8.

3.2 Effect of welding parameters on impact energy

As shown on Table 4, as heat input increased from 188.58 to 337.98 J/mm, the impact energy of weld metal increased from 47.71 to 94.32 J. But with further increasing heat input from 337.98 to 468 J/mm, impact energy of the weld metal dropped significantly (Fig. 9). It seems that the changes in impact energy of the weld metal is not just tied to the heat input; it is also significantly influenced by the weld bead size. For example, the following function shows approximately relationship between heat input and fillet weld leg size (Miller & Funderburk, 1998):

$$W = (H/500)^{1/2} \quad (3)$$

W = Fillet Weld Leg Size (in)

H = Heat Input (kJ/in)

As the weld bead size increases, which is corresponds to a higher heat input, the impact energy tends to decrease. In multiple-pass welds, a portion of the previous weld passes is refined, and the toughness improved, as the heat from each pass tempers the weld metals below it. If the weld beads are smaller,

more grain refinement occurs, resulting in better notch toughness, all other factors being even (Funderburk, 1999).

Fig.8. Microstructure of weld for (a) low heat input

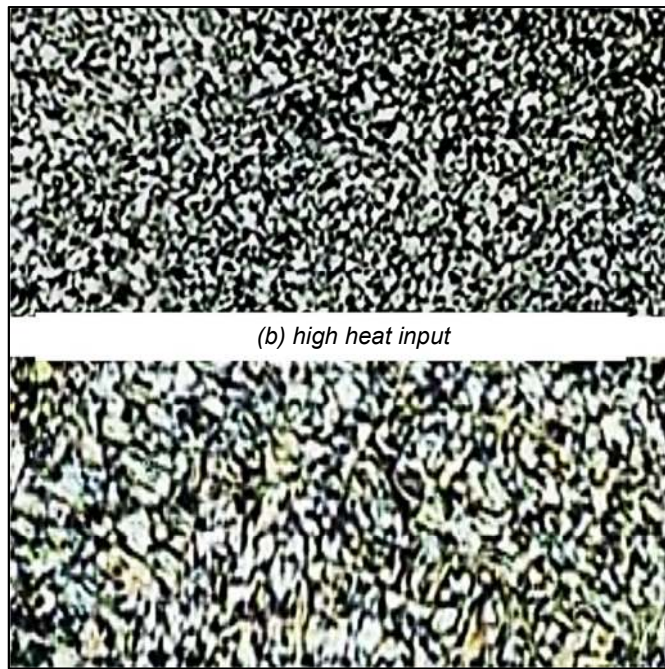
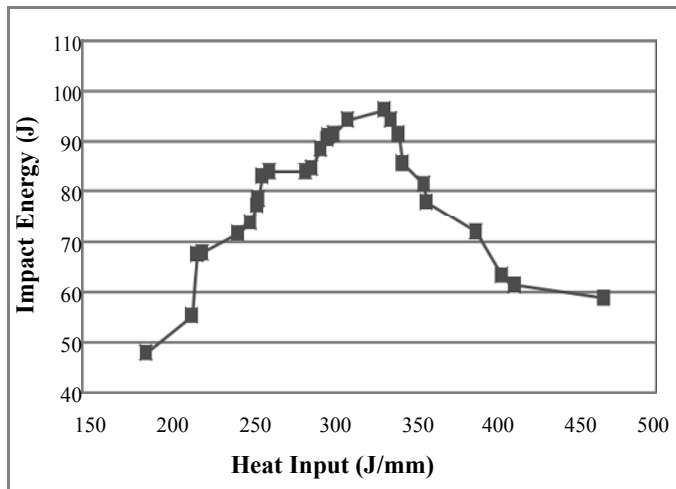


Fig.9. Impact energy of the weld metal vs. welding heat input.



3.3 Effect of welding parameters on penetration

The 27 welding samples for determining the bead penetration in different welding conditions are shown in Fig. 10. In Figs. 11-13, the welding speed was fixed on 50, 60, and 70 cm/min respectively, and the change in bead penetration was drawn vs. welding current for 20, 23, and 26 V arc voltage. A linear increase in bead penetration was observed with increasing welding current and arc voltage in different welding speeds. In Fig. 11, the welding speed was fixed on 50 cm/min. The largest penetration value of 3.150 mm was obtained in 150 A and 26 V condition, while the lowest penetration value was 2.411 mm in 110 A and 20 V condition.

In Fig. 12, the welding speed was fixed on 60 cm/min. The largest penetration value of 3.202 mm was obtained in 150 A and 26 V condition, while the lowest penetration value was 2.464 mm in 110 A and 20 V condition. In Fig. 13, the welding speed was fixed on 70 cm/min. The largest penetration value of 3.120 mm was obtained in 150 A and 26 V condition, and the lowest penetration value was 2.310 mm in 110 A and 20 V condition. The bead penetration increased with increasing welding speed from 50 to 60 cm/min. The 60 cm/min was the optimum value of welding speed to obtain maximum bead penetration. Bead penetration began to decrease in welding speeds higher than 60 cm/min. These results were similar to the results of previous literature (Tülbentci, 1990; Ates & Türker, 1999; Karadeniz *et al.*, 2007).

Fig.10. The 27 welding samples for determining the bead penetration in different welding conditions.

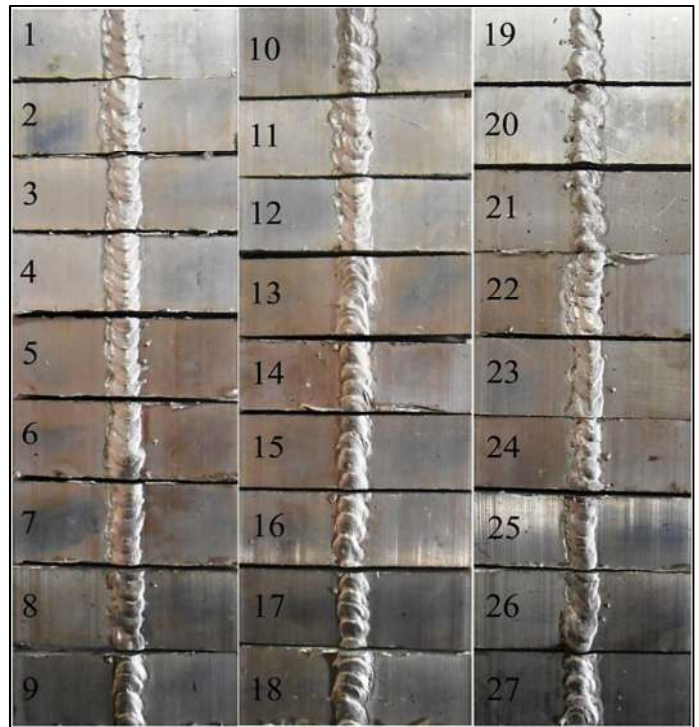


Fig.11. Penetration vs. welding current for 50 cm/min welding speed.

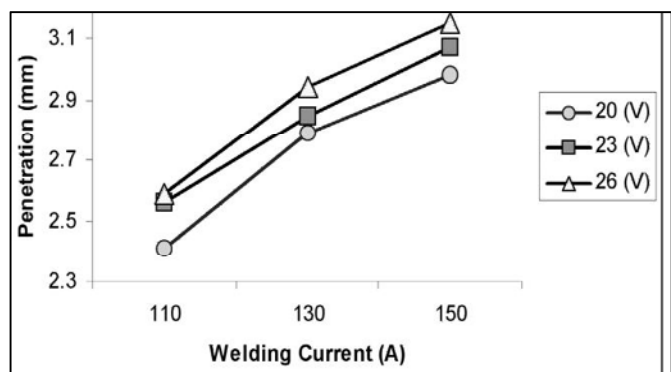


Fig.12. Penetration vs. welding current for 60 cm/min welding speed.

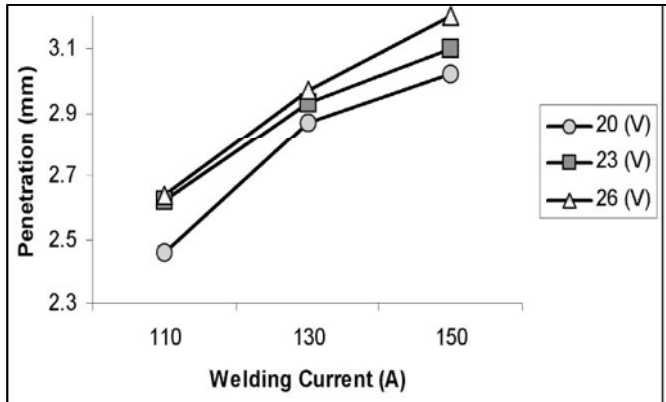
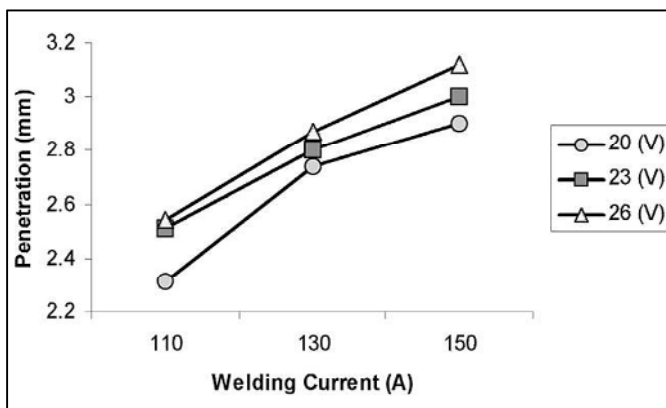


Fig.13. Penetration vs. welding current for 70 cm/min welding speed.



4. Conclusions

According to the results obtained from robotic MIG welding applied to AA6061 aluminum alloy plates with ~ 2.35 and 10 mm thickness:

The fatigue life of the weld metal decreased clearly with increasing arc voltage between 20 and 26 V and welding current between 110 and 150 A, whereas the effect of welding speed on fatigue life was reversed to other parameters. When welding speed increased, fatigue life of the weld metal also increased. Welding heat input increased by increasing arc voltage, welding current and decreasing welding speed. Impact energy of the weld metal increased slightly and then dropped significantly as welding heat input increased. The maximum value of impact energy for weld metal in the present study was 94.32 J that was obtained for $I=130$ A, $V=26$ V, and $S=60$ cm/min condition. The bead penetration increased linearly with increasing welding current between 110 and 150 A. In addition to the welding current, increasing arc voltage between 20 and 26 V also increased the bead penetration. However, its effect was not as much as welding current. When the welding speed was taken as a parameter, the largest bead penetration was obtained in 60 cm/min. The bead penetration increased with increasing welding speed between 50 and 60 cm/min, and then its value decreased after this point. The largest value of bead penetration in this study was 3.202 mm which was obtained in 150 A, 26 V, and 60 cm/min condition. The effect of welding current on bead penetration was greater than arc voltage and welding speed effect.

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6. References

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