



EFFECTIVE MODEL FOR ANALYSIS OF WOOD-FRAMED TIMBER STRUCTURES

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This paper presents new procedure modeling based on finite element method analysis of wood-framed timber structures. The fasteners linking boards of sheathing with the timber frame both modeled applying shell finite element, with individual material parameters, remain the main objective of this manuscript. Material parameters are obtained from experimental tests and numerical identification. The main objective of the paper is the elaboration of the numerical model with high precision of mapping, and, at the same time, diminishing the number of the unknown simplifying the process of the modeling of timber structures. The new presented method leads to a simplification of analysis of multistory wood-framed multifamily building structures.

Keywords: wood-framed buildings, numerical analysis, orthotropic material

1. INTRODUCTION

Wood-framed buildings represent a dominant branch of the building industry in the frame of residential construction. It has been underlined for four decades how low the energy consumption process of building elements composing in the plant is, as well as how short the time of realization is in the industrialization of construction operations. Most of light wood-framed buildings are constructed in the prefabricated systems.

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Construction technology consists of several stages of realization including displacements and lifting in the prefabricated plant, transport to the construction site, and finally assembly on site. The analytical models are focusing on the required load combinations and analysis appearing within the process of exploitation, and very often there are adoptions of a simplified form.

Due to recognizing the spatial, three-dimensional structure and behavior of the wall, floor diaphragms, and the whole building structure; their multi-layered combined structure shall be taken into account in the process of analysis.

Particularly difficult is precise formulation of connections between the timber frame and the boards of sheathing, inducing a large number of unknowns in the numerical analysis, and therefore the process of modeling becomes complicated. The three-dimensional wood-framed structure with a new model of fastener linking sheathing to framing is proposed in this paper. This new model of link in timber structure rationalizes to an accepted size volume of computational tasks moderating the precision of analysis.

2. FORMERLY ELABORATED ANALYTIC MODELS IN WOOD-FRAMED STRUCTURES

Analytical descriptions of wood-framed building structures with sheathing has been widely elaborated on since the seventies of the last century. Most of the proposed method of modeling is focused on the wall analysis due to detecting static and dynamic behavior and displacements of the diaphragm in its plane. There are recognized models regarding of mapping accuracy of construction details.

In the beam model [1, 2, 3, 4] frame elements of the timber structure are described as applying beam elements, while sheathing boards are represented by an adopted diagonal spring. The frame scheme of the structure is obtained in a result where triangle-creating beam elements are joined in nodes modeled applying non-dimensional spring elements of adequate stiffness.

In [5, 6, 7] diaphragms of wood-framed structures with sheathing are modeled in the form of plane models applying the finite element method with beam and shell plane elements.

In the three-dimensional model [8] all diaphragm building elements are represented applying shell finite elements describing the timber-framed structure and sheathing. These shell elements were proposed and described applying orthotropic material parameters. The fasteners linking frame to

sheathing were described adopting beam finite elements of isoparametric characteristics obtained from experimental tests of timber-to-sheathing board connections implemented in the FE-analysis.

Despite the significant number of proposed models, it still seems to be imperative to elaborate on a model easy in use, securing consistency of theoretic parameters obtained from the experiment at all stages of analysis; in the process of structure exploitation, transport, and assembly.

3. NEW ANALYTICAL MODEL PROPOSAL

A new three-dimensional (3D) model is proposed where all composing building large panel of the wood-framed structures with sheathing are both reducing the number of unknowns in the task and diminishing the size of the analytical problem. A new description of fastener linking sheathing with framing is proposed in the form of shell elements. The aim of introducing a new fastener model is its application in solutions of large tasks through a reduction of unknowns and a reduction of time for modeling in FE-analysis. These goals can be achieved through employment of wood-framed diaphragm shell elements of relatively big dimensions, condensed at the edges and corners of structures, linking frame to sheathing. The idea of this new model is shown in Figure 1a and the proposed model has been compared to the beam model presented in Figure 1b.

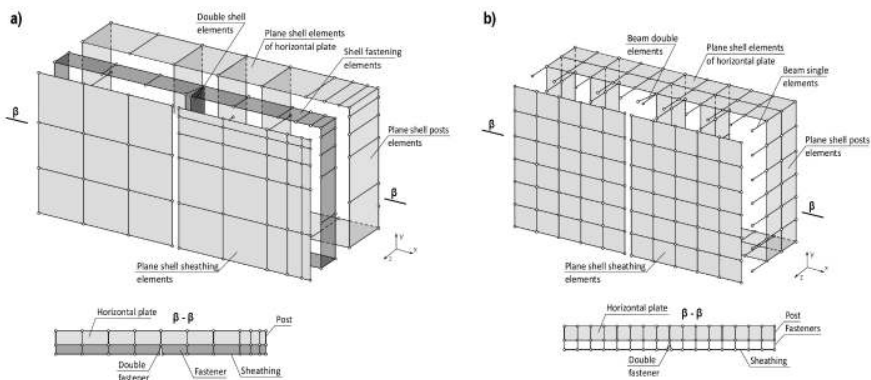


Fig. 1. Theoretical models used in analysis: a) proposed new model with application of shell elements with condensed discretization mesh at the edges and in the corners, b) former model with beam finite elements linking sheathing to framing of uniform spacing

This model allows us to group fasteners in one larger element, condensing the discretization mesh in the region of extreme or concentrated stressing. The linking fasteners are described applying shell elements similar in form to those describing framing and sheathing. For realization of this task it is required to determine adequate material and geometry parameters, and for fasteners these parameters arise from common work of linking metal staples, timber framing, and wood-derivative sheathing board.

In the shell elements based on the Reissner-Mindlin theory, the orthotropic material matrix is a function of six variables and has the form (1.1):

$$(1.1) \quad S = \begin{bmatrix} S_{11} & S_{12} & 0 & 0 & 0 \\ S_{21} & S_{22} & 0 & 0 & 0 \\ 0 & 0 & S_{44} & 0 & 0 \\ 0 & 0 & 0 & S_{55} & 0 \\ 0 & 0 & 0 & 0 & S_{66} \end{bmatrix}$$

where:

$$S_{11} = \frac{1}{E_1}, \quad S_{22} = \frac{1}{E_2}, \quad S_{44} = \frac{1}{2 \cdot G_{12}}, \quad S_{55} = \frac{1}{2 \cdot G_{23}}, \quad S_{66} = \frac{1}{2 \cdot G_{31}}, \quad S_{12} = -\frac{\nu_{21}}{E_2}, \quad S_{21} = -\frac{\nu_{12}}{E_1}$$

and E_{1i} E_2 are modules of longitudinal elasticity along the material axes, G_{12} is the modulus of transverse elasticity for the plane state of element, G_{23} and G_{31} are the shear modules in the normal planes and ν_{21} is the Poisson's ratio in the element plane. The system of coordinates describing timber frame structures and boards of sheathing is shown in Figure 2.

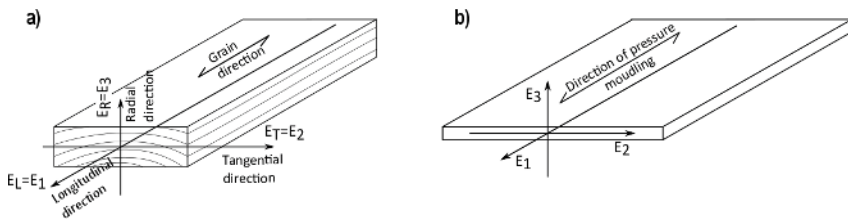


Fig.2 . Coordinates system of material axes in elements: a) timber framing, b) sheathing boards

Timber and OSB board parameters were obtained from tests of materials and they are to be used in direct application. The main problem refers to the evaluation of parameters of fasteners linking sheathing to framing.

Two stages are recognized in the analysis. At first, linking staples parameters were described in the form of isotropic beam elements spaced on 50 mm along the timber frame element (posts or horizontal plates). Then, parameters of staples were adopted in analysis in the form of orthotropic shell elements. In addition, timber frame elements and sheathing are modeled applying shell elements. It is indispensable to evaluate values of E and ν for linking beam elements and then E_1 , E_2 , G_{12} , G_{23} , G_{31} , ν_{21} for required shell elements.

4. ELEMENT PARAMETERS COMPOSING THE WALL DIAPHRAGMS

4.1. TIMBER FRAMING AND SHEATHING BOARDS

Material characteristics of posts and horizontal elements composing the wall diaphragms were obtained from experimental tests of samples cut out from spruce wood used for timber framing and sheathing boards OSB 3 thickness of 12mm. Obtained parameters are set in Table 1 .

Table 1. Material strength characteristics of spruce wood and OSB sheathing boards.

Material	Module of elasticity	Module of shear elasticity	ν ratio
Wood	$E_1 = E_L = 12000 \text{ MPa}$ $E_2 = E_T = 800 \text{ MPa}$	$G_{12} = G_{LT} = 670 \text{ MPa}$ $G_{21} = G_{LR} = 586 \text{ MPa}$ $G_{23} = G_{RT} = 34 \text{ MPa}$	$\nu_{21} = \nu_{LT} = 0.280$
OSB 3 sheathing board	$E_1 = 3703 \text{ MPa}$ $E_2 = 3260 \text{ MPa}$	$G_{12} = 1178 \text{ MPa}$ $G_{21} = 560 \text{ MPa}$ $G_{23} = 560 \text{ MPa}$	$\nu_{21} = 0.242$

4.2. FASTENERS LINKING SHEATHING TO FRAMING

4.2.1. EVALUATION OF MATERIAL PARAMETERS FOR STAPLE CONSIDERED AS THE BEAM FINITE ELEMENT

Material characteristics of connections cannot be directly read from the experimental tests. Experimental tests of joints give information on the deformability of joints, hence its relation in the formula $C=P/\delta$ between shear load P and slip δ in joints. The modulus of deformability represents steel fastener interaction and embedded materials where staples are sinking in. Evaluation of E and G module and ν ratio is conducted in numerical identification with determined deformability of joint.

Wall sheathing is linked to framing using A38 staples of fastener arms 1.60x1.30 mm in cross-section and arms in length of 37 mm. Fasteners (staples) are placed at an angle of 45° to the grain direction (along the longitudinal axis of timber framing – Figure 3a). Two arms of fastening staples are working in joints, and their cross-section moment of inertia according to Figure 3b is equal: $J_{x1} = J_{y1} = 51,697 \text{ mm}^4$.

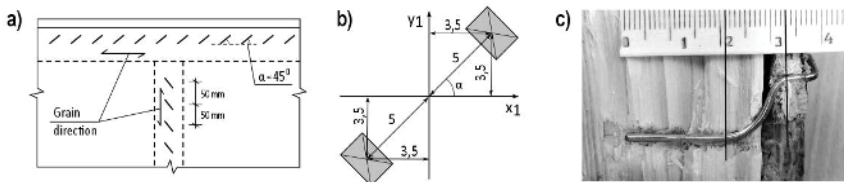


Fig. 3. a) Staples arrangement in joint, b) geometry of two arms of staple, c) fastener mode of failure

An adequate equivalent diameter of two arms of the cross-section area corresponds to a single rounded section of fastener 5.7 mm in diameter.

Within the tests (fig. 4) of connection displacements in joints in the elastic phase of loading exhibits slip equal 0.4 mm, perpendicular to grain direction and adequately 0.3 mm in the direction parallel to the grain. Corresponding loads applied in the tests to joints are 277.5 N and 158.04 N.

Deformability modulus computed from formula $C = \frac{P}{\delta}$ are, $C_{perp} = \frac{277.5}{0.4} = 693.75 \frac{N}{mm}$,

$C_{parallel} = \frac{158.04}{0.3} = 526.795 \frac{N}{mm}$. The average modulus of deformability value for both directions

is $C = 610.27 \frac{N}{mm}$.

Deformability modulus of staple fastener in the light of Standard PN-EN1995-1-1:2010 is equal

$K_{ser} = 600.81 \frac{N}{mm}$ and it is adopted in the task.

Fastener required material parameters are evaluated on the base of the theoretical model presented in work [8], where nails function as linking of sheathing to framing dowels. In the presented model the stapling fasteners are adopted in the form of rounded dia. 5.7 mm in the cross-section beam element. The 12 mm length of fastener has been used on the basis of the study mode of failure shown on Figure 3c.

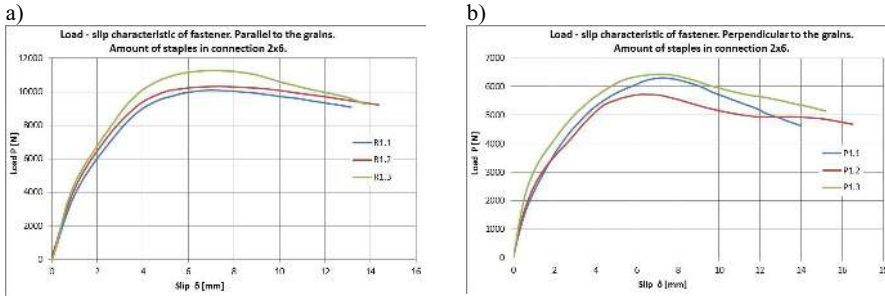


Fig. 4. Experimental test results of load-slip characteristics for staples fasteners:
a) load parallel to the grains, b) load perpendicular to the grains

Modulus of deformability $K_{ser} = 600.81 \frac{N}{mm}$ and deformation in the form of slip in joint $\delta = 0.4 mm$ corresponds to load to dowel equal $P = 240.324N$. Accepting determined in this way formula P/δ parameters: $E = 2500MPa$, $G=960MPa$ and $\nu=0.3$ were assigned based on canonical relations of the displacement method for both sides of the fixed beam. Parameters in the direction parallel/perpendicular to grain were separately determined accepting adequate joint deformability, according to tests.

4.2.2. MATERIAL PARAMETERS EVALUATION FOR STAPLED CONNECTION REGARDED THE SHELL FINITE ELEMENT

The transformation of beam fasteners into shell elements of constant thickness required assigning a value set in a matrix (1.1), element thickness and display reaction correctness to deformations in plate and plane state. Isotropic material parameters assigned above were accepted and then fit controlling concordance of loading with displacements determined in the form of modulus deformability K_{ser} . An identification process has been conducted in FE-analysis tasks for schemes shown in Figure 5. This process assumed determination of element thickness in flexure state (Figure 5a) and shear modulus G_{12} in the plate state (Figure 5b). A material coordinates system has been taken with accordance to Figure 6.

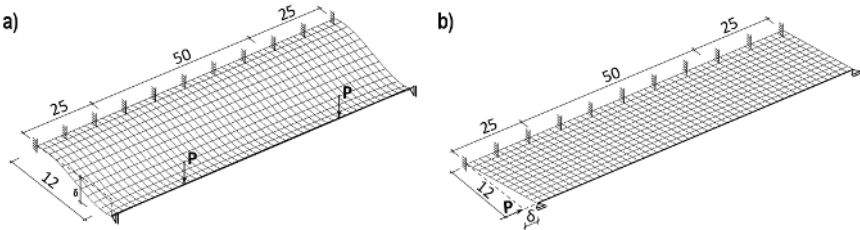


Fig.5. Analytical model of joint with shell fastening elements: a) perpendicular to grain, b) parallel to grain

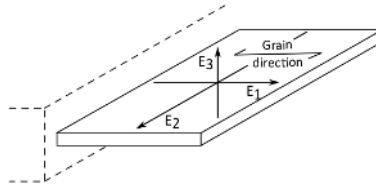


Fig. 6. Coordinates system of material for shell element adopted in model of joint

Established parameters are set in Table 2.

Table 2. Material parameters assessed for shell elements describing stapled connection

Parameter established in the FEM analysis						Thickness of shell elements h [mm]
Modulus of elasticity E_1 [MPa]	Modulus of elasticity E_2 [MPa]	Stiffness modulus G_{12} [MPa]	Stiffness modulus G_{1Z} [MPa]	Stiffness modulus G_{2Z} [MPa]	ν ratio	
2500	2500	72	960	960	0,3	2.03

5. VERIFICATION OF PRESENTED ANALYTICAL METHOD

A wall without openings measuring 2x1.20x2.50 m constructed of wood-frame, with both sides OSB 3 sheathing technology, has been analyzed. OSB sheathing was divided along the middle timber post of the wall, where both boards of sheathing were linked with two parallel rows of stapling fasteners. A concentrated load $P = 2.00$ kN was applied to the upper corner of wall causing bending of the diaphragm out of its plane (Figure 7a). The obtained results were compared to the experimental test results conducted on similar wall panels in the laboratory of the Chair of Structure Mechanics Bialystok University of Technology (Figure 7b). Displacements δ of wall out of plane at the height and

in the direction of P loading action were analyzed, and axial stress in the 1-1 cross-section of mostly stressed post as well as in the sheathing in the 2-2 cross-section of wall (half height of wall) were determined.

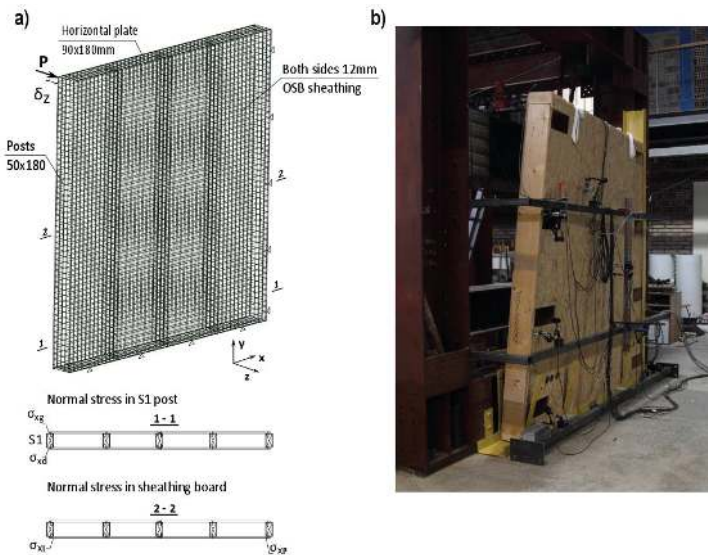


Fig.7. Wood-framed wall used in experimental test and analyses: a) discretization mesh and loading, b) view of experimentally tested panel

Analysis was conducted in four stages, through the kind and size of applied finite elements: small shell elements 5x5cm, medium shell elements 10x10cm, large shell elements 20x20cm, mixed in size shell elements with their condensation along the edges and in the corners.

Table 3. Results of displacements and stressing from FE-analysis applying varying finite elements in joint modeling

Kind of linking elements	Number of unknown	Displacements δ_z [mm]	Normal stress in cross-section				Degree of unknown in task
			Post S1		Sheathing board		
			σ_{xg} [kPa]	σ_{xd} [kPa]	σ_{xl} [kPa]	σ_{xp} [kPa]	
beam links	44769	39,13	-471	261	-14	-395	100%
small size of shell	44792	33,27	-562	304	-33	-341	100%
medium size of shell	13295	33,05	-762	510	-10	-321	30%
large size of shell	4121	32,45	-770	529	-31	-309	9%
mixed in size shell	5588	34,96	-699	522	-39	-311	12%
experimental test	--	36,21	-599	431	--	--	--

Linking elements were taken in the form of beam elements with dimensions $L=12\text{mm}$, $d=5.7\text{mm}$ and in the form of shell elements with dimensions of: $L=12\text{mm}$, $b=50\text{mm}$ (or less), $h=2.03\text{mm}$.

In the first stage shell elements of sheathing and framing were linked with beam elements. In the successive stages instead of beam linking elements the shell. Results obtained in analyses are set in Table 3, Figure 8, and Figure 9.

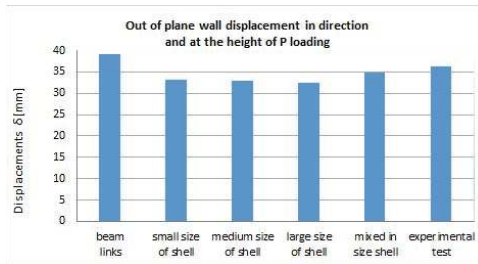


Fig. 8. Displacements δ out of the wall plane in the direction of loading P perpendicularly acting to the diaphragm

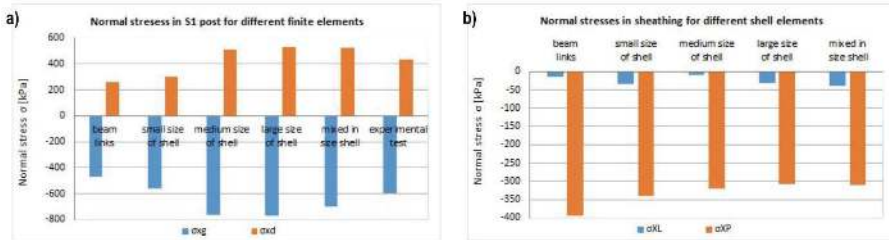


Fig.9. Normal stresses: a) along the grain direction in the cross-section of S1 post, b) parallel to the direction of OSB3 sheathing board, in the cross-section at the mid-height of wall diaphragm

6. CONCLUSIONS

Initial analytical beam models of fasteners linking sheathing to framing are based on the large number of finite elements, implicating adequately large number of unknowns. That analysis procedure allows us to solve problems of selected parts of buildings, like single walls, floors, or roof panels. Analysis of whole building structures with details of inter-elements connections creates a hard-to-resolve task.

It seems that the aim to evaluate analytical models in a lesser degree of complication in evaluation, being reduced not only to the plane elements devoid of three-dimensional form attributes (plate state or shell state); has been realized. The solved problem can be counted on to be precise, giving the pattern of stressing in all elements comprising the structure, and at the same time correctly imitating structural displacements.

A significant simplification on the stage of modeling three-dimensional (3D) structures and a considerable reduction in the number of unknowns is acquired when applying proposed model. An application of medium shell elements decreases the number of unknowns by 70%. Successively conducted analyses has proven that a better reflection of real structure behavior has been obtained applying a model of mixed-in-size finite shell elements, in addition to reducing by 80% the number of unknowns. The proposed solution can be successfully used in displacements and stressing analyses of three-dimensional wood-framed structures with sheathing for whole building or modular structures. In the author's opinion, the proposed model significantly simplifies the process of analysis, reflecting behaviors and responses of the structure under loading. Further analyses are being conducted, and they are essential for multistory and multifamily dwellings, where the process of modeling is particularly time-consuming.

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EFEKTYWNY MODEL ANALIZY SZKIELETOWYCH KONSTRUKCJI DREWNIANYCH

Słowa kluczowe: szkieletowe budynki drewniane, analiza numeryczna, materiał ortotropowy,

STRESZCZENIE:

W artykule przedstawiono nowy sposób modelowania szkieletowych konstrukcji drewnianych w oparciu o metodę elementów skończonych. Głównym zagadnieniem są łączniki szkieletu drewnianego z płytą poszycia, w opisie których przyjmuje się elementy powłokowe o szczególnych cechach materiałowych. Parametry materiałowe ustala się na podstawie prób materiałowych oraz identyfikacji numerycznej. Celem autora jest opracowanie modelu numerycznego o dużej dokładności odwzorowania przy jednoczesnym zmniejszeniu liczby niewiadomych i uproszczeniu procesu modelowania konstrukcji. W konsekwencji nowa metoda może ułatwić analizy budynków wielorodzinnych.

Proponuje się model przestrzenny (3D), który z jednej strony uwzględnia wszystkie elementy składowe panelowych konstrukcji szkieletowych, a z drugiej zmniejsza liczbę niewiadomych (w konsekwencji wielkość zadań obliczeniowych). Wprowadza się nowy opis łączników poszycia ze szkieletem drewnianym za pomocą elementów powłokowych. Główną intencją jest zastosowanie modelu do rozwiązywania dużych zadań przez redukcję niewiadomych i skrócenie czasu modelowania konstrukcji w programach MES. Cel może być osiągnięty poprzez zastosowanie w opisie konstrukcji jedynie powłokowych elementów skończonych o stosunkowo dużych wymiarach zagęszczonych na krawędziach i w narożach.

Taki model pozwala grupować łączniki w jeden większy element oraz zagęszczać siatkę dyskretyzacyjną w rejonach gdzie występują największe wyteżenia i koncentracja naprężeń. Łączniki opisuje się elementami powłokowymi podobnie jak rygle, słupki oraz płytę poszycia. Do realizacji zadania wymagane jest ustalenie odpowiednich parametrów geometrycznych i materiałowych, które w przypadku łączników są wynikiem współpracy trzech ośrodków: metalowej zszywki, drewnianego szkieletu konstrukcji oraz drewnopochodnej płyty poszycia. W proponowanym modelu przyjmuje się, iż wszystkie zastosowane materiały wykazują cechy ortotropowe ustalone na podstawie badań doświadczalnych.

Parametry drewna oraz płyty OSB są znane i możliwe do bezpośredniej aplikacji. Analizę obliczeniową łączników podzielono na dwa etapy. W pierwszym ustalono parametry zszywek opisanych w analizie za pomocą izotropowych elementów belkowych rozstawionych co 50mm. W drugim ustalono parametry zszywek przyjętych do analizy w postaci elementów powłokowych o charakterze ortotropowym.

Parametry materiałowe złączy nie mogą być odczytane bezpośrednio z badań doświadczalnych. W wyniku eksperymentu uzyskuje się informacje o podatności złącza tzn relację pomiędzy obciążeniem, a przemieszczeniem łącznika. Podatność jest wynikiem wzajemnego oddziaływania materiału zszywki oraz otoczenia, w którym jest ona zagłębiona. Ustalenia modułów E, G oraz ν dokonano w procesie identyfikacji numerycznej dla założonej podatności.

Podobnie poprzez identyfikację numeryczną ustalono parametry łączników w postaci elementów powłokowych o określonej grubości wykazując poprawność reakcji na odkształcenia w stanie płytowym i tarczowym.

Weryfikację proponowanego rozwiązania przeprowadzono na przykładach obliczeniowych tarczy ściennej poddanej zginaniu z płaszczyzny, obciążonej punktowo w jednym z naroży. Obliczenia wykonano przy zastosowaniu łączników

w postaci elementów belkowych oraz powłokowych o różnej wielkości (gęstości siatki). Wyniki porównano z rezultatami badań doświadczalnych ścian o podobnej konstrukcji.

Można przyjąć, iż dążenie do opracowania modelu, który będzie mniej skomplikowany w budowie, ale też nie sprowadzony jedynie do płaskich tarcz pozbawionych cech przestrzenności (stan płytowy, czy powłokowy) zostało zrealizowane. Zastosowane rozwiązanie należy zaliczyć do dokładnych dających obraz wytyczenia wszystkich elementów konstrukcji oraz poprawnie odwzorowujących jej odkształcenia. Jednocześnie uzyskano olbrzymie ułatwienie na etapie modelowania przestrzennego konstrukcji oraz znaczne ograniczenia w ilości niewiadomych. Zastosowanie elementów powłokowych o średniej wielkości zmniejszyło ilość niewiadomych o 70%. Kolejne analizy wykazały, iż lepsze odzwierciedlenie rzeczywistych reakcji konstrukcji uzyskano w modelu o mieszanych wielkościach elementów skończonych redukując jednocześnie ilość niewiadomych o około 80%.

Zaproponowane rozwiązanie może być z powodzeniem wykorzystane w analizach szkieletowych konstrukcji drewnianych ze współpracującym poszyciem. Zdaniem autora ułatwiają one w znacznym stopniu proces obliczeniowy zachowując pełny obraz odpowiedzi konstrukcji na obciążenia. W dalszym ciągu niezbędne są kolejne analizy, szczególnie dla całych budynków wielorodzinnych, gdzie proces budowania modelu jest szczególnie pracochłonny i czasochłonny.