Effects of Hall Current and Rotation on Magneto-Micropolar Generalized Thermoelasticity Due to Ramp-Type Heating

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Abstract In this work, a two dimensional problem in magnetic micropolar generalized thermoelastic medium, in the presence of a transverse magnetic field -taking into consideration the effect of Hall current- subjected to ramp-type heating, is investigated. The entire elastic medium is rotating with a uniform angular velocity. Laplace-Fourier transform technique is used to solve the problem. The transformed components of normal strain, normal stress, tangential couple stress, temper-ature distribution, and the current density components are obtained. The integral transforms have been inverted by using a numerical technique. Hall current effects and effect of rotation have been depicted graphically on the resulting quantities.

Keywords Hall Current, Micropolar, Thermoelasticity, Ramp-Type Heating

1. Introduction

The linear theory of elasticity is of paramount importance in the stress analysis of steel, which is the commonest engineering structural material. To a lesser extent, linear elasticity describes the mechanical behavior of the other common solid materials, e.g. concrete, wood and coal. However, the theory does not apply to the behavior of many of the new synthetic materials of the elastomer and polymer type, e.g. polymethyl-methacrylate (Perspex), polyethylene and polyvinyl chloride. The linear theory of micropolar elasticity is adequate to represent the behavior of such materials. For ultrasonic waves i.e. for the case of elastic vibrations characterized by high frequencies and small wavelengths, the influence of the body microstructure becomes significant. This influence of microstructure results in the development of new type of waves, not found in the classical theory of elasticity. Metals, polymers, composites, soils, rocks, concrete are typical media with microstructures. More generally, most of the natural and manmade materials including engineering, geological and biological media possess a microstructure. Eringen and Suhubi[1] and Suhubi and Eringen[2] developed the nonlinear theory of micro-elastic solids. Later Eringen[3-5] developed a theory for the special class of micro-elastic materials and called it the"linear theory of micropolar elasticity". Under this

theory, solids can undergo macro-deformations and macro-rotations.

The classical uncoupled theory of thermoelasticity predicts two phenomena not compatible with physical observations. First, the equation of heat conduction of this theory does not contain any elastic terms, second, the heat equation is of a parabolic type, predicting infinite speeds of propagation for heat waves.

Biot[6] introduced the theory of coupled thermoelasticity to overcome the first shortcoming. The governing equations for this theory are coupled, eliminating the first paradox of the classical theory. However, both theories share the second shortcoming since the heat equation for the coupled theory is also parabolic.

Two generalizations to the coupled theory were introduced. The first is due to Lord and Shulman[7], who obtained a wave-type heat equation by postulating a new law of heat conduction to replace the classical Fourier's law. Since the heat equation of this theory is of the wave-type, it automatically ensures finite speeds of propagation for heat and elastic waves. The remaining governing equations for this theory, namely, the equations of motion and constitutive relations, remain the same as those for the coupled and the uncoupled theories. The second generalization is known as the theory of thermoelasticity with two relaxation times, or the theory of temperature-rate-dependent thermoelasticity, and was proposed by Green and Lindsay[8]. It is based on a form of the entropy inequality proposed by Green and Laws[9]. It does not violate Fourier's law of heat conduction when the body under consideration has a center of symmetry, and it is valid for both isotropic and anisotropic

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bodies. Ezzat and Youssef[10] studied the generalized magneto-thermoelasticity in a perfectly

conducting medium.

The foundations of magnetoelasticity were presented by Knopoff[11] and Chadwick[12] and developed by Kaliski and Petykiewicz[13]. An increasing attention is being devoted to the interaction between magnetic field and strain field in a thermoelastic solid due to its many applications in the fields of geophysics, plasma physics and related topics. In all papers quoted above it was assumed that the interactions between the two fields take place by means of the Lorentz forces appearing in the equations of motion and by means of a term entering Ohm's law and describing the electric field produced by the velocity of a material particle, moving in a magnetic field.

Many authors have considered the propagation of electromagneto-thermoelastic waves in an electrically and thermally conducting solid. Paria[14] discussed the propagation of plane magneto-thermoelastic waves in an isotropic unbounded medium under the influence of a uniform thermal field and with a magnetic field acting transversely to the direction of the propagation. Paria used the classical Fourier law of heat conduction, and neglected the electric displacement. Wilson[15] extended Paria's results by introducing a component of the magnetic field parallel to the direction of the propagation. A comprehensive review of the earlier contributions to the subject can be found in Paria[16]. Among the authors who considered the generalized magneto-thermoelastic equations are Nayfeh and Namat-Nasser[17] who studied the propagation of plane waves in a solid under the influence of an electromagnetic field. They obtained the governing equations in the general case and the solution for some particular cases. Choudhuri[18] extended these results to rotating media. Sherief and Ezzat[19] solved a thermal shock half-space problem using asymptotic expansions. Lately, Rajneesh Kumar and Rupender[20] studied the effect of rotation in magneto-micropolar thermoelastic medium due to mechanical and thermal sources, Rajneesh Kumara and ManjeetSingh[21] solved the effect of rotation and imperfection on reflection and transmission of plane waves in anisotropic generalized thermoelastic media, R. Kumar, Praveen Ailawalia[22] studied moving load response in micropolar thermoelastic medium without energy dissipation possessing cubic symmetry, few attempts have been made to solve two-dimensional problems in this field Moncef Aouadi[23] introduced temperature dependence of an elastic modulus in generalized linear micropolar thermoelasticity.

When the magnetic field is very strong, the conductivity will be a tensor and the effect of Hall current cannot be neglected. The conductivity normal to the magnetic field is reduced due to the free spiraling of electrons and ions about the magnetic lines of force before suffering collisions and a current is induced in a direction normal to both the electric and magnetic fields. This phenomenon is called the Hall effect. In all of the above investigations, the effects of Hall current have not been considered. In this work, we introduced a new model of the equations of the generalized magneto micropolar thermoelasticity in the presence of transverse magnetic field, taking into consideration the effects of Hall current and rotation, is applied to both generalizations, Lord–Shulman theory and Green–Lindsay theory, as well as to the coupled theory.

2. Basic Equations

In the dynamical of linear theory of magneto micropolar thermoelasticity permeated by an initial strong magnetic field of strength $\mathbf{H} = (0, 0, H_o)$. We consider The elastic medium is rotating uniformly with an angular velocity Ω .

The governing equations of motion for homogenous, isotropic and elastic solid, when the Hall current and rotation effect is taken into account consists of

i. The equations of motion taking into account the Lorentz force have the form

$$\sigma_{\mathbf{j},\mathbf{ij}} + \mu_o \varepsilon_{\mathbf{ijr}} \mathbf{J}_{\mathbf{j}} \mathbf{H}_{\mathbf{r}} = \rho \left(\mathbf{u}_{\mathbf{i},\mathbf{tt}} + \Omega \times (\Omega \times u) + 2 \left(\Omega \times \frac{\partial u}{\partial t} \right) \right)^{(1)}$$
$$\varepsilon_{\mathbf{ijr}} \sigma_{\mathbf{jr}} + m_{j\mathbf{i},j} = j \rho \left(\phi_{\mathbf{i},\mathbf{tt}} + \Omega \times \frac{\partial \phi}{\partial t} \right)$$
(2)

where σ_{ij} is the force stress tensor, u_i is the components of the displacement vector, ϕ_i is the components of the microrotation vector, m_{ij} is the couple stress tensor, ρ is the density, j is the microinertia, ϵ_{ijr} is the permutation symbol, μ_o is the magnetic permeability, and J_r is the conduction current density, given by The generalized Ohm's law including Hall current:

$$J = \frac{\sigma_0}{1 + m^2} \left(E + \mu_0 \dot{u} \times H - \frac{1}{en_e} J \times H_0 \right)$$
(3)

where E is the intensity vector of the electric field, m (= $\omega_e t_e$) is the Hall parameter, t_e is the electron collision time, $\omega_e (= e B_o/m_e)$ is the electronic frequency, e is the charge of an electron, B_o is the magnetic induction, m_e is the mass of the electron, $\sigma_o (e^2 n_e t_e/m_e)$, is the electrical conductivity and n_e is the number density of electrons.

ii. The constitutive equation

$$\sigma_{ij} = \lambda u_{r,r} \delta_{ij} + \mu (u_{i,j} + u_{j,i})$$

$$+ k (u_{j,i} - \varepsilon_{ijr} \phi_r) - \gamma_1 (T + \nu T_{,t}) \delta_{ij}$$

$$m_{ij} = \alpha \phi_{r,r} \delta_{ij} + \beta \phi_{i,j} + \gamma \phi_{j,i}$$
(4)
(5)

where λ , μ are Lame's constants, α , β , γ , and k are micropolar constants, T is the absolute temperature of the medium, ν is the constant with dimension of time, called relaxation time, γ_1 is the material constant given by $\gamma_1 = (3 \lambda + 2\mu + K) \alpha_1$, α_1 being a coefficient of linear thermal expansion.

iii. The generalized equation of heat condition

$$KT_{,jj} = \rho c_E \left(T_t + \tau_o T_{,t} \right) + T_o \gamma_1 \left(u_{i,it} + n_o \tau_o u_{i,itt} \right)$$
(6)

where K is thermal conductivity, c_E is the specific heat at constant temperature, T_o is the uniform temperature, τ_o is an other relaxation time and n_o is a non-dimensional constant.

For L–S theory $n_0 = 1$, $\tau_o > 0$, $\nu = 0$, and for G–L theory $n_0 = 0$, $\tau_o > 0$, $\nu > 0$.

Substituting equations (4), and (5) into equation (5), and (6) we get

$$\begin{aligned} (\lambda + \mu)u_{j,ji} + (\mu + k)u_{i,jj} + k\varepsilon_{ijr}\phi_{r,j} - \gamma_1(T_{,i} + \nu T_{,it}) \\ + \mu_0\varepsilon_{rji}J_rH_j &= \rho \left(u_{i,tt} + \Omega \times (\Omega \times u) + 2 \left(\Omega \times \frac{\partial u}{\partial t} \right) \right) \end{aligned} (7) \\ (\alpha + \beta)\phi_{j,ji} + \gamma\phi_{i,jj} + k\varepsilon_{ijr}u_{r,j} - 2k\phi_i &= \\ j\rho \left(\phi_{i,tt} + \left(\Omega \times \frac{\partial \phi}{\partial t} \right) \right) \end{aligned} (8)$$

3. Formulation and Solution of the Problem

The rectangular Cartesian system (x, y, z) having origin on the surface z = 0 with z-axis vertical into the medium is introduction. In the following, we restrict our analysis parallel to xz-plane with $z \ge 0$, $u_i = (u, 0, w)$, $\varphi_i = (0, \varphi_2, 0)$ and $\Omega = (0, \Omega, 0)$, we also assume that E = 0, the generalized Ohm's law gives $J_y = 0$ everywhere in the medium. The current density components J_x and J_z are given by:

$$J_x = \frac{\sigma_o B_o}{1+m^2} \left(m \frac{\partial u}{\partial t} - \frac{\partial w}{\partial t} \right)$$
(9)

$$J_z = \frac{\sigma_o B_o}{1 + m^2} \left(\frac{\partial u}{\partial t} + m \frac{\partial w}{\partial t} \right)$$
(10)

Let us introduce the following non-dimensional variables:

$$\begin{aligned} x^{*} &= \frac{\eta_{o}}{c_{o}}, z^{*} = \frac{\eta_{o}}{c_{o}}, u^{*} = \frac{\rho \eta_{o} c_{o}}{\gamma_{1} T_{o}} u, w^{*} = \frac{\rho \eta_{o} c_{o}}{\gamma_{1} T_{o}} w, t^{*} = \eta_{o} t, \\ \tau^{*}_{o} &= \eta_{o} \tau_{o}, v^{*} = \eta_{o} v, T^{*} = \frac{T}{T_{o}}, \sigma^{*}_{ij} = \frac{\sigma_{ij}}{\gamma_{1} T_{o}}, m^{*}_{ij} = \frac{\eta_{o}}{c_{o} \gamma_{1} T_{o}} m_{ij}, \\ \varphi^{*}_{2} &= \frac{\rho c_{o}^{2}}{\gamma_{1} T_{o}} \varphi_{2}, M = \frac{\sigma_{o} B_{o}}{\rho c_{o}^{2} \eta_{o}}, \Omega^{*} = \frac{\Omega}{\eta_{o}}, \end{aligned}$$

where $c_o^2 = K/\rho$, $\eta_o = \rho c_E/k$, and M is the Hartmann number or magnetic parameter.

The system of equations (6)-(8), using relations (9), and (10), takes the following form – dropping the asterisks for convenience-,

$$\frac{\partial^2 u}{\partial t^2} = \frac{\lambda + \mu}{\rho c_o^2} \frac{\partial e}{\partial x} + \frac{\mu + k}{\rho c_o^2} \nabla^2 u - \frac{k}{\rho c_o^2} \frac{\partial \phi_2}{\partial z} + \Omega^2 u$$

$$- 2\Omega \frac{\partial w}{\partial t} - \left(1 + v \frac{\partial}{\partial t}\right) \frac{\partial T}{\partial x} + \frac{M}{1 + m^2} \left(\frac{\partial u}{\partial t} + m \frac{\partial w}{\partial t}\right)$$
(11)

$$\frac{\partial^2 w}{\partial t^2} = \frac{\lambda + \mu}{\rho c_o^2} \frac{\partial e}{\partial z} + \frac{\mu + k}{\rho c_o^2} \nabla^2 w + \frac{k}{\rho c_o^2} \frac{\partial \phi_2}{\partial x} + \Omega^2 w$$
(12)
+ $2\Omega \frac{\partial u}{\partial t} - \left(1 + v \frac{\partial}{\partial t}\right) \frac{\partial T}{\partial z} - \frac{M}{1 + m^2} \left(m \frac{\partial u}{\partial t} - \frac{\partial w}{\partial t}\right)$

$$\frac{\rho_j}{\gamma} \frac{\partial^2 \phi_2}{\partial t^2} = \left(\nabla^2 - 2k\right) \phi_2 + k \left(\frac{\partial u}{\partial z} - \frac{\partial w}{\partial x}\right)$$
(13)

$$\tau_{o} \frac{\partial^{2} T}{\partial t^{2}} = \left(\nabla^{2} - \frac{\partial}{\partial t}\right) T$$

$$- \frac{\gamma_{1}^{2} T_{o}}{K n_{o} o} \left(\frac{\partial}{\partial t} + n_{o} \tau_{o} \frac{\partial^{2}}{\partial t^{2}}\right) \left(\frac{\partial u}{\partial x} + \frac{\partial w}{\partial z}\right)$$
(14)

$$\sigma_{xx} = (\lambda + 2\mu + k)\frac{\partial u}{\partial x} + \lambda \frac{\partial w}{\partial z} - \gamma \left(1 + v \frac{\partial}{\partial t}\right)T \quad (15)$$

$$\sigma_{zz} = \left(\lambda + 2\mu + k\right) \frac{\partial w}{\partial z} + \lambda \frac{\partial u}{\partial x} - \gamma \left(1 + v \frac{\partial}{\partial t}\right) T \qquad (16)$$

$$\sigma_{yy} = \lambda \left(\frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} \right) - \gamma \left(1 + v \frac{\partial}{\partial t} \right) T$$
(17)

$$\sigma_{xz} = \mu \frac{\partial w}{\partial x} + (\mu + k) \frac{\partial u}{\partial z}$$
(18)

$$m_{xy} = \beta \frac{\partial \phi_2}{\partial x} \tag{19}$$

$$m_{zy} = \gamma \frac{\partial \phi_2}{\partial z} \tag{20}$$

Introducing potential functions $\Phi(x,z,t)$, and $\Psi(x,z,t)$ defined by

$$u = \frac{\partial \Phi}{\partial x} + \frac{\partial \Psi}{\partial z}, \quad w = \frac{\partial \Phi}{\partial z} - \frac{\partial \Psi}{\partial x},$$

$$e = \nabla^2 \Phi, \qquad \frac{\partial u}{\partial z} - \frac{\partial w}{\partial x} = \nabla^2 \Psi.$$
(21)

Substituting Eq. (21) into Eqs. (11)-(14) we obtain

$$\left(\frac{\lambda + 2\mu + k}{\rho c_o^2} \nabla^2 - \frac{\partial^2}{\partial t^2} + \frac{M}{1 + m^2} \frac{\partial}{\partial t} + \Omega^2\right) \Phi = (22)$$

$$\frac{1+v\frac{\partial}{\partial t}}{r} T + \left[\frac{Mm}{1+m^2} - 2\Omega\right] \frac{\partial \Psi}{\partial t}$$

$$\left(\frac{\mu+k}{\rho c_o^2} \nabla^2 - \frac{\partial^2}{\partial t^2} + \frac{M}{1+m^2} \frac{\partial}{\partial t} + \Omega^2\right) \Psi =$$

$$\frac{k}{\rho c_o^2} \phi_2 - \left(\frac{Mm}{1+m^2} + 2\Omega\right) \frac{\partial \Phi}{\partial t}$$
(23)

$$\left(\nabla^2 - \frac{\rho j}{\gamma} \frac{\partial^2}{\partial t^2} - 2k\right) \phi_2 = -k \nabla^2 \Psi$$
(24)

$$\left(\nabla^2 - \frac{\partial^2}{\partial t^2} - \frac{\partial}{\partial t}\right)T = \frac{\gamma_1^2 T_o}{K\eta_o \rho} \left(\frac{\partial}{\partial t} + n_o \tau_o \frac{\partial^2}{\partial t^2}\right) \nabla^2 \Phi \quad (25)$$

Taking Laplace transform defined by the relation:

$$\overline{f}(s) = \int_0^\infty e^{-st} f(t) dt$$

of both sides of (15)-(20) and (22)-(25) using the homogenous initial conditions, we obtain:

$$\left(\frac{\lambda+2\mu+k}{\rho c_o^2}\nabla^2 - \left(s^2\tau_o - \frac{sM}{1+m^2} - \Omega^2\right)\right)\overline{\Phi} =$$
(26)

$$(1 + \nu s)\overline{T} + s\left(\frac{Mm}{1 + m^2} - 2\Omega\right)\overline{\Psi}$$

$$\left(\frac{\mu + k}{\rho c_o^2}\nabla^2 - \left(\tau_o s^2 - \frac{Ms}{1 + m^2} - \Omega^2\right)\right)\overline{\Psi} = (27)$$

$$k - \overline{\tau} = \left(\frac{Mms}{1 + m^2} + 2\Omega\right)\overline{\Phi}$$

$$\frac{1}{\rho c_o^2} \phi_2 - s \left(\frac{1}{1 + m^2} + 2\Omega \right) \Phi$$

$$\left(\nabla^2 - \left(\frac{\rho j}{\gamma} s^2 - 2k \right) \right) \overline{\phi}_2 = -k \nabla^2 \overline{\Psi}$$
(28)

$$\left(\nabla^2 - \left(1 + \tau_o s\right)s\right)\overline{T} = \frac{\gamma_1^2 T_o}{K\eta_o \rho} s \left(1 + n_o \tau_o s\right) \nabla^2 \overline{\Phi}$$
(29)

$$\overline{\sigma}_{xx} = \left(\lambda + 2\mu + k\right) \frac{\partial \overline{u}}{\partial x} + \lambda \frac{\partial \overline{w}}{\partial z} - \gamma \left(1 + \nu s\right) \overline{T} \quad (30)$$

$$\overline{\sigma}_{zz} = (\lambda + 2\mu + k)\frac{\partial \overline{w}}{\partial z} + \lambda \frac{\partial \overline{u}}{\partial x} - \gamma (1 + \nu s)\overline{T} \quad (31)$$

$$\overline{\sigma}_{yy} = \lambda \left(\frac{\partial \overline{u}}{\partial x} + \frac{\partial \overline{w}}{\partial z} \right) - \gamma \left(1 + vs \right) \overline{T}$$
(32)

$$\overline{\sigma}_{xz} = \mu \frac{\partial \overline{w}}{\partial x} + (\mu + k) \frac{\partial \overline{u}}{\partial z}$$
(33)

$$\overline{m}_{xy} = \beta \frac{\partial \overline{\varphi}_2}{\partial x}, \ \overline{m}_{zy} = \gamma \frac{\partial \overline{\phi}_2}{\partial z}$$
 (33a)

We now use the Fourier transform with respect to the space variable z, defined by

$$\overline{f}^*(q) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} e^{iqz} f(z) dy$$

Taking the Fourier transform of both sides of (26)-(33)

$$\left(D^2 - \delta_1\right)\overline{\Phi}^* = \delta_2\overline{T}^* - \delta_3\overline{\Psi}^* \tag{34}$$

$$\left(D^2 - \delta_4\right)\overline{\Psi}^* = \delta_5\overline{\phi}_2^* + \delta_6\overline{\Phi}^* \tag{35}$$

$$\left(D^2 - \delta_7\right)\overline{\phi}_2^* = -k\left(D^2 - q^2\right)\overline{\Psi}^* \tag{36}$$

$$\left(D^2 - \delta_8\right)\overline{T}^* = \delta_9 \left(D^2 - q^2\right)\overline{\Phi}^* \tag{37}$$

$$\overline{\sigma}_{xx}^* = (\lambda + 2\mu + k)D\overline{u}^* + iq\lambda\overline{w}^* - \gamma(1 + vs)\overline{T}^* \quad (38)$$

$$\overline{\sigma}_{zz}^{*} = iq(\lambda + 2\mu + k)\overline{w}^{*} + \lambda D\overline{u}^{*} - \gamma(1 + vs)T^{*} \quad (39)$$

$$\overline{\sigma}^{*} = -\lambda(D\overline{u}^{*} + iq\overline{w}^{*}) - \gamma(1 + vs)\overline{T}^{*} \quad (40)$$

$$\sigma_{yy} = \lambda (Du + iqw) - \gamma (1 + Vs)I \qquad 40)$$

$$\overline{\sigma}_{xz}^{*} = \mu D \overline{w}^{*} + iq(\mu + k) \overline{u}^{*}$$

$$\overline{m}_{xz}^{*} = \beta D \overline{\phi}_{2}^{*}$$
(41)
(41)
(42)

$$\overline{m}_{xy} = \beta D\phi_2 \tag{42}$$

$$\bar{m}_{zy}^* = i\gamma q \,\bar{\phi}_2^* \tag{43}$$

$$\begin{split} \delta_{1} &= \frac{\rho c_{o}^{2}}{\lambda + 2\mu + k} \left(s^{2} \tau_{o} - \frac{Ms}{1 + m^{2}} - \Omega^{2} \right) + q^{2}, \, \delta_{2} = \frac{s \rho c_{o}^{2} \left(1 + vs \right)}{\lambda + 2\mu + k} \\ \delta_{3} &= \frac{s \rho c_{o}^{2}}{\left(\lambda + 2\mu + k\right)} \left(\frac{Mm}{\left(1 + m^{2}\right)} + 2\Omega \right) \\ \delta_{4} &= \frac{\rho c_{o}^{2}}{\mu + k} \left(s^{2} \tau_{o} - \frac{sM}{1 + m^{2}} - \Omega^{2} \right) + q^{2} \\ \delta_{5} &= \frac{sk}{\mu + k}, \quad \delta_{6} &= \frac{s \rho c_{o}^{2} Mm}{\left(\mu + k\right)} \left(\frac{Mm}{\left(1 + m^{2}\right)} - 2\Omega \right) \\ \delta_{7} &= \left(\frac{\rho j}{\gamma} s^{2} - 2k \right) + q^{2} \\ \delta_{8} &= \left(1 + \tau_{o} s \right) s + q^{2}, \quad \delta_{9} &= \frac{\gamma_{1}^{2} T_{o}}{K \eta_{o} \rho} s \left(1 + n_{o} \tau_{o} s \right) \end{split}$$

and the operator D means the derivative with respect to x. On Eqs. (34)-(37) and after some simplification, we arrive at the following

eighth order differential equation satisfied by $\overline{\Phi}^*, \overline{T}^*, \overline{\Psi}^*$ and $\overline{\varphi}_2^*,$

$$\left\{ D^8 - AD^6 + BD^4 - CD^2 + F \right\} \left(\overline{\Phi}^*, \overline{T}^*, \overline{\Psi}^*, \overline{\phi}_2^* \right) = 0 \qquad (44)$$

where
$$A = \delta_1 + \delta_2 \delta_9 + \delta_4 + k \delta_5 + \delta_7 + \delta_8$$
,
 $B = \delta_1 \delta_8 + \delta_2 \delta_9 q^2 + \delta_4 \delta_7 - \delta_5 q^2$
 $+ (\delta_1 + \delta_8 + \delta_2 \delta_9) (\delta_4 + \delta_7 - k \delta_5)$
 $C = (\delta_4 \delta_7 - \delta_5 q^2) (\delta_1 + \delta_8 + \delta_2 \delta_9)$
 $+ (\delta_1 \delta_8 + \delta_2 \delta_9 q^2) (\delta_4 + \delta_7 - k \delta_5)$
 $F = (\delta_1 \delta_8 + \delta_2 \delta_9 q^2) (\delta_4 \delta_7 - \delta_5 q^2)$

The solution of the Eq. (44) satisfying the radiation conditions that $\overline{\Phi}^*, \overline{\Psi}^*, \overline{\varphi}_2^*$ and \overline{T}^* tend to zero as x tends to infinity can be written as

$$\left(\bar{\Phi}^{*}, \bar{\Psi}^{*}, \bar{\phi}_{2}^{*}, \bar{T}^{*}\right)(x, q, s) = \sum_{i=1}^{4} \left(1, \ell_{1i}, \ell_{2i}, \ell_{3i}\right) A_{i} e^{-k_{i} x}$$
(45) where

$$\ell_{1i} = \frac{\delta_2 \delta_9 (k_1^2 - q^2) - (k_4^2 - \delta_8) (k_1^2 - \delta_1)}{\delta_3 (k_4^2 - \delta_8)}, \quad i = 1, 2, 3, 4$$

$$\ell_{2i} = \frac{(k_2^2 - \delta_4) \Big[\delta_2 \delta_9 (k_1^2 - q^2) - (k_4^2 - \delta_8) (k_1^2 - \delta_1) \Big]}{\delta_3 \delta_5 (k_4^2 - \delta_8)}$$

$$- \frac{\delta_6}{\delta_5}, \quad \ell_{3i} = \frac{\delta_9 (k_1^2 - q^2)}{(k_4^2 - \delta_8)}$$

and k_i (i=1,2,3,4) are the characteristic roots of the characteristic equation (36) which is

$$k^8 - Ak^6 + Bk^4 - Ck^2 + F = 0,$$

Eq. (21) together with Eq. (45), immediately give

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where

$$\overline{u}^{*}(x,q,s) = \sum_{j=1}^{4} (iq\ell_{1j} - k_j) A_j e^{-k_j x}$$
(46)

$$\overline{v}^{*}(x,q,s) = \sum_{j=1}^{4} \left(iq + k_{j} \ell_{1j} \right) A_{j} e^{-k_{j} x}$$
(47)

4. Application

The boundary of the half-space is affected by ramp-type heating, which depends on the coordinate z and the time t of the form

$$T(0, z, t) = G(t)F(z)$$
 (48)

where F(z) is an arbitrary function of z and G(t) is a function defined as Misra et al.,[25]:

$$G(t) = \begin{cases} 0 & t \le 0 \\ T_1 \frac{t}{t_o} & 0 < t \le t_o \\ T_1 & t > t_o \end{cases}$$
(49)

where t_o indicates the length of time to rise the heat and T_1 is constant, this means that the boundary of the half-space, which is initially at rest and has a fixed temperature T_o , is suddenly raised to a temperature equal to the function G(t)F(z) and maintained at this temperature from then on.

Applying the Laplace and Fourier transforms to both sides of Eq. (42), we obtain

$$\overline{T}^{*}(0,q,s) = \overline{G}(s)\overline{F}^{*}(q)$$
(50)
where $\overline{G}(s) = T_{1} \frac{\left(1 - e^{-st_{o}}\right)}{t_{0}s^{2}}$

We assume that, on the boundary x = 0 the displacement u of the body does not depends on x, hence we have Du(0, z, t) = 0 and the medium is subjected to a rough and rigid foundation enough to prevent the displacement w at any time and any point of z, so also we have w(0, x, t) = 0, m_{zy} = 0.

Applying the Laplace and Fourier transforms, we get

$$D\overline{u}^* = \overline{w}^* = \overline{m}_{zy}^* = 0 \tag{51}$$

Using the values in expressions (50), and (51), the above general expressions reduce in our case to the following form

$$\overline{u}^{*}(x,q,s) = \sum_{j=1}^{4} \left(iq\ell_{1j} - k_j \right) A_{j1} e^{-k_j x}$$
(52)

$$\overline{v}^{*}(x,q,s) = \sum_{j=1}^{4} (iq + k_{j}\ell_{1j}) A_{j1} e^{-k_{j}x}$$
 (53)

$$\overline{T}^{*}(x,q,s) = \sum_{j=1}^{4} \ell_{3j} A_{j1} e^{-k_{j}x}$$
(54)

$$\overline{\phi}_{2}^{*}(x,q,s) = \sum_{j=1}^{4} \ell_{2j} A_{jl} e^{-k_{j}x}$$
(55)

$$\bar{\sigma}_{xx}^{*} = \sum_{j=1}^{4} \begin{pmatrix} \lambda \left(k_{j}^{2} - q^{2}\right) - k_{j} \left(2\mu + k\right) \left(iq\ell_{1j} - k_{j}\right) \\ + \gamma \left(1 + vs\right)\ell_{3j} \end{pmatrix} A_{j1} e^{-k_{j}x} (56)$$

$$\bar{\sigma}^{*} = -\sum_{j=1}^{4} \begin{pmatrix} iq \left(2\mu + k\right) \left(iq + k_{j}\ell_{1j}\right) \\ - \lambda \left(iq + k_{j}\ell_{1j}\right) \end{pmatrix} A_{j1} e^{-k_{j}x} (57)$$

$$\bar{\sigma}_{zz}^{*} = \sum_{j=1}^{2} \left(+\lambda \left(k_{j}^{2} - q^{2}\right) - \gamma \left(1 + vs\right)\ell_{3j} \right) A_{j1}e^{-\kappa_{j}x}$$
(57)

$$\bar{\sigma}_{yy}^{*} = \sum_{j=1}^{4} \left(\lambda \left(k_{j}^{2} - q^{2} \right) - \gamma \left(1 + \nu s \right) \ell_{3j} \right) A_{j1} e^{-k_{j} x}$$
(58)

$$\overline{\sigma}_{xz}^{*} = \sum_{j=1}^{4} \left(iq(\mu+k) (iq\ell_{1j}-k_j) - \mu k_j (iq+k_j\ell_{1j}) \right) A_{j1} e^{-k_j x}$$
(59)

$$\overline{m}_{xy}^* = -\gamma \sum_{j=1}^4 k_j \ell_{2j} A_{j1} e^{-k_j x}$$
(60)

$$\overline{m}_{zy}^{*} = -i\gamma q \sum_{j=1}^{4} \ell_{2j} A_{j1} e^{-k_j x}$$
(61)

where

$$\begin{split} &A_{11} = \frac{P_1}{P}, \ A_{21} = \frac{P_2}{P}, \ A_{31} = \frac{P_3}{P}, \ A_{14} = \frac{P_4}{P} \\ &P = iq\gamma \Big[L_{11}k_1 \big(\ell_{22}k_2 \big(\ell_{33} - \ell_{34} \big) + \ell_{23}k_3 \big(\ell_{34} - \ell_{32} \big) + \ell_{24}k_4 \big(\ell_{32} - \ell_{33} \big) \big) \\ &- L_{12}k_2 \big(\ell_{21}k_1 \big(\ell_{32} - \ell_{34} \big) + \ell_{22}k_3 \big(\ell_{34} - \ell_{31} \big) + \ell_{24}k_4 \big(\ell_{31} - \ell_{33} \big) \big) \\ &+ L_{13}k_3 \big(\ell_{21}k_1 \big(\ell_{32} - \ell_{34} \big) + \ell_{22}k_2 \big(\ell_{33} - \ell_{31} \big) + \ell_{24}k_4 \big(\ell_{31} - \ell_{32} \big) \big) \\ &- L_{14}k_4 \big(\ell_{21}k_1 \big(\ell_{32} - \ell_{33} \big) + \ell_{22}k_2 \big(\ell_{33} - \ell_{31} \big) + \ell_{23}k_3 \big(\ell_{31} - \ell_{33} \big) \big) \Big] \\ P_1 = iqT_1 \frac{\big(1 - e^{-st_0} \big)}{t_0 s^2} \bigg[L_{12}k_2 \big(\ell_{23}k_3 - \ell_{24}k_4 \big) + L_{13}k_3 \big(\ell_{24}k_4 - \ell_{22}k_2 \big) \\ &+ L_{14}k_4 \big(\ell_{22}k_2 - \ell_{23}k_3 \big) + L_{13}k_3 \big(\ell_{21}k_1 - \ell_{24}k_4 \big) \bigg] \\ P_2 = iqT_1 \frac{\big(1 - e^{-st_0} \big)}{t_0 s^2} \bigg[L_{11}k_1 \big(\ell_{22}k_2 - \ell_{24}k_4 \big) + L_{13}k_3 \big(\ell_{21}k_1 - \ell_{24}k_4 \big) \\ &+ L_{14}k_4 \big(\ell_{21}k_1 - \ell_{22}k_2 \big) \bigg] \\ P_4 = iqT_1 \frac{\big(1 - e^{-st_0} \big)}{t_0 s^2} \bigg[L_{11}k_1 \big(\ell_{23}k_3 - \ell_{22}k_2 \big) + L_{12}k_2 \big(\ell_{21}k_1 - \ell_{23}k_3 \big) \\ &+ L_{14}k_4 \big(\ell_{21}k_1 - \ell_{22}k_2 \big) \bigg] \\ P_4 = iqT_1 \frac{\big(1 - e^{-st_0} \big)}{t_0 s^2} \bigg[L_{11}k_1 \big(\ell_{23}k_3 - \ell_{22}k_2 \big) + L_{12}k_2 \big(\ell_{21}k_1 - \ell_{23}k_3 \big) \\ &+ L_{13}k_3 \big(\ell_{22}k_2 - \ell_{21}k_1 \big) \bigg] \\ L_{1i} = k_i \big(k_i - iq\ell_{1i} \big), \qquad i = 1, 2, 3, 4 \end{split}$$

5. Particular Cases

i- If m = 0, in Eqs. (52)–(61), we obtain the components of displacements and tresses in magneto-micropolar generalized thermoelastic with rotating medium without Hall current effect.

ii- Taking Hartmann number M = 0, in Eqs. (52)–(61), we obtain the components of displacements and tresses in micropolar generalized thermoelastic with rotating medium.

iii. If the effect of rotation is absent ($\Omega = 0$), in Eqs. (52)–(61), we obtain the components of displacements and stresses in micropolar generalized thermoelastic medium with the following changed values of δ_1 , δ_3 , δ_4 , and δ_6 as

$$\delta_1 = \frac{s\rho c_o^2}{\lambda + 2\mu + k} \left(s\tau_o + \frac{M}{1 + m^2} \right) + q^2,$$

$$\delta_3 = \frac{\rho c_o^2 smM}{(\lambda + 2\mu + k)(1 + m^2)}$$

$$\delta_4 = \frac{s\rho c_o^2}{\mu + k} \left(s\tau_o + \frac{M}{1 + m^2} \right) + q^2$$

$$\delta_6 = \frac{s\rho c_o^2 Mm}{(\mu + k)(1 + m^2)}$$

iv. Taking $n_0 = 1$, $\tau_o > 0$, $\nu = 0$ in Eqs. (52)–(61), we obtain the corresponding expressions for magneto-micropolar thermoelastic with rotating for L–S theory.

v. Taking $n_0 = 0$, $\tau_o > 0$, $\nu > 0$ in Eqs. (52)–(61), we obtain the corresponding expressions for magneto-micropolar thermoelastic with rotating for G–L theory.

vi. Taking, $n_0 = 0$, $\tau_{o=} 0$, v= 0 we obtain the corresponding expressions for magneto-micropolar coupled thermoelastic with rotating medium for (C–T theory

6. Inversion of the Transforms

To obtain the solution of the problem in the physical domain (x,y, t), we have to invert the iterated transforms in Eqs. (52)–(61). These expressions can be formally expressed as functions of x and the parameter of the Fourier and Laplace transforms q and s of the form $\overline{f}^*(x,q,s)$.

First, we invert the Fourier transform using the inversion formula given previously. This gives the Laplace transform expression $\overline{f}(x,q,s)$ of the function f(x,y,t) as

$$\overline{f}(x,q,t) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} e^{-iqy} f(x,q,s) dq$$
$$= \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} (\cos(qy) f_e + i\sin(qy) f_o) dq$$

where f_e and f_o denote the even and the odd parts of the function $\overline{f}^*(x, q, s)$ respectively.

We shall now outline the numerical inversion method used to find the solution in the physical domain. For fixed values of x, y, and q the function inside braces in the last integral can be considered as a Laplace transform $\overline{g}(s)$ of some function g(t).

The inversion formula for the Laplace transform can be written as

$$g(t) = \frac{1}{2\pi i} \int_{c-i\infty}^{c+i\infty} e^{st} \overline{g}(s) ds$$

where c is an arbitrary real number greater than all the parts of the singularities $\overline{g}(s)$. Taking s = c + iy, the above integral takes the form

$$g(t) = \frac{e^{ct}}{2\pi} \int_{-\infty}^{\infty} e^{iyt} \,\overline{g}(c+iy) \, dy$$

Expanding the function $h(t) = \exp(-ct)g(t)$ in a Fourier series in the interval[0, 2L], we obtain the approximate formula.

$$g(t) = g_{\infty}(t) + E_D$$

where

$$g_{\infty}(t) = \frac{1}{2}c_o + \sum_{k=1}^{\infty} c_k \quad for \ 0 \le t \le 2L$$
 (62)

and

$$c_k = \frac{e^{ct}}{L} \operatorname{Re} \left[e^{ik\pi t/L} g\left(c + ik\pi t/L\right) \right]$$
(63)

 E_D , the discretization error, can be made arbitrary small by choosing c large enough.

Since the infinite series in Eq. (62) can be summed up to finite number N of terms, the approximate value of g(t) becomes

$$g_N(t) = \frac{1}{2}c_o + \sum_{k=1}^N c_k \quad for \ 0 \le t \le 2L \quad (64)$$

Using the above formula to evaluate g(t), we introduce a truncation error E_T which, must be added to the discretization error to produce the total approximation error.

Two methods are used to reduce the total error. First the "Korrecktur" method is used to reduce the discretization error. Next, the e algorithm is used to reduce the truncation error and hence to accelerate convergence.

The Korrecktur method uses the following formula to evaluate the function g(t):

$$g(t) = g_{\infty}(t) - e^{2cL}g_{\infty}(2L+t) + E'_D$$

where the discretization error $|E'_D| \ll |E_D|$. Thus, the approximate value of g(t) becomes

$$g_{NK}(t) = g_N(t) - e^{2cL}g_{N'}(2L+t)$$
(65)
N' is an integer such that N' < N.

We shall now describe the e-algorithm that is used to accelerate the convergence of the series in Eq. (64).

Let N = 2q + 1 where q is a natural number, and let

$$s_m = \sum_{k=1}^m c_k$$

be the sequence of partial sums of Eq. (64). We define the e-sequence by

$$\varepsilon_{o,m} = 0, \qquad \varepsilon_{1,m} = 0$$

and

$$\varepsilon_{p+1,m} = \frac{\varepsilon_{p-1,m+1}+1}{\varepsilon_{p,m+1}-\varepsilon_{p,m}}, \qquad p = 1,2,3,\dots$$

it can be shown that the sequence $\varepsilon_{1,1}$, $\varepsilon_{3,1}$, $\varepsilon_{5,1}$, ..., $\varepsilon_{N,1}$, converges to $f(x,y,t) + ED - c_0/2$ faster than the sequence of partial sums s_m (m = 1,2,3,...).

The actual procedure used to invert the Laplace transform consists of using Eq. (65) together with the ε -algorithm. The values of c and L are chosen according to the criteria outlined Honig and Hirdes[24].

7. Numerical Results and Discussion

The analysis is conducted for a magnesium crystal-like material. Following reference[25], the values of physical constants are

$$\begin{split} \lambda &= 9.4 \times 10^{10} \text{ Nm}^{-2}, \, \mu &= 4.0 \times 10^{10} \text{ Nm}^{-2}, \, k = 1.0 \times 10^{10} \text{ Nm}^{-2}, \\ \rho &= 1.74 \times 10^3 \text{ gm/cm}^3, \, \gamma &= 0.779 \times 10^{-9} \text{N}, \, j &= 0.2 \times 10^{-15} \text{ cm}^2, \\ c_E &= 1.04 \times 10^3 \text{ kgm}^{-3}, \, K^* &= 1.7 \times 10^2 \text{ Jm}^{-1} \text{s}^{-1} \text{deg}^{-1}, \, T_o &= 298 \text{ K}, \\ \nu &= 3.68 \times 10^6 \text{Nm}^{-21} \text{deg}^{-1}, \, \tau_o &= 0.02, \, n_o &= 0.05. \end{split}$$

we consider the following electric constants for our problem

 $\sigma_0 = 9.36 \times 10^5 \text{Col}^2/\text{Cal.cm.sec}, \text{ H}_0 = 10^5 \text{ Col/cm.sec}$

The computations are carried out for the non-dimensional time t=0.1, strip width a= 0.9×10^3 and rotation Ω =2and on the surface plane z=0. The distribution of non-dimensional transverse displacement u, non-dimensional normal displacement w, non-dimensional normal force stress σ_{zz} , non-dimensional tangential couple stress m_{zy} , non-dimensional temperature distribution T non-dimensional current density j_x and j_z non-dimensional distance x have been shown in Figs. 1–7.

The solid line represent magneto-micropolar generalized thermoelastic with Hall current effect and rotating medium MMGT(HR) and large dashes line represent magneto-micropolar generalized thermoelastic with Hall current effect MMGT(H), while small dashes line represent magneto-micropolar generalized thermoelastic in rotating medium without Hall current effect MMGT(R). The dot line represent magneto-micropolar generalized thermoelastic without Hall current effect and rotating medium MMGT.

Fig.1 Studying the effect of Hall parameter m on the temperature distribution against y for, from this figure we



Figure 1. Variation of temperature with the Hall parameter m

see that the all curves start from the same value 1 at x=0.0 then decreases till it tends to zero at x = 2, we observe that from this figure the temperature T decrease in the case MMGT(HR) in comparison to curve MMGT(R), while increases in comparison to curves MMGT and MMGT(H). The effect of parameter m on the transverse displacement u is presented in Fig. 2.It is noticed that from the graphic representation of the transverse displacement that the values are oscillatory for all the cases in the whole range and the values of u remain higher near the boundary condition in

magnitude for case MMGT(HR) as compared with the values for all cases and then increases. Fig. 3 describes the variations of the normal displacement w under the effect of all parameters, it is noticed that the normal displacement w records values lower in case MMGT(HR) as compared with the values for all cases. It is shown in Fig. 4 that the values of normal force stress for MMGT(H) and MMGT lie in a very short range. The variation for all cases being oscillatory in nature are comparable in magnitude and the magnitude of these oscillations decrease with increase in horizontal distance x. Fig. 5 shows that the Variation of couple stress m_{yz} decreases as m increases MMGT(HR). The figure indicate that m_{yz} records values higher in case MMGT(H) and all cases oscillations about y-axes.



Figure 2. Variation of transverse displacement with the Hall parameter m



Figure 3. Variation of normal displacement with the Hall parameter m



Figure 4. Variation of normal force stress with the Hall parameter m





Figure 6. Variation of current density component $\boldsymbol{J}_{\boldsymbol{x}}$ with the Hall parameter \boldsymbol{m}



Figure 7. Variation of current density component J_z with the Hall parameter m

Figs. 6, 7 describe the variations of two components of density component J_x and J_z respectively, it is evident that the values of both fields are decreased in the MMGT(HR) as compared with the values for cases MMGT and MMGT(H).

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