Effects of high-energy particle showers on the embedded front-end electronics of an electromagnetic calorimeter for a future lepton collider

The CALICE Collaboration

Abstract

Application Specific Integrated Circuits, ASICs, similar to those envisaged for the readout electronics of the central calorimeters of detectors for a future lepton collider have been exposed to high-energy electromagnetic showers. A salient feature of these calorimeters is that the readout electronics will be embedded into the calorimeter layers. In this article it is shown that interactions of shower particles in the volume of the readout electronics do not alter the noise pattern of the ASICs. No signal at or above the MIP level has been observed during the exposure. The upper limit at the 95% confidence level on the frequency of fake signals is smaller than $1\cdot 10^{-5}$ for a noise threshold of about 60% of a MIP. For ASICs with similar design to those which were tested, it can thus be largely excluded that the embedding of the electronics into the calorimeter layers compromises the performance of the calorimeters.

Keywords: Lepton collider; electromagnetic calorimeter; embedded electronics; fake hits

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38 1 Introduction

The central calorimeters of the detectors to be operated at a future lepton collider will have the readout electronics embedded into the active layers of the calorimeter [1, 2, 3]. The energy of electromagnetic showers produced in the final states ranges between a few MeV up to several hundreds of GeV. A natural question arising from this design is whether the cascade particles of the high-energy showers which penetrate through the electronics do create radiation induced effects in these circuits. These effects would compromise the precision measurements envisaged at the lepton collider. Possible radiation effects include Transient Effects and Single Event Upsets [4] which may create pulses which would be recorded as fake signals or, even worse, could cause damage to the readout electronics.

The CALICE collaboration is designing, building and operating large scale prototypes for the calorimeters at a future lepton collider [5]. Large statistics data samples have been recorded in test beam campaigns in order to understand the behaviour of highly granular calorimeters. This article describes the measurements conducted in a special set of runs in which an ordinary calorimeter layer of a prototype for a silicon tungsten electromagnetic calorimeter, called SiW Ecal hereafter, has been replaced by a special PCB allowing for the exposure of the readout electronics to particle showers. The data analysed here were recorded during the 2007 test beam campaign at CERN in the H6 test beam area

116 2 Experimental set-up and data taking

Figure 1 shows a perspective view on the *physics prototype* of the SiW Ecal. A comprehensive description of the physics prototype is given elsewhere [6]. Here only those features relevant for the present analysis will be outlined.

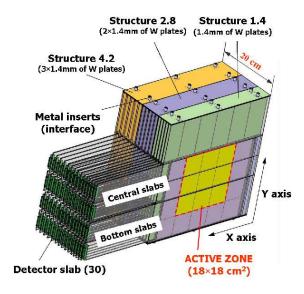


Figure 1: Schematic 3D view of the physics prototype.

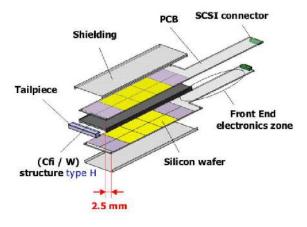


Figure 2: Schematic diagram showing the components of a detector slab.

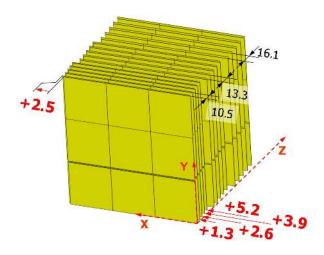


Figure 3: Illustration of layer offsets $(2.5 \,\mathrm{mm})$ and slabs offsets $(1.3 \,\mathrm{mm})$ of the physics prototype of the SiW Ecal as discussed in the text. Shown is also the total extension of the three modules in z-direction. All dimensions are in mm.

The physics prototype consists of 9720 $1x1 \, \mathrm{cm}^2$ wide calorimeter cells subdivided into 30 layers. The active zone covers $18 \times 18 \, \mathrm{cm}^2$ in width and approximately 20 cm in depth. The layers are composed alternately by W absorber plates and a matrix of PIN diode sensors on a silicon wafer substrate. At normal incidence, the prototype has a total depth of $24 \, X_0$ achieved using 10 layers of $0.4 \, X_0$ tungsten absorber plates, followed by 10 layers of $0.8 \, X_0$, and another 10 layers of $1.2 \, X_0$ thick plates. Each layer is subdivided into a central part featuring a 3×2 array of silicon wafers and a bottom part consisting of a 3×1 array of silicon wafers. Note that in the running period relevant for this analysis the bottom part of the first six layers was missing.

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The silicon wafers are mounted onto both sides of an H-shaped tungsten plate as shown in Figure 2. Such an entity is called a slab. In order to avoid an alignment of wafer boundaries, the layers within a slab are shifted by 2.5 mm in the positive x-direction with respect to each other. In the same way, two successive slabs are shifted by 1.3 mm with respect to each other. The layer offsets are illustrated in Figure 3.

As indicated in Figures 1 and 2, the readout electronics are located outside the absorber 134 structure and hence not exposed to high-energy electromagnetic showers. The main device 135 of the read out electronics is an 18 channel charge sensitive ASIC, called FLC_PHY3 which 136 is realised in 0.8 μ m AMS BiCMOS technology. One 6×6 sensor matrix is thus read out 137 by two ASICs. This provides redundancy by de-correlating ASIC and sensor response. As shown in Figure 4, the signal path starts with a variable gain charge preamplifier, followed 139 by two shaping filters for gains 1 and 10 with a shaping time of 180 ns for both gains. The 140 shaped signal is then propagated to a sample and hold device realised by a 2 pF capacitance. 141 After that the measured voltage, which is proportional to the charge at the input of the pre-amplifier, is written into a buffer designed to store the 18 signals as processed by the signal chain. The 18 signals are read one-by-one by the off-detector electronics. One channel covers a dynamic range equivalent to the energy deposition by about 600 Minimum Ionising Particles, MIPs, which has been considered to be sufficient for a beam test using primary electrons of an energy of up to 50 GeV.

For the present tests, FLC_PHY3 ASICs were exposed to electromagnetic showers. One ASIC has a surface of about $1.6 \times 2.3 \,\mathrm{mm^2}$. It is TQFP64 packaged such that the whole ensemble has outer dimensions of about $1 \times 1 \,\mathrm{cm^2}$ [7]. The shower particles may create charges and thus fake signals in the PMOS at the entrance of the pre-amplifiers of the 18 channels. The sensitive area of one channel is about $3000 \,\mathrm{\mu m^2}$ while the total surface of a channel is about $110000 \,\mathrm{\mu m^2}$. Signals created in the circuitry after the pre-amplifier which would appear immediately at the output of the ASIC cannot be recorded due to the sampling latency of 180 ns of the CALICE data acquisition system. Radiation effects could therefore only become apparent in case of a failure of the circuitry. Such a failure has not been observed during the tests presented in this article.

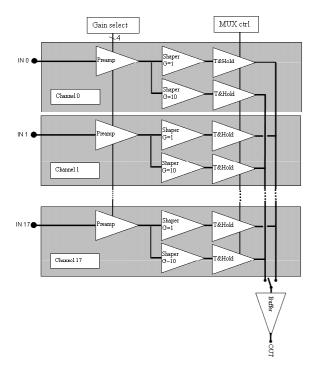


Figure 4: General block schematic of FLC_PHY3.

The special PCB is equipped with four ASICs in the nominal sensitive plane of the detector. It has been mounted directly on a spare H-board as shown in Figure 5. The special PCB has been placed within the physics prototype at the layer corresponding to the expected position of the shower maximum. In this configuration data with electrons with an energy of $70 \,\text{GeV}$ and $90 \,\text{GeV}$ have been recorded. The lateral spread of the electron beam at these energies is about 1 cm in diameter [6]. The beam has been positioned at five different points along the x-direction at the centre in y of each of the four ASICs as indicated for the 'ASIC 1' in Figure 6. Beam events triggered with scintillation counters, called $signal\ events$ hereafter, are interleaved during the data taking with $pedestal\ events$ triggered by an oscillator integrated

into the CALICE data acquisition system. For further details of the experimental set-up please consult [6, 8, 9]. Table 1 gives the number of recorded signal and pedestal events at each measurement point. The table also introduces the nomenclature used hereafter to identify the various measurement points.

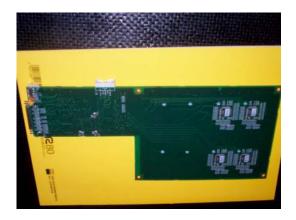




Figure 5: Left: Picture of the special PCB with the four ASICs used in the test. Right: The special PCB mounted on tungsten absorber and comparison with a regular slab.

171 3 Initial steps of data analysis

The data are verified for a proper alignment of the ASICs relative to the beam in lateral 172 direction and to the shower maximum in longitudinal direction. Figure 7 shows the spectra 173 of a run with electrons of 90 GeV. Here, the recorded data were reconstructed with the same 174 reconstruction chain as applied to the regular data taking [6, 8]. The energy deposition in 175 the detector is given in terms of MIPs and 1 MIP corresponds to about 45 ADC counts [6] 176 as recorded by the CALICE data acquisition system. The reconstruction chain introduces a zero suppression at 0.6 MIP corresponding to approximately 4.5 times the mean noise level 178 of 6 ADC counts. In addition, a correction for pedestal instabilities caused by insufficient 179 isolation of the power supply lines of the PCBs is applied [6]. After this correction the residual 180 pedestal instability is about 0.2% of a MIP (or 0.1 ADC counts). 181

The total energy spectrum exhibits a clear maximum well separated from residual noise and MIP events. The gap visible in the longitudinal shower profile indicates that the special

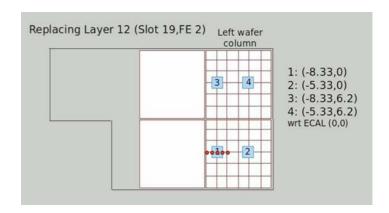


Figure 6: Schematic view of the special PCB. The red points indicate the nominal five impact points for a scan over ASIC 1. Identical scans have been performed for the other three ASICs.

layer has been placed close to the shower maximum. The lateral position of the special PCB, installed at the position of Layer 12, is identical to that of the Layer 2 of the prototype. As an example, Figure 8 shows the hit maps of layers 2 and 14 for a run in which the beam was incident on ASIC 4. The Layer 14 is the first regular layer behind the special PCB. Overlaid to the hit maps is the projected position of ASIC 4. The gaps in the lower parts of the hit maps can be explained by non-instrumented parts of the detector.

190 It is clearly visible that the beam hits the detector close to the ASIC position and that 191 the lateral shower development leads to a good coverage and thus good exposure to shower 192 particles of the ASIC.

In a next step the regular zero suppression was switched off in the CALICE reconstruction 193 program in order to be sensitive to the behaviour of the ASICs in the small signal range. For 194 technical reasons the first channel of each ASIC on the special PCB is discarded, leaving 17 195 signals per ASIC per event. As motivated by the energy spectrum shown in Figure 7, the 196 signal events are further selected by requiring an energy deposition of more than 2000 MIPs 197 in order to be unbiased by MIP-like events. This cut reduces the available statistics quoted 198 in Table 1 by approximately 15%. Still, no difference between the noise spectra obtained 199 for signal and pedestal events is expected. As an example, in Figure 9 the noise spectra of signal and pedestal events are compared the Measurement point 3 of Scan 4. Indeed, 201 no difference between the two data types can be observed. After this initial qualitative 202 comparison, the mean and the root mean square (RMS) for each ASIC at each measurement 203 point are extracted for signal and pedestal events. The results are displayed in Figure 10, 204 using the scan over ASIC 1 as an example. 205

The corresponding figures for the other scans are given in the appendix. From these figures the following conclusions can be drawn:

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- The mean and the RMS remain the same throughout all the runs. In particular no dependence on the scan position can be observed.
- The mean and RMS for signal and pedestal events are always nearly identical. Residual

Scan	Beam centred on	Measurement point	Position: x,y [cm]	Signal events	Pedestal events
		1	-9.33, 0	78293	14624
	1 ASIC 1	2	-8.83, 0	189966	37173
1		3	-8.33, 0	209312	38361
		4	-7.83, 0	65249	3602
		5	-7.33, 0	85543	4306
		1	-6.33, 0	85188	4678
		2	-5.83, 0	129778	6146
2	2 ASIC 2	3	-5.33, 0	213369	13719
		4	-4.83, 0	217111	11053
		5	-4.33, 0	89435	4254
		1	-9.33, 6.2	90395	4347
		2	-8.83, 6.2	228138	10296
3	ASIC 3	3	-8.33, 6.2	216877	9831
		4	-7.83, 6.2	218519	9462
		5	-7.33, 6.2	86989	3909
		1	-6.33, 6.2	66655	4223
	ASIC 4	2	-5.83, 6.2	214418	13666
4		3	-5.33, 6.2	314275	15264
		4	-4.83, 6.2	217415	11698
		5	-4.33, 6.2	85884	4949

Table 1: Protocol of the exposure test containing the identifiers of the measurement points, their position and the number of signal and pedestal events recorded at each position.

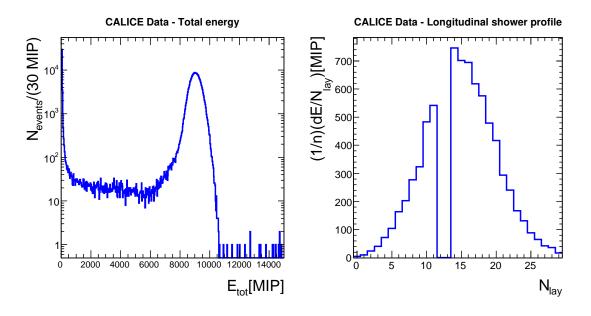


Figure 7: Total energy deposition and longitudinal shower profile for a run with electrons of 90 GeV during the test with the special PCB. The gap visible in the longitudinal shower profile is due to the replacement of a regular slab by the H-board carrying the special PCB.

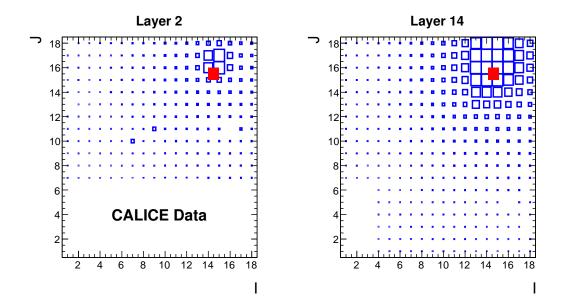


Figure 8: Hit maps shown as a function of the cell indices I, J in x and y-directions in layer 2 and 14. The area of the boxes represents the number of recorded hits in the individual cells. The position of ASIC 4, indicated by the full square, is projected into the planes of these layers.

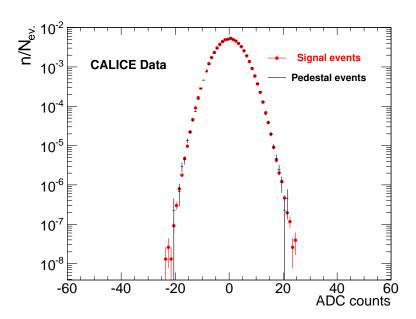


Figure 9: Noise spectrum for signal events and pedestal events. The figure displays the result for the run in which the beam was centred on ASIC 4. The distributions are normalised to unity.

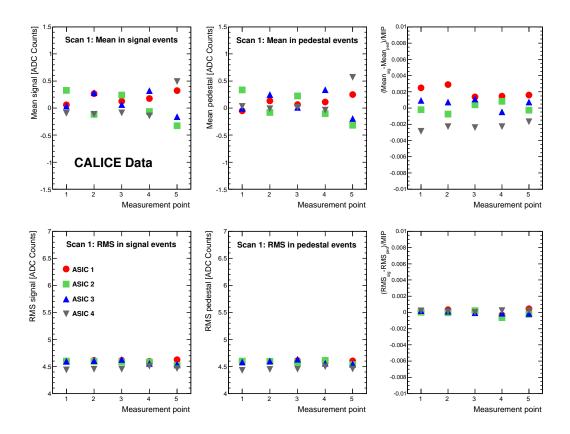


Figure 10: Mean and RMS for signal events and pedestal events. The very right part shows the corresponding differences normalised to the value of a MIP assumed to be 45 ADC counts. The figure displays the result for Scan 1 in which ASIC 1 is scanned. As a cross-check the results for all ASICs are shown.

differences are smaller than 0.4% of a MIP.

212 4 Detailed noise analysis

The high-energy showers penetrating the electronics may disturb the noise characteristics of the exposed ASICs. This perturbation may be revealed in changes of the coherent and incoherent noise levels of the ASICs. A very robust and widely used technique to analyse noise patterns in data is given by a *Principal Component Analysis (PCA)*. The analysis performed in this paper follows that presented in [10]. As was pointed out there and confirmed in present study, the PCA leads to more reliable results than a more simplistic approach based on direct and alternating sums.

4.1 Principal Component Analysis - PCA

The PCA can be subdivided into five steps which are introduced now. Each step will be illustrated by the results obtained for nominal central impact on the ASICs.

1. The vector of noise hits **b** for a given ASIC can be decomposed into

$$\mathbf{b} = \mathbf{u} + c\boldsymbol{\alpha},\tag{1}$$

where **u** represents the contribution of the incoherent noise. The vector α characterises the correlation among the ASICs. More specifically, its components quantify the relative contributions of the individual channels to the coherent noise. The scalar parameter c characterises the level of the coherent noise in a given event.

2. From this, the noise covariance matrix can be built as

$$B = \sigma^2 \mathbf{1} + \sigma_c^2 \alpha \alpha^T, \tag{2}$$

with $\langle u_i u_j \rangle = \sigma^2 \delta_{ij}$ being the incoherent noise squared, **1** the unit matrix and σ_c^2 being the variance of the c-parameter introduced before.

3. The vector α is the eigenvector of B with the largest eigenvalue given by $\omega_1 = \sigma^2 + \sigma_c^2$. In case of only one source of coherent noise, any other eigenvector orthogonal to α should have the eigenvalue σ^2 . In this model, the spectrum of eigenvalues is expected to be flat except for one eigenvalue from which the coherent noise can be derived. The Figure 11 shows the spectra of eigenvalues obtained for the four ASICs. The variance of the coherent noise σ_c^2 of the ASICs can be deduced from the largest eigenvalues and another one chosen from the flat parts of the spectra, which is reasonably fulfilled starting from Rank = 9. The eigenvalues at that rank are defined as σ^2 . The errors on the eigenvalues shown in the figure are derived according to the following plausibility consideration. According to [11] the eigenvalues are bounded by

$$\lambda_n + \sigma^2 b_- \le \omega_n \le \lambda_n + \sigma^2 b_+ \tag{3}$$

with $b_{\pm} = (1 \pm \sqrt{T/N})^2$ where T is the number of sources, here the ASIC channels, and N is the number of events. The λ_n are the true variances of the coherent noise where $\lambda_1 = \sigma_c^2$ in this analysis. The bounds span a range $\sigma^2(b_+ - b_-)$. For one source, i.e. T = 1, this agrees with the statistical error of the variance multiplied by a factor $\sqrt{2}$. Thus, to obtain the statistical error of the eigenvalues, the range of the bounds is calculated and divided by $\sqrt{2}$.

After these considerations, it can be concluded that the eigenvalues for the two event types agree within statistical errors, which is particularly true for the largest one which carries the information on the coherent noise.

Figure 12 shows the eigenvectors, normalised to unity, associated with the highest eigenvalue obtained in the same scan for signal and pedestal events. In some cases the eigenvectors feature the opposite sign. In that case also the reflected vector is given in the figure. This sign ambiguity of PCA is reported also in the literature, e.g. [12], and

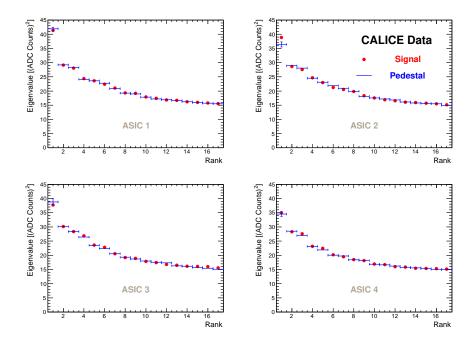


Figure 11: Eigenvalues as obtained in a Principal Component Analysis of signal and pedestal events for nominal central impact on the ASICs. The eigenvalues are ordered in decreasing order. The statistical error is given for the largest eigenvalue of the pedestal events.

constitutes no hint of an inconsistency. The eigenvectors are thus in good agreement for signal and pedestal events.

A representation of the coherent channel noise can now be achieved by multiplying the variance, σ_c^2 , with the component squared of the corresponding eigenvalue. The coherent noise is shown in Figure 13.

It is clearly visible that for ASIC 1 and ASIC 3 the coherent noise is concentrated around the central channel numbers. The source of the coherent noise is not known but with a value of maximal 5 (ADC counts)², see Figure 13, it is much smaller than the variance of the incoherent noise of about 20 (ADC counts)², see next step. There is no evidence that the observed coherent noise is different for signal and pedestal events.

4. The incoherent noise per channel can be obtained from the deflated matrix

$$B' = B - \sigma_c^2 \alpha \alpha^T. \tag{4}$$

In this matrix the off-diagonal elements are flat around a null value. The diagonal elements, however, can be interpreted as the channel independent incoherent channel noise squared. The matrices obtained upon central impact on the ASICs in signal events are displayed in Figure 14. As expected, they feature dominant diagonal elements.

For confirmation, the diagonal elements are displayed separately in Figure 15. As already mentioned above their values are around $20 \, (\mathrm{ADC} \, \mathrm{counts})^2$ and channel independent.

In Section 5 the incoherent channel noise will be employed in the noise simulation of the ASICs.

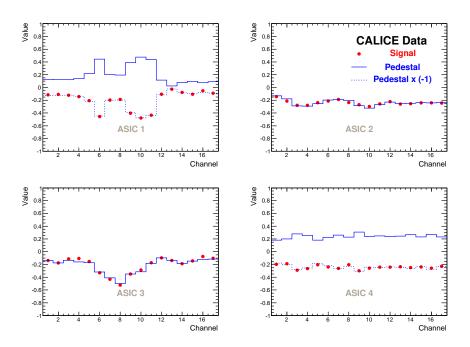


Figure 12: Eigenvectors associated to the largest eigenvalues as obtained in a Principal Component Analysis of signal and pedestal events for nominal central impact on the ASICs. These eigenvectors indicate the location of coherent noise within the ASICs. In case of a sign flip between the eigenvectors for signal and pedestal events, the reflected eigenvector for pedestal events is indicated, too.

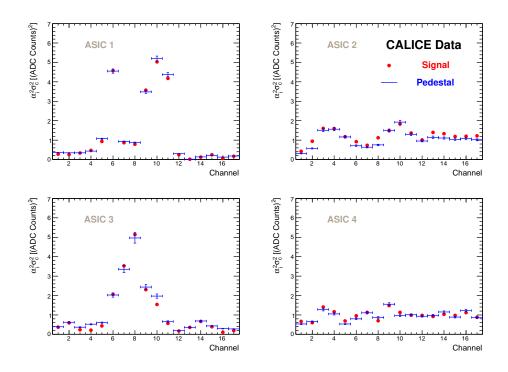


Figure 13: Level of coherent noise in the four ASICs.

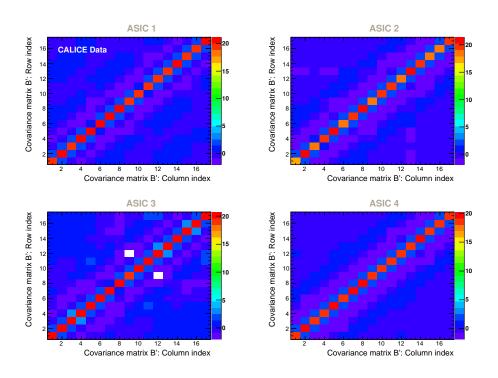


Figure 14: Deflated matrix B' for the four ASICs as obtained in a Principal Component Analysis for nominal central impact on the ASICs. Here, the matrices are shown for signal events. The colour represents the value of the matrix element in units of (ADC counts)².

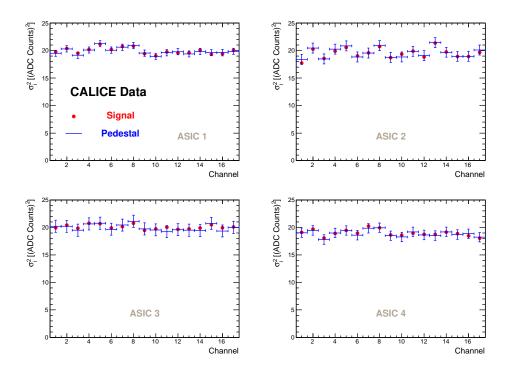


Figure 15: Level of incoherent noise in the four ASICs.

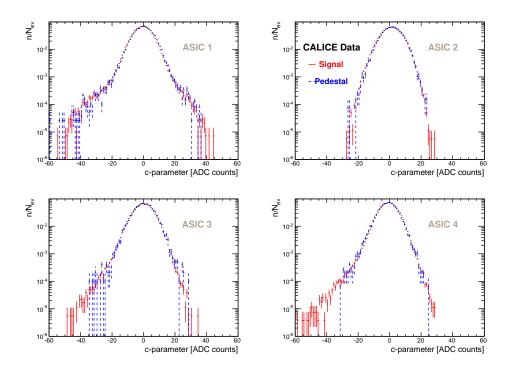


Figure 16: Spectra of the c-parameter as obtained for nominal central impact on the four ASICs for signal and pedestal events. See text for the definition of the c-parameter. The histograms are normalised to unity.

5. Since all channels of an ASIC can be assumed to be equal, the variance $\sum u_i^2$ reaches a minimum. Thus, the c-parameter can be estimated by requiring the quantity $\sum (b_i - \alpha_i)^2$ to be minimal. From this it follows that

$$c = \boldsymbol{\alpha} \cdot \mathbf{b}. \tag{5}$$

Using this, the coherent noise could be estimated and subtracted on an event-by-event basis. In this analysis the knowledge of the c-parameter together with other noise quantities will be exploited to simulate the noise of the ASICs. The c-parameter spectra for the four ASICs are given in Figure 16.

Again the spectra are very similar for signal and pedestal events. Since the statistics of the signal events are considerably larger than those of the pedestal events, the tails reach larger values.

The PCA allows for the conclusion that the presence of shower particles has no significant influence on noise pattern of the ASICs. In addition, it indicates that, in a yet more quantitative study, the pedestal events can be used to model the noise pattern in the signal events. This will be done in the following section.

5 Limits determination

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This section is dedicated to the determination of upper limits for having shower-induced fake 289 hits above a given threshold. As a first result it can be reported that no signal above a MIP is observed in the signal and the pedestal events, such that the upper limit on the probability 291 that shower particles induce a fake signal at the MIP level can be set to $6.7 \cdot 10^{-7}$ at the 95% confidence level. This number is derived from the run with the highest statistics listed in 293 Table 1. In the remainder of this section, this result is extended towards smaller thresholds. 294 As it is rather expected that the shower induces fake signals towards small ADC counts, the threshold is varied between 15 and 30 ADC counts, which corresponds to about 1/3 to 2/3 of the signal created by a MIP. This covers the region of noise cuts studied in [8] and allows for the investigation of the influence of the particle shower towards smallest ADC values. 298 Values smaller than 15 ADC counts have been discarded as these show a large sensitivity to 299 the residual pedestal instabilities. 300

Limits on signals in the presence of background

The comparatively small ADC values require the determination of the upper limits in the presence of background given by the intrinsic noise of the ASICs. In this case, the Poissonian probability density function f' for observing n events based on a sample statistics k is given by [13]:

$$f'(n; \lambda_S + \lambda_B) = f(n; \lambda_S + \lambda_B) / \sum_{n_B = 0}^{k} f(n_B; \lambda_B).$$
 (6)

Here, λ_S and λ_B are the Poisonnian parameters for Signal and Background, respectively. The probability density function $f(n; \lambda_S + \lambda_B)$ is the sum of the independent Poissonian distributions for signal and background to the Poissonian parameter $\lambda = \lambda_S + \lambda_B$. The probability distribution function in the denominator of Equation 6 ensures that f' is normalised to 1 for background only events. The sum runs over the possible number of background events, n_B , up to the sample statistics k. The probability distribution function to the probability density in Equation 6 reads

$$F'(\mathbf{k}; \lambda_S + \lambda_B) = \sum_{n=0}^{\mathbf{k}-1} f'(n; \lambda_S + \lambda_B) = P(\ell < \mathbf{k}), \tag{7}$$

where $P(\ell < k)$ is the probability to observe any number $\ell < k$. The upper limit $\lambda_S^{(up)}$ for signal events at the confidence level $\beta = 1 - \alpha$ can then be obtained from

$$\alpha = F'(\mathbf{k} + 1; \lambda_S^{(up)} + \lambda_B) \tag{8}$$

in case the background is known.

As there is no indication that the high-energy showers influence the ASIC response, the limits will be derived for those four measurement points in which the beam was incident on the nominal centre of one of the ASICs. The background expectation will be obtained from simulated events.

5.1 Noise simulation

The simulation of the noise starts out from the noise vector given in Equation 1. 321 incoherent noise is thus simulated using a Gaussian $G(x_m, \sigma_i)$ with the σ_i of the individual 322 ASIC-channels read off from the matrices given in Equation 2. The mean x_m of the Gaussian 323 is given by the mean measured in the pedestal events in a given run. The part covering 324 the coherent noise is realised by simulating the c-parameter spectrum and by multiplying 325 this spectrum with the corresponding component α_i of the eigenvector of a given ASIC. Figure 16 illustrates that the c-parameter spectrum cannot be approximated by a simple 327 Gaussian. Rather, it is simulated using an adaptive kernel estimation introduced in [14]. 328 Here, the kernel estimation which corresponds to the implementation in the RooFit package 329 is employed. The formula used to simulate the noise spectrum S'_i for a channel i thus reads 330

$$S_i' = G(x_m, \sigma_i) + (sign)K(c)\alpha_i. \tag{9}$$

The symbol K(c) describes the kernel estimation introduced before. The sign is given by the scalar product of the eigenvectors obtained for the signal events and pedestal events. The first aim of the simulation is to reproduce the measured pedestal spectra in this paper. Here and in the following it is ensured that the number of simulated events is at least 2.5 times larger than the number of measured events. Thus the statistical error of the simulation is smaller than that of the data. In order to obtain a maximal level of agreement between the simulated and the measured pedestal spectra, two free parameters are added to the Equation 9 leading to:

$$S_i = G(x_m - p_m, \sqrt{\sigma_i^2 - p_\sigma}) + (sign)K(c)\alpha_i.$$
(10)

These free parameters are used to account for residual off-diagonal elements in the matrices 339 of Equation 2. In addition, they account for imperfections caused by the loss of information 340 in using only the eigenvector with the largest eigenvalue. The free parameters are tuned 341 until a minimum χ^2/ndf is obtained upon comparing the spectra of the pedestal events with 342 the simulated ones. The range of values of the free parameters are $p_m = [-0.33, 0.25]$ and $p_{\sigma} = [1.1, 2.0]$. A comparison between the measured pedestal spectrum of ASIC 1 for Scan 1 and measurement point 3 is given in Figure 17. An excellent agreement between data and 345 simulation is achieved. The resulting χ^2/ndf as a function of the ASIC number for all runs 346 with central impact on one of the ASICs is shown in Figure 18. 347

Inspired by the work presented in [15], the number of hits in the simulated spectra are subject to a final correction. For each bin the inverse error function is calculated according to

$$e(\Delta x, \sigma) = \left[1 - erf\left(\frac{\Delta x}{2\sqrt{2}\sigma_b}\right)\right] \cdot \Delta x. \tag{11}$$

Here, Δx is the difference between simulation and pedestal events and σ_b is the statistical uncertainty of the data in that bin. This correction aims to balance out residual imperfections of the simulation without being too sensitive to statistical fluctuations appearing in the tails of the spectra of the pedestal events. After this final correction, the number of hits above a

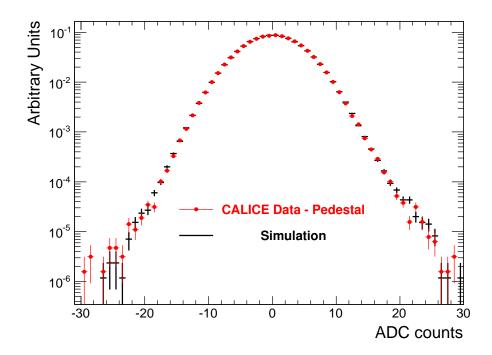


Figure 17: Comparison between the measured and simulated pedestal spectrum at the example of ASIC 1 in Scan 1 and measurement point 3. The details of the simulation are explained in the text.

given threshold in pedestal events is compared for data and simulation. The comparisons are made separately for negative and positive ADC counts and are shown in Figures 19 and 20. The error on the data is given by the 97.3% confidence interval around the measured number of hits. Towards large numbers of hits, this corresponds to the 3σ confidence interval. This interval is chosen since due to the complexity of the noise spectra not all potential effects are incorporated in the simulation. Systematic uncertainties of the noise modelling can be estimated from the spread of the simulated distributions of the four ASICs, which should in principle be identical. Data and simulation agree within the chosen confidence limit where the agreement is better for negative ADC counts. The agreement achieved validates the model for making reliable predictions of the expected number of events in signal events.

The comparison of the simulated spectra with those measured in the signal events is made in Figures 21 and 22. Data and simulation are still compatible. For most of the data points the agreement is within the chosen confidence interval. The deviations may not be attributed to the actual beam exposure since they occur in their majority for ASICs outside the actual electromagnetic shower. The agreement is worse towards smaller ADC values while towards large ADC values data and simulation agree within the chosen limits. The former discussion indicates that there is no measurable influence of the beam on the ASIC response. Therefore, in the following the upper limits on the frequency of fake hits are determined.

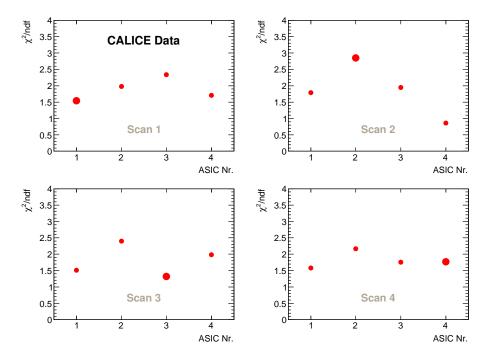


Figure 18: Resulting χ^2/ndf of the comparison between the measured and simulated pedestal spectra. The comparisons are made for the measurement points 3 in the scans, see Table 1. The ASIC which is actually exposed to the beam is indicated by a larger symbol. The ASIC number is given on the x-axis of the graph.

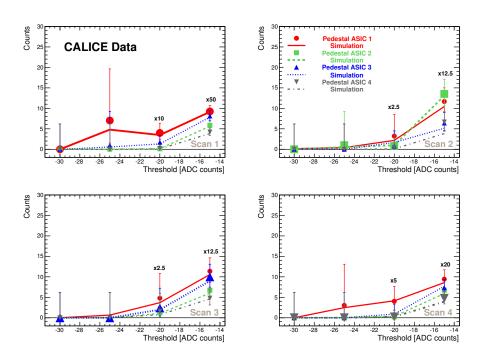


Figure 19: The measured counts below a threshold in pedestal events are compared with those obtained from simulation. The results given in this figure are for negative ADC counts. The error bars on the data points correspond to the 97.3% confidence interval. The comparisons are made for the measurement points 3 in the scans, see Table 1. The ASIC which is exposed to the beam is indicated by a larger symbol. For small absolute thresholds the number of counts have been downscaled by the factors indicated in the figure.

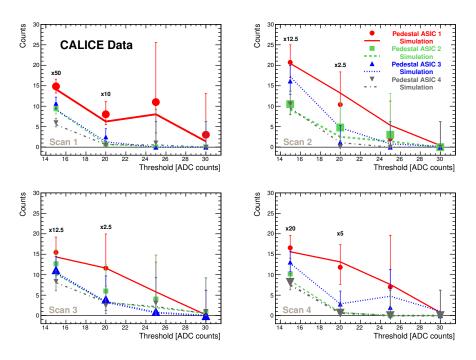


Figure 20: Same as Figure 19 but for positive hits.

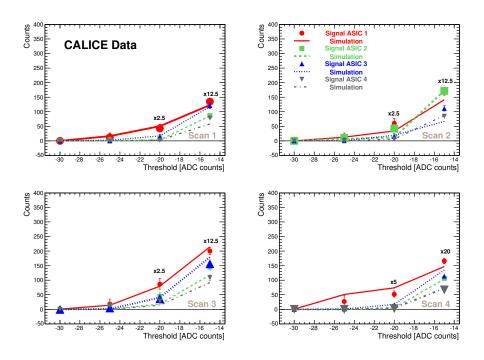


Figure 21: The measured counts below a threshold in signal events are compared with simulation. The results given in this figure are for negative ADC counts. The error bars on the data points correspond to the 97.3% confidence interval. The comparisons are made for the measurement points 3 in the scans, see Table 1. The ASIC that is exposed to the beam is indicated by a larger symbol. For small absolute thresholds the number of counts have been downscaled by the factors indicated in the figure.

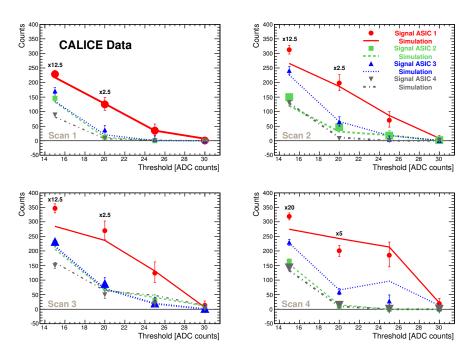


Figure 22: Same as Figure 21 but for positive hits.

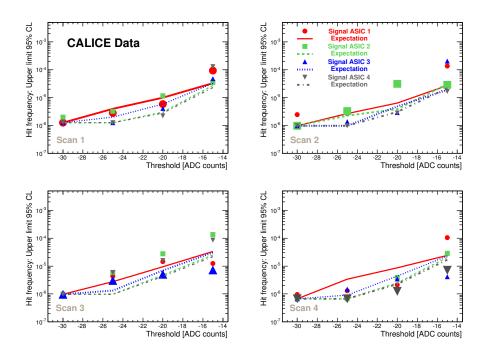


Figure 23: Upper limits on frequencies at the 95% confidence level of fake hits compared with those expected from the pure pedestal events. The limits are given as a function of a threshold for negative values of the ADC counts. The limits are shown for the measurement points 3 in the scans, see Table 1. The ASIC which is exposed to the beam is indicated by a larger symbol.

In application of Equations 6, 7 and 8, the sample statistics k is given by the number of hits above a given threshold and λ_B , i.e. the number of expected hits, is obtained from simulation. From this $\lambda_S^{(up)}$ is derived using a computer program available in [13]. Finally, $\lambda_S^{(up)}$ is divided by the total number of hits to calculate the frequency of fake hits. The upper limits at the $\beta=95\%$ confidence level on the frequency of fake hits are shown in Figures 23 and 24 separately for positive and negative ADC counts.

For each scan, the upper limits are determined for each of the four ASICs in order to compare the behaviour of an ASIC exposed to the electron showers with those not exposed to the showers. It may be seen that the determined upper limits are always smaller than $5 \cdot 10^{-4}$ for the smallest threshold value and smaller than 10^{-5} for the highest threshold value. The observed dependency on the threshold is the same whether or not the ASICs are exposed to the particle showers. The upper limits are compared with sensitivity limits, full lines in Figures 23 and 24, obtained when the frequencies observed in data are replaced by those expected from the simulation. In particular towards large threshold values the derived limits agree well with the expectation. Deviations from the expectation are observed both for ASICs exposed to showers and for those outside the showers.

This observation renders it unlikely that there is an influence of the beam on the measured signal. This is in particular true for threshold values relevant for physics analysis in which typically values below 25 ADC counts are discarded. Remaining deviations towards small

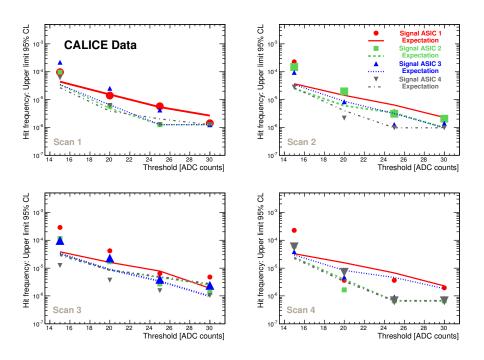


Figure 24: Same as Figure 23 but for positive hits.

thresholds from the expectation can be attributed to the influence by other parts of the 391 experimental set-up which are present when there is a large activity in the detector. These 392 interspersed signals are not taken into account in the simulation. 393

6 Conclusion and outlook 394

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A series of test runs has been performed and analysed in order to prove the feasibility of 395 having embedded readout electronics for a calorimeter proposed for a future lepton collider. 396 A detailed analysis of noise spectra of the ASICs exposed to high-energy electron beams has revealed no evidence that the noise pattern is altered under the influence of the electromag-398 netic showers. The probability to have fake signals above the MIP level is estimated to be smaller than $6.7 \cdot 10^{-7}$. The probability for a fake signal is less than 10^{-5} for a threshold of 400 2/3 of a MIP. For an event of the type $e^+e^- \to t\bar{t}$ at $\sqrt{s} = 500$ GeV at the lepton collider about 2500 cells of dimension 1×1 cm² are expected to carry a signal above noise level which 402 is typically defined to be (60-70)% of a MIP. The results presented in this article have re-403 vealed no problems for the design of embedded readout electronics for a detector for a lepton collider. It is furthermore unlikely that the residual deviations between the observed number of hits and those expected from normal noise fluctuations can be attributed to the influence 406 of the beam but rather to an imperfect modelling of the noise spectra for signal events. In this sense, the presented results constitute a conservative upper limit. 408

Currently, the CALICE collaboration is about to construct a technological prototype [16]. In contrast to the physics prototype, this technological prototype will have the readout electronics embedded by design. The ASICs employed therein are a straightforward further de-

velopment of those of the physics prototype [7] as described in this paper. The technological 412 prototype in general and the ASICs in particular are close to the design currently envisaged 413 for the International Linear Collider which is currently the most advanced proposal for a 414 future lepton collider. A series of tests as described in this article will have to be repeated for 415 this prototype as the electronics are more challenging than the one employed in the physics 416 prototype with respect to compactness and requirements of power saving. Upon repetition of the test a considerably larger amount of interleaved pedestal events will have to be recorded. Future tests should also be conducted with heavily ionising particles up to the point at which 419 radiation effects become apparent. With cross talk effects further reduced, such a research 420 program will allow for the establishment of a complete picture of the feasibility of embedded 421 electronics in radiation environments. 422

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Appendix - Mean and RMS of signal and pedestal events

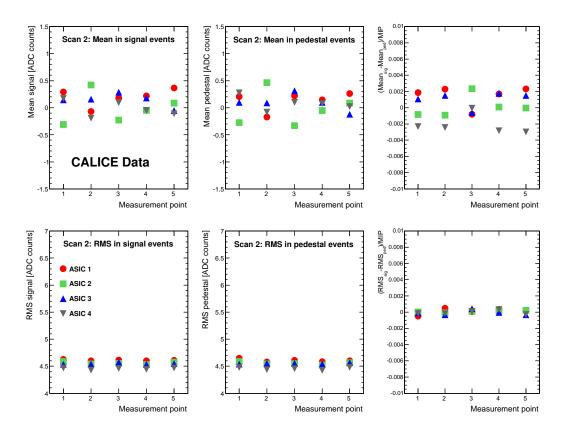


Figure 25: Mean and RMS for signal events and pedestal events. The very right part shows the corresponding differences normalised to the value of a MIP assumed to be 45 ADC counts. The figure displays the result for Scan 2 in which ASIC 2 is scanned. As a cross-check the results for all ASICs are shown.

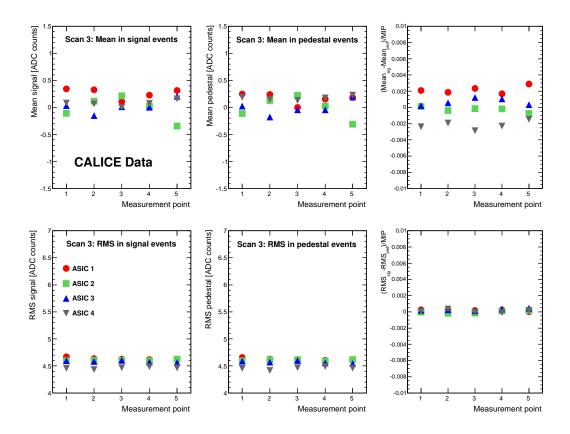


Figure 26: Mean and RMS for signal events and pedestal events. The very right part shows the corresponding differences normalised to the value of a MIP assumed to be 45 ADC counts. The figure displays the result for Scan 3 in which ASIC 3 is scanned. As a cross-check the results for all ASICs are shown.

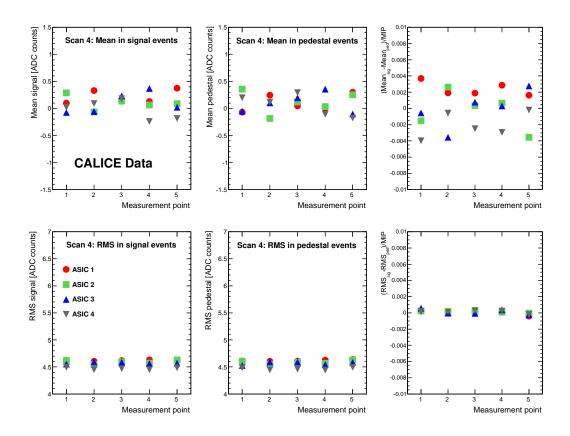


Figure 27: Mean and RMS for signal events and pedestal events. The very right part shows the corresponding differences normalised to the value of a MIP assumed to be 45 ADC counts. The figure displays the result for Scan 4 in which ASIC 4 is scanned. As a cross-check the results for all ASICs are shown.

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