

Effects on Load-Frequency Control of a Solar Power System with a Two-Area Interconnected Thermal Power Plant and its Control with a New BFA Algorithm

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Abstract—A control operation is the most important part of stabilization between load and frequency in a power system. The demand power change and the generated power change can disrupt the load-frequency balance. For this reason, the system frequency value should be controlled by some methods. In this study, a load frequency control was performed in a two-area power system. The renewable solar energy system and the interconnected power system were connected. In order to control the load-frequency balance, the classical PI, PID, Fuzzy Logic Controller (FLC) based PI and Bacterial Foraging Algorithm (BFA) based PI controller were separately designed and implemented to control the frequency value. All the trials were simulated and confirmed by the MATLAB/Simulink program. According to the results obtained from the control methods, the BFA-PI method provided better overshoots and BFA-PI had better settling times than the others.

Index Terms—Automatic generation control; Fuzzy control; Optimization; Power system stability.

I. INTRODUCTION

Energy demand is increasing as a result of the rapid industrialization in the world. As the conventional energy sources are limited, energy is becoming an important component. Electricity energy cannot be stored with high capacity, thus, the produced and consumed energy should always be equal [1], [2]. Frequency is the most important parameter of the stability of a power system. The aim here is to keep the power system in a normal operational status. Normal operational status consists of three parts. The first one is compensation of sudden load changes. The second one is meeting the active-reactive power balance. The third one is stable frequency [3].

An interconnected power system consists of several production-consumption centres that work in harmony with

each other. The stable operation of an interconnected grid depends on a balance between production and consumption centres [4], [5]. If there is an incompatibility between the power produced by generators that are connected to the grid and the power demanded by the load in stable operation, a change would occur in the operating frequency of the system. If the produced energy is greater than the consumed energy, the frequency increases; however, if the situation is vice versa, the frequency decreases. It is possible to take this difference to the level of zero by checking the speed of a turbine which moves the generator [6], [7]. The frequency value has to be between 49.2 Hz and 50.8 Hz, which is the international range according to the Union for the Coordination of the Transmission of Electricity (UCTE). The frequency value, which is 50 Hz in Turkey, must be within the legal limits for the continuity of this connection to UCTE. This also reveals an importance of load frequency control for interconnected grids [8].

Recently, different methods have been used to maintain the process of load frequency control. In a study by Cam *et al.*, a load frequency control in a two-area interconnected grid was maintained by conventional PI, fuzzy logic and PI controller programmed with fuzzy logic [1], [9], [10]. Additionally, in the literature some studies designed PID controllers that were set with the particle swarm optimization (PSO) method [11]. A similar study was achieved by applying an artificial neural grid (ANN) based controller to a three-zone interconnected grid [12], [13]. However, these studies were conducted on interconnected grids through conventional generator units. In this article, a solar energy plant, whose number has increased recently, was modelled and included in a two-area interconnected grid. The load-frequency balance was provided by PI, PID, BFA-PI and FLC-PI controllers, in which changing climatic conditions and sudden power decreases were taken into

account. The number of parameters controlled in the multi-zone power systems was exceeded. The increase in the number of parameters was applied and the control process were complicated. Thus, the frequency value was balanced in different power areas. Moreover, smart fuzzy logic controllers were designed to provide the frequency stability of multi-zone systems [14], [15]. Some studies were carried out in the literature in some specific areas integrated with solar energy. In a study, hysteresis control was achieved with fixed switching frequency. The hysteresis control was emphasised in the study by using a fixed switching frequency [16]. There are some studies in the literature on interconnection systems where wind turbines were used as a source of renewable energy. A study by Sharma *et al.* used the Symbiotic organisms search algorithm for LFC [17].

The study examined the impacts of solar energy plants, which are potentially the most common among the renewable energy sources, on the frequency value as a result of the inclusion to the two-area interconnected grid. As the operating conditions of solar energy plants are not the same as those of conventional fuel plants, they need a load frequency control. There is a rapid instability between the produced and the consumed energy values as a result of being climatic conditions and sudden decrease in the produced power value. This event could be observed more frequently in the areas with the possibility of sudden climatic condition changes. Generally, up to now, load-frequency control studies of modern control strategies with traditional energy sources were used. On the other hand, in interconnected grids that integrate solar energy systems, there are no studies on usage of modern techniques such as a FLC-PI. In this article, as an innovation about load-frequency control, BFA-PI and FLC-PI were designed as controllers in an interconnected grid with solar energy for a frequency correction.

II. PHOTOVOLTAIC POWER MODEL

A circuit model requires simulation of PV solar cells. Various models have been created since 1960s up to now [18]. Solar cells depend on variable light intensity and temperature on PV cells connected in serial or parallel. Their general static equivalent circuit model is represented by a dynamic characteristic, which is formed to meet the changes. Formation of a model such as the dynamic model has been an important issue for researchers for a long time [19], [20]. The simplest equivalent circuit of a PV solar cell is shown in Fig. 1(a). The solar cell is illustrated by a current source I_{ph} in Fig. 1(a). The current source shows the current, which is obtained by the effects of photons that come from daylight. I_D represents the inverse saturation current that occurs in the PV solar cell, while resistance represents the heat losses at the point P-N point. The output voltage that is obtained from the circuit in Fig. 1(a) is shown in (1) [21]–[23]. Here, A represents curve fitting factor, k represents Boltzmann constant, T_{cell} represents reference cell operating temperature, e represents electron charge, I_{ph} represents photocurrent, I_0 represents reverse saturation current of diode and I_{cell} represents Cell output current.

Figure 1(b) and Fig. 1(c) show the panel I-V and P-V characteristics obtained from the solar cell modelled according to (1)

$$V_{cell} = \left((A \times k \times T_{cell}) \times e \right) \times \ln \left((I_{ph} + I_0 + I_{cell}) \times I_0 \right). \quad (1)$$

III. TWO-AREA POWER SYSTEM

Synchronous generators are placed to provide power for the loads connected to the interconnected grid. However, diesel generators are used for the systems which are independent from the grid. The generators running with turbines are used in larger interconnected grids. The transfer functions used in the modelling of a turbine and a generator are given in (2) and (3) [24]. Here, $G_{T(s)}$ represents the turbines transfer function, $G_{G(s)}$ represents the generators transfer function, $T_{G(s)}$ represents speed governor time constant and $T_{T(s)}$ represents Turbine time constant:

$$G_{G(s)} = 1 / (T_{G(s)} + 1), \quad (2)$$

$$G_{T(s)} = 1 / (T_{T(s)} + 1). \quad (3)$$

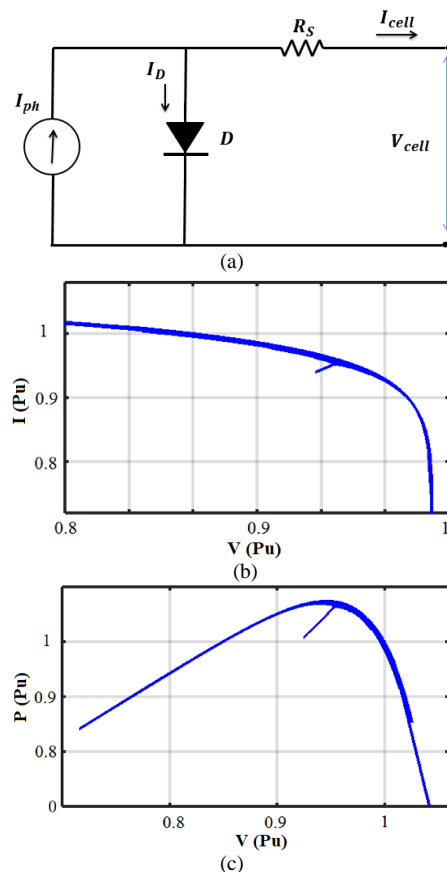


Fig. 1. Solar cells are reduced to the simplest equivalent circuit (a); solar cell I-V characteristic (b); solar cell P-V characteristic (c).

Frequency stability is the ability to keep the frequency stable after rapid changes, which cause instability between the produced and demanded powers in the system. The total power (P_1) in the first area is equal to the sum of the power of the generator (P_{G1}) and the solar energy systems (P_{V1}). It is given in (4)

$$P_1 = P_{G1} + P_{V1}. \quad (4)$$

Power balance ($P_{\Delta i}$) is disrupted when an inequality occurs either in the load side or in the production side. Here, P_{L1} refers to the load change in the first area

$$P_{\Delta 1} = P_1 + P_{L1}. \quad (5)$$

If P_{Δ} has a nonzero value, the frequency of the system would change. Frequency change ($\Delta\omega$) is expressed in (6). Here, K_S is defined as the characteristic constant of the system frequency in the first area

$$\Delta\omega = P_{\Delta 1}/K_S. \quad (6)$$

The transfer function, which represents the load changes that have impact on the system frequency, is presented in (7) [11]. Here, $M = 2 \times H$ and H represents inertia constant

$$G_L = 1/M(s) + 1. \quad (7)$$

The two-area renewable interconnected system used for this article is illustrated in Fig. 2. This interconnected power system consists of various components. The load-frequency control in this grid, in which the solar energy system is included, would ensure a balanced system. A control flow diagram was designed as indicated in Fig. 3. The MATLAB/Simulink program was used in this design.

A transmission line model that connects the two areas to each other was used in this design. The situations where loads changed were examined in this newly designed interconnected power system. Moreover, in order to take

into account any variation in the climatic conditions there were increases and decreases depending on time in the power generated by the photovoltaic (PV) power system. The load-frequency control system, which had all these parameters, was operated in two different ways.

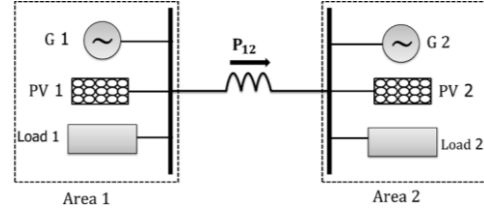


Fig. 2. Two-area interconnected grid schemas: (a) block diagram of the system in two interconnected areas; (b) two-area interconnected grid connection.

The primary frequency control is the frequency control, in which the power balance is achieved by setting the turbine speed regulator when the electricity energy is different in two different areas. The secondary frequency control is achieved by reducing the permanent frequency error to zero in the interconnected grid by controlling the power flow between the areas. Figure 3 shows the block diagram of the two-area interconnected grid with the PV power system. Here, the PV power is modelled as a P_u system. The power generated by the PV system was assessed. It was not needed to model converter.

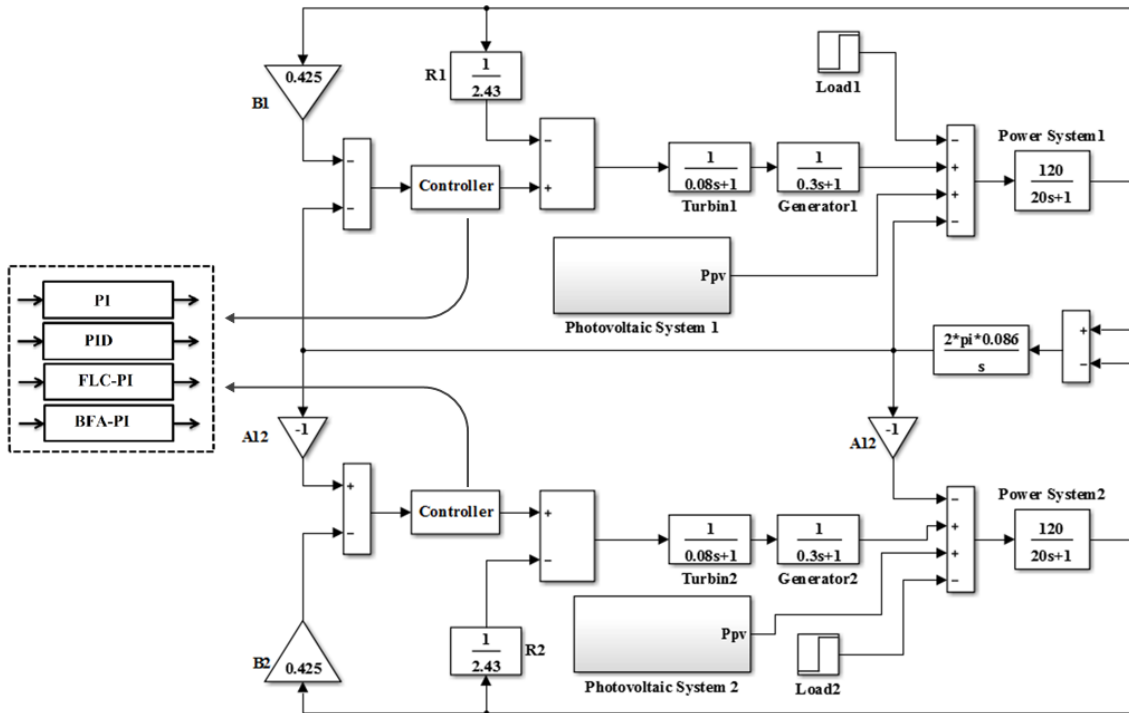


Fig. 3. Two-area interconnected grid block diagram with PV power system.

Area control error (ACE_i), which is required for frequency control, could be calculated as in (8)

$$ACE_1 = (-\Delta P_{12} - b_1 \times \Delta\omega), \quad (8)$$

where b_1 in (8) refers to the frequency bias. In other words, it is the expression of the change in the frequency ($\Delta\omega$) in the power unit, and it is obtained with (9) [12], [25]

$$b_1 = 1/R_1 + D_1. \quad (9)$$

Parameters of the Two-Area power system in the solar power system were taken from the literature [26].

IV. CONTROLLERS

A. Conventional PI and PID Controllers

P, PI and PID control methods are preferred mostly in load-frequency control studies in literature. Even if these studies seem to be enough, rapid climate changes and load fluctuations cause unstable systems [27], [28]. Controller

blocks need two types of signal in load-frequency control. The first one is the steady-state error. The second error is the value which represents the temporary overshoots. The temporary situation emerges in the time of excessive rise or fall in the frequency in sudden deflections. In this study, the performance of conventional and modern control techniques for load-frequency control in an interconnected power system with a two-area solar energy system is presented. During the control process, the Ziegler Nichols (ZN) method was applied for PI and PID, which are the conventional controllers, and its simulation was carried out. The parameters used in the two-area interconnected power system that was modelled are given in Fig. 3.

The expression that belongs to the control signal ($u_{(t)}$) which is required for the PI and PID controller is shown in (10). K_p represents control area gain

$$u(t) = K_p \left[e(t) + (1/T_i) \int_0^t e(t) dt + T_d (e(t)/dt) \right]. \quad (10)$$

B. Controller Designed with FLC-PI

It is difficult to apply the controls defined by conventional methods such as the ZN method to flexible and continuously changing systems. The parameters of these controls remaining constant are a disadvantage

$$u_{pi}(t) = \left[-K_p \times ACE_i - \int K_i (ACE_i) dt \right]. \quad (11)$$

On the other hand, a conventional control that is optimised and applied to the system is recommended for continuously changing systems. Here, the PI controller that was set with the fuzzy logic was used. It is given in (11). Thus, the control of the system was achieved in a more flexible way in comparison to conventional control systems. The error and the change of error utilised to set the PI controller are given in the block scheme in Fig. 4.

The membership functions employed in the FLC-PI controller and the ranges of these functions are shown in Fig. 5. These values are necessary for FLC-PI, which sets the PI controller [26], [29]–[31]. Fuzzy logic rules for FLC-PI controller are shown in Table I.

TABLE I. FUZZY LOGIC RULES FOR FLC-PI CONTROLLER.

		Fuzzy Logic Rules						
		$\Delta ACE(k)$						
ACE	$\Delta ACE(k)$	N_L	N_M	N_S	Z	P_S	P_M	P_L
N_L		P_L	P_L	P_L	P_L	P_M	P_M	P_S
N_M		P_L	P_M	P_M	P_M	P_S	P_S	P_S
N_S		P_M	P_M	P_S	P_S	P_S	P_S	Z
Z		N_S	N_S	N_S	Z	P_S	P_S	P_S
P_S		Z	N_S	N_S	N_S	N_S	N_M	N_M
P_M		N_S	N_S	N_M	N_M	N_M	N_L	N_L
P_L		N_S	N_M	N_L	N_L	N_L	N_L	N_L

Note: N_L : large negative, N_M : medium negative, N_S : small negative, Z: zero, P_S : small positive, P_M : medium positive, P_L : large positive.

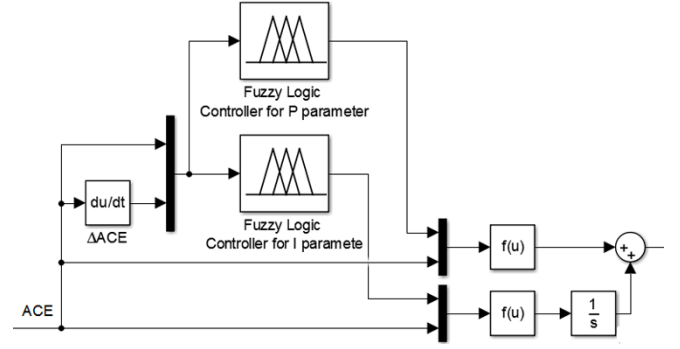


Fig. 4. FLC-PI controller block diagram.

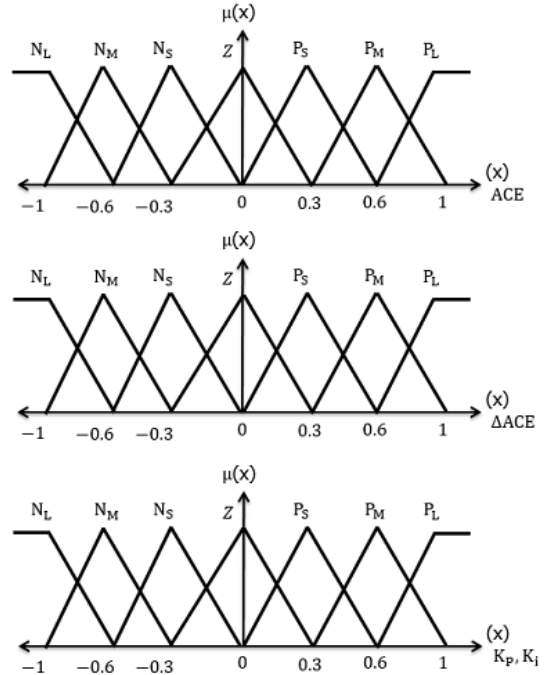


Fig. 5. Membership function for the FLC-PI controller.

C. Controlled Designed with BFA-PI

The basis of Bacteria Foraging Optimization was laid by Escherichia Coli, taking into account the processes that bacteria use in their nutritional search methods. BFA, based on a stochastic search technique, is the most effective method that considers population. The approach in this algorithm is inspired by the physical and biological life of bacteria. The first step in BFA is to transform the problem into the most appropriate algorithm. The second most important step is to arrange the bacteria according to the herd information. As a final step, it can be thought of as an optimal solution search [32]. An iteration of BFA comes from four basic stages. These are Chemotaxis, swarming, Reproduction and Elimination-Dispersal. The flow diagram of BFA is shown in Fig. 6.

Chemotaxis: A chemotactic step can be assigned as a tumble followed by a tumble or a tumble followed by a run lifetime. To symbolise a tumble, a unit length random way(j) is created. This will be used to describe the direction of movement after a tumble. The formula for changing direction in BFA can be defined as in (12). Where $i(j,k,l)$ represents the i 'th bacterium at j 'th chemotactic, k 'th reproductive and l 'th elimination and dispersal step. $C_{(i)}$ is the size of the step taken in the random direction specified by a tumble [33].

TABLE II. PI COEFFICIENTS OBTAINED WITH THE PROPOSED METHODS.

Controller	K_p	K_i
BFA-PI	0.96	0.5421

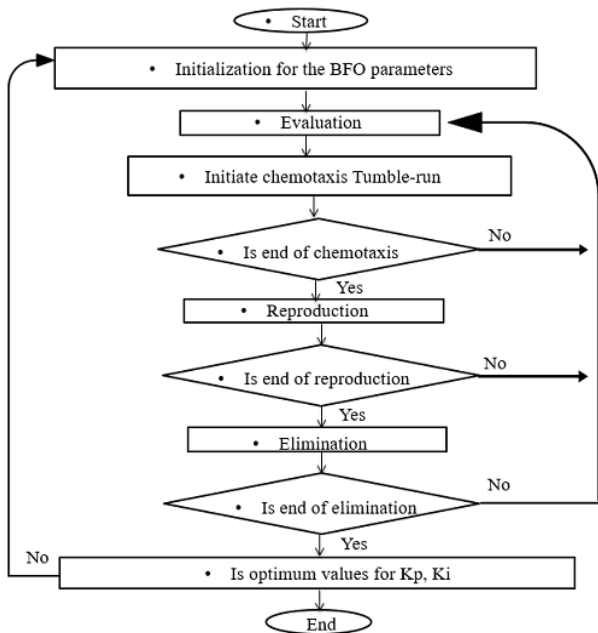


Fig. 6. Flow chart of BFA.

$$i(j+1, k, l) = i(j, k, l) + C(i) \times (j). \quad (12)$$

Swarming: Bacteria used in the optimization process need to attract other bacteria to reach the areas that are the richest in terms of food. Thus, a faster association is achieved. To achieve this, a penalty function based on the optimal bacteria and the relative distances of each bacterium until the call is added to the original cost function. In the last step, when all the bacteria enter the solution zone, the penalty function becomes zero.

Reproduction: In the next step, evolved by several chemotactic stages, the original set of bacteria reaches the reproduction phase. At this stage, the best bacteria set is divided into two groups. Half of the healthy bacteria are replaced by half of the other bacteria. In this phase, removal is made from the centre due to poor manager qualities. This keeps the bacteria population constant during the evolution process [34].

Elimination and dispersal: Sudden and unpredictable events may occur in BFA. This may greatly alter the smooth process of evolution and cause the set of bacteria to be removed from the centre and/or dispersed into a new environment. Most ironically, instead of disrupting the normal chemotactic growth of the bacteria set, it may place a newer set of bacteria close to the food location. Elimination and dispersal are parts of the long-range movement behaviour on the population level. In implementing optimization, it helps to reduce stagnation behaviour, which is common in such parallel search algorithms. The K_p and K_i coefficients obtained using BFA are shown in Table II. The parameters that BFA possesses are as follows: The dimension of the search space is 2, the number of the bacteria is 10, the number of the chemotactic steps is 5, the limits of the length of a swim is 10, the

number of elimination-dispersant events is 2, the number of bacteria reproductions is 1/2 and the respective probabilities of bacteria (eliminated) are 0.25.

V. RESULTS

In this study, the load-frequency control of a two-area interconnected power system, which included solar panels that are under the effect of climatic changes, was achieved. During the controlling process, the controllers were simulated separately in the designed system. Firstly, the conventional PI and PID controllers were modelled. The simulation was performed with FLC-PI and BFA-PI, which were modernised with fuzzy logic apart from the conventional controllers. During the simulation, the power obtained from the solar panels indicated changes due to the weather conditions in Fig. 7.

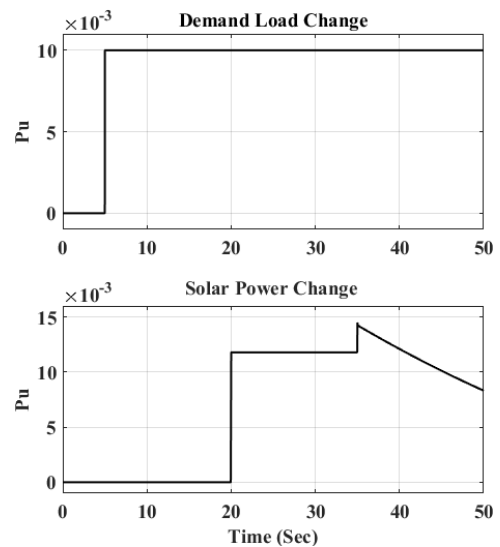


Fig. 7. Load power change and solar power change depending on weather conditions.

Besides, these power changes affect the interconnected grid as “load changes”. The parameters operated in the interconnected grid, which was modelled by including renewable energy, are shown in Fig. 3.

The decrease in the power demand of the load, the activation of the solar energy system and the power-time change intended for the regular power loss in the PV panels are demonstrated in Fig. 7. While operating the control process, a drastic action was taken into account to change the frequency in three different times. The first change was the sudden power loss with 0.01 pu in the fifth second at point A in Fig. 8(a). The second change was the inclusion of the power obtained from the solar energy system in the interconnected grid at point B in Fig. 8(a). When the reaction of the system takes a stable position against this sudden frequency change, a power increase occurs in the renewable solar energy system in the 35th second due to the weather conditions at point C in Fig. 8(a). Right after this, the power that comes regularly from the PV power system starts to decrease due to the weather conditions.

The gain controls of the applied conventional controllers were designed in the range of 0 sec–5 sec. These gain values are for K_p value of 1.1 and K_i value of 0.8 for PI, and K_p value of 1.4, K_i value of 2.0 and K_d value of 0.1 for PID.

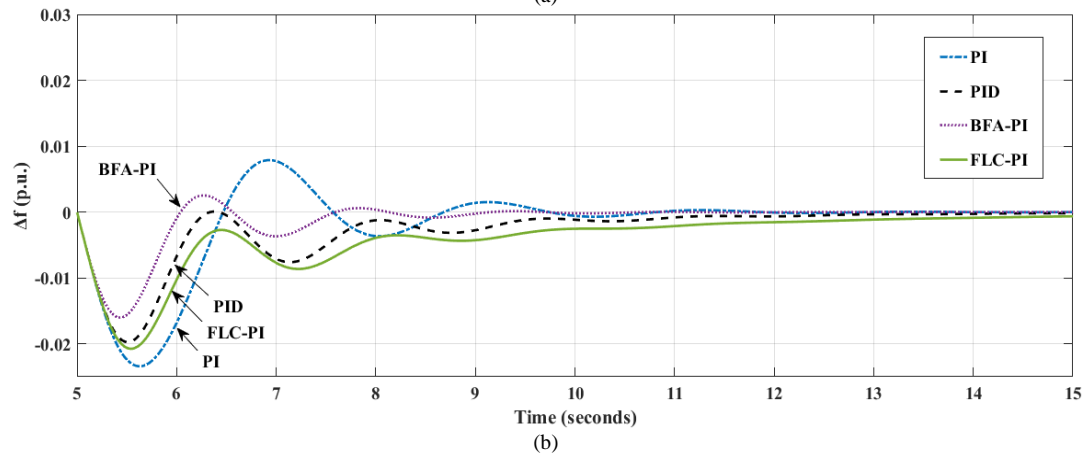
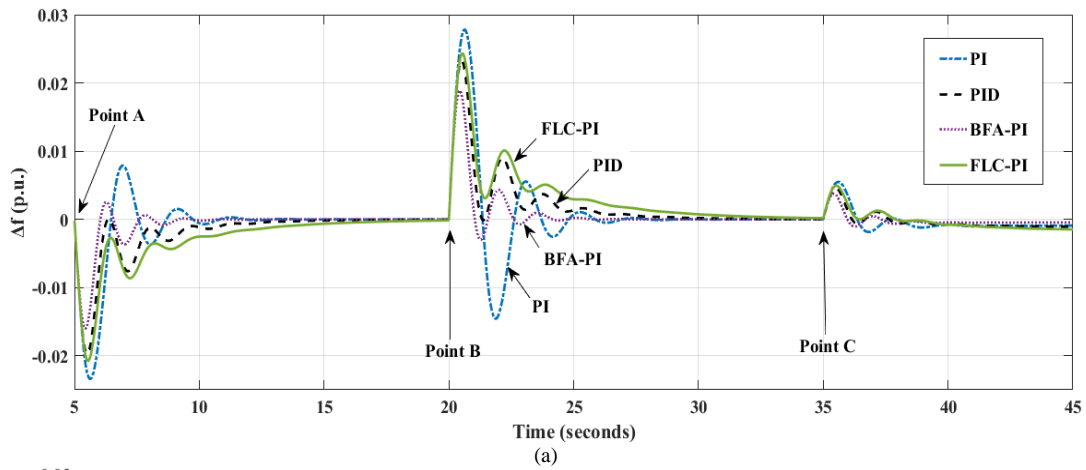


Fig. 8. Frequency change in entire simulation(a); frequency change during load increase (zoomed of point A) (b);

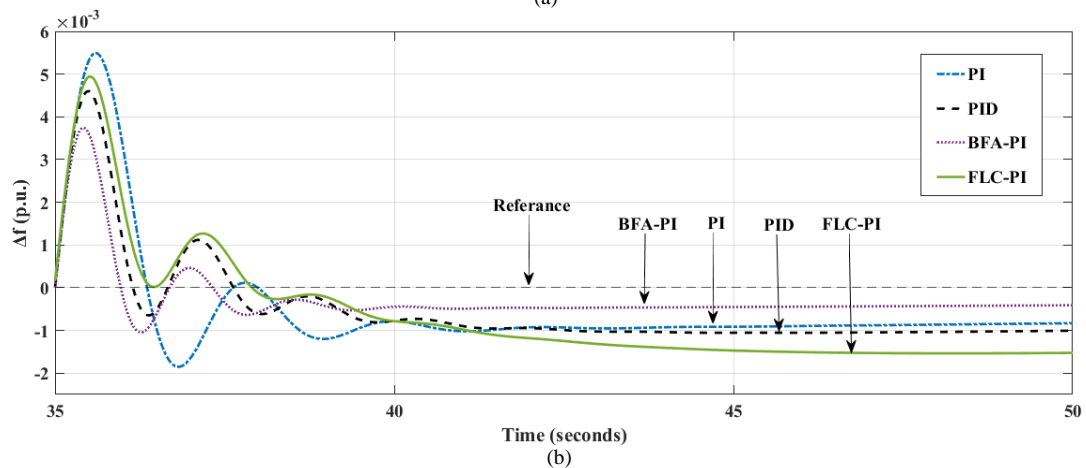
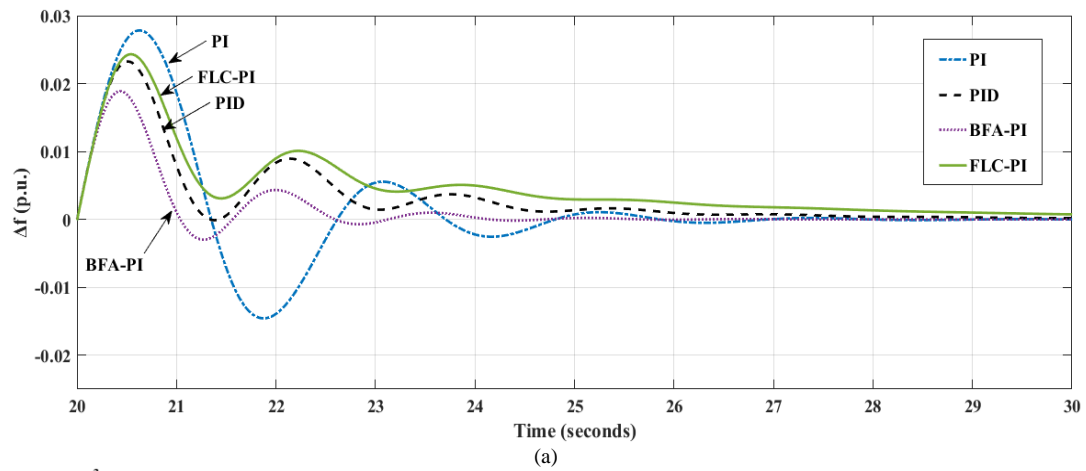


Fig. 9. Frequency change when solar power is suddenly included (zoomed of point B) (a); frequency change when solar power is in continuous reduction (shadowing effect) (zoomed of point C) (b).

The frequency change results of the conventional controllers and the other recommended FLC-PI and BFA-PI controllers are shown in Table III, Table IV and Table V. The positive and negative overshoot values in the frequency values of a 0.01 pu load reduction in the interconnected grid in the 5th second are shown in Table III and Fig. 8(b). As it is seen in this comparative table, there is no positive fluctuation in the FLC-PI controllers.

TABLE III. FREQUENCY CHANGE IN LOAD REDUCTION OF 0.01PU. (POINT A).

Controllers	Negative maximum Overshoots	Positive maximum overshoots
PI	-23×10^{-3}	8×10^{-3}
PID	-20×10^{-3}	1×10^{-3}
FLC-PI	-20×10^{-3}	-
BFA-PI	-16×10^{-3}	2×10^{-3}

The frequency fluctuations related to the changes in the 20th and the 30th seconds which define sudden power increases depending on the solar radiation in the interconnected renewable grids are shown in Fig. 9(a). Thus, the most remarkable result was the performance of BFA-PI in the control of load-frequency.

TABLE IV. FREQUENCY CHANGE IN SOLAR CHANGE OF 0.012 PU. (POINT B).

Controllers	Negative maximum Overshoots	Positive maximum overshoots
PI	-15×10^{-3}	27×10^{-3}
PID	-	23×10^{-3}
FLC-PI	-	24×10^{-3}
BFA-PI	-	8×10^{-3}

TABLE V. STEADY-STATE ERROR IN THE FREQUENCY OF CONTINUOUS REDUCTION OF THE SOLAR ENERGY SYSTEM (POINT C).

Controllers	Steady-State Error
PI	-9×10^{-3}
PID	-1×10^{-3}
FLC-PI	-1.5×10^{-3}
BFA-PI	-0.5×10^{-3}

The numerical results of the change in the frequency between the 35th and 50th seconds in Fig. 9(b) that led to a continuous decrease due to the adverse weather conditions in the PV energy system are depicted in Table V. It is seen that the BFA-PI controller minimised the steady-state error better than the other controllers in Fig. 9(b) and Table V.

The change in area control error throughout the entire simulation is shown in Fig. 10. This area control error was employed in the design of the proposed controls and it was defined as the most important variable in this study.

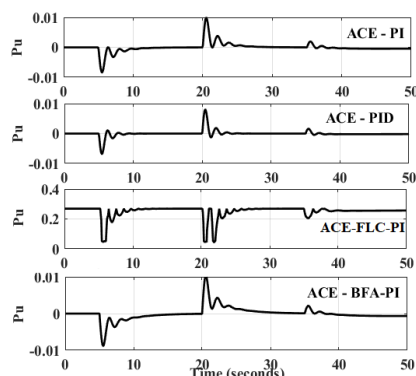


Fig. 10. ACE changes with different controllers.

VI. CONCLUSIONS

In this study, a two-area interconnected power system with a Solar Power System was modelled by using mathematical models in order to investigate the effects of renewable energy sources on load-frequency control. Additionally, some modern control techniques called FLC-PI and BFA-PI were also designed. Moreover, conventional PI and PID controllers were applied in the system to make comparisons with the others. All the controllers were implemented separately in order to set the varying frequency of the system to the nominal frequency during sudden load changes. According to the results, it was seen that the modern control techniques provided better results than the conventional controllers. In particular, the proposed BFA-PI controller had better values in terms of settling time and overshoot. Besides, it was seen that the proposed controllers could keep the steady-state errors in their nominal values. This situation was demonstrated prominently in the 35th second when there was a sudden drop in the power of the Solar energy system depending on the weather conditions. In conclusion, the study has shown that all the proposed methods could successfully maintain the frequency at the nominal value at load change points in comparison to other conventional methods.

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