Research Article

Efficiency and economic optimization of shell and tube heat exchanger using bacteria foraging algorithm



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Abstract

Shell and tube heat exchanger (STHE) is widely used in the industries for various purposes due to its capacity to withstand pressure. STHE has the drawback of more cost and lower efficiency. Many existing methods involve in applying the optimization technique to decrease the cost of the system. Existing method has the lower efficiency in the optimization due to the random initialization and poor convergence. This research applies the bacteria foraging algorithm (BFA) to increase the efficiency and decrease the cost of the STHE system. The BFA has the advantages of the faster convergence and the global search approach to increase the performance in design. The proposed BFA is evaluated in the two case studies and compared with the existing method. The proposed BFA in multi-objective optimization of STHE has the total cost of $41,464 \in$, while existing method has the total cost of $41,913 \in$. The proposed BFA method also achieved high heat efficiency coefficient of 1089, and the existing method has 1031.47.

Keywords Bacteria foraging algorithm · Faster convergence · Global search approach · Shell and tube heat exchanger

nbols	Pr	Prandtl number
Baffle spacing (m)	Pt	Tube pitch (m)
Specific heat (kJ/kg K)	Q	Heat transfer rate (W)
Capital investment (€)	Re	Reynolds number
Energy cost (€/kWh)	RI	Fouling resistance (m ² K/W)
Annual operating cost (€/year)	S	Heat transfer surface area (m ²)
Total discounted operating cost (€)	Т	Temperature (K)
Total annual cost (€)	U	Overall heat transfer coefficient (W/m ² K)
Tube diameter (m)	V	Fluid velocity (m/s)
Shell diameter (m)	Greek sy	mbols
	ΔP	Pressure drop (Pa)
	$\Delta T_{\rm LM}$	Logarithmic mean temperature difference (°C)
		Dynamic viscosity (Pa s)
• • •	ρ	Density (kg/m ³)
5	n. n	Overall pumping efficiency
-	•	
•	Subscrip	its
Equipment life (year)	i	Inlet
Number of tubes	0	Outlet
Pumping power (W)	s	Belonging to shell
	Baffle spacing (m) Specific heat (kJ/kg K) Capital investment (€) Energy cost (€/kWh) Annual operating cost (€/year) Total discounted operating cost (€) Total annual cost (€) Tube diameter (m) Shell diameter (m) Friction factor Correction factor Heat transfer coefficient (W/m ² K) Thermal conductivity (W/mK) Tube length (m) Mass flow rate (kg/s) Number of tube passes Equipment life (year) Number of tubes	Baffle spacing (m)PtSpecific heat (kJ/kg K)QCapital investment (€)ReEnergy cost (€/kWh)RlAnnual operating cost (€/year)STotal discounted operating cost (€)TTotal annual cost (€)UTube diameter (m)vShell diameter (m)Greek syFriction factor ΔP Correction factor ΔT_{LM} Heat transfer coefficient (W/m² K) μ Tube length (m) ρ Mass flow rate (kg/s) η Number of tube passesSubscriptionEquipment life (year)iNumber of tubes o

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- t Belonging to the tube
- e Equivalent
- w Tube wall

1 Introduction

Heat exchanger is core part in some industries like chemical industries, power plant, oil refining industries, etc. [1]. Traditional method in the STHE design applies the geometric assessment and operating constraints to select the design model [2]. The geometric feature of STHE and the fluid turbulence have impact on the exchanger efficiency [3]. Cost is the foremost objectives of the designers and industries to earn more profits [4]. Hence, the heat exchanger designing involves in investigating the geometric structure and operational parameter for improving thermal efficiency with cost constraint [5].

Proper design of the exchanger has impact on various aspects such as thermal stress, thermal drop, fluid dynamics properties, temperature, cleanability, fouling, and cost [6]. Experimental analysis of the heat exchanger involves in high cost and less flexibility for the analysis. Mathematical model of the heat exchanger in MATLAB tool helps to analyze the exchanger more flexible with less cost. Evolutionary algorithms have been applied by various researchers to optimize the design to increase the efficiency and reduce the cost. These methods solve the problems of multi-modality, nonlinearity, and noncontinuity, in which conventional methods found difficulty to solve [7]. Many optimization methods including particle swarm optimization (PSO) have been used to solve the optimization problem in design of STHE and found to have considerable performance for the method [8, 9]. Multi-objective optimization techniques were used to improve the design with the objective of both economic and efficiency [10]. In this research, the multi-objective optimization of BFA is used for the STHE with various parameter designs. The BFA has the advantages of faster convergence and the global search method to increase the performance. The simulation result shows that the BFA has the higher performance compared to existing method. The proposed BFA method has the advantages of the fast convergence and global search for the optimal solution of the design. The proposed BFA design provides the total cost of 41,464 €, and existing method has the total cost of 41,913 €. The heat efficiency of the BFA method is high compared to the other existing method due to its optimal design of the system.

The paper is formulated as the literature survey of optimization of STHE is given in Sect. 2, the explanation about

SN Applied Sciences

the performance of BFA is given in Sect. 3, STHE simulation results are briefly explained in Sect. 4, and Sect. 5 contains conclusion.

2 Literature survey

The STHE is used in the industries for the heat transfer, and this can withstand more pressure compared to other exchanger types. Various optimization techniques were applied in the STHE to increase the efficiency. The optimization techniques applied in the STHE with considerable performance were surveyed in this section.

Caputo et al. [11] applied the genetic algorithm (GA) for economic optimization of the STHE design. The GA method reduces the total cost and maintains system cost of pumping. The three case studies were used to analyze the performance of the GA method in terms of cost. The result shows that the GA method significantly reduces the cost of the system and increases the performance. The GA is depending on the initial population, and this affects the performance of the optimization.

Patel and Rao [12] established PSO for the STHE economic optimization of design, and the three design variables were used for the STHE optimization. The method is tested on the two different tube layouts for the analysis. The developed method is evaluated in four case studies to analyze the efficiency and accuracy. The result shows that the performance of PSO is higher than the GA in economic optimization of the STHE. Multi-objective optimization needs to be considered in this method for increasing the efficiency.

Sahin et al. [13] established the artificial bee colony (ABC) method for the economic optimization of the STHE design. Various designs like tube length, baffle spacing, etc., were considered in the optimization. The three case studies were used to analyze the efficiency of the ABC in optimization. The experimental result shows that the performance of the developed method is high compared to existing method in optimization technique. The developed method does not effectively analyze the design in the system. The efficiency of the heat exchange is affected and has the lower convergence in the process.

Hadidi and Nazari [14] developed biogeographybased optimization (BBO) for economic optimization of the STHE. There are various designs like tube length and baffle spacing, etc., and variables are considered in the optimization technique. The developed method is tested on the three case studies to analyze the performance. The developed method has the high performance compared to the existing technique in STHE economic optimization. The multi-objective optimization is required to be processed. This method has the poor convergence, and the search process needs to be improved.

lyer et al. [15] developed adaptive range genetic algorithm (ARGA), and the GA is combined with the cohort intelligence (CI) to utilize the sample space reduction. The correctness of ARGA is tested on the 50 standard test function. Various designs are used for the optimization of the STHE. The three case studies were used to evaluate the efficiency of the ARGA method. The simulation results show that the ARGA method has the higher performance compared to the existing method. The developed method is depending on the initial population, and this affects the performance of the optimization.

In order to overcome the above limitation of the existing method, the BFA method is proposed in the STHE optimization. The proposed BFA has the advantages of faster convergence and the global search method to increase the performance.

3 Proposed method

The several optimization techniques were applied in the multi-objective STHE design to increase the efficiency and decrease the cost. Existing method has the lower efficiency in the exchanger and more cost due to the design. In this research, BFA is proposed for the optimization in STHE design. Various designs are considered for the optimization process, and two case studies were used to analyze the BFA method efficiency. The general block diagram of BFA in STHE design is shown in Fig. 1.

3.1 Heat exchanger design formulation

Mathematical model of the STHE is discussed in this subsection. STHE is modeled in MATLAB based on mathematical expressions. The surface area (*S*) was calculated as based on Eq. (1)

$$S = \frac{Q}{U\Delta T_{\rm LM}F}$$
, $F = \text{correction factor}$ (1)

where heat transfer rate is represented by Q, ΔT_{LM} represents the temperature difference logarithmic mean of counter flow, and U represents overall heat transfer coefficient (HTC).

The *U* depends on heat transfer coefficient of shell and tube side and fouling resistance [16]. This is measured based on Eq. (2)

$$U = \frac{1}{\frac{1}{h_s} + R_{ls} + \frac{d_0}{d_i} \left(R_{lt} + \frac{1}{h_t} \right)}$$
(2)

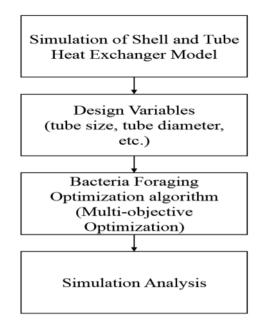


Fig. 1 The proposed BFA in STHE design block diagram

where $d_i = 0.8d_a$.

The shell-side HTC h_s is measured based on the segmental baffle of exchanger, denoted in Eq. (3).

$$h_{s} = 0.36 \frac{k_{s}}{D_{e}} \operatorname{Re}_{s}^{0.55} \operatorname{Pr}_{s}^{\frac{1}{3}} \left(\frac{\mu_{s}}{\mu_{w}}\right)^{0.14}$$
(3)

The tube-side heat transfer coefficient h_t is measured using Eq. (4).

$$h_{t} = \frac{k_{t}}{d_{i}} \left\{ \frac{f_{t} \left(\operatorname{Re}_{t} - 1000 \right) \operatorname{Pr}_{t}}{1 + 12.7 \sqrt{\frac{f_{t}}{8}} \left(\operatorname{Pr}_{t}^{\frac{2}{3}} - 1 \right)} \left[1 + \left(\frac{d_{i}}{L} \right)^{0.67} \right] \right\}$$
(4)
× (2300 < Re_t < 10,000)

Considering the cross-flow of adjacent baffle with $\Delta T_{\rm LM'}$ measured using Eq. (5).

$$\Delta T_{\rm LM} = \frac{\left(T_{is} - T_{ot}\right) - \left(T_{os} - T_{it}\right)}{\ln\left[\frac{T_{is} - T_{ot}}{T_{os} - T_{it}}\right]}$$
(5)

3.2 Bacteria foraging optimization algorithm

The BFA is optimization technique inspired from the e-coli bacteria foraging group method. Tensile flagella move the bacteria in particular direction, and in foraging, this performs tumble and swing. The bacteria rotate its flagella, and then bacterium tumbles to move in a nutrient gradient. The BFA method has the advantages of fast convergence in the process. Based on the inspiration of this process, e-coli bacteria phenomena [16] are developed with four steps. These four methods are discussed as follows.

3.2.1 Chemotaxis

The swimming and tumbling process is carried out in this step to enable the bacteria to move.

Assume that $\theta_i(j, k, l)$ denotes the *i*th bacterium position at *j*th chemotactic, with *l*th elimination–dispersal step and *k*th reproduction. The swimming and tumbling of the movement of bacteria can be represented in Eq. (6)

$$\theta_i(j+1,k,l) = \theta_i(j,k,l) + C(i)\frac{\Delta(i)}{\Delta T(i)\Delta(i)}$$
(6)

where θ_i denotes the objective function, and C(i) represents the tumble taken step size in random direction. The vector in the random direction is denoted as Δ whose elements are present between [-1, 1].

3.2.2 Swarming

The repellents and attractants were released in this step by e-coli cells to communicate with other cells. This step avoids noxious environments and combines into groups in rich nutrient environment. The cell-to-cell signaling equation is represented as given in Eq. (7)

$$J_{CC}(\theta, P(j, k, l)) = \sum_{i=1}^{s} J_{CC}(\theta, \theta^{i}(j, k, l))$$
$$= \sum_{i=1}^{s} \left[-d_{\text{attractant}} \exp\left(-w_{\text{repellent}} \sum_{m=1}^{P} \left(\theta_{m} - \theta_{m}^{i}\right)^{2}\right) \right]$$
(7)

where $J_{CC}(\theta, P(j, k, l))$ is the additional part with actual objective function with *S* denoting the total number of bacteria and *p* is the number of factors in search space, $\theta = [\theta_1, \theta_2, \dots, \theta_p]_T$ denote the location of the search space and θ mis denotes the *m*th components of the *i*th bacterium position θ_i , and different coefficients are used for signaling.

Table 1 Case study details	Table 1	Case study det	ails
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3.2.3 Reproduction

The least health bacteria die in this step $(S_r = S/2)$, and healthier bacteria are divided into two bacteria that are present in this vacant location.

3.2.4 Elimination-dispersal

The bacteria life may be affected due to change in the environment. To denote this process, each bacterium in population is eliminated based on probability $P_{\rm ed}$ and a new replacement is initialized randomly.

The part sequence matrix is used to denote the position of each bacterium, and pairwise interchange mutation is applied to find each bacterium movement during swimming and tumbling process. The bacteria position is updated in swimming and tumbling of chemotaxis as follows in Eq. (8)

$$\theta_i = (j+1,k,l) = f_1(C,\theta_i(j,k,l))$$
(8)

where f_1 denotes the mutation operation, and the number of random pairwise interchange is denoted as *C* for each mutation operation.

The optimized design provided by the BFA is evaluated in the heat exchanger simulation model, and various aspects are analyzed. The simulation result of the proposed BFA in multi-objective optimization of the STHE is discussed.

4 Simulation result

This research involves in applying the BFA method in the design of STHE for the multi-objective optimization. The proposed BFA is tested on the two case studies with various design parameters, and aspects are calculated. The cost measurement and the design of the case studies are based on the analysis used in research [15]. The proposed BFA is tested on the MATLAB installed in the system of Intel core i7 processor with 8 GB of RAM. Table 1 shows the details of the case study. The number of bacteria is set as 20, the number of chemotaxis steps is set as 2, the number of reproduction step is set as 100, and the number of swarming steps is set as 10.

Case study 1	Case study 2
4.34 (MW) heat duty, methanol-brackish water heat exchanger	1.44 (MW) heat duty, kerosene–crude oil heat exchanger

Table 2 Performance analysis of case study 1

Parameters	BBO [14]	ARGA [15]	BFA
<i>D</i> _s (m)	0.801	0.665	0.675
<i>L</i> (m)	2.04	1.263	1.52
<i>b</i> (m)	0.5	0.49	0.47
<i>d</i> ₀ (m)	0.01	0.01	0.01
<i>P</i> _t (m)	0.0125	0.012	0.012
<i>C</i> ₁ (m)	0.0025	0.002	0.002
n _t	2	2	2
N _t	3587	2625.87	2461.52
<i>v_t</i> (m/s)	0.77	1.049	1.053
Re _t	7642.4	10,440.1	11,212
Pr _t	5.7	5.694	5.682
$h_t (W/m^2K)$	4314	6196	6203
f _t	0.034	0.031	0.33
ΔP_t (Pa)	6156	9756.24	9821.26
$a_{\rm s}~({\rm m}^2)$	0.0801	0.065	0.0735
$D_e(\mathbf{m})$	0.007	0.007	0.007
$v_{\rm s}({\rm m/s})$	0.46	0.568	0.524
Re _s	7254	8912.33	7826
Pr _s	5.1	5.082	5.103
$h_{\rm s} ({\rm W}/{\rm m}^2{\rm K})$	2197	2422.8	2512.7
f _s	0.379	0.368	0.374
$\Delta P_{s}(Pa)$	13,799	10,746.3	11,213.2
$U (W/m^2K)$	755	1031.47	1089
S(m ²)	229.95	168.275	172.14
C _{inv} (€)	44,536	35,498.9	34,228
C _{annual} (€/year)	984	1043.96	1024
$C_{\mathrm{total}_{\mathrm{disc}}}(\in)$	6046	6414.68	6212
C _{total} (€)	50,582	41,913.5	41,464

4.1 Performance analysis on case 1

The performance of proposed BFA in the multi-objective optimization of the STHE in case study 1 is shown in Table 2. Various parameters are analyzed in the method and have the optimal value for the parameter settings. The existing optimization method in the design of the heat exchanger is used to compare with the proposed BFA method to analyze the performance.

The simulation result of proposed BFA in the optimization of the STHE is shown in Table 2. The experimental result shows that the proposed BFA has the higher performance than the other existing methods. The proposed BFA has the lower cost compared to the other optimization technique. The optimal value of the BFA is shown in Table 2 to increase the efficiency and decrease the cost. The proposed BFA has the total cost value of 41,464 € compared to the existing method of ARGA that has the total cost value of 41,913 €. The proposed method has the advantages of the fast convergence and global search for optimal solution that helps to provide better performance. The proposed BFA method is various parameters to find the optimal design specification for multi-objective optimization. The heat transfer coefficient and the total cost of the heat exchanger are two important parameters considered for the optimization. The length of the tube is the important parameter that increases the flow and heat transfer in the tube side. The number of tubes is reduced to decrease the cost, and also heat transfer rate of efficiency is maintained by the design of the heat exchanger.

The capital cost and total discount operating cost are compared with the existing method, as shown in

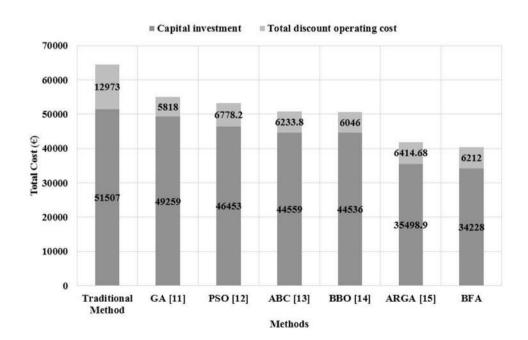


Fig. 2 The total cost of the proposed method

Table 3 Performance analysis of case study 2

Parameters	BBO [14]	ARGA [15]	BFA
<i>D</i> _s (m)	0.74	0.4	0.4
<i>L</i> (m)	1.199	0.71	0.72
<i>b</i> (m)	0.1066	0.154	0.132
<i>d</i> ₀ (m)	0.015	0.011	0.012
P_t (m)	0.0188	0.014	0.013
<i>C_I</i> (m)	0.0038	0.002	0.002
n _t	2	2	2
N _t	1061	635.229	652.124
<i>v_t</i> (m/s)	0.69	0.904	0.822
Re _t	2298	2300	2300
Pr _t	55.2	56.453	57.52
$h_t (W/m^2K)$	1251	1174.57	1263
f _t	0.05	0.049	0.05
$\Delta P_t(Pa)$	5109	5179.41	5189.73
$a_{\rm s}~({\rm m}^2)$	0.0158	0.012	0.012
D_e (m)	0.0149	0.008	0.008
$v_{\rm s}~({\rm m/s})$	0.432	0.524	0.562
Res	13,689	9073.64	9082.14
Pr _s	7.5	7.6	7.6
$h_{\rm s} ({\rm W}/{\rm m}^2{\rm K})$	1278	1857.58	1872
f _s	0.345	0.367	0.372
$\Delta P_{s}(Pa)$	15,275	9708	9827
$U (W/m^2K)$	317.75	336.128	321.26
S (m ²)	60.35	56.84	62.12
C _{inv} (€)	18,799	18,241.8	18,132.7
C _{annual} (€/year)	164.414	155.71	155.82
C _{total_{disc} (€)}	1010.25	956.79	937.84
$C_{\text{total}}(\in)$	19,810	19,198.6	18,824

Fig. 2. The proposed method has lower capital cost due to the minimization of the requirement in the manufacturing. The proposed method total cost is lower cost due to reduction of capital cost. The total cost of the proposed method design is low, and this is due to fast convergence and global search process of the proposed BFA method. The number of tubes is reduced in the proposed BFA design that majorly helps to reduce the cost of the exchanger.

4.2 Performance analysis on case 2

The proposed BFA is tested on case study 2 to analyze the performance, as shown in Table 3. Various design parameters are analyzed in the method for the optimum performance.

The proposed BFA is tested on case study 2 with different parameters and compared with the existing method, as shown in Table 3. This shows that the proposed BFA has higher performance compared to other existing methods in STHE optimization. The BFA method has fast convergence in the search process and able to analyze various parameters. This helps to find the optimal design for the heat exchanger with low cost and high efficiency. The proposed method decreases the cost compared to the other existing method in STHE. The total cost of BFA method is $18,824 \in$ compared to the existing ARGA method that has the cost of $19,198.6 \in$. The length of the tube and the number of tubes are increased by the proposed BFA design that helps to increase the heat transfer coefficient than the existing method.

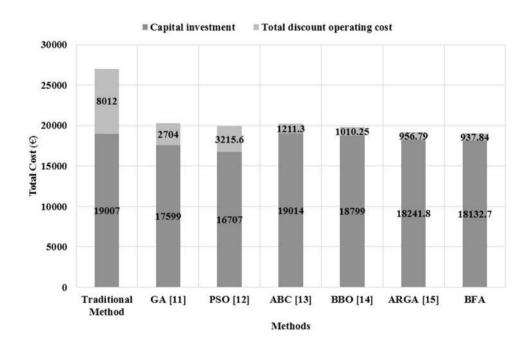


Fig. 3 The total discount

operating cost and capital

investment

The proposed BFA method of total discount operating cost and capital investment is shown in Fig. 3. This shows that the total cost of the proposed BFA design is lower than other existing methods. The proposed BFA method has the capital investment of $18,132 \in$, while existing method has the capital investment of $18,241.8 \in$. The proposed method decreases the total cost of the heat exchanger without affecting heat transfer efficiency of the system.

The proposed BFA has the higher performance in the economic design of the STHE system. The proposed BFA increases the efficiency of the method and decrease the cost of the system. Therefore, the proposed BFA method has a higher performance in the heat transfer efficiency and economic optimization of the design.

5 Conclusion

The cost of STHE is high, and the efficiency needs to be increased by applying the optimal design. Many existing methods are applied in the optimization of the STHE system to decrease the cost. In this research, BFA is applied to increase the performance and decrease the system cost. The proposed BFA method is evaluated on the two case studies and compared with the existing method to analyze the performance. The simulation result shows that the proposed BFA has the higher efficiency and lower cost for the STHE. The proposed BFA has the cost value of 18,824 €, while existing method ARGA method has the cost value of 19,198.6 €. The proposed BFA method has a heat transfer coefficient of 1089, while existing method has 1031.47. The proposed BFA method decreases the total cost of the heat exchanger and also increase the efficiency. In the both test case analysis, the proposed BFA method shows the lower cost in the design and high efficiency. The future work of this method involves in analyzing the different baffle cut designs for the STHE to increase the efficiency of the system.

Compliance with ethical standards

Conflict of interest The authors declare that they have no conflict of interest.

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