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Efficient Combinations of NOMA with Distributed Antenna Systems based on Channel Measurements for Mitigating Jamming Attacks

Joumana Farah¹, Eric Pierre Simon², Pierre Laly², Gauthier Delbarre²

Abstract—This study aims at proposing new efficient combinations of distributed antenna systems (DAS) with non orthogonal multiple access (NOMA) for combating the influence of harmful jamming on a downlink transmission system. A large set of practical channel measurements was performed in an indoor work environment in order to encompass a wide panoply of user positions, antennas, and jammer configurations. Then, three strategies were studied for the selection of subbands, antennas and transmit powers so as to alleviate the influence of jamming. First, a configuration where the paired users are served by a unique antenna was considered. Then, two other configurations were studied, where paired users are served by two different antennas. It was shown that, in these two strategies, under specific channel and power conditions, it is possible to allow both paired users to perform successive interference cancellation (SIC) to remove inter-user interference. The dual-SIC strategy, when applied with joint antenna transmission, presents a good robustness to jamming and yields important throughput gains, compared to the classical single-SIC scenario and single-antenna dual-SIC transmission.

Index Terms—NOMA, Distributed Antenna System, Antenna Selection, Subband Selection, Power Allocation, Channel Sounding.

I. INTRODUCTION

Distributed antenna systems (DAS) have recently driven a large amount of research works [1]–[6], for leveraging the performance of wireless communication systems. DAS relies on the deployment of the base station antennas in a distributed manner in each cell, rather than on a single tower at the cell center. The remote antennas, or remote radio heads (RRH), are connected to a baseband unit (BBU) by fiber optics links. Compared to centralized antenna systems (CAS), DAS allows an important reduction of local electromagnetic radiations and CO2 emissions, enhanced antenna-users radio links, and a more uniform coverage throughout the area. The advantages of DAS can even be better reaped by its association with appropriate signal multiplexing, such as non orthogonal multiple access (NOMA) [7]–[11]. NOMA has shown to be a prominent key in the upcoming generations of communication systems, for its high potentials in boosting the spectral efficiency and user fairness, as well as in reducing latency [12], compared to orthogonal multiple access (OMA) used in the fourth generation of mobile systems. Power-domain NOMA consists on multiplexing two or more users on the same frequency subband by allocating different power levels to users, based on their channel gains. At the receivers side, user separation, when possible, is performed using successive interference cancellation (SIC). To perform SIC, a user extracts its own signal by successively demodulating, decoding then re-encoding and subtracting the successively detected interfering signals, before proceeding to the demodulation and decoding of its own intended signal. Users that are not able to perform SIC directly proceed to their signal decoding, while treating other interfering signals as noise. Therefore, two separate sets of conditions are to be studied for the feasibility of NOMA [13] [14]: first, the conditions on the achievable rates at the respective users levels, from the information theory perspective, leading to the so-called SIC constraints. Then, the constraints on the received signals powers that allow the SIC applicability from a practical implementation perspective, called power multiplexing constraints (PMC): the signal to be decoded at a certain level must have a received power greater than that of all other interfering signals on the same subband, in order to guaranty SIC stability [15].

A few previous works have tackled the combination of NOMA with DAS. In [16], the outage probability of a NOMA-based cloud radio access network (C-RAN) is studied for the case of two users, both served by all RRHs. The results show the superiority of NOMA when compared to time division multiple access (TDMA). The work in [17] investigates the application of distributed NOMA for the uplink of a partially centralized C-RANs. In [18] [19], resource allocation is studied in NOMA-DAS for the context of mixed-traffic users. In [14], subband and power allocation in NOMA-DAS was tackled for the minimization of the downlink cell power under fixed user rates, and the study was then adapted to incorporate hybrid RRH-specific power constraints in [20]. It was shown that, under specific SIC and PMC constraints, the signals multiplexed on the same subband are sent from different RRHs, paired users can all cancel their respective interference, leading to the so-called "mutual SIC" (or "dual SIC") for the case of 2 users per subband. The latter was also applied for enhancing the spectral efficiency of Coordinated Multipoint (CoMP) systems [13]. However, none of these previous studies considered the impact of jamming on NOMA-DAS.

The jamming attacks consist in emitting a signal that covers the frequency bands employed by a wireless communication
The paper is organized as follows: In Section II, the NOMA-DAS system model is given with the proposed user-pairing scenarios. In Section III, we describe the measurement setup and environment. Then, in Section IV, we develop the SIC and PMC conditions for each user-pairing scenario. The proposed antenna and frequency selection technique is described in Section V. Performance evaluation of the resource allocation techniques is provided in Section VI, while Section VII concludes the paper.
study, a maximum of 2 RRHs are adaptively chosen to serve the paired users \(k_1\) and \(k_2\) on a subband. \(k_1\) and \(k_2\) are either served by the same RRH, as in Fig. 1a, or by two different RRHs, as in Fig. 1b. The first case will be referred to as single-SIC NOMA, since, as will be shown mathematically, when a unique RRH serves both paired users, only one of the latter can perform SIC. In the second case, two RRHs are used to transmit the two signals, leading to the possibility of both users performing SIC.

The conditions to allow dual-SIC NOMA were developed in [13] and [14] for the case of a jamming-free system. In this study, we develop these conditions for the jammed system, and show that even in the presence of jamming, dual-SIC is still possible, even though with harsher conditions. The dual-SIC case actually encloses two different possible scenarios: in the first one, referred to as dual-SIC NOMA with single-antenna transmission, each user receives its signal via one of the two involved RRHs only. In the second, referred to as dual-SIC NOMA with joint-antenna transmission, the signal of each user is jointly transmitted by both involved RRHs.

Let \(s_{k,r}\) be the signal transmitted from RRH \(r\) to user \(k\) with power \(P_{k,r}\). Note that, since only two users are considered for pairing on a subband, in the sequel, the indices \(k_1\) and \(k_2\) are respectively replaced by 1 and 2 in the power and channel variables. In the Single-SIC scenario, since the same RRH \(r\) transmits the signals of both paired users \(k_1\) and \(k_2\), the transmitted power-multiplexed signal is expressed by:

\[
x = \sum_{i=1}^{2} \sqrt{P_i} s_{i,r},
\]

where \(E[|s_{i,r}|^2] = 1, i = 1, 2\). The signal received at the level of each user can be written as:

\[
y_i = h_{i,r} x + h_{i,j} \sqrt{P_j} s_j + n_i, i = 1, 2,
\]

where \(s_j\) is the signal transmitted by the jammer (\(E[|s_j|^2] = 1\)) and \(n_i\) is an i.i.d. additive white Gaussian noise (AWGN) with zero mean and variance \(\sigma^2 = N_0 B / S\), where \(N_0\) is the noise power spectral density.

When dual-SIC NOMA with single-antenna transmission is used, the signal transmitted by RRH \(r_i\) (the RRH powering the signal of user \(i\)) is written as:

\[
x_i = \sqrt{P_{i,r}} s_{i,r},
\]

and the signal received by user \(i\) is now:

\[
y_i = \sum_{j=1}^{2} h_{i,r} x_j + h_{i,j} \sqrt{P_j} s_j + n_i, i = 1, 2.
\]

When the third transmission scenario is considered, i.e., dual-SIC NOMA with joint-antenna transmission, (3) and (4) are replaced by:

\[
x_i = \sum_{j=1}^{2} \sqrt{P_{j,r}} s_{j,r},
\]

and

\[
y_i = \sum_{j=1}^{2} h_{i,r} x_j + h_{i,j} \sqrt{P_j} s_j + n_i, i = 1, 2.
\]

The aim of this study is to dynamically select the best RRH (or couple of RRHs, depending on the pairing scenario) and subband, on which the two users \(k_1\) and \(k_2\) are paired, in such a way to maximize their sum-throughput, while taking into account the jammer presence. To this aim, after a detailed description of the channel measurements and a thorough study of the conditions inherent to the different user pairing scenarios, a novel RRH and subband selection technique is proposed in Section V. Also, the extension of the study to the multi-user pairing case is discussed therein.

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**III. Description of the Measurements**

In this section, we present the measurement campaign performed in the DAS context, on which we base our study to assess the different NOMA pairing combinations. We start by introducing the measurement equipment. Then, we describe the environment where measurements are carried out.
A. Measurement setup

Frequency-domain channel sounding measurements are performed in an indoor environment. A vector network analyzer (VNA) of type Agilent Technologies E5071C is used to sound the radio channel in an 18 MHz bandwidth centered at 3.5 GHz. In this frequency band, 1200 uniformly spaced frequency points, i.e., OFDM subcarriers, are sampled with a frequency spacing of 15 KHz, corresponding to the LTE/LTE Advanced mobile system parameters [27]. Each group of contiguous subcarriers constitutes one subband, which will be the basis of resource allocation in the following sections. The feeder cables used for the transmit and receive antennas are MegaPhase high performance RF coaxial cables. They are included in the VNA calibration to cancel their effect in the channel sounder. For each measurement, the VNA acquires 10 successive realizations of the whole frequency range, which are then averaged for the reduction of measurement noise. The transmitter is equipped with a patch antenna positioned at a height of 2m above ground level. The receiver is equipped with a EM-6116 omnidirectional antenna at 1.50m. Fig. 2 shows the transmitter and receiver in the considered environment.

Fig. 2: Practical setup for channel measurements

B. Measurement Environment

The measurements were conducted in the first floor of a typical indoor building, consisting of two rows of offices and laboratories, situated on both sides of a 35m long corridor. A map of the environment is shown in Fig. 3. All offices and lab rooms are separated by plaster walls, except for two concrete walls shown in the figure. The channels were sounded in the corridor (numbered #1) and 11 different selected rooms, numbered from #2 to #12. The set of measurements is obtained by moving the transmitter and receiver at different positions to constitute a DAS. Each position of the transmitter corresponds to an RRH, and each position of the receiver corresponds to a given user (U). The positions of the RRHs and users are specified as follows: a first index $i$ identifies the room, and a second index $j$ indicates the position within this room, yielding $\text{RRH}_{ij}$ and $\text{U}_{ij}$. The orientation of the RRH patch antenna is shown by arrows. In order to investigate several scenarios with different jammer positions, five of the transmitter positions are dedicated to the jammer (J) and spotted in red in Fig. 3.

IV. Analysis of the User-Pairing Scenarios

In this section, we derive the SIC conditions and power multiplexing constraints for the three user pairing scenarios: Single-SIC, dual-SIC with single antenna transmission, and dual-SIC with joint antenna transmission.

A. Single-SIC NOMA

In this first scenario, the signals of the two paired users $k_1$ and $k_2$, denoted respectively by $s_1$ and $s_2$ for simplicity, are transmitted by the same RRH $r \in \mathcal{R}$. Let $SINR^{(k_1)}_{s_2}$ the necessary Signal to Interference and Noise Ratio (SINR) at the level of user $k_1$ for decoding the signal $s_2$ of $k_2$. It is expressed as:

$$SINR^{(k_1)}_{s_2} = \frac{P_{2,r}h_{1,r}}{P_{1,r}h_{1,r} + P_J h_{1,j} + \sigma^2}. \quad (7)$$

Similarly, let $SINR^{(k_2)}_{s_2}$ the necessary SINR at the level of user $k_2$ for decoding $s_2$. It is given by:

$$SINR^{(k_2)}_{s_2} = \frac{P_{2,r}h_{2,r}}{P_{1,r}h_{2,r} + P_J h_{2,j} + \sigma^2}. \quad (8)$$

It is known, from the theory behind NOMA [8] [13] [14], that $k_1$ can successfully decode and cancel the interfering signal $s_2$ if:

$$SINR^{(k_1)}_{s_2} \geq SINR^{(k_2)}_{s_2}. \quad (9)$$

By developing and arranging $SINR^{(k_1)}_{s_2} - SINR^{(k_2)}_{s_2}$, it can be verified that (9) leads to the following condition:

$$P_J P_{2,r}(h_{1,r}h_{2,j} - h_{2,r}h_{1,j}) + \sigma^2 P_{2,r}(h_{1,r} - h_{2,r}) \geq 0. \quad (10)$$

Since, in practical interference-limited systems, additive noise is generally negligible with respect to interfering signals, the second term in (10) is negligible towards the first; therefore, (10) reduces to:

$$h_{1,r}h_{2,j} \geq h_{2,r}h_{1,j}. \quad (11)$$

From the practical perspective, in order to ensure SIC stability, i.e. minimize the chances of error propagation in SIC, since signal $s_2$ is to be decoded first, it must be the dominant one so that the receiver of $k_1$ can distinguish it from interference and background noise. In the presence of jamming, if the received power of $s_1$ and that of the jammer’s signal $s_J$ add up to a more powerful combined signal at $k_1$, their resulting interference will become dominant with respect to the signal $s_2$ received by $k_1$, therefore threatening its successful decoding. For this reason, the PMC for the decoding of $s_2$ at the level of $k_1$ is:

$$P_{2,r}h_{1,r} \geq P_{1,r}h_{1,r} + P_J h_{1,j}. \quad (12)$$

Using the same reasoning, by interchanging $k_1$, $k_2$ and $s_1$, $s_2$ in (7), (8), (9), and (10), it can be verified that $k_2$ can successfully decode and cancel the signal $s_1$ if:

$$h_{2,r}h_{1,j} \geq h_{1,r}h_{2,j}. \quad (13)$$

Consequently, it is clear that when conditions (11) and (12) are verified, only user $k_1$ can perform SIC, i.e., $k_2$ cannot. In...
this case, the normalized rates (spectral efficiencies) achieved by the two users are respectively:

\begin{align}
R_{k1} &= \log_2(1 + \frac{P_{1,r}h_{1,r}}{P_{j1}h_{1,j} + \sigma^2}), \\
R_{k2} &= \log_2(1 + \frac{P_{2,r}h_{2,r}}{P_{j2}h_{2,j} + \sigma^2}).
\end{align}

When (13) is verified, \( k_2 \) performs SIC, while \( k_1 \) does not. The corresponding PMC becomes:

\begin{align}
P_{1,r}h_{2,r} &\geq P_{2,r}h_{2,r} + P_jh_{2,j}. \quad (16)
\end{align}

The achieved rates are in this case:

\begin{align}
R_{k1} &= \log_2(1 + \frac{P_{1,r}h_{1,r}}{P_{j1}h_{1,j} + \sigma^2}), \\
R_{k2} &= \log_2(1 + \frac{P_{2,r}h_{2,r}}{P_{j2}h_{2,j} + \sigma^2}).
\end{align}

Note that when \( P_j = 0 \), conditions (10) and (12) reduce respectively to \( h_{1,r} \geq h_{2,r} \) and \( P_{2,r} \geq P_{1,r} \), which correspond to the SIC and PMC conditions in the classical jamming-free NOMA transmission [7] [8]. Also, the rates in equations (14), (15), (17), (18) become devoid of the jamming power terms. In practice, based on the received measurements of \( P_jh_{1,j} \) and \( P_jh_{2,j} \) (as explained in Section II), the BBU calculates the ratio: \( h_{2,j}/h_{1,j} = P_{j2}/P_{j1} \). If \( h_{2,j}/h_{1,j} \geq h_{2,r}/h_{1,r} \), the BBU performs power allocation while considering \( k_1 \) as the strong user on the considered subband, i.e., the user performing SIC, and \( k_2 \) as the weak user. Otherwise, \( k_2 \) is considered as the strong user.

**B. Dual-SIC NOMA with Single Antenna Transmission (Dual-SIC-SAT)**

In this pairing scenario, the two users \( k_1 \) and \( k_2 \) receive their signals \( s_1 \) and \( s_2 \) from two different RRHs \( r_1 \in \mathcal{R} \) and \( r_2 \in \mathcal{R} \), respectively, as shown in Fig. 1b. Only one selected RRH participates to transmit a user’s signal. In [14], where such a transmission scenario was studied in the absence of jamming, it was shown that, under specific channel and transmit power conditions, both users \( k_1 \) and \( k_2 \) are able to perform SIC to cancel their respective signals. The question that arises now is whether this mutual SIC can still take place in spite of the jamming, and if yes, under which conditions. In this scenario, the SINR expressions in (7) and (8) become respectively:

\begin{align}
SINR_{k1} &= \frac{P_{2,r}h_{2,r} + P_jh_{1,j} + \sigma^2}{P_{1,r}h_{1,r} + P_jh_{1,j} + \sigma^2}, \\
SINR_{k2} &= \frac{P_{2,r}h_{2,r}}{P_{1,r}h_{1,r} + P_jh_{1,j} + \sigma^2}.
\end{align}

\( k_1 \) can perform SIC if the inequality \( SINR_{k1} - SINR_{k2} \geq 0 \) holds. After rearranging its terms and neglecting the additive noise, this inequality is shown to be equivalent to:

\begin{align}
P_{1,r}P_{2,r}(h_{1,r}h_{2,r} - h_{1,r}h_{2,r}) + \frac{E}{F} \geq 0.
\end{align}

The condition for \( k_2 \) to perform SIC is \( SINR_{k1} - SINR_{k2} \geq 0 \), which leads to:

\begin{align}
P_{1,r}P_{2,r}(h_{1,r}h_{2,r} - h_{1,r}h_{2,r}) + \frac{E}{G} \geq 0.
\end{align}

Note that, if the common factor \( E \) in (21) and (22) is negative, i.e.,

\[ h_{2,r} \leq \frac{h_{2,r}}{h_{1,r}}. \]
$F$ and $G$ cannot be simultaneously positive, since:

$$(F \geq 0) \& (G \geq 0) \iff \left( \frac{h_{2,r_2}}{h_{1,r_2}} \geq \frac{h_{2,r_1}}{h_{1,r_1}} \right) \& \left( \frac{h_{2,r_1}}{h_{1,r_1}} \leq \frac{h_{2,r_2}}{h_{1,r_2}} \right)$$

$$\iff \frac{h_{2,r_2}}{h_{1,r_2}} \leq \frac{h_{2,r_1}}{h_{1,r_1}} \iff h_{2,r_2} \leq h_{1,r_2}.$$  \hspace{1cm} (23)

In other words, if $E \leq 0$, dual SIC between $k_1$ and $k_2$ is not possible. Conversely, if

$$\frac{h_{2,r_2}}{h_{1,r_2}} \leq \frac{h_{2,r_1}}{h_{1,r_1}}$$

then (23) can be true, under specific jamming conditions. Also, when $P_J = 0$, by inspecting (21) and (22), one can see that the dual SIC condition between $k_1$ and $k_2$ simply reduces to condition (24), as was the case in [14].

The PMCs at the levels of users $k_1$ and $k_2$ are respectively:

$$P_{1,r_2}h_{1,r_2} \geq P_{1,r_1}h_{1,r_1} + P_J h_{1,j},$$

$$P_{1,r_1}h_{2,r_2} \geq P_{2,r_2}h_{2,r_2} + P_J h_{2,j}.$$ 

The two above PMCs can be combined into the following one:

$$\frac{h_{1,r_1}}{h_{1,r_2}} + \frac{P_J h_{1,j}}{P_{1,r_1}h_{1,r_2}} \leq \frac{h_{2,r_2}}{h_{2,r_1}} \iff \frac{h_{2,r_2}}{h_{2,r_1}} \leq \frac{P_{2,r_2}}{P_{1,r_1}} \frac{h_{2,r_2}}{h_{2,r_1}}.$$  \hspace{1cm} (25)

When $P_J = 0$, (25) becomes simply:

$$\frac{h_{1,r_1}}{h_{1,r_2}} \leq \frac{P_{2,r_2}}{P_{1,r_1}} \frac{h_{2,r_2}}{h_{2,r_1}}.$$  \hspace{1cm} (26)

which corresponds to the jamming-free context [14]. More importantly, when inspecting (24) and (26), it can be clearly seen that, in the jamming-free case, when (24) is not verified, i.e. dual SIC is not possible between $k_1$ and $k_2$ with the current antenna selection (resp. $r_1$ and $r_2$), a simple RRH inversion is sufficient to enable dual SIC, i.e. $k_1$ is served by $r_2$ and $k_2$ by $r_1$. Unfortunately, this is no longer true in the presence of jamming, as shown by (23) and (25). In other words, when (24) is not verified, while $P_J \neq 0$, one can still consider inverting the RRHs to enlarge the ensemble of tested RRH pairs. However, there is no guarantee that this inversion will lead to a valid RRH pair. Finally, when (23) and (25) are both respected, the achieved user rates are:

$$R_{k_1} = \log_2(1 + \frac{P_{1,r_1}h_{1,r_1}}{P_{1,r_1}h_{1,r_1} + \sigma^2})$$

$$R_{k_2} = \log_2(1 + \frac{P_{2,r_2}h_{2,r_2}}{P_{2,r_2}h_{2,r_2} + \sigma^2}).$$  \hspace{1cm} (27)

C. Dual-SIC NOMA with Joint Antenna Transmission (Dual-SIC-JAT)

When joint transmission is considered on top of Dual-SIC NOMA, the two selected RRHs $r_1$ and $r_2$ participate in the transmission of each of the two signals addressed to $k_1$ and $k_2$. In this case, the SINR expressions become:

$$\text{SINR}_{k_1}^{(k_1)} = \frac{P_{2,r_2}h_{1,r_1} + P_{2,r_2}h_{1,r_2}}{P_{1,r_1}h_{1,r_1} + P_{1,r_1}h_{1,r_2} + P_J h_{1,j} + \sigma^2},$$

$$\text{SINR}_{k_2}^{(k_2)} = \frac{P_{2,r_2}h_{2,r_2} + P_{2,r_2}h_{2,r_2}}{P_{1,r_1}h_{2,r_1} + P_{1,r_1}h_{2,r_2} + P_J h_{2,j} + \sigma^2}. \hspace{1cm} (29)$$

The condition $\text{SINR}_{k_1}^{(k_1)} - \text{SINR}_{k_2}^{(k_2)} \geq 0$, necessary for $k_1$ to perform SIC, amounts to:

$$\left( h_{1,r_1}h_{2,r_2} - h_{1,r_2}h_{2,r_1} \right) (P_{2,r_1}P_{1,r_2} - P_{2,r_2}P_{1,r_1}) + P_J \left( P_{2,r_2}h_{1,r_1} + P_{2,r_2}h_{1,r_2} \right) h_{2,J} \geq 0 \hspace{1cm} \text{or}$$

$$-P_J \left( P_{2,r_2}h_{2,J} + P_{2,r_2}h_{2,J} \right) h_{1,J} \geq 0.$$  \hspace{1cm} (31)

Also, the necessary condition for $k_2$ to perform SIC is:

$$h_{2,r_1}h_{1,r_2} - h_{2,r_2}h_{1,r_1} \right) (P_{1,r_1}P_{2,r_2} - P_{1,r_2}P_{2,r_1}) + P_J \left( P_{1,r_1}h_{2,J} \right) h_{1,J} \geq 0.$$  \hspace{1cm} (32)

The PMCs at the levels of users $k_1$ and $k_2$ are respectively:

$$P_{2,r_1}h_{1,r_1} + P_{2,r_2}h_{1,r_2} \geq P_{1,r_1}h_{1,r_1} + P_{1,r_2}h_{1,r_2} + P_J h_{1,j},$$

$$P_{1,r_1}h_{2,r_2} + P_{1,r_2}h_{2,r_2} \geq P_{2,r_1}h_{2,r_1} + P_{2,r_2}h_{2,r_2} + P_J h_{2,j}.$$  \hspace{1cm} (33)

It is therefore clear that any power allocation scheme must abide by the four constraints (31), (32), (33) and (34), since they all include power variables. However, the SIC constraints (31) and (32) are non linear in $P_{k,r}$, which may hinder the problem feasibility. For this sake, in the sequel, we propose a simplification of the constraints.

The PMCs (33) and (34) can be rewritten as:

$$P_{2,r_2} - P_{1,r_1})h_{1,r_2} \geq (P_{1,r_1} - P_{2,r_1})h_{1,r_1} + P_J h_{1,j},$$

$$P_{1,r_1} - P_{2,r_1})h_{2,r_2} \geq (P_{2,r_2} - P_{1,r_2})h_{2,r_2} + P_J h_{2,j}.$$  \hspace{1cm} (35)

By inspecting (35) and (36), it can be deduced that the factors $P_{1,r_1} - P_{2,r_1}$ and $P_{2,r_2} - P_{1,r_2}$ always have the same sign. When $P_{1,r_1} - P_{2,r_1} \geq 0$ and $P_{2,r_2} - P_{1,r_2} \geq 0$, $P_{1,r_1}P_{2,r_2} \geq P_{1,r_2}P_{2,r_1}$. Also, (35) and (36) combine to:

$$\frac{h_{2,r_2}}{h_{2,r_1}} \geq \frac{P_J h_{2,j}}{P_{1,r_1}h_{1,r_2} - h_{1,r_1}(P_{2,r_2} - P_{1,r_1})}.$$  \hspace{1cm} (37)

Consequently, when the PMCs (33) and (34) are verified, $h_{2,r_2}/h_{2,r_1} \leq h_{1,r_1}/h_{1,r_2}$, and since $P_{2,r_1}P_{1,r_2} - P_{1,r_1}P_{2,r_2} \leq 0$, the common term $(h_{1,r_1}h_{2,r_2} - h_{1,r_2}h_{2,r_1}) (P_{2,r_1}P_{1,r_2} - P_{2,r_2}P_{1,r_1})$ in (31) and (32) is positive.

Similarly, when $P_{1,r_1} - P_{2,r_1} \leq 0$ and $P_{2,r_2} - P_{1,r_2} \leq 0$, $P_{1,r_1}P_{2,r_2} \leq P_{1,r_2}P_{2,r_1}$, (35) and (36) combine to:

$$\frac{h_{1,r_2}}{h_{1,r_1}} - \frac{P_J h_{1,j}}{h_{1,r_1}P_{2,r_2} - P_{1,r_2}} \leq \frac{P_{2,r_1} - P_{2,r_2}}{P_{2,r_1} - P_{2,r_2}} \leq \frac{h_{2,r_2}}{h_{2,r_1}} \leq \frac{h_{2,r_2}}{h_{2,r_1}} (P_{2,r_2} - P_{1,r_2}).$$

This leads to $h_{1,r_2}/h_{1,r_1} \leq h_{2,r_2}/h_{2,r_1}$, and since $P_{2,r_1}P_{1,r_2} - P_{1,r_1}P_{2,r_2} \geq 0$, the common term in (31) and (32) is also positive. Therefore, based on the positivity of this common
term, it is removed from the PMC constraints, and the four constraints (31), (32), (33) and (34) are finally re-written as:

\[
\begin{align*}
A(P)h_{2,j} - B(P)h_{1,j} &\geq 0, \\
C(P)h_{1,j} - D(P)h_{2,j} &\geq 0, \\
A(P) - D(P) - P_jh_{1,j} &\geq 0, \\
C(P) - B(P) - P_jh_{2,j} &\geq 0.
\end{align*}
\] (37)

\(A(P), B(P), C(P)\) and \(D(P)\) are linear functions of the power variables. Note that this simplification may reduce the search space of the power variables; however, the linearity of the constraints greatly counteracts this effect from the feasibility perspective.

When the constraints in (37) are verified, the achieved user rates are:

\[
\begin{align*}
R_{k_1} &= \log_2(1 + \frac{P_{1,r_1}h_{1,r_1} + P_{1,r_2}h_{1,r_2}}{P_jh_{1,j} + \sigma^2}), \\
R_{k_2} &= \log_2(1 + \frac{P_{2,r_1}h_{2,r_1} + P_{2,r_2}h_{2,r_2}}{P_jh_{2,j} + \sigma^2}).
\end{align*}
\] (38) (39)

V. Antenna and Frequency Selection

The selection of the optimum transmitting RRH (or RRH couple) and subband, for a particular user couple, is highly dependent on the transmit powers. Therefore, we start by describing the power allocation (PA) strategy for each user pairing. In the single-SIC NOMA scenario, the PA problem on a particular subband is expressed as:

\[
\max_{\{p_{1,r_1}, p_{2,r_2}\}} R_{k_1} + R_{k_2},
\] (40)

such that:

\[
\begin{align*}
&\{(12) \text{ verified if (11) is true}\}, \\
&\{(16) \text{ verified if (13) is true}\}, \\
&P_{1,r_1} + P_{2,r_2} \leq P_L.
\end{align*}
\] (40a) (40b) (40c)

\(P_L\) is the maximum power budget of an RRH. 

\(R_{k_1}\) and \(R_{k_2}\) are expressed by (14) and (15) respectively, if (11) is true, or by (17) and (18), respectively, if (13) is true. In the dual-SIC NOMA with single antenna transmission scenario, when (23) is verified, the PA problem is formulated as:

\[
\max_{\{p_{1,r_1}, p_{2,r_2}\}} R_{k_1} + R_{k_2},
\] (41)

such that:

\[
\begin{align*}
&\{(25) \text{ verified}\}, \\
&P_{1,r_1} \leq P_L/2, \\
&P_{2,r_2} \leq P_L/2.
\end{align*}
\] (41a) (41b) (41c)

\(R_{k_1}\) and \(R_{k_2}\) are now expressed by (27) and (28) respectively. As shown in constraints (41b) and (41c), the power budget of each involved RRH is set to \(P_L/2\), so that the total power budget of the RRHs powering the subband is kept equal to that of the single RRH involved in the single-SIC scenario. This allows a fair comparison between the different pairing schemes.

When dual-SIC NOMA is applied with joint antenna transmission, the PA problem becomes:

\[
\max_{\{p_{1,r_1}, p_{2,r_2}, p_{1,r_2}, p_{2,r_1}\}} R_{k_1} + R_{k_2},
\] (42)

such that:

\[
\begin{align*}
&\{(37) \text{ verified}\}, \\
&P_{1,r_1} + P_{2,r_2} \leq P_L/2, \\
&P_{2,r_1} + P_{2,r_2} \leq P_L/2.
\end{align*}
\] (42a) (42b) (42c)

\(R_{k_1}\) and \(R_{k_2}\) are given by (38) and (39) respectively.

We now move to the description of the general strategy for subband and RRH selection, for a couple of users \(k_1\) and \(k_2\). In the case of single-SIC NOMA, any couple \((r,s)\) of RRH \(r\) and subband \(s\) either verifies (11) or (13), and thus constitutes a possible candidate. Therefore, problem (40) is resolved for each couple \((r,s)\). The couple that yields the highest throughput is then used to serve \(k_1\) and \(k_2\). In Dual-SIC NOMA with single antenna transmission, only the triplets \((r_1,r_2,s)\), with \(r_1 \neq r_2\), and verifying (23), are tested by resolving problem (41). \(k_1\) and \(k_2\) are then assigned the triplet \((r_1,r_2,s)\) that yield the maximum throughput.

When joint antenna transmission is considered with Dual-SIC NOMA, problem (42) is resolved for all triplets \((r_1,r_2,s)\) such that \(r_1 \neq r_2\). Note that, in the three user pairing strategies, some of the candidates \((r,s)\) or \((r_1,r_2,s)\) do not yield valid solutions (i.e. the PA constraints cannot be met with positive power variables) and are eliminated. Also, the PA in Dual-SIC-JAT generally necessitates a higher complexity than that of Dual-SIC-SAT and Single-SIC, since four power variables are to be determined instead of two.

To determine the solution of each one of the problems (40), (41) and (42), one could use Lagrangian optimization. However, since multi-constraint problems with non-linear objective functions are at stake, we directly resort to the use of the Optimization Toolbox in Matlab to find the power allocation solutions.

Note that, while we focused our study on a particular user pair, in a practical system a large number of active users are generally present. Therefore, different user pairs are assigned separate subbands powered by one or two RRHs. Moreover, each user position considered in the channel measurements conducted in our study can be considered as a different user in a multi-user system. Such setup would be a generalization of the current study, where an assignment algorithm needs to be implemented to jointly perform user pairing, RRH and subband selection, and power allocation to all active users. Such a complete solution can be implemented by incorporating, within the current study, either a greedy algorithm [14] or a matching technique [19], in the DAS context. However, this is out of the scope of the current study, where the main focus is on the best RRH-subband selection to counteract the jamming effect.

The study, conducted in this work for the case of two-user clusters, can be extended to larger cluster sizes. For instance, if one considers clusters of three users per subband, mutual SIC between all cluster members would require two SIC processes at each user level (to cancel the interference of each of the two respective users), with two corresponding PMCs. This would amount to a total of 12 constraints instead of 4 in (37). Also, for each possible RRH and subband candidate, 8 decoding
orders need to be tested at the BBU (2 at the level of each user). The one that yields the best sum-throughput is then signaled by the BBU to the users through the RRHs. As was shown in [13], by the complete mutual SIC, and in contrast with traditional SIC procedures (where clustered users’ signals are powered by a unique RRH), successfully adding a user to a NOMA cluster is virtually equivalent to enlarging the system bandwidth. Therefore, a greater number of accommodated users per subband will translate into a higher performance in mutual SIC systems. However, this enlargement incurs a significant increase in complexity at the BBU level as well as at the user equipment levels, with a higher risk of error propagation at the SIC receivers. For all these reasons, we chose to limit the cluster size to two in this study. However, its extension to larger clusters could constitute an interesting perspective to be investigated in a future work.

VI. PERFORMANCE EVALUATION

The different resource allocation methods presented in this study are evaluated for the case of $S = 12$ subbands, where each subband is equivalent to 100 OFDM subcarriers. The noise power spectral density is $N_0 = 4 \times 10^{-18}$ mW/Hz. For each possible user couple $(k_1, k_2)$, the antenna and frequency selection technique is applied separately for each of the three DAS-NOMA pairing scenarios.

Fig. 4 shows examples of the measured transfer functions for five different combinations of users and RRHs. As expected, when the transmitter and receiver are in the same room (red curve), the line of sight dominates in the signal transmission which yields an almost flat transfer function with a high amplitude. The blue curve corresponds to the case where the transmitter and receiver are at the opposite ends of a row of rooms. In this case, besides suffering the large distance, the signal has to cross the concrete walls, yielding low amplitudes and highly frequency-selective fading. The black curve also corresponds to a scenario giving low channel amplitudes, where the transmitter antenna points towards the opposite direction of the receiver (see Fig. 3). The green and magenta curves correspond to a more moderate fading in comparison to the blue and black curves, since the user and transmitter are taken in separate but close rooms.

In Fig. 5, we represent the sum-throughput $(R_{k_1} + R_{k_2})$ averaged over all possible user couples considered in the study, while varying the jamming power $P_J$, for the case of a total transmit power $P_L = 1$W. The results show that, for a low jamming power (smaller than 1mW), both dual SIC strategies outperform Single-SIC. This observation is in line with the results obtained in [13] [14] in the jamming-free context. However, when $P_J$ increases, Single-SIC outperforms Dual-SIC-SAT with a throughput gain that can reach 7.7 bps/Hz at $P_J = 10$W. The quick performance degradation of Dual-SIC-SAT can be partly explained by the subtractive term in the right-hand part of inequation (25): When $P_J$ increases, this constraint becomes very hard to respect, which hinders the feasibility of problem (41). Therefore, the number of valid candidate antennas and subbands decreases quickly with $P_J$. At the same time, constraints (12) and (16) are easier to respect, leading to a higher number of possible candidates in Single-SIC. As for Dual-SIC-JAT, it constitutes the best user pairing strategy, with a good immunity to jamming power. Indeed, it outperforms both Single-SIC and Dual-SIC-SAT, with a performance gain over Single-SIC of 3.8 bps/Hz at $P_J = 0.1$W and that decreases with $P_J$. It should be noted that, even though we presented results with $P_J$ reaching a maximum value of 10W, the majority of commercial jammers are low-power jammers that usually operate in the range of a few watts, and seldom exceed 5W.

In Fig. 6, we represent the average sum-throughput obtained by varying the total system transmit power, for $P_J = 0.1$ and 1W. One can observe how the performance gain of Dual-SIC-JAT over Single-SIC increases with $P_L$, for example from 1.9 bps/Hz at $P_L = 0.5$W to 3.7 bps/Hz at $P_L = 10$W, for $P_J = 1$W. When $P_J = 0.1$W, the performance loss of Dual-SIC-SAT vs. Single-SIC decreases from 6 bps/Hz at $P_L = 0.5$W to 2.8 bps/Hz at $P_L = 10$W.

Table I shows examples of the obtained optimum sum-throughput for two different configurations of users and jam-
In Table II, the influence of the jammer deployment on a fixed user set (U51, U101) is shown, for the Dual-SIC-JAT method, with $P_J = 1\text{W}$ and $P_L = 1\text{W}$. Among the 5 jammer positions, the J4 position turns out to be the most dramatic one for this user couple. Indeed, J4 is relatively close to both users and the worst throughput is achieved, while the best RRHs selected to counteract its effect are RRH51 and RRH121, one in the same room as U51 and the other rather away from both users. A close maximum throughput is achieved when J2 is deployed, which is very close to U51. In this case, the two selected RRHs are in the same room as the other user. The jammer that has the least incidence on throughput is J3, since it is relatively far from both users. In this case, each of the selected RRHs is in the same room as one of the users. The same couple of RRHs is selected when jammer J1 is deployed, which is also relatively far from the users. This analysis shows the importance of taking into account the jammer position in the RRH and subband selection procedure, since particular RRH patterns appear depending on the jammer-users configuration.

<table>
<thead>
<tr>
<th>$k_1, k_2, J$</th>
<th>SIC</th>
<th>Rate</th>
<th>RRHs</th>
<th>Subband</th>
</tr>
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<tr>
<td>U12, U41, J4</td>
<td>Single</td>
<td>11.2</td>
<td>RRH41</td>
<td>12</td>
</tr>
<tr>
<td></td>
<td>Dual-SIC</td>
<td>8.6</td>
<td>RRH41, RRH102</td>
<td>12</td>
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<tr>
<td></td>
<td>Dual-JAT</td>
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<td>RRH12, RRH41</td>
<td>7</td>
</tr>
<tr>
<td>U51, U101, J3</td>
<td>Single</td>
<td>14.8</td>
<td>RRH51</td>
<td>8</td>
</tr>
<tr>
<td></td>
<td>dual SAT</td>
<td>17.5</td>
<td>RRH102, RRH91</td>
<td>5</td>
</tr>
<tr>
<td></td>
<td>dual JAT</td>
<td>23.6</td>
<td>RRH102, RRH51</td>
<td>5</td>
</tr>
</tbody>
</table>

TABLE I: Examples of the obtained optimum rates [bps/Hz], RRHs and subbands, for $P_J = 0.2\text{W}$ (first example) and $1\text{W}$ (second example) and $P_L = 1\text{W}$

Fig. 6: Sum-throughput versus $P_L$ for $P_J = 0.1$ and $1\text{W}$

TABLE II: Optimum rates [bps/Hz], RRHs and subbands, obtained by Dual-SIC-JAT, for a particular user couple, with the different Jammer positions, for $P_J = 1\text{W}$ and $P_L = 1\text{W}$.

VII. CONCLUSION

In this paper, three user-pairing strategies were proposed in the NOMA-DAS setting, in the aim of alleviating the influence of a jammer on downlink transmissions. Practical channel measurements were taken in an indoor environment, with a large number of users, antennas, and jammer positions. The theoretical foundations were developed for the three pairing strategies and incorporated in a subband and RRH selection technique. The results of this study show that, in contrast with those of previous works performed in a jamming-free NOMA-DAS context, the best pairing strategy greatly depends on the users positions and jamming conditions (jammer position and power). An adaptive choice between the three strategies should therefore be conducted so as to optimize the system performance. This study, performed in the DAS context, can also be directly applied to CoMP transmissions in multicell systems using joint transmission (JT) or dynamic point selection (DPS) [28].

REFERENCES


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