

REVIEW



Esophageal and transpulmonary pressure in the clinical setting: meaning, usefulness and perspectives

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Abstract

Purpose: Esophageal pressure (Pes) is a minimally invasive advanced respiratory monitoring method with the potential to guide management of ventilation support and enhance specific diagnoses in acute respiratory failure patients. To date, the use of Pes in the clinical setting is limited, and it is often seen as a research tool only.

Methods: This is a review of the relevant technical, physiological and clinical details that support the clinical utility of Pes.

Results: After appropriately positioning of the esophageal balloon, Pes monitoring allows titration of controlled and assisted mechanical ventilation to achieve personalized protective settings and the desired level of patient effort from the acute phase through to weaning. Moreover, Pes monitoring permits accurate measurement of transmural vascular pressure and intrinsic positive end-expiratory pressure and facilitates detection of patient–ventilator asynchrony, thereby supporting specific diagnoses and interventions. Finally, some Pes-derived measures may also be obtained by monitoring electrical activity of the diaphragm.

Conclusions: Pes monitoring provides unique bedside measures for a better understanding of the pathophysiology of acute respiratory failure patients. Including Pes monitoring in the intensivist's clinical armamentarium may enhance treatment to improve clinical outcomes.

Keywords: Esophageal pressure, Acute respiratory failure, Acute respiratory distress syndrome, Physiologic monitoring, Mechanical ventilation

Introduction

Esophageal pressure (Pes) measurement is a minimally invasive monitoring method used to assess respiratory mechanics. In acute respiratory failure patients, Pes tracings can be used to individually understand, define and evaluate the pathophysiological mechanisms of respiratory failure, to titrate invasive and non-invasive respiratory and pharmacological support and to follow the patient's

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clinical course. Nonetheless, Pes monitoring is still seldom used in the clinical setting; rather, it remains widely seen as a research tool. In an effort to clarify the usefulness of Pes measurement in the clinical setting, we address here the relevant technical, physiological and clinical details of this monitoring method to facilitate a better understanding of the information that can be obtained by bedside Pes measurement. Two recent reviews have dealt with the same topic [1, 2]. In our review we include updated information from the most recent literature and provide clinical threshold values for transpulmonary pressure (P_L) as reference to guide ventilation settings. We also include an extensive analysis on both the clinical value of transmural pulmonary vascular pressure measurements and the correlation between Pes and the electrical activity of the diaphragm. A number of case-scenarios in which Pes monitoring could be of help at the bedside are described (Table 1), and a video on the practical use of the technique is provided in the Electronic Supplementary Material (ESM).

Measurement of Pes

The catheter–balloon system: positioning and calibration

The most common technique for measuring Pes employs an esophageal balloon filled with air, connected to a long thin catheter. The first generation of custom-made esophageal balloons was primarily used for research purposes; since then, several types of second-generation balloons have been developed in the last decade which are currently available for bedside clinical use. Esophageal balloon catheters can be connected to dedicated monitoring devices, to accessory pressure ports of mechanical ventilators or to pressure transducers of multi-parametric monitors.

To obtain reliable Pes measurements, the esophageal balloon must be placed in an appropriate position and the balloon inflated with an adequate volume of air. An under-filled balloon does not properly transmit the Pes, whereas an over-filled balloon can over-estimate the pressure [3]. The “optimal” air filling volume depends on the design, dimensions, geometry and material of the esophageal balloon, which in turn affect its mechanical properties. The six most common commercially available esophageal catheters have recently been tested in vitro at an external pressure ranging from 0 to 30 cmH₂O. All of the catheters tested were found to accurately measure the surrounding pressure, but the optimal filling volume differed substantially among the catheters [4]. In addition, the minimum volume required for valid measurements was greater than those recommended previously and was dependent on the surrounding pressure [4]. Another study similarly found that the filling volume varied with the tested catheters and that the volume should be increased in the presence of high external pressure [5]. Physicians must account for these technical issues. In clinical practice, a

simple method to determine the optimal filling volume is to progressively inflate the balloon, within the catheter-specific adequate range of filling volumes, finally selecting the lowest volume associated with the largest tidal swings (inspiratory to expiratory) of Pes [4, 6].

Method to insert the catheter and validate Pes during mechanical ventilation

A video describing the insertion and interpretation of the Pes is provided in the ESM. After deflating the esophageal balloon and securing it with a three-way stopcock, it is introduced into the esophagus transorally or transnasally. The esophageal catheter is then gently advanced to a depth of about 55 cm to reach the stomach and inflated with the minimum recommended volume [4, 5]. The intragastric position of the catheter is confirmed by a positive pressure deflection during gentle external manual epigastric compression. Subsequently, the catheter is progressively withdrawn into the esophagus. Esophageal positioning is suggested by the appearance of cardiac artifacts on the pressure tracings and by the change from intra-abdominal to intra-thoracic pressure patterns. Placement of the esophageal balloon in the lower two thirds of the intra-thoracic esophagus has been suggested as a way to limit possible pressure artifacts due to non-homogeneous esophageal compression by external structures [7].

When spontaneous inspiratory efforts are present, the conventional test to validate the Pes measurement is to compare the simultaneous negative deflections of airway and esophageal pressures during an end-expiratory occlusion maneuver (the so-called Baydur test) [3, 8]. During the occluded inspiration, the change in airway (ΔP_{aw}) and esophageal (ΔP_{es}) pressure should be almost identical because there is no change in lung volume and, thus, no change in P_L . When the $\Delta P_{es}/\Delta P_{aw}$ ratio is within 0.8–1.2, the Pes measurement is considered to be reliable. Otherwise, the catheter should be repositioned and/or the balloon volume should be re-checked [3, 9]. In deeply sedated patients with or without paralysis, external manual compressions on the rib cage should be applied during an expiratory pause and simultaneous positive deflections of airway and esophageal pressures compared (positive pressure occlusion test) [1].

For the same esophageal catheter position, the Baydur and the positive pressure occlusion tests provide similar changes in airway and esophageal pressures [10]. The absolute value can be significantly higher when the esophageal balloon is placed in the lower third of the esophagus, compared to the middle one, due to the higher superimposed pressure generated by the heart and the lung. Moreover, the pressure generated by the esophageal wall as a reaction to balloon filling may increase the absolute value of Pes above the pleural pressure (P_{pl})

Table 1 Case-scenarios in which esophageal and transpulmonary pressure monitoring could be of help at the bedside

Case-scenario	Relevant Pes-derived measure ^a	Clinical significance	Clinical recommendation
Passively ventilated patient	Tidal ΔP_L	Measure of the tidal stress applied to lung parenchyma	Possibly keep below 10–12 cmH ₂ O in ARDS patients
	End Inspiratory P_L	Measure of the total stress applied to lung parenchyma	Possibly keep below 20–25 cmH ₂ O in ARDS patients
	End expiratory P_L	Negative value possibly indicating tendency of the alveoli and/or airways to collapse	Possibly keep above 0 cmH ₂ O in ARDS patients
	Transmural pulmonary vascular pressure	Effective pressure driving blood flow in intrathoracic vascular structures	Consider delta between CVP and end-expiratory Pes rather than CVP per se to better understand volume status of the patient
Ventilated patient with active breathing	Periodically interspersed negative Pes swings after passively delivered ventilator breaths	Detection of reverse triggering	Consider paralysis or modify sedation (reduce sedation to let the patient trigger)
	Transmural pulmonary vascular pressure	Effective pressure across intrathoracic vascular structures	Consider delta between CVP and end-expiratory Pes rather than CVP per se to better understand volume status of the patient
	End inspiratory P_L	Measure of the tidal stress applied to lung parenchyma	Possibly keep below 20–25 cmH ₂ O in ARDS patients
	P_{mus}	Measure of the pressure generated by the patient's inspiratory muscles	Normal values are between 5 and 10 cmH ₂ O
	Work of breathing	Measure of patient's total work during the respiratory cycle	Normal values are around 0.35 or 2.4 J min ⁻¹
	PTPes	Measure of patient's respiratory muscles effort to breathe	Normal values are around 100 cmH ₂ O s min ⁻¹
	Negative Pes swings without ventilator pressurization	Ineffective effort	Titrate PEEP and/or decrease support and/or consider NAVA
	Pes inspiratory time longer than ventilator inspiratory time	Double triggering or premature cycling	Increase ventilator Ti up to 0.8–1.0 s or consider switching to NAVA or PAV. Rule out non-ventilatory causes (metabolic acidosis, encephalopathy, etc.)
	No Pes swing prior to ventilator pressurization	Auto-triggering	Check for leaks, trigger settings, ventilator tubing (water in circuits) and/or decrease sedation
	Increasing PTPes and/or Pes swings along spontaneous breathing trial	High likelihood of failure to wean	Differentiate whether resistive or elastic workload increased and treat consequently. Reconnect to ventilator

ARDS Acute respiratory distress syndrome, CVP central venous pressure, NAVA neurally adjusted ventilatory assist, PAV proportional assist ventilation, PEEP positive end-expiratory pressure, P_L transpulmonary pressure, ΔP_L change in transpulmonary pressure, P_{mus} inspiratory muscle pressure, PTPes esophageal pressure–time product, Ti inspiratory time.

^a The end expiratory P_L is the absolute value. The end inspiratory P_L can be measured with the elastance method or the absolute value. They do not give the same results, the absolute value being generally lower

value. Therefore, a dedicated calibration procedure has been recently described that removes this artifact, resulting in the improved use of absolute values of P_{es} , especially when large-volume balloons are used [6]. While the presence of a nasogastric tube does not seem to significantly affect P_{es} measurement [11], nasogastric tubes equipped with an esophageal balloon are now available [4].

Transpulmonary pressure

Changes in transpulmonary pressure during mechanical ventilation: a measure of stress on the acute respiratory distress syndrome-injured lung

The clinical use of P_{es} measurement allows the estimation of P_L as the difference between P_{aw} and P_{pl} (estimated as P_{es}), which drives ventilation of the lung (including the airways). Here, we first look at the pathophysiological significance of the changes in P_L induced by ventilation.

The airway driving pressure (the change between end-expiratory total pressure to end-inspiratory plateau pressure) delivered by the ventilator to inflate the respiratory system (ΔP_{aw}) may be divided in two components: one to insufflate the lung, called change in transpulmonary pressure (ΔP_L), and one to move the chest wall, called change in pleural pressure (ΔP_{pl}), where ΔP_{pl} equals the changes of the esophageal pressure (ΔP_{es}) [12, 13]:

$$\Delta P_{aw} = \Delta P_L + \Delta P_{pl}$$

In this section, we will refer to tidal ΔP_L , ignoring for sake of simplicity the fraction of ΔP_L due to positive end-expiratory pressure (PEEP). As the changes in lung volume and chest wall volume are deemed to be identical, the expression above may be written as:

$$\Delta P_{aw}/\Delta V = \Delta P_L/\Delta V + \Delta P_{pl}/\Delta V$$

The elastance of the respiratory system (E_{rs}) is equal to the lung elastance (E_L) plus the chest wall elastance (E_{cw}). Since $E_{rs} = \Delta P_{aw}/\Delta V$ and $E_L = \Delta P_L/\Delta V$, the following expression may be derived:

$$\Delta P_L = \Delta P_{aw} \cdot (E_L/E_{rs})$$

This equation tells us that the pressure applied to the lung for a given driving pressure depends on the ratio between the E_L to the E_{rs} , irrespective of their absolute values. In normal subjects, the typical value of E_L/E_{rs} is equal to 0.5. In intensive care patients without respiratory or abdominal problems this ratio averages ≈ 0.7 ; in acute respiratory distress syndrome (ARDS) patients it may range from 0.5 (or even lower) to 0.9. Given these values, in a patient ventilated with PEEP 10 cmH₂O and a plateau pressure of 30 cmH₂O, the tidal ΔP_L may range from 10 cmH₂O {non-injurious, i.e. [(30 cmH₂O plateau

$P_{aw} - 10 \text{ cmH}_2\text{O PEEP}) \times 0.5\}$ to 18 cmH₂O {highly “bio-traumatic”, i.e. [(30 cmH₂O plateau $P_{aw} - 10 \text{ cmH}_2\text{O PEEP}) \times 0.9\}$, as discussed further in this review [12]. Thus, the lung protective ventilation strategy might be, theoretically, titrated to a “safe” tidal ΔP_L rather than to tidal volume [14].

When tidal ΔP_L is applied, it changes the lung volume (Δvolume). The ratio between Δvolume and the pre-inflation lung volume (V_0) is called *strain*. The tissue molecules which compose the extracellular matrix develop a force opposing the tidal ΔP_L , which is called *stress*. Stress and strain are nearly linearly related up to the total lung capacity. Therefore,

$$\text{stress} = K \times \text{strain}$$

meaning that

$$\Delta P_L = K \times \Delta V/V_0 \text{ [12, 15]}$$

The proportionality constant K is called specific lung elastance and is the tidal ΔP_L value at which V_0 doubles its size (without PEEP). In humans K is around 12–13 cmH₂O, which is substantially greater than other animal species [16, 17], and it seems to be similar in patients with ARDS and healthy subjects [15]. These concepts are summarized in ESM Fig. 1. As shown, when tidal ΔP_L approximates 20 cmH₂O, part of the lung enters its total lung capacity region. In healthy animals, when ventilation occurs in this area, lethal ventilator-induced lung injury develops within 24 h [17]. In clinical practice, it is rare to reach these values of tidal ΔP_L . However, it must be remembered that in ARDS a substantial fraction of the lung includes inhomogeneities which act as stress raisers, with the possible effect of doubling the locally applied pressure [18]. Therefore, a tidal ΔP_L of 10 cmH₂O—in the presence of stress raisers—may regionally increase transpulmonary and transalveolar pressure to 20 cmH₂O.

While waiting for more definitive evidence, tidal ΔP_L should probably be kept below 15–20 cmH₂O in patients with homogeneous lung parenchyma (normal, post-surgical patients) and possibly below 10–12 cmH₂O in patients with inhomogeneous lung parenchyma (ARDS).

When respiratory muscle activity is present, then the active changes in P_{pl} can dominate the P_L changes driving ventilation.

Transpulmonary pressure directly measured to guide mechanical ventilation in ARDS

Measurement of P_{es} also allows estimation of the absolute value of P_L , measured as the P_{aw} minus the P_{pl} and clinically estimated as $P_{aw} - P_{es}$. The alternative elastance-derived method for estimating P_L ($\Delta P_L = \Delta P_{aw} \cdot (E_L/E_{rs})$) was covered in the previous

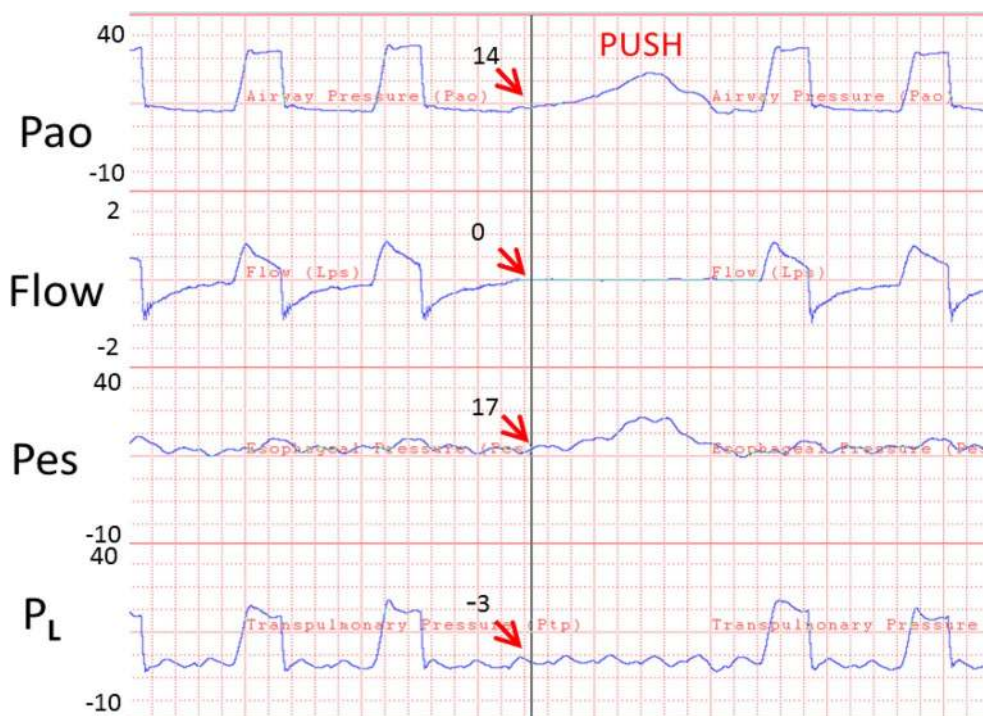


Fig. 1 Directly measured transpulmonary pressure in acute respiratory distress syndrome (ARDS). Airway opening pressure (P_{ao}), flow ($Flow$), esophageal pressure (P_{es}) and transpulmonary pressure (P_L) in a patient with ARDS on mechanical ventilation. At the end-expiratory occlusion (cursor) a total positive end expiratory pressure (PEEP) of 14 cmH₂O and a P_{es} of 17 cmH₂O result in a P_L of -3 cmH₂O. During the occlusion, a manual chest compression (*PUSH*) raises P_{ao} and P_{es} equally, indicating adequate balloon placement in the chest

section. In patients breathing on non-invasive ventilation, P_L is estimated using the pressure in the mask ($P_{mask} - P_{es}$). Due to the location of the esophagus in the supine position, an increase in P_{es} caused by mediastinal weight of 3–7 cmH₂O may exist in that position: whether P_{es} is higher than P_{pl} at the corresponding height in the chest is unclear [19]. Because P_{pl} varies spatially in the chest, P_{es} cannot theoretically represent P_{pl} over the entire lung. However, animal studies suggest that P_{es} represents well the pressure surrounding much of the lung [20].

In ARDS, ventilator settings are adjusted to reduce tidal overexpansion of the lungs by limiting tidal volume (and pressure) and to avoid repeated airspace collapse and derecruitment by maintaining adequate PEEP [21]. Pleural and intra-abdominal pressures vary widely and can be quite high in critical illness, regardless of chest wall compliance [22]. Therefore, a given PEEP applied by the ventilator could have varying effects on P_L . A clinical trial in ARDS patients compared PEEP adjusted to maintain a positive end-expiratory P_L (Fig. 1) with PEEP levels specified in the ARDSNet low-tidal volume table [23]. The P_L approach significantly improved oxygenation and compliance and showed a trend toward reduced

mortality [23]. This rationale was confirmed in animals with lung injury and different degrees of P_{es} elevation due to chest wall restriction. Targeting a positive end-expiratory P_L in chest-restricted animals maintained lung volume and lung compliance, reduced hypoxemia and decreased pulmonary edema, mechanical abnormalities, pro-inflammatory mediator release and histological signs of ventilator-induced lung injury [24].

Uncertainties of direct esophageal manometry include the spatial variation in P_{pl} and the mediastinal weight that elevates P_{es} in the supine position [19]. As previously discussed, adequate filling and positioning of the balloon is important to obtain reliable measurements.

Transmural vascular pressure

Transmural pulmonary vascular pressures

The force distending vascular walls is called the transmural pressure (P_{tm}) and is determined by the difference between the pressure inside and outside of the vessel [25]. An increase in P_{tm} implies an increase in volume of the vessel. Since we are surrounded by atmospheric pressure (P_{atm}), transducers are zeroed to P_{atm} , and the pressure inside systemic vessels is the P_{tm} . For alveolar vessels, however, P_{pl} (not P_{atm}) surrounds the vascular

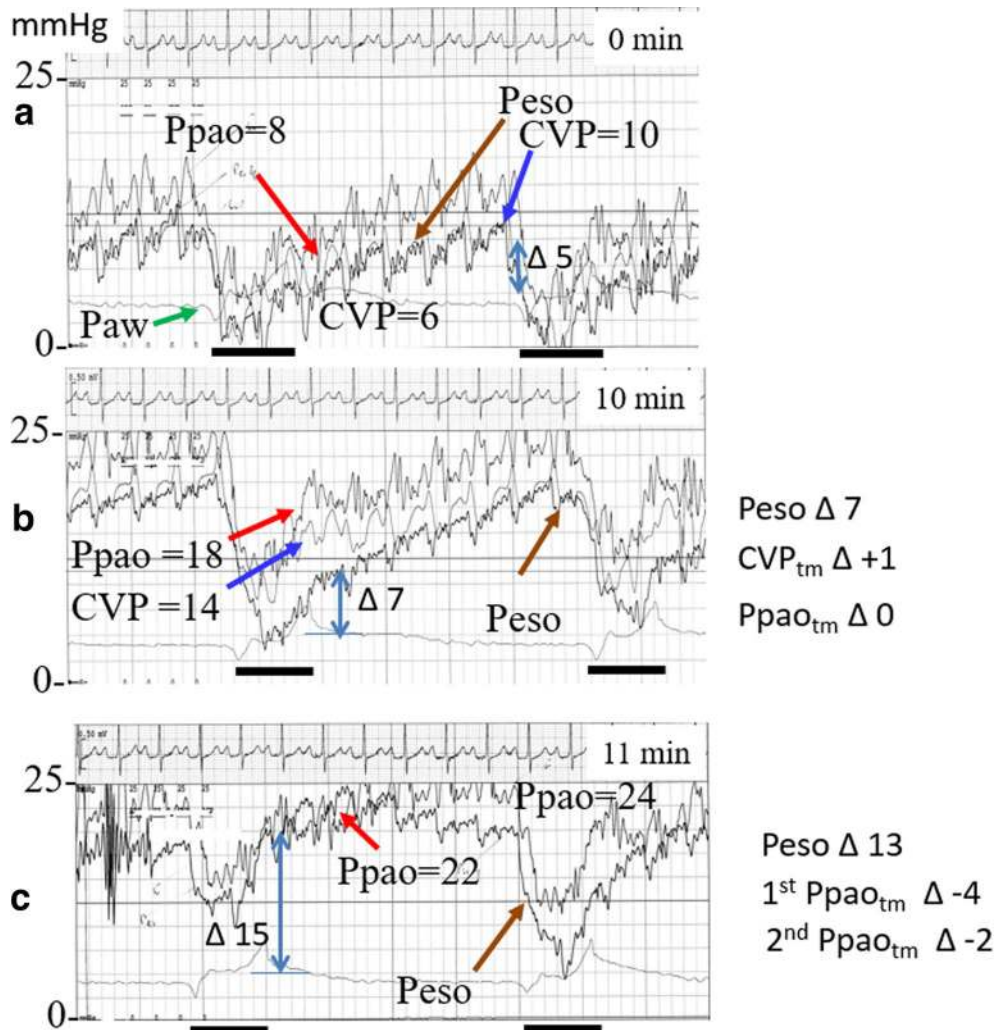


Fig. 2 Value of esophageal pressure (Peso)-derived transmural vascular pressure (Ptm). Examples of changing Ptm of the central venous pressure (CVP) and pulmonary artery occlusion pressure (Ppao) during pressure support. Black horizontal bars mark inspiration. Paw airway pressure. The subject has marked active expiration on all breaths. **a** CVP is 10 mmHg at end-expirations (it is overlapping the Peso) but 6 mmHg at the start of expiration, which is the likely the Ptm. **b** 10 min later, CVP has increased to more than Peso, so that CVP_{tm} (tm transmural) has increased, likely indicating recruitment of abdominal volume from the active expiration. Ppao_{tm} did not change. **c** 1 min later, only Ppao is shown. The Ppao_{tm} has decreased with some recovery late in expiration. It is likely that the rise in pleural pressure (P_{pl}) inhibited venous return with some later recovery because of the recruitment of abdominal volume. The subject likely was air stacking. Ptm measurements of CVP and Ppao would be very misleading without Peso. Double arrow indicates the change (Δ) in Peso from the baseline value. Peso is measured with a fluid-filled catheter so that only the Δ Peso is used. All changes are relative to the values shown in **a**

structures, and thus the value measured inside the vessel relative to Patm is no longer the Ptm.

Measurements of respiratory variations in P_{pl} obtained by esophageal devices can be used to determine changes in Ptm of pulmonary vascular structures that occur during the respiratory cycle [26, 27]. Measurements are usually obtained at end-expiration because this usually is when P_{pl} is closest to Patm. However, this may not be true when patients actively recruit expiratory muscles and increase P_{pl} during expiration (Fig. 2), or when P_{pl} is

elevated by intrinsic or extrinsic PEEP. Failure to appreciate over-estimation of Ptm can lead to important management errors. For example, a central venous pressure of 20 mmHg and a low cardiac output suggest depressed cardiac function, and diuresis or use of an inotrope is likely to be appropriate. However, if P_{pl} is 20 mmHg and the Ptm is actually zero, the patient needs volume and not an inotrope or diuretic.

Although transmural diastolic pressure of the right heart determines cardiac output, the directly measured

value—and not P_{tm} —determines venous return. Thus, a central venous pressure elevated by PEEP reduces the gradient for venous return and cardiac output. Maintenance of cardiac output requires an increase in the upstream venous pressure by either a decrease in vascular capacitance or a fluid bolus [28]. However, there is a price to pay. The high venous pressure will increase capillary leak. Furthermore, when the patient is extubated and the positive P_{pl} is removed, the gradient for venous return increases and the lungs can be flooded if the left ventricle cannot handle the increased volume [29].

On the left side of the heart, increasing P_{pl} reduces the afterload on the left ventricle for the heart is effectively lifted relative to the systemic circulation [30]. This tends to increase cardiac output, but the benefit may be offset by a decrease in venous return due to the increase in P_{pl} . An inspiratory decrease in P_{pl} adds an afterload to the left ventricle for the heart that is effectively lowered relative to the rest of the body [31, 32]. This also increases venous return. If the swings are large enough or long enough, the rise in left ventricular filling pressure can produce pulmonary edema, especially when left ventricular function is poor.

In summary, changes in P_{pl} during the respiratory cycle need to be considered when interpreting hemodynamic pressures. Interpretations are thus greatly benefitted with a simultaneous measurement of P_{pl} .

Muscular pressure

Effect of spontaneous breathing on transpulmonary pressure during assisted ventilation

Spontaneous breathing can offer protective effects to the injured lung: improved oxygenation and increased dorsal aeration/ventilation [33]. This results from the increase in P_L obtained by lowering P_{pl} ($P_L = P_{aw} - P_{pl}$) [32]. However, this protective role has generally been suggested in patients with less severe ARDS and modest spontaneous demands [34, 35]. Accumulating evidence indicates that spontaneous breathing might become deleterious in severe ARDS cases, as suggested by the beneficial effect of muscle paralysis observed in patients with severe ARDS [35, 36]. First, P_L calculated on P_{es} is likely to be injuriously high in severe ARDS, combined with the already high P_{aw} and uncontrollable spontaneous demands [35]. In contrast, in less severe ARDS, P_{aw} can be maintained at relatively low values, and spontaneous demands are often modest, thereby preventing injurious increases in P_L . Second, strenuous inspiratory efforts can shift air from non-dependent to dependent lung regions (i.e. *pendelluft*) even in the absence of large tidal volume and elevated P_{aw} [37]. This occurs because the negative changes in P_{pl} generated by diaphragmatic contraction have localized effects in dependent regions, and the

P_{pl} changes are not uniformly transmitted (i.e. solid-like behavior). To this end, lung recruitment might improve the correlation between P_{es} and the true maximal P_L because it decreases atelectatic 'solid-like' regions.

Despite these limitations, monitoring P_{es} in ARDS patients with spontaneous inspiratory effort is highly relevant. First, P_L calculated on P_{es} is a helpful measure for clinicians to detect the harm of spontaneous effort in severe ARDS, as suggested by large differences in P_L between in mild and severe ARDS when spontaneous effort is preserved [35]. In this regard, even if no "safe" values for P_L are reported, total end-inspiratory P_L should probably be maintained below 20–25 cmH₂O, which is known as the upper limit of physiological range [38]. Second, the intensity of *pendelluft* is proportional to the strength of the spontaneous effort (reflected by negative deflection of P_{es}) [37].

Finally, it is important to note that P_L can be divided into two components: the resistive pressure, necessary to generate airflow between the airway and the alveoli, and transalveolar pressure, the pressure needed to expand the alveoli. Hence, only under static conditions (i.e. in the absence of flow) does P_L equal the pressure distending the alveoli. Thus, unless mechanical properties change, P_L should not differ between assisted and controlled ventilation for comparable tidal volumes and flows.

P_{es} measurement to estimate respiratory muscle effort

Contraction of the respiratory muscles generates a negative swing in P_{pl} , which can be assessed by changes in P_{es} (Fig. 3). The pressure generated by the respiratory muscles (P_{mus}) is computed as the difference between the static recoil pressure of the chest wall ($P_{cw,rel}$, obtained from P_{es} recordings under passive conditions) and the swing in P_{es} obtained under active conditions:

$$P_{mus} = P_{cw,rel} - P_{es}$$

The chest wall compliance (the passive volume/ P_{es} relationship) can also be estimated from a theoretical value (4 % of the predicted vital capacity per cmH₂O).

Values of P_{mus} between 5 and 10 cmH₂O can be considered, as a crude estimate, to be the desirable respiratory effort during partial ventilatory support [39]. The work of breathing (WOB) of the respiratory muscles corresponds to the integral of the product of P_{mus} and the generated volume, represented graphically by the Campbell diagram [40] (Fig. 3):

$$WOB = \int P_{mus} \cdot dV$$

WOB is expressed in joules and can be reported per liter or per minute. Normal values are around 0.35 and 2.4 J min⁻¹, respectively [41]. WOB is computed based

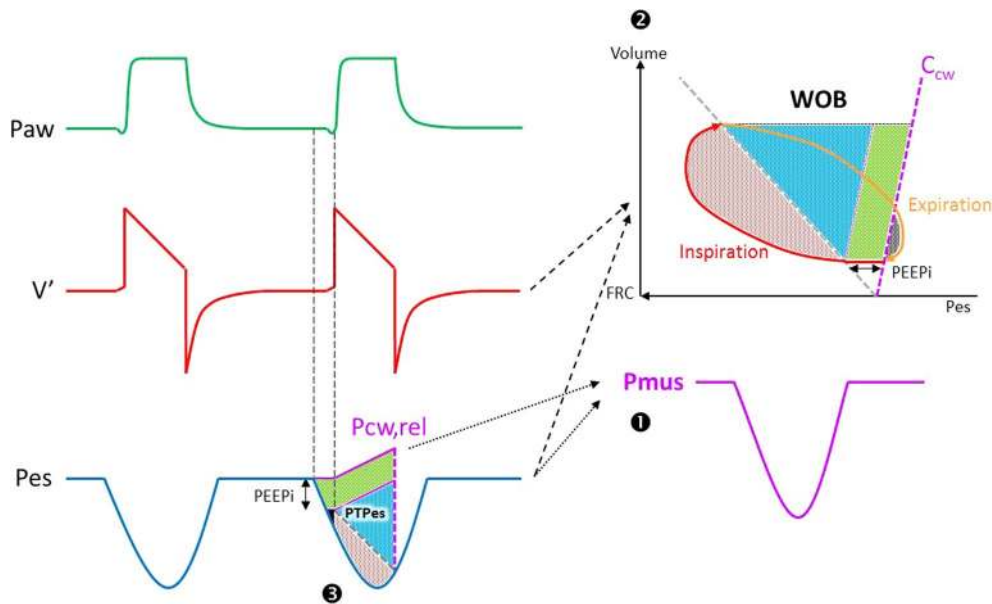


Fig. 3 Respiratory effort indices derived from the esophageal pressure analysis. The figure schematically represents airway pressure (P_{aw}), flow (V') and P_{es} of a patient with intrinsic PEEP ($PEEP_i$) under pressure support ventilation. The static recoil pressure of the relaxed chest wall ($P_{cw,rel}$), which represents the P_{es} that would be observed in passive conditions, has been superimposed to the P_{es} waveform. **①** The difference between $P_{cw,rel}$ and P_{mus} corresponds to the muscle pressure developed by the respiratory muscles (P_{mus}). **②** Campbell diagram: the work of breathing (WOB) is computed as the integral of the P_{mus} over the volume displaced. The chest wall compliance (C_{cw}) represents the value of the esophageal pressure when the muscles are relaxed and the volume passively insufflated above the functional residual capacity (FRC). Dashed gray line crosses the pressure–volume waveform at the zero-flow points. The pressure developed at the onset of the inspiratory effort without generating any volume represents the $PEEP_i$. These landmarks unveil the different components of the WOB : resistive (red area), elastic (blue area), related to the $PEEP_i$ (green area) and related to active expiration (grey area). **③** The P_{es} pressure–time product (PTP_{es}) corresponds to the area under the P_{mus} curve over the inspiratory time. The pressure developed between the start of the inspiratory effort and the onset of the inspiratory flow represents the amount of pressure needed to overcome the $PEEP_i$. An additional pressure is dedicated to trigger the ventilator. The end of the active inspiratory muscle contraction occurred after the maximal negative value of the esophageal waveform and corresponds, in the case of ventilator cycling synchronization, to the onset of the expiration. In these conditions, relying the two points of zero-flow (dashed gray line) unveils the P_{es} related to the dynamic lung compliance. The PTP_{es} can therefore be partitioned into the following parts: resistive (red area), elastic (blue area), related to the $PEEP_i$ (green area) and related to the inspiratory trigger (black area)

on volume displacement, and its value does not account for the duration of the respiratory effort and does not reflect the true energy expenditure of the respiratory muscles in the case of isometric effort.

The esophageal pressure–time product [42] (PTP_{es}), which represents the integral of the P_{mus} curve over time, circumvents these limitations:

$$PTP_{es} = \int P_{mus} \cdot dt$$

PTP_{es} is well correlated with the energy expenditure and oxygen consumption of the respiratory muscles. Normal values can be estimated to be between 50 and 150 $\text{cmH}_2\text{O} \cdot \text{s} \cdot \text{min}^{-1}$ [40]. Proper measurements of both WOB and PTP_{es} take into account the presence of intrinsic PEEP [43].

Non-invasive estimates of respiratory effort may be useful at the bedside. In patients who are assisted with proportional assist ventilation mode, the P_{mus} value can

be estimated from the value of the P_{aw} and the gain set by the clinician [39].

Clinical applications Clinicians may be interested in estimating respiratory muscle effort for several reasons. First, in the context of hemodynamic shock, respiratory muscle effort may account for a significant proportion of total body oxygen consumption, thereby limiting oxygen delivery to vital organs [44]. Ensuring adequate ventilation and sedation by monitoring respiratory muscle effort may help to optimize the distribution of oxygen delivery. Second, insufficient and (possibly) excessive levels of inspiratory effort during ventilation can injure the diaphragm [45–49]. Titrating ventilation support to achieve near normal levels of inspiratory effort may prevent diaphragm injury and accelerate liberation from ventilation. Third, monitoring inspiratory effort may help clinicians to recognize potentially injurious patterns in patients with ARDS receiving partially assisted ventilation, both

for the lungs and for the diaphragm [37]. The relevance of monitoring inspiratory effort during weaning trials is discussed in the section "[Pes monitoring during weaning from mechanical ventilation](#)" of this review.

Patient-ventilator asynchrony and the role of Pes monitoring

Mechanical ventilation, for the main part, is used as partial ventilatory support in situations where both the patient and the ventilator work together. Ideally, the ventilator settings should be adjusted to maintain a normal level of respiratory muscle activity and harmonious patient-ventilator interaction. Patient-ventilator asynchrony, which can be defined as a time mismatch between patient's effort and the ventilator breath duration, often occurs during assisted modes of ventilation and but is unrecognized. Many studies have demonstrated that major asynchrony is a common occurrence (at least 25 % of the patients) throughout the course of ventilation [50–52]. Thille et al. [52] demonstrated that asynchrony occurred during both assist-control and pressure support ventilation and that it was associated with a longer duration of ventilation in patients who had an asynchrony index indicating >10 % of completely asynchronous breaths [7.5 (interquartile range 3–20) vs. 25.5 (9.5–42.5) days]. An observational study in 50 patients by Blanch and colleagues [53] found that asynchrony was detected in all patients and in all ventilator modes. These authors reported that the mortality rates among patients in the Intensive Care Unit and hospital increased in patients who had high asynchrony index (>10 %); these patients also showed a trend toward longer duration of mechanical ventilation. Importantly, adjusting the ventilator settings can dramatically reduce asynchrony [54].

Detecting patient-ventilator asynchrony on the ventilator display without recording respiratory muscle activity is, however, not always easy and can be missed even by experts [55]. This difficulty justifies attempts to develop automated systems [56, 57] or to use an esophageal signal, such as the electrical activity of the diaphragm (EAdi) [58] or the Pes. The Pes recording can detect asynchrony by comparing the time occurrence of the changes in Pes with those of Paw and flow-time waveforms (Fig. 4). The major groups of asynchrony can be classified according to the phase of respiration as (1) trigger asynchrony, (2) cycling asynchrony and (3) flow delivery mismatch.

Trigger asynchrony

1. Ineffective effort is recognized by a negative Pes swing without ventilator pressurization. It occurs in situations combining auto PEEP and excessive ventilation, inducing low respiratory drive and low

inspiratory muscle effort, and it can be aggravated by a poorly sensitive triggering system. It occurs frequently with pressure support ventilation and is associated with poor outcomes.

2. Double triggering is the occurrence of two consecutive triggered breaths separated by a very short expiratory time. It occurs when the neural inspiratory time (Ti) is longer than machine Ti, usually in patients with a high respiratory drive.
3. Reverse triggering is a phenomenon of respiratory entrainment and defined as a muscular effort triggered by the ventilator, usually in highly sedated patients. It occurs during the insufflation phase or at the transition phase from mechanical inspiration to expiration and can then lead to double cycling [59].
4. Auto-triggering is defined as a cycle delivered by the ventilator without triggering by the patient. This type of asynchrony can be seen in case of circuit leaks or cardiac oscillations.

Cycling asynchrony

1. Premature cycling is defined as a cycle with the machine Ti shorter than the neural Ti.
2. Delayed cycling occurs when the machine Ti is longer than the neural Ti

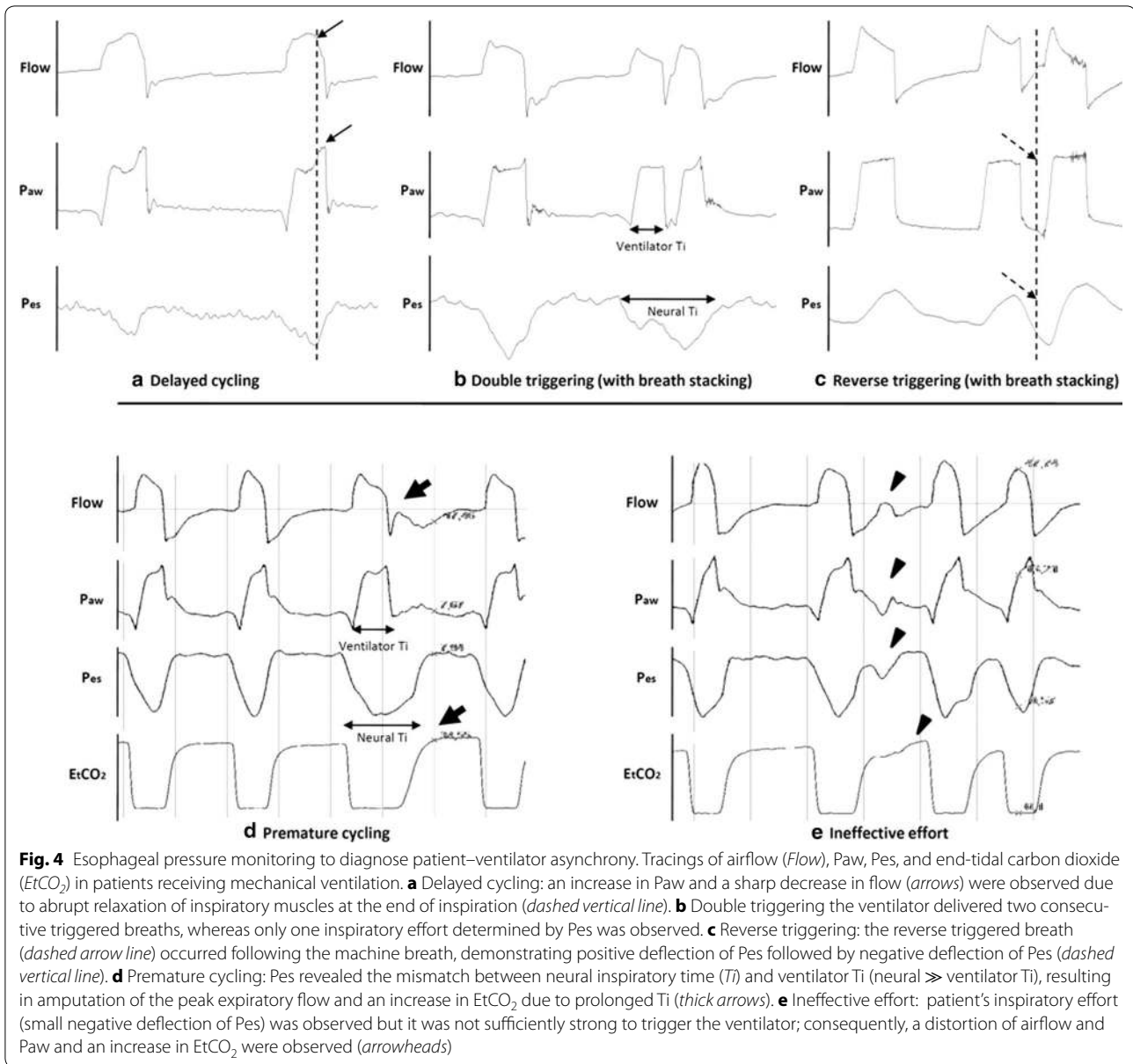
Flow delivery mismatch

1. Flow starvation occurs during volume control mode when the ventilator delivers a peak inspiratory flow that is lower than the patient's demand. This is not an asynchrony per se, but it usually requires a change in the settings.

Patient-ventilator asynchrony is common and is associated with poor clinical outcomes. Pes can be used to better detect asynchrony at the bedside and to adjust the ventilator settings accordingly. However, whether the asynchrony is an indicator of severity or constitutes a biomarker for another systemic feature that compromises patients' outcome warrants further investigation.

Pes monitoring during weaning from mechanical ventilation

The pathophysiology of weaning research has demonstrated that respiratory effort changes progressively as patients fail a weaning trial [60, 61]. During a trial of unassisted breathing, PTPes remained unchanged in patients who were successfully weaned from mechanical ventilation. In contrast, PTPes increased in patients who failed weaning because the mechanical load (resistive, elastic, and intrinsic-PEEP components) on the respiratory muscles increased [60, 62]. When the dominant functional abnormality was investigated in 17 patients who failed to be weaned, ten had worsening mechanics and muscle



function, and four had blood gas abnormalities; failure in weaning could not be explained by functional abnormalities in the remaining three patients, suggesting that behavioral factors may have contributed to this failure [60].

The practice of medicine, though based on scientific knowledge, is centered on individualized care. The physician's primary task is to figure out how scientific principles apply to one particular patient. By inserting an esophageal catheter in a difficult-to-wean patient, a clinician can determine whether worsening mechanics (most common cause) was responsible for weaning failure, and then take the necessary steps to correct the problem. If an increase in resistive work occurred during a failed

trial, then the management plan would focus on decreasing airway resistance by using bronchodilators and frequent suctioning or diuretics if the increase in resistance was due to bronchial edema. An increase in the elastic load could indicate that subclinical cardiogenic pulmonary edema may have been responsible for the failed trial (ESM Fig. 2). Indeed, pathophysiological studies have shown that cardiac performance worsens during weaning failure as a result of an increase in left ventricular afterload, which, in turn, is due to more negative swings in Pes [29, 63, 64].

Jubran et al. [65] showed that throughout a failed weaning trial, swings in Pes showed greater changes than the

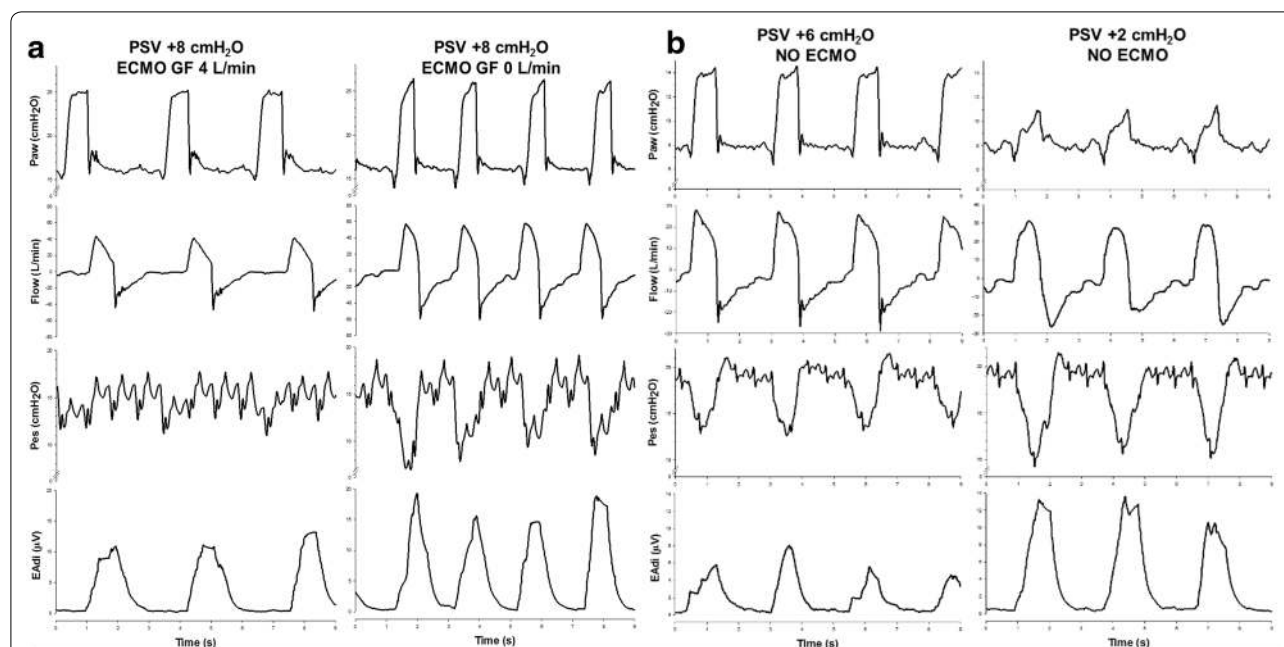


Fig. 5 Clinical validation of the correlation between electrical activity of the diaphragm (EAdi) and Pes swings at different levels of respiratory support. In two representative ARDS patients, amplitude of Pes swings and peak EAdi values increased by the same magnitude (*right side of each panel*) when: **a** the amount of CO₂ removed by the extracorporeal membrane oxygenation (ECMO) system decreased by the reduction of sweep gas flow (GF), without change in pressure support; **b** the pressure support level delivered by the ventilator was reduced. PSV Pressure support ventilation

rapid shallow breathing index (f/V_T). Accordingly, monitoring of Pes throughout a weaning trial may provide additional guidance over a single measurement and, thus, may enhance the predication of weaning success/failure. When the change in Pes was quantified, the Pes trend index was more accurate in predicting weaning outcome than first-minute measurements of either Pes swings or f/V_T [65]. If these results can be confirmed, the Pes trend index could provide a useful monitoring tool during weaning. Moreover, increases in Pes swings during the trial could alert a physician to institute therapy, such as bronchodilators, vasodilators or diuretics, at a time that might convert an unsuccessful trial into a successful one.

The correlation between diaphragm electrical activity and Pes swings

Obtaining reliable Pes measurements can sometimes be challenging, and the question of using other physiological signals to obtain similar information becomes relevant. The electrical activity of the diaphragm (EAdi), a direct expression of neural inspiratory activity, can be recorded in daily clinical practice by a nasogastric tube connected to a ventilator and equipped with electrodes [66]. EAdi could theoretically be used as an alternative to Pes to estimate inspiratory demand. Studies focusing on this issue have shown a tight correlation between EAdi and transdiaphragmatic pressure (Pdi) in healthy

volunteers and obstructive patients at rest, even in the presence of increased inspiratory flow rates or lung volumes [67–69]. EAdi and Pdi were also shown to be correlated and to be changed by the same magnitude during pressure support ventilation in a population of intubated patients suffering from acute respiratory failure when the level of assistance was increased [70]. The drops in both EAdi and Pes associated to external ventilatory assistance have also been correlated (Fig. 5) [71]. On the contrary, EAdi and Pdi amplitudes were found to be poorly correlated in patients with chronic obstructive pulmonary disease during incremental exercise [72], probably due to decreased neuro-muscular coupling in the presence of air trapping. In addition, it has been reported that the correlation factor (i.e. the slope of the linear correlation graph) between Pdi and EAdi differs between subjects, with one of the main reasons being individual anatomy [69]. Thus, EAdi amplitude can differ between subjects with similar inspiratory demand and requires calibration for inter-individual comparisons—for example, by dividing measured EAdi amplitude by the EAdi amplitude obtained during maximal voluntary inspiratory effort [69]. Two alternative calibration procedures that can be used for intubated patients with acute respiratory failure have recently been published [73, 74]. One of these, the Pmus/EAdi index (PEI), is measured during end-expiratory occlusion as the drop in Paw divided by the EAdi needed

to generate it. By multiplying peak EAdi values by PEI, it is possible to calculate the absolute values of a patient's inspiratory effort. The second procedure is the patient-ventilator breath contribution index [74], defined as the ratio between tidal volume and EAdi during an assisted breath divided by the same ratio measured during a subsequent unexpected non-assisted one. The correlation between the patient-ventilator breath contribution index and the $\Delta P_{\text{es}}/\Delta P_{\text{TPes}}$ ratio is significant. These two calibration approaches to compare absolute values of a patient's effort obtained from EAdi require further validation. It is also important to note that EAdi amplitude can be influenced by other factors, such as sedation [75] and clinical evolution [74].

EAdi can also be used to accurately monitor patient-ventilator synchrony [55, 75, 76]. Finally, as the EAdi value recorded at the onset of the inspiratory flow (auto-EAdi) is tightly correlated with the patient's auto-PEEP, as measured by Pes [77], EAdi can also be used to estimate auto-PEEP.

EAdi provides alternative and complementary information to Pes, but it cannot replace it. Thus, whether the practical advantages of using EAdi outweigh the additional information provided by Pes (e.g. P_{L}) must be decided on an individualized basis.

Conclusions and perspectives

The multiple applications already described support the notion that Pes monitoring is an essential tool for personalized medicine and for improving the capability of physicians to diagnose complex clinical conditions. The results of recent studies suggest that bedside decisions regarding ventilator settings, lung protection, sedation, paralysis, weaning or even hemodynamic support might radically change if it were possible to consider the information coming from Pes monitoring. Some technical aspects of Pes measurement will need further refinements (e.g., those involving quantitative measurements of the chest wall properties).

Both the approach of using absolute Pes values and the dynamic approach in which only the swings in Pes are quantified have shown promising results for ventilation adjustments [12, 20]. While the direct absolute method is simpler and has been made more reliable through the use of newly developed catheters and accurate calibration procedures, the dynamic approach, by testing a volume change, might better unveil the pathophysiological characteristics of the respiratory system. However, both methods require a number of assumptions: for the absolute P_{L} , that end-expiratory Pes is equal to the end-expiratory P_{pl} and that negative values of end-expiratory absolute P_{L} correspond to a tendency of the alveoli and/or small airways to collapse; for the

dynamic approach (testing a volume change), that P_{pl} is equal to zero at zero PEEP and that the E_{L} and Ers behave linearly throughout different lung volumes. In fact, especially when exploring the upper limits of lung stress, the two approaches have been found to produce conflicting results.

Synchronization with ventilator signals, automatic filling and automatic in vivo calibration are future developments that may enable this technology to be introduced into the daily clinical routine. Meanwhile, many of the clinical applications described in this review, with most of them tracking negative swings in Pes, such as the monitoring of asynchrony, over-assistance, strenuous efforts or difficult weaning, have been extensively validated, indicating that clinicians and patients likely benefit from the availability of this technology in daily clinical practice.

Electronic supplementary material

The online version of this article (doi:10.1007/s00134-016-4400-x) contains supplementary material, which is available to authorized users.

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Compliance with ethical standards

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Conflicts of interest

F. Mojoli, D. Chiumello and L. Gattinoni were involved in a University research spin-off for the development of NutriVent [Sidam, Mirandola (MO), Italy]. L. Blanch is inventor of one Corporació Sanitària Parc Taulí-owned U.S. patent (US Patent No. 12/538,940): "Method and system for managed related patient parameters provided by a monitoring device". L. Blanch owns stock options of BetterCare S.L., which is a research and development spin off of Corporació Sanitària Parc Taulí (Spain). Outside the submitted work, J. Mancebo reports grants from Covidien, non-financial support from Maquet and General Electric and personal fees from Covidien, Hamilton, Braun, Air-Liquide, Faron, and A-Lung. Outside the submitted work, L. Brochard reports grants from Covidien, Fisher Paykel, non-financial support from Maquet, Philips and General Electric and personal fees from Covidien and Maquet. All other authors declare that they do not have any conflicts of interest to declare.

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