ESTIMATION OF RESPONSE SPECTRA AND PEAK ACCELERATIONS FROM WESTERN NORTH AMERICAN EARTHQUAKES: AN INTERIM REPORT

By

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ABSTRACT

We have derived equations for predicting the larger horizontal and the random horizontal component of peak acceleration and of 2-, 5-, 10-, and 20- percent-damped pseudovelocity response spectra for 46 periods ranging from 0.1 to 2.0 sec. The equations were obtained by fitting a functional form to empirical data using a two-stage regression method. 271 two-component recordings from 20 earthquakes were used to develop the equations for peak acceleration, and 112 two-component recordings from 14 earthquakes were used for the response spectral equations. The data included a subset of those used in earlier studies by us (Joyner and Boore, 1981, 1982), augmented by data from three recent earthquakes with magnitudes close to 7: 1989 Loma Prieta, 1992 Petrolia, and 1992 Landers. Besides the addition of new data, this study differs from our previous work in several ways: records at distances equal to and greater than the distance to the first record triggered by the S wave were not included (this resulted in eliminating 56 records from our previous data set for peak horizontal acceleration and 19 records from our previous data set for response spectra; in addition, 7 records providing peak acceleration values were removed for a variety of other reasons), we used weighted regression in the second stage of the twostage regression, equations were evaluated at many more periods than previously and for four values of damping, and the smoothing of the regression coefficients over period was done by computer rather than by eye. In addition, we changed the way in which geologic conditions beneath the site are classified. Our previous studies used a binary rock/soil classification. In anticipation of future building code classifications, we now divide site geology into four classes, depending on the average shear-wave velocity in the upper 30m. Site class A includes sites where the average shear-wave velocity is greater than 750 m/s; site class B sites where the velocity is between 360 and 750 m/s; site class C sites where the velocity is between 180 and 360 m/s; and site class D sites where the velocity is less than 180 m/s (site class D class was poorly represented in the data set and has not been included in the analysis).

Compared to the predictions from our previous equations, the new results have a lower variance and show differences between site classes at all periods, not just at periods longer than about 0.3 sec. At distances within a few tens of kilometers the motions for our new class B and class C are similar to those for our old rock class and soil class respectively;

the motions for our new class A are lower than any of our previous predictions. At large distances the new equations predict larger motions, larger at 80 km by a factor of two or more.

INTRODUCTION

In earlier studies (Joyner and Boore, 1981; Joyner and Boore, 1982; and Joyner and Boore, 1988) we presented equations for peak horizontal acceleration, velocity, and response spectra as a function of earthquake magnitude, the distance from the earthquake source, and the type of geologic material underlying the site. These equations were based on data obtained through 1980, and they used a binary classification ("rock" and "soil") for the geologic materials. Many more data have been collected since 1980. In particular, three earthquakes in California (1989 Loma Prieta, 1992 Petrolia, and 1992 Landers) have provided data for a range of magnitude and distance, critical for engineering design, which was poorly represented in our previous work. Furthermore, it is likely that future editions of national building codes will use at least a four-fold classification of site geology, based on average shear velocity to a depth of about 30 m. Our long-term goal is to develop prediction equations incorporating all of the data recorded since our earlier work and to reprocess all of the data for the sake of uniformity and to extend the period range covered by the equations. We decided, however, that an interim report would be useful at this time. Most of the post-1980 data that we are not including in this interim study are for magnitudes and distances sampled relatively well in our previous studies, and we expect that the results of our final study will not change greatly from those in this interim report.

In this report we give only brief discussions of those matters that were explained in our previous reports; we concentrate instead on topics that are new in this study.

DATA

Ground Motion Data

The set of data to be used in the regression was chosen from the data used in our previous studies combined with recordings of the 1989 Loma Prieta, the 1992 Petrolia, and the 1992 Landers earthquakes. Most of the data were collected by the California Division of Mines and Geology's Strong-Motion Instrumention Program and the U.S. Geological Survey's National Strong-Motion Program. As in our previous studies, we used values for peak acceleration scaled directly from accelerograms, rather than the processed, instrument-corrected values. We did this to avoid bias in the peak values (e.g., Fig. 5 in Boore and Joyner, 1982) from the sparsely sampled older data. This bias is not such a problem with the more densely sampled recent data. With a few exceptions we used response spectra as provided by relevant agencies; the exceptions are the data collected by Southern California Edison Company and by S. Hough of the U.S. Geological Survey, for which we computed response spectra ourselves. (We use the notation *psv* for response spectra, and all uses of the term "response spectra" refer to pseudo-velocity response spectra, computed by multiplying the relative displacement spectra by the factor $2\pi/T$, where T is the undamped natural period of the oscillator [the *psv* provided by the U.S. Geological Survey for the Loma Prieta earthquake used the damped period, but in the worst case (20 percent damping) this amounts to a difference in response spectra of only 2 percent].)

As we did previously, to avoid bias due to soil-structure interaction, we did not use data from structures three stories or higher, from dam abutments, or from the base of bridge columns. In addition, we include no more than 1 station with the same site condition within a circle of radius 1 km. In such cases, we generally chose the station with the lowest database code number and excluded the others. The radius of 1 km is a somewhat arbitrary choice.

When a strong-motion instrument is triggered by the S wave, the strongest motion may be missed. In this study, unlike previous studies, we made a systematic effort to exclude records from instruments triggered by the S wave.

A strong-motion data set will be biased by any circumstance that causes low values of ground motion to be excluded because they are low, as happens when the ground motion is too weak to trigger the strong-motion instrument, when the ground motion is so weak that an instrument triggers on the S wave, or when records are not digitized because their amplitude is low. To avoid a bias toward larger values, we impose a distance cutoff for each earthquake, beyond which we ignore any data available for that earthquake. This cutoff should logically be a function of geologic condition and trigger level of the recording instrument. We have ignored geologic condition in the determination of cutoff distance in this report, but we have partially considered the effect of trigger level by distinguishing

between those stations employing a trigger sensitive to horizontal motion and those that were triggered on the vertical component of motion. Potentially, every earthquake could have two cutoff distances, depending on the type of trigger used in the recorder. In fact, this was only necessary for the 1971 San Fernando earthquake, which occurred during the time of transition between older instruments that trigger on horizontal motion and newer instruments that employ vertical triggers. For peak acceleration, the cutoff distance is equal to the lesser of the distance to the first record triggered by the S wave and the closest distance to an operational nontriggered instrument. For response spectra we chose to presume that amplitude is a factor in deciding which records are digitized, and we set the cutoff distance to the lesser of the distance to the first digitized record triggered by the S wave, the distance to the closest non-digitized recording, and the closest distance to an operational nontriggered instrument. The cutoff distances are given in Table 1. In Table 1, the greater-than sign indicates that the cutoff distance is at an unknown distance greater than that indicated. For the Landers earthquake the digitizing of the analog records is in the early stages, and few records from digital instruments have been released. It is likely that the cutoff distance for response spectra for the 1992 Landers earthquake will increase in the future.

In our previous studies we ignored the possible bias introduced by including records triggered by the S wave. Using the cutoff distances shown in Table 1 resulted in the elimination of 56 records from the peak acceleration data and 19 records from the peak velocity data set, a significant fraction of the data used in our previous studies. In addition, 7 records were deleted because information was available only for one horizontal component, because the record was obtained on a dam abutment, or because available information indicated that the site was underlain by muskeg or peat. Table 2 contains a listing of the records used in the previous study that were eliminated from the current analysis.

Because of the relatively low sampling rate of the older data (unevenly sampled, but usually interpolated to 50 samples/s), the response spectra are not well determined at periods less than 0.1 s. At longer periods, low signal to noise and filter cutoffs employed in the processing limit the generally useful band to periods less than about 2 to 4 s (we hope to extend this range in the future by reprocessing the data). We have used response spectra for periods between a maximum range of 0.1 and 2 s.

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The recording of the 1992 Petrolia earthquake at the Cape Mendocino station provided only lower bounds for the peak acceleration, and therefore the recording was not used for peak acceleration. According to numerical experiments mentioned by Shakal *et al.* (1992a), the high-frequency character of the acceleration trace associated with the peak motion makes the displacement and velocity records insensitive to the actual value of the peak motion. For this reason, we have used response spectra determined from the recording for periods greater than 0.1 sec in our analysis.

Predictor Variables

As before, we use moment magnitude as the measure of earthquake size and a distance equal to the closest horizontal distance from the station to the point on the earth's surface that lies directly above the rupture. We estimated the moment magnitudes and the areas of the rupture surface from a literature review of various published studies for each earthquake.

Unlike the earlier studies, we use a site classification scheme based on the shear velocity averaged over the upper 30m. This scheme, shown in Table 3, has been proposed by Roger Borcherdt and Thomas Fumal and is now being considered for use in the 1994 edition of the National Earthquake Hazard Reduction Program's recommended code provisions. When available, we used measurements from boreholes at the strong-motion sites. In most cases such measurements were not available, and then we estimated the site classifications by analogy with borehole measurements in similar geologic materials; the type of geologic materials underlying each site was obtained from site visits, consultation with geologists familiar with the area, and various geologic maps (in particular, the 1:250,000 scale maps published by the California Division of Mines and Geology; see also Fumal, 1991, who used more detailed maps). Although we expect that some of the site classifications will change as more data become available, we do not anticipate any significant changes in the regression coefficients as a result of such changes. Of the four site classes listed in Table 3, class D was poorly represented in the data set and has not been included in the analysis.

The earthquake-station pairs and the corresponding predictor variables are given in Tables 4 and 5 for peak acceleration and response spectra, respectively. The information in Tables 4 and 5 is sorted by date, site class, and distance, in that order. The site class is given in the column labeled G. In addition, Table 4 contains the peak acceleration values

(space does not allow a comparable listing of response spectral values). In both tables a borehole number is given if the site classification is based on a nearby borehole. The borehole information is contained in Table 6. The distribution in magnitude and distance space is shown in Figure 1, where the data used previously (but not wiinowed out of the current data set) and the data from the three recent earthquakes are plotted with different symbols. It is clear that the recent data fill an important gap in the previous data set. It should also be noted that very few data are available for distances beyond about 80 km.

METHOD

The coefficients in the equations for predicting ground motion were determined using a weighted, two-stage regression procedure (Joyner and Boore, 1993). In the first stage, the distance dependence was determined along with a set of amplitude factors, one for each earthquake. In the second stage, the amplitude factors were regressed against magnitude to determine the magnitude dependence. The second-stage regression used a weighting matrix with zero off-diagonal terms (equation (34) in Joyner and Boore, 1993); the value of σ_e was determined by finding the value that satisfies (or the non-negative value that most nearly satisfies) equation (33) in Joyner and Boore (1993).

We fit the following functional form to the data:

$$\log Y = b_1 + b_2(\mathbf{M} - 6) + b_3(\mathbf{M} - 6)^2 + b_4r + b_5\log r + b_6G_B + b_7G_C + \epsilon_r + \epsilon_e, \quad (1)$$

where

$$r = (d^2 + h^2)^{(1/2)}.$$
 (2)

In this equation Y is the ground motion parameter (in cm/s for response spectra and g for peak acceleration); the predictor variables are magnitude (M), distance (d, in km), and site classification ($G_B = 1$ for class B and zero otherwise; $G_C = 1$ for class C and zero otherwise); ϵ_r is an independent random variable that takes on a specific value for each record; and ϵ_e is an independent variable that takes on a specific value for each earthquake. The coefficients to be determined are b_1 through b_7 , h, and the variance of ϵ_e and ϵ_r (σ_e^2 and σ_r^2 , respectively). The earthquake-to-earthquake component of variability is represented by σ_e^2 , and all other components of variability are represented by σ_r^2 . Note that h is a fictitious depth that is determined by the regression. We present sets of equations for predicting both the larger of the two horizontal components and a randomly-oriented horizontal component of ground motion. To derive equations for the randomly-oriented component, we used the geometric mean of the two horizontal-component amplitudes for Yin equation (1) rather than choosing one of the horizontal components randomly. This will give the correct regression coefficients, but the variance of ϵ_r determined by the regression program will be reduced below that expected for the prediction of a random component of ground motion. To account for this, we computed the variance (σ_c^2) of the horizontal components from the following formula:

$$\sigma_c^2 = \frac{1}{nrecs} \sum_{j=1}^{nrecs} \left\{ \frac{1}{2} \left[\log Y_{1j} - \log Y_{2j} \right]^2 \right\},\tag{3}$$

where Y_{ij} is the *i*th component from the *j*th recording and the sum is taken over all records for which both horizontal components were available. The few records that did not have both horizontal components were not included in the sum, although the one available component was used in the regression to determine the coefficients in equation (1)). The variance σ_r^2 is then given by

$$\sigma_r^2 = \sigma_1^2 + \sigma_c^2,\tag{4}$$

where σ_1^2 is the variance from the first stage of our two-stage regression. The overall variance is given by combining the individual variances:

$$\sigma_{\log Y}^2 = \sigma_r^2 + \sigma_e^2. \tag{5}$$

RESULTS

Equation (1) was fit to the data period-by-period at the 46 periods between 0.1 and 2.0 s for which the response spectral values had been computed. These periods are distributed in a generally logarithmic manner over the interval. The data and regression fit for the second stage of the regression analysis are shown in Figure 2, for the random horizontal component of peak acceleration and 5-percent damped response spectra; plots for the other values of damping and for the larger of the horizontal components are similar and are not included in this report.

Plots of the coefficients versus period showed them to have fluctuations that lead to somewhat jagged spectra at a fixed distance and magnitude; the amplitude of the fluctuations is comparable to the uncertainty in the estimated coefficients. Because we wish our equations to produce smooth response spectra, we have smoothed the coefficients over period. After some experimentation with various smoothing schemes, we adopted the least-squares fit of a cubic polynomial as the best representation of the smoothed coefficients. The unsmoothed and smoothed coefficients for the 5-percent damped response spectra for the random horizontal component are shown in Figure 3; figures for the other dampings and for the larger horizontal component are collected at the end of the report in a multipart figure labeled A1.

Comparisons of response spectra computed from the unsmoothed and the smoothed regression coefficients are given in Figures 4, 5, and 6 for combinations of magnitudes, site classes, and distances. These figures illustrate the jaggedness that motivated our smoothing of the coefficients and also demonstrates the effectiveness of the smoothing procedure.

The smoothed coefficients for the random horizontal component and the larger horizontal component are given in Table 7 and 8, respectively. Each table contains four parts, corresponding to dampings of 2, 5, 10, and 20 percent. Note in the column headings for the tables that the uncertainties σ_1 , σ_c , σ_r , σ_e , and $\sigma_{\log Y}$ are represented by S1, SC, SR, SE, and SLOGY, respectively. The coefficients for predicting peak acceleration are given in Table 9.

Based on the magnitude and distance distribution shown in Figure 1, we stipulate that our equations not be used to predict motions at distances greater than 100 km or magnitudes less than 5.0 or greater than 7.7.

Several columns in Tables 7 and 8 have zero entries, for the following reasons. We initially fixed b_5 at -1, but this led to values of the coefficient b_4 greater than 0. Positive values of b_4 lead to unreasonable behavior at large distances. For this reason we set $b_4 = 0.0$ and solved for the geometrical-spreading surrogate, b_5 . The "SC" column represents the variance due to the difference in amplitude of the two horizontal components of motion at a site; it obviously has no meaning when peak motions from the larger horizontal component is being considered, and therefore the "SC" entries in Table 8 are set to zero.

Plots of selected ground motions against distance computed from the coefficients in Tables 7b and 9 are shown in Figure 7.

RESIDUALS

An important step in a regression analysis is a study of the residual of the data about the regression fits. We have already shown one such comparison (Figure 2), in which no systematic departures from the assumed model can be seen. We have plotted residuals of the logarithms of ground motion against distance for different site and magnitude classes, and we again we see no systematic differences between the data and the predictions (Figure 8).

DISCUSSION AND CONCLUSIONS

How do the new equations compare to our previous equations? Because of the difference in site classification, we cannot make a direct comparison. Predicted *psv* from old and new equations are shown in Figure 9 as a function of period for two magnitudes, with different curves for the various site classes for distances of 0 and 20 km. In general, at these distances the new site class A has lower motions than we would have predicted for rock sites; the motions from the new site class C are similar to those from the old soil class and the motions for the new site class B are similar to those for the old rock class. We found that many of our previously-designated rock sites fell into the B class, and therefore at first glance it is not surprising that the old rock and new class B predictions are similar. On the other hand, our old soil class was made up of a combination of B and C sites, and therefore Figure 9 suggests that the average ground motion from our new equations and new site classes, for a specific collection of sites, would be lower than from our old equations and site classes. Note also that the difference between the various site classes persists to low periods, unlike our previous finding.

The new equations give higher values than the old equations at large distances. At 80 km the new equations give values for the average of site classes B and C that are a factor of two or more greater than the values given by the old equations for soil (Figure 10). To understand better the reasons for the higher values at large distances we performed a series of analyses of the old data set. The results show that using weighted regression for the second stage of the analysis, winnowing the data set on the basis of the distance cutoff table, assigning new site classes to the older data, and including the new data from the three recent earthquakes all contributed to increasing the values for large distances.

Although not shown in the figure, the variance of the ground motions has been reduced in our new results. This is shown in Table 10 for 5 percent damped psv at periods of 0.3 and 1.0 s. A series of analyses of the old data set shows that the primary cause of the reduction in variance is the winnowing of the data set. The use of weighted regression for the second stage also contributed to the reduction in variance.

Although this is not the place for an extended discussion of the variations in the coefficients and their possible physical interpretation, we point out that a number of trends are similar to those found in our previous work: with increasing T, the magnitude dependence increases, as do the site factors and the variance. The coefficient h generally decreases with increasing period.

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· peak acceleration OFFDIST (km)	2.0 8.0 8.0 3.6 5.0 5.0 5.0 5.0 7.0 8.0 8.0 6.3 3.0 7.0 7.0 8.0 8.3 7.0 8.0 8.3 7.0 8.0 8.3 8.0 8.3 7.0 8.0 8.0 8.0 8.0 8.0 7.0 8.0 8.0 8.0 7.0 8.0 8.0 7.0 8.0 8.0 5.0 7.0 8.0 7.0 8.0 8.0 7.0 8.0 7.0 8.0 7.0 8.0 7.0 8.0 7.0 8.0 7.0 8.0 7.0 8.0 7.0 8.0 7.0 8.0 7.0 8.0 7.0 8.0 7.0 8.0 7.0 8.0 8.0 7.0 8.0 7.0 8.0 7.0 8.0 7.0 8.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7	5.3 (9.9 ances used for response spectra OFFDIST (km) 2.0 8.0 8.0 8.0 13.0 13.0 13.0 13.0 13.0 13.0 13.0 13	
Table 1a. Cutoff distances fo EQ# YEAR NAME	8 1940 Imperial Valley > 18 1952 Kern County 50 1966 Parkfield 58 1958 Borrego Mt. 56 1978 Sarrego Mt. 56 1971 Sar Fernando 72 1972 Bear Valley 76 1972 Sitta 27 1972 Managua 84 1973 Pt. Mugu 97 1974 Hollister 1979 Transmagua 84 1975 Covote Lake 1379 St. Elias 144 1979 Imperial Valley 51 1980 Livermore	349 1992 Petrolia 352 1992 Landers Table 1b. Cutoff distance dis Eq# YEAR NAME CU Eq# YEAR NAME CU 8 1940 1952 Kern County 18 1952 1952 Kern county 1951 San Fernando 58 1968 Borrego Mt. 64 1970 Lytle Creek 65 1972 Sitka 70 1977 San Fernando 74 1977 Managua 74 1977 Imperial Valley 74 <t< td=""><td></td></t<>	

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Table 2a. Records from previous work eliminated from the current regression analysis of peak acceleration.

LONG.	120.660 118.630	117.320 118.396 121.400 115.549	120.660 119.460 119.350	121.400	117.330 118.170	117.188 117.560 117.300 118.120 117.920	117.320 118.230 118.340	122.340 122.340	117.330 117.330	117.630 117.300	117.320	118.560 118.299 118.170 117.330	118.430 118.660 118.113 117.920 118.830 118.830 117.300	118.340 118.720 118.387
LAT.	35.285 38.550	34.060 37.360 36.850 32.794	35.285 35.150 35.160	36.850	34.200 34.150	33.843 33.370 34.310 34.510	34.060 33.770 34.090	37.980 37.980	34.280 34.200	34.360	34.060	34.610 34.118 34.150 34.280	34.578 34.578 34.578 34.578 34.510 34.940 34.310	34.090 34.808 33.801
DIST STATION	0 148.0 San Luis Obispo 0 359.0 Hawthorne, NV	0 156.0 Colton: SCE Substn. 0 224.0 Bishop 0 293.0 Hollister City Hall 0 370.0 El Centro Array Sta 9	10 63.6 San Luis Obispo 10 105.0 Taft 10 112.0 Buena Vista Pumping	10 123.0 Hollister City Hall	50 141.0 Devil Canyon 50 200.0 Pasadena - Old Seism Lab	50 105.0 Perris Dam 50 122.0 San Onofre 50 147.0 Cedar Springs - Pump House 50 197.0 Pasadena - Athenaeum 50 203.0 Pearblossom: Pumping Plant	0 130.0 Colton: SCE Substn. 50 187.0 Long Beach - Terminal Island 50 211.0 Hollywood Storage Bldg PE Lo	60 62.0 San Pablo 70 62.0 San Pablo	50 19.0 Cedar Springs - Miller Canyo 60 21.0 Devil Canyon	00 13.0 Wrightwood 00 22.0 Cedar Springs - Pump House	0 29.0 Colton: SCE Substn.	50 20.2 Lake Hughes Sta 9 50 21.1 Griffith Park Observatory 50 21.9 Pasadena - Old Seism Lab 50 87.0 Cedar Springs - Miller Canyo	 23.4 Lake Hughes Sta 1 24.2 Castaic 28.6 Palmdale: Fire Station 37.4 Pearblossom: Pumping Plant 64.0 Fort Tejon 66.0 Edmonston Pumping 88.0 Cedar Springs - Pump House 	50 24.6 Hollywood Storage Bldg PE Lo 50 46.7 Oso Pumping Plant 50 56.9 Palos Verdes Estates
Σ	7.4	7444 7444	6 6 6 1 1 1 1	6.1	6.6 6.6	00000 00000	000 000	5.0	~~~ ~~~	ភ្លំភ្លំ ភាគ	5.3	0000 0000	0000000 000000	6 6 6 6
DATE EARTHQUAKE	21-Jul-52 Kern County 21-Jul-52 Kern County	21-Jul-52 Kern County 21-Jul-52 Kern County 21-Jul-52 Kern County 21-Jul-52 Kern County	28-Jun-66 Parkfield 28-Jun-66 Parkfield 28-Jun-66 Parkfield	28-Jun-66 Parkfield	9-Apr-68 Borrego Mount 9-Apr-68 Borrego Mount	9-Apr-68 Borrego Mount 9-Apr-68 Borrego Mount 9-Apr-68 Borrego Mount 9-Apr-68 Borrego Mount 9-Apr-68 Borrego Mount	9-Apr-68 Borrego Mount 9-Apr-68 Borrego Mount 9-Apr-68 Borrego Mount	2-Oct-69 Santa Rosa, C 2-Oct-69 Santa Rosa, C	12-Sep-70 Lytle Creek 12-Sep-70 Lytle Creek	12-Sep-70 Lytle Creek 12-Sep-70 Lytle Creek	12-Sep-70 Lytle Creek	9-Feb-71 San Fernando 9-Feb-71 San Fernando 9-Feb-71 San Fernando 9-Feb-71 San Fernando	9-Feb-71 San Fernando 9-Feb-71 San Fernando 9-Feb-71 San Fernando 9-Feb-71 San Fernando 9-Feb-71 San Fernando 9-Feb-71 San Fernando 9-Feb-71 San Fernando	9-Feb-71 San Fernando 9-Feb-71 San Fernando 9-Feb-71 San Fernando

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18.230 19.206 18.990 17.320	21.400	39.670	34.642	18.496	21.500 21.681	21.815	21.577	41.966	21.550	21.803 21.952	14.700	21.620	21.620	16.655	16.389 16.782
33.770 34.145 35.030 34.060	36.850 1	59.510 1	58.382 1	34.312 1	39.550 1 39.727 1	39.717 1	39.149 1	60.023 1	37.118 1	37.046 1 36.974 1	32.730 1	37.800 1	37.800 1	33.989 1	33.925 1 33.918 1
Island															
1.4 Long Beach - Terminal 2.0 Port Hueneme 2.0 Wheeler Ridge 1.0 Colton: SCE Substn.	il.O Hollister City Hall	0.0 Yakutat, Alaska	5.0 Juneau	0.0 Jensen Filter Plant	8.0 Oroville 22.0 Paradise	1.0 Chico	0.0 Marysville	.0.0 Munday Creek, Alaska	1.6 Coyote Lake Dam	3.4 Corralitos 8.9 Capitola	4.0 Yuma	0.8 Delta Pumping Plant	1.1 Delta Pumping Plant	3.1 Whitewater Cyn	.7.7 Fun Valley 9.2 Cabazon
6.60 6.60 6.60 6.60 6.60 6.60 6.60 6.60	5.30 3	7.70 30	7.70 14	5.60 5	6.00 5.00 3	6.00 3	6.00 3	7.60 4	5.80	5.80 3	6.50 6	5.80 1	5.50 1	5.30 5	5.30 4
Feb-71 San Fernando Feb-71 San Fernando -Feb-71 San Fernando -Feb-71 San Fernando	-Feb-72 Bear Valley	-Jul-72 Sitka	-Jul-72 Sitka	-Feb-73 Point Mugu	-Aug-75 Oroville -Aug-75 Oroville	-Aug-75 Oroville	-Aug-75 Oroville	-Feb-79 St. Elias	-Aug-79 Coyote Lake	-Aug-79 Coyote Lake -Aug-79 Coyote Lake	-Oct-79 Imperial Vall	-Jan-80 Livermore Val	-Jan-80 Livermore Val	-Feb-80 Horse Canyon	-Feb-80 Horse Canyon -Feb-80 Horse Canyon
	-Feb-71 San Fernando 6.60 61.4 Long Beach - Terminal Island 33.770 118.230 -Feb-71 San Fernando 6.60 62.0 Port Hueneme -Feb-71 San Fernando 6.60 82.0 Wheeler Ridge	-Feb-71 San Fernando 6.60 61.4 Long Beach - Terminal Island 33.770 118.230 -Feb-71 San Fernando 6.60 62.0 Port Hueneme 34.145 119.206 -Feb-71 San Fernando 6.60 82.0 Wheeler Ridge 35.030 118.990 -Feb-71 San Fernando 6.60 91.0 Colton: SCE Substn. 34.060 117.320 -Feb-72 Bear Valley 5.30 31.0 Hollister City Hall 36.850 121.400	-Feb-71 San Fernando 6.60 61.4 Long Beach - Terminal Island 33.770 118.230 -Feb-71 San Fernando 6.60 62.0 Port Hueneme 35.030 118.990 -Feb-71 San Fernando 6.60 91.0 Colton: SCE Substn. 34.060 117.320 -Feb-72 Bear Valley 5.30 31.0 Hollister City Hall 36.850 121.400 -Jul-72 Sitka 7.70 300.0 Yakutat, Alaska 59.510 139.670	-Feb-71 San Fernando 6.60 61.4 Long Beach - Terminal Island 33.770 118.230 -Feb-71 San Fernando 6.60 62.0 Port Hueneme 34.145 119.206 -Feb-71 San Fernando 6.60 82.0 Wheeler Ridge 35.030 118.990 -Feb-71 San Fernando 6.60 91.0 Colton: SCE Substn. 34.060 117.320 -Feb-72 Bear Valley 5.30 31.0 Hollister City Hall 36.850 121.400 -Jul-72 Sitka 7.70 300.0 Yakutat, Alaska 59.510 139.670 -Jul-72 Sitka 7.70 145.0 Juneau 58.382 134.642	-Feb-71 San Fernando 6.60 61.4 Long Beach - Terminal Island 33.770 118.230 >Feb-71 San Fernando 6.60 82.0 Port Hueneme 34.145 119.206 >Feb-71 San Fernando 6.60 82.0 Wheeler Ridge 35.030 118.990 >Feb-71 San Fernando 6.60 91.0 Colton: SCE Substn. 34.060 117.320 >Feb-71 San Fernando 6.60 91.0 Colton: SCE Substn. 34.060 117.320 >Feb-72 Bear Valley 5.30 31.0 Hollister City Hall 36.850 121.400 Jul-72 Sitka 7.70 300.0 Yakutat, Alaska 59.510 139.670 Jul-72 Sitka 7.70 145.0 Juneau 58.382 134.642 Jul-72 Sitka 7.70 145.0 Juneau 58.382 134.642 Feb-73 Point Mugu 5.60 50.0 Jensen Filter Plant 34.312 118.496	-Feb-71 San Fernando 6.60 61.4 Long Beach - Terminal Island 33.770 118.230 -Feb-71 San Fernando 6.60 62.0 Port Hueneme 34.145 119.206 -Feb-71 San Fernando 6.60 91.0 Colton: SCE Substn. 34.060 117.320 >Feb-71 San Fernando 6.60 91.0 Colton: SCE Substn. 34.060 117.320 >Feb-72 Bear Valley 5.30 31.0 Hollister City Hall 36.850 121.400 >Jul-72 Sitka 7.70 300.0 Yakutat, Alaska 59.510 139.670 Jul-72 Sitka 7.70 45.0 Juneau 58.382 134.642 -Jul-72 Sitka 7.70 45.0 Juneau 58.382 134.642 -Feb-73 Point Mugu 5.60 50.0 Jensen Filter Plant 34.312 118.496 -Aug-75 Oroville 6.00 8.0 Oroville 50.77 121.500 -Aug-77 50 roville 5.00	-Feb-71 San Fernando 6.60 61.4 Long Beach - Terminal Island 33.770 118.230 -Feb-71 San Fernando 6.60 82.0 Wheeler Ridge 35.030 118.990 -Feb-71 San Fernando 6.60 82.0 Wheeler Ridge 35.030 118.990 -Feb-71 San Fernando 6.60 82.0 Wheeler Ridge 35.030 118.990 -Feb-71 San Fernando 6.60 91.0 Colton: SCE Substn. 34.060 117.320 -Feb-72 Bear Valley 5.30 31.0 Hollister City Hall 36.850 121.400 -Jul-72 Sitka 7.70 300.0 Yakutat, Alaska 59.510 139.670 -Jul-72 Sitka 7.70 145.0 Juneau 58.382 134.642 -Jul-72 Sitka 7.70 145.0 Juneau 58.382 134.642 -Feb-73 Point Mugu 5.60 50.0 Jensen Filter Plant 34.312 118.496 -Feb-73 Point Mugu 5.60 80.0 roville 39.550 121.500 -Aug-75 Oroville 6.00 38.0 roville 39.777 121.601 -Aug-75 Oroville 6.00 31.0 Chico 39.777 121.601 -Aug-75 Oroville 6.00	-Feb-71 San Fernando 6.60 61.4 Long Beach - Terminal Island 33.770 118.230 -Feb-71 San Fernando 6.00 82.0 Port Hueneme 34.145 119.206 -Feb-71 San Fernando 6.00 91.0 Colton: SCE Substn. 35.050 117.320 -Feb-71 San Fernando 6.00 91.0 Colton: SCE Substn. 35.050 117.320 -Feb-72 Bear Valley 5.30 31.0 Hollister City Hall 36.850 121.400 -Jul-72 Sitka 7.70 300.0 Yakutat, Alaska 59.510 139.670 Jul-72 Sitka 7.70 145.0 Juneau 58.382 134.642 Jul-72 Sitka 7.70 145.0 Juneau 58.382 134.642 Jul-72 Sitka 7.70 145.0 Juneau 58.382 134.642 Jul-72 Sitka 7.70 145.0 Juneau 34.312 118.496 Jul-72 Sitka 5.60 Jenesen Filter Plant 34.312 118.496 Jug-75 Oroville 6.00 30.0 roville 5.00 39.777 121.681 Jug-75	-Feb-71 San Fernando 6.60 61.4 Long Beach - Terminal Island 33.770 118.230 -Feb-71 San Fernando 6.60 82.0 Whert Humme 34.145 119.206 -Feb-71 San Fernando 6.60 91.0 Colton: SCE Substn. 34.060 117.320 -Feb-71 San Fernando 6.60 91.0 Colton: SCE Substn. 34.060 117.320 -Feb-71 San Fernando 6.60 91.0 Colton: SCE Substn. 34.060 117.320 -Feb-72 Bear Valley 5.30 31.0 Hollister City Hall 36.850 121.400 -Jul-72 Sitka 7.70 300.0 Yakutat, Alaska 59.510 139.670 Jul-72 Sitka 7.70 300.0 Yakutat 38.32 134.642 Jul-72 Sitka 7.70 300.0 Yakutat 34.312 118.496 -Feb-73 Point Mugu 5.60 8.0 Oroville 6.00 8.0 Oroville 39.550 121.500 -Aug-75 Oroville 6.00 30.0 Marysville 39.717 121.815 -Aug-75 Oroville 6.00 30.0 Marysville 39.749 <t< td=""><td>-Feb-71 San Fernando 6.60 61.4 Long Beach - Terminal Island 33.770 118.230 -Feb-71 San Fernando 6.00 82.0 Wheeler Rineme 34.165 117.205 -Feb-71 San Fernando 6.00 91.0 Colton: SCE Substn. 34.060 117.320 -Feb-71 San Fernando 6.00 91.0 Colton: SCE Substn. 34.060 117.320 -Feb-77 San Fernando 6.00 91.0 Colton: SCE Substn. 34.060 117.320 -Feb-77 San Fernando 6.00 91.0 Hollister City Hall 36.850 121.400 -Feb-73 Pairt 7.70 300.0 Yakutat, Alaska 59.510 139.670 -Jul-72 Sitka 7.70 145.0 Juneau 58.382 134.642 -Jul-72 Sitka 7.70 145.0 Juneau 58.382 134.642 -Jul-72 Sitka 7.70 145.0 Juneau 58.382 134.642 -Hug-75 Pointi Mugu 5.60 50.0 Jensen Filter Plant 34.312 118.496 -Hug-75 Oroville 6.00 30.0 Marysville 39.177 121.681 -Hug-75 Oroville 6.00 30.0 Marysville 39.149 121.577 -Hug-75 Oroville 6.00<td>-Feb-71 San Fernando 6.60 61.4 Long Beach - Terminal Island 33.770 118.230 -Feb-71 San Fernando 6.60 82.0 Wheeler Ruemen 34.060 117.320 -Feb-71 San Fernando 6.60 91.0 Cotton: SCE Substr. 34.060 117.320 -Feb-71 San Fernando 6.60 91.0 Cotton: SCE Substr. 34.060 117.320 -Feb-71 San Fernando 6.60 91.0 Cotton: SCE Substr. 34.060 117.320 -Feb-72 Bear Valley 5.30 31.0 Hollister City Hall 36.850 121.400 -Jul-72 Sitka 7.70 300.0 Yakutat, Alaska 59.510 139.670 -Jul-72 Sitka 7.70 300.0 Yakutat, Alaska 59.510 139.670 -Jul-72 Sitka 7.70 300.0 Yakutat, Alaska 58.382 134.642 -Jul-72 Sitka 7.70 30.0 Juneau 34.312 138.462 -Jul-72 Sitka 7.70 30.0 Juneau 34.312 138.4642 -Jul-72 Sitka 7.70 30.0 Su O Dense Filter Plant 34.312 34.642 -Hug-75 Oroville 6.00 30 39.747 21.3161 446 -Hug-75 Oroville</td><td>+Feb-71 San Fernando 6.60 61.4 Long Beach - Terminal Island 33.770 118.230 -Feb-71 San Fernando 6.60 92.0 More Huene 33.000 113.200 -Feb-71 San Fernando 6.60 91.0 Cotton: SEE Substn. 34.060 117.320 -Feb-77 San Fernando 6.60 91.0 Feutreme 35.00 118.990 -Feb-77 San Fernando 6.60 91.0 Hollister City Hall 36.50 121.400 -Feb-77 San Fulley 5.30 31.0 Hollister City Hall 36.550 121.400 -Jul-72 Sitta 7.70 30.0 Yakutat, Alaska 59.510 130.670 -Jul-72 Sitta 7.70 30.0 Varuat, Alaska 58.382 134.642 -Jul-72 Sitta 7.70 145.0 Jureau 34.312 118.496 -Jul-73 Sitta 7.70 145.0 Jureau 39.350 121.600 -Jul-75 Sitta 8.00 37.712 34.642 144.790 -Hug-75 Groville</td><td></td><td>1:eb-71 San Fernando 6.00 61, Long Baeene - Terminal Island 33:70 118:20 1:eb-71 San Fernando 6.00 91:0 Coltran: SCE Substr. 33:00 117:320 1:eb-71 San Fernando 6.00 91:0 Coltran: SCE Substr. 36:05 117:320 1:eb-71 San Fernando 6.00 91:0 Coltran: SCE Substr. 36:05 17:30 1:eb-72 Sitka 7.70 30:0 Yakuat, Alaska 59:510 139.670 1:ul-72 Sitka 7.70 30:0 Yakuat 59:511 139.670 1:ul-72 Sitka 7.70 Jareen filter Plant 34.312 148.666 1:ul-72 Sitka 7.70 Jareen 34.312 121.2150 1:ul-72 Sitka Sitka 37.1</td><td></td></td></t<>	-Feb-71 San Fernando 6.60 61.4 Long Beach - Terminal Island 33.770 118.230 -Feb-71 San Fernando 6.00 82.0 Wheeler Rineme 34.165 117.205 -Feb-71 San Fernando 6.00 91.0 Colton: SCE Substn. 34.060 117.320 -Feb-71 San Fernando 6.00 91.0 Colton: SCE Substn. 34.060 117.320 -Feb-77 San Fernando 6.00 91.0 Colton: SCE Substn. 34.060 117.320 -Feb-77 San Fernando 6.00 91.0 Hollister City Hall 36.850 121.400 -Feb-73 Pairt 7.70 300.0 Yakutat, Alaska 59.510 139.670 -Jul-72 Sitka 7.70 145.0 Juneau 58.382 134.642 -Jul-72 Sitka 7.70 145.0 Juneau 58.382 134.642 -Jul-72 Sitka 7.70 145.0 Juneau 58.382 134.642 -Hug-75 Pointi Mugu 5.60 50.0 Jensen Filter Plant 34.312 118.496 -Hug-75 Oroville 6.00 30.0 Marysville 39.177 121.681 -Hug-75 Oroville 6.00 30.0 Marysville 39.149 121.577 -Hug-75 Oroville 6.00 <td>-Feb-71 San Fernando 6.60 61.4 Long Beach - 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Terminal Island 33:70 118:20 1:eb-71 San Fernando 6.00 91:0 Coltran: SCE Substr. 33:00 117:320 1:eb-71 San Fernando 6.00 91:0 Coltran: SCE Substr. 36:05 117:320 1:eb-71 San Fernando 6.00 91:0 Coltran: SCE Substr. 36:05 17:30 1:eb-72 Sitka 7.70 30:0 Yakuat, Alaska 59:510 139.670 1:ul-72 Sitka 7.70 30:0 Yakuat 59:511 139.670 1:ul-72 Sitka 7.70 Jareen filter Plant 34.312 148.666 1:ul-72 Sitka 7.70 Jareen 34.312 121.2150 1:ul-72 Sitka Sitka 37.1</td> <td></td>	-Feb-71 San Fernando 6.60 61.4 Long Beach - Terminal Island 33.770 118.230 -Feb-71 San Fernando 6.60 82.0 Wheeler Ruemen 34.060 117.320 -Feb-71 San Fernando 6.60 91.0 Cotton: SCE Substr. 34.060 117.320 -Feb-71 San Fernando 6.60 91.0 Cotton: SCE Substr. 34.060 117.320 -Feb-71 San Fernando 6.60 91.0 Cotton: SCE Substr. 34.060 117.320 -Feb-72 Bear Valley 5.30 31.0 Hollister City Hall 36.850 121.400 -Jul-72 Sitka 7.70 300.0 Yakutat, Alaska 59.510 139.670 -Jul-72 Sitka 7.70 300.0 Yakutat, Alaska 59.510 139.670 -Jul-72 Sitka 7.70 300.0 Yakutat, Alaska 58.382 134.642 -Jul-72 Sitka 7.70 30.0 Juneau 34.312 138.462 -Jul-72 Sitka 7.70 30.0 Juneau 34.312 138.4642 -Jul-72 Sitka 7.70 30.0 Su O Dense Filter Plant 34.312 34.642 -Hug-75 Oroville 6.00 30 39.747 21.3161 446 -Hug-75 Oroville	+Feb-71 San Fernando 6.60 61.4 Long Beach - Terminal Island 33.770 118.230 -Feb-71 San Fernando 6.60 92.0 More Huene 33.000 113.200 -Feb-71 San Fernando 6.60 91.0 Cotton: SEE Substn. 34.060 117.320 -Feb-77 San Fernando 6.60 91.0 Feutreme 35.00 118.990 -Feb-77 San Fernando 6.60 91.0 Hollister City Hall 36.50 121.400 -Feb-77 San Fulley 5.30 31.0 Hollister City Hall 36.550 121.400 -Jul-72 Sitta 7.70 30.0 Yakutat, Alaska 59.510 130.670 -Jul-72 Sitta 7.70 30.0 Varuat, Alaska 58.382 134.642 -Jul-72 Sitta 7.70 145.0 Jureau 34.312 118.496 -Jul-73 Sitta 7.70 145.0 Jureau 39.350 121.600 -Jul-75 Sitta 8.00 37.712 34.642 144.790 -Hug-75 Groville		1:eb-71 San Fernando 6.00 61, Long Baeene - Terminal Island 33:70 118:20 1:eb-71 San Fernando 6.00 91:0 Coltran: SCE Substr. 33:00 117:320 1:eb-71 San Fernando 6.00 91:0 Coltran: SCE Substr. 36:05 117:320 1:eb-71 San Fernando 6.00 91:0 Coltran: SCE Substr. 36:05 17:30 1:eb-72 Sitka 7.70 30:0 Yakuat, Alaska 59:510 139.670 1:ul-72 Sitka 7.70 30:0 Yakuat 59:511 139.670 1:ul-72 Sitka 7.70 Jareen filter Plant 34.312 148.666 1:ul-72 Sitka 7.70 Jareen 34.312 121.2150 1:ul-72 Sitka Sitka 37.1	

Table 2b. Records from previous work eliminated from the current regression of response spectra.

	EARTHQUAKE	X	DIST	STATION	LAT.	LONG.
Jun-66 11-66	Parkfield Parkfield	6.10 6.10	63.6 105.0	San Luis Obispo Taft	35.285 35.150	120.660 119.460
Sep-70	Lytle Creek	5.30	19.0	Cedar Springs - Miller Canyo	34.280	117.330
Sep- 70	Lytle Creek	5.30	13.0	Wr i ghtwood	34.360	117.630
Feb-71 Feb-71 Feb-71	San Fernando San Fernando San Fernando	6.60 6.60 6.60	20.2 21.1 21.9	Lake Hughes Sta 9 Griffith Park Observatory Pasadena - Old Seism Lab	34.610 34.118 34.150	118.560 118.299 118.170
Feb-71 Feb-71 Feb-71 Feb-71 Feb-71 Feb-71	San Fernando San Fernando San Fernando San Fernando San Fernando San Fernando San Fernando	6.60 6.60 6.60 6.60 6.60 6.60	23.4 24.2 24.2 24.2 66.0 66.0	Lake Hughes Sta 1 Castaic Palmdale: Fire Station Pearblossom: Pumping Plant Fort Tejon Edmonston Pumping	34.674 34.560 34.578 34.578 34.510 34.870 34.940	118.430 118.660 118.113 117.920 118.830
Feb-71 Feb-71 Feb-71 Feb-71 Feb-71 Feb-71	San Fernando San Fernando San Fernando San Fernando San Fernando San Fernando San Fernando	6.60 6.60 6.60 6.60 6.60 6.60	24.6 46.7 56.9 61.4 82.0 82.0	Hollywood Storage Bldg PE Lo Oso Pumping Plant Palos Verdes Estates Long Beach - Terminal Island Port Hunenme Wheeler Ridge	34.090 34.808 33.801 33.770 35.030	118.340 118.720 118.387 118.387 118.230 119.206

PVJBOUT.OFR 7-16-93 11:36a

Table 3. Definition of site class

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SITE		3 S S
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Table 4. Records used the development of the equations for peak acceleration.

DATE EARTHQUAK	Σ	DIST STATION	LAT. LONG.	G HOLE	PA_H1 F	PA_H2	REFERENCE
19-May-40 Imperial /	/all 7.00	12.0 El Centro Array Sta 9	32.794 115.549	c 107	.359	.224	CIT: EERL 76-02
21-Jul-52 Kern Coun 21-Jul-52 Kern Coun 21-Jul-52 Kern Coun	y 7.40 y 7.40 y 7.40	42.0 Taft 85.0 Santa Barbara 109.0 Pasadena - Athenaeum	35.150 119.460 34.420 119.700 34.140 118.120	8 201 8 96 8 92	.196 .135 .054	.177 .090 .048	CIT: EERL 76-02 CIT: EERL 76-02 CIT: EERL 76-02
21-Jul-52 Kern Coun	:y 7.40	107.0 Hollywood Storage Bldg PE Lo	34.090 118.340	C 63	.062	.044	CIT: EERL 76-02
22-Mar-57 Daly City	5.30	8.0 San Fran.: Golden Gate Park	37.770 122.480	A 173	.127	.105	CIT: EERL 76-02
28-Jun-66 Parkfield 28-Jun-66 Parkfield	6.10 6.10	16.1 Cholame-Shandon: Temblor 17.3 Parkfield: Cholame 12W	35.710 120.170 35.639 120.404	8 200 8	.072	.282	CIT: EERL 76-02 CIT: EERL 76-02
28-Jun-66 Parkfield 28-Jun-66 Parkfield 28-Jun-66 Parkfield	6.10 6.10 6.10	6.6 Parkfield: Cholame 2 9.3 Parkfield: Cholame 5W 13.0 Parkfield: Cholame 8W	35.733 120.288 35.697 120.328 35.671 120.359	c 228 c 197 c 198	.509 .467 .279	.403	CIT: EERL 76-02 CIT: EERL 76-02 CIT: EERL 76-02
9-Apr-68 Borrego M	unt 6.60	45.0 El Centro Array Sta 9	32.794 115.549	c 107	.142	.061	CIT: EERL 76-02
9-Feb-71 San Fernal 9-Feb-71 San Fernar 9-Feb-71 San Fernar	do 6.60 do 6.60 do 6.60	17.0 Lake Hughes Sta 12 25.7 Pasadena - Athenaeum 60.7 Wrightwood	34.570 118.560 34.140 118.120 34.360 117.630	88 88 88 88 88 88	.374 .114 .057	.288 .103 .047	CIT: EERL 76-02 CIT: EERL 76-02 CIT: EERL 76-02
9-feb-71 San fernal	ndo 6.60	19.6 Lake Hughes Sta 4	34.650 118.478	c 71	.200	.159	CIT: EERL 76-02
30-Jul-72 Sitka	7.70	45.0 Sitka	57.060 135.320	A	.110	060.	USDC: USEa72
23-Dec-72 Managua	6.20	5.0 Managua: ESSO Refinery	12.145 86.322	ы	.390	.330	USGS: Circ. 713
21-Feb-73 Point Mugu	ı 5.60	16.0 Port Hueneme	34.145 119.206	ы	.130	.080	USGS: Circ. 713
28-Nov-74 Hollister	5.20	17.0 Hollister - Sago Vault	36.765 121.446	×	-011	.008	USGS: Brady
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3-XXX 5-XXX	S: OFR 9	0 USG	000	ຣິຍິ	Valley 33.512 116.800 B on 33.461 116.642 B	79.0 Cahuilla 79.4 Jule Can	7.30	Landers Landers	28- Jun-92 28- Jun-92
5-XXX 92-07	S: OFR 9. G: OSMS 9		88. 88.	8.e.	Ia: North FF 34.057 117.520 B 34.467 117.520 B	72.5 Phelan	7.30	Landers	28- Jun-92
2 - XXX	S: OFR 9		.12	:23	: N. F St. 34.183 117.295 B	76.0 San Bern	7.30	Landers	28- Jun-92
2-XXX	S: OFR 9		6,6	83	34.136 117.213 B 34.007 117 223 B	71.9 Highland	7.30	Landers	28 - Jun - 92 28 - Jun - 92
5- XXX 5- XXX	S: OFR 9			ິຮ	00 Kancin .: E. Highlands Plnt 34.122 117.158 B	66.9 San Bern	7.30	Landers	28-Jun-92
22-07	G: OSMS		95.5	32.8	In 35.268 116.684 B	65.0 Fort Irw	7.30	Landers	28- Jun-92 28- Iun-02
22-07	G: OSMS -		800	85	34.405 117.311 B	62.6 Hesperia	7.30	Landers	28- Jun-92 28- Jun-02
5-XXX 5-XXX	S: OFR 9	0 USG	00 26	68	nto Tunnel	61.7 San Jacıı 62.4 Garner Vi	7.30	Landers	28-Jun-92 28-Jun-92
5-XXX	S: OFR 9		36	ខេ	Forest Sta Garage 33.738 116.838 B	59.5 Cranston	7.30	Landers	28- Jun-92
5-XXX 	S: OFR 9		5.7 0 0	£.3	ek 34.080 117.044 B seek Dark 33.474 114.480 B	57.0 Mill Cre	7.30	Landers	28-Jun-92 28-Jun-92
3-xxx	S: OFR 9		.12	<u></u> ??	Lake " UNIC UIU " 34.230 110.733 B	45.4 Forest Fa	7.30	Landers	28-Jun-92
20-22	G: OSMS	8	21	5.5	34.887 117.047 B	37.7 Barstow	7.30	Landers	28- Jun-92 28- 1-m-02
5-XXX 5-XXX	S: OFR 9	4 USG	م 2.5	<u>е</u> г	m Springs 33.924 116.547 B Treek Fault 33.005 116.410 R	27.7 North Pa 27.8 Mission (7.30	Landers	28- Jun-92 28- Jun-92
5-xxx	S: OFR 9		57. 0	3.5 2	Construction 54,852 110,858 B 33,925 116,389 B	25.8 Fun Valle	7.30	Landers	28-Jun-92
2-07	G: OSMS			22:	ot Springs 33.962 116.509 B	22.5 Desert H	02.7	Landers	28-Jun-92
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33.888 117.640 C 34.056 117.748 C 7.30 115.3 Prado Dam 7.30 117.6 Pomona 28-Jun-92 Landers 28-Jun-92 Landers

.080 USGS: OFR 93-xxx .070 CDMG: OSMS 92-07

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Page 6 of 6

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Expanded References for Table 4:

ShortRef	LongRef
CDMG: 0SMS 89-06	Shakal et al. (1989)
CDMG: 05MS 92-05 CDMC: 05M5 02-07	Shakal et al. (1992a) Shift bis without and contain (1000)
CDMG: 05MS 92-09 CDMG: 05MS 92-09	cally UTV miles and geology (1772) Shakai et al (1902))
CDMG: OSMS PR 22	Porter (1978)
CDMG: OSMS PR 26	McJunkin and Ragsdale (1980a)
CDMG: OSMS PR 28	McJunkin and Ragsdale (1980b)
CIT: EERL 76-02	Calif. Inst. of Technology (1976)
NCEL: Lew2	T. K. Lew (1990)
SCE	S. Cal. Edison memorandom dated July 30, 1992, from T. A. Kelly
USDC: USEQ72	U. S. Dept. of Commerce (1974)
USGS+CDMG	PGA H1 from USGS: Circ. 914; the others are from CDMG: OSMS PR 28.
USGS: A	horīz. from USGS: OFR 79-1654; vert. scaled by R. L. Porcella
USGS: Brady	A. G. Brady (U.S. Geological Survey, written commun., 1977)
USGS: Circ. 713	U.S. Geological Survey (1974)
USGS: Circ. 717-A	U.S. Geological Survey (1975)
USGS: Circ. 818-A	U.S. Geological Survey (1979)
USGS: Circ. 854-B	U.S. Geological Survey (1980a)
USGS: Circ. 854-C	U.S. Geological Survey (1980b)
USGS: Circ. 914	U.S. Geological Survey (1981)
USGS: 0FR 79-1654	Porcella and Matthiesen (1979)
USGS: 0FR 79-385	PGA H1 provided by R. L. Porcella (written commun.); other values in Porcella et al. (1979)
USGS: OFR 89-568	Malëy et al. (1989)
USGS: OFR 93-XXX	Etheredge et al. (1993)
USGS: PP 1254	Brune et al. (1982)
USGS: Porcella .	R. L. Porcella (U.S. Geological Survey, written commun, various years)

Table 5. Records used in the development of the equations for response spectra.

	DATE	EARTHQUAKE	Σ	DIST STATION	LAT.	LONG. G	HOLE SOURC	щ
	19-May-40	Imperial Vall	7.00	12.0 El Centro Array Sta 9	32.794	115.549 C	107 n	
	21-Jul-52 21-Jul-52 21-Jul-52	Kern County Kern County Kern County	07.2 07.2 07.2	42.0 Taft 85.0 Santa Barbara 109.0 Pasadena - Athenaeum	35.150 34.420 34.140	119.460 B 119.700 B 118.120 B	201 n 92 n 72 n	
	21-Jul-52	Kern County	7.40	107.0 Hollywood Storage Bldg PE	Lo 34.090	118.340 C	63 n	
	22-Mar-57	Daly City	5.30	8.0 San Fran.: Golden Gate Par	k 37.770	122.480 A	173 n	
	28- Jun-66 28- Jun-66	Parkfield Parkfield	6.10 6.10	16.1 Cholame-Shandon: Temblor 17.3 Parkfield: Cholame 12W	35.710 35.639	120.170 B 120.404 B	200 n n	
	28-Jun-66 28-Jun-66 28-Jun-66	Parkfield Parkfield Parkfield	6.10 6.10 6.10	6.6 Parkfield: Cholame 2 9.3 Parkfield: Cholame 5W 13.0 Parkfield: Cholame 8W	35.733 35.697 35.671	120.288 C 120.328 C 120.359 C	228 n 197 n 198 n	
	9-Apr-68	Borrego Mount	6.60	45.0 El Centro Array Sta 9	32.794	115.549 C	107 n	
	9-Feb-71 9-Feb-71 9-Feb-71	San Fernando San Fernando San Fernando	6.60 6.60 6.60	17.0 Lake Hughes Sta 12 25.7 Pasadena - Athenaeum 60.7 Wrightwood	34.570 34.140 34.360	118.560 B 118.120 B 117.630 B	в 86 п 88 п	
	9-Feb-71	San Fernando	6.60	19.6 Lake Hughes Sta 4	34.650	118.478 C	71 n	
	30- Jul - 72	Sitka	7.70	45.0 Sitka	57.060	135.320 A	c	
	23-Dec-72	Managua	6.20	5.0 Managua: ESSO Refinery	12.145	86.322 C	c	
	28-Feb-79	st. Elias	7.60	25.4 lcy Bay	59.968	141.643 B	c	
	6-Aug-79	Coyote Lake	5.80	9.1 Gilroy Array 1	36.973	121.572 A	192 n	
	6-Aug-79	Coyote Lake	5.80	1.2 Gilroy Array 6	37.026	121.484 B	196 n	
	6- Aug- 79 6- Aug- 79 6- Aug- 79	Coyote Lake Coyote Lake Coyote Lake	5.80 5.80 5.80	3.7 Gilroy Array 4 5.3 Gilroy Array 3 7.4 Gilroy Array 2	37.005 36.987 36.982	121.522 C 121.536 C 121.556 C	195 n 194 n 193 n	
	15-0ct - 79 15-0ct - 79	Imperial Vall Imperial Vall	6.50 6.50	14.0 Parachute Test Site 26.0 Superstition Mtn	32.929 32.955	115.699 B 115.823 B	116 n n	
	15-0ct-79 15-0ct-79	Imperial Vall	6.50 6.50	.6 El Centro Array Sta 7 1.3 El Centro Array Sta 6	32.829 32.839	115.504 C	105 n 104 n	
	15-0ct-79 15-0ct-79 15-0ct-79	Imperial Vall	6.50 6.50	2.6 Bonds Corner 3.8 El Centro Array Sta 8 / 0 El Cantos Array Sta 8	32.693 32.810 32.810	115.530 C	n 70 106 1 10	
	15-0ct-79 15-0ct-79 15-0ct-79	Imperial value Imperial value Imperial value	6.50 6.50	4.0 cl centro Array Sta 2 5.1 El Centro: Differential Ar 6.8 El Centro Array Sta 4 7.5 Holtville	ra 32.796 32.864 32.864	115.432 C		
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25-Apr-92 Petrolia 25-Apr-92 Petrolia	7.10 7.10	12.3 Rio Dell 13.7 Fortuna: subermarket FF	40.503	124.100 B 124.145 B	υu
25-Apr-92 Petrolia	7.10	32.6 Shelter Cove	40.026	124.069 B	5
25-Apr-92 Petrolia	7.10	35.8 Eureka: Apartment Bldg FF	40.801	124.148 B	U
28-Jun-92 Landers	7.30	2.1 Upper Johnson Valley	34.568	116.612 A	s
28-Jun-92 Landers	7.30	41.9 Twentynine Palms	34.021	116.009 A	U
28-Jun-92 Landers	1.50	51.3 Silent Valley (Poppet Flat)	33.851	116.852 A	U
28-Jun-92 Landers	7.30	11.3 Joshua Iree	34.131	116.314 B	U
28-Jun-92 Landers	7.30	17.7 Morongo Valley: MVB	34.049	116.576 B	σ
28-Jun-92 Landers	7.30	22.5 Desert Hot Springs	33.962	116.509 B	ο U
28-Jun-92 Landers	7.30	22.8 Coolwater Generating Station	34.852	116.858 B	s
28-Jun-92 Landers	7.30	27.7 North Palm Springs	33.924	116.547 B	0
28-Jun-92 Landers	7.30	27.8 Mission Creek Fault	33.905	116.419 B	0
28-Jun-92 Landers	7.30	37.7 Barstow	34.887	117.047 B	ο U
28-Jun-92 Landers	7.30	65.0 Fort Irwin	35.268	116.684 B	U
28-Jun-92 Landers	7.30	26.3 Yermo	34,903	116.823 C	U
28-Jun-92 Landers	7.30	36.7 Palm Springs	33.829	116.501 C	0
28-Jun-92 Landers	7.30	54.9 Indio - Coachella Canal	33.717	116.156 C	U U

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Footnotes for Table 5:

REFERENCE CODE

- : 0
- Response spectra from the California Strong-Motion Instrumentation Program.
- Response spectra computed from digital uncorrected acceleration time series recorded on temporary deployments of GEOS instruments; data provided by S. Hough. 5
- Response spectra from tapes distributed by the World Data Center A for Solid Earth Geophysics, National Geophysical Data Center, Boulder, Colorado; primary data providers are the U.S. Geological Survey and the California Strong-Motion Instrumentation Program. c
- Response spectra computed from digital uncorrected acceleration time series provided by Dennis Ostrom of the Southern California Edison Company. s
- Response spectra from U. S. Geological Survey computer files, provided by P. Mork.

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Table 6: Borehole Information (AvgVel in m/s).

	101E#	¥ SITE NAME	LAT.	LONG.		COMMENTS	REFERENCE
		Pulgas Water Temple (APEEL #9 ?)	37.478	122.322	454	tt extrapolated 1.9m	Gibbs et al. (1975)
	12	Pise Lookout (APEEL #10)	37.461	122.343	401	tt extrapolated 2.2m	Gibbs et al. (1975)
	8:	Upper Van Norman Dam	34.314	118.491	282	tt extrapolated 3.7m	Gibbs et al. (1980)
	31	HOLLYWOOD STORAGE	780.45	118.558	518	to tt extrapolation	Fumal et al. (1982b)
	54	Camp Munz Laba Wumbar Eira Station	340.45	110.400	100	tt extrapolated J.JII ++ overseolated Zm	rundietai. (19020) Eumolistai (10836)
	212	Littlerock P.O.	34.521	117,981	424	tt extrapolation 2m	Fumal et al. (1982b)
	78	Pearblossom Pumo Plant	34.510	117.922	520	tt extrapolation 5m	Fumal et al. (1982b)
	2	Palmdale Holiday Inn	34.581	118.123	561	no tt extrapolation	Fumal et al. (1982b)
	80	Palmdale Fire Station	34.575	118.102	448	no tt extrapolation	Fumal et al. (1982b)
	81	Wheeler Ridge	35.026	118.992	347	no tt extrapolation; long. in OFR off by 1 deg.	Furmal et al. (1984)
	82	Edmonston Pump Plant	34.941	118.824	674	tt extrapolation 0.5m	Fumal et al. (1984)
	83	Fort Tejon	34.871	118.898	397	no tt extrapolation	Fumal et al. (1984)
	200	Oso Pumping Plant	34.811	118.721	309	tt extrapolated 3m	Fumal et al. (1984)
	00	LLIZADETN LAKE FIFE STATION	1.0.40	10.200		to tt extrapolation	Fummal et al. (1984) Firmed at al (1984)
	200	Waili SPIIIGS Camp Linghtwood	145.45	117 633	2000	LLEX.LIENCIALEU YII Do tt extremolation	Fumal et al. (1904) Fumal et al (1084)
	68	Allen Ranch	34.277	117.334	811	tt extrapolated 7.5m	Fumal et al. (1984)
	80	Cedar Springs Dam	34.308	117.315	480	no tt extrapolation	Fumal et al. (1984)
	22	Caltech Athenaeum	34.136	118.121	417	tt extrapolated <u>6</u> m	Fumal et al. (1984)
	22	Caltech Old Seismo Lab	34.148	118.171	984 1	tt extrapolated 5m	Fumal et al. (1984)
	3 8	Griffith Observatory	54.120	118.299	682	tt extrapolated /m	Fumal et al. (1984)
	23	Palos Verges Santa Bambana Calint Valina	000.00 707 72	110.200		assumed IUUUM/S TOF LAST J.JM ++ oversooloted fm	rumatetat. (1904) Ermaiatat 1087)
	20	Bonde Forner	104 02	115 228	200	IL EXIL applaced DI	rumater at. (1704) Darrella /1086)
	:8	Holtville P.O.	32.812	115.377	201		Porcella (1984)
	100	El Centro Array 2	32.916	115.366	190		Porcella (1984)
3:	101	El Centro Arraý 3	32.894	115.380	165		Porcella (1984)
2	102	El Centro Array 4	32.864	115.432	211		Porcella (1984)
	103	El Centro Array 5	32.855	115.466	207		Porcella (1984)
	201	El Centro Array 6	52.859	115.487			Porcella (1984)
	55	El Centro Array 7	52.829	115.504	212		Porcella (1984)
	<u>8</u>	El Centro Array 8 El Contro Arroy 0	118.75	250.011			Porcella (1984)
	108	EL CENTRO ALLAY 7 FL Centro Arrav 10	32.780	115.567	202		Porcella (1984)
	86	El Centro Array 11	32.752	115.594	196		Porcella (1984)
,	110	El Centro Array 12	32.718	115.637	210	tt extrapolated 2.5m	Porcella (1984)
	111	El Centro Array 13	32.709	115.683	252		Porcella (1984)
	112	El Centro Differential Array	32.796	115.535	200		Porcella (1984)
	113	Imperial County Services Bldg	32.793	115.564	189		Porcella (1984)
	1 t - + -	Brawley Airport Unitmonland Eine Station	220.22	202 211	105		POFCELLE (1904)
		Derechite Tert Station				tt avtranolated 1 Zm	POLCELLE (1904) Dorrella (1904)
	12	Calibatria Fire Station	33, 130	115.520	197	tt extrapolated 5.9m	Porcella (1984)
	118	Salton Sea Wildlife Refuge	33. 180	115.620	169	tt extrapolated 2.3m	Porcella (1984)
	119	Alameda Naval Air Station	37.785	122.308	191		Gibbs et al. (1992)
	122	Oakland Outer Harbor Wharf	37.813	122.318	<u>3</u> 1		Gibbs et al. (1992)
		San Francisco Airport	37.622	122.398	224	-	Gibbs et al. (1992)
	128	Ireasure Istand Delo Alto 2 story	070-15	C/C.221	202		LIDDS ET BL. (1992) LE Gibbe unitten rommen 1003
	129	Presidio	37.791	122.458	594		J.F. Gibbs. Written comm. 1993
	130	Corralitos	37.046	121.804	460		J.F. Gibbs, written comm., 1993
	131	Gilroy #7	37.649	121.434	333		J.F. Gibbs, written comm., 1993
	22	Voods i de	37.429	122.255	455		J.F. Gibbs, written comm., 1993
	21 21 21	Oakland 2-story	37.80/	122.265	515 215		J.F. GIDDS, Written comm., 1995 I E Cibbo unitton comm. 1002
		SLAU 2 Summaral o	207.72	102.221	140		JE Cibbe unitten comm. 1993
	137	Havward City Hall	37.681	122.081	743		J.F. Gibbs, written comm. 1993
	139	Emeryville	37.841	122.295	196		J.F. Gibbs, written comm., 1993
	140	Fremont	37.535	121.930	283	-	J.F. Gibbs, written comm., 1993
	141	Sunol	37.597	121.880	405		J.F. Gibbs, written comm., 1993
		BOREHOLE.OFR 7-15-93	d67:7			Page 1	of 2
		BOREHOLE.OFR 7-15-93	d67:7				Page 1

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Note: AVGVEL = 30m divided by the travel time to 30m; units are m/s.

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Smoothed coefficients of equations for the random horizontal component of 2 percent damped PSV (cm/s; distance in km).

Table 7a.

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	SLOG	22	N, N	i,	22	5	25	12	22	22	22	22.	ių.	20	32	N	N, X	5	2.2	ίŅ	Ń	ο'n	8.	92	200	22	10	8	8.5	88	Ř.	ถึง	5	
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horizo in km)	S1	.191	-187 186	.185	181	184	184	181	.185	.186	.187	187	.189	.190	191	. 193	.193	.195	.196 106	<u></u>	.201	203	-204	202	.207	-208	210	.211	-212 -212	212	.212	212 212	.212	Ę.
random istance	-	6.27 6.65	6.91 7.08	7.18	2.2	7.21	7.16	7.02	6.83	0.02 6.39	6.17	2°2	5.50	5.30	5.10 4.91	4.74	4.57	4.26	4.13 7.83	3.57	3.36	3.07	2.98	2.22	2.88	2.90	14.7	3.36	3.62	2. 4 4. 26	4.62	5.01 5.01	5.85	= 100.0
or the m/s; d	B7	.136	124	-206	722	.246	.258	.279	.297	.329	.343	356	.378	.387	405 405	413	.420	.433	439	404	727.	C04.	167.	202	.513	.517	528	.532	.535	.538	.539	-539 539	.537	⇒ppu
tions 1 PSV (c	B6	.071	.093	.127	153	163	172	.18	-203	.224	.232	-239	.251	-256	764	-267	12.	.276	279	-289	.293	300	303		.312	-314	762	.328	.333	342	347	.351	360	= 7.7 =
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le 7b.	81	1.725	1.782 1.828	1.864	1.872	933	1.948 1.050	1.967	1.978	1.982	1.979	1.974	1.959	1.950	1.930	1.920	1.910	1.890	1.881	1.835	1.815	1.781	1.766	cc/-1	1.722	1.724	1.701	1.696	1.695	1.700	1.706	1.715	737	uations
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Smoothed coefficients of equations for the random horizontal component of 10 percent damped PSV (cm/s; distance in km).

Table 7c.

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The equations are to be used for 5.0 <= M <= 7.7 and d <= 100.0 km.

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Smoothed coefficients of equations for the random horizontal component of 20 percent damped PSV (cm/s; distance in km).

Table 7d.

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81	1.939	2.089 2.089	2.118 2.142	2.160 2.173	2.183 2.190	2.197	2.193	2.176	2.153	2.140 2.127	2.114	2.088	2.075 2.063	2.051	1.997	1.974	1.937	1.922	1.899	1.890	1.875	1.872	1.881	1.892	1.922	1.941	1.986	uations
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Table 8a.

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The equations are to be used for 5.0 <= M <= 7.7 and d <= 100.0 km.

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Table 8b. Smoothed coefficients of equations for the larger horizontal component of 5 percent damped PSV (cm/s; distance in km).

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Smoothed coefficients of equations for the larger horizontal component of 10 percent damped PSV (cm/s; distance in km).

Table 8c.

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The equations are to be used for 5.0 <= M <= 7.7 and d <= 100.0 km.

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Smoothed coefficients of equations for the larger horizontal component of 20 percent damped PSV (cm/s; distance in km).

Table 8d.

The equations are to be used for 5.0 <= M <= 7.7 and d <= 100.0 km.

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Table 9. Coefficients of equations for the random and larger horizontal components of peak acceleration (in g; distance in km).

SLOGY	.230	•
SE	.093 .068	
SR	.193	
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s1	.193	
Ŧ	5.57 5.48	
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B6	.162	
85		
B4	0.0	
83	0.0	
82	.229	
81	105	
Component	random larger	

The equations are to be used for 5.0 <= M <= 7.7 and d <= 100.0 km.

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Table 10. Comparison of uncertainiesin the old and new regressionresults.T(sec)SLOGY-OLDSLOGY-OLD0.30.340.27

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Figure 1. The distribution of the data in magnitude and distance space (each point represents a recording). The data points labeled old data are the ones that were also used in previous studies. The top frame is for the peak acceleration data set and the bottom is for the response spectral data set.



Figure 2a. The data and regression for the second stage of the analysis, for peak acceleration and 5 percent damped response spectra at selected periods.



Figure 2b. The data and regression for the second stage of the analysis, for peak acceleration and 5 percent damped response spectra at selected periods.



Figure 3a. The unsmoothed and smoothed coefficients (light and heavy lines, respectively) for the 5 percent damped response spectra of the random horizontal component.



Random component, 5 percent PSV

Figure 3b. The unsmoothed and smoothed coefficients (light and heavy lines, respectively) for the 5 percent damped response spectra of the random horizontal component.



Figure 4. 5 percent damped, random component response spectra for magnitude 7.5 at 0 km distance, predicted from the unsmoothed and smoothed regression coefficients. The three sets of curves are for site classes A, B, and C.



Figure 5. 5 percent damped, random component response spectra for site class C at 0 km distance, predicted from the unsmoothed and smoothed regression coefficients. The three sets of curves are for magnitudes 5.5, 6.5, and 7.5.



Figure 6. 5 percent damped, random component response spectra for magnitude 7.5 and site class C, predicted from the unsmoothed and smoothed regression coefficients. The five sets of curves are for distances of 0, 10, 20, 40, and 80 km.



Figure 7. Attenuation with distance of peak acceleration and response spectra for the random horizontal component.



Distance (km)

Figure 8a. Residuals $(\log Y_{observed} - \log Y_{predicted})$, as a function of distance for magnitude groups and site classes.



Figure 8b. Residuals ($\log Y_{observed} - \log Y_{predicted}$), as a function of distance for magnitude groups and site classes.



Figure 9a. Comparison of random component, 5 percent damped response spectra computed from our previous equations and our new equations for the various site classes.



Figure 9b. Comparison of random component, 5 percent damped response spectra computed from our previous equations and our new equations for the various site classes.



Figure 10a. Comparison of ground motions computed from our previous equations and our new equations as a function of distance for magnitudes 6.5 and 7.5 and soil site classes.



Figure 10b. Comparison of ground motions computed from our previous equations and our new equations as a function of distance for magnitudes 6.5 and 7.5 and soil site classes.



Figure A1a. Smoothed and unsmoothed regression coefficients.



Random component, 2 percent PSV

Figure A1b. Smoothed and unsmoothed regression coefficients.



Figure A1c. Smoothed and unsmoothed regression coefficients.



Random component, 10 percent PSV

Figure A1d. Smoothed and unsmoothed regression coefficients.

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Figure A1e. Smoothed and unsmoothed regression coefficients.



Random component, 20 percent PSV

Figure A1f. Smoothed and unsmoothed regression coefficients.



Figure A1g. Smoothed and unsmoothed regression coefficients.



Larger component, 2 percent PSV

Figure A1h. Smoothed and unsmoothed regression coefficients.



Figure A1i. Smoothed and unsmoothed regression coefficients.



Larger component, 5 percent PSV

Figure A1j. Smoothed and unsmoothed regression coefficients.

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Figure A1k. Smoothed and unsmoothed regression coefficients.



Larger component, 10 percent PSV

Figure A11. Smoothed and unsmoothed regression coefficients.



Figure A1m. Smoothed and unsmoothed regression coefficients.



Larger component, 20 percent PSV

Figure A1n. Smoothed and unsmoothed regression coefficients.