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Evaluating Effects of Dredging-Induced Underwater Sound on Aquatic Species: A Literature Review

Burton C. Suedel, Andrew D. McQueen, Justin L. Wilkens, and Morris P. Fields

September 2019



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Evaluating Effects of Dredging-Induced Underwater Sound on Aquatic Species: A Literature Review

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Abstract

At any given moment, there may be multiple underwater sounds emanating from both natural and anthropogenic sources. Dredging activities such as the excavation, transit, and placement of material generate underwater sound. This report documents research into the biological effects of underwater sound from dredging and other anthropogenic sources to help evaluate the potential ecological risks of dredging activities. Effects data generated from exposures to anthropogenic sound sources indicate that dredging-induced sounds do not pose a significant risk of direct injury or mortality to aquatic biota. A notable exception, and much less common, is blasting activities used to remove rock and other hard substrata in navigation channels. In terms of potential non-lethal responses, low-frequency sounds produced by dredging overlap with the hearing frequency ranges of select fish and mammal species, which may pose risks for auditory temporary threshold shifts, auditory masking, and behavioral responses. To better understand the ecological risk associated with dredging sounds, a risk-based approach is needed that utilizes the available data and other site-specific information appropriate for evaluating underwater sound. The information reported herein can be used in an exposure assessment as part of a broader framework for evaluating and managing underwater sound effects on aquatic life.

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Preface

This report is part of a larger study, "Risk Characterization of Underwater Noise." This project was funded by the U.S. Army Corps of Engineers (USACE), Engineering Research and Development Center (ERDC), Dredging Operations and Environmental Research (DOER) program. Dr. Todd Bridges was the DOER program manager.

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Unit Conversion Factors

Multiply	Ву	To Obtain	
cubic feet	0.02831685	cubic meters	
cubic inches	1.6387064 E-05	cubic meters	
cubic yards	0.7645549	cubic meters	
degrees (angle)	0.01745329	radians	
degrees Fahrenheit	(F-32)/1.8	degrees Celsius	
Fathoms	1.8288	meters	
Feet	0.3048	meters	
foot-pounds force	1.355818	joules	
gallons (U.S. liquid)	3.785412 E-03	cubic meters	
Hectares	1.0 E+04	square meters	
horsepower (550 foot-pounds force per second)	745.6999	watts	
Inches	0.0254	meters	
inch-pounds (force)	0.1129848	newton meters	
Knots	0.5144444	meters per second	
Microns	1.0 E-06	meters	
miles (nautical)	1,852	meters	
miles (U.S. statute)	1,609.347	meters	
miles per hour	0.44704	meters per second	
Mils	0.0254	millimeters	
square feet	0.09290304	square meters	
square inches	6.4516 E-04	square meters	
square miles	2.589998 E+06	square meters	
square yards	0.8361274	square meters	
Yards	0.9144 meters		

Executive Summary

In the last couple decades, there has been a growing concern about the potential adverse effects of underwater anthropogenic sounds on aquatic life. In the aquatic soundscape, sound can originate from many anthropogenic sources, including construction of marine infrastructure and industrial activities, such as drilling and subsea surveys, pile driving, military activities, vessel movements, and dredging. Understanding underwater sound effects of dredging in the context of other anthropogenic activities will allow the U.S. Army Corps of Engineers (USACE), which annually dredges approximately 200 million cubic yards of sediment, to manage dredging operations appropriately whenever underwater sound is a concern.

Underwater sound from natural and anthropogenic sources is composed of many frequencies and amplitudes, which produce a combination of acoustic waves. Sound pressure level (SPL) in decibels (dB) is commonly used to quantify underwater sound, and there are a variety of SPL quantification methods used to describe acoustical properties. Due to the diversity of acoustic metrics, it is critical to use caution when comparing reported sound levels across studies. Additionally, it is crucial to understand the differences between sound source levels and organism received levels (the latter is dependent on the sound source characteristics and the sound propagation in the aquatic environment, and receptor sensitivity).

Dredge-induced underwater sounds are temporally and spatially dynamic, and dependent on site-specific activities and conditions. Dredging activities produce predominantly low-frequency (<1,000 Hertz [Hz]) sounds, which are typically continuous and non-impulsive (e.g., do not exhibit a rapid sound pressure rise time and decay). A notable exception is during blasting activities when rock and other hard substrata need to be removed in ship channels to ensure navigation safety. Dredging sounds have lower intensities in comparison to other anthropogenic activities (e.g., explosions, pile driving, seismic airguns, echosounders, and powered movement of large ships). In general, SPLs are relatively consistent among dredging types, in spite of the variability of site-specific conditions present when they were measured. Direct mechanical injury and mortality in aquatic species following underwater sound exposures are generally limited to highintensity impulsive sounds (e.g., explosions, pile driving). The currently available effects data from anthropogenic sources indicate that dredginginduced sounds do not pose a significant risk to direct injury or mortality to aquatic biota. In terms of potential non-lethal responses, low-frequency sounds produced by dredging overlap with the hearing frequency ranges of select fish and mammal species, which may pose risk for auditory temporary threshold shifts, auditory masking, and behavioral responses.

A critical aspect of the underwater sound risk framework is to identify and mitigate appropriate ecological risks, and to avoid managing ecologically insignificant risks that would pose unnecessary constraints and costs on dredging operations. Mitigation strategies to manage risks of underwater sound effects on aquatic biota generally include avoidance and minimization. Prior to the application of mitigation technologies, cost of implementation should be weighed against risk reduction to ensure practical and cost-efficient approaches are selected (i.e., cost versus benefit comparisons).

Recently updated technical guidelines have been developed by the National Oceanic and Atmospheric Administration (NOAA) National Marine Fisheries Service (NMFS) that proposed acoustic exposure criteria for select classes of marine mammals (NMFS 2016). The NMFS (2016) technical guidance document does not specifically address dredgingrelated sounds and the proposed exposure criteria are not broadly applicable to dredging. In terms of evaluating risks associated with underwater sound for site-specific activities, the technical guidance recommends the use of effects thresholds to be used with site-specific characteristics such as the sound source, environmental site conditions that influence sound propagation, and marine mammal occurrence and behavior near the sound activity (e.g., species, density, occurrence, etc.). NMFS (2016) acknowledges that alternative approaches may be used if site-specific information or data indicate it can produce a more accurate estimation of auditory risk.

To effectively understand the ecological risk associated with dredging sounds, a risk-based approach is needed that utilizes the available data and other site-specific information appropriate for evaluating the underwater sound of concern. Overall, the information reported herein regarding underwater sound produced by dredges can be used in an exposure assessment as part of a broader framework for assessing and managing underwater sound effects on aquatic life.

1 Introduction

1.1 Background

Underwater sounds can have a variety of adverse effects on aquatic life, ranging from subtle to strong behavioral reactions, even death. Some documented sub-lethal behavioral differences include startle response, habituation, attraction to or avoidance of the sound source, altered swimming behavior, and avoidance of habitat (e.g., feeding or spawning grounds) (Hawkins and Popper 2016). It is well documented that short and impulsive sounds such as those produced from pile-driving strikes, seismic airguns, and military sonar can cause behavioral reactions by fishes and cetaceans (i.e., whales, dolphins, and porpoises) up to distances of several miles from the sound source. Certain sounds can also mask communication between whales or fish (Clark et al. 2009; Erbe 2011). Masking may be particularly important for soniferous fishes (e.g., cods, croakers, groupers; Erbe 2011). These species produce sounds associated with spawning behavior, aggregating behavior, and orientation. If the anthropogenically produced sound level is sufficiently intense, sound can affect hearing and extreme sounds can lead to injury or even death. Factors that have been observed to influence response to sound stimuli include life history stage, size relative to wavelength of sound, anatomical differences, and location in the water column relative to the source (Hawkins and Popper 2016).

Research about the effects of underwater sound on aquatic life has been carried out for several decades, but there are still many uncertainties, especially with regard to the significance of sound risks posed by dredging activities. In particular, the extrapolation of effects on an individual to effects at the population or community level is highly uncertain. It is therefore important to develop a framework whereby the assessment of various sources of underwater sound can be made to improve the ability to manage such stressors.

There are multiple sources of underwater sound from natural and anthropogenic sources. Some natural sounds include vocalizations of marine life, and wind, waves, rain, and subsea volcanic and seismic activity. Some anthropogenic sources of sound originate from construction of marine infrastructure and industrial activities, such as drilling, subsea mining, military activities, vessel movements, and dredging. An important data gap is the impacts of dredging-induced sound (e.g., excavation, transit, placement) to aquatic biota and the potential impacts of dredginginduced sound in the context of other anthropogenic sources.

1.2 Objective

The objective of this report is to perform a focused literature review of the available studies to develop an improved understanding of the effects of underwater dredging sounds on aquatic life. Understanding underwater sound effects of dredging in the context of other anthropogenic activities will allow USACE, which annually dredges approximately 200 million cubic yards (myd³) of sediment, to manage dredging operations appropriately whenever underwater sound is a primary concern.

1.3 Approach

To address the stated objective, this report documents the peer-reviewed literature and government reports investigating underwater sound effects on aquatic life. Specifically, this report (1) includes a focused literature review of the natural and anthropogenic sources of underwater sound reported since 2000 (Section 3); (2) documents underwater sounds associated with anthropogenic sources (including dredging operations) and resultant effects on aquatic life (Sections 4, 5); (3) documents risk management options for underwater sound (Section 6); (4) summarizes the effects of underwater sound in the broader context of other natural and anthropogenic sources and as they relate to the NOAA NMFS underwater sound regulations published in 2016 (Section 7); and (5) recommends a path forward for assessing the risk of dredging-induced underwater sound on aquatic life (Section 8). This research is needed so the effects of underwater sound generated from dredging activities can be more completely understood-and such risks, if unacceptable, managed through application of appropriate risk management practices. The results of this work will be used to develop a framework for how underwater sound risks to aquatic life can be assessed and managed.

2 Underwater Sound Overview

This section outlines basic acoustic concepts, terminology, metrics, and measurement methods as it relates to underwater sound. This includes a brief review of the primary sound characteristics (wavelength, frequency, amplitude, and velocity) and components (pressure and particle motion). Types of sounds, sound fields, and frequency analyses (e.g., octave band analysis) are also discussed, as they are commonly used to determine and describe the sources of sound presented in the report. In addition, sound propagation and the effects of the environment on sound are presented. More detailed information about the fundamentals of underwater sound or acoustics is available from multiple sources (e.g., Richardson et al. 1995; Bradley and Stern 2008; OSPAR 2009a; Van der Graaf et al. 2012; Nedelec et al. 2016; NMFS 2016). Other specific topics about sound found in the report but not discussed here will be introduced as they appear.

Underwater sound from dredging can emanate from a variety of sources. As an example, when a backhoe dredge lowers a digging bucket on the end of an articulated arm and contacts the bottom sediment, the action vibrates particles, resulting in a sound that propagates as a longitudinal wave with repeating areas of compression and rarefaction of particles and pressure. When the particles are compressed together, part of the absorbed energy dissipates as a result of being transformed into heat, and part is transmitted through the absorbing particle and into the next. The particles vibrate back and forth in the direction of the sound wave with the speed of sound, but do not move along with the wave. The sound wave propagates through the water before the energy eventually dissipates.

The major components of a sound wave are pressure (in Pascal) and particle motion (displacement, velocity and acceleration of water in the sound wave). Sound wave pressure is measured using a hydrophone, an underwater microphone that detects changes in pressure caused by sound waves, which are converted to electrical signals. Methods available to measure particle motion include (1) calculating pressure gradients between two hydrophones; (2) measuring with velocity sensors; and (3) measuring with accelerometers (Martin et al. 2016). Perception of sound by a biological receptor is primarily the function of wavelength, frequency, amplitude, velocity, time and space. Under harmonic conditions, a pure tone is graphically presented as a single sine wave, which describes the wave at a given point over time; however, a single sine wave is rare. More commonly, sound is complex and usually composed of many frequencies and amplitudes that produce a combination of sinusoidal waves that can be challenging to quantify. Metrics used to describe sound characteristics are described below.

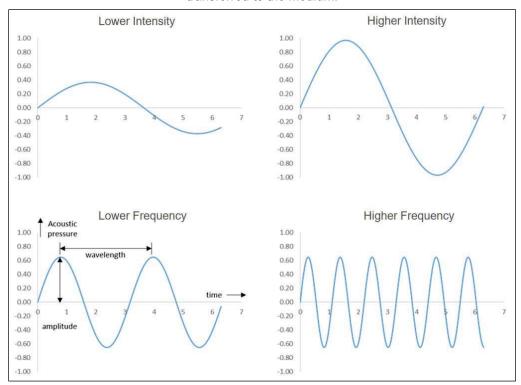
2.1 Wavelength, frequency, amplitude, and velocity

Wavelength is the distance traveled between successive pressure waves, or the distance the wave travels in one cycle of vibration.

Frequency is described in units of Hertz (Hz), where 1 Hz is equal to one cycle per second (i.e., wavelengths per second). Humans are able to hear frequencies between 20 Hz and 20 kHz (1 kHz = 1,000 Hz). Sounds less than 20 Hz are referred to as infrasound, and sounds higher than 20 kHz are ultrasound. Higher frequency (>2 kHz) sounds have shorter wavelengths, faster cycles, and a higher pitch, whereas lower frequency (<500 Hz) sounds have longer wavelengths, slower cycles, and a lower pitch. In water, a low frequency wave travels further than a high frequency wave because there is less energy adsorbed.

The **amplitude** of sound pressure changes is proportional to the maximum distance a vibrating particle is displaced. The change in pressure can be described by maximum pressure amplitude(P_M), or the root-mean-square (RMS) amplitude and is expressed in Pascal (Pa; Newton per meter squared). Decibel (dB) is a dimensionless unit commonly used as a metric to describe sound and is calculated using the ratio of a measured pressure to a reference pressure value. Amplitude determines the "loudness" or intensity. Unlike frequency and wavelength, which remain constant for a given sound, amplitude is dynamic and based on the energy of the sound (Figure 1). Low variations in amplitude results in quieter sounds, while higher variation results in more intense sounds.

The **speed of sound** is defined as the distance that a point on a wave travels per unit time and is often expressed as meters per second. Water is dense (e.g., air is 1.275 kilograms per cubic meter [kg/m³] or \approx 800 times less dense than water; freshwater= 1,000 kg/m³; seawater= 1,025 kg/m³ at 4 °C) and mostly incompressible (smaller changes in pressure); therefore, sound travels relatively fast (air 340 meters per second [m/s]; water 1,500 m/s) from particle to particle. If a sound in water and in air have the same amplitude, then the relative intensity is greater, speed is faster, and distance is longer in water. Figure 1. Acoustic pressure or sound pressure measured in water. The top left figure shows a sine wave with a lower amplitude, resulting in a lower intensity sound in comparison to the figure in the top right. The lower frequency sine wave in the bottom left completed two cycles, while the higher frequency completed six in the same time. The lower frequency wave has the same amplitude as the higher frequency, but the lower frequency wave would travel further in water because there is less energy transferred to the medium.



2.2 Types of sound

Time and space are commonly used to describe sound. Time is used to describe long or short events, while space is used to describe the temporal and spatial extent of the sound. There are many types of sounds characterized by their temporal variations in sound pressure levels, but sounds generally fall under the broad categories of continuous, non-continuous, or impulsive (ISO 12001 (1996)). A continuous or steady sound has negligible fluctuations of sound pressure levels during the observation period, while a non-continuous or non-steady sound is described by significant fluctuating pressure levels during the observation period. Non-continuous may be further described as a fluctuating sound, whereby the sound level pressure changes continuously and is highly variable; or intermittent sound, whereby the sound level drops to the level of background repeatedly. An impulsive sound is one or more bursts or pulses of sound energy, each pulse less than 1 sec in duration. Broadband and tonal sounds are discussed in underwater sound literature. Tonal

sounds can be either continuous or non-continuous and characterized by one or two single frequencies, while broadband sound is sound in which the energy is distributed over a range of frequencies.

2.3 Sound fields

The area around a sound source has been categorized into several fields to help measurements and include near, far, free, direct, and reverberant fields (see ISO 12001 (1996)). Understanding the sound fields around a source is critical for placement of sound measurement devices (e.g., hydrophones) for accurate acoustic measurements. The near field is the region close to the sound source where the sound pressure and particle velocity are not in phase (i.e., the sound pressure level can vary significantly with small changes in position). The near field is generally about one wavelength in distance from the source. In the far field, the sound level drops about 6 dB each time the distance from a point source is doubled and the sound pressure and particle velocity are in phase (i.e., interferences associated with waves reaching the receiver at different time is minimal). The free field is a region in space where sound propagates free from any form of obstruction. The direct field is the part of the sound wave that has not been reflected by any surface or obstacle. The reverberant field is the part of the sound wave that has been propagated from a source that has been reflected at least once.

2.4 Sound propagation

The sources of sound mentioned so far are commonly categorized as point source or line source. In ideal conditions, sound pressure typically drops to half its value from a point source when the distance doubles. In a medium free of boundaries or reflecting surfaces, the sound source propagates a wave in all directions in the shape of a sphere. However, reflective surfaces make this a rare phenomenon. For example, a sphere may be present for a short time before it encounters a reflecting surface, such as the sea floor or water surface, and then becomes more cylindrical as the sphere spreads further. It has also been shown that the propagation of sound from a point source is often directional, whereby a greater amount of wave energy goes in some directions more than others. An example of a point source may be a stationary bucket dredge, piling, or an explosion. A line source, such as a busy highway, or—in the case of underwater sound—perhaps a pipe carrying dredged material, drops about 3 dB for a doubling of distance

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from the source because the sound spreads out from the source as a wave front in a direction perpendicular to the line source.

Reflecting surfaces underwater affect the sound propagated and make it more difficult to determine the direction and characteristics of the sound source because part of the energy is reflected, refracted, absorbed, scattered, and transmitted by the surface. Reflecting surfaces near the receiver (i.e., marine animal) also affect the sound heard. Adding to the complexity is multipath propagation whereby the sound can reach the receiver by two or more paths or directions due to reflection and refraction. This can make it difficult to isolate the sound source. Temperature, salinity, and pressure can also affect underwater sound propagation. Overall, many variables can affect the propagation and in turn the detection of sound, including levels of ambient sounds, sound-spreading characteristics (spherical, cylindrical, directional), channelization, absorption losses, scattering losses, and the initial sound intensity (amplitude) and frequency. The significance of each variable is relative to local site conditions and may vary for a number of reasons depending on, for example, temperature, salinity, depth, and bottom topography. Overall, it should be noted that direct comparisons of sound levels among studies should be done with caution. Studies are often not directly comparable as the sound source level is estimated by propagation (or transmission) loss based on scaling factors. Estimation of sound energy loss and prediction of source levels can be "back-calculated" using scaling factors (Equation 1).

$$Trasmission \ loss = x Log\left(\frac{P_0}{P_R}\right) \tag{1}$$

Where x is the scaling factor (e.g., spherical and cylindrical spreading), P_0 is the acoustic pressure at a point 1 m from the source, and P_R is the acoustic pressure at a distance of "R" in meters. Therefore, original reports detailing the scaling approach should be reviewed before making interpretations (WODA 2013).

2.5 Frequency analysis

Sounds have been described using frequency analysis. A frequency analysis is useful to show that a sound is composed of a number of discrete frequencies present simultaneously. The accuracy and precision of the analysis is user-defined and determines the number of discrete frequencies displayed. In underwater sound research, the pressure changes detected by a hydrophone are commonly displayed on a calibrated sound-level meter. To perform frequency analysis, a filter is commonly used between the hydrophone and meter, which only allows the electrical output of the hydrophone in 1 Hz intervals to the meter. The filter allows for the meter to provide the distribution of amplitudes for individual frequencies. A graph of the sound pressures in 1 Hz intervals over a range of frequencies is called its spectrum.

Frequency analysis has been used to help identify underwater sound sources. Frequency analysis using individual frequency bands is generally avoided because it is difficult to analyze. Instead, researchers often use bands of frequencies, which have been standardized to help facilitate comparison of measurements between instruments. The widest band used in this analysis is the octave band, which represents a doubling in frequency between adjacent bands. Each band is described by its center frequency. Each measurement band contains equal energy; thus the octave band level is constant with frequency. Resolution can be improved by separating the octaves into three parts, or 1/3 octave. By using a 1/3 octave band filter, the sound from each machine, for example, can be distinguished more easily.

2.6 Sound pressure and particle motion

Mammal hearing is more sensitive to sound pressure, whereas fish and invertebrates primarily sense particle motion, but a sound wave can also be a combination of both components.

The Sound Pressure Level (SPL), expressed as L_p in dB is commonly used to describe sound (ANSI 1994). The decibel is a dimensionless unit calculated using the ratio of a measured value (p) to a reference value (Equation 2). Because the range of intensities that the receptor can respond to is large, the number is converted to a logarithmic scale for easier interpretation.

$$SPL(Lp; as dB) = 10 \log_{10} \frac{P^2}{P_{ref}^2}$$
 (2)

where *P* is the RMS sound pressure and P_{ref} is the reference pressure level. Decibels are a relative measurement that relate the intensity of a pressure wave to a standard reference pressure. In water, a standard pressure of 1 micropascal (µPa) is used, where $M = 1 \ge 10^{-6}$. The intensity of a sound at any point near the source of the sound is analogous to sound pressure level that reaches the receiver. The sound is more intense the closer the receiver is to the source and changes with time, space, and environmental factors. In the field, accurate SPLs are often difficult to obtain due to reflection off nearby objects and interference from other sound sources. Nonetheless, when appropriate controls and supporting information are available, meaningful SPLs can be obtained and compared. To make comparisons possible, it has been recommended that SPLs using the dB level should include, at minimum, the reference pressure (e.g., 20 dB re 1 μ Pa RMS) as well as how the sound pressure was measured (Madsen 2005).

Sound Exposure Level (SEL) is commonly used as a cumulative metric to describe single impulsive sounds and cyclical impulsive sounds. SEL is the total sound produced from a single sound event and is the integration of all the acoustic energy contained within the event. SEL takes into account both the intensity and the duration of a sound event. The reference value for SEL is in dB re 1 μ Pa²s. The SEL can represent either all energy received at a particular location in the water column of a given impulse or sequence of impulses (cumulative SEL or SEL_{cum}).

Peak and peak-to-peak sound pressure level may also be used to describe / quantify impulsive sounds. Peak pressure is the maximum sound pressured during a stated time interval, while peak-to-peak is sum of the peak positive (highest amplitude) and peak negative (lowest amplitude) sound pressure during a stated time interval. In terms of defining biological effect thresholds for underwater sound, SELs and Peak / Peakto-Peak sound pressure levels are commonly used (Southall et al. 2007; Carlson et al. 2007; Oestman et al. 2009; NMFS 2016).

Most fishes and invertebrates cannot directly sense the sound pressure component; rather, they detect particle-motion (Radford et al. 2012; Nedelec et al. 2016; Hawkins and Popper 2017; Popper and Hawkins 2018). The particle-motion component of sound can be expressed as displacement (meters), velocity (meters per second), or acceleration (meters per second squared) of the medium in the sound wave. Nedelec et al. (2016) noted under specific conditions particle motion can be calculated from sound pressure measurements, but relatively shallow water areas generally do not allow for direct comparison; therefore, a particle-motion sensor is recommended (Martin et al. 2016). In comparison to hydrophones, the use of underwater particle motion detectors is a relatively new method because only recently has the technology become commercially available (Nedelec et al. 2016). Particle motion is an important component, since fishes and invertebrates account for most of the marine animals (Hawkins and Popper 2017).

2.7 Sound and noise

Defined by the receiver or user, a sound can contain both useful information as well as be accompanied by useless information considered noise (Bradley and Stern 2008). Noise could be anthropogenic sounds, ambient sounds, or perhaps some type of mechanical interference when measuring the sound. In underwater sound research, noise is usually used in the context of something undesirable: noise is hazardous to health; it interferes with vocal animals. Communication noise is also otherwise disturbing and commonly propagating from an anthropogenic source and therefore useless. Because noise is defined by the receiver or user, it is often subjective, making it therefore challenging to use the term consistently. This document uses the less subjective and more scientifically established term, "sound" (e.g., Sound Pressure Level *not* Noise Pressure Level), except in cases where a scientific definition is used, such as ambient noise.

2.8 Summary

Sound results in a mechanical wave with pressure fluctuations. Sound pressure and particle motion are the primary components of a sound wave. Perception of sound is primarily the function of wavelength, frequency, amplitude, velocity, time, and space. Sound is complex and usually composed of many frequencies and amplitudes, which produce a combination of sinusoidal waves that can be disordered or random and difficult to spatially quantify. The SPL in decibels (dB) is commonly used to describe underwater sounds. SPLs are typically qualified by the methods used to estimate or summarize the acoustical properties. Common examples include RMS, peak-to-peak, or frequency bands (1/3 octave analysis or Hz range). Additionally, underwater sound propagation estimations are used to estimate SPLs at distances from the source (e.g., 1 m from source). In contrast, SELs are metrics used to estimate underwater sound exposures to biological receptors that have an integrated duration of acoustical exposure (e.g., 1 µPa² s and cumulative SEL). This report uses the less subjective and more scientifically established term "sound," instead of "noise."

3 Review of Underwater Sounds Produced by Natural and Anthropogenic Sources

To better understand the potential adverse effects from dredge-induced sounds, it is important to understand the contribution of the underwater soundscape from natural and anthropogenic sources.

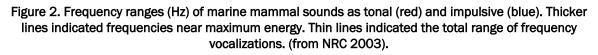
3.1 Natural sound sources

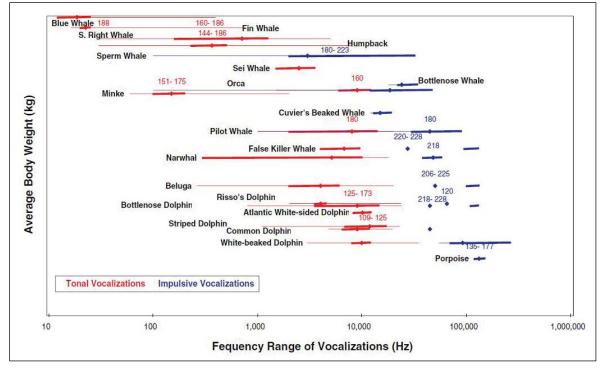
Hearing and communication systems of marine animals are assumed to be adapted to natural sources of sound. Natural sound sources in the ocean include sound by marine animals and—more broadly—sounds produced by wind, waves, rain, thunder, earthquakes, and volcanic eruptions (Wenz 1962; Koper and Plön 2012; NRC 2003; Ainslie et al. 2009).

3.1.1 Marine animals

Marine animals actively and passively use underwater sound for a variety of functions, underscoring the important role sound plays for many marine species (NRC 2005; Hawkins and Popper 2016). Marine animals can actively produce sound for communication, orientation, navigation, and localization of prey (Koper and Plön 2012). Frequencies produced by marine animals can range from infrasound to ultrasound.

Examples of sounds made by shellfish include snapping shrimp (*Alpheus* spp. and *Synalpheus* spp.) that produce sounds from tens of Hertz to >200 kHz, peaking between 2 and 5 kHz. Male ghost crabs (*Ocypode* spp.) produce a lower frequency sound (150-800 Hz). There is considerable variability in the sounds fishes produce. Fish sounds encompass a wide frequency band ranging from 0.4-4 kHz to 0.1-2 kHz. Marine mammals, such as manatees, dugongs, and seals, produce sounds ranging between 1-25 kHz. Whales and dolphins produce both mid- and high-frequency sounds depending on the species. Toothed whales and dolphins produce low- to mid- and high-frequency sounds ranging from 1-200 kHz (OSPAR 2009a). Baleen whales produce low- and mid-frequency sounds of 0.01-28 kHz (NRC 2003; Koper and Plön 2012; Figure 2).





3.1.2 Natural earth sound sources and frequencies

The weather is the source of various underwater sounds and natural sound sources are the dominant long-term average ocean sound at all frequencies in the absence of shipping (NRC 2003). The natural movement of waves as driven by wind is the most dominant natural sound source. Such sound tends to increase with increasing surface wind speed. Sound generated by waves is typically below 10 Hz, but ranges from 1 Hz to 100 kHz (NRC 2003). Waves breaking along the shore produce sound in the 100 to 700 Hz range (Koper and Plön 2012; Figure 3).

During storm events, rain, thunder, and lightning produce sound in the ocean. Rain generates sound over a wide frequency band (1 to 50 kHz) (Wenz 1962). Thunder can increase sound levels by 10 dB within the 10-250 Hz frequency band at a depth of 400 m at distances between 5 and 10 kilometers (km). A lightning strike on the water can generate an instantaneous sound of 260 dB in the frequency range of 10 to 1,000 Hz, peaking between 100 and 300 Hz (NRC 2003; Koper and Plön 2012; Figure 3).

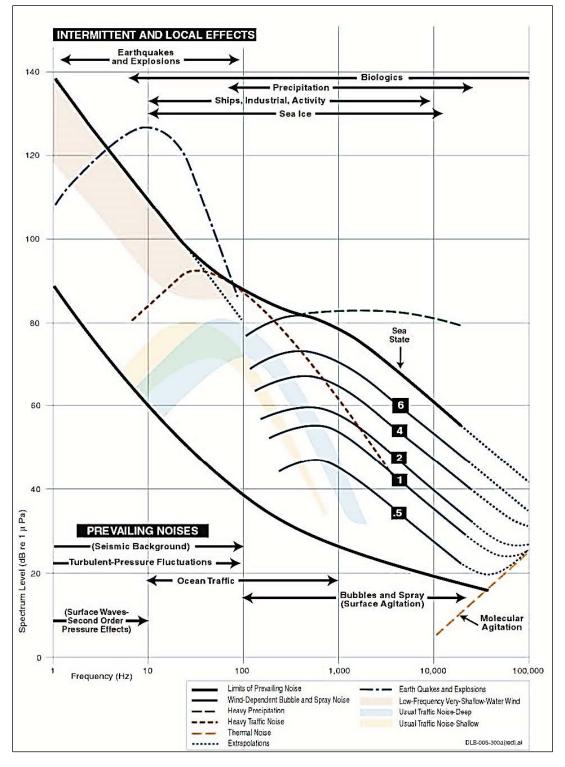


Figure 3. SPLs (dB re 1 μPa) and frequencies (Hz) of marine ambient sound. (from NRC 2003 (adapted from Wenz 1962)).

In Cook Inlet, Alaska, Dickerson et al. (2001) monitored ambient sound unrelated to anthropogenic sources. These sound sources were attributed to wind- and wave-driven turbulence, tidal flows, and precipitation. Ambient sound measurements were taken in a location away from the influence of dredging activities. Peak relative SPL was measured at 73.2 dB re 1 μ Pa-m at a peak frequency of 57.8 Hz. At Cook Inlet ambient sound relative SPL averaged 60 dB re 1 μ Pa-m at frequencies less than 100 Hz and were about 50 dB re 1 μ Pa-m level at frequencies ranging from 100 Hz to 1 kHz.

Earthquakes and volcanic eruptions can be a significant source of sound in the ocean at relatively lower frequencies (<100 Hz). Seismic activities in the Pacific Ocean are a relatively frequent source of sound, producing up to 10,000 events per year. Seismic events in the North Atlantic produce roughly 3,500 events per year. In both oceans, source levels of these events exceed 200 dB (Wenz 1962; NRC 2003; Koper and Plön 2012).

In colder regions, sea ice contributes to ambient underwater sounds, which include straining and cracking of ice due to thermal effects; and grinding, sliding, and crunching due to contact of pack ice and bergs (Wenz 1962). Frequencies associated with sea ice movement span a wide frequency range (10 to >10,000 Hz; Figure 3), with the main energy in the lower frequency bands (e.g., <1000 Hz; Wenz 1962; Lewis and Denner 1987). Lewis and Denner (1987) measured the ambient sound of sea ice movement in the Beaufort Sea (marginal sea of the Arctic Ocean). Underwater sound characteristics of sea ice movements were typically lower frequency, with the highest SPLs recorded in the 10 and 32 Hz frequency bands. In general, SPLs attributed to sea ice movement range from 60 to 90 dB re 1 μ Pa (Lewis and Denner 1987).

3.2 Anthropogenic sound sources

Anthropogenic underwater sound sources can be classified as impulsive (e.g., explosions, pile driving, geophysical surveys, acoustic deterrents) or non-impulsive (e.g., dredging, shipping, sonar and depth sounders) (Table 1).

Anthropogenic Sound	Underwater Sound Source		
	Explosions		
Ineresteisen	Pile Driving		
Impulsive ^a	Geophysical Surveys (airguns)		
	Sonar, Depth Sounders, Acoustic Deterrents		
	Dredging		
Non-impulsive ^b	Commercial Shipping		
	Energy Industry (e.g., oil and gas exploration and windfarms)		

^aimpulsive = brief duration (< 1 s), with rapid rise time and decay, repetition or as single event (ANSI 2005; NMFS 2016)

^bnon-impulsive = typically do not have a high peak sound pressure with rapid rise time or decay. Can include broadband, narrowband or tonal, brief or prolonged, continuous or intermittent (ANSI 1995; NMFS 2016)

3.2.1 Impulsive anthropogenic sound sources

3.2.1.1 Explosions

The sounds generated by explosions are typically described by a large zeroto-peak SPL. Application of underwater explosions are typically limited to military (e.g., military ship hull integrity trials) and construction (blasting rock beds; NRC 2003; Popper et al. 2014), and sometimes by dredging operations to break up rock substrates (Section 4.5). Aspects describing the characteristics of the pressure waves produced by explosions include the peak pressures, SEL, rise time, and decay. In general, explosions characteristically have a nearly instantaneous pressure rise time and lower frequencies (<1000 Hz; OSPAR 2009a; Popper et al. 2014). As an example, SPLs reported for ~0.5 to 45 kg of TNT range from 272 to 287 dB re 1 µPa (zero-to-peak) at 1 m (OSPAR 2009a). In some instances, blasting is necessary to remove hard rock and substrate prior to dredging (Hempen et al. 2007; Carlson et al. 2011; Tripathy and Shirke 2015). However, it should be noted that open-water explosions have substantially greater pressure waves in the water column as compared to confined (borehole placement) blasts (Hempen et al. 2007; IADC 2016).

3.2.1.2 Pile driving

Impulsive sounds generated by pile driving can generate SPLs ranging from 243 to 257 dB re 1 μ Pa at 1 m (peak-to-peak). The predominate energy from

pile driving is at frequencies ranging from 100 to 500 Hz (OSPAR 2009a). Characteristics of pile driving that can influence the source level include the following: method of pile driving (e.g., impact or vibropiling), pile material, diameter of the pile, and substrate (OSPAR 2009a; Popper et al. 2014; Reinhall et al. 2015). Sound characteristics of pile driving are impulsive, with a relatively rapid rise time. Due to the repetitive nature of pile driving, the sound exposure level (SEL) is commonly expressed as cumulative acoustic energy across a set number of strikes (Halvorsen et al. 2012a; Popper et al. 2014; Casper et al. 2012; 2016).

3.2.1.3 Geophysical surveys (seismic airguns)

Explorations surveying bottom substrates are commonly conducted using seismic airguns. The sound characteristics from seismic airguns are typically unidirectional (directed toward seafloor), with the main energy at a lower frequency (20-50 Hz) (OSPAR 2009b; Popper et al. 2014). These sounds are impulsive, occurring in regular intervals (typically every ~10 s; Popper et al. 2014). The acoustic pressure from airgun arrays is directly proportional to its operating pressure, with SPLs from arrays back-calculated to ~260 dB 1 μ Pa at 1 m (zero to peak; NRC 2003; OSPAR 2009a).

Acoustics surveys (e.g., seismology, tomography, thermometry) are conducted by research programs such as the Acoustic Thermometry of Ocean Climate (ATOC). These larger-scale acoustic experiments are generally infrequent (less than a dozen per year). A typical survey uses a low-frequency sound source (30-900 Hz) deployed at depths >800 m with a source level of 195 dB re 1 μ Pa at 1 m (NRC 2003).

3.2.1.4 Sonar, depth sounders, and acoustic deterrents

Modern sonar used by the military typically operates in the frequency range of 0.2 to 10 kHz (Sivle et al. 2015). Sonar operating in midfrequency (2.8 to 8.2 kHz) has underwater SPLs ranging from 223 to 235 dB 1 μ Pa at 1 m (peak; OSPAR 2009a). Low-frequency active sonar operates below 500 Hz (Popper and Hastings 2009), with peak SPLs reported up to 215 dB 1 μ Pa at 1 m (OSPAR 2009a).

In contrast to military sonars, fish finders and commercial depth sounders operate at higher frequencies, typically between 24 and 200 kHz (OSPAR 2009a), and project a lower power signal and shorter pulse lengths (OSPAR 2009b). Although there is high variability among ecosounder source SPLs, some have source SPLs exceeding 220 dB 1 μ Pa at 1 m (at 15.5 kHz with short 24 ms pulses; OSPAR 2009b).

Acoustic deterrents are devices to deter animals from approaching a specific area (e.g., fish farm, pile-driving operations; Ainslie et al. 2009). For example, the use of seismic airguns as deterrents have been investigated for repelling sea turtles from dredging operations at SPLs of 175 to 179 dB (Moein et al. 1994). Commercially available deterrents targeting dolphins and harbor porpoises have source levels ranging from 130-150 dB re 1 μ Pa²m² (at randomized intervals of 200-400 millisecond [ms]) with frequency ranges from 5 to 60 kHz (Ainslie et al. 2009).

3.2.2 Non-impulsive anthropogenic sound sources

3.2.2.1 Dredging

In general, dredging sound is described by relatively low frequencies (typically <1,000 Hz; Robinson et al. 2011; Reine et al. 2014a,b; Reine and Dickerson 2014). Sound decibel levels recorded from various dredging types (i.e., CSD, TSHD, GD, and BHD) range from ~100 to ~190 dB re 1 μ Pa at 1 m (Dickerson et al. 2001; Thomsen et al. 2009). Sounds emanating from dredging operations are discussed in greater detail in Section 4.

3.2.2.2 Commercial shipping

Reine et al. (2012a) recorded measurements at 11 locations in New York Harbor to characterize ambient sound in the absence of dredging activities (e.g., wind, waves, tidal flows, precipitation, and traffic sound from fishing and commercial shipping vessels). The authors reported a range of ambient sounds from 97 to 131 dB re 1 μ Pa RMS (mean = 117 dB re 1 μ Pa) (Figure 4).

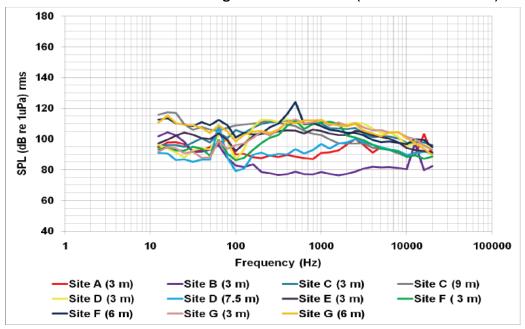


Figure 4. Example SPL results (dB re 1 µPa) from 1/3-octave analysis for monitoring ambient underwater sound at 11 sites throughout New York Harbor (from Reine et al. 2012a).

Reine et al. (2014a) measured ambient underwater sound (absent of dredging activities) at four locations (inshore, offshore, borrow area, and pump-out stations) and two water depths (3 and 6 m) and across various wind speed conditions ranging from Beaufort 1 (1-2 knots) to Beaufort 4 (11-15 knots) at Wallops Island, Virginia. Combining measurements across all sampling days, sites, water depths, and weather conditions yielded an ambient SPL RMS of 117 dB re 1 μ Pa and a 1/3 octave SPL of 121 dB re 1 μ Pa.

To place underwater sounds produced by dredges into context with commercial shipping vessels, sound data were collected for several commercial ships and ferries (Staten Island ferry, *NYK Constellation*, *Maersk Idaho*, *CSAV Licanten*, and *Zim Savannah*) operating in New York Harbor, New York, and Newark Bay, New Jersey (Reine et al. 2014a; Reine and Dickerson 2014). In New York Harbor, sound measurements were obtained from the ferry servicing the Staten Island St. George Ferry Terminal to the Battery in lower Manhattan. The ferry is approximately 310 feet (ft) (94 m) in length and 70 ft (21 m) in width and weighs 3,200 tons. Propulsion is provided by a 10,000 horsepower (hp) diesel electric engine. Vessel draft is 13.6 ft (4.1 m). SPLs were recorded from either the port or starboard side, depending on the ferry's direction of travel at distances ranging from 298 to 830 m. Received levels were lowest when the ferry was approaching the listening platform. For example, at 750 m from the source, SPLs RMS were 136 dB when the ferry was approaching the listening platform and 139.62 dB when the vessel was departing. An SPL RMS of 144.2 dB was recorded at a distance of 298 m from the source. Assuming a loss of 37.1 dB (propagation loss of 15 LogR), the source level would back-calculate to 181.3 dB re 1 μ Pa at 1m.

During a second monitoring event, the hydrophone was lowered to 30 ft (9.1 m) in 45 ft (13.6 m) of water. SPLs were recorded as the ferry departed the Battery and concluded when the ferry arrived at the St. George Terminal. SPLs increased from 125.2 dB as the ferry was departing the Battery (900 m from the source), peaking at 142 dB at 352 m off the port side of the ferry, before decreasing to 132.2 dB before arrival in St. George Terminal. The lowest SPL measured (125.2 dB at 930 m) exceeded the average background by 7.2 dB. During this monitoring event, the ferry source SPL reached 180.2 dB re 1 µPa at 1 m.

The *NYK Constellation* is a 55,000-gross-ton cargo vessel 294 m long and 32 m wide. Its fully loaded draft is 35 ft (10.6 m). Output power is 41,129 kilowatts (kW). Underwater sounds were recorded as the ship entered Newark Bay, New Jersey. SPLs were recorded at distances ranging from 122 to 1,442 m. Hydrophone depth was 10 ft (3 m) in 22 ft (6.7 m) of water. The vessel approached the listening platform from the bow at a distance of 1,400 m. At this distance, the SPL was 134 dB, exceeding background by 16 dB. An SPL of 150 dB at 122 m occurred after the vessel passed the listening platform. Assuming a loss of 31.3 dB (propagation loss of 15 LogR), the source level back-calculated to 181.3 dB re 1 µPa at 1m.

The *Maersk Idaho* is a dry cargo container vessel, 300 m long and 32 m wide. It has a gross weight of 51,000 tons and a draft of 35 ft (10.6 m). Output power is 43,070 kW. This vessel was monitored during departure from the South Elizabeth Terminal in Newark Bay. Two tugs were used to assist the *Maersk Idaho* from her berth. An SPL of 147 dB (at 622 m from the source) occurred during this phase of the departure in which underwater sounds were generated by both the cargo ship and the tugs assisting the vessel. Assuming a loss of 41.9 dB (propagation loss of 15 LogR) at 622 m, the source level back-calculated to 188.9 dB re 1 μ Pa at 1m.

The *CSAV Licanten* is a 39,941-gross-ton cargo vessel measuring 260 m in length and 32 m in width. It has a maximum draft of 12.6 m. The vessel was monitored as it passed through Anchorage Channel, New York

Harbor, into the Kill van Kull waterway (KVK). The hydrophone was deployed at a depth of 30 ft (9.1 m) in 45 ft (13.6 m) of water. SPLs were recorded at distances ranging from 353 to 900 m. An SPL of 141.8 dB was recorded 353 m from the source, exceeding background by 23.8 dB. The source level reached 180 dB re 1 μ Pa at 1 m, assuming a loss of 38.2 dB (propagation loss of 15 LogR). At a distance of 900 m, the SPL (133.76 dB) still exceeded background by approximately 16 dB.

The Zim Savannah is a 55,592-gross-ton container vessel, 294 m long and 32 m wide. It has one main engine (104 revolutions per minute [rpm]) capable of outputting 51,485 kW. It has four auxiliary engines capable of generating 1,780 kW. Bow-thruster output is 2,000 kW. The vessel has a draft of 12.5 m. This vessel was monitored passing through the KVK into Anchorage Channel, upper New York Harbor. Hydrophone depth was 30 ft (9.1 m) in 46 ft (13.9 m) of water. SPLs were recorded at distances ranging from 230 to 1,269 m. SPLs decreased across this range from 141.7 to 129.2 dB. The source level, assuming a loss of 35.43 dB (propagation loss of 15 LogR) and an SPL of 141.7 dB (321 m), the authors estimated the source level SPL as 179.3 dB re 1 μ Pa at 1 m.

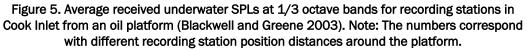
Merchant et al. (2016) reported results from a two-year underwater sound field monitoring project that was conducted to support UK policy objectives under the EU Marine Strategy Framework Directive (MSFD). Field data were collected at 12 sites around the UK during 2013 and 2014. Among the monitored 12 field locations, sound exposure varied considerably, ranging from a relatively remote site in the Celtic Sea to several sites within the North Sea with fishing vessel traffic. Median sound ranged from 81 to 95 dB re 1 μ Pa for 1/3 octave bands from 63-500 Hz. Despite the relatively close distance to shipping lanes, the Celtic Sea site was determined to be relatively undisturbed by anthropogenic sounds, with the lowest measured sound levels at 125 Hz and below. The median SPL in the Celtic Sea and Southern North Sea were 82 and 95 dB re 1 μ Pa, respectively.

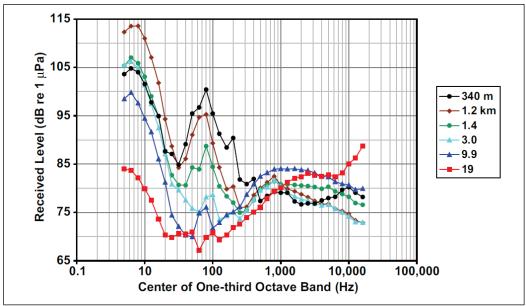
Merchant et al. (2016) also demonstrated the relative sensitivity of the RMS method to outliers when processing acoustical data. At all frequencies and locations measured, the calculated RMS exceeded the 97th percentile (Merchant et al. 2016), indicating that RMS metrics are greatly influenced by upper bound values. This study also demonstrated that based on the variability associated with ambient noises, monitoring programs are unlikely to be able to detect upward or downward trends

within reasonable timeframes (e.g., decades). Therefore, the results indicate that for monitoring ambient noise levels, absolute noise thresholds would be more beneficial than trend-based indicators.

3.2.2.3 Energy industry (oil and gas, windfarms)

Blackwell and Green (2003) measured underwater sounds near an offshore oil platform in Cook Inlet, Alaska. The highest broadband (10-20,000 Hz) sound level recorded was 114 dB re 1 μ Pa at a distance of 1.2 km (Figure 5). In general, the acoustic signature measured from the oil platform was lower frequency (<1,000 Hz), with the majority (84%) of the strongest tones occurring below 500 Hz. One third octave band levels underwater for all recording stations had a peak noise around 80 Hz.





Operation of offshore wind farms are also a source of underwater sound. During operation, wind turbines produce sounds with frequencies at peak energies of 30 to 200 Hz (OSPAR 2009a). "Low-power" (< 1MW) turbines have sound source levels ranging from 142 to 153 dB (peak spectral energy at 16 Hz; Nedwell and Howell 2004). Nedwell et al. (2007) monitored sound at a windfarm and found that operational underwater sound was comparable to ambient background conditions, with underwater source levels near (<5 m) the turbines measured at 124 dB as compared to 122 dB outside the 500 m proximity. In addition to operation, the construction and decommissioning also are potential sound sources (i.e., pile driving, drilling, rock layering; Nedwell and Howell 2004).

3.2.3 Summary of natural and anthropogenic underwater sound sources

The ambient underwater soundscape is diverse, with natural physical and biological sounds contributing a wide spectrum of frequencies and SPLs (Table 2 and 3). In general, underwater sounds can be categorized by impulsive and non-impulsive. Common metrics to describe sound characteristics include SPL (e.g., peak, RMS), frequency (bandwidth and "main energy" (i.e., the majority of energy of a sound event occurring in a given frequency range)), and signal duration. Natural or ambient conditions can be diverse, with biological sounds from vocal species having high intensity (SPLs), which can exceed 200 dB 1 μ Pa at 1 m (Table 3). The highest intensity anthropogenic sounds (>200 dB 1 μ Pa at 1 m) are from impulsive sounds, which include explosions, pile driving, seismic surveys, and sonar (Table 3). Non-impulsive anthropogenic sounds include shipping, dredging, and energy production (e.g., wind turbine and oil/gas drilling), which typically have SPLs <200 dB 1 μ Pa at 1 m (Table 3).

Frequency Underwater Sound Source		
1 to 10 Hz	explosions	
1 10 10 112	ship propellers	
	explosions	
	seismic airguns	
10 to 1,000 Hz	sonar (low frequency)	
10 10 1,000 112	dredging	
	shipping	
	construction and industrial activities	
	seismic airguns	
1,000 to 10,000 Hz	sonar (mid-frequency)	
1,000 to 10,000 Hz	seafloor profiles	
	depth sounders	
	sonar (high-frequency)	
10,000 to 100,000 Hz	fish finders	
	acoustic Doppler profiles	
	mine hunting	
>100,000 Hz	fish finders	
× 100,000 HZ	high-resolution seafloor mapping	
	research sonars	

Table 2. Underwater sound frequency ranges of anthropogenic sources (NRC 2003;
Appendix A).

Sound Source	Source Level dB re 1 µPa at 1 m, (unless otherwise stated)	Frequency (kHz)	Main Energy (kHz)	Reference		
Natural						
Biological						
sperm whale click	236 (RMS)	5 to 40	15	Mohl et al. 2003		
snapping shrimp	183 - 189 (peak)	< 2 to 200	2 to 5	Au and Banks 1998		
harbor porpoise click	205 (peak)	110 to 160	130 to 140	Villadsgaard et al. 2007		
Physical						
waves	~40 - 80	0.001 to 100	NR	Wenz 1962; NRC 2003		
weather (rain, thunder)	~80	1 to 50	NR	Wenz 1962; NRC 2003		
ambient harbor ^a	60 - 73.2	0.1 to 100	NR	Dickerson et al. 2001		
Anthropogenic						
Offshore Construction						
explosives	272 - 287 (peak)	0.002 to 1	0.006 to 0.021	OSPAR 2009a		
confined blasting	220 (peak)	0.004 to 1	NR	Hall 2010		
pile driving	243 - 257 (peak)	0.02 to 20	0.1 to 0.5	OSPAR 2009a		
Seismic surveys						
airgun array	260 - 262 (peak)	0.01 to 100	0.01 to 0.12	OSPAR 2009a		
Sonar						
echosounders	235 (peak)	variable	1.5 to 36	OSPAR 2009a		
military sonar						
(low-frequency)	215 (peak)	0.1 to 0.5	NR	OSPAR 2009a		
military sonar						
(mid-frequency)	223 - 235 (peak)	2.8 to 8.2	4	OSPAR 2009a		
Offshore industrial activities						
wind turbine	142 (RMS)	0.016 to 20	0.03 to 0.2	OSPAR 2009a		
drilling	145 - 190 (RMS)	0.010 to 10	<0.1	OSPAR 2009a		
Shipping						
small boats and ships	160 - 180 (RMS)	0.02 to 1	> 1	OSPAR 2009a		
large vessels	180 - 190 (RMS)	0.006 to 30	> 0.02	OSPAR 2009a		
New York Harbor						
(ambient) ^b	75 - 125			Reine et al. 2014		
Dredging				0		
				Greene 1987; Reine et		
CSD	168 - 175	0.03 to 20	0.02 to 1	al. 2012b; Reine and Dickerson 2014		
	T00 - T12	0.03 10 20	0.02 (0 1	Nedwell et al. 2008; de		
TSHD	172 - 190	0.03 to 20	0.03 to 1	Jong et al. 2010		
GD	107 - 124°	0.03 to 20	0.02 to 1	Dickerson et al. 2001		
				Nedwell et al. 2008;		
BHD	163 - 179	0.03 to 20	0.13 to 1.25	Reine et al. 2012a		
				peak = maximum		
^a Ambient sound measured a	t Cook Inlet, Alaska (absent o	f shipping noise)		pressure		
	RMS = root mean					

 $^{\rm b}\!Ambient$ harbor sounds (with shipping) measured at 3 m depth $^{\circ}\!124$ dB was measured at 158 m from sound source

peak = maximum pressure RMS = root mean square NR = not reported

4 Review of Underwater Sounds Produced by Dredging Operations

In this section, what is currently known about sources of underwater sound produced by dredging activities is presented. Studies reporting underwater sounds emanating from operating dredges are limited to the last couple of decades. The Central Dredging and World Dredging Associations (CEDA and WODA, respectively) and the Convention for the Protection of the Marine Environment of the North-East Atlantic (OSPAR) have recently published general overviews of underwater sounds produced by various dredge types (CEDA 2011; WODA 2013; OSPAR 2009a,b).

The following sections describe the common dredge types followed by a review of studies conducted to describe sounds emanating from these dredge types. In addition, acoustical properties associated with confined rock blasting are discussed below due to the association with dredging operations to remove hard rock or substrate.

4.1 Dredging types

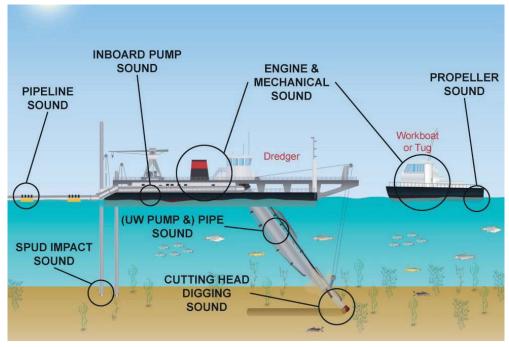
Most dredges share three main categories of activities that produce most of the underwater sound: excavation, transit, and dredged material placement (CEDA 2011). Dredging produces sounds that are continuous, discontinuous, and/or cyclic in nature. The two main categories of dredges are hydraulic and mechanical dredges.

4.1.1 Hydraulic dredges

Hydraulic dredges work by sucking a mixture of dredged material and water from the bottom. The two main types of hydraulic dredges are cutter suction dredges and trailing suction hopper dredges (CEDA 2011; WODA 2013).

4.1.1.1 Cutter suction dredges (CSD)

Cutter suction dredges (CSD) suck material through an intake pipe and then push the material out of a discharge pipeline directly into a transport barge or a placement site. A cutterhead at the suction end of the intake pipe rotates in contact with the sediment bed while swinging laterally into the sediment surface. Some cutterheads are capable of dredging rock-like formations such as basalt or limestone. The dredge incrementally advances forward by alternately swiveling on spud poles or pushing ahead on a travelling spud while anchored cables on each side of the dredge control lateral movement. Because CSDs use pipelines to dispose of dredged material directly into a transport barge or a placement site, the operations are usually continuous (i.e., 24 hours, 7 days a week) until the job is completed. Figure 6 illustrates the sources of sounds associated with CSDs (CEDA 2011).





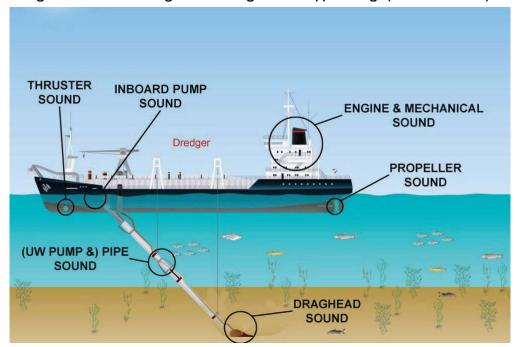
Primary sources of continuous CSD sounds include: (1) dredged material collection sounds originating from the rotating cutterhead in contact with the sediment and intake of the sediment-slurry; (2) sounds generated by pumps and impellers pushing sediment-slurry through pipes; (3) transport sounds resulting from the movement of sediment-slurry through pipes; and (4) ship machinery sounds, including those associated with the lowering and lifting of spuds and moving anchored cables.

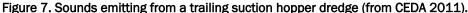
The duration of production cuts in dredging activities depends on depth of cutterhead insertion, type of material being excavated, and width of the navigation channel (Reine et al. 2012b). The USACE Navigation Data Center (NDC) (<u>www.navigationdatacenter.us</u>) contains historical data for dredging projects, including start and end dates for CSD projects dating back to 1983. The average duration of a contracted dredging project was 107 days

(median = 64 days), while a federal dredging project average was 41 days (median = 32 days). There have been approximately 2,779 CSD projects since the 1980s, making this the most widely used dredging method contracted or used by USACE in the United States.

4.1.1.2 Trailing suction hopper dredges (TSHD)

Trailing suction hopper dredges (TSHD) are ships with propulsion and large hoppers for containing dredged material. During dredging, long intake pipes, termed drag arms, extend from the ship and drag along the bottom. Erosion, teeth, and water jets loosen the material, and pumps are then used to suck the material from the bottom into the hopper. When the hopper is full, dredging stops, and the ship travels to a dredged material placement site where the material is discharged from the bottom of the ship, or pumped out through a discharge pipeline. The length of time dredging stops is dependent on the haul distance to the placement site. Figure 7 illustrates the sources of sounds associated with TSHDs (CEDA 2011).





Continuous TSHD sounds are produced from the ship's propulsion during dredging and transit to the placement site. Sounds associated with dredging are considered discontinuous and cyclic because dredging stops when the hopper is full and the ship moves to and from the dredging area and placement site. During dredging, the draghead produces continuous sounds when it makes contact with the bottom substrate as the draghead trails beneath the dredge during advancement. The sound produced during filling of the hopper is associated with propeller and engine sound, with additional sounds emitted by pumps and generators. It was determined with historical data obtained from the USACE NDC (http://www.navigationdatacenter.us/dredge/dredge.htm) that the average duration of a contracted TSHD project was 99 days (median = 70 days), while the average duration of federal dredging projects was 27 days (median = 14 days). There have been approximately 1,697 TSHD projects since the 1980s, and it is the second most-used dredging method behind CSD by the USACE in the United States.

4.1.2 Mechanical dredges

Mechanical dredges remove material by scooping it from the bottom substrate. The two main types are grab dredges and backhoe dredges (CEDA 2011, WODA 2013). Both dredge types are relatively stationary operations and commonly use barges to transport material to the placement site. The USACE NDC

(http://www.navigationdatacenter.us/dredge/dredge.htm) does not distinguish between a grab dredge and a backhoe dredge, so all bucket and mechanical dredge start and end dates were reviewed. The average duration of a project was 102 days (median = 58 days). There have been approximately 1,077 mechanical dredging projects since the 1980s, and mechanical dredging is the third most-used dredging method behind CSD and TSHD, respectively, in the United States.

4.1.2.1 Grab dredges (GD)

The GD, also referred to as a clamshell or bucket dredge in U.S. parlance, is a commonly used mechanical dredging method in the United States. The GD is a stationary operation with or without propulsion. Grab dredges can be held in place with spuds or anchors. Often, several barges are used to store and transport the dredged material for placement. The dredging activity occurs in intervals and is regularly repeated whereby the grab is lowered, closed, hoisted, swung to the barge, and the bucket opened to release the material. Figure 8 illustrates the sources of sounds associated with GDs (CEDA 2011).

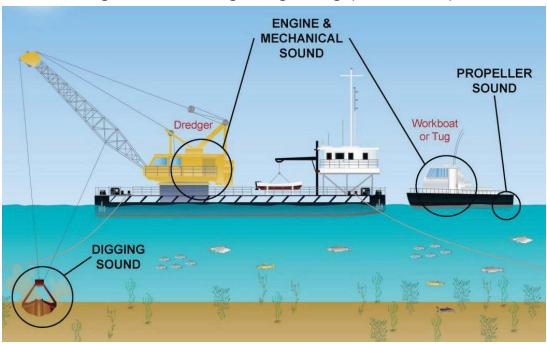


Figure 8. Sounds emitting from a grab dredge (from CEDA 2011).

Dickerson et al. (2001) and Clarke et al. (2002) described GD operations as a discontinuous and cyclic sound produced by winches and derrick movement, bucket contact with the substrate, digging into substrate, bucket closing, and emptying of material into a barge or scow. The sounds are repeated approximately every minute, with intermittent interruptions due to barge maneuvering and maintenance activities.

4.1.2.2 Backhoe dredges (BHD)

A BHD is a stationary platform with a hydraulic excavator having a single digging bucket positioned on the end of an articulated arm. The BHD digs by drawing bottom sediment backwards and is typically used to work in harder material than GDs. The BHD sits on a barge that is anchored, and the position is maintained with spud poles to provide a stable platform to account for the reaction forces from digging. Similar to the GD, several barges are used to store and transport material dredged by the BHD. The workflow is also similar to the GD in that dredging occurs in regular intervals (discontinuous) and is repeated (cyclic), whereas the backhoe is lowered, drawn backwards to fill with sediment, lifted, swung to the barge, and the bucket inverted to release the material. Figure 9 illustrates the sources of sounds associated with BHDs (CEDA 2011).

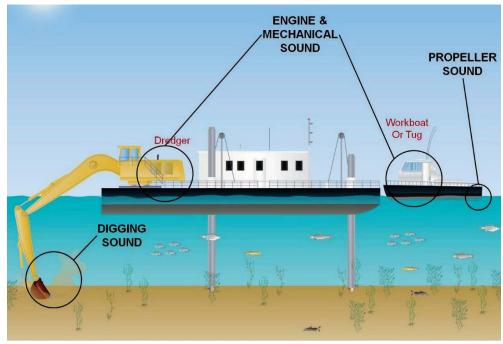


Figure 9. Sounds emitting from a backhoe dredge (from CEDA 2011).

Sound sources produced by BHD originate from several sources. Grinding and scraping sounds are produced when the backhoe is drawn backwards to fill with material. Sounds are produced by hydraulic pumps and the articulated bucket support arm during subsequent lifting of the material from the substrate through the water column. Sounds are transmitted through the hull of the receiving barge during placement into it. Onboard machinery associated with winches, generators, and engines also produce sounds. Other periodic sounds include the movement of spud poles or anchor cables. Engine sounds are produced by tugboats and tenders when they are used to transport barges with sediment to placement sites.

4.2 Dredging studies: hydraulic and mechanical dredges

Field studies have been performed that investigated the sounds produced during dredging operations, predominantly conducted in the United Kingdom (UK) and U.S. Nedwell et al. (2008) and the Marine Aggregate Levy Sustainability Fund (MALSF) published reports that documented the underwater sound generated from dredging operations in UK harbors. Numerous field studies have been performed by various investigators when the Port of Rotterdam was expanded in the Netherlands. In the United States, investigators at the USACE published a series of reports on the underwater sounds produced by various dredge types operating in nearshore and offshore scenarios.

4.2.1 United Kingdom: Nedwell et al. (2008)

Nedwell et al. (2008) measured underwater sound produced by the BHD *Manu Pekka* as it operated in a harbor in Lerwick, Shetland. After excavation by the BHD, the dredged material was transferred into an adjacent moored scow. Once loaded, the scow was transported to a reclamation area where the material was placed.

At a distance of 7 m from the BHD, the underwater sound generated by the dredge was reported as being caused by the ship generators (continuous sound) and movement of the articulated bucket support arm (non-continuous sound; Figure 10). Based on a 10 log (R/1 m) scaling, the source level was estimated to range from 140 to 145 dB re 1 μ Pa (10 to 15 Pa) at 1 m. An increase in underwater sounds was observed when the bucket struck the seabed, followed by more intense sound levels as the bucket was drawn backwards, which produced grinding and scraping sounds when the bucket was filled with material (Figure 11). During this period, the underwater sound source levels were estimated increased from 145 to 162 dB re 1 μ Pa at 1 m. The material dumped into the scow was also measured at a distance of 7 m, but this sound source did not significantly contribute to the overall measured sound level.

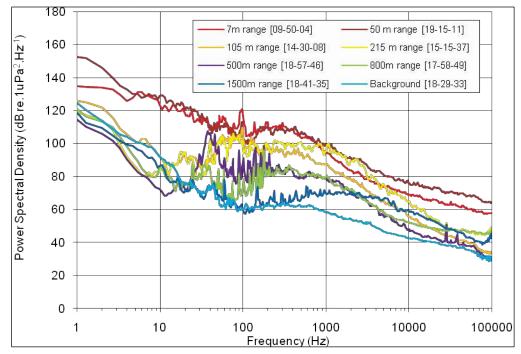


Figure 10. Variation in spectral levels of underwater sound resulting from backhoe excavation dredging operations in Lerwick, Shetland (UK) (from Nedwell et al. 2008).

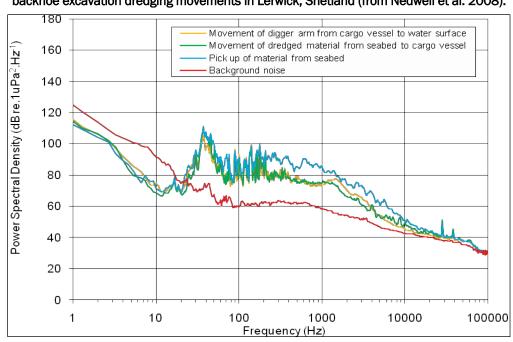


Figure 11. Comparison of spectral levels of underwater sound resulting from various backhoe excavation dredging movements in Lerwick, Shetland (from Nedwell et al. 2008).

At 105 m from the BHD, the bucket grinding and scraping was still audible and reached a maximum SPL of 145 dB re 1 μ Pa. More commonly, the underwater sound emanating from the BHD operations ranged from 132 dB re 1 μ Pa to 136 dB re 1 μ Pa (Nedwell et al. 2008). Based on a 10-log (R/1 m) scaling factor, source SPLs were estimated at 163 dB re 1 μ Pa at 1 m.

Overall, Nedwell et al. (2008) observed that BHD activities increased the underwater sound relative to background sound levels at frequencies from about 20 Hz to approximately 20 kHz. A relatively continuous sound was generated by the dredge at the low frequency range from 20 to 80 Hz, with peak spectral sound levels occurring between 35 and 45 Hz (Figure 11). These sounds were relatively consistent regardless of the dredging arm activity; therefore, they were likely a feature of the dredging generator systems.

4.2.2 United Kingdom: Robinson et al. (2011)

The MALSF published a study (Robinson et al. 2011) that provided data for the underwater sound levels generated by the seven TSHDs during marine aggregate (sand and gravel) excavation at three locations along the UK coast. Dredging (i.e., draghead on seabed, pump on, excavating aggregate, speed 1 - 2 knots) and turning (i.e., draghead raised, pump on or off, state when turning at end of track) modes were assessed in water depths ranging from 27 m to 45 m.

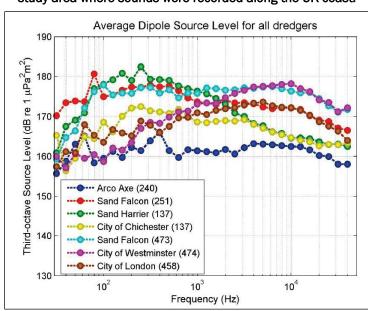


Figure 12. Underwater sound output measured from seven TSHD in the UK fleet during typical operating conditions (taken from Robinson et al. 2011). Numbers in parentheses indicate study area where sounds were recorded along the UK coast.

The results of the study indicated that the main energy of underwater sound originating from dredges were at frequencies less than 500 Hz (Figure 12) and were similar to those measured for cargo ships traveling at speeds reasonable for harbor transit (around 8-16 knots). Analysis of the data indicated that the primary source of higher frequency sounds (> 1,000 Hz) were due to the abrasion of the aggregate material passing through the draghead, suction pipe, and pump (and possibly cavitation). Elevated broadband sound depended on the aggregate type being extracted, with coarse gravel generating greater SPLs than sand. Dredge transit sounds were not measured during this study.

4.2.3 The Netherlands: Maasvlatke 2 studies

The Port of Rotterdam began a major expansion beginning in 2008 to meet ever-increasing demands to accommodate larger cargo vessels. During the construction of Maasvlatke 2 expansion, several dredges (i.e., TSHD) were monitored and underwater sound during operations were measured (de Jong et al. 2010; Heinis et al. 2013).

During the Port of Rotterdam expansion, de Jong et al. (2010) measured underwater sound produced by several TSHD. Underwater sound was measured for dredging, transit, pumping, and discharge of sediment, which consisted mostly of sand. The authors developed a sound propagation model for shallow water areas and provided an estimate of the dipole source level spectra covering a wide frequency band. Dipole source levels of underwater sound accounts for the interactions of the direct and surface reflected sound propagation paths.

The results indicated that the greatest SPLs were recorded for large dredges during transit (at speeds up to 16 knots). The activity of dredging sand yielded source levels typically less than those for dredges in transit (Figure 13). Similarly, the activities of pumping and rainbowing (i.e., aerial discharge of dredged material as a fountain; in this case, while stationary) resulted in source levels similar to those recorded when dredging sand. Sand dumping produced the lowest SPLs, but the authors attributed this to the absence of cavitation sound from the propellers and bow thrusters which dominated all other measured dredging activities. The frequency range was typically between 500 Hz and 10 kHz. Broadband sound characteristics greater than 100 Hz were similar across dredging activities except sand dumping. The average dredging sounds measured among TSHD during operations were strikingly similar (Figure 14). In the 50 to 1000 Hz frequency range, TSHD SPLs ranged from 160 to 186 dB re 1 mPa-m in 1/3 octave band (Figure 14). Overall, the authors indicated that cavitation sounds from propellers and bow thrusters were the main sound sources, especially during dredging and pumping (de Jong et al. 2010).

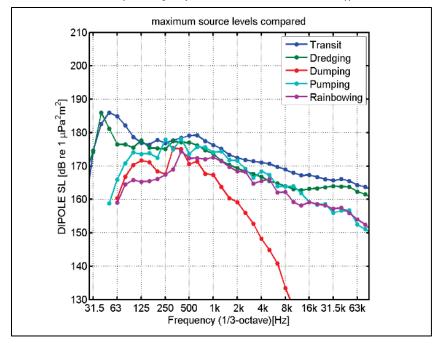
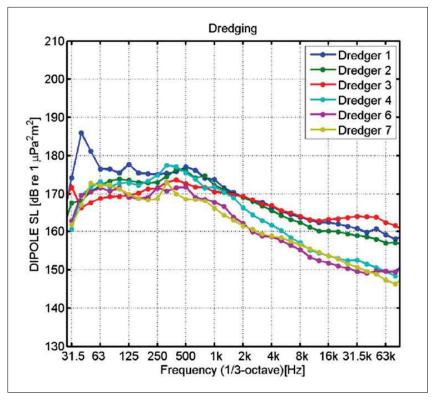


Figure 13. Dipole source level (dB re $1 \mu Pa^2m^2$) in third octave bands (maximum of all measurements for each activity) for TSHD in transit, and while dredging, dumping, pumping, and rainbowing (from de Jong et al. 2010 (actually copied from Ainslie et al. 2012)).

Figure 14. Comparison of dipole source level (dB re 1 mPa²m²) in 1/3 octave bands of 6 TSHD (from de Jong et al. 2010).



4.2.4 United States: Dickerson et al. (2001)

A study (Dickerson et al. 2001) was performed to characterize underwater sounds of a GD operation. Underwater sound was monitored for GD operations in Cook Inlet, Alaska, where the GD *Viking* was used to deepen the navigation channel and the GD *Crystal Gayle* was used to dredge the port docks. The GD operations were described as a repetitive sequence of sounds, with the sounds repeated on approximately 1 minute (min) intervals with periodic interruptions due to barge maneuvering and maintenance activities. SPLs (dB re 1 μ Pa RMS) were recorded for six GD sound events measured at a distance of 150 m (Table 4).

Dredge activity	SPL at 150 m (dB re µPa RMS)	Peak frequency (Hz)	Comment
Bucket striking channel bottom	124	162.8	-
Bucket digging	113.2	40.4	for coarse sediment and/or gravel
Bucket closing	99.2	316.3	lowest underwater sound during dredge cycle
Winch in/out	116.6	34.9	-
Dumping material into barge	108.6	82.1	sounds were dependent on volume of material in barge, as more material was placed in barge, SPLs were often less due to loss of transmission through material and hull
Emptying barge at placement site	108.7	45.8	-

Table 4. SPLs (dB re 1 µPa RMS) recorded for six GD sound events measured at a distance of 1.	50 m.
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As a basis for comparison, ambient sound measurements taken in a location away from the influence of dredging activities yielded peak ambient sound at 73.2 dB (relative dB RMS) at a peak frequency of 57.8 Hz. In general, ambient sound averaged 60 dB at frequencies less than 100 Hz and about 50 dB level at frequencies ranging from 100 Hz to 1 kHz.

Underwater sounds produced from GD operations were quite variable, depending on the phase of the operation. Underwater sounds produced during GD operations in decreasing order of sounds produced were bucket striking the channel bottom, winch motor, bucket digging, bucket closing, and dumping material in a hopper barge. The buckets striking the channel bottom were dependent on substrate type, as buckets striking coarse sediments produced more sound than strikes in unconsolidated muds. Sounds produced during bucket closing events were variable and not always audible. Sound produced from dumping material into the hopper barge attenuated most rapidly with increasing distance from the sound source, with no audible sounds detected beyond 1,200 m. The authors reported that SPLs (relative dB RMS) diminished from 15 to 30 dB at 150 m and 5,500 m distance from the dredge source. All dredging—related sounds were not detectable beyond 5.5 km, with the exception of the bucket striking the channel bottom, which was slightly above background at 7 km.

4.2.5 United States: Clarke et al. (2002)

Clark et al. (2002) characterized underwater sounds generated by GD, CSD, and TSHD operations. The 1,500 hp GD *Viking* (10 yd³ (8.4 m³) bucket) was monitored while dredging coarse sand and gravel in Cook Inlet, Alaska, during the deepening of the entrance channel to the Port of Anchorage. The CSD *James B*, a 10,000 hp dredge with a 24-inch (0.6 m) discharge pipe diameter (Lake Michigan Contractors Dredge), was monitored during channel maintenance in Mississippi Sound, Mississippi. The TSHD *Stuyvesant* (Bean Stuyvesant), a 15,000 hp dredge with an 11,140 yd³ (9,314 m³) capacity, was monitored during maintenance and subsequent transport of dredged material to an offshore placement site in upper Mobile Bay, Alabama.

The authors found that the intensity, periodicity, and spectra of sounds produced differed substantially between the three dredges studied. Consistent with sounds observed by Dickerson et al. (2001), GDs produce a repetitive sequence of sounds generated by winches, bucket impact with the substrate, bucket closing, and bucket emptying. Sounds from the CSD generated more continuous sound produced as the cutterhead rotated in bottom sediment. TSHD sounds were produced from two continuous sources (engine and propeller sounds), and sounds from the draghead contacting sediments. The authors noted that underwater sounds produced by dredges are dependent on several factors, including substrate type, geomorphology of the waterway, site-specific hydrodynamic conditions, equipment maintenance status, and skill of the dredge plant operator.

The authors reported sound attenuation over distance when the GD's bucket struck the channel bottom. A reduction of 30 dB re 1 μ Pa-m occurred between the 150 m (124.01 dB re 1 μ Pa-m; peak frequency 162.9 Hz) and 5,000 m distance from the dredge (94.97 dB re 1 *m*Pa-m; peak frequency 72.7 Hz). The authors detected only faintly audible sounds at 7 km from the sound source.

4.2.6 United States: Reine et al. (2012a)

Reine et al. (2012a; also reported in Reine et al. 2014a) characterized sounds produced by the dredge *New York*, a 3,434-hp BHD (Great Lakes Dredge and Dock) during removal of coarse gravel-sized rock in New York/New Jersey Harbor as part of a channel deepening project. The authors also monitored ambient sounds in several locations in the harbor unrelated to dredging operations.

Most of underwater sounds recorded during operation of the BHD were of low frequency, generally in the range of 130 Hz to 1.25 kHz. The lowest frequency sounds (< 200 Hz) were associated with spud walking; the highest frequencies (1.25 kHz) were associated with raising or lowering the spuds during movement or anchoring. The most intense sounds were when the bucket was drawn backwards to fill with material, which produced grinding and scraping sounds and when the spuds were raised and lowered. Source levels for the bucket were 179 dB re 1 μ Pa at 1 m. Source levels were less when spuds were raised and lowered (176 dB re 1 μ Pa at 1 m) and during spud walking (172 dB re 1 μ Pa at 1 m).

The authors also reported source levels for four other sound events during BHD activities, all with similar source levels. These sound sources included popping sounds (SPL = 167.1 dB re 1 μ Pa at 1 m), engine/generator sounds (SPL = 167 dB re 1 μ Pa at 1 m), barge loading sounds (SPL = 166 dB re 1 μ Pa at 1 m), and hydraulic ram sounds (SPL of 164 dB re 1 μ Pa at 1 m).

A plot of ambient sound measurements (e.g., wind, waves, tidal flows, precipitation, and traffic sound from fishing and commercial shipping vessels) recorded at 11 locations in the harbor indicated a range from 97 to 131 dB re 1 μ Pa RMS (mean = 117 dB re 1 μ Pa). The use of spuds, bottom grabs, and spud walking exceeded the maximum ambient SPL by 45 dB, 48 dB, and 41 dB, respectively. The SPL levels for popping, engine/generator, barge loading, and hydraulic ram sound sources exceeded maximum ambient SPLs by 33 to 36 dB re 1 μ Pa at 1 m.

The source range for the BHD *New York* for all sound sources measured was 164 to 179 dB re 1 μ Pa at 1 m. Similarly, in the only other BHD sound reported in the literature, the *Manu Peeka* had a measured sound source of 163 dB re 1 μ Pa at 1 m (Nedwell et al. 2008). Both reported BHD SPLs were slightly less when compared to source levels reported for CSD (168-

178 dB re 1 μ Pa at 1 m; Greene 1987) and TSHD (190 dB re 1 μ Pa at 1 m) reported by Nedwell et al. (2008).

4.1.3 United States: Reine et al. (2012b)

Reine et al. (2012b) reported the results of underwater sound monitoring during the fracturing of limestone rock in New York/New Jersey Harbor as part of a channel deepening project. The resultant fractured material was removed by a BHD as described in Reine et al. (2012a) and Reine et al. (2014a). The CSD *Florida* (Great Lakes Dredge and Dock) had suction and discharge diameters of 940 mm and 914 mm, respectively, and used a 3,000 hp Esco 54D 3.3 m diameter (diam) cutter rotating at 26 rpm. The total installed power was 25,400 hp, of which 10,000 hp operated the main pump.

Most of the underwater sounds produced by the CSD *Florida* were relatively continuous and at a low frequency—generally less than 1000 Hz—occurring most frequently in the 800 Hz, 1,000 Hz, and 2,500 Hz 1/3-octave bands. The CSD rock-fracturing source level ranged between 170 and 175 dB re 1 μ Pa at 1 m, with sound levels decreasing with increasing distance from the dredge. The farthest distance the authors detected sound was about 800 m. Using a fitted regression (15LogR), the authors back-calculated SPL as loss attributable to practical spreading and 175 dB as a source level, estimating the SPL would diminish to 132 dB at a distance of 800 m from the dredge, approximating the maximum (131 dB) ambient value (see Reine et al. 2012a; previous section).

Figure 15 plots SPL versus distance during monitoring of the dredge *Florida* operations, signifying the variation recorded in SPL at distance and depth. SPL differed by as much as 10 to 15 dB at distances of less than 200 m, but typically this variance decreased to less than 4 dB with increasing distance from the dredge. Overall, the authors observed considerable variability in SPL measured at specific distances, a fact that they attributed to distance from the sound source, orientation related to the dredge, position of the *Florida* swinging laterally, and to the non-continuous sediment removal process.

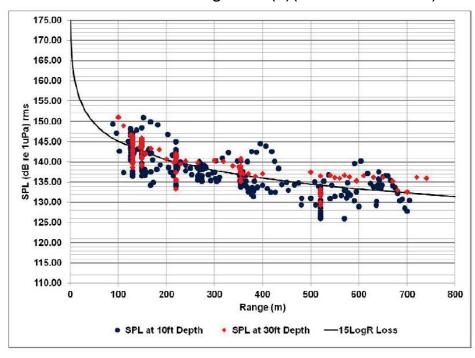
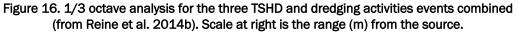


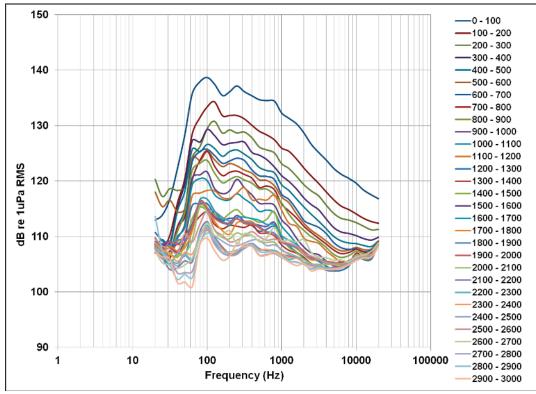
Figure 15. Underwater sound results for 1/3 octave (SPL in dB re 1μ Pa) RMS versus distance from the dredge source (m) (from Reine et al. 2012b).

4.2.8 United States: Reine et al. (2014b)

Underwater sounds were characterized for three TSHD during sand excavation from an offshore borrow area and during transfer of the sediment at the placement site at Wallops Island, Virginia (Reine et al. 2014b). Sound sources related to TSHD operations were excavation, pump-out of material, pump-out of clear water during pipe flushing, transit to the borrow site (hopper empty) and transit to the pump-out stations (hopper loaded). Of the three TSHD monitored, the dredge *Liberty Island* is larger and more powerful than the smaller *Padre Island* and *Dodge Island*. The propulsion power (kW) for the *Liberty Island* was 2.3 times greater than the *Padre Island* and 3.3 times greater than the *Dodge Island*. In transit, the dredge *Liberty* Island transited at 12 knots, the *Dodge Island* at 11 knots, and the *Padre Island* at 10 knots.

Source Levels (dB re 1 μ Pa at 1 m, RMS) back-calculated by the authors using fitted regression (15.788LogR) ranged from 161.3 dB to 176.7 dB re 1 μ Pa at 1 m RMS. The highest SL were produced by the Dredge *Liberty Island*, which had nearly twice the installed power (12,300 kW) than the dredges *Padre Island* and *Dodge Island* (each with installed power of approximately 7,000 kW). Transit produced the highest SL regardless of whether the hopper was empty or full. At 50 m from the source—the closest distance monitored by the authors results from the 1/3-octave analysis for all three dredges and activities combined resulted in an overall SPL of 147.7 dB (Figure 16). Sediment removal produced the most underwater sound (151 dB), followed closely by transition from transit to digging (150 dB). The TSHD activities producing the least sound were transition from pump-out to transit and pump-out of seawater during flushing of dredge pipes. SPLs (1/3-octave) averaged 138 to 139 dB, roughly 12-15 dB less than during sediment removal. On a 1/3 octave basis, the greatest sounds produced by the three TSHD monitored were less than 500 Hz (Figure 16).





The authors also measured ambient underwater sound (absent of dredging activities) at four locations (inshore, offshore, borrow area, and pump-out stations) at two water depths (3 and 6 m) and for wind speeds ranging from Beaufort 1 (1-2 knots) to Beaufort 4 (11-15 knots). Combining measurements across all sampling days, sites, water depths, and weather conditions yielded an ambient SPL of 117 dB re 1 μ Pa and a 1/3 octave SPL of 121 dB. The two activities producing the most underwater sound (sediment removal at 151 dB) and transition from transit to digging

(150 dB) exceeded ambient level by about 29-30 dB. Attenuation to ambient was dependent on the sound source, but at a 2.5 km distance from the dredge, underwater sounds generated by all three dredges for all TSHD activities had reduced to ambient levels.

4.2.9 United States: Reine and Dickerson (2014)

Reine and Dickerson (2014) monitored underwater sounds generated by the CSD *Veracious* (Vortex Marine) during maintenance dredging in the Stockton Deepwater Ship Channel, California. The total power of the *Veracious* operating the main pumps (1,000 hp) was used to pump dredged material through a 16 inch (in.) (0.4 m) pipeline to an upland confined placement facility.

Most of the underwater sounds produced by *Veracious* were of relatively low frequency (< 1,000 Hz). Source level, determined by the authors via curvilinear regression, ranged from 151 dB (upstream, bow) to 157 dB (downstream, astern) re 1 μ Pa at 1 m. An average SL of 153 dB re 1 μ Pa at 1 m was determined for all data combined.

The authors reported data for ambient sound from eight locations in the Port Stockton navigation channel study area in the absence of dredging activities. The authors reported a 50th percentile SPL of the ambient data at 118 dB. This value incorporated generator sound (from moored ships) and port activity sounds, but did not include underwater sound generated from vessels transiting the study area. The average SL of 153 dB re 1 μ Pa at 1 m for all dredging activities was 35 dB greater than the 50th percentile ambient SPL (118 dB).

4.3 Blasting

Overall, blasting is not routinely required in navigational dredge operations. In some cases, however, bottom substrate hardness or geotechnical characteristics inhibit the ability to dredge navigation channels using hydraulic or mechanical methods. In these situations, underwater blasting may be necessary to fragment the substrate prior to dredging. The energy distribution from an underwater explosion is categorized into two phases: pressure (shock) wave (>200 Hz) and bubble pulse (<200 Hz; Baker 2008; Normandeau 2012). In addition to wave propagation in the water column, ground vibrations following blasts are important exposure characteristics. Underwater explosions detonated freely in the water column (e.g., on a rock surface) produce substantially greater shock waves (up to 10 times greater) as compared to explosives used in boreholes, which are designed to minimize propagation of pressure waves in the water column and potentially lessen effects on aquatic biota (Hempen et al. 2007; IADC 2016). Therefore, the ecological risks associated with charges detonated in confined boreholes will be fundamentally different as compared to open-water blasts.

Acoustical characteristics monitored in terms of "peak" SPLs from underwater blasting using confined boreholes in shallow water (i.e., 10 m) were approximately 220 dB re 1 μ Pa at 1 m from source, decreasing to 180 dB re 1 μ Pa at 1,000 m distance from source (Hall 2010). Important components of blasting that influence pressure wave propagation (e.g., SPL, pounds per second inch (psi), etc.) and ground vibrations include the quantity and size of charges, characteristic of rock, borehole placement, water depth, and firing sequence (IADC 2016). Few studies were found monitoring blasting events during dredging activities; these are discussed below. It should be noted that reported metrics related to blasting (e.g., psi, ground particle motion (mm/s)) make comparisons across studies challenging.

Carlson et al. (2011) monitored underwater rock blasting in a 1-mile section of the Columbia River during the 2011 navigation expansion project. For the widening and deepening of the channel, blasting was used in conjunction with dredging to remove approximately 300,000 m³ of basalt rock formations. The study monitored 99 blast events over approximately four months. Charges were confined to boreholes with stemming (i.e., boreholes back-filled with pea gravel). Blast events resulted in very complex underwater sound, which was influenced by the array of blast charges and sequence of blasts. Underwater blast pressures measured in kilopascals, kPa (where k = 1,000), in the immediate vicinity of the blasting zone ranged from 28 kPa to 164 kPa (4 to 24 psi). During the blasting events, detailed surveys of fish were conducted to evaluate potential adverse effects (discussed in more detail in Section 5.2).

Hempen et al. (2007) recorded underwater blast pressures during a Miami Harbor Channel Deepening project. Blast charges were confined in boreholes with stemming (i.e., boreholes back-filled with aggregate material). Maximum pressure following blasting was approximately 30 psi. Maximum recorded pressures generally did not clearly correlate with charge weight. This was likely the case due to the other factors influencing the pressure wave (e.g., firing sequence, borehole depth and confinement, etc.). The range of pressures recorded (from confined holes) ranged from 10 to 90 psi. Overall, this study was one of the first to confirm in the field that detonations in open water produce higher amplitudes and more rapidly oscillating shock waves as compared to rock removal (borehole) blasts.

Tripathy and Shirke (2015) monitored 36 blast events during drilling and blasting of rock associated with the dredging and deepening of a port in Mumbai, India. Underwater drilling, blasting, and dredging was used to remove approximately 25,000 m³ of basalt rock. Due to the proximity of the blasting to historical and culturally significant structures near the port, ground vibrations following blasts were monitored. "Safe" levels of ground particle motion were based on existing recommendations for historical structures. During the 36 blast events, ground vibrations were <0.25 mm/s, below the threshold of vibrations levels (>1 mm/s) estimated to be protective of structural damage. The Tripathy and Shirke (2015) study confirmed that use of boreholes and delayed detonations substantially reduced the effects of underwater shock waves and shock wave propagation as compared to open-water blasting.

4.4 Summary

Underwater sound produced by hydraulic and mechanical dredge operations in the U.S. and Europe has been studied for several decades (Table 5; Figure 17). Acoustical characteristics related to the dredge activity can be categorized as excavation, transiting, and placement. Primary sources of sound from dredging are commonly machinery, propulsion, and excavation of substrate (e.g., aggregate). Cavitation sounds from propellers and pumps were the primary source of the highest continuous SPLs reported. Dredging activities producing the lowest SPLs generally included sand depositing, depositing in a scow or hopper, and bucket closing on the channel bottom. Overall, source level SPLs associated with dredging operations commonly range from approximately ~100 to 190 dB (RMS) re 1 µPA at 1 m. In general, SPLs from dredging activities are similar to levels reported for underwater sound associated with commercial shipping (Figure 17). It should be noted that the acoustical characteristics are often summarized as single maximum recorded values near the dredge (i.e., 1 m from source). Additionally, a single sound event (e.g., propeller cavitation) can skew the calculated SPLs (RMS) and may not provide an accurate representation of the dredging operation.

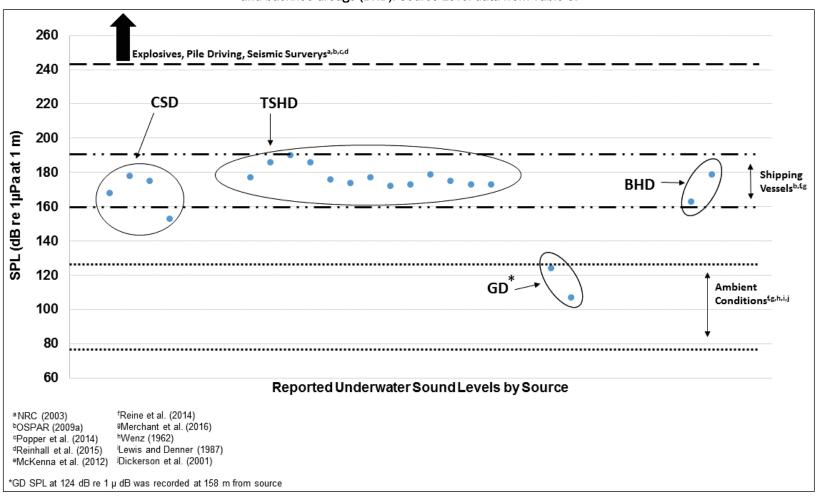


Figure 17. Summary of underwater SPLs by dredging type: cutter suction dredge (CSD); trailing suction hopper dredge (TSHD); grab dredge (GD); and backhoe dredge (BHD). Source Level data from Table 5.

Dred for Dred for size Sound pressure Deck enestral level (dD 4/2 Octave receive								
Dredger type	Reference	Ship name	Installed power (kW)	Dredger size indicator	Sound pressure level	Peak spectral level (dB re 1 µPa/Hz)	1/3 Octave receive levels (dB re 1 μPa)	
CSD	Greene 1987ª	Beaver Mackenzie	1,100- 1,300	Transfer rate: 100,000 m³/day	168 dB re 1 µPA-m in 1/3 Octave at 80 Hz ^a	122 dB (120 Hz, 190 m)	128 dB (80 Hz, 200 m)	
CSD	Greene 1987ª	Aquarius	12,889	Transfer rate: 100,000 m³/day	178 dB re 1 μPA-m in 1/3 Octave at 125 Hz ^a	122 dB (200 Hz, 200 m)	134 dB (160 Hz, 125 Hz)	
CSD	Clarke et al. 2002	James B*	6,300	10,000 hp with a 24" discharge pipe	-	112 dB (105 Hz, < 500 m)	-	
CSD	Reine et al. 2012 ^b	Florida*	25,400	10,000 hp with a 130" cutter	175 dB re 1 µPa-m	-	-	
CSD	Reine and Dickerson 2014	Veracious*	1,000	-	153 dB re 1 µPa-m	-	-	
TSHD	Greene 1987ª	Cornelis Zanen	12,064	Capacity 8,000 m ³	142 dB (at 930 m)	125 dB (175 Hz, 930 m)	-	
TSHD	Greene 1987ª	Geophotes X (Inai Selasih)	15,384	Capacity 8,000 m ³	139 dB (at 430 m)	125 dB (100 Hz, 430 m)	147 dB (80 Hz, 500 m)	
TSHD	Greene 1987ª	W.D. Gateway	13,870	Capacity 12,000 m ³	131 dB (at 1.5 km)	131 dB (350 Hz, 1.5 kM)	-	
TSHD	Clarke et al. 2002	Stuyvesant*	15,000	Capacity 9,314 m ³	-	142 dB (105 Hz, >40 m)	-	
TSHD	Defra 2003	Acro Adur	1,100	Capacity 2,890 m ³	-	122 dB (320 Hz, 50 m)	-	
TSHD	Gerstein et al. 2006	Columbia	2,800	-	177 dB re 1 µPa-m	-	-	
TSHD	Parvin et al. 2008°	The City of Westminster	2 x 1,950	Capacity 2,700 m ³	186 dB re 1 µPa-m	125 dB(80 Hz, 251 m)	126 dB (31.5 Hz & 100 Hz, 514 m)	
TSHD	Nedwell et al. 2008 ^d	-	-	-	190 dB re 1 µPa-m	-	-	
TSHD	de Jong et al. 2010 ^{e,f}	Dredger #1	8,000- 30,000	Capacity 3,000- 20,000 m ³	186 dB re 1 µPa-m in 1/3 Octave at 45 Hz	-	-	
TSHD	de Jong et al. 2010 ^e	Dredger #2	8,000- 30,000	Capacity 3,000- 20,000 m ³	176 dB re 1 μPa-m in 1/3 Octave at 500 Hz	-	-	

Table 5. Summary of underwater sound measurements by dredging type.

Dredger type	Reference	Ship name	Installed power (kW)	Dredger size indicator	Sound pressure level	Peak spectral level (dB re 1 µPa/Hz)	1/3 Octave receive levels (dB re 1 µPa)
TSHD	de Jong et al. 2010 ^e	Dredger #3	8,000- 30,000	Capacity 3,000- 20,000 m ³	174 dB re 1 µPa-m in 1/3 Octave at 350 Hz	-	-
TSHD	de Jong et al. 2010 ^e	Dredger #4	8,000- 30,000	Capacity 3,000- 20,000 m ³	177 dB re 1 µPa-m in 1/3 Octave at 300 Hz	-	-
TSHD	de Jong et al. 2010 ^e	Dredger #6	8,000- 30,000	Capacity 3,000- 20,000 m ³	172 dB re 1 µPa-m in 1/3 Octave at 63 Hz	-	-
TSHD	de Jong et al. 2010 ^e	Dredger #7	8,000- 30,000	Capacity 3,000- 20,000 m ³	173 dB re 1 μPa-m in 1/3 Octave at 45 Hz	-	-
TSHD	Robinson et al. 2011	Sand Harrier	3,824	Capacity 2,700 m ³	-	-	181 (159 Hz, 137 m)
TSHD	Robinson et al. 2011	Sand Falcon	2 x 2,460	Capacity 4,832 m ³	-	-	180 (80 Hz, 251 m)
TSHD	Robinson et al. 2011	Arco Axe	2,940	Capacity 2,890 m ³	-	-	166 (398 Hz, 240 m)
TSHD	Robinson et al. 2011	City of Chichester	2,720	Capacity 1,418 m ³	-	-	173 (251 Hz, 137 m)
TSHD	Robinson et al. 2011	City of London	4,080	Capacity 2,652 m ³	-	-	174 (5,012 Hz, 458 m)
TSHD	Robinson et al. 2011	City of Westminster	4,080	Capacity 2,999 m ³	-	-	178 (1,000 Hz, 474 m)
TSHD	Reine et al. 2014 ^g	Liberty Island*	12,353	Capacity 5,003 m ³	179 dB re 1 µPa-m	-	-
TSHD	Reine et al. 2014 ^g	Dodge Island*	6,972	Capacity 2,754 m ³	175 dB re 1 µPa-m	-	
TSHD	Reine et al. 2014 ^g	Padre Island*	7,006	Capacity 2,754 m ³	173 dB re 1 µPa-m	-	-
TSHD	Reine et al. 2014 ^{g,i}	Atchafalaya*	2,209	Capacity 2,300 m ³	173 dB re 1 μPa-m	-	
GD	Dickerson et al. 2001 and Clarke et al. 2002	Viking*	1,500	10 m ³ bucket	-	124 dB re 1 µPa (162.8 Hz, 158 m)	-

Dredger type	Reference	Ship name	Installed power (kW)	Dredger size indicator	Sound pressure level	Peak spectral level (dB re 1 µPa/Hz)	1/3 Octave receive levels (dB re 1 µPa)
GD	Dickerson et al. 2001	Crystal Gayle*	-	-	-	107 dB re 1 µРа-m at 91.5 Hz	-
BHD	Nedwell et al. 2008	Manu Peeka	1,515	14m³ bucket	163 dB re 1 µPa-m ^e	-	-
BHD	Reine et al. 2012 ^{b,c}	New York*	3,434	18 m³ bucket	179 dB re 1 µPa-m	-	-

Dashes indicate data not reported; Asterisks by ship name indicate USACE sponsored study

^aAcoustic data presented in the original Greene (1987) publication were presented as received levels and spectra and were reprocessed to source levels and 1/3 octave spectra in Richardson et al. (1995)

 $^{\mathrm{b}}$ Reine et al. (2012a,b; 2014) used a 15.778 log (R/ 1 m) to back-calculate source levels

^cReported in Reine et al. (2014)

^aNedwell et al. (2008) estimated TSHD source level based on spherical spreading (10 log (R/1 m)) based on measures 200 m from source.

ede Jong et al. (2010). SPLs sourced from figure 5.8 (p 38); units express as dB re 1 μPa²m² are the same as "dB re 1 μPa at 1 m"

fde Jong et al. (2010) reports that the highest dB measured (186 dB) occurring at low frequency was likely due to propeller cavitation.

^gReine et al. (2014) data sourced from Table 23 (p. 75) of technical report. SL based on a 15.778LogR obtained from fitted regression.

^hNedwell et al. (2008) used scaling factor of 10 log (R/1 m) to back-calculate source level.

ⁱReine et al. (2014) references the TSHD (Atchafalya) reported as an average of SPLs measured.

Dredging-induced underwater sounds are temporally and spatially dynamic, and dependent on site-specific activities and conditions. In general, dredge-related sounds are mostly continuous and non-impulsive sounds. The duration of underwater sounds depends on the type of dredge operation. Hydraulic dredges generate continuous sounds as the cutterhead rotates on the channel bottom or when the draghead contacts the sediment. There are also continuous sounds from vessel propulsion (engine and propeller). Mechanical dredge work occurs in regular intervals (discontinuous) and is repeated (cyclic) often. Sounds originate from winches and derrick movements, machinery and propulsion, and digging.

The type of material dredged (e.g., rock, gravel, sand, mud) affects the frequency of underwater sounds. Dredging sounds are predominantly lower frequency, with reported peak spectral levels below 500 Hz (Table 5). Underwater sounds produced by dredges and the radiated distance are dependent on several factors, including substrate type, geomorphology of the waterway, site-specific hydrodynamic conditions, equipment maintenance, and dredge operator skill. It is anticipated that within dredge types, larger dredges have higher SPLs as compared to smaller dredges. However, based on the currently available dredge sound data (Table 5), there were no apparent relationships associated with installed power and underwater SPLs within dredge types.

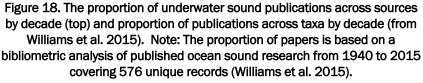
5 Review of Underwater Sound Effects

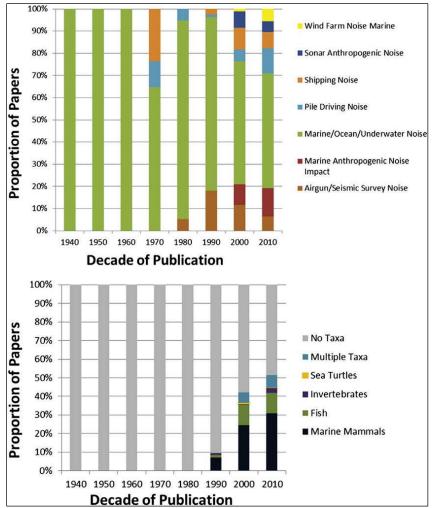
Sound is an important sensory function for many marine organisms (Hawkins 2008; OSPAR 2009b). Marine mammals, fish, and invertebrates have special mechanisms for emitting and detecting underwater sound (Popper 2003; OSPAR 2009b). Underwater sound is biologically important for communication, orientation, predator avoidance, and foraging (OSPAR 2009b). It is recognized that sound emanating from anthropogenic sources may have a diverse range of physiological and behavioral effects on marine biota (Southall et al. 2007; Popper et al. 2014), and there is a growing international focus to better understand these interactions (Popper and Hastings 2009). Only recently (past few decades) has the field of study developed investigating the potential effects associating underwater sound from industrial activities to various marine taxa (Figure 18; Williams et al. 2015).

Aquatic Noise Trust (organized by Arthur et al.) has held four conferences on anthropogenic underwater sound research since 2007. The most recent of these was the 4th International Conference on the Effects of Noise on Aquatic Life held in Dublin, July 2016. Papers presented at previous conferences were published as extended abstracts in a variety of forums, including as a Special Issue in the journal *Bioacoustics* (Hawkins 2008; Volume 17, Nos. 103); a book titled *The Effects of Noise on Aquatic Life* (published in a special issue of *Advances in Experimental Medicine and Biology* 730, DOI 10.1007/978-1-4419-7311-5_5 (2012)); and a third book titled *The Effects of Noise on Aquatic Life II* (Popper and Hawkins 2016).

In addition, a publically available library database for research related to underwater sound is supported by E&P Sound and Marine Life Program under the direction of the International Association of Oil and Gas Producers (IOGP). The online database provides access to project reports, peer-reviewed publications, factsheets, and content from IOGP-funded research and can be found at <u>http://www.soundandmarinelife.org</u>.

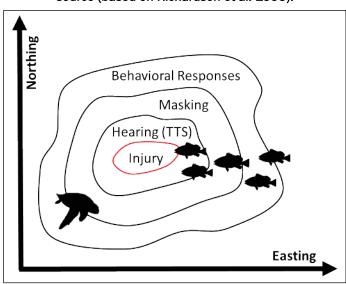
This section discusses effects on marine biota from natural and anthropogenic sound sources in the aquatic environment. This review is meant to be strategic, focusing on literature that will provide insight to potential risks associated with underwater sound emanating from dredging operations. The goal of this literature review was to include underwater sounds from natural and anthropogenic sources that span from lower intensity (non-impulsive) to higher intensity (impulsive) sounds. This "span" of sound exposures was used to provide context for source levels (SPLs) and frequencies emanating from dredging operations (typically lower intensity non-impulsive sounds). Additionally, the intent was to include literature that reported biological responses to sound that spans from sub-lethal to lethal responses, in efforts to provide context for potential risks associated with the acoustical characteristics of dredging. It should be noted that there should be caution when directly comparing across studies, due to the lack of standardized underwater sound measurement techniques and methods for measuring biological responses (Thomsen et al. 2016; Erbe et al. 2016).

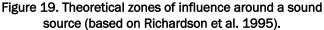




5.1 Effects overview

A key principle to understanding and predicting adverse effects from underwater sound is to develop exposure-response relationships of underwater sound for environmentally relevant organisms (Boyd et al. 2008; Thomsen et al. 2016). Reported effects to marine biota following exposures to anthropogenic sounds (e.g., pile driving, sonar, and shipping) range from lethal to sub-lethal (behavioral effects). The spectrum of species responses to underwater sound is generally described by direct injury, effects on hearing, masking, and behavioral responses (Figure 19).





Based on the characteristics of underwater sound associated with various dredging operations, there is general consensus that there is not a significant risk of mortality or permanent injury to marine biota when dredging bottom substrates (Todd et al. 2015). The effects of underwater sound emanating from dredging operations are anticipated to have masking effects or alter behavioral responses (Hawkins et al. 2015). Dredging operations and other anthropogenic sounds (e.g., shipping vessels) can produce lower-frequency sounds (20 to 1,000 Hz) that overlap the detectable frequency range of marine organisms. A notable exception is during blasting activities when rock and other hard substrata need to be removed in ship channels to ensure navigation safety. These higher intensity sounds have a rapid rise time and can cause direct injury and auditory effects due to the high level of sound pressure (e.g., 270-280

dB zero to peak) and propagation of shock waves (Richardson et al. 1995; OSPAR 2009a).

Common types of species responses to underwater sound and response metrics are briefly described below.

5.1.1 Death and injury

Direct injury and tissue trauma are typically limited to high amplitude impulsive sounds generated from explosions, impact pile driving, and seismic airguns (OSPAR 2009a). For example, explosions have the highest peak levels of anthropogenic sounds with a rapid rise-time. Explosions also produce shock waves, which propagate differently than acoustical waves (Richardson et al. 1995). Shock waves can cause direct mechanical damage due to the force of impact. In general, gas-containing organs (e.g., swim bladders, gastrointestinal tract, and lungs) are especially susceptible to damage. Boundary layers of tissues, where tissues of different densities intersect, are also susceptible to damage from impulsive sounds (Richardson et al. 1995). The auditory system is particularly susceptible to rapid pressure fluxes due to its adaptation to respond to pressure changes. Also, rapid changes in pressure can cause barotrauma in fishes (Popper et al. 2014). Barotrauma is damage to tissues or organs from blood gasses that come out of solution, or gas volumes expanding and contracting rapidly in tissues (e.g., swim bladders) causing damage or rupture (Popper et al. 2014).

5.1.2 Effects on hearing

Sound effects on hearing can be permanent or temporary, affecting the auditory structure (e.g., hair cells of the inner ear), nerve fibers, or other tissue structures in the auditory pathway of exposed fish and marine mammals. Permanent threshold shifts (PTS) occur when there is a permanent loss of the hearing sensory function (OSPAR 2009a). Additionally, short-term reduction in hearing known as temporary threshold shifts (TTS) are commonly used as a metric for determining auditory impairment (Erbe 2011). The degree of PTS and TTS is a function of the auditory exposure (e.g., pressure level, duration, rise time; Erbe 2011).

In general, onset of TTS follows a predictive exposure-response relationship (Weilgart 2007; Finneran 2008). The following are general observations of TTS reported by Finneran (2008):

- Degree of TTS will generally increase with exposure SPL and duration.
- Short durations of sounds require greater SPLs to induce the same level of TTS compared to sounds of longer duration.
- SPLs or duration of exposure **alone** are poor predictors of TTS.
- Recovery is an important consideration for TTS.
- It appears that recovery period occurs faster for larger auditory threshold shifts, and slower for smaller shifts.

The majority of mammal and fish auditory threshold shifts are measured based on behavioral studies (training mammals to respond to "audible" tones) or electrophisologically derived data using auditory-evoked potentials (AEP) measures. Discrepancies between behavioral and AEP auditory methods have been identified, with AEP-derived TTS observed at 20-40 dB higher than behaviorally derived TTS (Finneran 2008; NMFS 2016).

Both fish and marine mammals can recover from TTS, with recovery times to "baseline" occurring on the order of minutes to days (Popper et al. 2005; Lucke et al. 2009; Kastelein et al. 2008, 2012, 2017a). Although PTS and TTS are useful metrics to determine auditory injury, there is uncertainty as to the environmental relevance of measurable auditory shifts to overall animal fitness and survival (Tougaard et al. 2016).

5.1.3 Masking

Masking is an animal's diminished ability to detect relevant sounds against background due to increased ambient sound (Southall et al. 2007). This may affect the organism's ability to orient, navigate, and select habitat. Masking may be particularly important for soniferous fish (soundproducing fish; e.g., cods, croakers, groupers) that produce sounds associated with spawning behavior, aggregating behavior, and orientation (Hawkins et al. 2015). In marine mammals, masking can affect communication networks between individuals of a social group or between groups (Janik 2005; Clark et al. 2009). Masking is "biologically significant" when there is a measureable decrease in animal fitness (e.g., growth, reproduction; Carr and Erbe 2008). It should be noted that organisms can compensate for background sounds using a number of different mechanisms. These compensation mechanisms can be as simple as timing vocalizations to minimize overlap or waiting for the interfering sound to subside (Clark et al. 2009). An organism may also increase the level of vocalization above the interfering noise, which is known as the "Lombard Effect." The Lombard Effect is an automatic and involuntary change in the vocalization intensity in the presence of background sound needed to maintain a constant signal-tonoise ratio. This effect has been confirmed with marine mammals and fish (Scheifele et al. 2005; Holt and Johnston 2014; Neenan et al. 2016). It should be noted that although masking is often referenced as an important effects endpoint in regard to underwater sound, there are significant information gaps on the masking effects of anthropogenic sounds to marine organisms (Hawkins et al. 2015; Hawkins and Popper 2016).

5.1.4 Behavioral effects

Recent studies investigating behavioral effects from underwater sound have primarily focused on startle responses and avoidance (Everley et al. 2016; Hawkins and Popper 2016). Behavioral responses to sound could be significant to an individual animal when it interferes with normal behavior or activity, or affects growth, survival, or reproduction (NRC, 2005). It is critical to link behavioral responses to "vital" population level responses (e.g., survival, reproduction, growth) to understand and predict population changes (Boyd et al. 2008).

5.1.5 Population-level effects on fitness and survival

Population-level effects to marine biota following anthropogenic sounds have not been well studied (Popper et al. 2014). Predictive models for marine mammals have been developed; however, these models have not been validated (NRC 2005). A severe limitation for modeling efforts are the lack of robust sound exposure-response data. For marine mammals, Population Consequences of Acoustic Disturbance (PCAD) model (NRC 2005) was developed to estimate changes in population growth rates and ecosystem dynamics, through the effects of acoustic disturbance on individual fitness and fecundity (CEFAS 2015). To date, the use of this model has been limited due to the lack of empirical data to derive model parameters (CEFAS 2015; Hawkins and Popper 2017).

5.2 Effects on fish

In general, fish have a lower sound frequency detection range as compared to marine mammals. Fish can detect frequency ranges between 30 to 1,000 Hz (Erbe 2011), and some fish can even detect infrasound (< 20 Hz; e.g., Clupeid spp.) and ultrasound (> 20,000 Hz; e.g., Atlantic herring; Normandeau Associates 2012). More commonly, the 100 to 400 Hz frequencies are detected by a majority of fish studied (Offutt 1974; Yan 2001; Codarin et al., 2009; Parmentier et al. 2011). In general, this means that high-frequency (>10,000 Hz) sounds (e.g., sonar) are not expected to overlap with hearing frequencies of most fish species (Slabbekoorn 2016). Fish appear to be particularly well adapted to detecting lower frequency sounds (<1,000 Hz), like those emanating from shipping or dredging operations. To date, less than 100 fish species have audiograms of hearing thresholds that overlap with shipping vessel frequencies (Neenan et al. 2016). Although only a small percentage (<1%) of the total fish species (>30,000) have been part of bioacoustics investigations (Erbe 2011), these studies are improving our understanding of the potential risk to fish exposed to underwater sound.

SPLs are an important metric when considering the interaction with airfilled cavities (i.e., swim bladders) (Slabbekoorn 2016). However, fish are also sensitive to the particle motion of sound detected by auditory hair cells (OSPAR 2009a). A topic of future study that was identified at a World Organization of Dredging Association (WODA) workshop hosted in 2015 "Workshop on Underwater Sounds" included using particle motion as a metric for addressing underwater sound exposure to fish, as compared to the more commonly expressed sound pressure (dB) descriptions. In comparison to hydrophones, the use of underwater particle motion detectors is a relatively new method because only recently has the technology become commercially available (Nedelec et al. 2016). Therefore, particle motion data are not commonly reported as acoustic measures describing anthropogenic sounds, but they are likely to become an important component for evaluating effects on fish (Hawkins and Popper 2017).

5.2.1 Direct injury

Sound sources causing direct injury or mortality to fish are generally limited to high-intensity impulsive sounds. Explosions and pile driving sound effects on fishes have resulted in barotrauma and include immediate lethality, rupturing of swim bladders, hemorrhaging of various organs and tissue, and swim bladder deflation (Popper et al. 2014; Casper et al. 2016). In general, smaller body size and presence of swim bladders make fish more susceptible to impulsive sounds like blasting or pile driving (Yelverton et al. 1975; Richardson et al. 1995; Popper et al. 2014). To date, direct mortality has not been documented or observed to occur in association with dredging sounds, with the exception of underwater blasting of rock formations in navigation channels (Carlson et al. 2011).

Carlson et al. (2011) monitored underwater rock blasting in a 1-mile section of the Columbia River during a widening and deepening project. Blasting was conducted over a 4-month time period, with a total of nine blasting events monitored. Underwater blast pressure ranged from 28 kPa to 164 kPa (4 to 24 psi). During blasting events, native fish species in the affected area of the reach were monitored. Additionally, caged juvenile salmonids were placed near the blasts to provide additional data for estimating mortality. Based on the field observations and mortality estimations, there was no observed or predicted mortality for adult salmon or Eulachon species of fish. Over the four-month monitoring period, the total "take" was three dead sturgeon recovered following the 99 blasting events.

In field experiments, Govoni et al. (2008) measured the responses of juvenile and adult spot (*Leiostomus xanthurus*) and pinfish (*Lagodon rhomboides*) to underwater explosions. Following explosions, spot were more sensitive to shockwaves as compared to pinfish. Differences in fish responses were attributed to anatomical differences of the swim bladder. Results indicated that the recently transformed juveniles were the most sensitive to shock waves. For larval and early juvenile fish, 50% mortality occurred at impulse pressures ranging from 5.3 to 8.9 Pa-s for pinfish and spot, respectively (Govoni et al. 2008).

Casper et al. (2016) empirically derived injury thresholds (barotrauma and onset of TTS) to impulsive sounds through laboratory experiments. Six species were used in the experiments, including juvenile Chinook salmon (*Oncorhynchus tshawytscha*), lake sturgeon (*Acipenser fluvecens*), Nile tilapia (*Oreochromis niloticus*; Cichlidae), Mozambique tilapia (*Oreochromis mossambicus*; Cichlidae), hogchoker (*Trinectes maculates*; Achiridae), and hybrid striped bass (white bass *Morone chryspos* x striped bass *Morone saxatilis*; Moronidae). The results indicated that fish with swim bladders (e.g., salmon) had onset of injury at SEL_{cum} of 210 dB re 1 μ Pa²s. Major conclusions from this study included that barotrauma effects were not observed in species without swim bladders (e.g., hogchokers), onset of damage to auditory damage were substantially higher than barotrauma injuries, and barotrauma effects did not occur until the SEL_{cum} were substantially above interim regulations (Casper et al. 2016).

5.2.2 Effects on hearing

Fish auditory sensitivities to underwater sound can be categorized into hearing generalists and hearing specialists. Hearing generalists have a narrow frequency bandwidth of auditory detection and have lower sensitivities to SPLs (e.g., Gadidae (cod); Salmonidae (salmon); Chapman and Hawkins 1973; Hawkins and Johnstone 1978; OSPAR 2009a; Popper and Hastings 2009). In contrast, hearing specialists have anatomical structures (e.g., connections between inner ear structures and swim bladders) that increase the hearing frequency thresholds as compared to generalists. Examples of hearing specialists include Otophysi (e.g., catfish), Clupeiformes (e.g., herrings and sardines), Sciaenids (e.g., drums and croakers), and Holocentrids (e.g., squirrelfishes) (Popper and Hastings 2009).

Fish can regenerate lost or damaged sensory cells of the ear (Smith 2016); therefore, permanent hearing loss or permanent threshold shifts (PTS) are unlikely to occur. In contrast, the adverse effect endpoint of concern in fish is the temporary loss of hearing, referred to as a temporary threshold shifts (TTS). One method for experimentally testing temporary hearing loss in fish following sound exposure is directly measuring the density of hair cells in the inner ear and estimating and performing hearing tests by recording auditory-evoked potentials (AEPs). AEP methods use electrodes non-invasively attached to the head, where electrophysiological responses to sounds are measured. Measuring AEPs takes a considerable amount of time and specialized equipment, and therefore is relatively challenging to perform (Smith 2016). Fish TTS have been measured from non-impulsive sounds (dredging, shipping, and simulated playback sounds ("white noise") and impulsive sounds (e.g., pile driving, and seismic airguns). Auditory effects to fish exposed to anthropogenic underwater sounds are discussed below by sound source.

5.2.2.1 Dredging

No studies were found where underwater sound effects of dredging were directly measured for fish. However, several studies have made comparisons from measured dredging or shipping sounds to Fisheries Hydroacoustics Working Group (FHWG) exposure criteria or literaturederived effect levels in efforts to estimate potential injury risk.

Heinis et al. (2013) measured underwater sound of shipping and dredging activities (TSHD) during the expansion of the Port of Rotterdam in the Netherlands. Although behavioral effects of fish were not measured, Heninis et al. (2013) compared the measured underwater acoustics of dredging sounds to fish TTS criteria developed by FHWG (Oestman et al. 2009; Table 6) for pile-driving noises. Following dredging operations, 24 hr SEL_{cum} of 182 and 186 dB re 1 μ Pa²s were estimated for regular shipping activity and regular shipping with dredging, respectively. Heinis et al. (2013) estimated that dredging operations from TSHDs in the port of Rotterdam expansion project exposed smaller fish (< 2 gram) to sound levels slightly exceeding the fish TTS criteria of 183 dB re 1 μ Pa²s. However, the authors estimated that larger fish (> 2 g) were not at risk for auditory injury following exposures from shipping and dredging sounds.

Nedwell et al. (2008) measured BHD and TSHD sound in Southhampton, UK, waters and calculated sound exposures above "hearing thresholds" (denoted dB_{ht}) for Atlantic salmon (*Salmo salar*). Underwater sound above 50 dB_{ht} were used as behavioral disturbance thresholds for salmon. Measurements during operations indicated that the highest sound levels were when the excavator was in contact with the seafloor. BHD sound levels were above 50 dB_{ht} in the immediate (< 15 m) vicinity of the operation, but declined below "behavioral" thresholds at distances greater than 15 m. For TSHD noises, it was estimated that sound levels greater than 50 dBht were limited to a distance within 50 m from the source.

In the UK, underwater sound generated by a TSHD *Acro Adur* was monitored to estimate the potential dredging-related sounds to fish (Department for Environment, Food and Rural Affairs (DEFRA) 2003). Underwater sound was measured when the draghead was in contact with the seafloor and the seawater and fine dredged material was overflowing from the screening spillways. Underwater sound levels at 50 m from the dredge (hopper capacity of 2,980 m³) were 117 dB (at 200 Hz) and 122 dB at 320 Hz. The authors estimated the potential dredging-related sound effects to fish based on comparisons of measured underwater sounds to literature derived auditory threshold effects. Based on these comparisons, it was concluded that fish (Clupeidae (e.g., herring, shads, sardines) and flat fish (e.g., plaice and dab)) were not at risk to suffer auditory injury.

5.2.2.2 Shipping

Liu et al. (2013) conducted laboratory experiments to measure effects of playback sounds from a 2,000-horsepower (hp) containership on the onset of TTS of Chinese suckers (*Myxocyprinus asiaticus*). The maximum instantaneous SPL measured from the containership at a distance of 25 m was 142.8 dB re 1 μ Pa. TTS was estimated using AEP methods, with durations of exposure of 1, 2, 4, 8, and 24 hours. After 24 hours of sound playback exposures, measurable auditory threshold shifts (TTS) were measured at all frequencies tested (100 – 3,000 Hz). Following the sound exposures, fish hearing recovered to baseline within 96 hours.

5.2.2.3 Broadband "white noise"

Smith et al. (2006) investigated the regenerative capabilities of the inner ear of fish following exposures to sound. The study measured the relationship between hair cell damage and physiological changes in auditory responses following noise exposures. Smith et al. (2006) exposed goldfish (Carassius auratus; hearing specialist) to "white noise" at 170 dB re 1 µPa RMS for 48 hours in a bandwidth ranging from 0.1 kHz to 10 kHz in laboratory experiments. Following exposures, fish had a mean temporary threshold shift (TTS) of 16 dB averaged across all frequencies, in addition to statistically significant hair cell loss as compared to untreated control. Following sound exposures, fish were allowed to recover for one week. During the recovery period, both hair cell regrowth and TTS were observed to recover to baseline. Hair cells regenerated at a linear rate following noise exposures. Hair cell loss was 85% immediately following sound exposures. After seven days of recovery, hair cell loss decreased to ~47%. With hair cell regeneration, functional hearing also increased (i.e., TTS decreased). TTS decreased from 16 dB (immediately following exposures) to 4 dB at 7 days' exposure (Smith et al. 2006; Smith 2016). This study demonstrated the onset of inner ear damage to noise exposures and the regenerative responses of the hair cells and functional hearing during the recovery period.

Amoser and Ladich (2003) measured auditory shifts of two hearing specialist (goldfish (*Carassius auratus*) and catfish (*Pimelodus pictus*)) exposed to broadband "white-noise" measurements in laboratory experiments. To discern potential effects of sound duration to the onset of hearing loss, the study was conducted using 12- and 24-hour exposure durations. Hearing effects were determined using auditory brainstem responses (ABR), and recovery was measured after 3, 7, and 14 days. Following exposures to broadband white noise at SPLs of 158 dB re 1 μ Pa, a significant loss of hearing was observed for both species with a loss of up to 26 dB in goldfish and 32 dB in catfish. The duration of sound exposure had no apparent effect on extent of hearing loss, with no differences in hearing sensitivities following 12- and 24-hour exposures, with recovery occurring within 3 days for goldfish and 14 days for catfish (Amoser and Ladich 2003).

Using these data (i.e., Amoser and Ladich 2003 and Smith et al. 2006), Popper et al. (2014) proposed fish sound exposure criteria for shipping and continuous sounds (Table 6).

Response	Type of Fish	Exposure Level		
Recoverable injury	Swim bladder involved in hearing (primarily pressure detection)	170 dB re 1 μPa RMS for 48 h ^a		
TTS	Swim bladder involved in hearing (primarily pressure detection)	158 dB re 1 μPa RMS for 12 h ^b		

Table 6. Shipping and continuous sounds exposure guidelines for fish (reported in Popper etal. 2014).

^aDerived from Smith et al. (2006) regarding exposures of goldfish (*Carassius auratus*) to broadband "white noise"

^bDerived from Amoser and Ladich (2003) for TTS onset for goldfish (*Carassius auratus*) and catfish (*Pimelodus pictus*) exposed to broadband "white noise"

5.2.2.4 Seismic Airgun Exposures

Popper et al. (2005) examined the onset of TTS in fish species following sound exposures from a seismic airgun array. The study was conducted in the Mackenzie River Delta, where fish were held in cages and exposed to five or 20 seismic airgun shots. TTS shifts were quantified using auditory brainstem responses (ABRs) for three fish (northern pike (*Esox lucius*); broad whitefish (*Coregonus nasus*); and lake chub (*Couesius plumbeus*)). The study was designed to mimic a single pass of an airgun array used for river seismic surveys. Sound exposures had an average SEL of 177 dB re 1 μ Pa²s, for durations of 40 s. The greatest TTS were observed at 20 dB (at 400 Hz) and 35 dB (at 400 Hz) in northern pike and lake chub, respectively. No apparent hearing effects were observed for broad whitefish following airgun exposures. Hearing loss recovery occurred within 18 and 24 hours for the lake chub and northern pike, respectively. Based on the conservative nature of the experimental design, the authors concluded that the fish species evaluated were not likely to be adversely impacted by a seismic airgun survey.

Popper et al. (2014) estimated seismic airgun acoustic criteria for fish based on effects data derived from Halvorson et al. (2011; 2012a, b) and Popper et al. (2005) (Table 7).

Table 7. Seismic airgun exposure guidelines for fish (reported in Popper et al. 2014). Mortality and recoverable injury data based on Halvorson et al. (2011, 2012a, b); TTS impairment based on Popper et al. (2005).

Response	Type of Fish	Exposure Level		
	No swim bladder (particle motion detection)	>216 dB SEL _{cum} or >213 dB peak		
Recoverable Injury	Swim bladder not involved in hearing (particle motion detection)	>203 dB SEL _{cum} or >207 dB peak		
	Swim bladder involved in hearing (primarily pressure detection)	$>203 \text{ dB SEL}_{\text{cum}} \text{ or } >207 \text{ dB peak}$		
	No swim bladder (particle motion detection)	>>186 dB SEL _{cum}		
TTS	Swim bladder not involved in hearing (particle motion detection)	>>186 dB SELcum		
	Swim bladder involved in hearing (primarily pressure detection)	186 dB SELcum		

Notes: peak and RMS sound pressure level dB re 1 µPa; SEL dB re 1 mPa²s

5.2.2.5 Pile driving

Auditory effects criteria for fish have been developed for estimating onset of injury from impulsive (pile-driving) sounds. Carlson et al. (2007) provided sound exposure criteria for fish during pile-driving activities on a sliding scale corresponding to fish mass (between 0.5 and 200 g; for nonauditory tissue damage; Table 8). Effects criteria were based on nonauditory tissue damage, auditory tissue damage, and TTS. Due to the nature of pile-driving sounds, the criteria was broken down by peak SEL and cumulative SEL. Cumulative SELs are calculated based on Hastings and Popper (2005; Equation 3)

Response	Hearing Type	Peak SEL	SELcum	Application Notes					
Auditory tissue damage (hair cells)	generalist	>206	>213	Accumulation of SEL should not be reinitiated if SELcum is >213 dB					
	generalist	>206	>189	After an 18-hour non-					
	specialist	>205	>185	exposure period, reset accumulation of SELs					
TTS	generalist		185	After an 18-hour non-					
	specialist	205	183	exposure period, reset accumulation of SELs					

Table 8. Carlson et al. (2007) recommended interim sound exposure criteria for fish.

SEL_{cum} = 10 log (#pile strikes) + single strike SEL

The Fisheries Hydroacoustic Working Group (FHWG) revisited the criteria and simplified them based on fish size (estimating the smallest fish likely to be encountered in the field is 2 g). The FHWG, which is composed of representatives from NOAA, USFWS, DFG, and the USACE met in 2008 to further discuss injury thresholds. Following the meeting, the agreed-upon criteria for injury to fish from pile-driving activities were proposed (as reported in Oestman et al. 2009; Table 9):

Table 9. Fisheries Hydroacoustic Working Group (FHWG) recommended
interim sound exposure criteria for fish (reported in Oestman et al. 2009).

Interim Criteria for Injury	Agreement in Principle		
Peak	206 dB (all size of fish)		
SELcum	187 dB - fish ≥ 2 g		
SELCUIT	183 dB - fish < 2 g		

More recently, Popper et al. (2014) estimated pile-driving acoustic criteria for fish based on effects data derived from Halvorson et al. (2011; 2012a, b) and Popper et al. (2005) (Table 10).

(3)

Table 10. Pile-driving exposure guidelines for fish (reported in Popper et al. 2014). Mortality and recoverable injury data based on Halvorson et al. (2011; 2012a, b); TTS impairment based on Popper et al. (2005).

Response	Type of Fish	Exposure Level		
	No swim bladder (particle motion detection)	>216 dB SEL _{cum} or >213 dB peak		
Recoverable Injury	Swim bladder not involved in hearing (particle motion detection)	>203 dB SEL _{cum} or >207 dB peak		
	Swim bladder involved in hearing (primarily pressure detection)	>203 dB SEL _{cum} or >207 dB peak		
	No swim bladder (particle motion detection)	>>186 dB SELcum		
TTS	Swim bladder not involved in hearing (particle motion detection)	>>186 dB SEL _{cum}		
	Swim bladder involved in hearing (primarily pressure detection)	186 dB SEL _{cum}		

Notes: peak and RMS sound pressure level dB re 1 µPa; SEL dB re 1 mPa²s

5.2.3 Masking

No studies were found that measuring masking to fish communication related to dredging-induced sounds. However, Codarin et al. (2009) conducted laboratory sounds using boating sound playbacks to investigate the potential impact of the communication of three vocal fish species (Mediterranean damselfish (*Chromis chromis*), brown meagre (*Sciaena umbra*), red-mouthed goby (*Gobis cruentatus*)). Playback audio of ambient sounds and boating sounds from an 8.5-m-long 163 hp diesel craft were used with acoustic frequency main energy below 1,000 Hz, and a source SPL of 142.3 dB re 1 μ PA at 1 m. Results indicated that vessel sounds could impact the communication of fish, interfering with the detection of conspecific sounds (Codarin et al. 2009).

5.2.4 Behavioral effects

There are a few field studies available that estimate the avoidance behavior of "free swimming" fish to anthropogenic sounds. There are a number of challenges in discerning differences in behavioral responses for free swimming fish. Such challenges include "weak" biological responses to stimuli and absence of protocols for standardizing observational methods. Determining the "normal" variance of behavior is challenging due to the multivariate and intrinsic nature of organisms' behavioral changes in time and space (Erbe et al. 2016). Simpson et al. (2015) investigated the behavioral impacts to juvenile European eels (*Anguilla anguilla*) to simulated shipping sound playbacks in laboratory and open-water experiments. Eels exposed to playbacks of shipping sounds at approximately 153 dB re 1 μ Pa at 1 m had slower startle responses to ambush predators, diminished spatial performance, and elevated ventilations and metabolic rates (stress indicators) as compared to control individuals. These results showed underwater sound effects of shipping-affected physiological and behavioral endpoints.

Jung and Swearer (2011) conducted a field study to determine the potential behavioral avoidance of larval fish (multiple species) exposed to recorded playbacks of underwater sounds emitted from recreational boat traffic. The study was conducted in open water where fish were held in experimental traps and exposed to the playback sounds. Received levels were 107 dB re 1 μ Pa RMS (boat only) and 111 dB re 1 μ Pa RMS (boat and ambient noise). The results indicated no significant differences among the boat playback traps or control in terms of abundance or diversity of larval fish. This study concluded that recreational boating sounds were not expected to have an adverse effect on recruitment of larval fish.

In addition, a few studies have demonstrated measurable changes in biometric stress responses following shipping sound playbacks to fish. Wysocki et al. (2006) measured increased cortisol secretion in three species of fish (carp (*Cyprinus carpio*)), gudgeon (*Gobio gobio*), and European perch (*Perca fluviatilis*)) following exposure to shipping playback sounds at SPLs of 153 dB re 1 μ Pa at a duration of 30 min. Also, Celi et al. (2016) measured increases in a number of biometric stress indices of gilthead seabream (*Sparus aurata*) following ten-day exposures to shipping sound playback as compared to a control.

In the most comprehensive study found, Kastelein et al. (2008) tested startle responses of fish species in laboratory exposures to determine threshold effect levels. Fish were exposed to pure tones at frequencies ranging from 0.1 to 64 kHz, and "reaction thresholds" were estimated when 50% or more of the population reacted to the stimulus. In general, this study demonstrated that reactions to underwater sounds vary by frequency and are dependent on the auditory thresholds of fish species. The following general observations were made by the authors:

• Sea bass (*Dicentrarchus labrax*) had a 50% reaction during exposures of SPLs ranging from 100 to 160 dB re 1 μPa at frequency bands

between 0.1 and 0.7 kHz. Startle responses are 0-30 dB above reported hearing thresholds.

- Atlantic herring (*Clupea harengus*; a hearing "specialist") had a 50% reaction during exposures of SPLs ranging from 160 to 180 dB re 1 μ Pa at a narrow frequency band of 4 kHz. The startle responses were ~30 dB above auditory hearing thresholds.
- Pollack (*Pollachius pollachius*) response threshold levels were not achievable based on the study design. It is likely that response thresholds were >180 dB (the maximum SPL achievable in the experimental design).
- Horse mackerel (*Trachurus trachurus*) had a 50% reaction during exposures of SPLs ranging from 100 to 170 SPL (dB re 1 μ Pa) at frequencies between 0.1 and 2 kHz.
- Pout (*Trisopterus luscus*) had a 50% reaction at SPLs ranging from 100 to 140 dB re 1 μ Pa at frequencies between 0.1 and 0.25 kHz.

More recently, Kastelein et al. (2017b) conducted a laboratory-scale study to discern the acoustic dose-behavior response relationship in sea bass (*Dicentrarchus labrax*) following exposures to pile-driving sound playbacks. Initial behavioral responses, in terms of swim speed and direction, were monitored in addition to sustained responses, which included changes in school cohesion, swimming depth, and speed. Results indicated that the 50% initial response (i.e., sudden, short-lived changes in swim behavior) threshold occurred at SEL (expressed as a "single strike") of 131 and 141 dB re 1 μ Pa²s for small (31 centimeters [cm]) and large (44 cm) fish, respectively. This study found no evidence of any sustained responses to sound exposures, indicating that longer-term behavioral responses are unlikely within the range of exposures measured in this study (SEL 122 to 158 dB dB re 1 μ Pa²s; Kastelein et al. 2017b).

5.2.5 Fish Effects Summary

To date, the authors are unaware of any studies that have directly measured effects of underwater dredging sounds on fish species. A few studies have estimated effects on fish by comparing sounds from fielddredging operations to literature-derived TTS effects criteria. The currently available effects data from anthropogenic sources indicate that dredging-induced sounds do not pose a significant risk to direct injury or mortality in juvenile or adult fish. Mortality of fish following exposures to anthropogenic sounds is generally limited to high-intensity impulsive sounds (e.g., explosions, pile driving, airguns; Table 11).

	Exposure Level	_				
Source	SEL _{cum} (dB re 1 µPA ² s), unless otherwise noted	Frequency (kHz)	Species (life stage)	Effect	Reference	
Explosion	234 (SPL zero-to-peak)	NR	Spot, pinfish (late larvae)	Lethal effects	Govoni et al. 2008	
Colorado obra	220-242 (SPL zero-to-peak)	NR	Cod, saithe, herring, turbot, plaice (eggs and larvae)	Injuries and lethal effects in some species	Booman et al. 1996	
Seismic airgun	180 (mean SEL); 207 (peak SPL)	<0.04	Northern pike, lake chub, broad whitefish (adult and YOY)	TTS (pike and chub), TTS recovery within 24 h	Popper et al. 2005	
	217	NR	Chinook salmon (juveniles)	No mortality; onset of injury with evidence of recovery	Casper et al. 2012	
Pile driving	210	<1	Chinook salmon (juveniles)	Onset of injury ^a	Halvorsen et al. 2012b	
	207	NR	Lake sturgeon, Nile tilapia (juveniles)	Onset of injury ^a	Halverson et al. 2012a	
	190 (SPL dB re 1 µPa RMS; TSHD)	0.08 to 1	Atlantic salmon	no significant behavioral effects	Nedwell et al. 2008	
Dredging	163 (SPL dB re 1 µPa RMS; BHD)	0.08 to 1	Atlantic salmon	no significant behavioral effects	Nedwell et al. 2008	
	117-122 (SPL dB re 1 μPa at 50 m)	<1	Clupeidae and flat fish	no auditory injury risk	DEFRA 2003	
Shipping + Dredging	186 (24 h exposure)	0.5 to 10	ND (modeled fish exposure)	Exceeded TTS risk threshold for fish < 2g ^b	Heinis et al. 2013	
Shipping	182 (24 h exposure)	0.5 to 10	ND (modeled fish exposure)	Did not exceed TTS risk threshold for fish >2g ^b	Heinis et al. 2013	
Simulated playback	170 (dB re 1 µPa RMS)	0.1 to 10	Goldfish (adult)	TTS; inner ear hair cell loss; TTS recovery within 8 d°	Smith et al. 2006	
	~150 dB (SPL db re 1 μPa; nine month duration)	0.1 to 5	Rainbow trout (life cycle)	No hearing loss detected	Wysocki et al. 2007	
	137-147 (SPL dB re 1 µPa)	0.16 to 0.5	Herring (adult)	No differences in fish behavior (school size, rise time)	Handegard et al. 2016	

RMS = root mean

^bTTS risk thresholds for fish < 2 g = 183 dB re 1 μ Pa²s; TTS risk thresholds for > 2 g = 187 dB re 1 μ Pa²s (originally based on Oestman et al. 2009) square °8 d post-exposures TTS recovery to baseline was observed; correlating with inner ear hair cell density recovery NR = not reported Note: Booman et al. (1996) data cited as reported in Bolle et al. (2016)

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Of the few studies available that evaluated sub-lethal effects of dredginginduced sounds (i.e., DEFRA 2003; Nedwell et al. 2008; Heinis et al. 2013), there was no evidence of risk for auditory injury (TTS) or behavioral effects for larger-bodied fish (>2 g). In terms of adverse effects to smaller-bodied fish, Heinis et al. (2013) estimated based on "worst case" scenario that smaller-bodied fish (>2 g) were at risk in the immediate vicinity of the sound source (<20 m). In terms of masking and behavioral responses, lower-frequency sounds (<1,000 Hz) emanating from shipping and dredging are of particular interest due to the overlap of hearing detection of many fish species.

5.3 Effects on marine mammals

The published literature on the effects of underwater sound on marine mammals is more extensive than that for fish (William et al. 2015). This trend is likely based on the regulatory focus of larger charismatic marine mammals (e.g., whales, seals, dolphins). Many of the controlled experiments conducted on marine mammals were tonal or playback sounds. Only a few studies were found that estimated effects of dredgingrelated sounds on marine mammals (Richardson et al. 1990; Gilmartin 2003; Gerstein et al. 2006; Hoffman 2010; Heinis et al. 2013).

As reported in the literature, the effects of underwater sound on marine mammals range from direct mortality, auditory, and non-auditory physiological effects, masking, and behavioral responses (Erbe 2011). Field surveys collected synoptically with naval sonar exercises, seismic surveys, and pile-driving activities provide sound exposure data for potential adverse effects to marine mammals (Foote et al. 2004; Tougaard et al. 2009; Brandt et al. 2011; Tyack et al. 2011; Dahne et al. 2013). In addition, controlled laboratory experiments have also been conducted investigating threshold levels of auditory effects from sound playbacks (Finneran et al. 2002; Kastelein et al. 2012, 2013a,b). The NOAA NMFS's 2016 technical guidance is an additional resource that provides a comprehensive review and study of peer-reviewed literature and government reports on the impacts of underwater sound on marine mammals (discussed further in Section 7).

There are numerous marine mammals for which auditory sensitivities and vocalization patterns overlap sounds generated by anthropogenic activities (see Appendix A for more information). Echolocating marine mammals (e.g., dolphins and porpoises) have acute hearing and may be particularly sensitive to lower frequency sounds (Kats 2009). In general, available sound effect data are limited to Pinnipeds (e.g., seals, sea lions), and Odontocetes (e.g., dolphins, whales), with limited data available for Sirenians (manatees).

5.3.1 Direct injury

High intensity sounds (e.g., explosions, sonar) have been linked to mortality in a variety of marine mammal species (Koper and Plön 2012). Reports of direct injury to underwater explosions are typically anecdotal observations, with very few instances of reported details regarding the acoustical characteristics or shock waves associated with exposures. Near a site that had conducted repeated offshore blasting (with explosives up to 5000 kg), two humpback whales were found with mechanical injuries to the ears—ruptured tissues, which eventually lead to death (Ketten 1995).

Indirect injury attributed to high-intensity sounds include the rapid dive or rise time of marine mammals, which can lead to embolism (gas bubbles in bloodstream) causing damage to tissues and organs. Mass stranding of cetaceans (e.g., whales, dolphins, porpoises) following military sonar operations have been well documented, where recovered animals had evidence of hemorrhaging of internal organ or tissues (Koper and Plön 2012). Todd et al. (2015) conducted a literature review of the impacts of marine dredging activities on marine mammals. Key findings from this review estimated that it is unlikely that dredging-related sounds would physiologically damage marine mammal auditory systems; however, there may be risk associated with masking and behavioral disturbances. Todd et al. (2015) indicated that, based on overlap of baleen whale communications at low frequencies, they might be at higher risk to dredging-related sounds. With the exception of underwater blasting of rock formations to widen or deepened a navigation channels, direct injury leading to mortality in marine mammals has not been documented in association with navigation dredging projects (Todd et al. 2015).

5.3.2 Effects on hearing

5.3.2.1 Dredging

To date, there are no studies that have directly measured hearing loss (PTS or TTS) in mammals in relation to dredging sounds. However, a single study was conducted in 2013 that measured the acoustic signatures during

shipping and dredging activities and related those to existing auditory effects thresholds (i.e., Southall et al. 2007).

Heinis et al. (2013) measured underwater sounds of shipping and TSHD dredging activities during the expansion of the Port of Rotterdam in the Netherlands. Sound measures were modeled and compared to PTS and TTS auditory thresholds (i.e., Southall et al. 2007). Measured SPLs for 24-hour exposures were 186.6 dB re 1 μ Pa²s. Sound exposures were weighted for swim behavior of harbor porpoises and seals in relation to the sound sources. Estimated 24-hour exposures for harbor porpoises and seals were 180.5 and 182.4 dB re 1 μ Pa²s, respectively. Exposures were compared against conservative thresholds developed by Southall et al. (2007) for PTS and TTS risk for harbor porpoises and harbor seals. Using a worst-case scenario assumption of swimming behavior of marine mammals, Heinis et al. (2013) estimated that less than 0.1% of harbor porpoises and seals were exposed to the risk of TTS during dredging activities of the Rotterdam expansion project.

5.3.2.2 Tonal frequencies

The U.S. Navy Marine Mammal Program (MMP) has conducted TTS experiments using marine mammals (i.e., bottlenose dolphins and belugas; Finneran 2008). TTS were estimated based on behavioral responses to sound exposures (trained to vocalize when hearing test tones) and auditory-evoked potentials (AEPs). Major findings from these studies were the following:

- Extent of TTS generally increases with exposure SPL and duration; however, these alone are poor predictors for TTS.
- Onset of TTS from "steady-state" sounds up to ~16 sec can be predicted using an equal energy relationship.
- Dolphins with onset of behaviorally measured TTS up to 33 dB have completely recovered after several days.
- Differences among TTS measured behaviorally and electrophysiologically (AEPs) were dramatically different, whereas TTS measured using AEPs were always larger.

Data derived from these studies are in part the basis for the development of auditory exposure guidelines (PTS and TTS; Southall et al. 2007; NOAA et al. 2016). TTS criterion is generally accepted as an appropriate metric for estimating auditory injury and establishing exposure limits due to the relative sensitivity of mammals' inner ear to sound exposures (Southall et al. 2007) and the ability to reliably measure TTS in captive marine mammals (Tougaard et al. 2009).

The initial effort for developing underwater sound exposure criteria for mammals was proposed by Southall et al. (2007), which relied on the available exposure-response data and calculated auditory frequencyweighted threshold functions to develop TTS and PTS criteria. Since then, a number of studies that improved knowledge about the effects of underwater sound sources (Finneran 2015; Erbe et al. 2016) resulted in a new comprehensive study of the current state of the science and the acoustic thresholds to inform revised NOAA (July 2016) technical guidance. NOAA (2016) marine mammal effects guidelines are discussed in greater detail in Section 7. Studies investigating the auditory effects for mammals from specific anthropogenic sound sources are discussed below.

5.3.2.3 Seismic airgun

There are a number of studies that have experimentally tested the auditory shifts of marine mammals to impulsive seismic airgun exposures. TTS shifts in marine mammals are measured using either behavioral (trained response) or electrophysiological methods (i.e., auditory-evoked potentials).

Finneran et al. (2002) exposed bottlenose dolphins (*Tursiops truncates*) and white whales (*Delphinapterus leucas*) to single pulses from seismic airguns in laboratory experiments. Temporary shifts in masked hearing thresholds (MTTS) were estimated using behavioral responses, and defined as 6 dB increase or larger shift from baseline. Following a single pulse of 186 dB re 1 μ Pa²s at 400 Hz frequencies, threshold shifts of 7 dB were observed in the white whale. Auditory recovery was observed within 2 dB to baseline (pre-exposure thresholds) within 4 min post-exposure. The bottlenose dolphin did not have any measureable shift in auditory thresholds at the highest exposure conditions tested (188 dB re 1 μ Pa²s).

In another laboratory study using bottlenose dolphins (*Tursiops truncates*), Schlundt et al. (2016) measured shifts in auditory thresholds following exposures of 10 pulses from seismic airguns. Auditory shifts were estimated using behavioral methods only, due to the inconclusive results from attempted AEP methods. After cumulative SEL exposures of 189-195 dB re 1μ Pa²s (212 dB re 1 μ Pa (peak-to-peak)), there were no measureable TTS in any of the individuals used. However, behavioral responses were measured in two of the individuals that exhibited an "anticipatory" response to the airgun exposures. These results suggest that the auditory responses of dolphins may be less sensitive than previously predicted.

Lucke et al. (2009) measured TTS in harbor porpoises (*Phocoena phocoena*) following a single impulse exposure from a seismic airgun in a laboratory study. Auditory shifts were estimated using electrophysiological methods and TTS onset was defined as differences of twice the standard deviation from average hearing threshold or a 6 dB from baseline (Southall et al. 2007). At an SEL of 165.5 dB re 1 μ Pa²s, porpoises had a 9.1 dB TTS. Within 3 hours of the initial exposure, TTS decreased by 2.9 dB, with full recovery to baseline estimated to occur within 12 to 55 hours. Similarly, Kastelein et al. (2017a) observed onset of ~4 dB TTS in harbor porpoises after exposures to multiple airgun shots (10 to 20) with sound exposures of SELcum 188 to 191 dB re 1 μ Pa²s. Porpoise TTS recovery was observed within 12 min post exposure (Kastelein et al. 2017a). Overall, these studies demonstrate that mammal TTS onset can occur from impulsive sounds, and auditory recovery to pre-exposure conditions have been observed within minutes to days.

5.3.3 Masking

A few studies were identified that estimated the influence of low-frequency continuous sounds from shipping and dredging operations to communication or auditory masking of marine mammals (manatee and whales). Gerstein et al. (2006) estimated zones of auditory masking to manatee during TSHD operations in the St. Johns River in Jacksonville, FL. The primary goal was to discern whether manatees had an increased risk of vessel strikes due to the underwater sound of dredging activities. Masking was defined by the critical ratio of manatee's auditory sensitivities, ambient noise conditions, acoustical characteristics of TSHD, and speed of approaching vessels. It should be noted that no behavioral parameters were assessed during the study because no manatees were observed in the study area prior to, during, or after operations. The major sources of underwater sound that were relatively continuous included cavitation from dredge propellers, draghead vacuuming, and the submerged slurry pump out pipeline. Sound pressures levels measured during operations ranged from 169 to 177 dB re 1 µPa at 1 m. Gerstein et al. (2006) estimated that TSHD acoustical properties created zones of auditory masking in the vicinity of the operations; the zones may increase the probability of vessel strikes. Zones of masking for manatee were estimated to be 512 m and 4,096 m from the

dredge, for boats approaching at speeds of 5 and 24 miles per hour (mph), respectively. This study empirically demonstrated the potential masking zones that could increase the risks associated with manatee boat strikes.

More recently, Clark et al. (2009) investigated the acoustic masking influence of shipping sound on singing fin (*Balaenoptera physalus*), singing humpback (Megoptera novaeangliae), and calling right (Eubalaena glacialis) whale species. The purpose of the study was to provide an analytical approach to address the challenges with quantifying masking effects in a dynamic acoustical communication space. To demonstrate the approach, the authors used a combination of modeling and analytical techniques for estimating the overlap of shipping sound and the target whales' communication space. The resultant modeling provided signal-to-noise ratios (SNR) for estimating the amount for which sound reduces the ability of a receiving animal to discern other biological underwater sounds. Of the three species evaluated, it was determined that the North Atlantic right whale was compromised by sound from commercial shipping traffic (Clark et al. 2009). This study was one of the first to define parameters to address the spatial and temporal aspects of quantifying masking effects from shipping sounds.

5.3.4 Behavioral effects

There are numerous behavioral responses observed for marine mammals such as humpback whales, porpoises, and seals exposed to anthropogenic sounds. Generally, studies investigating behavioral responses to sound are anecdotal field observations that offer limited data for understanding exposure response relationships. Behavioral responses to sound include avoidance, startle responses, swim direction and speed, dive duration, surfacing duration and interval, respiration (blow rate), movement towards or away from sound, or changes in acoustic vocalization behavior (Erbe 2011). Reports of marine mammal behavioral responses near dredging activities are discussed below.

5.3.4.1 Dredging

Hoffman (2010) investigated the potential adverse effects of dredging on a threated whale species near Cook Inlet, Alaska. USACE annually dredges approximately 1.6 million m³ of material from the Port of Anchorage near the head of Cook Inlet (Hoffman 2010). Beluga whales are listed as threatened under the Endangered Species Act (ESA); therefore, a

biological assessment was conducted that focused on the potential impacts of dredging on Beluga whales. Whales were often observed within a few meters of cargo ships and dredges at the Port of Anchorage; however, it was unclear if whales were tolerating the underwater sound or had become habituated to it. The hearing frequencies of beluga whales are best between 10 and 100 kHz, which is typically above the lower frequency ranges associated with dredging and shipping (Hoffman 2010; Appendix C). Based on a biological impact analysis, it was concluded that dredging and placement did not adversely affect beluga whales.

In a comprehensive 2-year study by Richardson et al. (1990), behavioral reactions of bowhead whales were observed near dredging and drilling operations in the Canadian Beaufort Sea. In addition to observational data collected during active operations, open-water experiments were conducted using sound playbacks of underwater sounds associated with drillships and dredge sounds (Richardson et al. 1990).

Richardson et al. (1990) conducted observational studies during active dredging operations and behavioral data were recorded. Occasionally, bowhead whales were observed near <5 km dredging operations. The closest recorded whale activity during operations was at a distance of 0.8 km from the suction dredge *Beaver Mackenzie*. During one dredging operation, two groups of bowhead whales were observed at 13 km from hopper dredges unloading, with corresponding received sound levels estimated at 115-117 dB re 1 μ Pa in the 20-1000 Hz frequency band (authors did not estimate based on SEL; i.e., duration of sound exposure unknown). These bowheads engaged in normal activities during this time. Even when the dredge began to approach and unload, there was no apparent change in behavior and no orientation away from the dredge.

Richardson et al. (1990) also conducted open-water playback exposures of recorded sounds of drill ships and dredges. The underwater sound exposures were 30-40 min durations, repeated seven times. Following playback sounds, behavioral characteristics of bowhead whales that were measured included call rates, feeding, and surfacing cycles. Peak source levels of playback experiments ranged from 155 to 164 dB re 1 μ Pa at 1 m (broadband). Estimated received levels of low-frequency sounds (20-1,000 Hz) to the farthest whales during the experimental periods ranged from 94 dB to 122 dB re 1 μ Pa. In general, there was no one behavioral variable that was consistently altered during playback experiments.

Overall, bowheads tended to orient and move away during playbacks. During one playback experiment, feeding ceased and whales moved away from sound source. Sometimes the duration of surfacing and number of blows were reduced; however, there was no evidence of alterations of call types, intervals between respirations, frequencies of turns, or dive behavior following playback sounds.

Overall findings of this study were that there was broad overlap between received sound levels to which bowheads did and did not respond to sound playbacks; however, approximately 50% of bowheads reacted when received underwater sound level was 115 dB re 1 μ Pa in the 20-1,000 Hz frequency band. This corresponded to approximately 20 to 30 dB above ambient sound conditions. In terms of zones of influence around dredges, the following observations were made:

- Dredging sounds were estimated to be above background at 15 km from dredge.
- The audible zone (based on signal-to-noise ratios) was estimated to be 29 km from dredge source.
- The radii of responsiveness (eliciting a behavioral response) were estimated to be 4.6 km (broadband) and 2.8 km (1/3 octave band) from the dredge.

Gilmartin (2003) observed behaviors of Hawaiian monk seals (*Monachus schauinslandi*) during grab dredging operations in early 1990 at Tern Island at French Frigate Shoals, Hawaii. Seals transiting the area during dredging did not appear startled or adversely affected, with no observable change in swim speed or direction. Pirotta et al. (2013) observed avoidance behavior of bottlenose dolphins during dredging activities in the Aberdeen Harbor (Scotland). It was also determined that dolphins responded to high levels of boat traffic. It should be noted that dredging often occurs in areas with other sources of anthropogenic sounds (e.g., shipping); therefore, it can be challenging to attribute field-observed effects directly to dredging activities (Todd et al., 2015).

5.3.5 Marine mammals effects summary

As compared to other taxa, marine mammals have been more extensively studied in terms of responses to underwater sound. Auditory injury has been observed for impulsive (pile driving, seismic surveys) and continuous sounds (broadband sound playbacks; Table 12). Common metrics of sound-related injury are described by PTS or TTS. The TTS criterion is generally accepted as a reliable metric for estimating sound-related injury and has been used for establishing exposure limits due to the relative sensitivity of the inner ear of mammals to sound exposures (Southall et al. 2007) and the ability to reliably measure TTS in captive marine mammals (Tougaard et al. 2009).

In terms of mammal responses to dredging-induced sounds, there are limited data directly measuring the onset of auditory injury. Based on the data available for mammal responses to other anthropogenic underwater sounds, risks associated with dredging are likely limited to masking and behavioral effects (Thomsen et al. 2016). Only a single study to date has estimated the onset of PTS and TTS from dredging sounds (Heinis et al. 2013). During the expansion of the Port of Rotterdam, long-term monitoring of TSHD and shipping sounds were used to estimate the potential risks for harbor porpoises and seals using exposure modeling. Results from this study did not indicate that harbor porpoises or seals would exceed PTS or TTS thresholds during dredging operations (Heinis et al. 2013).

In terms of behavioral responses to dredging activities observed in the field, whales and seals had no adverse reactions or avoidance behavior near active dredging operations. Following playback sounds from dredging activities, bowhead whales sometimes exhibited avoidance or altered feeding behaviors (Richardson et al. 1990). A 1-year field study evaluating avoidance behavior in harbor porpoises revealed that there may be short-term avoidance of areas near dredging activity; however, these effects were short-term and porpoises return to the areas after the dredging activity was completed (Diederichs et al. 2010). Based on observational studies, pinnipeds (seals) did not exhibit avoidance or altered behavior near dredging activities (Gilmartin 2003). There is some evidence that sirenians (manatee) may be susceptible to low-frequency sounds masking boating sounds (Gerstein et al. 2006).

	Exposure Level					
Source	SEL _{cum} (dB re 1 µPa ² s), unless otherwise noted	Frequency (kHz)	Species	Effect	Reference	
	186 dB re 1 µPa²s; 226 (SPL peak-to-peak)	0.4 and 30	White whale (adult)	7 and 6 dB MTTSª	Finneran et al. 2002	
Seismic airgun	188 dB re 1 µPa²s; 226 (SPL peak-to-peak)	0.4, 4, and 30	Bottlenose dolphin (adult)	No observable MTTS	Finneran et al. 2002	
	189-195; 193-209 (SPL peak-to- peak)	NR	Atlantic bottlenose dolphin (adult)	No observable TSS	Schlundt et al. 2016	
	165.5	0.5 to 20	Yangtze finless porpoise	9.1 dB MTTS, with recoveryb	Lucke et al. 2009	
Sound playback	163 (SPL; 60 min continuous exposure)	~4	Harbor seal	44 dB TSS, with recovery ^c	Kastelein et al. 2013a	
("white noise")	151-190	~4	Bottlenose dolphin	15 dB TSS, with recoveryd	Kastelein et al. 2012	
Sonar	142 (SPL dB re 1 µPa RMS)	3.5 to 8	Blainville's beaked whales	echolocation alterations, modified diving behavior	Tyack et al. 2011	
Pile driving	194	0.08 to 0.2	Harbor porpoise (field observations)	behavioral effects (avoidance)	Brandt et al. 2011	
File unwing	139-152	~0.25	Harbor porpoise (field observations)	behavioral effects (avoidance)	Dahne et al. 2013	
	177 (SPL dB re 1 μPa RMS)	0.1 to 10	Modeled manatee masking zone	512-4,096 m auditory masking zone	Gerstein et al. 2006	
	115-117 (SPL dB re 1 μPa "received level")	0.02 to 1	Bowhead whales (field observations)	no observable behavioral response	Richardson et al. 1990	
	94-122 (SPL dB re 1 µPa "received level")	0.02 to 1	Bowhead whales (dredging sound playback)	inconclusive behavioral responses	Richardson et al. 1990	
Dredging	NR	NR	Hawaiian monk seals (field observations)	no adverse behavioral response	Gilmartin 2003	
	NR	NR	Beluga whales (impact assessment)	no adverse effects reported	Hoffman 2010	
	NR	NR	Bottlenose dolphins (field observations)	avoidance behavior	Pirotta et al. 2013	
	NR	NR	Harbor porpoise (field observation)	Short-term avoidance behavior	Diederichs et al. 2010	
Shipping +	182 (24 hour exposure)	0.5 to 10	Modeled seal behavior (AQUARIUS)	did not exceed TTS risk threshold ^e	Heinis et al. 2013	
Dredging	180 (24 hour exposure) 0.5 to 10		Modeled harbor porpoise behavior (AQUARIUS)	did not exceed TTS risk threshold ^f	Heinis et al. 2013	

Table 12. Overview of effects of underwater sound on mammal species from anthropogenic sources.

	Exposure Level	_				
Source	SEL _{cum} (dB re 1 µPa ² s), unless otherwise noted	Frequency (kHz)	Species	Effect	Reference	
	176 (24 hour exposure)	0.5 to 10	Modeled seal behavior (AQUARIUS)	did not exceed TTS risk threshold ^e	Heinis et al. 2013	
Shipping	170 (24 hour exposure)	0.5 to 10	Modeled harbor porpoise behavior (AQUARIUS)	did not exceed TTS risk threshold ^f	Heinis et al. 2013	
0pp8	117 (SPL dB re 1 µPa RMS)	NR	St. Lawrence river belugas	increased level of vocalizations	Scheifele et al. 2005	
	generalized comparisons to shipping traffic ^g	NR	Killer whales (adult)	increased duration of calls	Foote et al. 2004	

^aHearing thresholds recovery occurred approximately 4 min postexposure

^bEstimated recovery <6 dB MTTS was 55 h

^cHearing recovered 4 d post-exposure

^dEstimated recovery time varied between 4 and 96 min

MTTS = masked hearing threshold

eCalculated SEL values were below the TTS threshold values of 183 (seal; Southall 2007) fCalculated SEL values were below the TTS threshold values of 195 (harbor porpoise; Southall 2007)

Analysis of whale behavior (duration of calls) with increased boat noise during 1973 and 2003.

NR = not reported

5.4 Effects on other marine species

5.4.1 Sea turtles

Significant data gaps exist in terms of sea turtle responses to underwater sound. Willis (2016) reports that the vocalizations and best hearing frequencies for turtles are around 300-500 Hz. Only a few species having published audiograms (exceptions are loggerhead turtle (*Caretta caretta*); green turtle (Chelonia mydas); Kemp Ridley (Lepidochelys kempi); and red-eared slider (*Trachemys scripta elegans*) (Appendix A)). Preliminary data suggests sea turtles are somewhat resistant to high-intensity explosives, suggesting that sea turtles are also resistant to impulsive sounds (e.g., pile driving, seismic airguns; Ketten et al. 2005; Popper et al. 2014). One study evaluating sound exposures to turtles, Moein et al. (1994), investigated the potential adverse effects of seismic airgun deterrents to loggerhead sea turtles in an effort to minimize the turtles' activity around dredging operations. Following exposures to dB levels ranging from 175-176 (reference pressure not stated), sea turtles experienced slight shifts in auditory capabilities. Based on the lowerfrequency hearing range of turtles, there may be potential for behavioral or masking effects of lower-frequency anthropogenic sounds.

5.4.2 Invertebrates

Reponses of aquatic invertebrate species to underwater sound are discussed below and organized based on sound source. To date, the authors are unaware of any studies that have evaluated the effects of invertebrates following dredging-induced sounds.

5.4.2.1 Shipping and low-frequency sounds

Wale et al. (2013a) measured stress-related biomarkers (oxygen consumption rates) of shore crabs (*Carcinus maenas*) following single and repeated exposures of playbacks of ambient and shipping underwater sounds in controlled tank-based exposures. Sound playback exposures were 108-111 and 148-155 dB RMS for ambient ship sounds, respectively. Following repeated exposures to shipping sounds, shore crabs had an increase in oxygen consumption as compared to ambient sound playback exposures. In addition, heavier crabs had stronger responses to shipping sounds as compared to lighter crabs, indicating that there was a size dependency to the exposure-response relationship. In another behavioral study by Wale et al. (2013b) using similar experimental methods and the same sound exposure characteristics, behavioral responses in terms of foraging activity and antipredator responses following shipping playback sounds were measured. There were no measurable differences among the number of crabs finding a food source or time taken to find a food source; however, there were significantly more crabs distracted during feeding when exposed to shipping sounds as compared to ambient sounds. In terms of antipredator behavior in shore crab, crab exposed to shipping noise took significantly longer to return to shelter in the immediate aftermath of a simulated attack (Wale et al. 2013b).

In one of the most comprehensive studies reviewed, Sole et al. (2013) conducted controlled laboratory experiments using four cephalopod species (cuddlefish (*Sepia officinalis*), octopus (*Octopus vulgaris*), and squid (*Lobigo vulgarus* and *Illex condientii*)) exposed to low frequency sounds (50-400 Hz). Following sound exposures, the whole inner ear structure of the cephalopod's sensory organs (statocyst) were evaluated for apparent damage using scanning (SEM) and transmission (TEM) electron microscopy techniques. Peak sound exposure levels were 175 dB re 1 μ Pa at 1-s sweeps for a duration of 2 hour at a frequency of 50-400 Hz. Following exposures, sensory organs were examined and compared to untreated controls. Following sound exposures, there was observed statocyst damage (lesions, hair cell loss, etc.) in cephalopod species. The results from this study indicate that high-intensity, low-frequency sounds can damage sensory organs in cephalopod (i.e., squid, octopus, cuddlefish) species.

5.4.2.2 Underwater explosions

In general, invertebrates are less sensitive to pressure-related damage following underwater explosions as compared to many marine mammal species (Keevin and Hempen et al. 1997). This is likely related to the lack of gas-containing organs susceptible to mechanical injury in vertebrates. A number of studies have measured mortality of invertebrates (shellfish and crab) as a function of distance from detonation sources of explosions. White shrimp near a blasting site using 33 m of 100 g/33 cm of detonation cord had 30% and 0% mortality at distances of 11 and 46 m from source, respectively (Linton et al. 1985 (cited in Keevin and Hempen 1997)). Anon (1948) (cited in Keevin and Hempen et al. (1997)) measured blue crab (*Callinectes sapidus*) mortality following blasts from 30 lb of TNT. At distances of 8 and 46 m from blasts, blue crab mortality was 89% and 7%,

respectively. Lobsters (*Panulirus interruptus*) within 15-17 m of a blasting site using 9.1 kg of 60% petrogel had no mortality.

5.4.2.3 Seismic surveys

A few studies have investigated the potential influences of open-water seismic surveys to the catch yields of commercially relevant species of shellfish. Andriguetto-Filho et al. (2005) conducted a field investigation on the potential impact of seismic prospecting on shrimp fisheries (southern white shrimp (*Litopenaeus schmitti*); southern brown shrimp (Farfantepenaeus subtilis); and the Atlantic seabob (Xyphopenaeus kroyeri)) by comparisons of bottom trawl yields before and after the use of airguns. The airgun array produced peak SPLs of 196 dB re 1 µPa at 1 m shooting every 12 s. Catch yields were compared from pre-seismic surveys and 12-36 hours post airgun arrays. The results indicated no measureable differences in ship trawl yields after seismic prospecting. Parry and Gason (2006) conducted a statistical analysis of historical commercial catch rates of rock lobster (Palinuvidae family) to measure the potential adverse effects associated with coinciding seismic surveys. Based on the analysis of catch rates and corresponding seismic surveys, there was no apparent relationship of lobster catch yields to seismic surveys.

In one of the first studies to investigate the effects of underwater sound on larval abnormalities, de Soto et al. (2013) measured the potential adverse effects of seismic pulses to scallop larvae development in controlled laboratory experiments. Playbacks of seismic pulses were conducted in bench-scale experiments with SPL exposures of 160-164 dB RMS re 1 μ Pa, corresponding to a sound exposure level of 161-165 dB RMS re 1 μ Pa²s. Following noise exposures, scallop larvae had significant developmental delays and 46% developed body abnormalities.

5.4.2.4 Broadband noise

A few studies have been conducted evaluating the effects associated with the ambient "broadband" noise associated with the maintenance and rearing of marine animals. Lagardere (1982) and Regnault and Langardere (1983) compared the health of brown shrimp (*Crangon crangon*) in ambient rearing tank conditions compared to soundproofed tanks with 30 dB lower sounds. The results indicated that experimental tank environments with prevailing ambient sounds resulted in a significant reduction in growth and reproduction rates of the shrimp as compared to soundproofed tanks (Lagardere 1982; Regnault and Lagardere 1983).

5.5 Effects summary

Anthropogenic underwater sound effects range from direct mortality to a variety of non-lethal responses. Typically, mortality observed for marine biota to anthropogenic sound is limited to high-intensity impulsive sounds (e.g., explosions). With the exception of blasting events in navigation channels, sounds associated with dredging activities are not at sufficient intensities (SPLs) to pose risks of mortality or permanent injury (Boyd et al. 2008; Todd et al. 2015). Ecological risks associated with sounds from dredging activities are anticipated to be limited to non-lethal effects, which include auditory injury, masking, and behavioral responses (Boyd et al. 2008; Todd et al. 2015; Hawkins et al. 2015).

Auditory injury (in terms of PTS and TTS) has been observed for a number of mammal and fish species exposed to both impulsive and continuous underwater sounds. Common metrics of sound-related injury are described by PTS or TTS. The TTS criterion is generally accepted as a reliable metric for estimating sound-related injury and has been used for establishing exposure limits due to the relative sensitivity of the inner ear to sound exposures (Southall et al. 2007; Carlson et al. 2007; Oestman et al. 2009) and the ability to reliably measure TTS in captive organisms (Tougaard et al. 2009). To date, no auditory exposure-response data exist for dredging related sounds to aquatic organisms. Of the single study that estimated auditory risks of dredging operations by comparing sound metrics to existing auditory thresholds, there was no evidence of exceeding TTS risk thresholds for mammals or larger fish (>2 g), and slight risk on TTS for small (<2 g) fish in the immediate vicinity (<20 m) of the sound source (Heinis et al. 2013).

In terms of behavioral responses to dredging operations, a few species of whales and seals have demonstrated no adverse responses or avoidance near dredging (Richardson et al. 1990; Hoffman et al. 2010). Following playback sounds from dredging activities, bowhead whales sometimes exhibited avoidance or altered feeding behaviors (Richardson et al. 1990). Based on observational studies, pinnipeds (e.g., seals) did not exhibit avoidance or altered behavior near dredging activities (Gilmartin 2003). There is some evidence that low-frequency sounds from dredging activities may mask approaching boating sounds to sirenians (manatee, etc.) (Gerstein et al. 2006). It should be noted that there is uncertainty as to the appropriateness of using sound metrics for predicting biological responses. To date, dredging sounds have been described using SPLs RMS; however, comparisons to effects thresholds are limited to peak SPLs (for impulsive sounds) or SELs (cumulative).

6 Managing Risks from Underwater Sound

For dredging, there is a need to develop an appropriate risk-based framework to address the sound exposure of nearby biota to dredging sounds (e.g., excavation, transport, and placement). Accurate characterization of the acoustic exposure and biological responses is a critical step preceding risk management. A risk-based approach provides a systematic framework for characterizing exposures and biological responses to inform actions such as mitigation (Boyd et al. 2008; Thomsen et al. 2016; Merchant et al. 2017). A critical aspect of any successful underwater sound risk framework is to identify and mitigate appropriate ecological risks and to avoid managing ecologically insignificant risks that would pose unnecessary constraints and costs on dredging operations.

In general, mitigation techniques are implemented when risk management determined sound exposures are predicted to exceed threshold levels for one or more aquatic species occurring nearby (as defined by legislation, biological significance, or societal views) (Boyd et al. 2008). Based on management strategies used for other underwater sound sources (e.g., pile driving, drilling, shipping), there are a number of sound mitigation alternatives to consider. In general, the objective of these strategies is to alter the sound exposure to aquatic organisms through avoidance or minimization (Boyd et al. 2008).

6.1 Avoidance

6.1.1 Exclusion zones

Avoidance can be achieved by establishing "exclusion zones" surrounding a sound source (von Lüders and Gill 2008; ACCOBAMS 2013). These zones are intended to delineate distances from the sound source that pose risk to biological receptors and thereby exclude target organisms from those areas during operations. Exclusion zones are commonly established for high-intensity impulsive sounds (e.g., explosions, pile driving; ACCOBAMS 2013). Due to the complexity of sound propagation, exclusion zone dimensions are typically established using a combination of sound propagation modeling techniques and field monitoring (Greene and Blackwell 2008). The goal of an exclusion zone is to eliminate the source of the sound if organisms move within the zone (von Lüders and Gill 2008; NOAA 2016); therefore, a combination of visual and acoustic monitoring protocols can be used to observe biological activity within the zones. Dedicated marine mammal observers (MMO) or protected species observers (PSOs) can monitor zones prior to and during operations to provide real-time information (ACCOBAMS 2013; NOAA 2016). Additionally, passive acoustic monitoring systems can be used to detect the presence of vocally active species around exclusion zones, especially when visual observations by MMOs are impaired (i.e., during night and inclement weather, or due to submerged animals; Verfuss et al. 2018). If organisms are observed inside exclusion zones, operations are halted until the organisms have vacated the zone (NOAA 2016). Monitoring efforts are generally limited to larger animals that surface or more vocal species that can be readily detected using acoustic monitoring. There are ongoing efforts to broadly standardize MMO methods and qualifications (von Lüders and Gill 2008). In the United States, NOAA has provided a Technical Memorandum "National Standards for a Protected Species Observer and Data Management Program" to provide guidance to PSOs for standardizing methods (Baker et al. 2013). The level of effort and cost for establishing exclusion zones are largely dependent on the duration and location of dredging operations.

An experimental exclusion zone method applied to minimize biota exposures near the sound source is to implement "soft-starts" or "rampup" of high intensity sounds in an effort to provide time for biota to move away from the sound source prior to the production of full intensity sounds (ACCOBAMS 2013). However, ramp-ups have not been fully validated as effective means of deterring organisms; therefore, there are still questions about their utility in implementation (Convention on Biological Diversity (CBD) 2012).

6.1.2 Biological deterrents

To aid in minimizing biological impacts, there are also a number of tools and techniques that can be used to actively deter animals in an effort to minimize overlap with unwanted underwater sounds (OSPAR 2009a). Underwater biological deterrents have been used for a variety of applications to restrict animal movement. Commonly used methods include acoustic deterrent devices (ADDs), acoustic harassment devices (AHDs), visual deterrents (flashing lights), physical or electrical barriers (netting, electric field), and chemical deterrents (taste or smell deterrent) (NOAA 2015, 2016). These techniques have been effectively used to deter animals from pile-driving exclusion zones. Verfuss et al. (2016) reported that ADDs, such as pingers and seal scarers, effectively deter porpoises and seals from pile-driving exclusion zones in the UK. Limitations to biological deterrents include habituation, select number of target species, and animals may not respond if other "motivational" factors (e.g., food availability) are present (Verfuss et al. 2016).

6.1.3 Spatial and temporal restrictions

An effective management tool for mitigating the effects of underwater sound is establishing seasonal or spatial restrictions on operations (OSPAR 2009b; CBD 2012). Establishing "environmental windows" of operation are designed to eliminate sound exposures during periods where resident biota are at sensitive stages (e.g., breeding or spawning seasons; OSPAR 2009a; Todd et al. 2015). Some examples of seasonal restrictions include minimizing the overlap with susceptible activities such as mating, breeding, feeding, or migration. Spatial restrictions would include protecting ecologically sensitive areas (e.g., spawning sites, protected vegetation).

In the context of dredging operations, environmental windows are a common management practice that have been in use for decades to limit the environmental impacts of dredging (Reine et al. 1998; Suedel et al. 2008; Todd et al. 2015). Environmental windows for dredging operations are implemented for a variety of reasons to restrict environmental impacts for a variety of species and habitats. Although underwater sound has not been a primary driver for creating the existing temporal or spatial restrictions for dredging operations, the current restrictions likely provide concurrent mitigation of underwater sound. Clearly, there is a need to evaluate whether existing restrictions also provide mitigation of sounds associated with dredging.

6.2 Minimization

6.2.1 Acoustic damping

To date, the authors are unaware of any engineered acoustic damping techniques applied specifically for dredging operations. However, damping approaches have been developed to attenuate underwater sound from impulsive pile-driving and drilling sounds. These include enclosures (e.g., coffer dams, pile sleeves), air-bubble curtains, or engineered sound curtains (e.g., hydro sound dampers). A physical barrier can decrease sound by reflecting sound waves and impeding their path. Sound-damping materials that have demonstrated utility include air (coffer dams) or air-filled materials (e.g., foam sleeves; Nehls et al. 2007; ACCOBAMS 2013). Pile-driving field demonstration results indicate foam sleeves used on piles provided sound reduction by 10 and 20 dB at 1 kHz and 10 kHz, respectively (Nehls et al. 2007).

Bubble curtains are another method of sound reduction that have been used for the attenuation of a variety of impulsive sounds (e.g., pile driving, drilling; ACCOBAMS 2013). Typically, bubble curtains release air bubbles at the seafloor and are allowed to rise and encapsulate the sound source. Bubble curtains inhibit sound transmission by scattering, dissipating, and absorbing sound waves by resonating vibrating air bubbles (Wursig et al. 2000; Nehls et al. 2007). In general, the sound attenuation efficiencies of air bubbles are a function of the uniform distribution of consistent air bubble shapes. However, in practice, achieving a uniform distribution of free air bubbles in water is challenging due to varying ambient hydrodynamic conditions. Larger air bubbles with lower resonate frequency are more efficient at attenuating lower-frequency sounds (<1 KHz), but are relatively unstable and challenging to produce (Kuhn et al. 2012). Therefore, air bubble curtains are typically more efficient at attenuating higher frequency sounds (400-6,400 Hz; Wursig et al. 2000). Wursig et al. (2000) observed a 3-5 dB sound reduction in overall broadband frequencies, and up to 20 dB in the 1.6-6.4 kHz bands. In general, technical limitations of effectively implementing bubble curtains include achieving effective distribution around the sound source, maintaining a consistent distribution of bubble sizes, and the lack of sound mitigation at lower-range frequencies (<1 kHz) (Nehls et al. 2007; Kuhn et al. 2012).

Hydro sound dampers (HSDs) are an alternative method to bubble curtains. HSDs use small gas-filled bladders and robust polyethylene foam elements fixed to a fishnet "curtain" that surrounds a sound source. Measured sound reductions of 20-22 dB (broadband frequencies) HSDs have been achieved in wave flumes testing simulated pile-driving operations (Kuhn et al. 2012). Bruns et al. (2014) implemented HSDs during off-shore pile-driving construction activities to minimize the potential sound exposures to harbor porpoises and seals. During field demonstrations of HSD for off-shore pile driving, underwater sound reduction of up to 25 dB (SEL) was achieved (Bruns et al. 2014).

6.2.2 Equipment design or retrofit

Due to the recent focus on low-frequency sound generated by commercial shipping vessels, there is a growing international interest to incorporate sound reduction technology in ship design or retrofitting. The International Maritime Organization (IMO) (2014) released guidelines providing general sound reduction advice to ship designers, builders, and operators. Underwater sound from vessels is generally broken down into two main categories: propeller/thruster sound and machinery sound. Therefore, IMO design recommendations focused on three main areas that generate the majority of underwater sound: propellers, hull design, and onboard machinery. It should be recognized that the cost associated with equipment design and retrofit is strongly dependent on the ship design, operational parameters, and mandatory requirements that are ship and situation dependent (IMO 2014). In general, the cost of sound control treatment for a conventional marine vessel when incorporated into the design phase is approximately 1-3% of the vessel cost (Fisher and Pettit 2014). Alternatively, retrofits to existing vessels can cost up to 10 times greater as compared to incorporating the treatment technology earlier in the design phase (Fisher and Pettit 2014).

Propeller design considerations for sound reduction focus on decreasing the extent of cavitation (formation of water vapor cavities caused by pressure changes as water moves across a propeller blade; IMO 2014). Cavitation can be reduced by increasing uniformity in flow conditions around the propeller/thruster (Spence 2007). Design alterations to propeller diameter, blade number, pitch, skew, and sections can optimize the propeller load and provide a greater probability of uniform water flow into the propellers and less cavitation (IMO 2014; Nolet 2017). In addition, vessel hull design can be optimized to make the wake field propagating into the propeller more homogeneous to decrease cavitation (IMO 2014). However, technical or geometrical constraints may limit the design options (IMO 2014).

Onboard machinery—predominantly the main drive systems—also contribute to the overall sound budget of commercial shipping operations. For typical commercial vessels, vibration from power generation and propulsion equipment are major contributors to underwater sound (Spence 2007). A large proportion of vessel drive systems are diesel or diesel-electric engines. Vibration-damping devices can be used to decrease the overall sound of diesel engines (Nolet 2017), with both resilient mounts and "floating decks" used to isolate machinery vibration from the vessel's hull. Even with relatively simple designs, damping devices can reduce sound by 20 dB at 200 Hz (Spence 2007). In general, diesel electric engines produce less underwater sound than diesel engines, and diesel generators can be more effectively isolated with vibration-isolation devices (Nolet 2017).

The opportunity for achieving the greatest reduction in underwater sound is incorporating structural designs that mitigate sound during the design of new vessels. Sound reduction modifications to existing ships may prove to be economically impractical (IMO 2014). Modifications to existing ships that have shown a meaningful reduction in underwater sound include design and installation of modified propellers, installation of wakeconditioning devices, and installation of air injection to propellers (in ballast condition; IMO 2014).

Prior to investing in modifications to ship design, sound reduction modifications should be based on credible methods to clearly identify the primary source(s) of sound. With an increasing implementation of sound reduction engineering, there are a few classification societies (e.g., American Bureau of Shipping (ABS), Det Norske Veritas, Bureau Veritas) working with stakeholders establishing sound reduction classification systems to assist shipbuilders and operators in decision-making (Nolet 2017). Current gaps of information for implementing sound reduction technologies include lack of neutral testing facilities to validate manufacturing claims, relationship of sound reduction alterations to ship efficacy, and validation studies before and after sound control modifications are installed (ACCOBAMS 2013; Nolet 2017).

Examples exist in the navigation industry of organizations that have shown initiative to implement sound mitigation technology into ship design. For example, the Port of Vancouver recently established sound mitigation efforts associated with port activity (Brown 2016). The port authority established long-term sound-monitoring goals and identified specific mitigation efforts for underwater sound, including recognizing the use of "green vessel technology," changes to operational activities of vessels, recognition of certification programs for quiet vessels, and developing sound criteria for vessels entering the port (Brown 2016).

6.2.3 Equipment operation and maintenance

Alterations in operation and maintenance of existing equipment can also decrease underwater sound levels. For example, speed reduction is effective in decreasing sound for vessels equipped with fixed-pitch propellers and can be further decreased if the vessel drops below cavitation inception speeds (IMO 2014; Nolet 2017). For vessels with controllable pitch propellers, optimum combinations of shaft speed and propeller pitch can be used to decrease cavitation and sound (IMO 2014).

Cleaning propellers and underwater hull surfaces can also reduce underwater sound from commercial vessels. These maintenance activities decrease roughness and turbulence, thereby decreasing cavitation and vessel sound (IMO 2014). Additionally, onboard machinery is another source of vibration, and some consideration should be given to the selection, layout, and optimization that may contribute to reducing underwater sound (IMO 2014). An example layout may include "decoupling" equipment from the water surface to minimize underwater sound (Wursig et al. 2000). In terms of dredging-specific equipment, adequate maintenance of a dredge plant, including lubrication and repair of winches, generators, and propulsion components, could potentially mitigate underwater sound (WODA 2013). In relation to mitigating techniques for hopper dredges, Gerstein et al. (2006) suggested insulating and elevating the slurry pipeline (eliminating the contact with water) and minimizing the number and distance of transects from pump stations.

6.2.4 Reduction in operation power levels

Minimization of sound levels could be achieved by reducing the duration of a dredging or shipping activity or by limiting the number of times a system (e.g., propulsion) emits sound. Additionally, planning to use the lowest practical source of power to achieve the task could reduce sound levels (ACCOBAMS 2013). In the context of dredging, there would be a need to evaluate the relationship with operational power levels and underwater sound levels prior to altering operations to weigh cost versus benefit.

6.2.5 Alternate technologies

Using alternative technologies or strategies that have decreased sound risks may also be identified to achieve the same operational goals. This could include the strategic selection of "quieter" equipment or vessels for operation.

6.3 Summary

Techniques for mitigating underwater sound can be informed by a riskbased approach (Boyd et al. 2008; Thomsen et al. 2016). For simplicity, mitigation strategies that can alter the risks associated with underwater sound can be categorized into avoidance and minimization techniques. Avoidance includes the creation of exclusion zones or spatial or temporal restrictions (windows) to limit animal exposures. Minimization measures involve the deployment of biological deterrents and acoustic damping devices to minimize sound at the source. Retrofits and modifications to existing commercial vessels and improved designs of new vessels may offer the best prospects for reducing underwater sound produced by commercial vessels, including dredges. Sound minimization techniques used in practice include, for example, the reduction in power and use of alternative technologies to reduce sound at the source.

A critical aspect of any successful underwater sound risk framework is to identify and mitigate appropriate ecological risks and to avoid managing ecologically insignificant risks that would pose unnecessary constraints and costs on operations. If mitigation technologies are necessary to manage risks for dredging-induced sound, cost of implementation should be weighed against risk reduction to ensure practical and cost-efficient approaches are selected (i.e., cost versus benefit comparisons).

7 NOAA NMFS Marine Mammal Acoustic Technical Guidance

7.1 Overview

In July 2016, NOAA NMFS released the new technical guidance document for assessing the effects of anthropogenic sound on marine mammal hearing (NMFS 2016). Prior to this document, NMFS relied on generic acoustic threshold studies to assess the auditory impacts on marine mammals. In the 1990s, the Permanent Threshold Shift (PTS) for cetaceans was set at RMS SPL 180 dB and RMS SPL 190 dB for pinnipeds (NOAA 1998; HESS 1999). Due to lack of sound effects data at the time, NMFS set conservative and generic thresholds as single points of reference that could not account for the varied noise sources and hearing sensitivities of marine mammals. Since then, more comprehensive data sets for underwater sound effects on marine mammals have become available (Southall et al. 2007; Finneran 2015; Erbe et al. 2016). The improved understanding of acoustic thresholds allowed for a better evaluation of anthropogenic sound effects on marine mammals (Finneran and Jenkins 2012; NOAA 2014). The resulting information required a new comprehensive study of the current state of the science and the acoustic thresholds that were deemed sufficient to develop revised technical guidance.

The NMFS's 2016 technical guidance is a comprehensive review and study of peer-reviewed literature and government reports on the impacts of underwater sound on marine mammals. The technical guidance relied heavily upon the Finneran (2016) technical report "*Auditory Weighting Functions and TTS/PTS Exposure Functions for Marine Mammals Exposed to Underwater Noise*," which updated the underwater acoustic thresholds for TTS and PTS in marine mammals only. From the Finneran (2016) study, the NMFS updated the acoustic thresholds to a new standard to estimate PTS onset from all sound sources and use it to determine estimates for TTS from underwater impulsive and non-impulsive sounds. The NMFS 2016 acoustic thresholds are more complex than previous thresholds, but are more representative of the current scientific knowledge with regard to marine mammal hearing thresholds and potential responses to underwater sounds.

The purpose of the technical guidance was to provide NMFS analysts, managers, other action proponents and stakeholders (including other

federal agencies) the most current information for determining how their underwater activities are going to result in auditory impacts to marine mammals from acoustic exposure. Because of differences between the new weighting factors and single reference point values, the NMFS acknowledges that the approach provided makes general or direct comparisons between the updated acoustic thresholds and previous thresholds difficult. Also, NMFS acknowledges the new marine mammal weighting functions and SEL_{cum} metrics may be difficult to implement in practice. For this reason, NMFS developed a set of tools to incorporate these new metrics (this is addressed in Appendix D of the technical guidance and User Spreadsheet, both of which can be found at

http://www.nmfs.noaa.gov/pr/acoustics/guidelines.htm).

The technical guidance is not meant to represent the entirety of an effects analysis, but rather provide an additional tool to evaluate the adverse effects of underwater sound for marine mammals (NMFS 2016). Other sources of information that should be considered for a comprehensive risk assessment include behavioral impact thresholds, auditory masking assessments, and effects at the population level. NMFS indicates the technical guidance can be used as one line of evidence in the assessment of the proposed action and for input into the findings required by NOAA under relevant statutes (NMFS 2016).

7.2 Background information

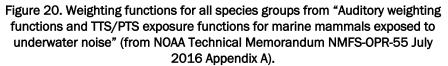
NOAA was tasked to provide

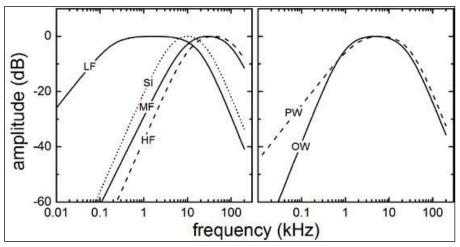
"...technical guidance for assessing the effects of underwater anthropogenic (human-made) sound on the hearing of marine mammal species under the jurisdiction of the National Marine Fisheries Service (NMFS) and was completed in collaboration with the National Ocean Service (NOS), Office of National Marine Sanctuaries. Specifically, it (the technical guidance document) identifies the received levels, or acoustic thresholds, at which individual marine mammals are predicted to experience changes in their hearing sensitivity (either temporary or permanent) for acute, incidental exposure to underwater anthropogenic sound sources."

This guidance was published in July 2016 (NMFS 2016).

This technical guidance used the newly available scientific information and provided a method for acoustic thresholds for onset of TTS and PTS in marine mammals. This guidance updated the methods used by NMFS and provided a framework to evaluate PTS onset caused by man-made impulsive and non-impulsive sound sources. The NMFS guidance focused on five marine mammal groups under NMFS jurisdiction (low- (LF): mid-(MF), and high- (HF) frequency cetaceans, and otariid (OW) and phocid (PW) pinnipeds). The technical guidance does not include sirenians or manatees; however, Finneran (2016) included the sirenians group.

Animals are not equally sensitive to sound at all frequencies; therefore, auditory weighting functions are used. For each marine mammal group, a frequency-dependent weighting function and threshold for TTS and PTS were derived from currently available data on the hearing abilities of and the noise effect on these groups (Figure 20). The parameters needed to calculate the weighting function amplitudes are displayed in Table 13.





$\left[\left(f/f\right)^{2a} \right]$			Non-impulsive Impulse								
$W(f) = C + 10\log_{10}\left\{\frac{(f/f_1)^{2a}}{\left[1 + (f/f_1)^2\right]^a \left[1 + (f/f_2)^2\right]^b}\right\}$			TTS threshold	PTS threshold		TTS eshold		PTS reshold			
Group	а	b	f <u>1</u>	f2	С	SEL	SEL	SEL	peak SPL (unweighted)	SEL	peak SPL (unweighted)
LF	1	2	0.20	19	0.13	179	199	168	213	183	219
MF	1.6	2	8.8	110	1.20	178	198	170	224	185	230
HF	1.8	2	12	140	1.36	153	173	140	196	155	202
SI	1.8	2	4.3	25	2.62	186	206	175	220	190	226
OW	2	2	0.94	25	0.64	199	219	188	226	203	232
PW	1	2	1.9	30	0.75	181	201	170	212	185	218

Table 13. Summary of weighting function parameters and TTS/PTS thresholds. SEL thresholds are in dB re 1 µPa²s and peak SPL thresholds are in dB re 1 µPa (from NOAA Technical Memorandum NMFS-OPR-55 July 2016 Appendix A).

Each group of marine mammals had frequency-dependent weighting functions and numeric thresholds for TTS and PTS onset, which was determined from the available data. The auditory weighting functions are based on a generic band-pass filter described by Equation 4:

$$W(f) = C + 10 \log_{10} \left\{ \frac{\binom{f}{f_1}^{2a}}{\left[1 + \binom{f}{f_1}^2\right]^a \left[1 + \binom{f}{f_2}^2\right]^b} \right\}$$
(4)

where, W(f) is the weighting function amplitude (in dB) at the frequency f (in kHz). The shape of the filter is defined by the parameters C, f_1 , f_2 , a, and b:

- C = weighting function gain (dB). The value of "C" defines the vertical position of the curve. Changing the value of C shifts the function up/down. The value of C is often chosen to set the maximum amplitude of W to 0 dB (i.e., the value of C does not necessarily equal the peak amplitude of the curve).
- f1 = low-frequency cutoff (kHz). The value of "f1" defines the lower limit of the filter pass-band; i.e., the lower frequency at which the weighting function amplitude begins to decline or "roll-off" from the flat, central portion of the curve. The specific

amplitude at *f*1 depends on the value of *a*. Decreasing *f*1 will enlarge the pass-band of the function (the flat, central portion of the curve).

- $f_2 = high-frequency\ cutoff\ (kHz)$. The value of " f_2 " defines the upper limit of the filter pass-band; i.e., the upper frequency at which the weighting function amplitude begins to roll off from the flat, central portion of the curve. The amplitude at f_2 depends on the value of b. Increasing f_2 will enlarge the pass-band of the function.
- a = low-frequency exponent (dimensionless). The value of "a" defines the rate at which the weighting function amplitude declines with frequency at the lower frequencies. As frequency decreases, the change in weighting function amplitude becomes linear with the logarithm of frequency, with a slope of 20*a* dB/decade. Larger values of *a* result in lower amplitudes at *f*1 and steeper roll-offs at frequencies below *f*1.
- *b* = *high-frequency exponent* (dimensionless). The value of "*b*" defines the rate at which the weighting function amplitude declines with frequency at the upper frequencies. As frequency increases, the change in weighting function amplitude becomes linear with the logarithm of frequency, with a slope of -20b dB/decade. Larger values of b result in lower amplitudes at *f*2 and steeper roll-offs at frequencies above *f*2.

7.3 Technical guidelines for marine mammals

For the development of PTS and TTS thresholds, NMFS divided sound sources into two categories: impulsive and non-impulsive. The NOAA technical guidance used the following definitions:

- Impulsive: produce sounds that are typically transient, brief (less than 1 s), broadband, and consist of high-peak sound pressure with rapid rise time and rapid decay (ANSI 1986; National Institute for Occupational Safety and Health (NIOSH) 1998; ANSI 2005).
- Non-impulsive: produce sounds that can be broadband, narrowband, or tonal, brief or prolonged, continuous or intermittent) and typically do not have a high-peak sound pressure with rapid rise/decay time that impulsive sounds do (ANSI 1995; NIOSH 1998).

Sound sources such as sonars and vibratory pile drivers would therefore be considered non-impulsive, while explosives, impact pile drivers, and air guns would be considered impulsive. Harmonic signals or sounds with duration greater than 5 to 10 cycles were generally considered to be steady state. Based on these definitions, while it is possible that dredges could emit impulsive sounds (e.g., hard-bottom strike from bucket or backhoe dredges); the vast majority of dredge-related sounds would be considered non-impulsive (e.g., marine vessels, engines, pumps, etc.), according to this definition.

Because there is a frequency-dependent nature to the effect of sound, auditory weighting functions were used to account for frequency hearing sensitivities of marine mammals. The auditory weighting function is a mathematical function used to emphasize marine mammal-sensitive sound frequencies. A function-dependent filter (i.e., the frequency where weighting function amplitude begins to decline from the flat, central portion of the function) is applied to a sound level before a single, weighted sound exposure level (SEL) is calculated. This weighting function is a "band-pass" type filter that resembles an inverted "U" when plotted versus frequency (see Figure 20 as an example). The weighting function is essentially flat over a limited range of frequencies, called the "pass-band," and drops off at frequencies above and below the "pass-band."

By comparison, auditory weighting functions for humans are based on equal loudness contours in a human listener. Equal loudness contours are defined as curves that show the combination of SPL over the frequency spectrum that results in a sensation of constant loudness when presented as a pure tone. For humans, NMFS created equal loudness contours from data collected during loudness comparison tasks (i.e., feedback during auditory tasks). But these data were difficult to collect from non-verbal animals; therefore, equal loudness contours were only available for a single marine mammal (a dolphin) and only for a limited range (2.5 -113 kHz). A substitute used for these loudness comparison tasks was to measure reaction times to tones and correlated behavioral responses to subjective loudness. From these, reaction time versus SPL curves of equal response latency were created and used to give an approximate equal loudness curve.

The Equal Energy Hypothesis (EEH) is one assumption that NMFS made when applying the SEL_{cum} metric. It assumes that sounds of equal SEL_{cum} produce equal risk for hearing loss (i.e., short-duration sounds with a higher energy level would have a similar risk as a longer duration sound with a lower energy). Henderson et al. (1991) showed this to be the case in humans and terrestrial mammals, but the EEH does not always accurately describe the exposure situations for marine mammals due to the inherent complexity of predicting threshold shifts (e.g., Kastak et al. 2007; Mooney et al. 2009a; Mooney et al. 2009b; Finneran et al. 2010a; Finneran et al. 2010b; Finneran and Schlundt 2010; Kastelein et al. 2012; Kastelein et al. 2013b; Kastelein et al. 2014; Popov et al. 2014).

The factors associated with TS-like sound level (i.e., sensation level, overall level, and level above background), the duration, duty cycle (intermittent or continuous), number of transient components, and frequency of sound are all important considerations (e.g., Buck et al. 1984; Clark et al. 1987; Ward 1991; Lataye and Campo 1996). This is especially the case for exposure to impulsive sound sources (Danielson et al. 1991; Henderson et al. 1991; Hamernik et al. 2003), which is why acoustic thresholds in this technical guidance are also expressed as a Peak SPL Metric (PK). In most cases, the EEH method gives a good first-order approximation, especially for the higher-level, short duration sound exposures, such as those that are most likely to result in TTS for marine mammals (Finneran 2015).

For terrestrial mammals, impulsive sounds can have a greater risk of causing direct mechanical fatigue to the inner ear compared to sounds that are strictly non-impulsive (Henderson and Hamernik 1986; Levine et al. 1998; Henderson et al. 2008). The risk of damage from impulsive (transient) sounds usually does not depend on the duration of the exposure. This concept of "critical level" (where the damage switches from primarily metabolic to more mechanical and short-duration impulses can be less than the ear's integration time) leading to the potential to damage beyond the level the ear can perceive (Akay 1978).

Industrial noise standards for humans recognize and provide for separate acoustic thresholds for impulsive sound sources using the PK metric (Occupational Safety and Health Administration; OSHA 2013; 29 CFR 1910.95; Starck et al. 2003). Due to this, Sel_{cum} is not the appropriate metric to use for all the effects of impulsive sounds (National Institute for Occupational Safety and Health [NIOSH] 1998), which is why the instantaneous PK level has also been included as part of the NMFS's dual metric for threshold of impulsive sounds. Auditory weighting is not used with the PK threshold as the direct mechanical damage associated with

high peak sound pressures typically does not strictly reflect the frequencies an individual species hears best (Ward 1962; Saunders et al. 1985; ANSI 1986; DOD 2004; OSHA 2013; 29 CFR 1910.95). Thus, the NMFS (2016) guidance recommends that the PK thresholds should be unweighted/flatweighted within the entire frequency band of a hearing group. It should be noted that for non-impulsive sounds, the SEL_{cum} threshold will likely result in the largest isopleth (delineation of area from source) as compared to the PK threshold. So, for the majority of non-impulsive sounds, the PK threshold is considered unnecessary. However, if the non-impulsive sound has the potential of exceeding the PK threshold associated with impulsive sounds, these thresholds should be considered (i.e., using dual metrics.)

For the development of the NMFS auditory-weighted functions, marine mammals were divided into six hearing groups. For each group, a frequency-dependent weighting function and threshold for onset of TTS and PTS were derived from the available data on hearing abilities and effects of sound on these marine mammals. Available measured or predicted auditory threshold data and equal latency contours were used to create the weighting function curves for each of the groups. Marine mammal groups with measured TTS data were used to adjust the weighting function parameters to provide the best fit to the experimental data. This method was then applied to weighting functions of the other marine mammal groups that did not have measured TTS data. This methodology was used to develop the updated NMFS auditory weighted functions used to predict auditory thresholds for select marine mammals.

The NMFS auditory guidelines were not specifically targeting dredging. The study was assessing the ranges of the marine mammal hearing and what levels of anthropogenic sounds generated from human activities could adversely impact the hearing of select marine mammal groups. The NMFS guidance is intended to develop acoustic thresholds for assessing the effects of anthropogenic underwater sound on marine mammals. The potential uses and implications for dredging-related activities are discussed below.

7.4 Implication to dredging-induced underwater sound

The NMFS (2016) technical guidance document does not identify or address dredging sounds. Instead, the technical guidance document focused on a number of other anthropogenic sound activities; for example, pile driving, airguns, and tactical sonar. The majority of dredging occurs in the relatively shallow water depths (< 20 m) of coastal waterways and is performed by hydraulic and mechanical dredges. These shallow-water coastal areas are dynamic environments with a variety of bottom habitats as well as many types of ambient and anthropogenic sound sources; therefore, estimations of received sound levels should be made with caution. Considerations of how the NMFS (2016) technical guidance relates to dredging-related sounds, data limitations, and uncertainties are outlined below.

7.4.1 Acoustic terminology – application to dredging sounds

The sound thresholds proposed in the NMFS technical guidance are organized into two broad categories: (1) impulsive and (2) non-impulsive sounds. The acoustic metrics chosen for impulsive sound thresholds include peak SPL (SPL_{peak}; 1 μ Pa) and cumulative SEL (SEL_{cum}; 1 μ Pa²s). These are defined as "dual" metrics, meaning that NMFS considered onset of PTS to occur if either metric is exceeded. For non-impulsive sounds, the single metric SEL_{cum} (1 μ Pa²s) is used. The updated NMFS (2016) guidance eliminated the use of a single exposure metric (SPL_{rms}) for non-impulsive sounds, and relies exclusively on a time-integrated exposure metric SEL_{cum}.

To date, the primary metric used to describe dredging sounds have been the SPL_{rms} metric (Dickerson et al. 2001; Clarke et al. 2002; Reine et al. 2012; Reine et al. 2014), which are not directly comparable to either of the NOAA sound threshold metrics (SPL_{peak} or SEL_{cum}). Efforts are underway to establish standardized methods for measuring and reporting sounds related to dredging activities, but to date no single method has been adopted (Jones and Marten 2016). The SELcum metric has duration incorporated (1 µPa²s), and therefore is not directly comparable to other metrics that compare SELs (1 μ Pa; NMFS 2016) and cannot be converted to SEL_{rms} with any reliability. Since there is no direct conversion between SPL_{rms} and SEL_{cum}, it is difficult to know what SEL would be generated by dredging activities; therefore, it is unclear if dredging would exceed the proposed PTS thresholds for non-impulsive sounds. Additionally, the NMFS intends for the SEL_{cum} metric to account for the accumulated exposure within a twenty-four-hour period. For dredging and other sources of anthropogenic noise, NOAA does not address how a 24-hour exposure criterion could be measured or applied by considering intermittent periods of no sound production. Dredge-related sounds are often intermittent due to stoppages for crew changes, placement transit, maintenance of equipment, and/or breakdowns. Additionally, dredging

activities have diverse sound characteristics occurring over various spatial and temporal scales. The NMFS guidelines state:

"The recommended application of the SEL_{cum} metric is for individual activities/sources. It is not intended for accumulating sound exposure from multiple activities occurring within the same area or over the same time or to estimate the impacts of those exposures to an animal occurring over various spatial or temporal scales. Current data available for deriving acoustic thresholds using this metric are based on exposure to only a single source and may not be appropriate for situations where exposure to multiple sources is occurring." (page 28; NMFS 2016). For this reason, the methodology proposed in the NOAA guidance is not applicable to operating dredges where multiple sounds are being generated from various components of the dredge (e.g., propeller, drag arm, etc.) that are acting in concert, producing an overall continuous, non-impulsive sound source.

It should be noted that "effective quiet" is the maximum SPL that will fail to produce any significant auditory threshold shift despite the duration of accumulation (Ward et al. 1976; NMFS 2016). This should be considered when estimating SEL_{cum} so that risk expectations are managed. For example, low SPLs with sufficiently long durations could theoretically accumulate to exceed SEL_{cum} acoustic thresholds, when the actual or likely risk is extremely low (e.g., humans exposed to normal conversation dB levels every day are not subjected to greater risk of TTS onset; NMFS 2016; p.122).

7.4.2 Uncertainty and data limitations

NMFS (2016) recognizes the inherent data limitations for establishing effects thresholds, including a limited number of species, individuals within a species, and the presence of multiple concurrent sound sources. Broad data limitations for the development of the NMFS guidelines include the following:

- No direct measurements of marine mammal PTS have been published. PTSs have been derived from mathematical models, TTS is used to extrapolate onset of PTS;
- Estimations of PTS are based on very limited TTS data within each hearing functional group;

- Existing use of "representative" surrogate individuals for establishing PTS onset thresholds for species where limited (or no) data exist (e.g., LF cetaceans); and
- Hearing sensitivity can vary among individuals within the same species based on a variety of parameters (e.g., age, previous exposure, etc.).

Currently, TSS measurements exist for four species of cetaceans (bottlenose dolphins, belugas, harbor porpoises, and Yangtze finless porpoises) and three species of pinnipeds (northern elephant seal, harbor seal, and California sea lion). Due to the absence of LF cetacean audiogram data, multiple assumptions were made to estimate TS onset. For these reasons, NOAA incorporated a broader weighting/ exposure function than any other functional hearing group to account for the inherent uncertainty associated with these estimates.

NMFS recognizes the limitations of the available data for the development of certain aspects of the criteria; therefore, re-evaluations of effects thresholds will be conducted as new data become available. NMFS expects to update the effects thresholds every 3 to 5 years to incorporate new data and methods. NMFS (2016) indicates that the authors of Southall et al. (2007) are preparing an updated publication of the original "Marine Mammal Noise Exposure Criteria: Initial Scientific Recommendations." If alternative methods are proposed by Southall et al. for predicting lowfrequency cetaceans, the NMFS are likely to re-evaluate the methodology to be applied to additional receptors (e.g., other marine mammals and fish) and other anthropogenic sound sources.

As the understanding of effects of underwater sound improves, it is anticipated that acoustic thresholds are going to become more complex; and likely more challenging for implementation (NMFS 2016). For example, prior NMFS guidance relied on only two generic marine mammal auditory effects thresholds, SPL RMS 180 and 190 dB for cetaceans and pinnipeds, respectively. Clearly, more complex sound effects thresholds need to be balanced with practical application (cost versus benefit) to aid in proper implementation by users (e.g., action proponents, managers, etc.; NMFS 2016). It should be noted that standardization of measurement parameters and protocols has been identified as a critical need by the international scientific community engaged in underwater sound research. Until such standardization has been sufficiently developed to be implementable, it will remain difficult—if not impossible—to establish criteria sufficiently robust to be site- and activity-specific.

7.5 Summary

The NMFS (2016) technical guidance document does not specifically address dredging-related sounds and the proposed thresholds are not broadly applicable to navigation dredging. The NMFS (2016) technical guidance states that it is not meant to represent the entirety of an effects analysis; rather, it should provide an additional tool to aid in evaluating the adverse effects of underwater sound for marine mammals (NMFS 2016). In terms of evaluating risks associated with underwater sound for site-specific activities, the technical guidance recommends the use of effects thresholds to be used in conjunction with site-specific characterization. NMFS site parameter recommendations include characterization of the sound source, environmental site conditions that influence sound propagation, and marine mammal occurrence and behavior near the sound activity (e.g., species, density, occurrence, etc.). NMFS acknowledges that alternative approaches may be used if sitespecific information or data indicate it can produce a more accurate estimation of auditory risk. Alternative approaches that have been subjected to independent peer review may be proposed by federal agencies or prospective action proponents if the approach demonstrates it is "likely to produce a more accurate estimate of auditory impact for the project being evaluated" (NMFS 2016). The scope of the NMFS (2016) guidelines limits their applicability for addressing dredge-related sounds due to the limitations in comparable sound exposure metrics and acoustical exposure considerations. Alternatively, a risk-based approach specific to dredginginduced sounds is needed to sufficiently understand the potential ecological risks to effectively apply such threshold limits in practice.

8 Summary and Path Forward

This literature review was needed to develop an improved understanding about underwater dredging sound effects on aquatic life. Underwater sound from natural and anthropogenic sources are composed of many frequencies and amplitudes, which produce a combination of acoustic waves that can be disordered or random and difficult to spatially quantify. The sound pressure levels (SPLs) in decibels (dB) are commonly used to quantify underwater sounds. SPLs are typically specified in metrics referring to the acoustical properties. Common examples include rootmean-square (RMS), peak-to-peak, or frequency bands (1/3 octave analysis or Hz range). Due to the diversity of acoustic metrics, it is critical to use caution when comparing reported sound levels across studies. Additionally, it is crucial to understanding the differences between sound source levels and organism-received levels (the latter is dependent on the sound source characteristics and the sound propagation in the aquatic environment, and the receptor sensitivity).

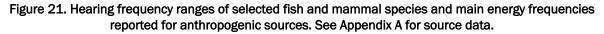
Dredge-induced underwater sounds are temporally and spatially dynamic, and dependent on site-specific activities and conditions. Dredging produces predominantly low-frequency (<1,000 Hz; Figure 21) sounds that are typically continuous and non-impulsive (e.g., do not exhibit a rapid sound pressure rise time and decay). A notable exception is during blasting activities when rock and other hard substrata need to be removed in ship channels to ensure navigation safety. Dredging sounds are comparatively lower intensities in contrast to other activities (e.g., explosions, pile driving, seismic airguns, echosounders, and large ships). It should be noted that the acoustical characteristics are often summarized as single maximum recorded values near the sound source (i.e., 1 m from the source). Additionally, a single sound event (e.g., propeller cavitation) can skew the calculated SPLs (RMS) and may not provide an accurate representation of the sounds being generated by a dredging operation.

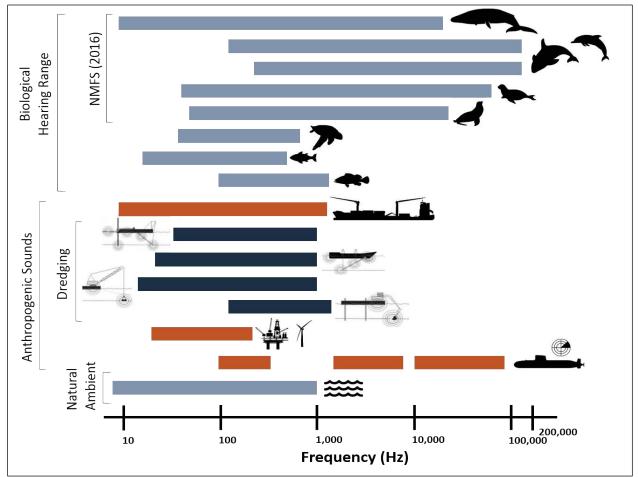
Based on the review results of existing effects data, direct mechanical injury and mortality in aquatic species following underwater sound exposures are limited to high-intensity impulsive sounds (e.g., explosions, pile driving). The currently available effects data from anthropogenic sources indicate that dredging-induced sounds do not pose a significant risk to direct injury or mortality to aquatic biota. In terms of potential non-lethal responses, low-frequency sounds produced by dredging activities overlap with the hearing frequency ranges of select fish and mammal species; this may pose risks for auditory temporary threshold shifts, auditory masking, and behavioral responses. Overall, there has been significant progress in the understanding of the characteristics of dredgerelated sounds in the last couple of decades. Although there are gaps of exposure-response data for dredging-induced sounds, in general there is no direct evidence of lethal effects to aquatic biota, and few data indicating that non-lethal effects (e.g., behavioral) are pervasive.

A critical aspect of any successful underwater sound risk framework is to identify and mitigate appropriate ecological risks, and to avoid managing ecologically insignificant risks that would pose unnecessary constraints and costs on operations. Mitigation strategies to manage risks of underwater sound effects on aquatic biota generally include avoidance and minimization. Prior to the application of mitigation technologies, cost of implementation should be weighed against risk reduction to ensure practical and cost-efficient approaches are selected (i.e., cost versus benefit comparisons).

Recently updated technical guidelines have been developed by the NMFS (2016) that proposed acoustic exposure criteria for select classes of marine mammals (NMFS 2016). The NMFS technical guidance document does not specifically address dredging-related sounds and the proposed exposure criteria are not broadly applicable to dredging. In terms of evaluating risks associated with underwater sound for site-specific activities, the technical guidance recommends the use of effects thresholds to be used with site-specific characteristics such as the sound source, environmental site conditions that influence sound propagation, and marine mammal occurrence and behavior near the sound activity (e.g., species, density, occurrence, etc.). NMFS acknowledges that alternative approaches may be used if site-specific information or data indicate it can produce a more accurate estimation of auditory risk.

To improve understanding of the ecological risks associated with dredging sounds, a risk-based approach is needed that maximizes the data and other site-specific information to evaluate the underwater sound of concern. Additional study is needed to improve our understanding of whether the updated thresholds developed by NOAA indicate potential risks during dredging rock-blasting activities and whether the thresholds are relevant to dredging in coastal waterways. Overall, the information reported herein regarding underwater sound produced by dredging can be used in an exposure assessment as part of a broader framework for assessing and managing underwater sound effects on aquatic life.





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Appendix A

			Estimated Hearing Range Frequency (Hz)		
Species/ Group	Common Name	Scientific Name	min	max	Reference
Low-frequency (LF) cetaceans	Baleen whales	-	7	35,000	NMFS 2016 ^a
Mid-frequency (MF) cetaceans	dolphins, toothed whales, beaked whales, bottlenose whales	-	150	160,000	NMFS 2016ª
High-frequency (HF) cetaceans	true porpoises, Kogia, river dolphins, cephalorphynchid sp., hourglass dolphin & Peale's dolphin	, - chid sp., - phin &		160,000	NMFS 2016ª
Phocid pinnipeds (PW)	true seals	-	50	86,000	NMFS 2016 ^a
Otariid pinnipeds (OW)	sea lions and fur seals	-	60	39,000	NMFS 2016 ^a
Chelonians	Loggerhead turtle	Caretta caretta	50	900	Ketten and Bartol 2006; Martin et al. 2012
Chelonians	Green turtle	Chelonia mydas	100	800	Ketten and Bartol 2006
Chelonians	Kemp Ridley	Lepidochelys kempi	100	500	Ketten and Bartol 2006
Chelonians	red-eared slider	Trachemys scripta elegans	400	500	Christensen- Dalsgaard et al. 2012
Teleosts	Brown meagre	Sciaena umbra	100	3,000	Codarin et al. 2009
Teleosts	Mojorra	Eucinostomus argenteus	100	1,800	Parmentier et al. 2011
Teleosts	Oyster toadfish	Opsanus tau	100	800	Yan 2001
Teleosts	Red-mouthed goby	Gobius cruentatus	100	700	Codarin et al. 2009
Teleosts	Mediterranean damselfish	Chromis chromis	100	600	Codarin et al. 2009
Teleosts	Atlantic codfish	Gadus morhua	10	600	Offutt 1974

Table A1. Estimated hearing frequencies of aquatic biota.

^aNMFS (2016); represents generalized hearing range for species category as a composite; Table ES1; p. 3 (NMFS 2016).

	Main Energ	y Frequency		
	Rang	ge (Hz)		
Sound Source	min max		Reference	
Natural Ambient Conditions ^a	10	1,000	Wenz, 1962; NRC, 2003	
Shipping	10	1,000	NRC, 2003; McKenna et al. 2012	
Dredging - CSD	20	1,000	Reine et al. 2012b; Reine and Dickerson 2014	
Dredging - TSHD	30	1,000	de Jong et al. 2010	
Dredging - GD	20	1,000	Dickerson et al. 2001	
Dredging - BHD	130	1,250	Reine et al. 2012a	
Oil and gas drilling	10	100	OSPAR 2009a; Blackwell and Green 2003	
Wind turbine	30	200	OSPAR 2009a	
Military sonar (low-frequency)	100	500	OSPAR 2009a	
Military sonar (mid-frequency)	2,800	8,200	OSPAR 2009a	
Military sonar (high frequency)	10,000	15,500	Cox et al. 2006	

^asurface waves, precipitation, prevailing winds, surface agitation

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activities such biological effe dredging activ pose a signific used to remov produced by d temporary three sounds, a risk- underwater son assessing and 15. SUBJECT Aquatic spece framework	noment, there m as the excavatio ects of underwate ities. Effects dat ant risk of direct e rock and other redging overlap eshold shifts, auc based approach und. Overall, the managing under TERMS cies, DOER, dr	n, transit, and p r sound from d a generated from injury or mort hard substrata with the hearin litory masking, is needed that u information re water sound eff	placement of material redging and other ant m exposures to anthro ality to aquatic biota. in navigation channel g frequency ranges of and behavioral respo tilizes the available d ported herein can be ects on aquatic life.	generate underwa hropogenic source opogenic sound so A notable exception s. In terms of pote E select fish and manual nses. To better und lata and other site- used in an exposur- y sonar, pile driv	ter sound es to help urces indi on, and m ntial non- ammal sp derstand t specific in re assessm ving, und	and anthropogenic sources. Dredging . This report documents research into the evaluate the potential ecological risks of cate that dredging-induced sounds do not uch less common, is blasting activities lethal responses, low-frequency sounds ecies, which may pose risks for auditory he ecological risk associated with dredging nformation appropriate for evaluating nent as part of a broader framework for			
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