

Experimental characterization of the COndensation PArTicle counting System for high altitude aircraft-borne application

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Abstract. A characterization of the ultra-fine aerosol particle counter COPAS (COndensation PArTicle counting System) for operation on board the Russian high altitude research aircraft M-55 Geophysika is presented. The COPAS instrument consists of an aerosol inlet and two dual-channel continuous flow Condensation Particle Counters (CPCs) operated with the chlorofluorocarbon FC-43. It operates at pressures between 400 and 50 hPa for aerosol detection in the particle diameter (d_p) range from 6 nm up to 1 μ m. The aerosol inlet, designed for the M-55, is characterized with respect to aspiration, transmission, and transport losses. The experimental characterization of counting efficiencies of three CPCs yields d_{p50} (50% detection particle diameter) of 6 nm, 11 nm, and 15 nm at temperature differences (ΔT) between saturator and condenser of 17°C, 30°C, and 33°C, respectively. Non-volatile particles are quantified with a fourth CPC, with $d_{p50}=11$ nm. It includes an aerosol heating line (250°C) to evaporate H₂SO₄-H₂O particles of 11 nm < d_p < 200 nm at pressures between 70 and 300 hPa. An instrumental in-flight inter-comparison of the different COPAS CPCs yields correlation coefficients of 0.996 and 0.985. The particle emission index for the M-55 in the range of 1.4–8.4 × 10¹⁶ kg⁻¹ fuel burned has been estimated based on measurements of the Geophysika's own exhaust.

1 Introduction

In-situ measurements of fine aerosol particles ($d_p < 1000$ nm) from high-altitude aircraft are essential for studies concerning the atmospheric radiative budget, stratospheric chemistry, aerosol processes of the tropical tropopause region, polar stratospheric cloud (PSC) microphysics, as well as for comparisons with ground based or satellite borne remote sensors. Stratospheric aerosol particles scatter solar radiation and these particles exert a significant influence on the stratosphere's radiation budget and on the Earth's planetary albedo, especially after volcanic injections (Hamill et al., 1997, and references therein). Another important objective of investigations is to determine the quantitative and qualitative contribution of aerosol particles to chemical transformation processes in the stratosphere. The particles provide the essential surfaces for important chemical reactions (Prather and Rodriguez, 1988; Peter, 1997). For example, stratospheric aerosol particles play a significant role in heterogeneous processes forming reactive chemical species which are known to participate in ozone depletion (Wennberg, et al., 1994; Murphy and Ravishankara, 1994; Carslaw et al., 1994; Peter, 1997; Borrmann et al., 1997; Voigt et al., 2000, 2003).

A major fraction of the stratospheric aerosol is assumed to consist of ~75-weight-percent solution of sulfuric acid and water (H₂SO₄/H₂O) (Rosen, 1971; Arnold et al., 1998; Murphy et al., 2007). Besides H₂SO₄ and H₂O, also refractory compounds are found in stratospheric particles, such as soot (or other refractory carbonaceous material), meteoric material, and volcanic ashes (Turco et al., 1982; Murphy et al.,



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1998, 2007; Cziczo, 2001; Curtius et al., 2005). Particularly the refractory material might have a significant impact on various processes such as PSC activation in the polar winter vortex (Peter, 1997; Murphy et al., 1998, 2007; Curtius et al., 2005; Voigt et al., 2005).

Since 2002, the University of Mainz and the Max Planck Institute for Chemistry in Mainz (Germany) developed and operated two separate units of aircraft-borne dual-channel condensation particle counters (CPCs), the **CO**ndensation **PA**rticle counting **S**ystems (COPAS), on board the high altitude research aircraft M-55 Geophysika (<http://emz-m.ru/M55-e.htm>). This study provides a detailed description and comprehensive characterization of the CPCs counting efficiency and other critical instrument parameters at the relevant atmospheric conditions. The characterization also includes coincidence studies (miscounting two or more individual particles as only one in the detector), as the coincidence effect is strongly dependent on the individual CPC design. Also subject of the experiments was to characterize the vaporizing properties of the aerosol pre-heating device. Furthermore, a limited number of flight measurements are used for a reliability study, to demonstrate the instrumental performance and the limits of the COPAS operation, particularly with respect to the flight altitude. Finally, two crossings of the M-55's own exhaust at altitudes of 16–18 km were used to provide an order of magnitude estimate of the particle emission index of the M-55.

2 Details of the instrumental design

The COPAS instrument was originally based on a CPC design developed by the University of Denver (USA) for measurements on board the NASA ER-2 (Wilson et al., 1983a, b). The terminus of two dual-channel CPCs is used in this study to refer to the two independent units, each containing two coupled CPCs. For technical reason the two CPCs of a unit are thermally coupled by a common heat sink and both CPCs of a unit sample from a common aerosol inlet, but there is an independent aerosol inlet for each unit.

The information from the four CPC channels is used to obtain a) the total number concentration of particles with diameters >11 nm, b) the number concentration of ultra-fine particles (with diameters $6 \text{ nm} < d_p < 15 \text{ nm}$) by operating two CPCs with different temperatures of the saturator and the condenser, and c) the concentration of stratospheric aerosol particles with temperature-stable cores >11 nm diameter by using an aerosol heating line upstream of one COPAS channel. The particle fraction which remains after passing the heated (250°C) aerosol line is specified to be non-volatile with respect to 250°C in the following.

The two almost identical units of the dual-channel COPAS are positioned at different locations on board of the M-55, one in an instrument bay that is part of the main body of the aircraft and one in a bay under the left wing. The independent

measurements of the disjunct units also provide possibilities to cross-check and verify the data from the different channels and from the often redundant information additional reliability of the data is assured.

The COPAS CPCs are thermo-diffusion-type counters (Rosen et al., 1974; Sinclair and Hoopes, 1975; Wilson et al., 1983a, b; Stolzenburg and McMurry, 1991) which are usually operated with butanol ($\text{C}_4\text{H}_9\text{OH}$) or FluorInert FC-43 ($(\text{C}_4\text{F}_9)_3\text{N}$), a commercially available fluorocarbon, as working fluids. The process of thermo-diffusion in the condenser volume leads to supersaturation followed by particle growth up to sizes at which the particles are sufficiently large to be optically detected. To allow for continuous sampling with a frequency ~ 1 Hz and precise measurements at particle concentrations $<100 \text{ cm}^{-3}$, this working principle is used for COPAS instead of expansion-type CPCs (e.g. Kürten et al., 2005).

The d_{p50} characterizing a CPC is defined as the particle diameter for which

$$d_{p50} = \frac{n_{\text{det}}(d_p)}{n_{\text{real}}(d_p)} = 0.5, \quad (1)$$

here $n_{\text{det}}(d_p)$ is the detected number concentration of monodisperse particles of size d_p and $n_{\text{real}}(d_p)$ is the real number concentration. Commercially available CPCs usually have a d_{p50} between 2.5 and 20 nm. CPCs used on research aircraft in the past typically had d_{p50} of 3–10 nm (Wilson et al., 1983b; Dreiling and Jaenicke, 1988; Brock et al., 1995; Hermann and Wiedensohler, 2001; Minikin et al., 2003). Reviews on the general designs and the development of different types of CPCs are available from McMurry (2000) and Spurny (2000).

The COPAS operation principle with actively controlled volumetric sample air flow is shown in Fig. 1. Each dual channel COPAS is equipped with one aerosol inlet. The incoming airflow is split into two equal CPC flows. In each CPC channel, the incoming airflow is split again into two subflows. The major part of the flow ($\sim 90\%$) is cleaned from aerosol particles by a total aerosol filter. Subsequently, the cleaned air becomes saturated with the vapor of the working liquid in the saturator chamber in which a constant temperature is maintained (COPAS-I: both channels 32°C ; COPAS-II: 24°C and 40°C for channel one and two, respectively). The remaining fraction of the incoming air ($\sim 10\%$) is the sample flow which carries the aerosol particles. This flow passes a capillary with a nozzle-shaped tip. At the exit of this capillary the two subflows – the sample flow and the particle-free, saturated air – are merged again. The saturated airflow now acts as a sheath flow which focuses the sample flow into the condenser and thus helps to avoid particle losses due to turbulences, diffusion, and thermophoretic effects (Wilson et al., 1983b). In the condenser the total air flow is cooled to temperatures of 2°C (COPAS-I) and 7°C (COPAS-II) leading to a supersaturation of the working fluid vapor. This supersaturation drives the growth of the aerosol particles to sizes

that are detectable by a suitable photo-optical sensor which is comparable to the detector of the CPC TSI model 3760 (TSI Incorporated, 2002).

The total flow rates of the COPAS units are monitored by use of differential pressure sensors at the sample flow capillary and the common exhaust line for both CPCs (cf. Fig. 1). The automated flow regulation (with 10 Hz integration loop frequency) of each COPAS instrument controls the air pump frequency (and therefore the flow rate of both CPCs of one COPAS) according to settings which can be described by the linear relation $y=a \cdot x+b$ of total standard volume flow rate (y) in $\text{cm}^3 \text{min}^{-1}$ as a function of ambient pressure (x) in hPa with the parameters for COPAS-I: $a=2.09$, $b=40.60$ and COPAS-II: $a=2.23$, $b=36.56$. The automated flow regulation generally works within an accuracy range of $\pm 15\%$. However, if ascent and descent rates of the airborne platform significantly exceed 10 m s^{-1} the differential pressure measurement shows disturbances, probably caused by turbulent flow conditions within the flow measurement volume. Irregular flow measurements have direct influence on the air flow regulation and therefore on the instrumental performance (cf. Sect. 8).

The differential pressure measurement requires a calibration related to the volume flow rate, which is dependent on the pressure conditions. A bubble flow meter was used to calibrate the flow rate derived from the changes of measured differential pressure of each COPAS channel in the pressure range of 1000–50 hPa.

2.1 Adaptation to airborne operation

The COPAS CPCs – intended for aircraft-based operation up to 21 km – are mounted within the aircraft's hull but exposed to a wide range of ambient conditions such as pressures as low as 50 hPa, temperature conditions from $+50^\circ\text{C}$ (on the runway) down to -80°C at the tropical tropopause, and changes between these extremes within ~ 30 min. Important properties of the COPAS instruments, compared to commercially available CPCs, are:

- The saturator of each COPAS channel is equipped with an active heating device. Thus the saturator temperature is maintained at its set-points within $\pm 0.5^\circ\text{C}$ during a complete flight (in the Arctic as well as in tropical regions).
- FluorInert (FC-43) is preferably used as the working liquid instead of butanol. In particular, for CPC applications at high altitudes with pressure conditions below 200 hPa the use of FC-43 is favored due to its better performance. FC-43 has a three times smaller diffusion coefficient than butanol. Thus at ambient pressure below 200 hPa butanol condensation on the particles while passing the saturator is not sufficiently efficient anymore. Detailed discussion concerning the pressure dependent performance of butanol compared

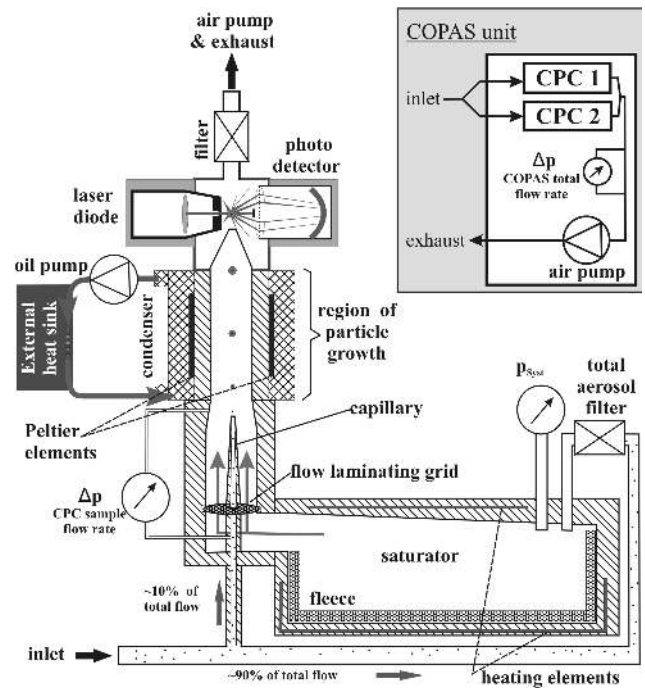


Fig. 1. Flow scheme of a COPAS CPC channel. Two such counter channels are implemented in one COPAS instrument unit. Two COPAS units (with two CPC channels each) are mounted at different locations on the M-55 Geophysika.

to FC-43 as CPC working fluid are provided by Hermann et al. (2005). FC-43 has also been used on the NASA ER-2 (J. C. Wilson, personal communication).

- Peltier elements are used for the cooling of the condenser, with their warm sides being cooled by a low viscosity silicone oil circuit. A custom-designed oil circuit is running through the shaft of the inlet probe, where the oil is efficiently cooled (cf. Sect. 2.3). Minimum oil temperatures of $< -37^\circ\text{C}$ are reached during flight. The Peltier elements are adjusting the temperature to a set point with an accuracy of $\pm 0.5^\circ\text{C}$.
- The air flow through the COPAS unit is regulated as a function of ambient pressure by a frequency-controlled air pump (Brey G12/02-8) with an accuracy of $\pm 0.151 \text{ min}^{-1}$ at standard temperature and pressure (STP).
- The data acquisition and control of COPAS is achieved by custom-made electronics. Data are typically recorded with 1 Hz frequency on flash memory (PCMCIA card).

2.2 The inlet probe

The two COPAS inlet probes consist of three parts, the base plate, the shaft, and the inlet head. Figure 2 shows a

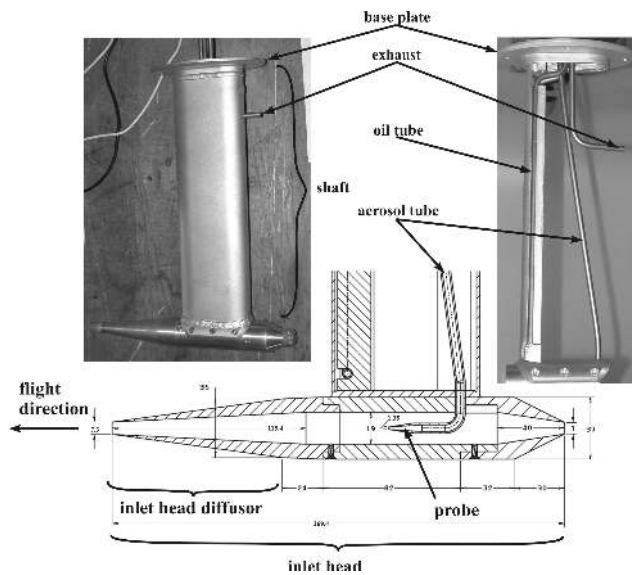


Fig. 2. The COPAS aerosol inlet for measurements on-board the M-55. The inlet head consists of a diffuser-type entrance with sharp inlet lips. Inside the head, the so-called probe is implemented, also equipped with a diffuser-type inlet with sharp lips. The inlet shaft includes the aerosol intake and exhaust lines as well as the heat exchanger pipes for the silicone oil coolant circuit (dimensions in millimeter).

schematic drawing of the different parts and photographic images of the device.

For the COPAS measurements on board the M-55 diffuser-type, non-shrouded inlets with sharp-edged inlet lips were used (2.9° diffuser half-angle), a custom-made reproduction of the inlet used on board the NASA ER-2 which is described in detail by Wilson et al. (1992). Each of the two inlets is mounted with a negative angle related to the longitudinal axis of the M-55 respecting the aircraft's positive mean angle of attack of about $7\text{--}8^\circ$ at flight altitudes above 5 km. Thus, for cruising flight operations the aerosol inlet is mounted isoaxial within accuracy of $\pm 1^\circ$. Below 5 km altitude, particularly during take-off and landing phase, the inlet is misaligned from isoaxial condition by up to $\pm 6^\circ$.

The shaft length of 300 mm insures an aerosol probing outside the boundary layer of the M-55 (Myasishchev Design Bureau, 2002). Beside the aerosol sampling line and the exhaust tube the shaft contains the oil cooling circuit.

2.3 The condenser cooling oil circuit

Figure 3 shows the measured oil temperature during a flight in tropical regions (12 February 2005, TROCCINOX mission, Araçatuba, Brazil) as an example for extreme ambient temperature conditions influencing the COPAS measurement performance. The ambient temperature as well as the oil temperature is shown as a function of flight altitude. From the temperature profiles it becomes obvious that high ambient

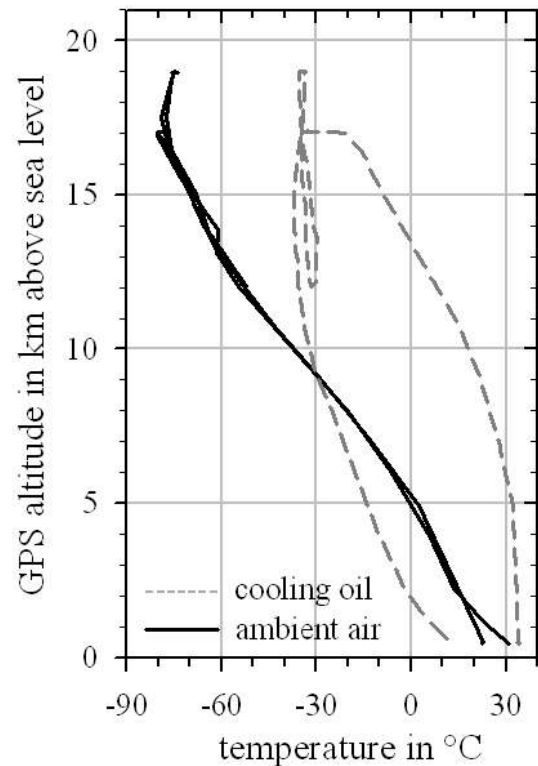


Fig. 3. Vertical ambient temperature profile and the recorded temperature of the cooling oil circuit during a flight (12 February 2005, longitude: $41^\circ\text{--}51^\circ$ west; latitude: $17^\circ\text{--}21^\circ$ south) in tropical regions (State of São Paulo, Brazil).

temperatures on the ground caused oil temperatures of up to 33°C . During ascent, the oil temperature remained above 10°C until reaching flight altitudes of 12 km. At 12 km altitude an oil temperatures of 10°C is reached for which the condenser temperature is in the range of given settings. For oil temperatures above 10°C the condenser temperatures are out of range and according measurement data have to be discarded from further analysis (cf. Sect. 8).

3 Determination of COPAS sampling characteristics

The performance of an aerosol inlet system can be described by the inlet particle sampling efficiency (aspiration and transmission) and the transport efficiency through the sampling lines to the instruments (Baron and Willeke, 2001). The aspiration is related to the fraction of the ambient particles which enter the aerosol inlet, while the transmission efficiency denotes the particle fraction that passes through the inlet. The transport efficiency is determined by the particle losses in the sampling line between the inlet and the instrument and describes the fraction of particles that are able to reach the detection chamber. The following three sections describe

the sampling efficiency of the COPAS aerosol inlet and the aerosol sampling line transport efficiency.

3.1 Aspiration efficiency of the COPAS aerosol inlet

For representative measurements an aerosol probe must sample outside of the aircraft boundary layer and outside of zones of depletion or enhancement for particles caused by the flow distortion around the aircraft hull. These conditions are met for both COPAS inlet positions on board the M-55. Deviations from the isoaxial alignment of the COPAS aerosol inlet above 5 km flight altitude in the range of $\pm 1.5^\circ$ can be neglected for sub-micrometer particle sampling. Particle losses due to anisoaxial sampling become significant for particles and droplets $> 1 \mu\text{m}$ only (Baron and Willke, 2001).

To evaluate the isokinetic property of the COPAS aerosol inlet 2-D CFD modeling studies with FLUENT were performed by Walter (2004). For the calculations compressible gas properties were assumed considering the maximum flight speed of the M-55 of up to Mach 0.7. For both the inlet head diffuser and the probe diffuser the calculations yield the ratios R of air flow velocities between outside and inside the respective inlet entrance. The results of $R_{ih}=1.2$ for the COPAS inlet head and $R_p=1.7$ for the probe sampling indicate sub-isokinetic sampling conditions for both entrances.

For calculation of the aspiration efficiency the equations from Hangal and Willeke (1990) are used for ambient pressure of 50 hPa, considering that anisokinetic effects have the largest impact on particle losses at lowest pressure conditions. Calculations were made related to the R of the inlet head and the probe. The sub-isokinetic sampling conditions become significant for particle sizes well above $d_p=500 \text{ nm}$. However, as the particle number concentration in the upper troposphere and lower stratosphere (UT/LS) is strongly dominated by the sub-micrometer particles of $d_p < 500 \text{ nm}$ (Thomas et al., 2002; Deshler et al., 2003) the results indicate that at UT/LS conditions the obtained aspiration efficiency of the inlet has negligible impact on the measurement with COPAS.

3.2 Transmission efficiency

Hermann et al. (2001) provide results of wind tunnel experiments with an aircraft-borne aerosol inlet. They showed that in the COPAS relevant particle size range the transmission is independent from the Reynolds-number and that the transmission efficiency of their inlet decreased for particles larger than 200 nm, reaching zero at about $3 \mu\text{m}$. Without having performed such wind tunnel experiments we assume that the findings of Hermann et al. (2001) can be transferred to our inlet as it represents a very similar non-shrouded diffuser-type inlet head with a sharp-edged inlet entrance. Hermann et al. (2001) obtained transmission efficiencies above 75% for submicron particles. As the sampling inside the COPAS inlet is realized as forward facing probe in contrast to the

backward facing probe in Hermann et al. (2001) the transmission efficiency of the COPAS inlet should be even higher. Considering the small number concentration of particles with $d_p > 1 \mu\text{m}$ in the UT/LS (Thomas et al., 2002; Deshler et al., 2003) the transmission of the COPAS aerosol inlet can be estimated to be about 1 for $d_p < 500 \text{ nm}$ and better than 0.75 for the sub-micron particle size range of $500 \text{ nm} < d_p < 1 \mu\text{m}$.

3.3 Transport efficiency

A general problem arises from the fact that any correction of the measured particle number concentration related to the particle diffusion losses in the sampling lines requires the knowledge of the initial aerosol size distribution. Only for the measurement of the ultra-fine nucleation-mode particles with $6 \text{ nm} < d_p < 15 \text{ nm}$, an estimated correction is feasible, but this is also the size range which is most sensitive to particle diffusion losses.

For the diffusion loss mechanism, the particle fraction that penetrates the aerosol lines have been calculated using the empirical equations given by Baron and Willeke (2001) and Hinds (1999). The number concentration of ultrafine particles is determined by subtracting the measurements of the two COPAS CPCs with $d_{p50} \approx 6 \text{ nm}$ ($\Rightarrow n_6$) and $d_{p50} \approx 15 \text{ nm}$ ($\Rightarrow n_{15}$). This yields the number concentration of particles in the size range between 6 and 15 nm (n_{6-15}). Calculated mean particle losses $\bar{\Lambda}_{6-15}$ for the particles between 6 and 15 nm are given in Table 1. From $\bar{\Lambda}_{6-15}$ a correction factor κ_L (for pressure conditions $< 150 \text{ hPa}$, $150\text{--}300 \text{ hPa}$, and $> 300 \text{ hPa}$) was calculated to correct the ultrafine particle number concentration n_{6-15} :

$$\kappa_L = \frac{100\%}{100\% - \bar{\Lambda}_{6-15}}, \quad (2)$$

here, $\bar{\Lambda}_{6-15}$ is given in percent.

4 Determination of COPAS detection and counting characteristics

For several CPC models, information on their performance at reduced pressures is available in the literature based on experimental as well as theoretical work (Heintzenberg and Ogren, 1985; Dreiling and Jaenicke, 1988; Noone and Hansson, 1990; Zhang and Liu, 1990, 1991; Saros et al., 1996; Cofer et al., 1998; Hermann and Wiedensohler, 2001, and Hermann et al., 2005). A detailed description of both, the instrumental development and the instrument performance of those CPCs at reduced operating pressure, is given by Hermann and Wiedensohler (2001) who also provided a description of a low-pressure calibration setup. This setup allows for generating monodisperse aerosol particles in different materials and for operating at a pressure range from 1000 hPa down to 50 hPa. All experimental characterizations presented in this study concerning the pressure dependent

Table 1. Pressure dependent particle losses (bold characters in %) inside the aerosol inlet tubes and according mean particle loss $\bar{\Lambda}_{6-15}$ (in %) for the particle size range $6 \text{ nm} < d_p < 15 \text{ nm}$. Resulting correction factor κ_L (dimensionless) are exclusively used for the ultra-fine size fraction n_{6-15} determined from results of COPAS-II.

pressure in hPa	particle diameter in nm										$\bar{\Lambda}_{6-15}$	resulting κ_L
	6	7	8	9	10	11	12	14	15			
70	36	30	26	23	20	18	16	14	13	21.8	1.28	
150	31	26	22	20	17	16	14	12	11	18.8	1.23	
300	26	22	19	17	15	13	12	10	9	15.9	1.19	
400	22	19	16	14	13	11	10	8	7	13.3	1.15	

Table 2. Resulting d_{p50} of each COPAS channel obtained from the experimental CPC characterization studies at two operating pressure conditions with Ag-particles. Additionally, respective ΔT for each COPAS channel and according factor of supersaturation f_S of the working fluid FC-43 is listed.

	$d_{p50} \pm \bar{\sigma}_\eta$ (in nm)			
	COPAS-I channel		COPAS-II channel	
	1	2	1	2
70 hPa	12.4±1.8	9.5±1.1	12.3±0.6	6.0±0.3
300 hPa	11.1±1.0	10.6±0.7	18.8±0.9	6.6±0.2
ΔT	30°C		17°C	33°C
f_S	7.5		3.2	8.4

counting efficiencies of the COPAS CPCs were carried out at the calibration facility of the Leibniz Institute for Tropospheric Research, Leipzig, Germany.

The ratio between n_{det} and the n_{real} at a given particle size is defined as the counting efficiency $\eta(d_p)$ of a particle counter. The counting efficiency at which $\eta(d_p)=50\%$ determines d_{p50} . The d_{p50} can be determined as a function of the supersaturation and can be adjusted within a certain range by changing the temperature difference ΔT between the saturator (T_{Sat}) and the condenser (T_{Cond}).

An additional important parameter for CPC characterization is the pressure dependent maximum asymptotic counting efficiency. This parameter describes the plateau value of the counting efficiency for larger aerosol particles. Hermann and Wiedensohler (2001) showed for the Model 7610 (TSI Inc.), operated with butanol, that the maximum asymptotic counting efficiency decreases significantly with decreasing pressure for pressures below 300 hPa. However, Hermann et al. (2005) showed that the maximum asymptotic counting efficiency is close to 1 for $p < 300$ hPa when FC-43 is used as working fluid inside the same CPC type.

Silver (Ag) particles were used in this study to determine the counting efficiencies of the COPAS CPCs, as Ag particles can be produced easily in sufficiently high number concentration for particle diameters of a few nanometers

(<4 nm). Furthermore, silver particles can be generated in nearly spherical shape (Ku and Maynard, 2006) and they are physically stable and inert with respect to chemical reactions.

The calibration set-up used for the COPAS characterization is described in detail by Hermann and Wiedensohler (2001) and Hermann et al. (2005). The calibration aerosol is charged by a neutralizer (^{241}Am source) and a monodisperse fraction is selected by a Differential Mobility Analyzer (DMA, Vienna-type, short). The COPAS CPC is positioned parallel to an Aerosol Electrometer used as the reference counter. Both instruments are operated inside the low pressure part of the calibration set-up. For the COPAS characterization pressures from 70 hPa to 300 hPa were covered. The operating temperatures of the COPAS-I were $T_{\text{Sat}}=32^\circ\text{C}$ and $T_{\text{Cond}}=2^\circ\text{C}$ ($\Rightarrow \Delta T=30^\circ\text{C}$), common for both channels. The channels 1 and 2 of COPAS-II were operated with $T_{\text{Sat}}=24^\circ\text{C}$ and $T_{\text{Cond}}=7^\circ\text{C}$ and $T_{\text{Sat}}=40^\circ\text{C}$ and $T_{\text{Cond}}=7^\circ\text{C}$ ($\Rightarrow \Delta T_1=17^\circ\text{C}$ and $\Delta T_2=33^\circ\text{C}$), respectively. Resulting supersaturation factors from ΔT setting of each COPAS CPC are listed in Table 2.

Figure 4 A-D shows the results of the characterization of both COPAS CPCs for a particle sizes range of $5 \text{ nm} < d_p < 35 \text{ nm}$ for $p=70$ and 300 hPa. The error bars on the x-axis represent theoretical values of the bandwidth of the DMA transfer function. The error bars on the y-axis display the standard deviation of the measurements. For each particle diameter and both pressure conditions four measurement points were recorded.

Table 2 summarizes the resulting d_{p50} dependent on ΔT for the COPAS channels for two pressure conditions. For the field measurements, the two channels of COPAS-I, with similar $d_{p50} \approx 11 \text{ nm}$, are used to study the non-volatile fraction of the total particle number concentration. The difference in the efficiency characteristic between the two COPAS-I channels results from the mounted (but not heated) heating line at channel 1 (see Fig. 4a). Two effects can be observed due to the elongated aerosol tube – a shift of d_{p50} to larger sizes and a decreased maximum asymptotic counting efficiency for channel 1 (7–12% lower compared to channel 2). These effects are caused by additional particle losses. Nevertheless, the decreased maximum asymptotic counting efficiency

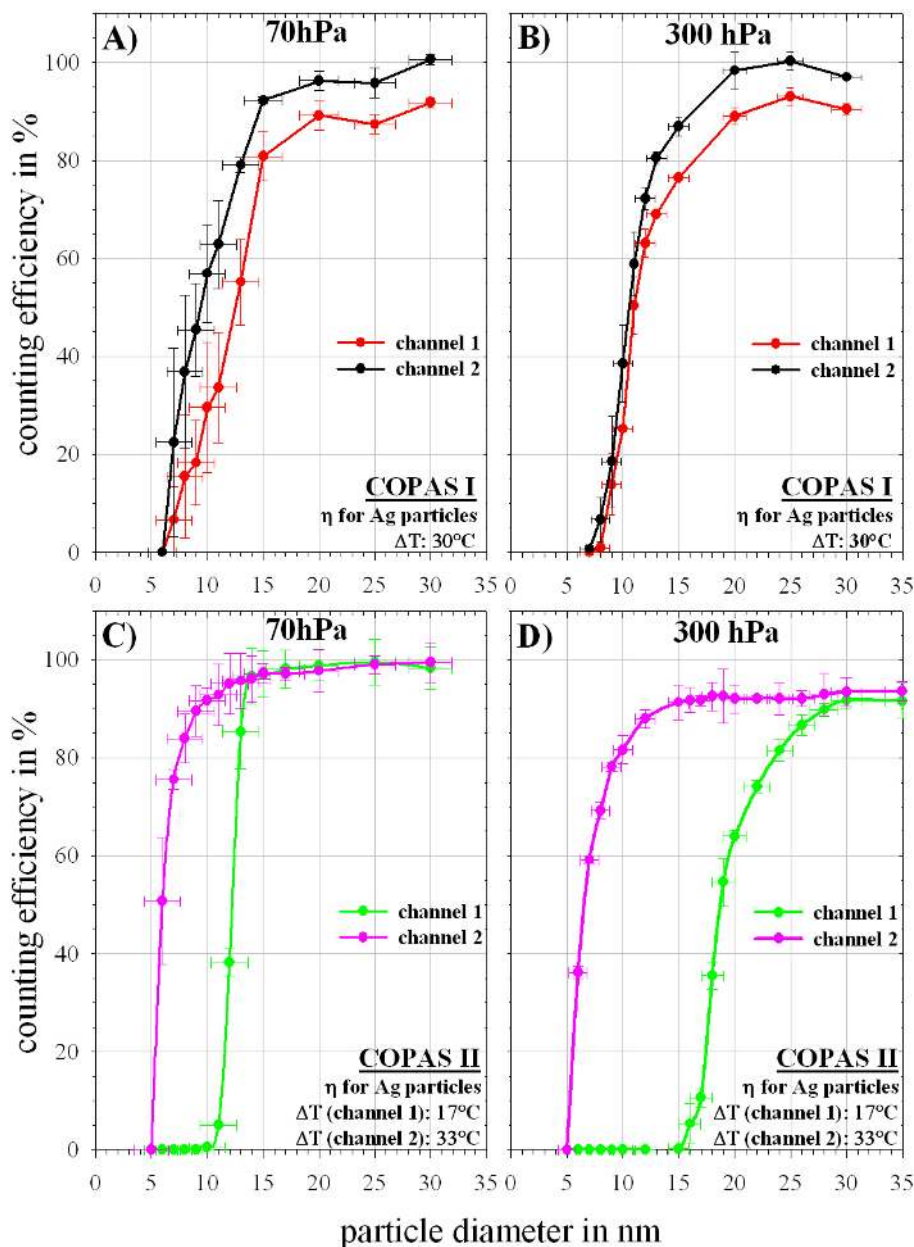


Fig. 4. Results of the experimental COPAS CPC counting efficiency characterizations compared to an Aerosol Electrometer at two different system pressures, 70 hPa and 300 hPa. Graphs A) and B) show the counting efficiency curves of COPAS-I, channel 1 (red) and channel 2 (black) operating with a common ΔT of 30°C. The mounted (but not heated) heating line at the aerosol tube of channel 1 and the associated additional particle losses explain the observed differences between the curves. Graphs C) and D) show the result of COPAS-II channel 1 (green) and channel 2 (pink) operated with different ΔT .

yields a correction of the heated channel measurements of generally not more than 10%.

The channels of COPAS-II have significantly different d_{p50} , $d_{p50} \approx 12$ nm (at 70 hPa) for channel 1 (with increasing atmospheric pressure up to $d_{p50} \approx 19$ nm (at 300 hPa) and $d_{p50} \approx 6$ nm for channel 2, nearly independent of pressure. For sake of simplicity, also a pressure independent mean d_{p50} of 15 nm for channel 1 is generally assumed. The difference

between the two COPAS II channels is used to investigate the occurrence or absence of freshly nucleated aerosol particles in the atmosphere.

The accuracy of the COPAS measurements was also determined from the characterisation experiments. The total accuracy is estimated to be within $\pm 10\%$.

Table 3. Pressure dependent volume flow rates for the COPAS CPCs, according residence times for the aerosol particles inside the photo-optical detector volume and the coincidence parameter.

pressure p in hPa	volume flow Q in $\text{cm}^3 \text{s}^{-1}$	residence time t in μs	coincidence parameter $c \times 10^5$ in cm^3
70	16.4	0.6	0.98
150	10.1	1.0	1.01
300	6.1	1.5	0.92
600	4.0	2.5	1.00

5 Coincidence and homogeneous nucleation

Coincidence describes the classification of two or more particles simultaneously present in a detection volume and therefore registered as one single particle (Raasch and Umhauer, 1984). We estimated the true particle number concentration n_{real} from the measured particle number n_{det} according to Jaenicke (1970, 1972); Hermann and Wiedensohler (2001) using the coincidence parameter of the optical detector $c=10^{-5} \text{ cm}^3$ (TSI Incorporated, 2002) (cf. Table 3). For particle number densities below $\sim 10^4 \text{ cm}^{-3}$ coincidence is not influencing the counting results significantly. Such high concentrations are rarely encountered in the UT/LS. For the rare cases where the measured particle number concentration significantly exceeds 10^4 cm^{-3} , the measurements with COPAS are corrected by a factor κ_C which is parameterized by $\kappa_C = \exp(1.23 \times 10^{-5} \cdot n_{\text{det}})$.

To determine the operational limits above which homogeneous nucleation of the CPC working fluid starts to occur (e.g. Hämeri et al., 1995), the temperature difference ΔT was increased stepwise when operating in particle-free conditions to check at which point a signal in the CPC occurs. At 50 hPa significant particle concentrations were not observed until a ΔT of 42°C was reached. At 100 hPa, homogeneous nucleation occurred only for $\Delta T > 47^\circ\text{C}$. Therefore, for the range of temperature differences used for the COPAS instruments ($17\text{--}33^\circ\text{C}$), the process of homogeneous nucleation of the working fluid can be excluded.

6 The particle volatilization efficiency of the heated channel

Previous work on volatilization properties of aerosols, particularly oriented to the stratospheric $\text{H}_2\text{SO}_4\text{-H}_2\text{O}$ aerosol component, has been performed by Rosen (1971), Deshler et al. (1993), and Brock et al. (1995).

The volatilizing behavior of the COPAS heating line was studied by laboratory experiments using a pure $\text{H}_2\text{SO}_4\text{-H}_2\text{O}$ calibration aerosol. Prior to the measurements, all inner surfaces of the stainless steel tubes of the calibration setup were

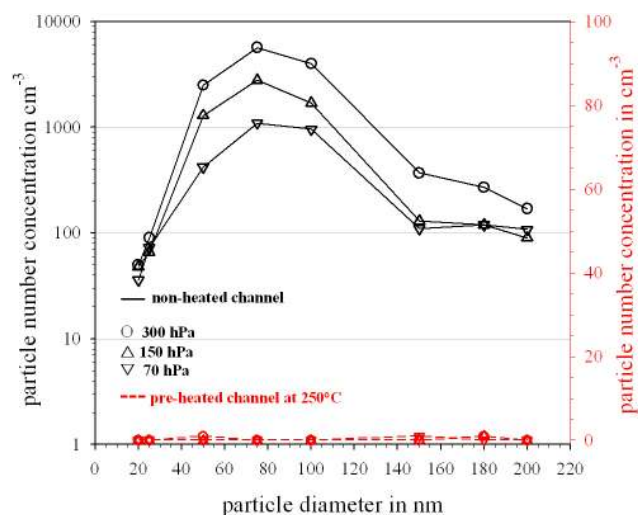


Fig. 5. Result of the experimental aerosol heating line characterization with pure $\text{H}_2\text{SO}_4\text{-H}_2\text{O}$ aerosol at a pre-heating temperature of 250°C for three operating pressures: 70 hPa, 150 hPa, and 300 hPa. The comparison was made between the pre-heated (red) and the non-heated (black) channel of COPAS-I. Note the different scales of the ordinates.

cleaned with citric acid ($\text{C}_6\text{H}_8\text{O}_7$) to prevent contamination of the calibration aerosol by residues of, e.g., Ammonia. High purity nitrogen (5.0) was used as the carrier gas for the particles. The $\text{H}_2\text{SO}_4\text{-H}_2\text{O}$ particles were generated with a particle generator (Middlebrook et al., 1997; Böttger, 2000) by heating a small reservoir of 90-weight-percent solution of H_2SO_4 and H_2O .

The freshly generated polydisperse aerosol was separated with an electrostatic classifier (Model 3080N, TSI Incorporated) and the size-selected calibration aerosol was transferred into a low pressure sampling volume via a critical orifice. For these experiments the results from the heated channel were compared with the measurements from the unheated channel of the COPAS I instrument, where both channels have a d_{p50} of $\sim 11 \text{ nm}$ (see Fig. 4a and b). First studies at 70 hPa showed that particles with $d_p=50 \text{ nm}$ were volatilized to sizes smaller than the d_{p50} of COPAS-I already at heating temperatures of 176°C . To insure the total volatilization of particles with sizes $d_p > 50 \text{ nm}$ the temperature of the COPAS aerosol heating line was set to 250°C . For three pressures, i.e., 70 hPa, 150 hPa, and 300 hPa, the heating efficiency was characterized for pure $\text{H}_2\text{SO}_4\text{-H}_2\text{O}$ aerosol particles in the size range of $20 \text{ nm} < d_p < 200 \text{ nm}$. The results of the heating line characterization are shown in Fig. 5. At an operation temperature of 250°C and over the pressure range 70–300 hPa the aerosol pre-heater volatilizes more than 98% of the $\text{H}_2\text{SO}_4\text{-H}_2\text{O}$ particles. Although, we were not able to generate $\text{H}_2\text{SO}_4\text{-H}_2\text{O}$ particles of sizes larger than 200 nm within this study we assumed from laboratory as well as field study experience that this volatilization

efficiency of the aerosol pre-heater is also valid for particles with $d_p > 200$ nm. This concept has been successfully applied for the differentiation of pure stratospheric sulphuric acid droplets from droplets containing residues of meteoric ablation (Curtius et al., 2005).

7 Characterization experiments during flight operation

A cross-correlation of the COPAS CPCs (Fig. 6) was performed to demonstrate the coherence of the measurements and to provide in-flight quality control. Therefore the data of altogether six measurement flights were used when all three unheated COPAS channels were operated on the M-55 with identical settings ($d_{p50} \approx 10$ nm). During these flights still all COPAS CPCs were operated with butanol as working fluid (Curtius et al., 2005), the COPAS setup has been changed for use of FC-43 after this campaign. The correlations were obtained using 15-s averaged data of particle number concentration by (1) inter-comparing the two CPC channels contained inside COPAS-II (Fig. 6a) and by (2) cross-comparing one CPC channel from COPAS-I with one channel from COPAS-II (Fig. 6b). The correlation coefficients of 0.996 (Fig. 6a) and 0.985 (Fig. 6b) illustrate a high level of consistency between the COPAS CPCs.

8 Examples of arctic and tropical measurements

Vertical profiles of the particle number concentration of two typical flights are shown in Fig. 7 to demonstrate the COPAS measurement results. These flights are chosen to discuss instrumental limitations with respect to flight conditions, particularly at low flight altitudes. In the graphs the particle number concentration is given as 15-s averages. All particle number concentrations presented in this paper refer to ambient conditions.

The upper panel of Fig. 7 depicts a flight on 2 February 2003 (longitude: 10° – 30° east; latitude: 68° – 76° north) at Arctic regions during the EUropean Polar stratospheric cloud and Lee-wave EXperiment (EUPLEX). During this campaign both COPAS instruments were operated with the working fluid butanol and with the same differential temperatures ΔT yielding the same d_{p50} of 10 nm for all channels. In the lower panel of Fig. 7 data are shown from a flight on 12 February 2005 (longitude: 41° – 51° west; latitude: 17° – 21° south) during the Tropical Convection, CIrrus and Nitrogen OXides Experiment (TROCCINOX), when both COPAS instruments were operated with FC-43 as the working fluid. The ΔT for each of the non-heated CPCs was set to yield $d_{p50}=6$ nm (n_6), $d_{p50}=11$ nm (n_{11}), and $d_{p50}=15$ nm (n_{15}), respectively (cf. Sect. 4). COPAS-I measured the total number concentration n_{11} as well as the non-volatile particle number (n_{11nv}). On the right side of each panel the respective fraction of non-volatile particles is shown.

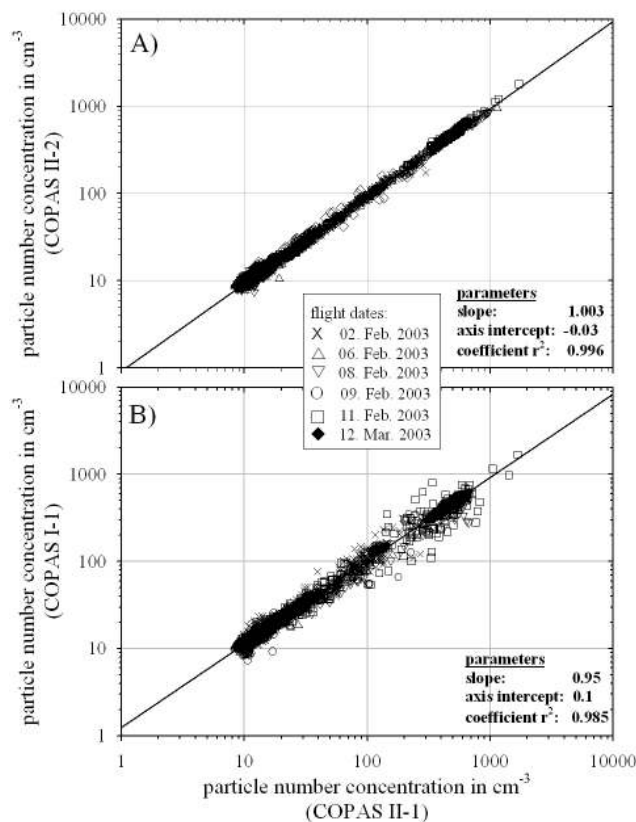


Fig. 6. Correlation of COPAS ambient particle number density measurements (15 s average) from six flights in the arctic lower stratosphere when both COPAS instruments were operated with butanol as well as the same ΔT and therefore identical d_{p50} . (A) COPAS-II inter-comparison between two channels of the same instrument with a correlation coefficient of 0.996. (B) Cross-comparison between one channel of COPAS-I and one channel of COPAS-II with a correlation coefficient of 0.985 (adapted from Curtius et al., 2005).

The example from our tropical measurements yields good agreement (not graphically illustrated herein) with previously published tropical vertical particle distributions (Brock et al., 1995) up to UT/LS altitudes for undisturbed stratospheric conditions. The polar measurements show the difference between the conditions in polar tropospheric air ($\Theta < 370$ K – influenced by air masses from lower latitudes) and polar vortex air masses ($\Theta > 380$ K – nearly isolated from influences of lower latitudes).

From the profile of the non-volatile aerosol fraction during the arctic measurements the enhanced particle number at $\Theta > 435$ K is assumed to mainly contain non-volatile material (50%, and with increasing altitude up to 70%). For detailed discussions concerning this observation inside the polar winter vortex see Curtius et al. (2005). The non-volatile particle fraction of the tropical measurements decreases well below 50% above the tropical tropopause, and above a transition region ($\Theta > 400$ K) a nearly constant value of about

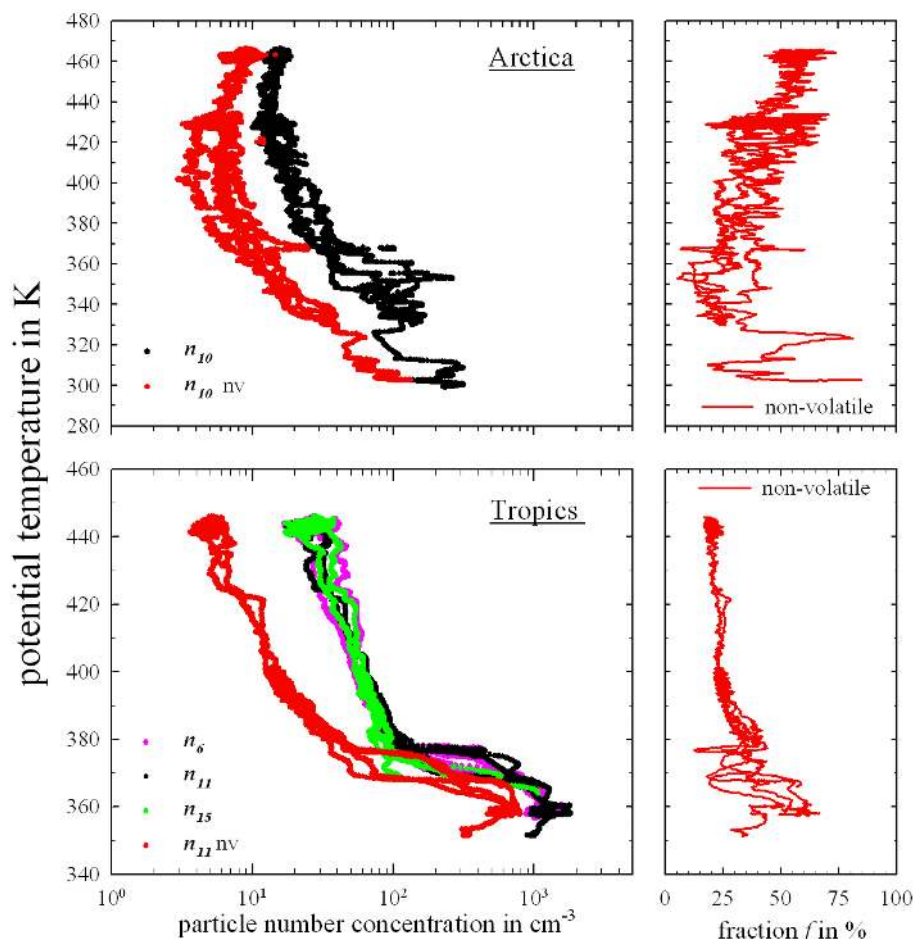


Fig. 7. Vertical profiles of particle number concentration (left) and the vertical distribution of the non-volatile aerosol fraction (right) measured by COPAS at two different measurement locations. Data are shown as 15-s running averages versus potential temperature as the vertical coordinate. Upper panel: Flight example from 2 February 2003 (longitude: 10°–30° east; latitude: 68°–76° north) during the polar mission EUPLEX. COPAS working fluid: butanol. Lower panel: Flight example from 12 February 2005 (longitude: 41°–51° west; latitude: 17°–21° south) during the tropical mission TROCCINOX. COPAS working fluid: FC-43.

25% for the non-volatile aerosol fraction is found. While for the measurements inside the polar vortex the non-volatile material is transported mainly from higher (mesospheric) altitudes with subsiding air masses, at tropical latitudes the non-volatile particle fraction is most likely maintained by transport processes between the Tropical Tropopause Layer (TTL) and the stratosphere (Hamill et al., 1997).

The COPAS data do not extend down to ground level. The measurements from ground level to altitudes of 7–12 km have to be analyzed carefully with respect to data quality. For the particular cases measurement data from flight altitudes lower than 7.5 km ($\Theta=300$ K for the polar measurement) and 11.5 km ($\Theta=350$ K at tropical latitudes) were rejected if one of the following three aspects limited the COPAS measurements:

1. the automated flow regulation of COPAS did not work properly caused by fast ascent or descent rates of $>10 \text{ m s}^{-1}$.

2. high ambient temperatures at the ground prior to the flights prevented the cooling system of the COPAS condensers to work efficiently immediately after take-off, e.g., for the measurement presented in Sect. 2.3 the condenser cooling circuit was not working properly until the aircraft reached an altitude of 12 km.
3. using FC-43 as the working fluid, at ambient pressures >400 hPa the CPC d_{p50} as well as the maximum asymptotic counting efficiency can change significantly (cf. Hermann et al., 2005).

9 Aerosol observation in M-55 plumes

Several observations of enhanced particle number concentration during two research flights during the TROCCINOX and the SCOUT missions were caused by crossings of the M-55 own exhaust at altitudes between 16 and 18 km. The

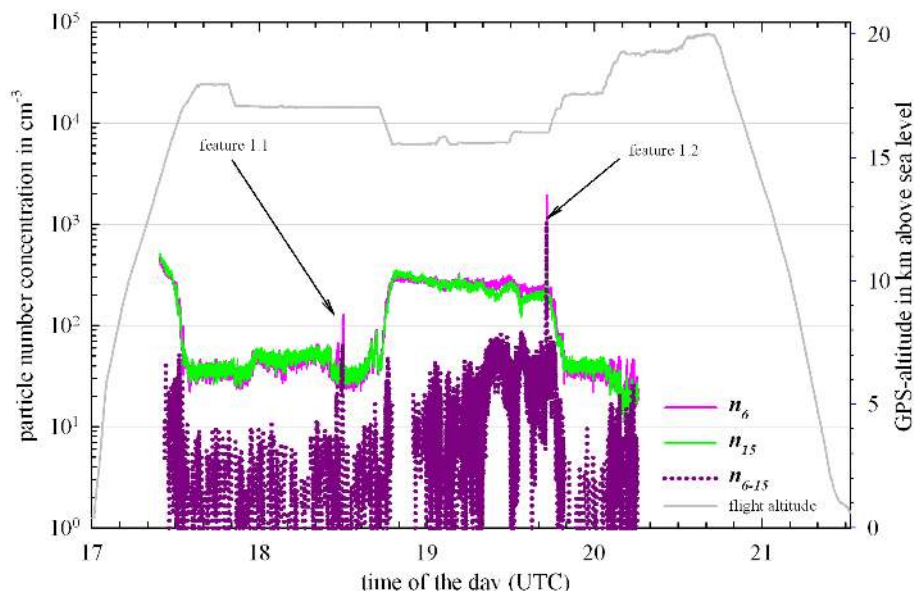


Fig. 8. Time series of COPAS measurements during the flight on 5 February 2005 (longitude: 48°–54° west; latitude: 19°–22° south). Displayed are the measured (1 Hz) ambient particle number concentration n_6 (pink) and n_{15} (green) of COPAS-II as well as the GPS-altitude during the flight (grey line). Two observations of enhanced particle number concentrations are denoted as feature 1.1 and feature 1.2. Additionally, the time series of the ultra-fine particle number concentration difference between n_6 and n_{15} (n_{6-15}) (purple dots) is shown, corrections for coincidence and for particle losses inside the sample lines have been applied.

plumes were identified by simultaneous short term increases in the particle number concentrations and the concentration of nitrogen oxides ($\text{NO}_x = \text{NO} + \text{NO}_2$) detected by the German Aerospace Center (DLR) using a chemiluminescence technique. The NO_x instrument on board the M-55 is described in detail by Voigt et al. (2006). We can exclude civil aviation as potential source of these particle and NO_x enhancements, as the plumes were detected at altitudes between 16 and 18 km, more than 4 km above the cruise altitudes of commercial aircraft. Additional confidence in the plume crossings was given by air mass back trajectories calculations (Corti et al., 2008, or HYSPLIT (<http://www.arl.noaa.gov/ready/hysplit4.html>)). This combined evidence from in situ data and trajectory modelling also suggests that it is unlikely, that the enhancements were caused by lightning.

The 1 Hz – time series of the particle number concentration measured with COPAS-II during a tropical flight on 5 February 2005 (48°–54° W, 19°–22° S) of the TROCCINOX mission is shown in Fig. 8. The ultra-fine particle number concentration n_{6-15} was calculated and was corrected for diffusional losses ($\kappa_L = 1.28$, cf. Sect. 3.3 and Table 1). Two distinct increases, feature 1.1 and 1.2, in particle concentration occur in this time series. Due to instrumental background measurements of the NO_x instrument during feature 1.1 we refrain from a detailed discussion of feature 1.1. Feature 1.2 is caused by the crossing of M-55 exhaust as supported by simultaneous particle and NO_x enhancements. For this feature, the plume age was estimated to be in the range of 8000 s from the trajectory calculations.

The second example is taken from a flight on 25 November 2005 (127°–132° E, 9°–13° S) during the mission Stratosphere-Climate Links with Emphasis On the Upper Troposphere and Lower Stratosphere (SCOUT-O₃), see Fig. 9. Figure 10 shows the flight track of the M-55 indicating a high probability of exhaust crossing. We further focus on feature 2.3 with an estimated plume age of 2600 s to make use of the simultaneous NO_x measurements, while NO_x data were not enhanced for features 2.1 and 2.2.

We determine the particle emission indices $EI [n]$ of the M-55 aircraft engines at UT/LS conditions using the measured enhancement in NO_x mixing ratios inside aircraft exhaust as a normalizing factor. This method has already been applied for other aircraft (Fahey et al., 1995a, b; Schlager et al., 1997; Anderson et al., 1999), particularly for plume ages in the range of hours. The $EI [n]$ of an aircraft engine, in units of particle number per kg fuel burned, was calculated by using following equation (Anderson et al., 1999).

$$EI[n_i] = \left(\frac{\Delta n_i}{\Delta \text{NO}_x} \right) \cdot EI[\text{NO}_x] \cdot \frac{M_{\text{air}}}{(\rho \cdot M_{\text{NO}_2})} \quad (3)$$

where:

Δn_i = particle number concentration in the plume related to background concentrations in cm^{-3} , the index i distinguishes the CPC d_{p50}

ΔNO_x = differential NO_x mixing ratio in the plume related to background values, in ppt

M = molecular Mass, $M_{\text{air}} = 29$ u, $M_{\text{NO}_2} = 46$ u

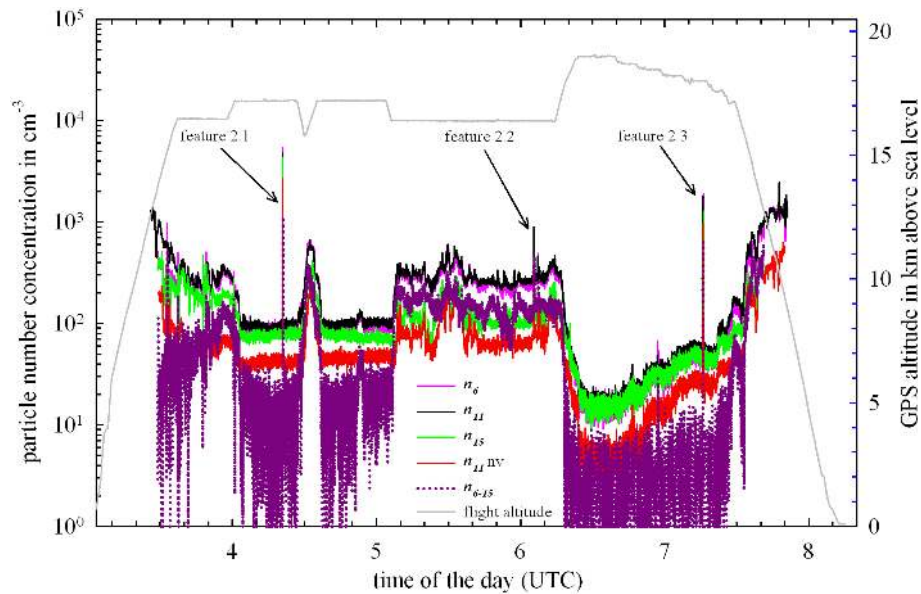


Fig. 9. Time series of COPAS measurements during the flight on 25 November 2005 (longitude: 127°–132° east; latitude: 9°–13° south). Displayed are the measured particle number concentration n_6 (pink), n_{11} (black), and n_{15} (green) as well as $n_{10\text{ nv}}$ (red) and n_{6-15} (purple dots), corrections for coincidence and for particle losses inside the sample lines have been applied. The GPS-altitude during the flight is indicated (grey). Three observations of enhanced particle number concentrations are denoted as feature 2.1, 2.2 and feature 2.3.

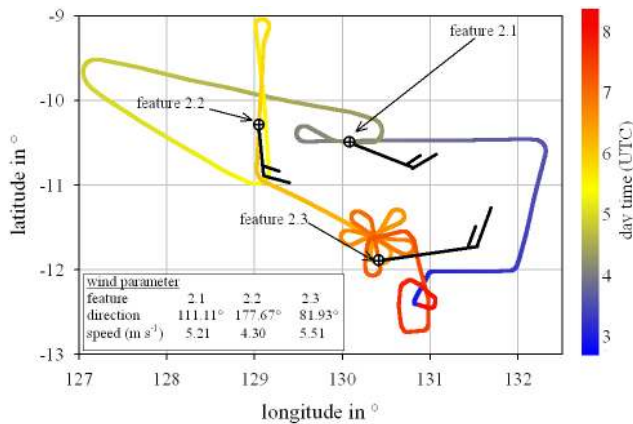


Fig. 10. Projection of the flight path for 25 November 2005. The flight path is shown coloured dependent on flight time, potential plume encounters are labelled as feature 2.1, 2.2, and 2.3, respectively.

ρ = air density, in kg m^{-3} , at flight conditions during observed event.

The integrated signal (ΔX) of observed enhancement of a species X related to background conditions is given as:

$$\Delta X = \Delta t_{\text{obs}} (X_{\text{plume}} - X_0) \quad (4)$$

Here, Δt_{obs} is the duration of an enhancement observation and the bracket term is the difference of measured number concentrations, or mixing ratio, inside the plume (X_{plume}) related to background conditions outside the plume (X_0).

An order of magnitude estimate of the $EI [n_i]_{M-55}$ has been derived from the particle number measurements and a comparison of the $EI [\text{NO}_x]$ of the M-55 and the NASA ER-2 high altitude research aircraft. Fahey et al. (1995b) determined an $EI [\text{NO}_x]_{ER-2}$ of the NASA ER-2 at cruising flight condition of about 3.6–4.3 g kg^{-1} .

The fuel consumption of the M-55 has been recorded during flight. As the aircraft was ascending, the fuel consumption was increased by a factor of 1.8 compared to cruise during feature 1.2, indicative for engine's full-load operation. This full-load operation of aircraft engines might change the fuel-to-oxygen ratio inside the turbines, causing inefficient fuel burning and enhanced emission indices compared to cruising conditions. For feature 2.3 at cruise the fuel consumption equals 846 kg h^{-1} . As an approximation for this study, the NO_x emission index for the M-55 is estimated to $EI [\text{NO}_x]_{M-55} = 1-1.5 \cdot EI [\text{NO}_x]_{ER-2} = 3.6-6.5 \text{ g kg}^{-1}$. This value is comparable to NO_x emission indices for small jet aircraft, e.g. the DLR Attas VFW-614 with $EI [\text{NO}_x]_{Attas} \approx 7 \text{ g kg}^{-1}$, the Boeing B737 with $EI [\text{NO}_x]_{B737} = 9.4-11.4 \text{ g kg}^{-1}$ (Schulte et al., 1997), or the Boeing B727 with $EI [\text{NO}_x]_{B727} = 7.7 \text{ g kg}^{-1}$ (Schumann et al., 1998).

The ultra-fine particle number concentration n_{6-15} as well as n_6 and n_{15} were used to determine the $EI [n_i]_{M-55}$ from the plume 1.2 encounter related to background concentrations n_o outside of the plume were: $n_6 = 1930 \text{ cm}^{-3}$ (for $n_o = 220 \text{ cm}^{-3}$), $n_{15} = 880 \text{ cm}^{-3}$ (for $n_o = 180 \text{ cm}^{-3}$), and $n_{6-15} = 1050 \text{ cm}^{-3}$ (for $n_o = 50 \text{ cm}^{-3}$) for 5 s maximum

Table 4. Particle EI values for the M-55 Geophysika estimated from two crossings of the own exhaust plume at different plume ages (pa) in relation to according EI of other high altitude reaching aircraft, the NASA ER-2 (Anderson et al., 1999) and the Concorde (Fahey et al., 1995a) – other d_{p50} than given for COPAS are denoted within brackets behind the EI value.

EI [n_i] $\times 10^{16}$ kg ⁻¹ fuel burned	M-55 Geophysika		NASA ER-2		Concorde
	feature 1.2 pa: 8000 s	feature 2.3 pa: 2600 s	pa: ~8000 s	pa: ~2600 s	averages for pa: 960–3480
EI [n_6]	3.5–6.3	4.7–8.4			
EI [n_{11}]	–	4.4–8.0	13 (n_8)	10.4 (n_8)	17–65 (n_8)
EI [n_{15}]	1.4–2.6	3.1–5.6	14.4 (n_{17})	9 (n_{17})	–
EI [n_{6-15}]	2.0–3.7	2.1–3.8	–	–	–
EI [n_{11} nv]		2.4–4.4	0.43 (n_{17} nv)	0.3 (n_{17} nv)	7.2 (n_8 nv)

particle enhancement in the plume. The total plume encounter lasted 18 s in the aerosol data and 20 s as derived from NO_x data with a Δ NO_x of 150 ppt.

Measured maxima of the n_i during the plume 2.3 observation are $n_6=1910$ cm⁻³ and $n_{15}=1280$ cm⁻³ (both for $n_o=47$ cm⁻³), $n_{6-15}=830$ cm⁻³ at a background concentration of <10 cm⁻³, $n_{11}=1820$ cm⁻³ (for $n_o=50$ cm⁻³) and n_{11} nv=990 cm⁻³ (for $n_o=25$ cm⁻³). Here the observed NO_x enhancement amounts to Δ NO_x=80 ppt for 25 s.

Based on these data, we determine the EI [n_i]_{M-55} between 1.4 – 8.4×10^{16} particles per kg fuel as listed in Table 4 for both cases. Generally, the EI [n_i] for both the M-55 and the NASA ER-2 are of similar magnitude. However, an uncertainty of about $\pm 50\%$ has to be considered for the calculated EI [n_i]_{M-55} mainly caused by the uncertainty of estimated EI [NO_x]_{M-55}. Further, aerosol processing, particularly in the ultra-fine size mode, within a time span of up to 8000 s has significant influence on the accuracy of calculated EI [n_i]_{M-55}. Despite large uncertainties, our analysis presents the first order of magnitude estimate of the EI [n_i]_{M-55} for the high altitude research aircraft M-55.

10 Summary

A description and characterization of the two COndensation PArticle counting Systems (COPAS) for aircraft-borne measurements on board the high altitude research aircraft M-55 has been presented. The two COPAS units, designed for aerosol concentration measurements in the UT/LS region, include two CPCs each. Three CPC channels are usually operated with different ΔT settings inside the counters in order to have three different d_{p50} of 6, 11, and 15 nm. Thereby the number concentration of ultra-fine, freshly nucleated particles can be derived in addition to measurement of the total particle number concentration. The fourth CPC channel is operated with an aerosol pre-heater to quantify the non-volatile fraction of the aerosol particles. Overall, COPAS

proved to be a reliable and robust instrument for aircraft-borne particle concentration measurements in the UT/LS region.

The performance of the COPAS aerosol inlet, constructed for operation on the M-55, has been discussed with respect to particle aspiration, transmission, and transport. Concerning aspiration and transmission of the COPAS aerosol inlet it is estimated that particles with diameters of up to one micrometer enter the aerosol inlet and pass the aerosol lines without significant particle losses. However, concerning the transmission efficiency of the aerosol inlet, only additional wind tunnel studies could provide a complete characterization. Furthermore, in such wind tunnel studies, it should also be investigated whether the use of a shroud would be beneficial (Baumgardner et al., 1991; Murphy and Schein, 1998; Twohey, 1998; Weber et al., 1998). Particle losses inside the inlet system are assumed to be negligible for particle sizes smaller than 500 nm.

The counting efficiency as a function of particle size and pressure was determined for each of the four COPAS CPC channels. The result of this CPC characterization allows for setting the d_{p50} to different particle sizes. For our measurements, the d_{p50} sizes were typically set to $d_{p50}=6$ nm (COPAS-II-2), $d_{p50}=11$ nm (COPAS-I-2) and $d_{p50}=15$ nm (COPAS-II-1). From the readings of the three counters, recent nucleation events can be identified by subtraction. The aerosol pre-heater (upstream of COPAS-I-1 with $d_{p50}=11$ nm), which was characterized with respect to its ability to completely vaporize pure H₂SO₄-H₂O particles, allows for physico-chemical aerosol studies concerning the volatility of the UT/LS aerosol. A pre-heating temperature of 250°C was chosen to volatilize the main component of UT/LS aerosol, namely H₂SO₄-H₂O.

The performance of the COPAS instruments was demonstrated in several case studies. Cross-correlation of two COPAS channels, for two channels of the same COPAS and for two channels of two independent COPAS instruments,

illustrates the high consistency of the COPAS measurements. Two typical flight examples were used to describe the results from the COPAS measurements and the instrumental limitations with respect to flight altitude.

High ascent and descent rates of the measurement platform have significant impact on the performance of the COPAS particularly at low flight altitudes. Ascent and descent rates exceeding 10 m s^{-1} up to flight altitudes of 7–12 km significantly impact the reliability of COPAS measurements.

Finally, particle emission indices $EI [n_i]_{M-55}$ were estimated for the M-55 from two plume crossings, identified by enhanced particle number concentrations and simultaneously increased NO_x mixing ratio. The estimated average $EI [n_i]_{M-55} \approx 5 \times 10^{16} \text{ kg}^{-1}$ fuel burned is comparable to results of the NASA ER-2.

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