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1 **Fast oxidation of sulfur dioxide by hydrogen**  
2 **peroxide in deliquesced aerosol particles**

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9

10 **Classification: PHYSICAL SCIENCES: Earth, Atmospheric, and Planetary**  
11 **Sciences**

12 **Abstract**

13 Atmospheric sulfate aerosols have important impacts on air quality, climate, and human  
14 and ecosystem health. However, current air-quality models generally underestimate the  
15 rate of conversion of sulfur dioxide (SO<sub>2</sub>) to sulfate during severe haze pollution events,  
16 indicating that our understanding of sulfate formation chemistry is incomplete. This  
17 may arise because the air-quality models rely upon kinetics studies of SO<sub>2</sub> oxidation  
18 conducted in dilute aqueous solutions, and not at the high solute strengths of  
19 atmospheric aerosol particles. Here, we utilize an aerosol flow reactor to perform direct  
20 investigation on the kinetics of aqueous oxidation of dissolved SO<sub>2</sub> by hydrogen  
21 peroxide (H<sub>2</sub>O<sub>2</sub>) using pH-buffered, submicrometer, deliquesced aerosol particles at  
22 relative humidity of 73 to 90%. We find that the high solute strength of the aerosol  
23 particles significantly enhances the sulfate formation rate for the H<sub>2</sub>O<sub>2</sub> oxidation  
24 pathway compared to the dilute solution. By taking these effects into account, our  
25 results indicate that the oxidation of SO<sub>2</sub> by H<sub>2</sub>O<sub>2</sub> in the liquid water present in  
26 atmospheric aerosol particles can contribute to the missing sulfate source during severe  
27 haze episodes.

28 **Keywords: air pollution; Chinese haze; sulfate aerosol; sulfur dioxide oxidation;**  
29 **aerosol kinetics; multiphase chemistry**

30 **Significance**

31 Atmospheric sulfate aerosol particles contribute significantly to poor air quality and  
32 direct forcing of the Earth's climate. However, air pollution and climate models  
33 simulate the formation of sulfate using acid rain chemistry known to be appropriate  
34 only for cloud water conditions. By measuring the oxidation of sulfur dioxide (SO<sub>2</sub>) by  
35 hydrogen peroxide (H<sub>2</sub>O<sub>2</sub>) directly in hygroscopic, pH-buffered aerosol particles with  
36 high solute strength characteristic of many tropospheric conditions, we show that  
37 sulfate formation occurs significantly faster than under the cloudwater conditions  
38 previously explored. In part, ionic strength and general acid catalysis effects drive the  
39 fast chemistry. These results indicate that the H<sub>2</sub>O<sub>2</sub>-driven oxidation of SO<sub>2</sub> in aqueous  
40 aerosol particles can contribute to the missing sulfate source during severe haze  
41 pollution events.

## 42 **Introduction**

43 Sulfate aerosol is an important component of fine particulate matter that impacts air  
44 quality, climate, and human and ecosystem health (1-3). Atmospheric models currently  
45 generate aerosol sulfate either via condensation of H<sub>2</sub>SO<sub>4</sub>, which is formed via gas-  
46 phase oxidation of SO<sub>2</sub>, or via a suite of oxidation processes involving SO<sub>2</sub> dissolved  
47 in cloudwater. Although the aerosol liquid water content (AWC) is generally much  
48 lower than cloud liquid water, it is possible that such aerosol multiphase oxidation  
49 processes may be important in polluted and high relative humidity conditions. However,  
50 it is uncertain whether the kinetics of aqueous oxidation of dissolved SO<sub>2</sub> by different  
51 oxidants investigated in bulk solution with low ionic strength (< 5 molal) are applicable  
52 to the high solute concentration situations that prevail for aerosol particles. Measuring  
53 the kinetics of aqueous oxidation of dissolved SO<sub>2</sub> in aerosol particles is thus critical to  
54 the accurate modeling of aerosol sulfate in the atmosphere.

55       Assessing the rate of aerosol sulfate formation in polluted conditions can evaluate  
56 the atmospheric importance of multiphase oxidation processes. In particular, rapid  
57 sulfate production has been observed during cloud-free, severe haze events in China,  
58 with the peak sulfate mass concentration reaching as high as ~ 300 μg m<sup>-3</sup> (4-8).  
59 However, current air-quality models that include gas-phase oxidation of SO<sub>2</sub> by the  
60 hydroxyl radical (9) and aqueous oxidation of dissolved SO<sub>2</sub> by hydrogen peroxide  
61 (H<sub>2</sub>O<sub>2</sub>) (10), O<sub>3</sub> (10), O<sub>2</sub> catalyzed by transition metal ions (TMI, i.e., Fe (III) and Mn  
62 (II)) (11-14), methyl hydrogen peroxide (15), and peroxyacetic acid (15) cannot capture  
63 these high levels of aerosol sulfate (5, 16, 17), indicating that our understanding of

64 sulfate formation chemistry is fundamentally incomplete. Oxidation of dissolved SO<sub>2</sub>  
65 by NO<sub>2</sub> may be important if the aerosol pH is high (4, 6) and inclusion of a hypothetical  
66 heterogeneous oxidation process in aerosol particles can greatly improve the model  
67 performance (17). Overall, the formation mechanism of the missing sulfate source  
68 remains unclear and controversial (4, 6, 18-26).

69 Oxidation experiments with high solute strength aerosol face significant  
70 challenges due to the need for online measurement of the reaction kinetics using aerosol  
71 particles, and the necessity for good control of AWC and aerosol pH (27). Sulfate  
72 formation rates for many aqueous SO<sub>2</sub> oxidation pathways involving O<sub>3</sub>, O<sub>2</sub>+TMI, and  
73 NO<sub>2</sub> are strongly pH-dependent (6) and are subject to 1 to 2 orders of magnitude change  
74 if the pH changes by 1 unit because the solubility and effective Henry's law constant of  
75 SO<sub>2</sub> positively depend on pH (28). This sensitivity of sulfate formation rates to pH  
76 poses experimental challenges in controlling aerosol pH because product hydrogen ions  
77 (H<sup>+</sup>) will perturb the aerosol pH. As an exception, the rate of aqueous oxidation of  
78 dissolved SO<sub>2</sub> by H<sub>2</sub>O<sub>2</sub> is largely pH-independent for pH above 2 because the effects  
79 arising from the pH dependence of the SO<sub>2</sub> solubility and the reaction rate constant  
80 offset each other (10). This characteristic makes the SO<sub>2</sub>-H<sub>2</sub>O<sub>2</sub> reaction a useful system  
81 to isolate the effects of solute strength from aerosol pH on the sulfate formation rate.

82 Here, we study pH-buffered submicrometer, deliquesced aerosol particles in an  
83 aerosol flow tube to create high solute strengths, enabling direct investigation of the  
84 kinetics of aqueous oxidation of dissolved SO<sub>2</sub> by H<sub>2</sub>O<sub>2</sub> in aerosol particles. Six types  
85 of seed aerosols were investigated, with aerosol pH buffered at 2.3 to 4.8 as calculated

86 using the E-AIM model (29, 30) and a Pitzer activity coefficient model (31): A) a  
87 mixture of sodium chloride (NaCl)/malonic acid/sodium bimalonate (molar ratios  
88 20:1:1, 6:1:1, 2:1:1 and aerosol pH 2.3–2.5), B) NaCl/sodium bimalonate/sodium  
89 malonate (molar ratios 20:1:1, 6:1:1, 2:1:1 and aerosol pH 4.8), C) sodium nitrate  
90 (NaNO<sub>3</sub>)/malonic acid/sodium bimalonate (molar ratio 20:1:1 and aerosol pH 2.8), D)  
91 NaNO<sub>3</sub>/sodium bimalonate/sodium malonate (molar ratio 20:1:1 and aerosol pH 4.0),  
92 E) malonic acid/sodium bimalonate (molar ratio of 1:1 and aerosol pH 2.8), and F)  
93 sodium bimalonate/sodium malonate (molar ratio of 1:1 and aerosol pH 3.9).

94 In part, the individual aerosol particles components were chosen to be  
95 representative of species found in the atmosphere. More importantly, they satisfy the  
96 demands of the experiment (see detailed explanation in *SI Appendix*, section S1) by  
97 providing different aerosol pH and different AWC (32), and by enabling explicit  
98 examination of the effects of aerosol pH and solute strength on the sulfate formation  
99 rate. Aerosol mass spectrometry (33) (AMS) quantitatively characterized the  
100 composition of seed aerosols and the sulfate that forms. A scanning mobility particle  
101 sizer (SMPS) was used to measure particle-size distributions and to determine the AWC.  
102 All experiments were performed at 21 to 25 °C and high relative humidity (RH) (73 to  
103 90%) to ensure that the seed aerosol particles are deliquesced; see Methods and *SI*  
104 *Appendix*, section S1 for details on the experimental conditions, choice of aerosol  
105 systems to study, instrument operation, and data analysis.

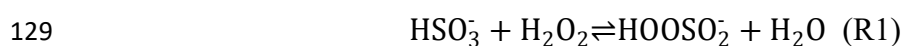
106 The overall goal of this work is to measure the sulfate formation rates on aerosol  
107 particles with high solute concentrations, to enable comparison with the literature

108 parameters that have previously been obtained in bulk solutions. The results will  
109 provide an improved quantitative understanding of sulfate aerosol formation during  
110 severe haze pollution events.

## 111 **Results**

112 The kinetics of aqueous oxidation of dissolved SO<sub>2</sub> by H<sub>2</sub>O<sub>2</sub> in a mixture of NaCl and  
113 malonic acid buffer aerosol particles (molar ratio of 20:1:1) at pH 2.5 are shown in Fig.  
114 1. Results for the other aerosol types are qualitatively similar and shown in *SI Appendix*  
115 Fig. S3. The partial pressures of SO<sub>2</sub> and H<sub>2</sub>O<sub>2</sub> were kept constant and in excess in each  
116 experiment so that the aerosol sulfate that forms is solely dependent on the reaction  
117 time. The dissolved sulfate concentrations, [SO<sub>4</sub><sup>2-</sup>] (molality units), show strong linear  
118 correlations ( $r^2 > 0.96$ ) with the reaction time (Figs. 1A and C). As well, the slopes of  
119 the sulfate formation rate versus initial SO<sub>2</sub> and H<sub>2</sub>O<sub>2</sub> concentrations using log-log plots  
120 (Figs. 1B and D) are close to unity ( $1.03 \pm 0.14$  and  $1.19 \pm 0.03$ , respectively),  
121 suggesting first-order reactions in dissolved SO<sub>2</sub> and H<sub>2</sub>O<sub>2</sub>. Except for some data points  
122 associated with the particles containing NaCl or NaNO<sub>3</sub>, the estimated buffer capacity  
123 is higher than the amount of H<sup>+</sup> formed (see *SI Appendix*, section S1). It is possible that  
124 HCl or HNO<sub>3</sub> evaporate from the particles under those conditions, removing acidity.  
125 Nevertheless, the strong correlations in Fig. 1A and C show no signs of a slower  
126 reaction when a large amount of sulfate forms.

127 Overall, these observations are consistent with the assumed mechanism for the  
128 reaction (34):







132 As well, it is known that weak acids, HX, can act as proton donors to promote the  
 133 reaction through general acid catalysis:



135 The overall rate expression (34, 35) valid for  $\text{pH} > 2$  is:

136 
$$\frac{d\text{SO}_4^{2-}}{dt} = (k + k_{\text{HX}} [\text{HX}][\text{H}^+]^{-1}) K_{\text{a}1} H_{\text{SO}_2} P_{\text{SO}_2} H_{\text{H}_2\text{O}_2} P_{\text{H}_2\text{O}_2} \quad (1)$$

137 where  $k = k_{\text{R}3} K_{\text{R}1} K_{\text{R}2}$ , and  $k_{\text{R}3}$  is a reaction rate coefficient,  $K_{\text{R}1}$  and  $K_{\text{R}2}$  are  
 138 thermodynamic equilibrium constants,  $K_{\text{a}1}$  is the thermodynamic dissociation constant  
 139 of  $\text{H}_2\text{SO}_3$ , and  $H_i$  and  $P_i$  represent the Henry's law constant and partial pressure of  
 140 species  $i$ , respectively.  $k_{\text{HX}}$  is the overall rate constant for the general acid catalysis  
 141 mechanism. We note that Eq. 1 is only applicable to ideal solutions. Known  
 142 modifications to Eq. 1 for ionic strength effects are presented in *SI Appendix*, Table S4.

143 To convert the measured sulfate formation rate to units of  $\mu\text{g m}^{-3} \cdot \text{h}^{-1}$ , which are  
 144 used for comparison to field measurements, the following equation was used:

145 
$$\frac{d\text{SO}_4^{2-}}{dt} (\mu\text{g m}^{-3} \text{h}^{-1}) = 3600 \text{ s h}^{-1} \cdot 96 \text{ g mol}^{-1} \cdot \frac{d\text{SO}_4^{2-}}{dt} (\text{molal s}^{-1}) \cdot \frac{\text{AWC}}{\rho_w} \quad (2)$$

146  
 147 where AWC is in units of  $\text{mg m}^{-3}$  and  $\rho_w$  is the water density in  $\text{kg L}^{-1}$ . Note that in  
 148 previous studies (6, 19), an equivalent expression was employed with the sulfate  
 149 formation rate in units of  $\text{M s}^{-1}$ . While this is appropriate for dilute conditions, for  
 150 solutions with high ionic strength the aerosol liquid water volume is substantially  
 151 smaller than the total aerosol volume and so Eq. 2 is more accurate. As a result, we

152 determine the  $\text{SO}_2$ - and  $\text{H}_2\text{O}_2$ -dependent sulfate formation rates in molal  $\text{s}^{-1}$ , as  
153 illustrated by the slopes in Fig. 1A and C.

154 Fig. 2A and B show the ratio of the measured sulfate formation rates to the  
155 modeled ones for all six types of seed aerosol as a function of total solute concentration  
156 and ionic strength, respectively. Modeled sulfate formation rates were calculated based  
157 on the literature parameters of  $\text{SO}_2$  oxidation by  $\text{H}_2\text{O}_2$  obtained in bulk solutions,  
158 without taking the effects of ionic strength and general acid catalysis into account; see  
159 *SI Appendix*, section S2 for details. Overall, the measured sulfate formation rates are  
160 higher than the modeled values. For the mixed NaCl and malonic acid buffer aerosol  
161 particles with low ionic strengths ( $I < 7$  molal) and low concentrations of malonic acid  
162 ( $< 0.6$  molal) (Exp 1 through 7 and 12), the measured sulfate formation rates are  $2.1 \pm$   
163  $0.1 - 2.9 \pm 0.6$  times larger than the modeled ones. Overall, we conclude for these  
164 particles types that the pH does not affect the kinetics between pH values of 2.3 and 4.8.  
165 This is consistent with the bulk solution kinetics in the literature for solution pH values  
166 above 2.

167 For the more concentrated solutions ( $I > 7$  molal), the ratio of the measured to the  
168 modeled sulfate formation rate displays strongly increasing trends with increasing  
169 malonic acid concentration and ionic strength as shown in Fig. 2B. The ratio is as high  
170 as  $33 \pm 4$  to  $51 \pm 9$  for the malonic acid buffer aerosol particles at pH 3.9 with ionic  
171 strength of around 14 molal. We believe there are at least 2 effects driving the increase:  
172 general acid catalysis by malonic acid and ionic strength effects. In addition, there is

173 possibility of salting-in effects of  $\text{SO}_2$  and  $\text{H}_2\text{O}_2$  at high solute strengths, including the  
174 impact of high buffer concentrations, that are difficult to estimate.

175 To illustrate the general acid effects, the measured sulfate formation rate increases  
176 with malonic acid concentration for the mixed NaCl and malonic acid buffer aerosol  
177 particles at pH 2.3 to 2.4 at relatively constant ionic strengths of 3.9 and 6.6 molal (*SI*  
178 *Appendix*, Fig. S6 and Table S1, Exp# 13 through 18).

179 To isolate the ionic strength effect, it is necessary to account for the general acid  
180 catalyzed enhancement. To do this, we linearly fit the two  $k_{\text{HX}}$  reaction rate coefficients  
181 that we measured (*SI Appendix*, Fig. S6) as a function of ionic strength (*SI Appendix*,  
182 Fig. S7A), and use this fit to account for the general acid effect according to Eq. 1. The  
183 dependence of  $k_{\text{HX}}$  on ionic strength arises because  $k_{\text{HX}}$  is dependent on the  $\text{pK}_a^*$  of the  
184 general acid (*SI Appendix*, Fig. S7B) and the first  $\text{pK}_a^*$  of malonic acid depends on  
185 ionic strength (*SI Appendix*, Fig. S7C), where  $K_a^*$  is the stoichiometric dissociation  
186 constant. From this analysis we conclude that the general acid catalysis effect on the  
187 systems with highest ionic strength (14 molal) is negligible and that the significant  
188 increase of the sulfate formation rate is largely due to the effect of ionic strength on the  
189 proton-catalyzed mechanism and, potentially, the salting-in of reactants as well. This is  
190 consistent with previous studies at lower ionic strengths ( $\sim 5$  molal NaCl) that have  
191 found enhancements in the proton-catalysis reaction rate coefficient  $k$  (34) and the  
192 Henry's law constant of  $\text{H}_2\text{O}_2$  (36) (*SI Appendix*, Fig. S5). Referring to the reaction  
193 mechanism above, the strong dependence of the rate constant on ionic strength arises  
194 by lowering the stoichiometric dissociation constant of  $\text{HOOSO}_2\text{H}$  (reverse of Reaction

195 R2) (34). In particular, at high ionic strength there will be less water to stabilize the ions  
196 into which HOOSO<sub>2</sub>H dissociates.

197 Relative to modeled rates in pure water, we plot the dependence of the  
198 enhancement factor of only the proton-catalyzed sulfate formation rate on ionic strength  
199 in Fig. 2C, i.e., the general acid catalyzed sulfate formation rate was subtracted from  
200 the measured sulfate formation rate to yield the proton-catalyzed sulfate formation rate  
201 (see details in *SI Appendix*, section S3). This factor reflects the overall effects of ionic  
202 strength on the reaction rate coefficient  $k$ , Henry's law constants of H<sub>2</sub>O<sub>2</sub> and SO<sub>2</sub>, and  
203 the first stoichiometric dissociation constant of H<sub>2</sub>SO<sub>3</sub>. We note that some data points  
204 are negative after correcting for the general acid effects. The enhancement factor is ~  
205 1.5 at ionic strengths of 2 to 6.5 molal. This is relatively good agreement given that we  
206 estimate that the uncertainties in our rates is on the order of a factor of two, when  
207 considering individual uncertainties in the kinetics plots, sulfate quantification, and  
208 determination of AWC. The enhancement factor increases to  $33 \pm 4$  to  $51 \pm 9$  at ionic  
209 strengths of 14 molal. For comparison, the modeled enhancement factors for ionic  
210 strength of 0 to 5 molal solutions were calculated using parameters obtained in bulk  
211 solutions (34, 36, 37); see *SI Appendix*, section S2 for details. The model results were  
212 also extrapolated to ionic strength of up to 43 molal using the functional formula  
213 derived in the past using much more dilute solutions. The high enhancement factors at  
214 high ionic strength ranges, which are within those (13 through 43 molal) of urban  
215 pollution episodes (6), indicate that ionic strength effects on the aqueous oxidation of  
216 SO<sub>2</sub> by H<sub>2</sub>O<sub>2</sub> in aerosol particles should be considered in air quality models.

## 217 **Discussion**

218 By directly investigating the kinetics of aqueous oxidation of dissolved SO<sub>2</sub> by H<sub>2</sub>O<sub>2</sub> in  
219 aerosol particles under well-controlled experimental conditions, we have examined  
220 solute strength effects on the sulfate formation rate. The major result is that there is an  
221 enhancement in the kinetics above the rate that prevails in dilute solutions typical of  
222 cloudwater. We believe that the enhancement effect is due to ionic strength effects and  
223 general acid catalysis arising from the malonic acid buffer, as well as potentially to  
224 salting-in of the reactants.

225 Overall, the rate of this multiphase reaction is driven by the volume of liquid water  
226 present. When clouds are present, the liquid water content is many orders of magnitude  
227 higher than in aerosol particles, even for highly polluted conditions. Under such  
228 conditions, SO<sub>2</sub> oxidation will proceed preferentially in the cloud droplets. Similarly,  
229 this aerosol multiphase reaction is unlikely to be important in clean conditions when  
230 the aerosol liquid water content is very low. However, it has the potential to have  
231 atmospheric importance under polluted conditions.

232 To illustrate, Fig. 3 shows the steady-state sulfate formation rates by aqueous SO<sub>2</sub>  
233 oxidation through different reaction pathways in aerosol particles following the  
234 approach of Cheng et al. (6). According to their work and that of Zheng et al. (17), a  
235 missing sulfate source of anywhere from 0.3 to 5 μg m<sup>-3</sup> ·h<sup>-1</sup>, depending on the PM<sub>2.5</sub>  
236 level, is needed to explain the sulfate formation during haze episodes in Beijing in  
237 January 2013 (see figure 3 of ref. (6)). Based on this model (6), the NO<sub>2</sub> reaction  
238 pathway may be the missing sulfate source if the aerosol pH is above 6 while the TMI

239 reaction pathway will dominate sulfate formation if the aerosol pH is below 4.5.  
240 However, ionic strength effects on sulfate formation rate were not taken into account in  
241 the model of Cheng et al. (6).

242 By incorporating the enhancement factors of sulfate formation rate at high ionic  
243 strength (around 14 molal) into the model, the sulfate formation rate for the H<sub>2</sub>O<sub>2</sub>  
244 reaction pathway increases from  $\sim 0.07 \mu\text{g m}^{-3} \text{h}^{-1}$  to  $2.3\text{--}3.6 \mu\text{g m}^{-3} \text{h}^{-1}$ . Recently, Ye et  
245 al. (18) have reported that H<sub>2</sub>O<sub>2</sub> concentrations during Beijing haze events were more  
246 than 1 order of magnitude higher than the value (0.01 ppb) assumed in the model of  
247 Cheng et al. (6). By updating the model with a H<sub>2</sub>O<sub>2</sub> concentration of 0.1 ppb, the sulfate  
248 formation rate for the H<sub>2</sub>O<sub>2</sub> reaction pathway increases to  $23.2\text{--}36.0 \mu\text{g m}^{-3} \text{h}^{-1}$ .

249 We also investigated the effects of ionic strength on the aqueous TMI-catalyzed  
250 oxidation rate of dissolved SO<sub>2</sub> by O<sub>2</sub> in aerosol particles. We find that the sulfate  
251 formation rate is slower by a factor of  $\sim 85$  at an ionic strength of 2.8 molal compared  
252 to that in dilute solution; see *SI Appendix*, section S4 for details. By taking the impact  
253 of ionic strength on the TMI reaction pathway into consideration, we find that the  
254 sulfate formation rate for the H<sub>2</sub>O<sub>2</sub> reaction pathway is larger than all other reaction  
255 pathways for aerosol pH levels up to 6.2. This pH value exceeds the reported aerosol  
256 pH values (4 to 5) during severe haze episodes in northern China (see ref. (38) and  
257 references therein). As the sulfate formation rate for the H<sub>2</sub>O<sub>2</sub> reaction pathway is  
258 independent of aerosol pH for pH levels above 2, the sulfate formation can be  
259 maintained at a high rate even when the aerosol particles become more acidic.

260 These results draw attention to the rates of formation of H<sub>2</sub>O<sub>2</sub> that are required to  
261 sustain the aerosol-mediated SO<sub>2</sub> oxidation. To our knowledge, the mixing ratio of H<sub>2</sub>O<sub>2</sub>  
262 was not measured for the January 2013 severe haze conditions presented in Fig. 3 (6).  
263 Modeling of H<sub>2</sub>O<sub>2</sub> measurements in Beijing during March 2016 was consistent with a  
264 production rate of 0.5 ppbv d<sup>-1</sup>, with more H<sub>2</sub>O<sub>2</sub> formed via alkene ozonolysis than via  
265 the HO<sub>2</sub> self-reaction (39). Assuming that H<sub>2</sub>O<sub>2</sub> production limits the rate of sulfate  
266 formation, this H<sub>2</sub>O<sub>2</sub> production rate can account for up to 20% of the missing sulfate  
267 source in the January 2013 case and roughly 1/3 of the sulfate formed in January and  
268 February 2015 reported by Wang et al. (4). These estimates are highly uncertain,  
269 however, being dependent on the photochemical conditions that give rise to H<sub>2</sub>O<sub>2</sub>.

270 Our results highlight the important role of high solute strength in sulfate formation  
271 in deliquesced aerosol particles. Specifically, there is the need for an improved  
272 understanding on the role of ionic strength effects on atmospheric aqueous multiphase  
273 chemistry, as pointed out by a recent review of the field of laboratory atmospheric  
274 chemistry (40). As well, the importance of general acid catalysis needs to be considered  
275 not only for the many organic acids that are present under pollution conditions but  
276 potentially also for ammonium ions which are present in aerosol particles at very high  
277 concentrations. While such rate enhancements may arise under any conditions with a  
278 high aerosol liquid water content and solute concentrations, for the specific Chinese  
279 haze situation it is particularly important to assess these effects on the reactions of  
280 organic hydroperoxides, NO<sub>2</sub> and O<sub>3</sub> that also oxidize dissolved SO<sub>2</sub> (41), over a range

281 of aerosol pH. This will permit a more comprehensive assessment of the overall rate of  
282 multiphase sulfur oxidation under cloud-free conditions.

## 283 **Methods**

284 **Aerosol particle generation.** Our goal was to investigate the kinetics of aqueous oxidation of  
285 dissolved SO<sub>2</sub> by H<sub>2</sub>O<sub>2</sub> in high solute strength aerosol particles, achieved by generating pH-buffered  
286 polydisperse deliquesced aerosol particles using a constant output atomizer (TSI 3076) from the  
287 following solutions: A) a mixture of NaCl/malonic acid/sodium bimalonate (10/0.5/0.5 mM,  
288 3/0.5/0.5 mM, and 1/0.5/0.5 mM); B) NaCl/sodium bimalonate/sodium malonate (10/0.5/0.5 mM,  
289 3/0.5/0.5 mM, and 1/0.5/0.5 mM); C) NaNO<sub>3</sub>/malonic acid/sodium bimalonate (10/0.5/0.5 mM); D)  
290 NaNO<sub>3</sub>/sodium bimalonate/sodium malonate (10/0.5/0.5 mM); E) malonic acid/sodium bimalonate  
291 (5/5 mM); and F) sodium bimalonate/sodium malonate (5/5 mM). A small fraction of the humidified  
292 aerosol flow from the atomizer was mixed with a humidified N<sub>2</sub> flow and entered the kinetics flow  
293 tube, resulting in high relative humidity (73-90%) to ensure that the seed aerosol particles are  
294 deliquesced and maintain enough aerosol liquid water to enable aqueous oxidation. Additional  
295 details on generating seed aerosols are provided in *SI Appendix*, section S1.

296 **Flow tube experiments.** A schematic of the full experimental setup is shown in *SI Appendix*, Fig.  
297 S1. All experiments were conducted in a vertically oriented pyrex flow tube (length 95 cm, inner  
298 diameter 6.2 cm) at a total flow rate of 1500 sccm at laminar flow conditions (Reynolds Number  
299 ~34), in which constant flows of SO<sub>2</sub> (10, 25, or 50 sccm carrier gas), gas phase H<sub>2</sub>O<sub>2</sub> (10 or 20  
300 sccm carrier gas), and aerosol particles were well mixed. Gas-phase H<sub>2</sub>O<sub>2</sub> was generated by  
301 bubbling N<sub>2</sub> through an aqueous H<sub>2</sub>O<sub>2</sub> solution (15% or 30% by weight) and injected into the central  
302 portion of the humidified aerosol flow by a movable stainless-steel injector tube that is inserted



303 axially down the center of the flow tube, enabling variable reaction time in a step-wise manner. In  
304 each experiment, the aerosol particles were first characterized in the presence of SO<sub>2</sub> and absence  
305 of H<sub>2</sub>O<sub>2</sub> to quantify the background sulfate concentrations. Then the aqueous oxidation of SO<sub>2</sub> was  
306 initiated by introducing H<sub>2</sub>O<sub>2</sub>. Before entering the instruments for aerosol composition  
307 characterization, the aerosol particles alternatively passed through or bypassed a diffusion dryer to  
308 remove or sustain aerosol water. Experiments with different initial concentrations of SO<sub>2</sub> and H<sub>2</sub>O<sub>2</sub>  
309 as well as seed aerosol types were carried out at 21 to 25 °C and high relative humidity (73 to 90%).  
310 All reported sulfate concentrations were corrected for the background sulfate concentrations. Details  
311 of the experimental setup and procedure are provided in *SI Appendix*, section S1.

312 **Measurements.** Both compact and high-resolution time-of-flight aerosol mass spectrometers (33)  
313 (C-ToF-AMS and HR-ToF-AMS; Aerodyne Research) were deployed to characterize the  
314 concentration and chemical composition of aerosol particles. Prior to the experiments, the ionization  
315 efficiency (IE) of the AMS was calibrated using 300 nm ammonium nitrate particles. The sulfate  
316 was measured in the form of sodium sulfate because the sulfuric acid that was generated in the  
317 reaction was buffered by sodium bimalonate or sodium malonate. Therefore, a sulfate fragmentation  
318 table without water fragments was used (42). The relative ionization efficiency (RIE) of sulfate was  
319 determined for sodium sulfate to be 0.12 and 0.24 for the C-ToF-AMS and HR-ToF-AMS,  
320 respectively, and applied to the quantification of sulfate concentrations. The difference between  
321 sulfate concentrations simultaneously measured by these two AMS was within 10%. A collection  
322 efficiency of unity was assumed for the deliquesced aerosol particles (43). An SMPS (TSI) was used  
323 to measure the particle size distributions. Gas-phase monitors were used to measure SO<sub>2</sub> (Model  
324 43i; Thermo) and H<sub>2</sub>O<sub>2</sub> (PI2114; PICARRO) gas-phase mixing ratios. Details regarding the

325 comprehensive calibration and operation of the AMS are described in *SI Appendix*, section S1.

326 **Calculation of aerosol pH, sulfate molality and ionic strength.** The relative concentrations of the  
327 solutes in the aerosol particles were assumed to be the same as in the solution in the atomizer with  
328 no fractionation, resulting in aerosol particles pH buffered at 2.3 to 4.8, estimated using the E-AIM  
329 model (29, 30) and a Pitzer activity coefficient model (31). Here, pH is defined as the negative  
330 logarithm with base 10 of the molality-based  $H^+$  activity.

$$331 \quad \text{pH} = -\log_{10}(\gamma_{H^+} m_{H^+}) \quad (3)$$

332 where  $\gamma_{H^+}$  and  $m_{H^+}$  represent the molality-based activity coefficient and molality of  $H^+$ , respectively.

333 For the mixture of NaCl and organic buffer, the molalities of all ions and neutral species were first  
334 estimated using the E-AIM model which were then input to the Pitzer model to calculate the  
335 equilibrium speciation to determine the aerosol pH. Given that the Pitzer model is developed for  
336 systems with NaCl and relatively low concentrations of malonic acid species, the aerosol pH for  
337 other systems (i.e. with no NaCl present) was estimated using the E-AIM model only. For  
338 comparison, the Pitzer model gave approximately 0.4 unit lower pH values for the mixture of  
339 NaCl/malonic acid/sodium bimalonate and 1 unit higher pH values for the mixture of NaCl/sodium  
340 bimalonate/sodium malonate compared to the E-AIM model results (*SI Appendix*, Fig. S9). We note  
341 that 1 unit difference of pH will not impact our conclusions given that the enhancement factors for  
342 the proton-catalyzed sulfate formation rate at the highest ionic strength (~14 molal) are pH-  
343 independent (*SI Appendix*, section S5 and Fig. S10A).

344 The sulfate molality was calculated from the sulfate concentrations ( $\mu\text{g m}^{-3}$ ) and aerosol liquid  
345 water volume, which was determined as the volume difference between the deliquesced and  
346 effloresced aerosol particles bypassing or passing through the diffusion dryer. We note that there is

347 an inherent assumption that the molar volumes of the solutes are the same in the dry and wet cases.  
348 For comparison, the aerosol liquid water volume was also determined by multiplying the total  
349 measured aerosol volume by the ratio of the aerosol liquid water volume to the total aerosol volume  
350 estimated using the E-AIM model, resulting in an enhancement factor of  $19 \pm 3$  to  $30 \pm 5$  for the  
351 proton-catalyzed sulfate formation rate at ionic strengths of 14 molal (*SI Appendix*, section S5 and  
352 Fig. S10B). This does not impact our conclusion that the oxidation of SO<sub>2</sub> by H<sub>2</sub>O<sub>2</sub> in aerosol  
353 particles can contribute to the missing sulfate source during severe haze episodes.

354 The ionic strength was calculated via the following equation:

$$355 \quad I = \frac{1}{2} \sum m_i z_i^2 \quad (4)$$

356 where  $m_i$  and  $z_i$  represent the molality of each ion and its corresponding charge, respectively. The  
357 ionic strength was estimated using the E-AIM model (29) assuming the relative composition of the  
358 aerosol particles to be the same as in the solution (*SI Appendix*, Table S1).

359 **Data availability.** All data are available from the corresponding author on request.

## 360 **Acknowledgments**

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## 363 **Author contributions**

364 T.L. and J.A. designed the research project; T.L. performed the research; T.L., S.C., and J.A.  
365 analyzed data and T.L. and J.A. wrote the paper.

## 366 **Competing interests**

367 The authors declare no competing interests.

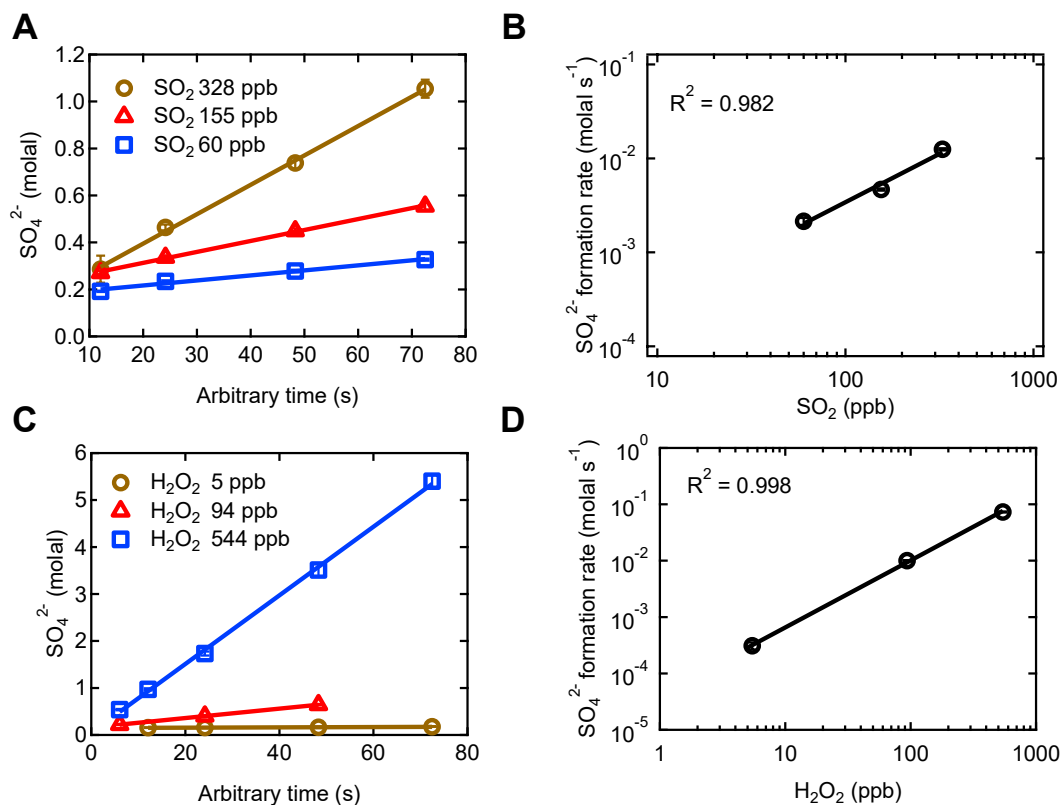
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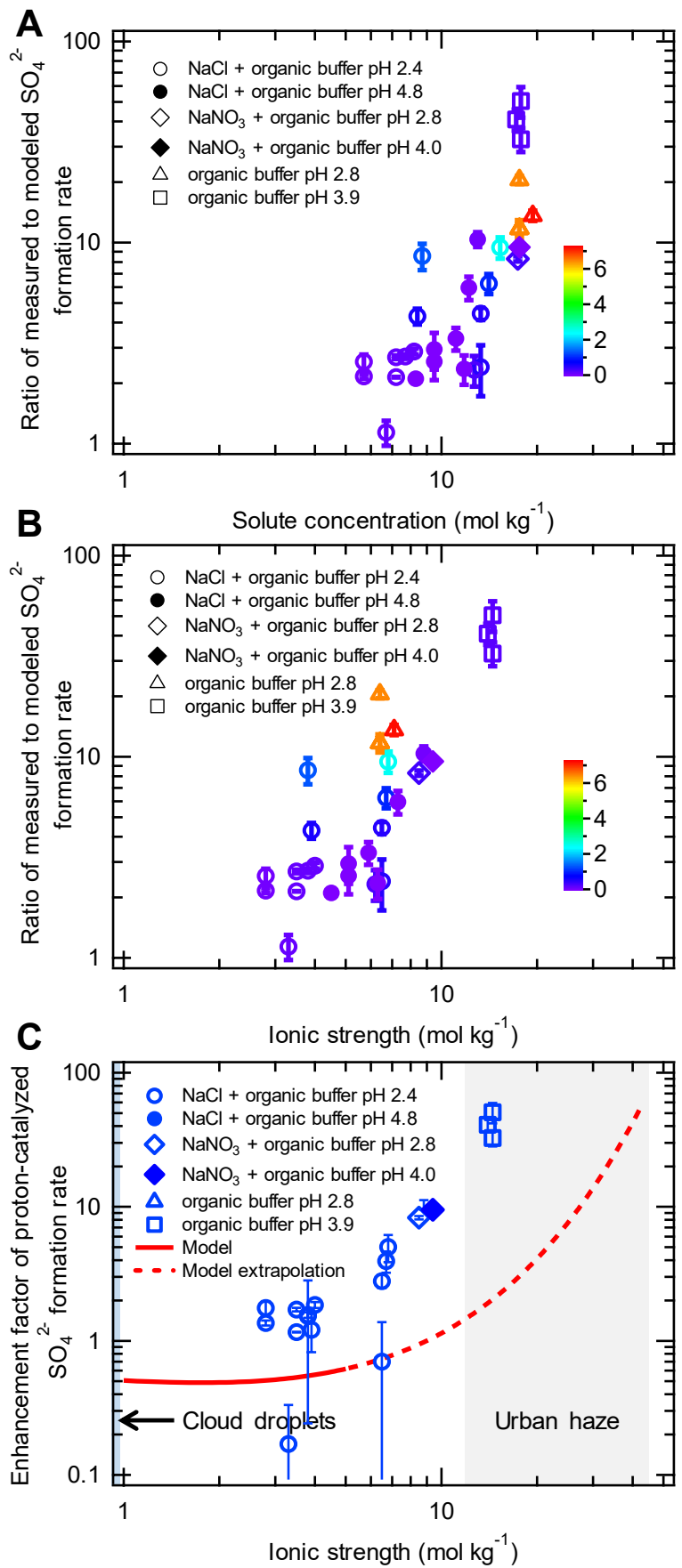
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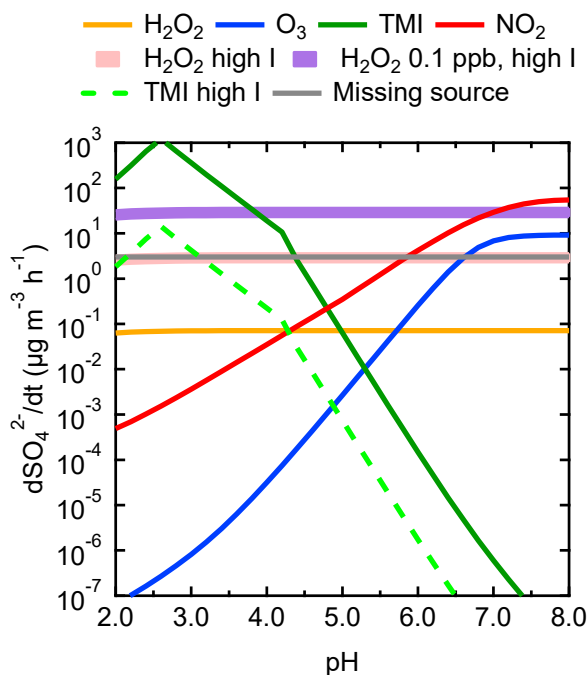
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472 **Fig. 1. Kinetics of aqueous oxidation of SO<sub>2</sub> by H<sub>2</sub>O<sub>2</sub> in a mixture of NaCl and**  
 473 **malonic acid buffer aerosol particles (molar ratio of 20:1:1) at pH 2.5. (A)** Sulfate  
 474 concentrations (units of molal) as a function of reaction time for initial SO<sub>2</sub>  
 475 concentrations of 60, 155, and 328 ppb, for a H<sub>2</sub>O<sub>2</sub> mixing ratio of 94 ppb (*SI Appendix*,  
 476 Table S1, Exp 7 through 9). **(B)** Dependence of sulfate formation rate (molal s<sup>-1</sup>) on  
 477 initial SO<sub>2</sub> concentrations, for a H<sub>2</sub>O<sub>2</sub> mixing ratio of 94 ppb. **(C)** Sulfate concentrations  
 478 as a function of reaction time for initial H<sub>2</sub>O<sub>2</sub> concentrations of 5, 94, and 544 ppb,  
 479 for a SO<sub>2</sub> mixing ratio of 340 ppb (*SI Appendix*, Table S1, Exp 10 through 12). **(D)**  
 480 Dependence of sulfate formation rate on initial H<sub>2</sub>O<sub>2</sub> concentrations, for an SO<sub>2</sub> mixing  
 481 ratio of 340 ppb. All error bars represent 1 SD; they are generally smaller than the  
 482 symbol size.





484 **Fig. 2. Ratio of the measured to modeled sulfate formation rates and enhancement**  
485 **factor of proton-catalyzed sulfate formation rate. (A)** Dependence of the ratio of the  
486 measured to modeled sulfate formation rate on total solute concentration and malonic  
487 acid concentrations for a mixture of NaCl and organic buffer aerosol particles (circle  
488 symbols), NaNO<sub>3</sub> and organic buffer aerosol particles (rhombus symbols) and organic  
489 buffer aerosol particles at aerosol pH of 2.8 (triangle symbols) and 3.9 (square symbols).  
490 **(B)** Same as Fig. 2A but plotted against ionic strength. See *SI Appendix*, Fig. S4 for an  
491 equivalent plot where RH is indicated. **(C)** Dependence of the enhancement factor of  
492 proton-catalyzed sulfate formation rate on ionic strength. The calculated proton-  
493 catalyzed sulfate formation rates for organic buffer aerosol particles at aerosol pH of  
494 2.8 and most data for the NaCl and organic buffer aerosol particles at aerosol pH of 4.8  
495 were negative and so are not plotted. The model results (solid line) describe the effects  
496 of ionic strength on the proton-catalyzed sulfate formation rate measured in bulk  
497 solutions (34, 36, 37). The model extrapolation is shown as a dashed red line. Light  
498 blue- and gray-shaded areas indicate characteristic ionic strength ranges for cloud  
499 droplets and aerosol particles during urban haze episodes, respectively. All error bars  
500 are derived from the uncertainties of the measured sulfate formation rates.



501

502 **Fig. 3. Sulfate formation rates by aqueous SO<sub>2</sub> oxidation in aerosol particles under**

503 **severe haze conditions.** Colored solid lines represent sulfate formation rates calculated

504 for different reaction pathways at conditions of: [SO<sub>2</sub> (g)] = 40 ppb, [H<sub>2</sub>O<sub>2</sub> (g)] = 0.01

505 ppb, [NO<sub>2</sub> (g)] = 66 ppb, [O<sub>3</sub> (g)] = 1 ppb, pH-dependent concentrations of [Fe (III)]

506 and [Mn (II)] (6), AWC = 300 µg m<sup>-3</sup>, aerosol droplet radius R<sub>p</sub> = 0.15 µm, T = 271 K,

507 and I = 0 molal. The total soluble Fe and Mn are 18 and 42 ng m<sup>-3</sup>, respectively. The Fe

508 (III) concentration may be limited by the solubility of Fe(OH)<sub>3</sub> in which case the

509 saturated concentration of Fe(III) was estimated from the solubility product equilibrium

510 constant of Fe(OH)<sub>3</sub> (K<sub>sp</sub> = 2.6 × 10<sup>-38</sup>) (44). The pink-shaded area represents the sulfate

511 formation rate for H<sub>2</sub>O<sub>2</sub> reaction pathway accounting for the rate enhancement at I = 14

512 molal (and [H<sub>2</sub>O<sub>2</sub> (g)] = 0.01 ppb). The purple-shaded area represents the sulfate

513 formation rate for H<sub>2</sub>O<sub>2</sub> reaction pathway at I = 14 molal and a higher concentration of

514 [H<sub>2</sub>O<sub>2</sub> (g)] = 0.1 ppb as observed during Beijing haze events (18). The dashed green

515 line indicates the sulfate formation rate for TMI reaction pathway accounting for the

516 impact of ionic strength. The grey line shows a missing sulfate formation rate of 3 µg

517 m<sup>-3</sup> · h<sup>-1</sup> as a reference. This figure is constructed using the characteristic data conditions

518 from ref. 6 along with additional components related to our analysis.

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7 Supplementary Information for  
8

9 Fast oxidation of sulfur dioxide by hydrogen  
10 peroxide in deliquesced aerosol particles

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20 **This PDF file includes:**

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22       Supplementary text  
23       Figures S1 to S10  
24       Tables S1 to S5  
25       SI References  
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## 34 **Supplementary Information Text**

### 35 **1 Flow tube experiments and instrument operation**

#### 36 **1.1 Flow tube experiments**

37 A schematic of the experimental setup is shown in Fig. S1. All experiments were conducted  
38 in a vertically oriented pyrex flow tube (length 95 cm, inner diameter 6.2 cm) at a total  
39 flow rate of 1500 sccm at laminar flow conditions ( $Re \sim 34$ ). The interior walls of the flow  
40 tube were coated with a thin layer of halocarbon wax to minimize the wall loss of  $SO_2$  and  
41  $H_2O_2$ . A constant output atomizer (TSI Aerosol Generator 3076), operated at a flow rate of  
42 3 slpm, was used to generate pH-buffered polydisperse deliquesced aerosol particles from  
43 the following solutions: A. a mixture of NaCl/malonic acid/sodium bimalonate (10/0.5/0.5  
44 mM, 3/0.5/0.5 mM, and 1/0.5/0.5 mM), B. NaCl/sodium bimalonate/sodium malonate  
45 (10/0.5/0.5 mM, 3/0.5/0.5 mM, and 1/0.5/0.5 mM), C.  $NaNO_3$ /malonic acid/sodium  
46 bimalonate (10/0.5/0.5 mM), D.  $NaNO_3$ /sodium bimalonate/sodium malonate (10/0.5/0.5  
47 mM), E. malonic acid/sodium bimalonate (5/5 mM), and F. sodium bimalonate/sodium  
48 malonate (5/5 mM). The solutions were freshly prepared before each experiment. A  
49 fraction of the humidified aerosol flow was passed through a Kr-85 neutralizer (TSI Inc.)  
50 and mixed with a humidified  $N_2$  flow and a dry  $SO_2$  flow and then entered the kinetics flow  
51 tube from the side inlet perpendicular to the flow tube. The majority of the atomizer output  
52 went to the exhaust. The humidified  $N_2$  flow was produced by bubbling  $N_2$  gas (from liquid  
53  $N_2$ ) through MilliQ water.  $SO_2$  was delivered by a flow of 10, 25, or 50 sccm from a  
54 cylinder (11 ppm in  $N_2$ , Linde) to achieve three different  $SO_2$  concentrations in the flow  
55 tube. Three different gas-phase  $H_2O_2$  mixing ratios were achieved by bubbling 10 sccm  $N_2$   
56 gas through an aqueous  $H_2O_2$  solution (15% by weight) and 20 sccm  $N_2$  gas through a 15%  
57 or 30%  $H_2O_2$  solution. The  $H_2O_2$  flow was introduced into the central portion of the

58 humidified aerosol flow through a 3-mm O.D. PFA Teflon tube shielded with a 6-mm O.D.  
59 movable stainless steel injector tube that is inserted axially down the center of the flow  
60 tube, enabling variable reaction times. The flow was drawn down the flow tube by the  
61 pumping action of a scanning mobility particle sizer (SMPS), an aerosol mass spectrometer  
62 (AMS), an SO<sub>2</sub> monitor, and an additional pump. For supplementary experiments, an H<sub>2</sub>O<sub>2</sub>  
63 monitor was connected instead of the pump to quantify the H<sub>2</sub>O<sub>2</sub> concentrations in the  
64 absence of seed aerosols. All experiments were carried out at 21-25 °C and RH of 73-90%  
65 (Table S1). RH was measured by an in-line digital hygrometer (Vaisala M170). The RH  
66 was controlled by adjusting the humidity of the humidified N<sub>2</sub> flow and kept constant to  
67 within ~1% over the course of an experiment. Note that all the H<sub>2</sub>O<sub>2</sub>/SO<sub>2</sub> experiments were  
68 conducted in N<sub>2</sub> carrier gas to minimize the potential for O<sub>2</sub> oxidation of the SO<sub>2</sub>.

69 For each kinetics run, the aerosol particles were first characterized in the presence of  
70 SO<sub>2</sub> and the absence of H<sub>2</sub>O<sub>2</sub> to quantify the background sulfate formation between the  
71 interaction of SO<sub>2</sub> and seed aerosols. Then the aqueous oxidation of SO<sub>2</sub> was initiated by  
72 introducing H<sub>2</sub>O<sub>2</sub>. The reaction time was adjusted by pushing the movable injector all the  
73 way in the flow tube in a stepwise manner from 60 cm to 10 cm away from the bottom.  
74 Reverse order of pulling the movable injector all the way out did not affect the sulfate  
75 formation rate. Fig. S2 shows the time series of RH, SO<sub>2</sub>, particle volume, organics and  
76 sulfate concentrations for a typical experiment. As described above, the RH was stable over  
77 the course of the experiment. The sulfate concentration decreased with the decrease of the  
78 reaction time while the volumes of dry and wet aerosol particles remained relatively  
79 invariable. For the quantification of sulfate, the background sulfate signal was subtracted  
80 from the total steady-state sulfate concentrations. The contributions of background sulfate

81 to the total steady-state sulfate concentrations were all less than 7%. For aerosol particles  
82 with only organic buffer present, the estimated buffer capacity (defined as the amount of  
83  $H^+$  needed to change the pH by 1 unit) can buffer 2.5 – 4.3 molal of  $H^+$ , which is typically  
84 higher than the amount of  $H^+$  formed. However, for the particles containing NaCl or  $NaNO_3$ ,  
85 the estimated buffer capacity is 0.1 – 1.3 molal of  $H^+$ , which is lower than the amount of  
86  $H^+$  formed for some data points. It is possible that HCl or  $HNO_3$  evaporate from the  
87 particles under those conditions, removing acidity.

## 88 **1.2 Instrument operation**

89 Compact and high-resolution time-of-flight aerosol mass spectrometers (1) (C-ToF-AMS  
90 and HR-ToF-AMS; Aerodyne Research) were deployed to characterize the concentration  
91 and chemical composition of aerosol particles for experiments with and without NaCl  
92 present, respectively. The HR-ToF-AMS was operated in the high sensitivity V-mode with  
93 a time resolution of 1 minute. The toolkit Squirrel 1.60Q and Pika 1.20Q were used to  
94 analyze the AMS data. The concentration of sulfate ( $\mu g\ m^{-3}$ ) was calculated by summing  
95 the nitrate-equivalent masses of each high-resolution ion associated with the sulfate  
96 fraction. The sulfate was measured in the form of sodium sulfate since the sulfuric acid that  
97 forms was buffered by sodium bimalonate or sodium malonate. For sodium sulfate, there  
98 is no pathway to produce water fragments after vaporization and ionization. Therefore, a  
99 sulfate fragmentation table without water fragments was used (2). Prior to the experiments,  
100 the ionization efficiency (IE) of the AMS was calibrated using 300 nm ammonium nitrate  
101 particles. The relative ionization efficiency (RIE) of sulfate was determined for sodium  
102 sulfate. Polydisperse pure sodium sulfate was atomized to the AMS and SMPS  
103 simultaneously. The sodium sulfate particles were passed through a diffusion dryer to

104 remove aerosol water before they were sampled to the SMPS, while they were kept in the  
105 liquid phase without passing through a diffusion dryer prior to characterization by AMS,  
106 wherein the collection efficiency of particles was assumed to be unity (3). The particle size  
107 distributions measured by SMPS were converted to mass concentrations using the density  
108 of sodium sulfate of  $2.68 \text{ g cm}^{-3}$  (4), and converted to sulfate concentrations via the sulfate  
109 mass fraction of sodium sulfate. The RIE of sulfate was derived by comparing the sulfate  
110 concentrations measured by AMS and SMPS, determined to be 0.12 and 0.24 for C-ToF-  
111 AMS and HR-ToF-AMS, respectively. The higher RIE for HR-ToF-AMS is likely due to  
112 its higher vaporizer power of 5 Watt than that of 4.6 Watt for C-ToF-AMS. After applying  
113 the RIE calibration, the difference between sulfate concentrations simultaneously  
114 measured by these two AMS was within 10%.

115 The SMPS instrument consists of a differential mobility analyzer (DMA, TSI 3081)  
116 and a condensation particle counter (CPC, TSI 3772). The aerosol and sheath flow rates  
117 were  $0.3$  and  $3 \text{ L min}^{-1}$ , respectively, allowing for a size distribution scans ranging from  
118  $15\text{--}410 \text{ nm}$ .

### 119 **1.3 Choice of aerosol systems**

120 The constraints for the experiment were to: i) work with aerosol components with variable  
121 hygroscopicity, to enable variations in solute strength, ii) have the ability to add pH buffers  
122 to the particles, iii) use aerosol particle solutions for which there are rigorous  
123 thermodynamic predictions of hygroscopicity and acidity, and iv) have the ability for  
124 sulfate yields to be accurately quantified with an aerosol mass spectrometer.

125 As a result, i) We chose to work with NaCl, NaNO<sub>3</sub>, and organic acid particles, given  
126 their variable hygroscopicities. ii) To control the pH, we chose to use organic acid buffers

127 given that the malonate/bimalonate/malonic acid system establishes pH values close to  
128 those of atmospheric aerosol. As well, organic acids are common urban aerosol  
129 constituents. iii) All of the individual components (chloride, sodium, nitrate  
130 malonate/bimalonate/malonic acid) are modelled by the E-AIM thermodynamic model,  
131 allowing for pH and ionic strength assessments. Note, for example, that we considered  
132 using phosphate pH buffers but they are not in E-AIM, nor are they atmospherically  
133 relevant. iv) These experiments cannot be conducted with an aerosol system largely  
134 composed of sulfate (e.g.  $(\text{NH}_4)_2\text{SO}_4$ ) because sulfate is the reaction product, i.e. it is  
135 required to start with low sulfate mass loadings so that the formation of sulfate can be  
136 clearly observed during the reaction. Similarly, we could not use  $\text{NH}_4^+$  as an initial  
137 component of the aerosol particles because the formation of  $(\text{NH}_4)_2\text{SO}_4$  during the reaction  
138 would drastically change the sensitivity of the AMS to sulfate during the experiment  
139 (because the relative ionization efficiency of sulfate in  $(\text{NH}_4)_2\text{SO}_4$  is very different from  
140 that of  $\text{Na}_2\text{SO}_4$ ). In particular, as the reaction proceeded, a varying ratio of  $(\text{NH}_4)_2\text{SO}_4$  to  
141  $\text{Na}_2\text{SO}_4$  would be formed. By only using  $\text{Na}^+$  as the cation in the particles, we are fully  
142 confident that the reaction product is  $\text{Na}_2\text{SO}_4$ , which is a species for which the aerosol mass  
143 spectrometer can be calibrated. As well, by not using  $\text{NH}_4^+$  as the cation, we avoid  
144 complications arising from  $\text{NH}_3$  evaporation, with associated impacts on aerosol pH.

## 145 **2 Modeled $\text{SO}_4^{2-}$ formation rate**

146 Modeled sulfate formation rates were calculated based on the literature parameters of  
147 aqueous  $\text{SO}_2$  oxidation by  $\text{H}_2\text{O}_2$  obtained in bulk solutions, without taking the effects of  
148 ionic strength and general acid catalysis into account. The rate expressions, rate  
149 coefficients and equilibrium constants that we used to calculate the aqueous-phase



150 concentrations of  $\text{SO}_2$  and  $\text{H}_2\text{O}_2$  are shown in Tables S2 and S3, respectively. Note that we  
151 assume the sulfate formation rate in molal  $\text{s}^{-1}$  equals to that in  $\text{M s}^{-1}$  for the dilute solutions.

152 The modeled enhancement factors of sulfate formation rate in the main text Fig. 2C  
153 were calculated based on parameters obtained in bulk solutions (5-7) for ionic strength of  
154 0-5 molal, accounting for the overall effects of ionic strength on the proton-catalyzed  
155 reaction rate coefficient  $k$ , Henry's law constants of  $\text{H}_2\text{O}_2$  and  $\text{SO}_2$ , and the first  
156 stoichiometric dissociation constant of  $\text{H}_2\text{SO}_3$ . The effects of ionic strength on the reaction  
157 rate coefficient  $k$  and equilibrium constants are shown in Table S4 and Fig. S5. With the  
158 increase of ionic strength, the reaction rate coefficient  $k$  decreases first, followed by a  
159 minimum and then an increase while the first stoichiometric dissociation constant of  $\text{H}_2\text{SO}_3$   
160 shows a reverse trend. Increasing the ionic strengths, the Henry's law constants of  $\text{H}_2\text{O}_2$   
161 and  $\text{SO}_2$  show trends of slight increase and decrease, respectively.

162 Also, we performed very preliminary calculations to assess how ionic strength in an  
163 ammonium sulfate particle may affect reactant concentrations, as compared to the results  
164 for  $\text{NaCl}$  and  $\text{NaNO}_3$ . The two Henry's law constants on the right hand side of Equation (1)  
165 of the main paper both involve uncharged solution species. The sulfate ion tends to have a  
166 salting-out effect relative to  $\text{Na}^+$ ,  $\text{Cl}^-$  and  $\text{NO}_3^-$ , so it is expected that the stoichiometric  
167 values of  $\text{H}_{\text{SO}_2}$  and  $\text{H}_{\text{H}_2\text{O}_2}$  are somewhat smaller in a largely  $\text{SO}_4^{2-}$  medium. However, the  
168 activity coefficients of such species generally vary less with the composition of the solution  
169 than do those of ions, consequently the salt effects on the dissociation constant  $K_{a1}^*$  are  
170 likely to be much larger. If it is assumed that the activity coefficients of  $\text{H}^+$  and  $\text{HSO}_3^-$  have  
171 approximately the same values in aqueous  $(\text{NH}_4)_2\text{SO}_4$  as  $\text{H}^+$  and  $\text{HSO}_4^-$ , we calculate that  
172 the stoichiometric value of  $K_{a1}^*$  is increased by the following factors relative to its value in

173 NaCl: 21 (90% RH,  $I_{\text{NaCl}} = 2.8 \text{ mol kg}^{-1}$ ,  $I_{(\text{NH}_4)_2\text{SO}_4} = 9.2 \text{ mol kg}^{-1}$ ) and 68 (80% RH,  $I_{\text{NaCl}} =$   
174  $5.1 \text{ mol kg}^{-1}$ ,  $I_{(\text{NH}_4)_2\text{SO}_4} = 17.5 \text{ mol kg}^{-1}$ ), i.e. this would lead to an enhancement effect in  
175 the kinetics. By contrast, calculations comparing  $\text{NaNO}_3$  and  $\text{NaCl}$  media yield values  
176 similar to each other which is consistent with our experimental results. We neglected the  
177 activity coefficient of  $\text{H}_2\text{SO}_3$  in these calculations, on the assumption that its variation  
178 across the different salt media would be much smaller than that of the product of the  $\text{H}^+$   
179 and  $\text{HSO}_3^-$  activity coefficients. Note that we cannot estimate what the ionic strength  
180 effects are for the rate constant in Equation (1) for sulfate solutions.

### 181 **3 General acid catalysis**

182 Fig. S6 shows that the measured sulfate formation rate increases with the increase of  
183 malonic acid concentration at relatively constant pH and ionic strengths (Exp# 13-18),  
184 providing clear evidence that malonic acid buffer catalyzes the aqueous oxidation of  $\text{SO}_2$   
185 by  $\text{H}_2\text{O}_2$ . The reaction rate coefficient of general acid catalysis  $k_{\text{HX}}$  has been found to be  
186 negatively correlated with the  $\text{pK}_a^*$  of acid (8) (Fig. S7B). Based on this relationship,  
187  $k_{\text{malonic acid}}$  is estimated to be 43 times higher than  $k_{\text{bimalonate}}$ , so the general acid catalysis  
188 induced by bimalonate can be neglected. The  $k_{\text{malonic acid}}$  values for ionic strengths of 3.9  
189 and 6.6 molal were then determined to be  $5.61 \times 10^5$  and  $1.32 \times 10^5 \text{ molal}^{-2} \text{ s}^{-1}$  from Fig. S6.  
190 We linearly fit these two rate constants (Fig. S7A) as a function of ionic strength. The ionic  
191 strength-dependent general acid catalyzed sulfate formation rate was then calculated (using  
192 Equation 1 in the main text) and subtracted from the measured sulfate formation rate to  
193 determine the proton-catalyzed sulfate formation rate. The justification for decreasing  
194 values for  $k_{\text{malonic acid}}$  as a function of ionic strength is that the  $\text{pK}_a^*$  of malonic acid

195 increases with ionic strength for concentrated solutions (Fig. S7C). Fig. S7B demonstrates  
196 that larger values of the  $pK_a^*$  lead to smaller values of  $k_{\text{malonic acid}}$ .

#### 197 **4 TMI experiments**

198 We also utilized the kinetics flow tube to investigate the effects of ionic strength on  
199 aqueous phase TMI catalyzed oxidation of dissolved  $\text{SO}_2$  by  $\text{O}_2$  in aerosol particles. The  
200 experimental conditions are shown in Table S5. The pH-buffered polydisperse deliquesced  
201 aerosol particles with three different concentrations of TMI were prepared by atomizing  
202 the following solutions: a mixture of NaCl/malonic acid/sodium bimalonate (10/0.5/0.5  
203 mM) with 1  $\mu\text{M}$  iron (III) chloride ( $\text{FeCl}_3$ ) and 50  $\mu\text{M}$ , 0.2 mM, and 2 mM manganese (II)  
204 chloride ( $\text{MnCl}_2$ ), respectively. All experiments were conducted at pH of 2.8 to ensure high  
205 solubility of Fe (III). Unlike the  $\text{H}_2\text{O}_2$  experiments, the  $\text{SO}_2$  flow for TMI experiments was  
206 introduced into the central portion of the humidified aerosol flow through the movable  
207 stainless steel tube, enabling variable reaction time. For an experimental run, the aerosol  
208 particles were first characterized in the absence of  $\text{SO}_2$  to quantify the background sulfate  
209 in the seed aerosols. Then the aqueous oxidation of  $\text{SO}_2$  was initiated by introducing  $\text{SO}_2$ .  
210 The TMI experiments were conducted in air as a carrier gas, given that  $\text{O}_2$  is the oxidant.

211 Modeled sulfate formation rates were calculated based on the literature parameters of  
212 aqueous  $\text{SO}_2$  oxidation by TMI+ $\text{O}_2$  obtained in bulk solutions, without taking the effects  
213 of ionic strength into account. The relevant rate expressions, rate coefficients and  
214 equilibrium constants that we used to calculate the aqueous-phase concentrations of  $\text{SO}_2$   
215 are shown in Tables S2 and S3, respectively. Regarding the calculation of Fe (III) and Mn  
216 (II) concentrations in the aerosol particles, the molality of NaCl in the aerosol particles was  
217 first estimated using the E-AIM model (9). The Fe (III) and Mn (II) aerosols were expected

218 to undergo the same degree of concentration after atomization. The molality of Fe (III) and  
219 Mn (II) was then estimated from the NaCl molality accordingly. The Fe (III) concentration  
220 may be limited by the solubility of Fe(OH)<sub>3</sub> in which case the saturated concentration of  
221 Fe (III) was estimated from the solubility product equilibrium constant of Fe (OH)<sub>3</sub> ( $K_{sp} =$   
222  $2.6 \times 10^{-38}$ ) (10). Table S5 shows a comparison between the measured and modeled sulfate  
223 formation rates for the TMI experiments. We find that the sulfate formation rate for TMI  
224 oxidation decreases by a factor of approximately 85 at an ionic strength of 2.8 molal  
225 compared to that calculated for the dilute solution. The effect of ionic strength can be well  
226 described by the extended Debye-Hückel equation (Fig. S8) (11, 12). The fitting parameter  
227 of -3.02 is within the range of -2 for Fe (III) and -4 for Mn (II) (11, 12). In the main paper  
228 Fig. 3, we note that we likely overestimate the sulfate formation rate that will prevail for  
229 the TMI oxidation pathway at high ionic strength by using the inhibition factor obtained at  
230 a lower ionic strength of 2.8 molal.

## 231 **5 Uncertainties of aerosol pH and aerosol liquid water volume**

232 Fig. S9 shows a comparison of aerosol pH for the mixture of NaCl and organic buffer  
233 estimated using the E-AIM and Pitzer models. The Pitzer model gave approximately 0.4  
234 unit lower pH values for the mixture of NaCl/malonic acid/sodium bimalonate and 1 unit  
235 higher pH values for the mixture of NaCl/sodium bimalonate/sodium malonate compared  
236 to the E-AIM model results. The enhancement factors for the proton-catalyzed sulfate  
237 formation rate at the highest ionic strength (~14 molal) remain unchanged when the E-AIM  
238 aerosol pH was used for the calculation (Fig. S10A). Therefore, the aerosol pH differences  
239 between the E-AIM and Pitzer models will not impact our conclusions.

240 We also determined the aerosol liquid water volume by multiplying the total measured  
241 aerosol volume by the ratio of the aerosol liquid water volume to the total aerosol volume  
242 estimated using the E-AIM model. The estimated aerosol liquid water volume is 1.0–1.9,  
243 3.2–3.4, 2.9–4.9, and 1.7–2.0 times higher than the measured aerosol liquid water volume  
244 for the mixture of NaCl and organic buffer, NaNO<sub>3</sub> and organic buffer, organic buffer at  
245 pH 2.8, and organic buffer at pH 3.9, respectively. Consequently, the enhancement factor  
246 for the proton-catalyzed sulfate formation rate at ionic strengths of 14 molal decreases to  
247  $19 \pm 3 - 30 \pm 5$  (Fig. S10B). The sulfate formation rate for the H<sub>2</sub>O<sub>2</sub> reaction pathway in  
248 the main paper Fig. 3 will be lowered to 13.5–21.3  $\mu\text{g m}^{-3} \text{h}^{-1}$ , remaining larger than the  
249 sulfate formation rates from other pathways. Therefore, using the estimated aerosol liquid  
250 water volume in the calculation will not impact our conclusion that the oxidation of SO<sub>2</sub>  
251 by H<sub>2</sub>O<sub>2</sub> in aerosol particles can contribute to the missing sulfate source during severe haze  
252 episodes.

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293

294 **Table S1. SO<sub>2</sub>/H<sub>2</sub>O<sub>2</sub> experimental conditions and results.**

Exp #	Aerosol type <sup>a</sup>	RH (%)	T (°C)	SO <sub>2</sub> (ppb)	H <sub>2</sub> O <sub>2</sub> (ppb)	Aerosol pH <sup>b</sup>	Ionic strength (molal)	Malonic acid (molal)	Bimalonate (molal)	Measured SO <sub>4</sub> <sup>2-</sup> formation rate (molal s <sup>-1</sup> )	Modeled SO <sub>4</sub> <sup>2-</sup> formation rate (molal s <sup>-1</sup> ) <sup>c</sup>	Calculated proton-catalyzed SO <sub>4</sub> <sup>2-</sup> formation rate (molal s <sup>-1</sup> ) <sup>d</sup>
1	A1	74	23	341	94	2.3	6.5	0.547	0.368	0.0112	0.0047	0.0033
2	A1	75	23	347	94	2.3	6.2	0.330	0.224	0.0107	0.0046	
3	B1	78	21	348	94	4.8	6.3	0.027	0.207	0.0129	0.0055	
4	B1	83	22	343	94	4.8	5.1	0.017	0.176	0.0149	0.0051	
5	B1	82	22	343	94	4.8	5.1	0.017	0.176	0.0124	0.0048	
6	B1	86	22	343	94	4.8	4.5	0.013	0.159	0.0101	0.0048	
7	A1	86	22	328	94	2.4	3.8	0.190	0.155	0.0125	0.0046	0.0072
8	A1	90	22	60	94	2.5	2.8	0.137	0.121	0.0021	0.0008	0.0015
9	A1	89	22	155	94	2.5	2.8	0.137	0.121	0.0047	0.0022	0.0029
10	A1	88	22	340	5	2.5	3.3	0.164	0.139	0.00031	0.00027	0.00005
11	A1	87	22	340	544	2.5	3.5	0.177	0.147	0.0730	0.0271	0.0463
12	A1	87	22	340	94	2.5	3.5	0.177	0.147	0.0100	0.0047	0.0054
13	A1	74	23	345	94	2.3	6.5	0.547	0.368	0.0197	0.0044	0.0124
14	A2	73	24	345	94	2.3	6.7	1.060	0.705	0.0272	0.0043	0.0171
15	A3	73	24	345	94	2.3	6.8	2.452	1.664	0.0409	0.0043	0.0217
16	A1	85	25	316	94	2.4	4.0	0.203	0.163	0.0103	0.0036	0.0066
17	A2	85	24	316	94	2.4	3.9	0.595	0.480	0.0156	0.0036	0.0044
18	A3	85	25	316	94	2.4	3.8	1.326	1.083	0.0306	0.0036	0.0055
19	B1	79	24	350	94	4.8	5.9	0.024	0.198	0.0146	0.0044	
20	B2	78	24	350	94	4.8	7.3	0.068	0.584	0.0246	0.0041	
21	B3	78	24	350	94	4.8	8.8	0.121	1.207	0.0427	0.0041	0.0427
22	C	78	23	245	221	2.8	8.5	0.431	0.354	0.0616	0.0074	0.0616
23	D	78	23	245	221	4.0	9.4	0.024	0.343	0.0714	0.0075	0.0714
24	E	73	22	359	94	2.8	7.1	7.055	5.251	0.0683	0.0050	
25	F	74	22	359	94	3.9	14.5	0.256	3.043	0.1644	0.0050	0.1644
26	E	75	21	70	94	2.8	6.4	6.381	4.847	0.0225	0.0011	
27	E	75	21	179	94	2.8	6.4	6.381	4.847	0.0329	0.0028	
28	F	74	21	179	94	3.9	14.5	0.256	3.043	0.1426	0.0028	0.1426
29	E	75	23	349	94	2.8	6.4	6.381	4.847	0.0558	0.0047	
30	F	75	23	349	94	3.9	14.0	0.244	2.947	0.1958	0.0048	0.1958

295 <sup>a</sup> Six types of seed aerosols. A: NaCl/malonic acid/sodium bimalonate (A1: molar ratio of 20:1:1; A2:  
296 molar ratio of 6:1:1; A3: molar ratio of 2:1:1); B: NaCl/sodium bimalonate/sodium malonate (B1: molar  
297 ratio of 20:1:1; B2: molar ratio of 6:1:1; B3: molar ratio of 2:1:1); C: NaNO<sub>3</sub>/malonic acid/sodium  
298 bimalonate (molar ratio of 20:1:1); D: NaNO<sub>3</sub>/sodium bimalonate/sodium malonate (molar ratio of 20:1:1);  
299 E: malonic acid/sodium bimalonate (molar ratio of 1:1); F: sodium bimalonate/sodium malonate (molar  
300 ratio of 1:1).

301 <sup>b</sup> Aerosol pH of type A and B was estimated using the Pitzer model; C, D, E and F was estimated using the  
302 E-AIM model.

303 <sup>c</sup> Modeled sulfate formation rates were calculated based on the literature parameters of aqueous SO<sub>2</sub>  
304 oxidation by H<sub>2</sub>O<sub>2</sub> obtained in bulk solutions, without taking the effects of ionic strength and general acid  
305 catalysis into account.

306 <sup>d</sup> The calculated proton-catalyzed sulfate formation rates were determined by subtracting the general acid  
307 catalyzed sulfate formation rate from the measured sulfate formation rate. For experiments 2-6, 19, 20, 24,  
308 26, 27, and 29, the measured sulfate formation rates were lower than the estimated general acid catalysis  
309 sulfate formation rates; therefore, the calculated proton-catalyzed sulfate formation rates for these  
310 experiments were negative and not presented.



311 **Table S2. Aqueous reactions rate expressions and rate coefficients.**

Oxidants	Sulfate formation rate (molal s <sup>-1</sup> )	Reference
H <sub>2</sub> O <sub>2</sub>	$k'[\text{H}^+][\text{HSO}_3^-][\text{H}_2\text{O}_2(\text{aq})]/(1+K[\text{H}^+])$ $k' = 7.45 \times 10^7 \times e^{(-4430 \times (1/T - 1/298))} \text{ M}^{-2} \text{ s}^{-1}$ $K = 13 \text{ M}^{-1}$	Hoffmann and Calvert (13)
TMI+O <sub>2</sub>	$k_2[\text{H}^+]^{-0.74}[\text{S(IV)}][\text{Mn(II)}][\text{Fe(III)}]$ (pH ≤ 4.2) $k_2 = 3.72 \times 10^7 \text{ M}^{-2} \text{ s}^{-1}$ $k_3[\text{H}^+]^{0.67}[\text{S(IV)}][\text{Mn(II)}][\text{Fe(III)}]$ (pH > 4.2) $k_3 = 2.51 \times 10^{13} \text{ M}^{-2} \text{ s}^{-1}$	Ibusuki and Takeuchi (14)

312

313 **Table S3. Equilibrium constants for calculating aqueous-phase concentrations.**

Species	Aqueous-phase concentration expressions	Equilibrium constants <sup>a</sup>	References
SO <sub>2</sub>	$[H_2SO_3] = H_{SO_2} \times p_{SO_2}$	$H_{SO_2} = 1.23 \times e^{(3145.3 \times (\frac{1}{T} - \frac{1}{298}))}$	Seinfeld and Pandis (15)
	$[HSO_3^-] = K_{a1} \times [H_2SO_3] / [H^+]$	$K_{a1} = 1.3 \times 10^{-2} \times e^{(1960 \times ((\frac{1}{T} - \frac{1}{298})))}$	
	$[SO_3^{2-}] = K_{a2} \times [HSO_3^-] / [H^+]$	$K_{a2} = 6.6 \times 10^{-8} \times e^{(1500 \times ((\frac{1}{T} - \frac{1}{298})))}$	
H <sub>2</sub> O <sub>2</sub>	$[H_2O_2(aq)] = H_{H_2O_2} \times p_{H_2O_2}$	$H_{H_2O_2} = 1.3 \times 10^5 \times e^{(7297.1 \times (\frac{1}{T} - \frac{1}{298}))}$	Seinfeld and Pandis (15)

314 <sup>a</sup>H and K<sub>a</sub> are in units of M atm<sup>-1</sup> and M, respectively.

315 **Table S4. Ionic strength (*I*) effects on aqueous reaction rate coefficient and**  
 316 **equilibrium constants.**

Parameter	Expressions	Notes	References
	$\frac{d\text{SO}_4^{2-}}{dt} = (k + k_{\text{HX}} [\text{HX}][\text{H}^+]^{-1}) K_{a1}^* \text{H}_{\text{SO}_2} P_{\text{SO}_2} \text{H}_{\text{H}_2\text{O}_2} P_{\text{H}_2\text{O}_2}$		
<i>k</i>	$\log\left(\frac{k}{k_{I=0}}\right) = 0.36I - \frac{1.018\sqrt{I}}{1+0.17\sqrt{I}}$	<i>I</i> <sub>max</sub> = 5 molal	Maaß et al. (6)
H <sub>H<sub>2</sub>O<sub>2</sub></sub>	$\frac{H_{\text{H}_2\text{O}_2}}{H_{\text{H}_2\text{O}_2}^{I=0}} = 1 - 1.414 \times 10^{-3} I^2 + 0.121I$	<i>I</i> <sub>max</sub> = 5 molal	Ali et al. (7)
H <sub>SO<sub>2</sub></sub>	$\log\left(\frac{H_{\text{SO}_2}}{H_{\text{SO}_2}^{I=0}}\right) = \left(\frac{22.3}{T} - 0.0997\right) \times I$	<i>I</i> <sub>max</sub> = 6 molal	Millero et al. (5)
K <sub>a1</sub> <sup>*</sup>	$\log\left(\frac{K_{a1}^*}{K_{a1}^{I=0}}\right) = 0.5 \times \sqrt{I} - 0.31 \times I$	<i>I</i> <sub>max</sub> = 6 molal	Millero et al. (5)
K <sub>a2</sub> <sup>*</sup>	$\log\left(\frac{K_{a2}^*}{K_{a2}^{I=0}}\right) = 1.052 \times \sqrt{I} - 0.36 \times I$	<i>I</i> <sub>max</sub> = 6 molal	Millero et al. (5)

317

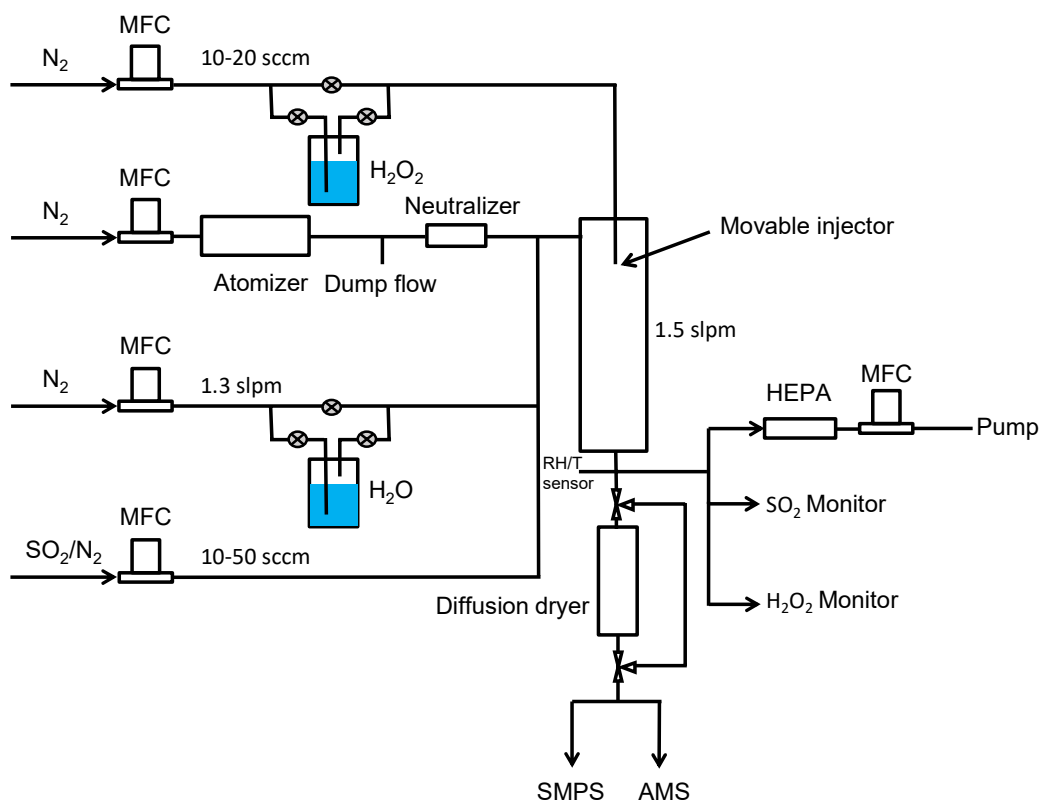
318 **Table S5. SO<sub>2</sub>/TMI experimental conditions and results.**

Exp #	Aerosol type <sup>a</sup>	RH (%)	T (°C)	SO <sub>2</sub> (ppb)	Aerosol pH	Fe (III) (mmolal) <sup>b</sup>	Mn (II) (mmolal) <sup>b</sup>	Ionic strength (molal)	Measured SO <sub>4</sub> <sup>2-</sup> formation rate (molal s <sup>-1</sup> )	Modeled SO <sub>4</sub> <sup>2-</sup> formation rate (molal s <sup>-1</sup> )
31	G	92	22	316	2.8	0.194 <sup>c</sup>	11.5	2.34	0.000621	0.046
32	H	94	22	307	2.8	0.176	352	2.82	0.015	1.277
33	I	94	24	292	2.8	0.176	35.2	1.87	0.0024	0.109

319 <sup>a</sup>Three types of seed aerosols. G: NaCl/malonic acid/sodium bimalonate/FeCl<sub>3</sub>/MnCl<sub>2</sub> (10/0.5/0.5/0.001/0.05  
320 mM) in atomizer solution; H: NaCl/malonic acid/sodium bimalonate/FeCl<sub>3</sub>/MnCl<sub>2</sub> (10/0.5/0.5/0.001/2 mM)  
321 in atomizer solution; I: NaCl/malonic acid/sodium bimalonate/FeCl<sub>3</sub>/MnCl<sub>2</sub> (10/0.5/0.5/0.001/0.2 mM) in  
322 atomizer solution.

323 <sup>b</sup>For each experiment, the molality of NaCl in the aerosol particles was first estimated using E-AIM model  
324 (9). The Fe (III) and Mn (II) aerosols were expected to undergo the same degree of concentration after  
325 atomization. The molality of Fe (III) and Mn (II) was then estimated from the NaCl molality accordingly.

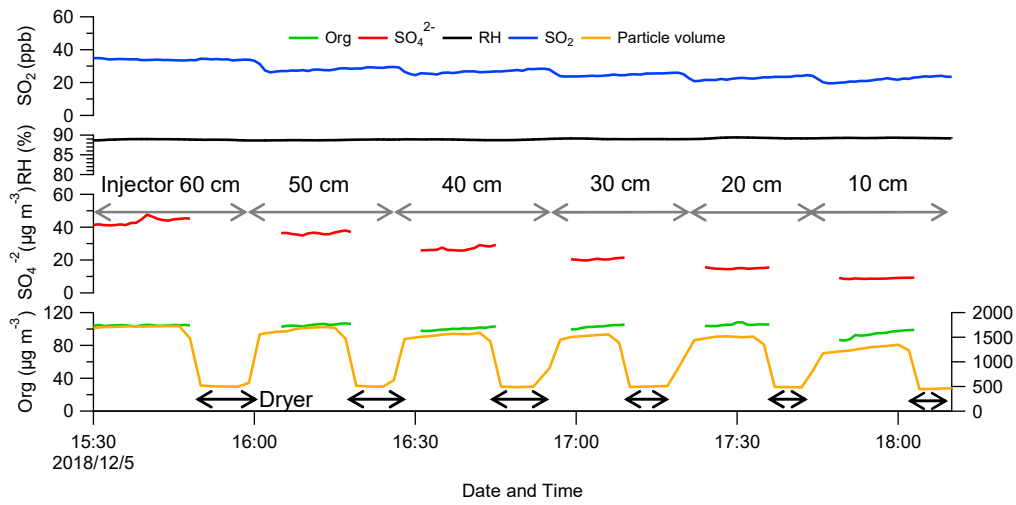
326 <sup>c</sup>The Fe (III) concentration may be limited by the solubility of Fe (OH)<sub>3</sub> for Exp # 31. The saturated  
327 concentration of Fe (III) was estimated from the precipitation equilibrium of Fe (OH)<sub>3</sub> ( $K_{sp} = 2.6 \times 10^{-38}$ )  
328 (10).



329

330 **Fig. S1.** Schematic of the experimental setup.

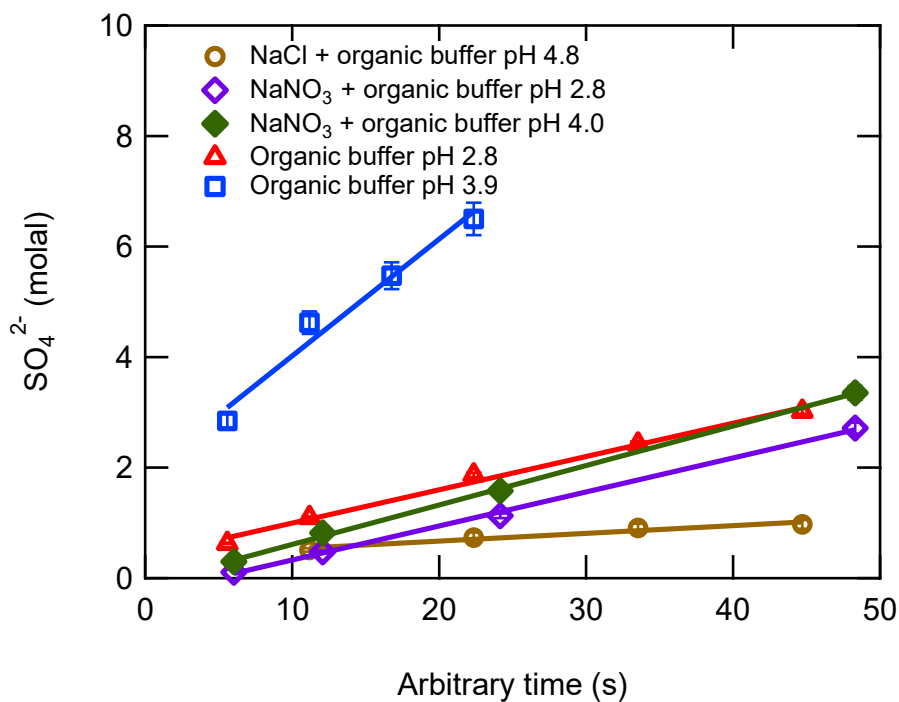
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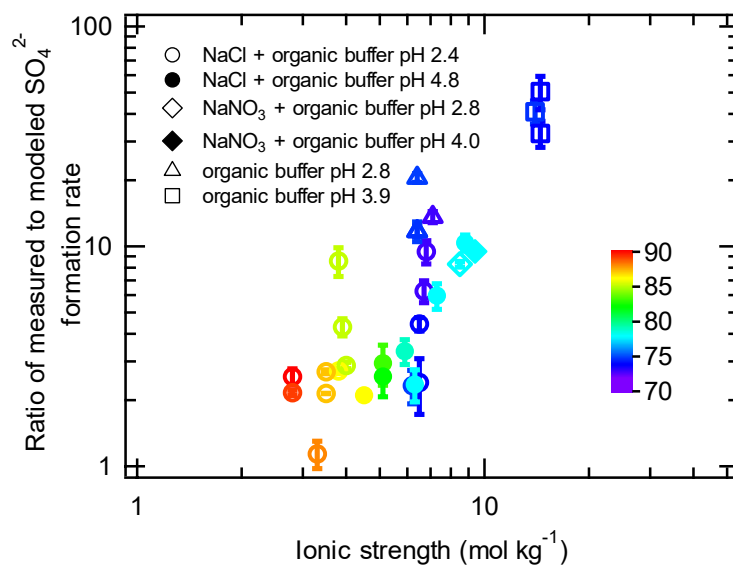
333 **Fig. S2.** Time series of RH, SO<sub>2</sub>, particle volume, organics and sulfate concentrations for  
 334 an experiment during which the aerosol water content was measured at each position,  
 335 showing that it remains stable. For most experiments, the AWC was only measured once  
 336 during the experiment.

337



338

339 **Fig. S3.** Kinetics of aqueous oxidation of SO<sub>2</sub> by H<sub>2</sub>O<sub>2</sub> in a mixture of NaCl and malonic  
 340 acid buffer aerosol particles at pH 4.8 (Exp# 3), NaNO<sub>3</sub> and malonic acid buffer aerosol  
 341 particles at pH 2.8 (Exp# 22) and pH 4.0 (Exp# 23), malonic acid buffer aerosol particles  
 342 at pH 2.8 (Exp# 29) and 3.9 (Exp# 30).

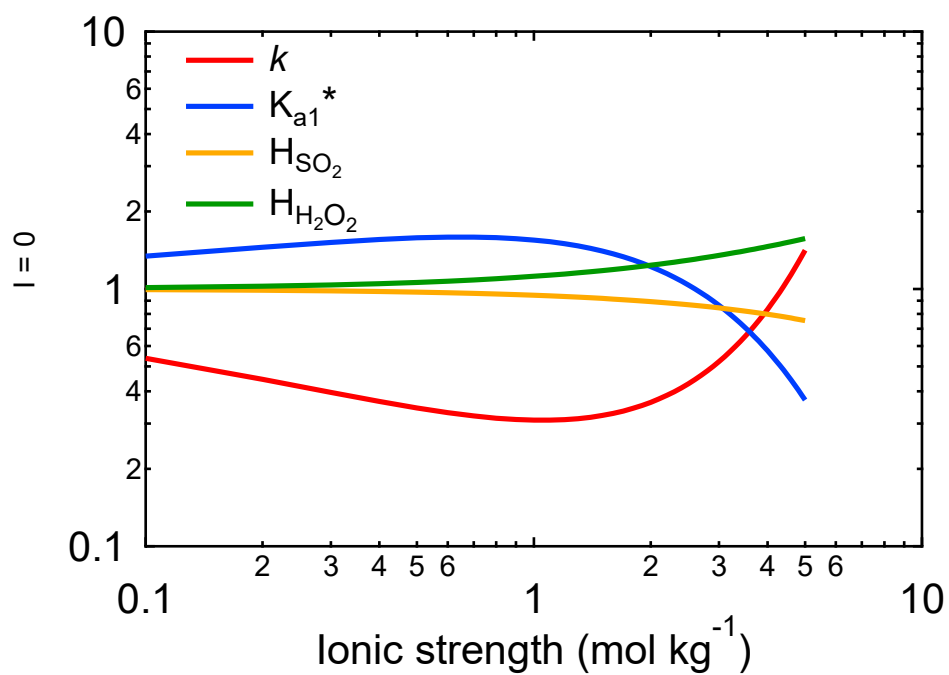


343

344 **Fig. S4.** Dependence of the ratio of the measured to modeled sulfate formation rate on

345 ionic strength and RH.

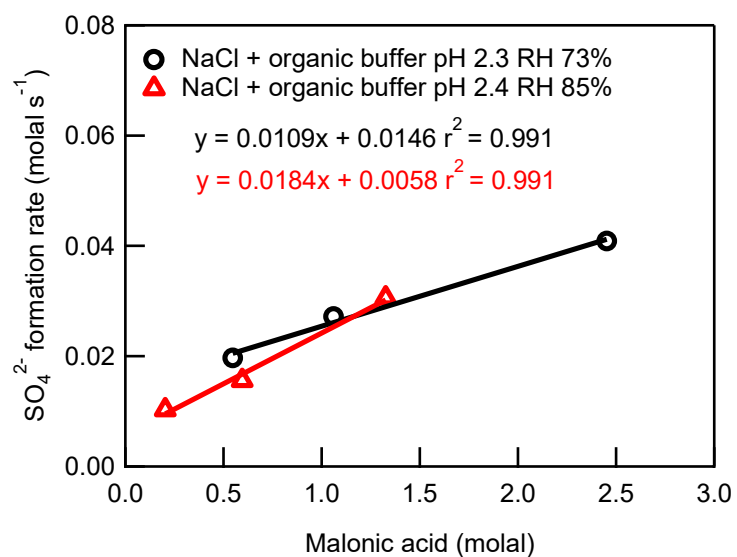




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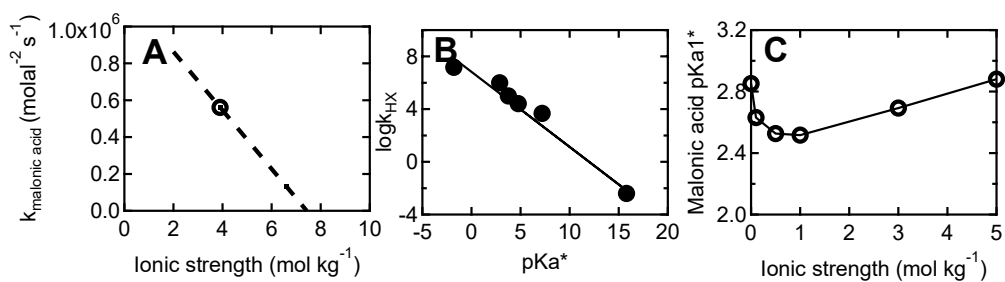
347 **Fig. S5.** Effects of ionic strength on aqueous reaction rate coefficient and stoichiometric  
 348 equilibrium constants for the  $SO_2$ - $H_2O_2$  reaction. The parameter  $p$  represents the reaction  
 349 rate coefficient or equilibrium constants.

350



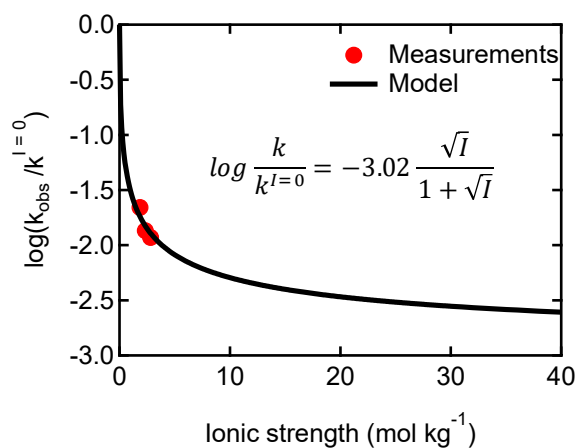
351

352 **Fig. S6.** Plot of sulfate formation rate as a function of malonic acid concentration for a  
 353 mixture of NaCl and malonic acid buffer aerosol particles at pH 2.3 at RH of 73% ( $I =$   
 354 6.6 molal, Exp# 13-15) and pH 2.4 at RH of 85% ( $I = 3.9$  molal, Exp# 16-18).



355

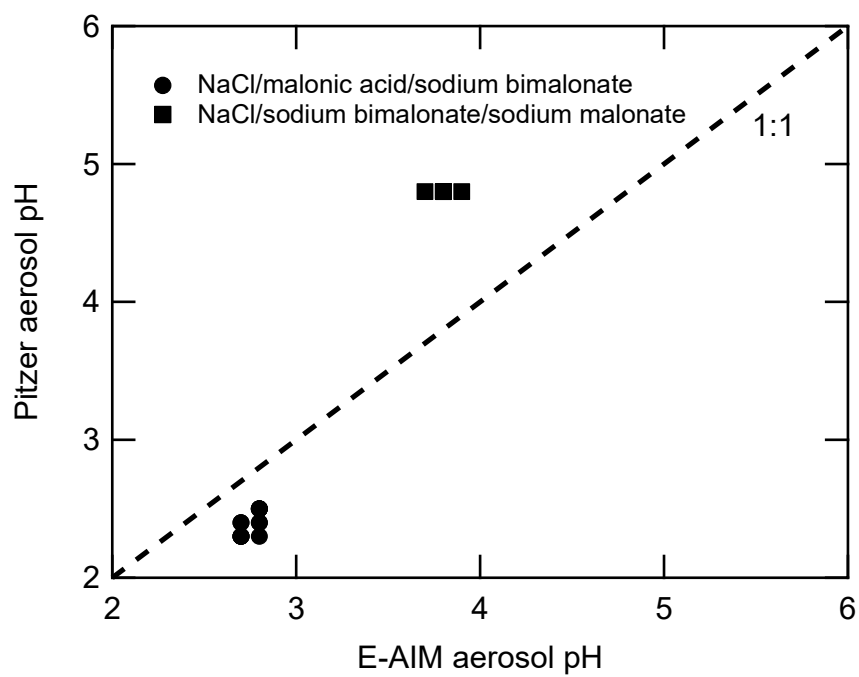
356 **Fig. S7 (A)** Dependence of  $k_{\text{malonic acid}}$  on the ionic strength. The  $k_{\text{malonic acid}}$  data for ion  
 357 strengths of 3.9 and 6.6 molal were determined from Fig. S6, using Equation (1) and the  
 358 calculated molality of  $\text{H}^+$ . The fitting equation is  $k_{\text{malonic acid}} = -1.59 \times 10^5 I + 1.18 \times 10^6$  **(B)** Plot  
 359 of  $\log k_{\text{HX}}$  versus  $\text{pKa}^*$  of acid HX at 285 K and ionic strength of 0.5 molal. This figure is  
 360 adapted from Drexler et al. (8) and the units for  $k_{\text{HX}}$  are  $\text{M}^{-2} \text{s}^{-1}$ . The fitting equation is  $\log$   
 361  $k_{\text{HX}} = -0.57 \text{pKa}^* (\text{HX}) + 6.83$ . **(C)** Dependence of the first  $\text{pKa}^*$  of malonic acid on the  
 362 ionic strength. This figure is adapted from Kettler et al. (16).



363

364 **Fig. S8** Impact of ionic strength on the sulfate formation rate of aqueous phase TMI-  
 365 catalyzed oxidation of dissolved SO<sub>2</sub> by O<sub>2</sub> in aerosol particles. The effect of ionic strength  
 366 can be well described by the extended Debye-Hückel equation (11, 12), shown as an inset  
 367 in the figure. The fitting parameter of -3.02 is within the range of -2 for Fe (III) and -4 for  
 368 Mn (II) (11, 12).

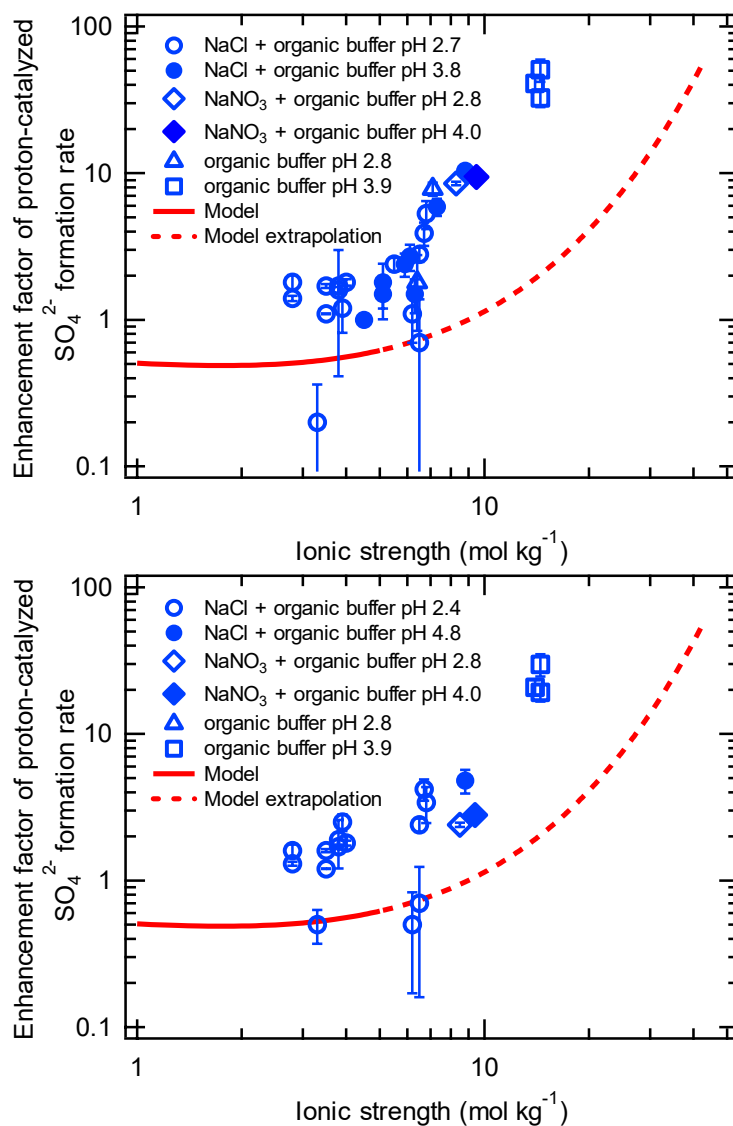
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370

371 **Fig. S9** Comparison of aerosol pH for the mixture of NaCl and organic buffer calculated  
372 using the Pitzer and E-AIM models.

373



374

375 **Fig. S10** Dependence of the enhancement factor of proton-catalyzed sulfate formation rate  
 376 on ionic strength. **(A)** Aerosol pH for the mixture of NaCl and organic acid buffer was  
 377 estimated using the E-AIM model. **(B)** Aerosol liquid water volume was determined by  
 378 multiplying the total measured aerosol volume by the ratio of the aerosol liquid water  
 379 volume to the total aerosol volume estimated using the E-AIM model.