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FIBER OPTIC BOLOMETER

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Han et al.

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(54) **FIBER OPTIC BOLOMETER**

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G01J 5/08 (2006.01)
G01N 21/41 (2006.01)
G01N 21/45 (2006.01)
G01N 21/47 (2006.01)
G01J 3/45 (2006.01)
G01B 9/02 (2006.01)

(52) **U.S. Cl.**
CPC **G01J 5/0853** (2013.01); **G01J 5/0821** (2013.01); **G01N 21/412** (2013.01); **G01N 21/474** (2013.01); **G01N 2021/458** (2013.01); **G01N 2021/4742** (2013.01)

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CPC G01J 3/26; G01J 5/0821; G01J 5/0853; G01F 1/661; G01N 21/412; G01N 21/474; G02B 6/29359
See application file for complete search history.

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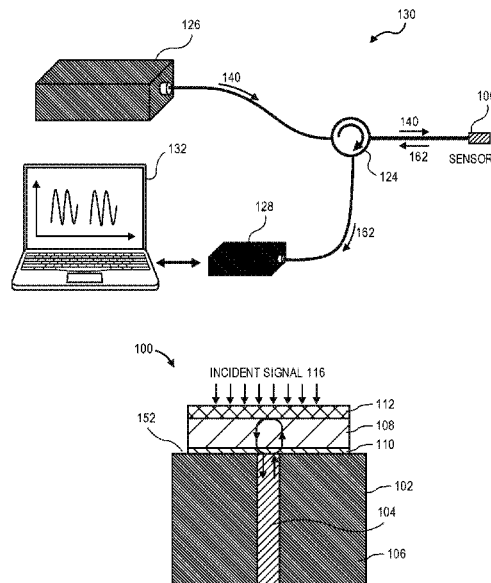
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(57) **ABSTRACT**

The present disclosure is directed to a fiber optic bolometer device. In an implementation, a fiber optic bolometer device includes an optical fiber and a silicon layer that comprises a Fabry-Pérot interferometer. The silicon layer includes a first surface and a second surface. The fiber optic bolometer device includes a reflective dielectric film disposed over the first surface of the silicon layer where the reflective dielectric film is adjacent to an end face of the optical fiber. The fiber optic bolometer device also includes an absorptive coating disposed over the second surface of the silicon layer (e.g., the surface distal to the end face of the optical fiber).

20 Claims, 14 Drawing Sheets



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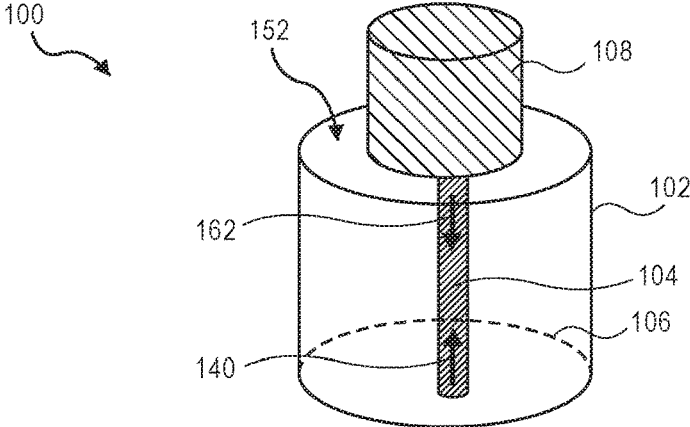


FIG. 1A

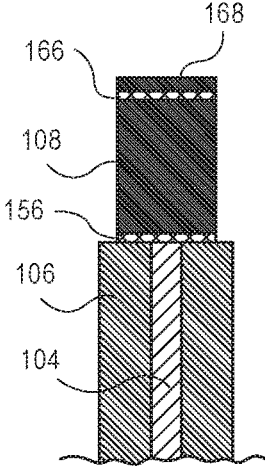


FIG. 1B

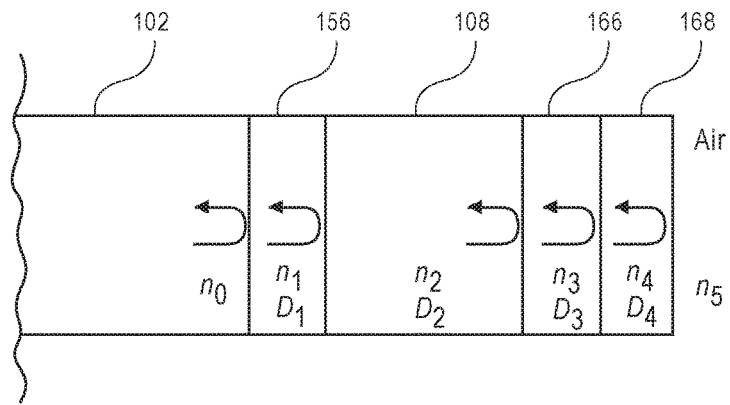


FIG. 1C

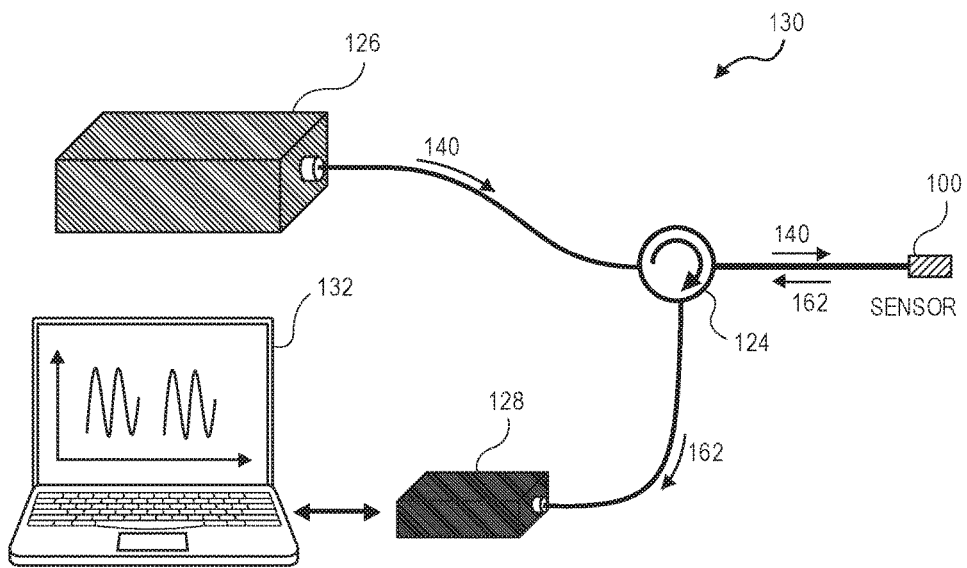


FIG. 1D

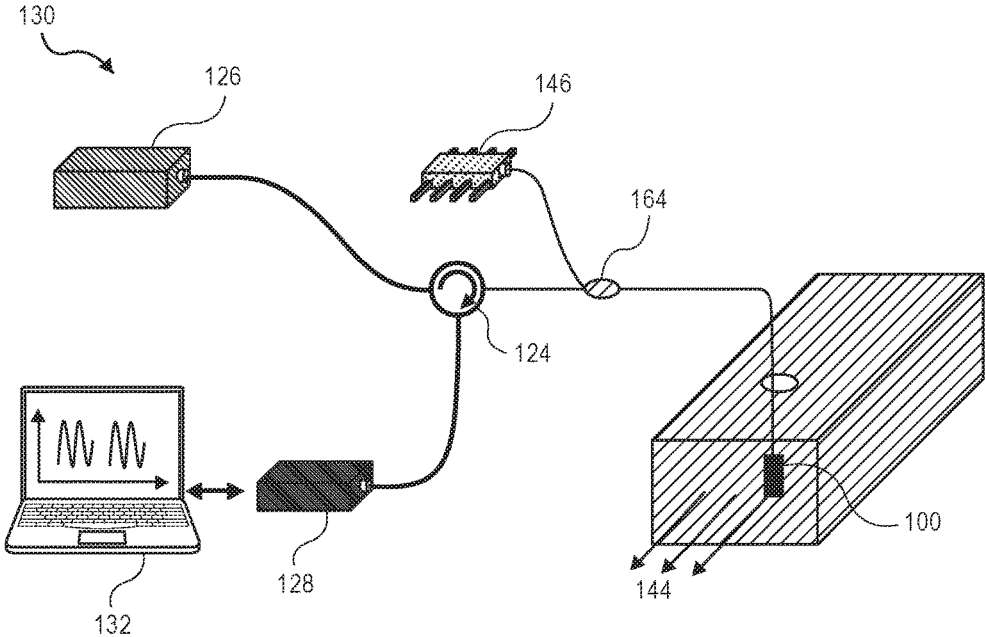


FIG. 1E

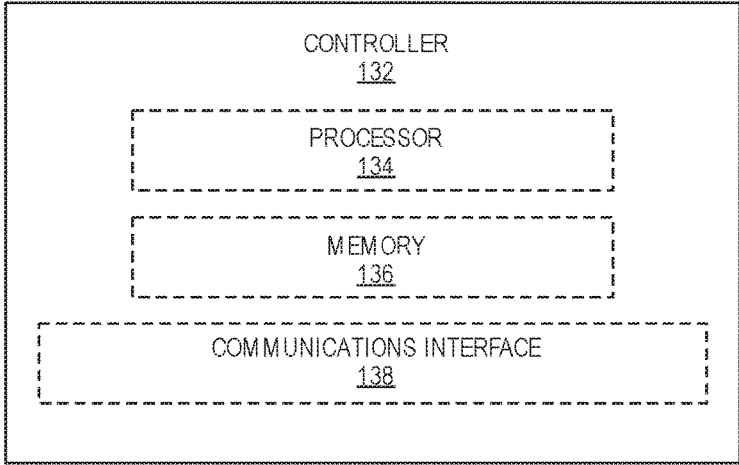


FIG. 1F

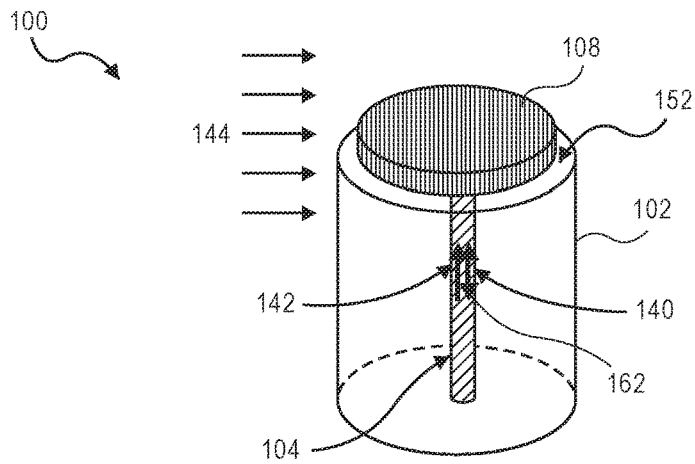


FIG. 1G

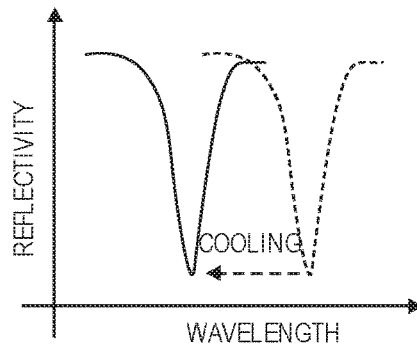


FIG. 1H

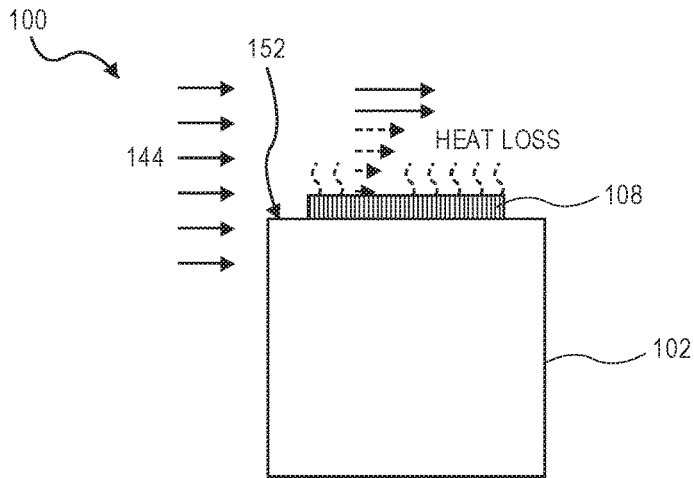


FIG. 1I

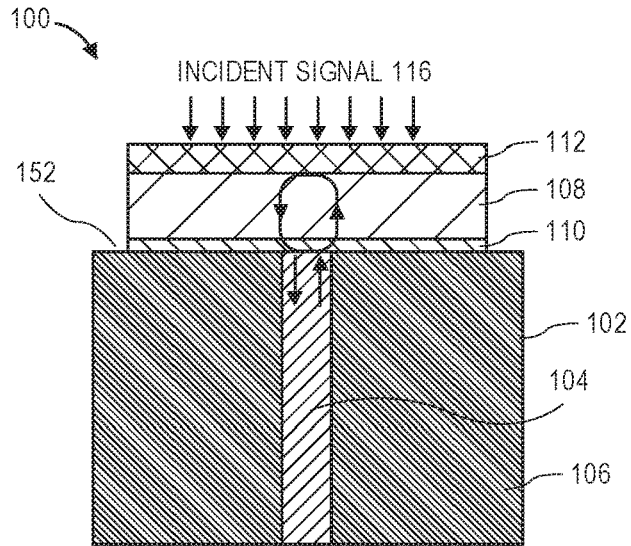


FIG. 1J

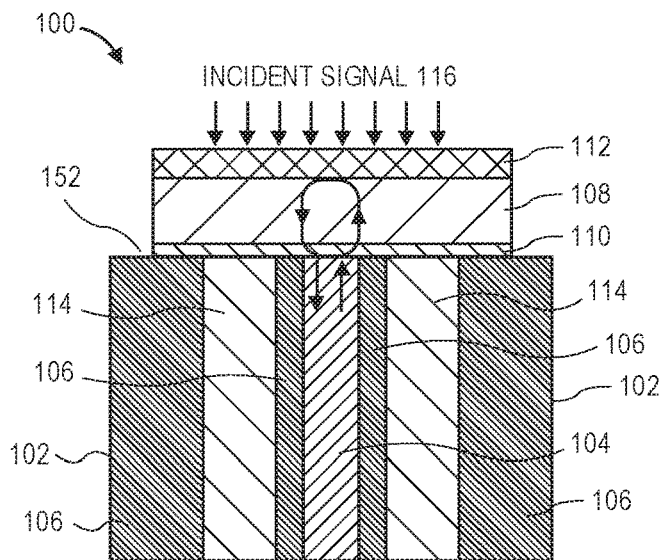


FIG. 1K

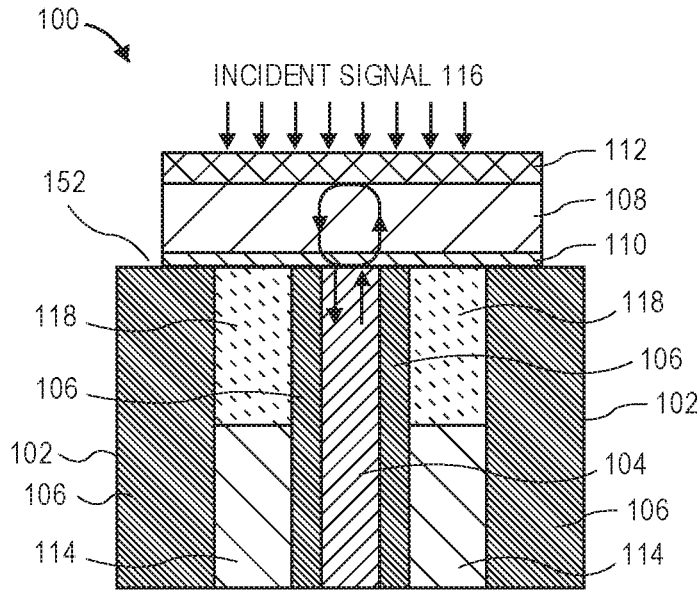


FIG. 1L

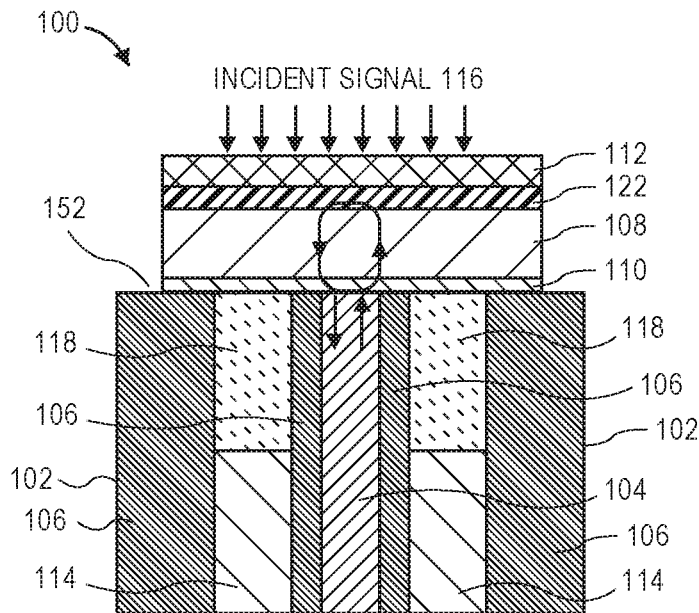


FIG. 1M

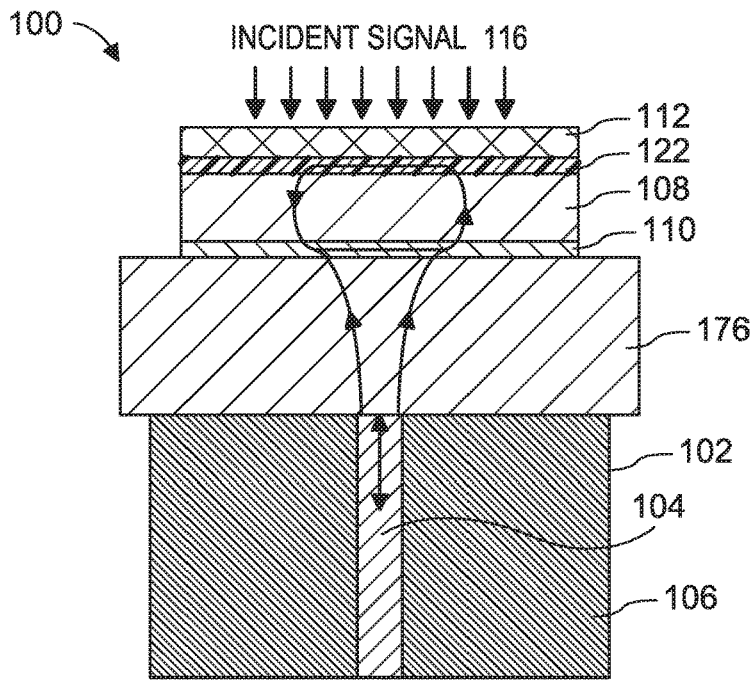


FIG. 1N

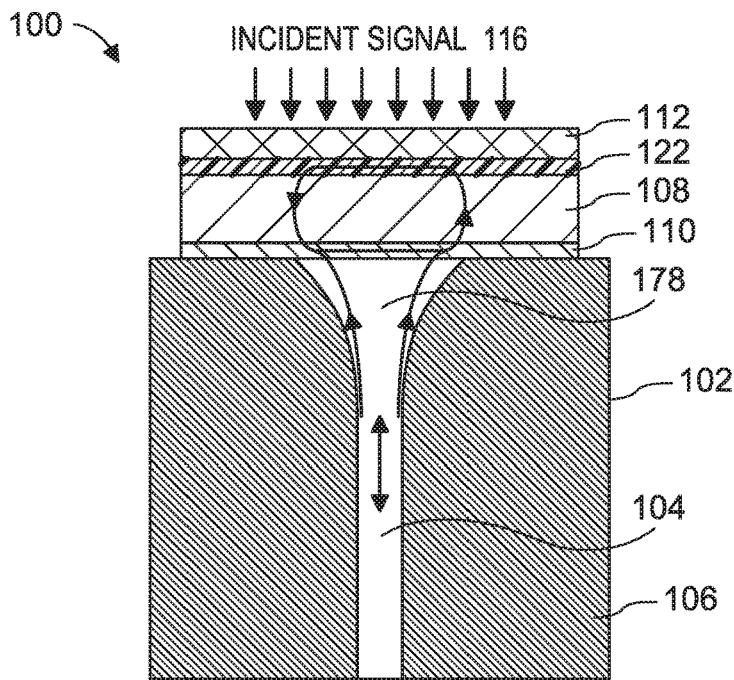


FIG. 1O

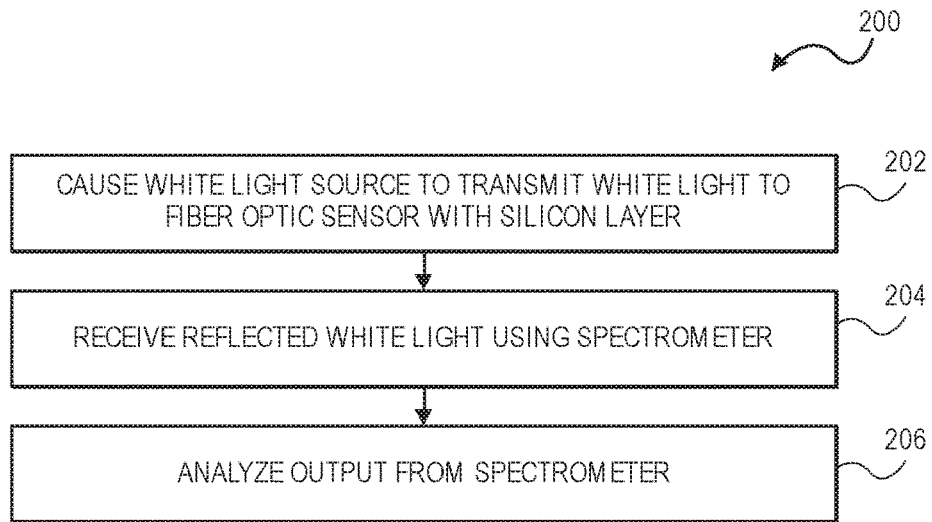


FIG. 2A

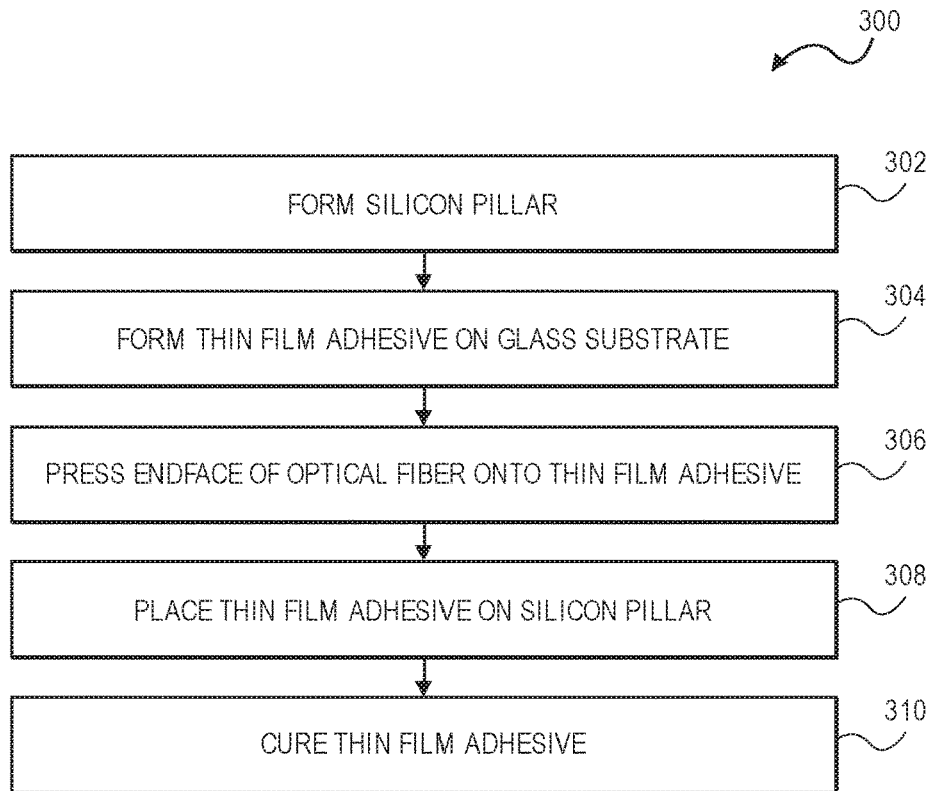


FIG. 2B

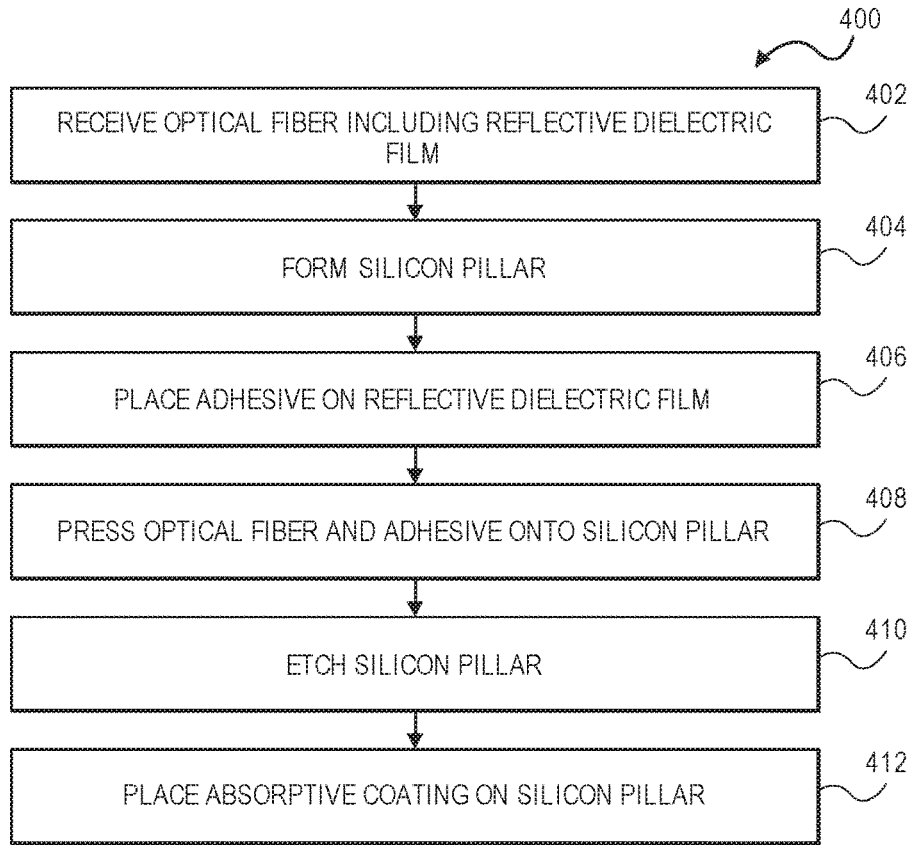


FIG. 2C

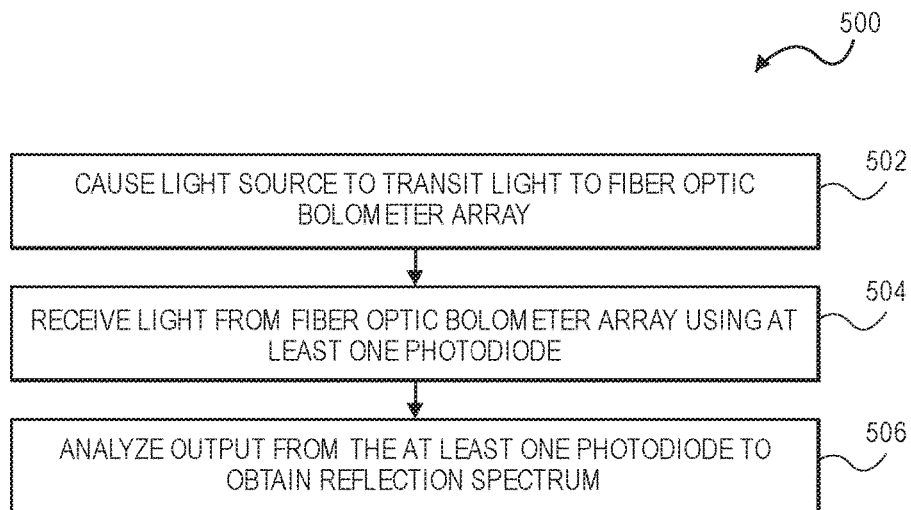


FIG. 2D

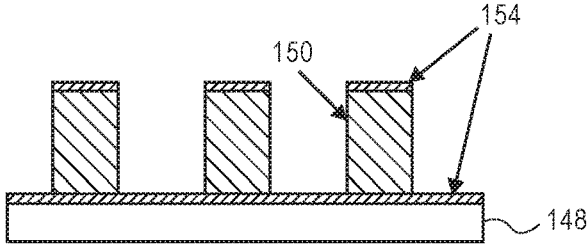


FIG. 3A

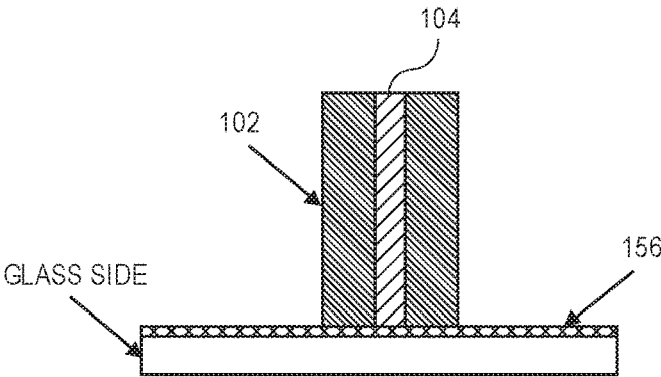


FIG. 3B

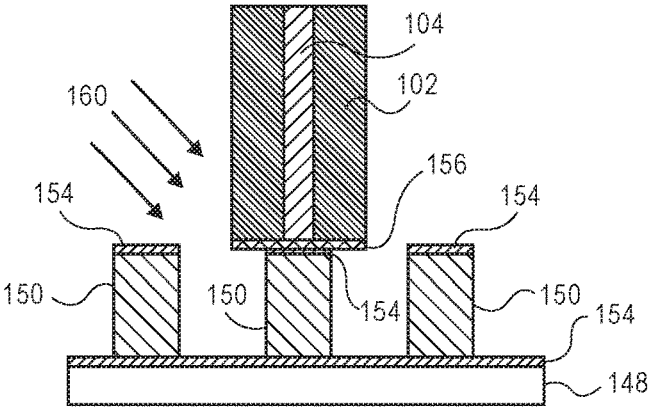


FIG. 3C

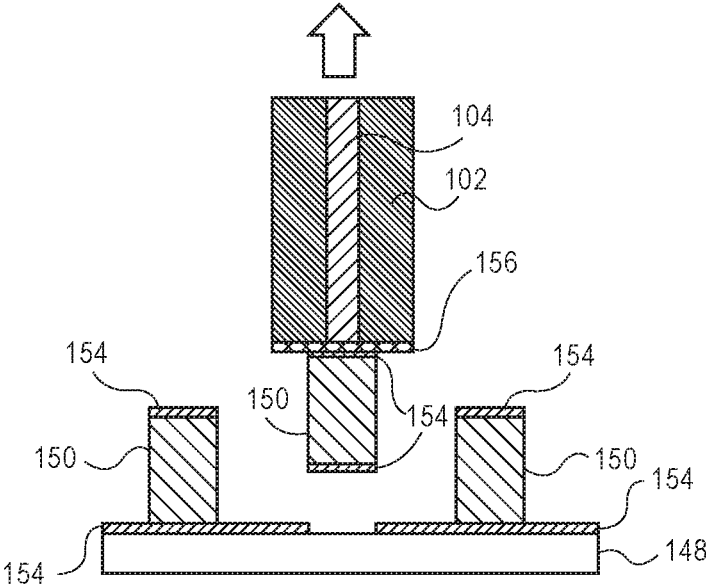


FIG. 3D

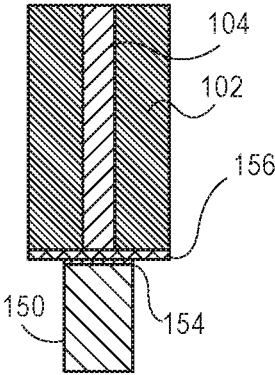


FIG. 3E

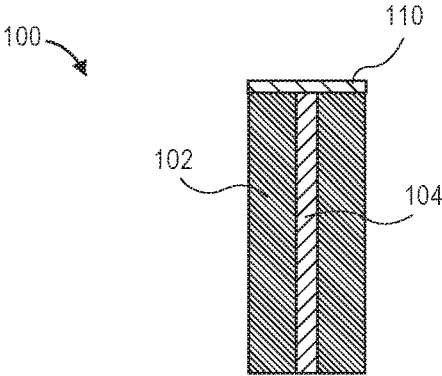


FIG. 4A

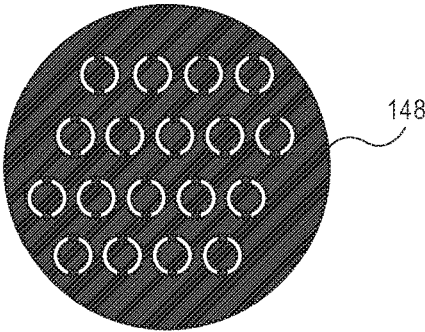


FIG. 4B

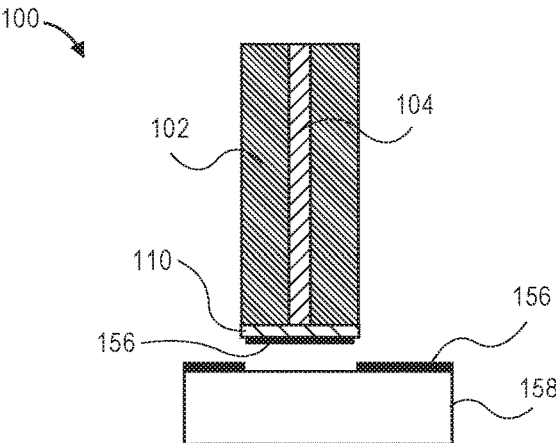
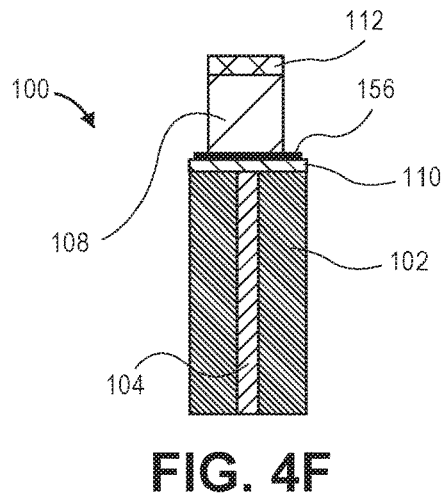
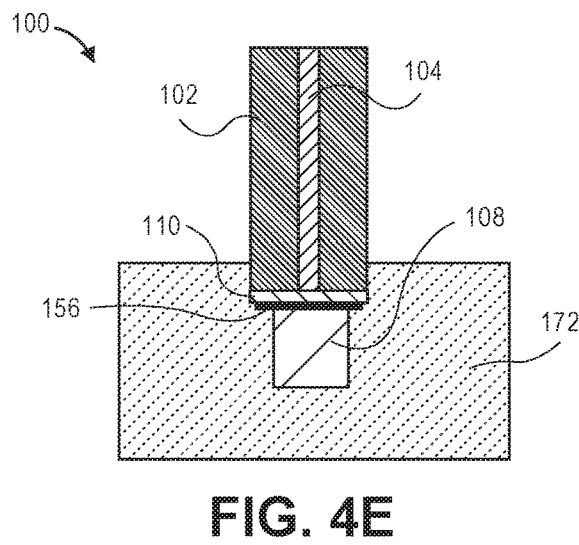
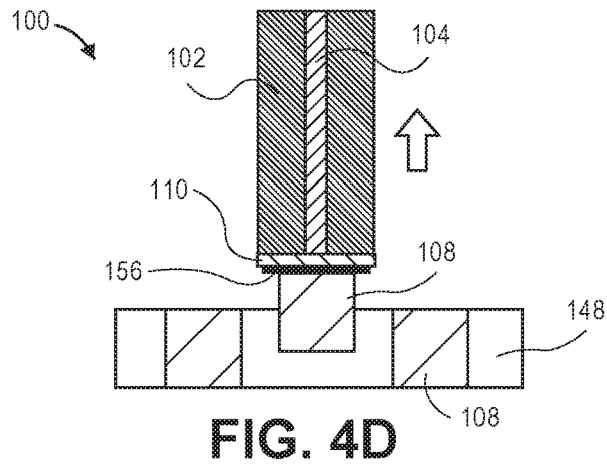


FIG. 4C



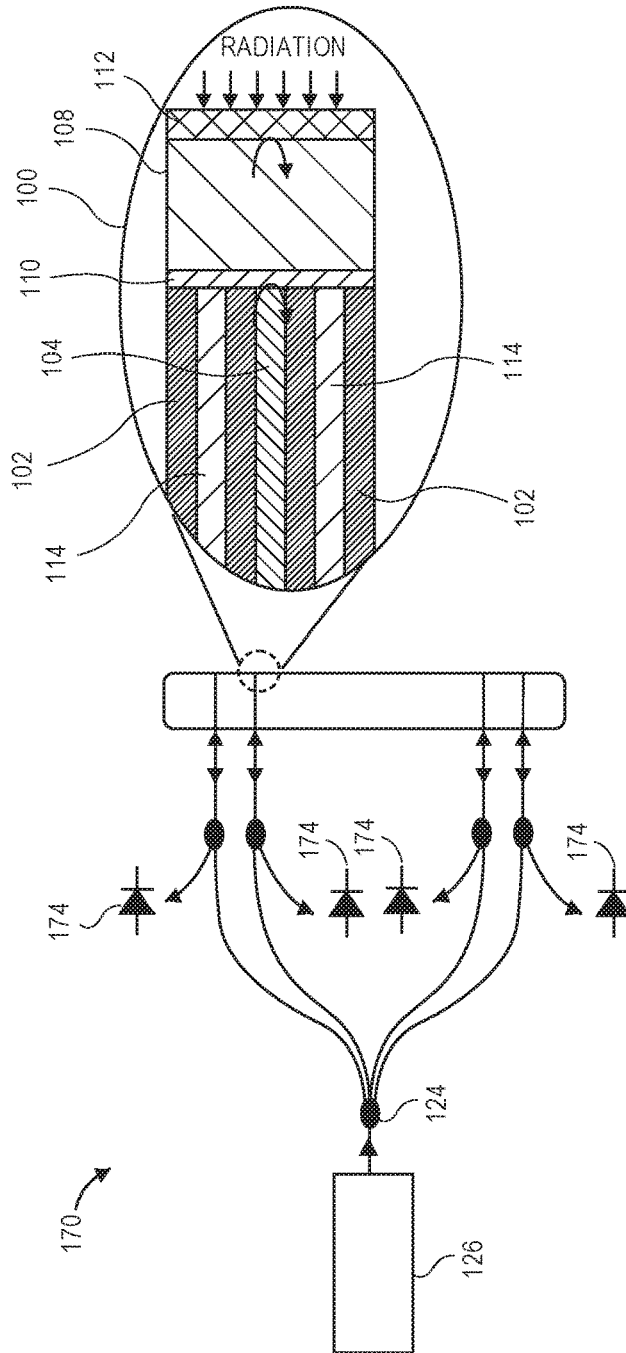


FIG. 5

1

FIBER OPTIC BOLOMETER**CROSS-REFERENCE TO RELATED APPLICATIONS**

The present application claims the benefit under 35 U.S.C. § 119(e) of U.S. Provisional Application Ser. No. 62/347,148, filed Jun. 8, 2016, and titled "FIBER OPTIC BOLOMETER." U.S. Provisional Application Ser. No. 62/347,148 is herein incorporated by reference in its entirety.

STATEMENT REGARDING FEDERALLY SPONSORED RESEARCH AND DEVELOPMENT

This invention was made with government support under Contract No. DE-AC05-00OR22725 awarded by the U.S. Department of Energy. The government has certain rights in the invention.

BACKGROUND

An optical fiber can include a flexible, transparent fiber made of extruded glass (silica) or plastic. Light can be transmitted between two ends of the optical fiber, which may be used in fiber-optic communications. A fiber optic sensor uses an optical fiber either as the sensing element (e.g., an intrinsic sensor) or as a means of relaying signals from a remote sensor to electronics that process a signal within the optical fiber (e.g., an extrinsic sensor). Fiber-optic sensors, such as intrinsic sensors, utilize optical fibers to measure temperature, strain, pressure, and/or other characteristics associated with the optical fiber.

SUMMARY

A fiber optic bolometer device is described herein. In an implementation, a fiber optic bolometer device includes an optical fiber and a silicon layer that comprises a Fabry-Pérot interferometer. The silicon layer includes a first surface and a second surface. The fiber optic bolometer device includes a reflective dielectric film disposed over the first surface of the silicon layer where the reflective dielectric film is adjacent to an end face of the optical fiber. The fiber optic bolometer device also includes an absorptive coating disposed over the second surface of the silicon layer (e.g., the surface distal to the end face of the optical fiber). This absorptive coating may also serve as a mirror of the Fabry Pérot interferometer.

This Summary is provided to introduce a selection of concepts in a simplified form that are further described below in the Detailed Description. This Summary is not intended to identify key features or essential features of the claimed subject matter, nor is it intended to be used as an aid in determining the scope of the claimed subject matter.

DRAWINGS

The detailed description is described with reference to the accompanying figures. The use of the same reference numbers in different instances in the description and the figures may indicate similar or identical items.

FIG. 1A is an isometric view illustrating an embodiment of a fiber optic sensor that includes a silicon layer disposed on an end face of an optical fiber, in accordance with an example implementation of the present disclosure.

2

FIG. 1B is a partial side elevation cross section view illustrating an embodiment of a fiber optic sensor that includes multiple cascaded silicon layers disposed on an end face of an optical fiber, in accordance with an example implementation of the present disclosure.

FIG. 1C is a partial side elevation cross section view illustrating an embodiment of a fiber optic sensor that includes multiple cascaded silicon layers disposed on an end face of an optical fiber, in accordance with an example implementation of the present disclosure.

FIG. 1D is an environmental view illustrating an embodiment of a fiber optic sensing system that includes a fiber optic sensor with a silicon layer disposed on an end face of an optical fiber, in accordance with an example implementation of the present disclosure.

FIG. 1E is an environmental view illustrating an embodiment of a fiber optic sensing system that includes a fiber optic sensor with a silicon layer disposed on an end face of an optical fiber, in accordance with an example implementation of the present disclosure.

FIG. 1F is an environmental view illustrating an embodiment of a controller used in a fiber optic sensing system, in accordance with an example implementation of the present disclosure.

FIG. 1G is an isometric view illustrating an embodiment of a fiber optic sensor that includes a silicon layer disposed on an end face of an optical fiber, in accordance with an example implementation of the present disclosure.

FIG. 1H is a graphical depiction illustrating a wavelength shift that represents a temperature change using a fiber optic sensor that includes a silicon layer disposed on an end face of an optical fiber, in accordance with an example implementation of the present disclosure.

FIG. 1I is a side elevation cross sectional view illustrating an embodiment of a fiber optic sensor that includes a silicon layer disposed on an end face of an optical fiber, in accordance with an example implementation of the present disclosure.

FIG. 1J is a side elevation cross sectional view illustrating an embodiment of a fiber optic bolometer sensor that includes a silicon layer disposed on an end face of an optical fiber where the silicon layer includes a reflective dielectric film disposed over a first surface and an absorptive and reflective coating disposed over a second surface in accordance with an example implementation of the present disclosure.

FIG. 1K is a side elevation cross sectional view illustrating an embodiment of fiber optic bolometer sensor in accordance with an example implementation of the present disclosure.

FIG. 1L is a side elevation cross sectional view illustrating an embodiment of fiber optic bolometer sensor in accordance with an example implementation of the present disclosure.

FIG. 1M is a side elevation cross sectional view illustrating an embodiment of fiber optic bolometer sensor in accordance with an example implementation of the present disclosure.

FIG. 1N is a side elevation cross sectional view illustrating an embodiment of fiber optic bolometer sensor in accordance with an example implementation of the present disclosure.

FIG. 1O is a side elevation cross sectional view illustrating an embodiment of fiber optic bolometer sensor in accordance with an example implementation of the present disclosure.

3

FIG. 2A is a flow diagram illustrating an example process for using a fiber optic sensor that includes a silicon layer disposed on an end face of an optical fiber, such as the fiber optic sensor illustrated in FIGS. 1A through 1G.

FIG. 2B is a flow diagram illustrating an example process for fabricating a fiber optic sensor that includes a silicon layer disposed on an end face of an optical fiber, such as the fiber optic sensor illustrated in FIGS. 1A through 1G.

FIG. 2C is a flow diagram illustrating an example process for fabricating a fiber optic bolometer device that includes a silicon layer disposed on an end face of an optical fiber, such as the fiber optic sensor illustrated in FIGS. 1J through 1M.

FIG. 2D is a flow diagram illustrating an example process for demodulating an array of fiber optic bolometer devices that includes a silicon layer disposed on an end face of each optical fiber, such as the fiber optic bolometer device illustrated in FIGS. 1J through 1M.

FIG. 3A is a diagrammatic partial cross-sectional side elevation view illustrating the fabrication of a fiber optic sensor that includes a silicon layer disposed on an end face of an optical fiber, such as the fiber optic sensor illustrated in FIGS. 1A through 1G, in accordance with the process shown in FIG. 2B.

FIG. 3B is a diagrammatic partial cross-sectional side elevation view illustrating the fabrication of a fiber optic sensor that includes a silicon layer disposed on an end face of an optical fiber, such as the fiber optic sensor illustrated in FIGS. 1A through 1G, in accordance with the process shown in FIG. 2B.

FIG. 3C is a diagrammatic partial cross-sectional side elevation view illustrating the fabrication of a fiber optic sensor that includes a silicon layer disposed on an end face of an optical fiber, such as the fiber optic sensor illustrated in FIGS. 1A through 1G, in accordance with the process shown in FIG. 2B.

FIG. 3D is a diagrammatic partial cross-sectional side elevation view illustrating the fabrication of a fiber optic sensor that includes a silicon layer disposed on an end face of an optical fiber, such as the fiber optic sensor illustrated in FIGS. 1A through 1G, in accordance with the process shown in FIG. 2B.

FIG. 3E is a diagrammatic partial cross-sectional side elevation view illustrating the fabrication of a fiber optic sensor that includes a silicon layer disposed on an end face of an optical fiber, such as the fiber optic sensor illustrated in FIGS. 1A through 1G, in accordance with the process shown in FIG. 2B.

FIG. 4A is a diagrammatic partial cross-sectional side elevation view illustrating the fabrication of a fiber optic bolometer device that includes a silicon layer disposed on an end face of an optical fiber, such as the fiber optic bolometer device illustrated in FIGS. 1J through 1M, in accordance with the process shown in FIG. 2C.

FIG. 4B is a top plan view illustrating the fabrication of a fiber optic bolometer device that includes a silicon layer disposed on an end face of an optical fiber, such as the fiber optic bolometer device illustrated in FIGS. 1J through 1M, in accordance with the process shown in FIG. 2C.

FIG. 4C is a diagrammatic partial cross-sectional side elevation view illustrating the fabrication of a fiber optic bolometer device that includes a silicon layer disposed on an end face of an optical fiber, such as the fiber optic bolometer device illustrated in FIGS. 1J through 1M, in accordance with the process shown in FIG. 2C.

FIG. 4D is a diagrammatic partial cross-sectional side elevation view illustrating the fabrication of a fiber optic bolometer device that includes a silicon layer disposed on an

4

end face of an optical fiber, such as the fiber optic bolometer device illustrated in FIGS. 1J through 1M, in accordance with the process shown in FIG. 2C.

FIG. 4E is a diagrammatic partial cross-sectional side elevation view illustrating the fabrication of a fiber optic bolometer device that includes a silicon layer disposed on an end face of an optical fiber, such as the fiber optic bolometer device illustrated in FIGS. 1J through 1M, in accordance with the process shown in FIG. 2C.

FIG. 4F is a diagrammatic partial cross-sectional side elevation view illustrating the fabrication of a fiber optic bolometer device that includes a silicon layer disposed on an end face of an optical fiber, such as the fiber optic bolometer device illustrated in FIGS. 1J through 1M, in accordance with the process shown in FIG. 2C.

FIG. 5 is an environmental view illustrating an embodiment of a fiber optic bolometer device array that includes multiple fiber optic bolometer devices with a silicon layer and an absorptive layer disposed on an end face of an optical fiber, in accordance with an example implementation of the present disclosure.

DETAILED DESCRIPTION

Measurement of speed of gas or liquid flow is of great practical importance in a variety of industries, such as food inspection, pharmacy, oil/gas exploration, environmental, high-voltage power systems, chemical plants, and oceanography research. Owing to their many unique advantages, such as small size, light weight, immunity to electromagnetic interference, remote sensing capability, harsh environment tolerance, and capability for distributed or quasi-distributed measurement fiber-optic sensors, such as temperature sensors, flowmeters, or anemometers, have proven to be attractive alternatives to their traditional mechanical or electromagnetic counterparts.

In addition to sensitivity and temperature range, two important sensor parameters include temperature resolution and speed (or response time). Temperature resolution, defined as the minimum detectable temperature changes, is determined by both the sensor sensitivity (defined as the sensor output from a given temperature change) and the noise of the sensor system, while the response time is mostly limited by the time constant of the heat transfer process between the sensing element and the surrounding environment. The sensing element of many fiber-optic temperature sensors is part of the fiber itself, which is made of fused silica. The temperature resolution and the speed are limited by the relatively low thermo-optic coefficient (TOC) and thermal diffusivity of the glass material that lead, respectively, to a reduced sensor sensitivity and increased time for the temperature of the sensing element to reach equilibrium with the surrounding environment. For example, it is well-known that a fiber Bragg grating (FBG), whose reflection spectrum features a single reflection peak, exhibit a temperature sensitivity of about $10 \text{ pm}/^\circ \text{C}$. A fiber modal interferometer based on a single mode-multimode-single mode fiber structure has been reported to have a temperature resolution of 0.2°C . Many all-silica-fiber-based temperature sensors possess relatively low sensitivity and relatively low temperature resolution. As to the response time, a package of a FBG with a copper tube encapsulation can greatly reduce the response time of the sensor from several seconds to 48.6 milliseconds (ms) in water. A response time of 16 ms in air has been demonstrated for a microfiber coupler tip temperature sensor.

Compared to fused silica, crystalline silicon is a much more desirable sensor material for high-resolution and high-speed temperature sensing. Silicon is highly transparent over the infrared wavelength and has a TOC approximately 10 times larger than that of fused silica used for the sensing element for most fiber-optic sensors, resulting in potentially much higher temperature sensitivity. In addition, a silicon-based temperature sensor also has high speed because of the large thermal diffusivity of silicon, which is comparable to many metals (e.g., aluminum and gold) and is more than 60 times larger than fused silica. However, the use of silicon as a temperature sensing element has not been utilized on a large scale for high-resolution and high-speed temperature sensing. The dependence of the absorption of a silicon film on temperature for temperature sensing and the sensor has shown a relatively low temperature resolution of $\pm 0.12^\circ\text{C}$. and a long response time on the order of 1 second (s). A simpler structure with a thin silicon film (thickness $< 1\ \mu\text{m}$) deposited directly on the fiber end through electron-beam evaporation has shown a temperature resolution of only 3°C . In this case, radio-frequency sputtering was applied to simplify the deposition process, and the resolution was mainly limited by the small thickness of the silicon film that led to broad spectral fringes. Instead of silicon film, a silicon micro-waveguide patterned on a micro-electro-mechanical system (MEMS) was developed as temperature sensor, and due to the increased length of the Si sensing element, the temperature resolution was improved to 0.064°C . However, it is a challenge to integrate the fiber and the MEMS into a single sensor device, and the large size of previous sensing elements also limit their temperature measurement speed.

Accordingly, a fiber optic sensor, a process for utilizing a fiber optic sensor, and a process for fabricating a fiber optic sensor are described, where a double-side-polished silicon pillar is attached to an optical fiber tip and forms a Fabry-Pérot (FP) cavity and a sensor head. As described herein, the Fabry-Pérot (FP) cavity may comprise a Fabry-Pérot (FP) cavity bolometer (e.g., a fiber-optic bolometer device or a fiber-optic bolometer sensor). The bolometer is configured to measure the power of incident electromagnetic radiation via the heating of a material with a temperature-dependent electrical resistance.

In an implementation, a fiber optic bolometer device includes an optical fiber and a silicon layer that comprises a Fabry-Pérot interferometer. The silicon layer includes a first surface and a second surface. The fiber optic bolometer device includes a reflective dielectric film disposed over the first surface of the silicon layer where the reflective dielectric film is adjacent to an end face of the optical fiber. The fiber optic bolometer device also includes an absorptive coating disposed over the second surface of the silicon layer (e.g., the surface distal to the end face of the optical fiber).

Example Implementations

FIGS. 1A through 1N illustrate a fiber optic sensor **100** (fiber optic bolometer device **100**) and fiber optic sensing system **130** in accordance with an example implementation of the present disclosure. The fiber optic sensor **100** can include an optical fiber **102** configured to be coupled to a light source **126** and a high speed spectrometer **128**. The fiber optic sensor **100** and fiber optic sensing system **130** may be utilized as a temperature sensor in determining temperature in gas and liquid.

In implementations, the optical fiber **102** can include a flexible, transparent fiber core **104** made of extruded glass (e.g., silica) or a polymer. The optical fiber **102** can be

configured to transmit light between the two ends of the optical fiber **102**. In some instances, the optical fiber **102** may be immune to electromagnetic interference.

The optical fiber **102** can include the core **104** and/or a cladding **106**. The core **104** may include a fiber of glass and/or plastic that extends along the length of the optical fiber **102**. The core **104** may be surrounded by a cladding **106**, which may include a material with a lower index of refraction than the core **104**. In embodiments, the cladding **106** may include a cladding of a different glass and/or plastic, a buffer layer, and/or a jacket.

In some instances, the polarization of the light in regular single-mode optical fibers may not be stable. Mechanical or thermal perturbations to the optical fiber **102** may change the polarization. Due to the potential birefringence of the silicon layer **108** and/or the reflective dielectric thin film **110**, the optical length of the FPI may be dependent on the light polarization. The changes of the polarization may lead to the change of the optical signal, which may not be distinguished from the change from the radiation. To eliminate the issues from the birefringence of the FPI, some embodiments of the fiber optic sensor **100** may include an optic fiber **102** comprising polarization-maintaining fibers (PMFs), where the polarization of the light beam in the fiber is maintained during the light propagation in the fiber.

As illustrated in FIG. 1A, the fiber optic sensor **100** can include a silicon layer **108** disposed on an end face **152** of the optical fiber **102** (e.g., a cleaved portion of the optical fiber **102**), which forms a sensor head. In implementations, the silicon layer **108** can include a silicon pillar and/or a silicon-based film. In a specific embodiment, the silicon layer **108** includes a double-sided polished silicon pillar. In another specific embodiment, the silicon layer **108** can include a piece of a silicon wafer bonded to the end face **152**. The silicon layer **108** may include various diameters and/or lengths. For example, the silicon layer **108** can include a silicon pillar with a diameter between about $80\ \mu\text{m}$ to $100\ \mu\text{m}$ with a length of about $200\ \mu\text{m}$. In another example, the silicon layer **108** may include a piece of silicon that is approximately $10\ \mu\text{m}$ thick. In yet another example, the silicon layer **108** can include a piece of silicon that is approximately $200\ \mu\text{m}$ thick. It is contemplated that the silicon layer **108** may include other diameters and/or lengths. The silicon layer **108** diameter is generally less than the diameter of the optical fiber **102**, which leads to a fast temperature response. The silicon in the silicon layer **108** is highly transparent over the infrared wavelength and has a TOC approximately 10 times larger than that of the silica used in the optical fiber **102** for most fiber-optic sensors, resulting in potentially much higher temperature sensitivity. In addition, the fiber optic sensor **100** also has high speed because of the large thermal diffusivity of silicon, which is comparable to many metals (e.g., aluminum and gold) and more than 60 times larger than fused silica. In other implementations, the silicon layer **108** may be replaced with other materials that have large thermal diffusivity and high thermo-optic and thermal expansion coefficients. Further, it is contemplated that the silicon layer **108** can include other configurations, such as a cuboid configuration.

As illustrated in FIGS. 1B and 1C, the fiber optic sensor **100** may include cascaded Fabry-Pérot cavities. In these implementations, the fiber optic sensor **100** can include an adhesive **156** disposed on an end face **152** of the optical fiber **102**, a silicon layer **108** disposed on the adhesive **156**, a second adhesive **166** disposed on the silicon layer **108**, and a second silicon layer **168** disposed on the second adhesive **166**. The silicon layer **108** and the second silicon layer **168**

include the same material so that each has the same responsiveness to temperature. In such a way, the large free spectrum range (FSR) of the envelope originating from the second silicon layer **168** (the second Fabry-Pérot interferometer) provides large dynamic range, while the recognized dense fringes with small FSR stemming from the silicon layer **108** (the first Fabry-Pérot interferometer) offers high resolution due to the narrow fringes. The adhesive **156** and/or the second adhesive **166** can include materials suitable to bond the optical fiber **102**, the silicon layer **108**, and/or the second silicon layer **168** (e.g., a UV glue, etc.). Additionally, the adhesive **156** and/or the second adhesive **166** can be the same or similar diameter as the silicon layer **108** and/or second silicon layer **168**, while the thickness of the adhesive **156** and/or the second adhesive **166** can be only a few microns (e.g., <1 μm , 2 μm , 3 μm , etc.). Because the adhesive **156** and/or the second adhesive **166** are very thin compared to the silicon layer **108** and the second silicon layer **168**, they show negligible influence on the reflection spectrum of reflected light **162**. In specific embodiments, the silicon layer **108** and the second silicon layer **168** can be the same or similar diameters but have different lengths (e.g., the silicon layer **108** is 200 μm in length and the second silicon layer **168** is 10 μm in length). It is contemplated that the silicon layer **108** and/or the second silicon layer **168** can include a variety of lengths and/or diameters. In FIG. 1C, n_i and D_i represent the refractive index and separation of the i^{th} layer, respectively. These implementations provide an optical fiber thermometer based on double cascaded Fabry-Pérot interferometers both made from the same material of silicon but with vastly different cavity lengths to achieve both large dynamic and high resolution.

In implementations, the fiber optic sensor **100** defines and includes a Fabry-Pérot (FP) cavity. A Fabry-Pérot cavity (or Fabry-Pérot interferometer) can include a cavity formed by the optical fiber **102** and the silicon layer **108** disposed on the end face **152** of the optical fiber **102**. Due to the thermo-optic effect, temperature variations change the optical thickness of the FP cavity and consequently cause spectral shifts in its reflection spectrum.

As illustrated in FIG. 1D, the fiber optic sensing system **130** can include the fiber optic sensor **100**, a light source **126**, a circulator **124**, a spectrometer **128**, and a controller **132**. In some implementations, the fiber optic sensing system **130** may include a heating light source **146**.

In implementations, the light source **126** (e.g., a broad band source) transmits light to the circulator **124** and the fiber optic sensor **100**. In one specific embodiment, light source **126** includes a wavelength swept laser, such as a high-speed, narrow-linewidth, and wavelength-swept laser. In another specific embodiment, light source **126** includes a laser diode. In yet another specific embodiment, light source **126** includes a white light source (e.g., 1550 nm). It is contemplated that the light source **126** can include other types of light sources. In implementations, the light source **126** is optically coupled to the optical fiber **102**, which is optically coupled to a circulator **124**. Additionally, the light source **126** can be coupled to and controlled using controller **132**.

As illustrated in FIG. 1E, the fiber optic sensing system **130** may include a heating light source **146** configured to provide heating light **142**. In these embodiments, the heating light source **146** can include a light source, such as a red laser diode, that is optically coupled to the optical fiber **102** using a coupler **164**. In one specific instance, the heating light source **146** can include a 635 nm diode laser. The heating light source **146** may include other light sources that

provide light, which can be absorbed by the fiber optic sensor **100** and/or the silicon layer **108**. Additionally, the heating light source **146** can be controlled using controller **132**.

A circulator **124** can include a fiber-optic component used to separate optical signals in optical fiber **102**. In implementations, circulator **122** can direct transmitted light **140** from light source **126** (and/or heating light **142** from heating light source **146**) to fiber optic sensor **100** while directing reflected light **162** from the fiber optic sensor **100** to spectrometer **128**.

The fiber optic sensing system **130** can include a spectrometer **128** coupled to the optical fiber **102** and a controller **132**. In implementations, a spectrometer **128** can include a light sensor, such as a photodetector, configured to detect reflected light **162** and the associated spectra from the optical fiber **102** and fiber optic sensor **100**. In a specific embodiment, the spectrometer **128** may include a high-speed photodetector (e.g., the high speed spectrometer from Ibsen Photonics, I-MON 256 USB, Denmark). Additionally, the spectrometer **128** can be coupled to and controlled using controller **132**.

As reflected light **162** is received and/or detected by spectrometer **128**, a shift in wavelength is detected when temperature changes at the silicon layer **108**. The wavelength of the N^{th} fringe peak, $\lambda_{N^{\text{th}}}$, of the reflection spectrum is given as

$$\left(N + \frac{1}{2}\right)\lambda_N = 2nL \quad \text{Eq. 1}$$

where n and L are, respectively, the RI and cavity length of the FP cavity. Both n and L are dependent on temperature due to the thermo-optic effect and the thermal expansion of the silicon material. Therefore, temperature change can be measured by monitoring $\lambda_{N^{\text{th}}}$. From Eq. 1, the temperature sensitivity is given by

$$\frac{\partial \lambda_N}{\partial T} = \lambda_N \left(\frac{1}{n} \frac{\partial n}{\partial T} + \frac{1}{L} \frac{\partial L}{\partial T} \right) \quad \text{Eq. 2}$$

Although Eqs. 1 and 2 only depict one of the multiple peaks in the reflected spectrum from the sensor, in some cases, an average wavelength may be applied to significantly reduce the noise level or increase the resolution. This average wavelength can be obtained from multiple peaks or valleys or both.

The sensitivity depends on the TOC and the thermo-expansion coefficient (TEC) of the sensing material. The TOC and TEC for silicon are, respectively, 1.5×10^{-4} RIU/ $^{\circ}\text{C}$. and 2.55×10^{-6} m/(m. $^{\circ}\text{C}$.) at 25°C . To estimate the sensitivity, these values are applied to Eq. (2) at the peak wavelength λ_N around 1550 nm and the RI of silicon is assumed to be 3.4. From this, the sensitivity of the temperature sensor proposed here is estimated to be 72 pm/ $^{\circ}\text{C}$. As a comparison to the all-fiber based sensor, the TOC and TEC for fused silica are, respectively, 1.28×10^{-5} RIU/ $^{\circ}\text{C}$. and 5.5×10^{-7} m/(m. $^{\circ}\text{C}$.) at 25°C ., both of which are much smaller than those for silicon. Assuming the RI of silica at 1550 nm is 1.5, the sensitivity of an all-fiber based sensor is about 14 pm/ $^{\circ}\text{C}$., which is more than 5 times smaller than the fiber optic sensor **100**.

The high RI (about 3.4) of silicon over infrared wavelength range produces a high reflectivity at the interfaces

between silicon layer **108** and the surrounding environment and between silicon layer **108** and the fiber end face **152**, which facilitates to obtain a large optical power and a high fringe-visibility of the interferometric spectrum from the FP cavity for improving the sensor resolution. In addition, the high RI and the relatively long FP cavity yield a large number of fringes within the wavelength range of the spectrometer, which can be exploited to further increase the temperature resolution.

The fiber optic sensor **100** also features a short response time. Due to the high thermal diffusivity of silicon and the small size of the sensor head, the temperature within the FP cavity can quickly reach equilibrium with surroundings.

As illustrated in FIG. 1B, the fiber optic sensing system **130** can include a controller **132** that is configured to determine a shift in spectra detected by spectrometer **128** using a fiber optic sensor **100**. The controller **132** can be coupled to the components of the fiber optic sensing system **130**. Additionally, the controller **132** may be configured in a variety of ways. As illustrated in FIG. 1E, the controller **132** is illustrated as including a processor **134**, a memory **136**, and a communications interface **138**. The processor **134** provides processing functionality for the fiber optic sensor **100** and may include any number of processors, micro-controllers, or other processing systems, and resident or external memory for storing data and other information accessed or generated by the fiber optic sensor **100**. The processor **134** may execute one or more software programs that implement the techniques and modules described herein. The processor **134** is not limited by the materials from which it is formed or the processing mechanisms employed therein and, as such, may be implemented via semiconductor(s) and/or transistors (e.g., electronic integrated circuits (ICs)), and so forth.

The memory **136** is an example of a non-transitory computer storage device that provides storage functionality to store various data associated with the operation of the fiber optic sensor **100**, such as the software program and code segments mentioned above, computer instructions, and/or other data to instruct the processor **134** and other elements of the fiber optic sensor **100** to perform the techniques described herein. Although a single memory **136** is shown, a wide variety of types and combinations of memory may be employed. The memory **136** may be integral with the processor **134**, stand-alone memory, or a combination of both. The memory may include, for example, removable and non-removable memory elements such as RAM, ROM, Flash (e.g., SD Card, mini-SD card, micro-SD Card), magnetic, optical, USB memory devices, and so forth.

The communications interface **138** is operatively configured to communicate with components of the fiber optic sensor **100**. For example, the communications interface **138** can be configured to transmit data for storage in the controller **132**, retrieve data from storage in the controller **132**, and so forth. The communications interface **138** is also communicatively coupled with the processor **134** to facilitate data transfer between components of the fiber optic sensing system **130** and the processor **134** (e.g., for communicating inputs to the processor **134** received from a device communicatively coupled with the fiber optic sensing system **130**). It should be noted that while the communications interface **138** is described as a component of fiber optic sensing system **130**, one or more components of the communications interface **138** can be implemented as external components communicatively coupled to the fiber optic sensing system **130** via a wired and/or wireless connection.

The fiber optic sensing system **130** can also comprise and/or connect to one or more input/output (I/O) devices (e.g., via the communications interface **138**) including, but not necessarily limited to a display, a mouse, a touchpad, a keyboard, and so on.

The communications interface **138** and/or the processor **134** can be configured to communicate with a variety of different networks including, but not necessarily limited to: a wide-area cellular telephone network, such as a 3G cellular network, a 4G cellular network, or a global system for mobile communications (GSM) network; a wireless computer communications network, such as a WiFi network (e.g., a wireless local area network (WLAN) operated using IEEE 802.11 network standards); an internet; the Internet; a wide area network (WAN); a local area network (LAN); a personal area network (PAN) (e.g., a wireless personal area network (WPAN) operated using IEEE 802.15 network standards); a public telephone network; an extranet; an intranet; and so on. However, this list is provided by way of example only and is not meant to be restrictive of the present disclosure. Further, the communications interface **138** can be configured to communicate with a single network or multiple networks across different access points.

In one specific embodiment illustrated in FIGS. 1G through 1I, the fiber optic sensor **100** can function as a fiber optic anemometer. In this embodiment, the transmitted light **140** (e.g., white-light centered at 1550 nm) is injected through the optical fiber **102** to the FP defined in the fiber optic sensor **100** by the optical fiber **102** and the silicon layer **108**, and the reflection spectrum of the reflected light **162** can be recorded by a high-speed spectrometer **128**. At the same time, heating light **142** from a heating light source **146** (e.g., 635 nm diode laser) can be guided through the same optical fiber **102** to the heat the FP. Silicon has a band gap energy of 1.11 eV and is highly transparent to the transmitted light **140** but is opaque to the heating light **142**. Therefore, the FP temperature can be effectively increased by the heating light **142**. When air moves (e.g., air convection **144**) over the surface of a hot silicon layer **108**, a cooling effect from the moving air reduces the temperature of the silicon layer **108** and the FP and introduces a shift to the fringe valley wavelength of the reflection spectrum, as schematically shown in FIGS. 1H and 1I. The wavelength shift can be separated by the spectrometer **128** and/or the controller **132** into a wind-temperature-induced wavelength shift and a wind-speed-induced wavelength shift. As a result, temperature self-compensated measurement of wind speed can be achieved by comparing the shift in the wavelengths of a fringe valley when the heating laser is turned on and off to determine temperature-compensated wind speed. It should be pointed out that although it is implemented as an anemometer in this example, it is not limited to measuring only the wind or air flow. Any other kind of flows (e.g., water flow) that can bring about the cooling effects to the heated sensor head can be measured.

FIG. 1J illustrates an embodiment of a fiber-optic sensor **100** that comprises a bolometer. As described above, a bolometer measures or detects power flux from electromagnetic radiation or particles by the heating of the respective material. In this embodiment, a Fabry-Pérot interferometer (FPI) is coupled to the end face **152** of an optical fiber **102**. The FPI can be formed by a silicon pillar (e.g., silicon layer **108**) with a first side of the silicon pillar coated with an absorptive and reflective layer (e.g., coating) **112** and the other side (e.g., a side distal from the first side and proximate to the end face **152**) with reflective dielectric thin film **110**. It is contemplated that absorptive coating **112** can include

multiple metal coatings with the same or different materials. It is also contemplated that the reflective dielectric thin film **110** can include multiple layers of the same or different materials. The FPI can be connected to the end face **152** on the reflective dielectric thin film **110** side. The reflective dielectric thin film **110** serves as a mirror for the FPI. The absorptive coating **112** functions both as a second mirror for the FPI and as an absorptive element that absorbs an incident signal **116** and conducts heat to the silicon pillar. The choice of absorptive coating **112** material and thickness may be optimized to adjust the thermal properties of the combined pillar and its wavelength dependent absorptivity. Signals that penetrate through the absorptive coating **112** can also contribute to the heating of the silicon pillar but do not perturb its operation as an FPI. The heating of the silicon pillar increases the optical length of the FPI via increasing both the refractive index and the physical length of the silicon pillar through, respectively, the thermal optic effect and the thermal expansion of silicon material. The change in the optical length of FPI shifts the interferometric fringes in the reflection spectrum of the FPI, which can be measured by the light guided to the FPI through the optical fiber **102**. The two mirrors (e.g., reflective dielectric thin film **110**, absorptive coating **112**) with high reflectivity can yield a large Finesse and narrow spectral features of the FPI, leading to high resolution in determining the wavelength shift of the fringes. The transmitted light **140** (e.g., light from a light source **126**) should have wavelengths transparent to the silicon pillar. In one implementation, the transmitted light **140** wavelength is the 1550 nm window where a large of low-cost fiber-optic components and devices are available.

The fiber optic sensor **100** parameters, including the type and thickness of the absorptive coating(s) **112**, the thickness of the silicon pillar, the reflectivity of the reflective dielectric thin film **110**, can be optimized for different applications. For example, the absorptive coating **112** may include a gold metal coating, which serves as an excellent mirror with a reflectivity >95% over a broad wavelength range. A few micrometer gold coating can serve as good absorptive element from x-ray to the short end of the visible. Another choice of the metal may include platinum, which is commonly used in electronic resistive bolometers as the absorptive element. The thickness of the silicon pillar and the metal film can be designed to maximize the sensitivity in terms of minimally resolvable power of the incident signal.

Another function of the optical fiber **102** is to provide a thermal reservoir to the FPI. The optical fiber **102** can include specialty fibers to tune the performance of the bolometer. For example, the optical fiber **102** may include microstructured fibers, photonic crystal fibers, or side-hole fibers to tune the speed and sensitivity of the bolometer. For example, FIGS. 1K and 1L illustrates a specific optical fiber **102** that includes a side hole fiber, with cladding **106** that has at least one cavity **114** (e.g., an empty hole or space) along at least a portion of the length of the optical fiber **102**. The at least one cavity **114** can be disposed proximate to an end face in the optical fiber **102**. The cavities **114** effectively reduces the thermal conductivity of the fiber optic sensor **100**. Because of the cavities **114**, the heat transfer from the FPI to the optical fiber **102** becomes less efficient; therefore, increasing the sensitivity of the bolometer but reducing its speed. In some implementations, as shown in FIG. 1M, the cavity **114** can be filled with a thermal conductor **118** (e.g., thermal conductive medium), such as metal, that can help to

dissipate the heat from the FPI to the optical fiber **102** to reduce the sensitivity and increase the speed of the fiber optic sensor **100**.

FIG. 1M illustrates a specific embodiment where the fiber optic sensor **100** includes a mirror coating **122** dedicated as a highly reflective mirror for the FPI. The mirror coating **122** can be disposed between the absorptive coating **112** for signal absorption and the silicon pillar (e.g., silicon layer **108**). In implementations, the mirror coating **122** may include a metal (e.g., gold) or a multilayer dielectric coating, similar to the reflective dielectric thin film **110** on the other side of the FPI. In instances where a mirror coating **122** includes a metal, a small amount of the light power can be absorbed to heat up the FPI (e.g., ~2% of light power can be absorbed by a mirror coating **122** including gold at about 1550 nm). As a result, the light power is maintained at a constant level. Otherwise, light power fluctuations may change the FPI temperature and can be mistakenly explained as the changes of the radiation signal. When a dielectric mirror coating **122** is used, the absorption of the light power may be smaller than a metal mirror coating **122**. In the specific embodiment illustrated in FIG. 1M, the absorptive coating **112** can function mainly for the absorption of the incident signal **116**. In addition, materials other than metal can also be used for the absorptive coating **112**. With the absorptive coating **112**, in general, any material that can convert the power flux into heat may be used. For example, the absorptive coating **112** may include carbon, which can be used as an absorber for radio frequency waves.

FIG. 1N illustrates an embodiment where the fiber optic sensor **100** includes a graded-index (GRIN) lens **176** disposed between the optical fiber **102** and the silicon layer **108**. The profile of the light beam in a regular single mode fiber is close to that of a Gaussian beam and the mode field diameter is usually small (e.g., less than 15 μm). As the light beam exits the optical fiber **102** and travels into the FPI, the diffraction, which can be more prominent for smaller light beam, may limit the finesse of the FPI. The fiber optic sensor **100** illustrated in FIG. 1N can increase the size of the light beam in the FPI and increase the finesse of the FPI using a graded-index (GRIN) lens **176**, which may also include a short-section of GRIN multimode fiber (MMF), that is inserted between the silicon layer **108** and the optical fiber **102**. The GRIN lens **176** (and/or the MMF) functions as a light collimator, which can expand the light beam size to reduce light diffraction and increase finesse.

FIG. 1O illustrates an embodiment where the fiber optic sensor **100** includes an optical fiber **102** with an expanded core **178** disposed proximate to and/or abutted against the silicon layer **108** and/or reflective dielectric thin film **110**. In this embodiment, the core **104** of the optical fiber **102** can be gradually expanded resulting in an expanded core **178**. As the core **104** is gradually expanded toward the expanded core **178**, the light beam profile can be gradually enlarged. In implementations, the expanded core **178** can be obtained by locally heating the fiber to a high temperature.

Example Processes

The following discussion describes example techniques for utilizing a fiber optic sensor and fiber optic sensing system, such as the fiber optic sensor **100** and fiber optic sensing system **130** described in FIGS. 1A through 1M. FIG. 2A depicts an example process **200** for using a bolometer device **100**.

As shown in FIG. 2A, a light source is caused to transmit light through a fiber optic to a fiber optic sensor (Block **202**). In this implementation, controller **132** can cause light source **126** to transmit light (e.g., transmitted light **140**) through

optical fiber **102** and circulator **124** to fiber optic sensor **100**. Controller **132** can control the duration and intensity that the light source **126** transmits the transmitted light **140**. In some specific implementations, controller **132** can cause heating light source **146** to transmit heating light **142** through the optical fiber **102** to the fiber optic sensor **100** and the silicon layer **108** for providing heat.

Reflected light from the fiber optic sensor is received using a spectrometer (Block **204**). The spectrometer **128** can receive the reflected light **162** and associated spectra, which can be recorded and/or analyzed by spectrometer **128** and/or controller **132**.

An output from the spectrometer is analyzed based on the received reflected light (Block **206**). In implementations, the controller **132** and/or the spectrometer **128** can analyze the reflected light **162** and the spectra to determine a wavelength shift in the spectra, which indicates a change in temperature. A variety of methods may be utilized to analyze and/or determine the wavelength shift in the spectra and for tracking the average wavelength. In a specific embodiment, analyzing an output from the spectrometer based on received reflected light can include using an average wavelength tracking method to further increase the resolution of wavelength and/or measurand.

The following discussion describes example techniques for fabricating a fiber optic sensor, such as the fiber optic sensor **100** described in FIGS. **1A** through **1M**. FIG. **2B** depicts an example process **300** for fabricating the fiber optic sensor **100**. FIGS. **3A** through **3E** illustrate a section an exemplary fiber optic sensor **100** during fabrication (such as the fiber optic sensors **100** described in FIGS. **1A** through **1M**).

FIG. **2B** depicts an example process **300** for fabricating a fiber optic sensor **100**. As shown in FIG. **2B**, a silicon pillar is formed on a silicon substrate (Block **302**). FIG. **3A** illustrates forming at least one silicon pillar **150** that will function as a sensor head for the fiber optic sensor **100**. In one specific implementation, a double-side-polished silicon wafer (e.g., 200 μm thick) can be bonded on top of another larger silicon wafer using a layer of photoresist **154**. The larger silicon wafer can function as a silicon substrate **148** to facilitate the fabrication and later as a support for the fabricated silicon pillar **150**. Then another layer of photoresist **154** can be coated on the top of the double-side-polished silicon wafer and patterned accordingly using photolithography techniques. The patterned top silicon layer can be etched all the way to the silicon substrate **148** and the second layer of photoresist **154** using, for example, deep-reactive-ion-etching, leaving the upstanding silicon pillar(s) **150** attached to the silicon substrate **148**.

Then, a thin film adhesive is formed on a glass substrate (Block **304**). In some specific embodiments, such as the one illustrated in FIG. **3B**, an adhesive **156** including a thin film of UV-curable glue can be spin-coated on a piece of glass substrate **158**. It is contemplated that forming a thin film adhesive **156** may include using other adhesives and/or other methods for depositing and/or forming the adhesive **156**. In embodiments, the adhesive **156** may include a thin film adhesive (e.g., UV-curable glue, an epoxy-based adhesive, and/or a gel-based adhesive).

Shown in FIG. **3C**, an end face of an optical fiber is pressed onto the thin film adhesive (Block **306**). In implementations, the adhesive **156** can be transferred to a cleaved and cleaned end face **152** of an optical fiber **102** by pressing the end face **152** of the optical fiber **102** to the adhesive **156**

on the glass substrate **158**. Subsequently, the end face **152** and the adhesive **156** can be released from the glass substrate **158**.

As illustrated in FIGS. **3D** and **3E**, the optical thin film adhesive on the end face is placed onto the silicon pillar to provide the fiber optic sensor (Block **308**). The optical fiber **102** with the silicon pillar **150** (silicon layer **108**) attached can be lifted from the silicon substrate **148** and the second layer of photoresist **154**. Further, fabrication of the fiber optic sensor **100** may include cleaning residual photoresist **154** from the end of the silicon pillar **150** (e.g., with alcohol). Due to the ultra-thin thickness of the residual photoresist **154** between the optical fiber **102** and the silicon pillar **150**/silicon layer **108**, the reflection spectrum of the FP cavity within the fiber optic sensor **100** is not affected.

Then, the thin film adhesive is cured (Block **310**). In implementations, the adhesive **156** can be cured, for example, by UV irradiation (e.g., UV light **160**). It is contemplated that other bonding technology may be implemented to mount the silicon layer **108** (or other material) to the end face **152** of the optical fiber **102**, such as physical contact bonding.

It is contemplated that the above steps may be repeated to form a fiber optic sensor **100** with cascaded Fabry-Pérot cavities. For example, the optical fiber **102** with the silicon pillar **150** may be further pressed onto a second adhesive **166** on a glass substrate, placed on a second silicon pillar (e.g., second silicon layer **168**), and cured using UV light, to form a fiber optic sensor **100** with two Fabry-Pérot interferometers. Further Fabry-Pérot interferometers may be fabricated by repeating the above steps.

As described above, a first side (e.g., side or surface distal to the end face **152**) of the silicon pillar **150**/silicon layer **108** can be coated with an absorptive layer (e.g., coating) **112** and a second side (e.g., side or surface proximal or adjacent to the end face **152**) of the silicon pillar **150**/silicon layer **108** can be coated with a reflective dielectric thin film **110**. Thus, as described above, suitable techniques can be employed to deposit (e.g., coat) the respective surfaces of the silicon pillar **150**/silicon layer **108** with the respective absorptive layer (e.g., coating) **112** and/or the reflective dielectric thin film **110**.

FIG. **2C** illustrates an exemplary process **400** for fabricating a bolometer device **100**. As shown in FIG. **2C**, an optical fiber including a reflective dielectric film on a cleaved endface of the optical fiber is received (Block **402**). FIG. **4A** illustrates receiving at least one optical fiber **102** having a reflective dielectric thin film **110** disposed on a cleaved end of the optical fiber **102**. In some instances, multiple optical fibers **102** can include the reflective dielectric thin film **110** for batch processes.

FIG. **2C** illustrates forming at least one silicon pillar (Block **404**). In implementations, forming at least one silicon pillar **150** (e.g., silicon layer **108**) can include forming a silicon pillar **150**/silicon layer **108** that will function as a sensor head for the fiber optic bolometer device **100**. In one specific implementation, the at least one silicon pillar **150** can be prepared by patterning and DRIE etching a silicon wafer **148** with a selected thickness after which each silicon pillar **150** can be attached to the silicon wafer **148** main frame through very thin arms (see FIG. **4B**). The patterned top layer of the silicon wafer **148** can be etched all the way through the silicon substrate **148** using, for example, deep-reactive-ion-etching (DRIE), leaving the upstanding silicon pillar(s) **150** attached to the silicon substrate **148**. In some specific embodiments, the reflective dielectric thin film **110** can be deposited on the surface of the silicon wafer **148**

15

instead of the optical fiber endface **152** before patterning and dry etching the silicon wafer **148**.

Then, a thin film adhesive is placed on the reflective dielectric thin film (Block **406**). In some specific embodiments, such as the one illustrated in FIG. 4C, an adhesive **156** including a thin film of UV-curable glue can be spin-coated on a piece of glass substrate **158**. It is contemplated that forming a thin film adhesive **156** may include using other adhesives and/or other methods for depositing and/or forming the adhesive **156**. In embodiments, the adhesive **156** may include a thin film adhesive (e.g., UV-curable glue, an epoxy-based adhesive, and/or a gel-based adhesive). The optical fiber **102** can then be dipped onto the adhesive **156** and the substrate **158** and removed.

As illustrated in FIG. 2C, the adhesive on the end face of the optical fiber is placed onto the silicon pillar (Block **408**). As shown in FIG. 4D, the optical fiber **102** with the silicon pillar **150** (e.g., silicon layer **108**) attached can be lifted from the silicon substrate **148**. In a specific implementation, the optical fiber **102** with the adhesive **156** (e.g., UV glue) can be pushed and/or placed onto the silicon pillar **150** and exposed to UV light to cure the adhesive **156** so that the silicon pillar **150** is firmly attached to the optical fiber endface **152**, after which the optical fiber **102** can be lifted up with the silicon pillar **150**, where the silicon pillar **150** breaks/detaches from the silicon wafer **150** at the thin arm formed during initial etching.

Next, the silicon pillar is etched (Block **410**). In this step, etching the silicon pillar **150** can include can include fine-tuning the thickness of the silicon pillar **150** using, for example, wet etching (e.g., wet etchant **172** as shown in FIG. 4E), to control the wavelength positions of the interferometric fringes of the Fabry-Pérot interferometer within the bolometer device **100**.

As illustrated in FIG. 2C, an absorptive coating is then placed on the silicon pillar (Block **412**). In one specific embodiment, as shown in FIG. 4F, placing an absorptive coating **112** on the silicon pillar **150** can include applying a gold coating on the silicon pillar **150** on the optical fiber endface **152** using, for example, plating, sputtering, and/or other deposition processes.

It is contemplated that the above steps may be repeated to form a fiber optic sensor **100** with cascaded Fabry-Pérot cavities. For example, the optical fiber **102** with the silicon pillar **150** may be further pressed onto a second adhesive **166** on a glass substrate, placed on a second silicon pillar (e.g., second silicon layer **168**), and cured using UV light, to form a fiber optic sensor **100** with two Fabry-Pérot interferometers. Further Fabry-Pérot interferometers may be fabricated by repeating the above steps.

Multiple bolometers can be assembled to form a 2-D array and several bolometers can share a single tunable laser for signal demodulation, as illustrated in FIG. 3. In this example, a tunable laser, such as a distributed feedback (DFB) laser diode or an external cavity semiconductor laser, is used and the bolometers that share this laser are made to have their spectral notches within the wavelength tunable range of the laser. The light from the laser is split into each of the bolometers through a fiber-optic coupler and the reflected light from each bolometer is guided to a photodetector through a fiber-optic coupler or fiber-optic circulator. A separate photodetector is needed for each bolometer. The wavelength of the tunable laser is tuned and the waveform in the time domain from the photodetector is converted to the wavelength-domain to obtain the reflection spectrum of the bolometer.

16

FIG. 2D depicts an example process **500** for demodulating the fiber optic bolometer device **100**. Multiple fiber optic bolometer devices **100** can be assembled to form a 2-D bolometer array **170**, and several fiber optic bolometer devices **100** can share a single tunable laser (e.g., light source **126**) for signal demodulation, as illustrated in FIG. 5. As shown in FIG. 2D, a light source is caused to transmit light through a fiber optic to a fiber optic bolometer device array (Block **502**). In this implementation, controller **132** can cause light source **126** to transmit light (e.g., transmitted light **140**) through optical fiber **102** and circulator **124** to fiber optic bolometer device array **170**. Controller **132** can control the duration and intensity that the light source **126** transmits the transmitted light **140**. In a specific implementation, a light source **126** can include a tunable laser, such as a distributed feedback (DFB) laser diode or an external cavity semiconductor laser, and the fiber optic bolometer devices **100** in the fiber optic bolometer device array **170** that share the laser diode are configured to have their spectral notches within the wavelength tunable range of the laser diode. The transmitted light **140** from the light source **126** is split into each of the bolometers (four are illustrated in FIG. 5) through a fiber-optic coupler **124**.

Reflected light from the fiber optic sensor is received using at least one photodiode (Block **504**). In embodiments, the at least one photodiode **174** can be included in a spectrometer **128**. The spectrometer **128** can receive reflected light **162** and associated spectra from each of the fiber optic bolometer devices **100**, which can be recorded and/or analyzed by spectrometer **128** and/or controller **132**. The reflected light **162** from each fiber optic bolometer device **100** can be guided to a photodetector **174** through a fiber-optic coupler or fiber-optic circulator **124**. In general, a separate photodetector **174** is needed for each fiber optic bolometer device **100**.

An output from the at least one photodiode is analyzed based on the received reflected light (Block **506**). In implementations, the controller **132**, the at least one photodiode **174**, and/or the spectrometer **128** can analyze the reflected light **162** and the spectra to determine a wavelength shift in the spectra, which indicates a change in temperature. A variety of methods may be utilized to analyze and/or determine the wavelength shift in the spectra and for tracking the average wavelength. In a specific embodiment, analyzing an output from the spectrometer based on received reflected light can include using an average wavelength tracking method to further increase the resolution of wavelength and/or measurand. The wavelength of the light source **126** (e.g., tunable laser) can be tuned and the waveform in the time domain from each photodetector **174** can be converted to the wavelength-domain to obtain the reflection spectrum of each fiber optic bolometer device **100**.

CONCLUSION

Although the subject matter has been described in language specific to structural features and/or process operations, it is to be understood that the subject matter defined in the appended claims is not necessarily limited to the specific features or acts described above. Rather, the specific features and acts described above are disclosed as example forms of implementing the claims.

What is claimed is:

1. A fiber optic bolometer device comprising:
an optical fiber;

- a silicon layer disposed on an end face of the optical fiber, the silicon layer comprising a first surface and a second surface, where the silicon layer comprises a Fabry-Pérot interferometer;
 - a reflective dielectric film disposed over the first surface of the silicon layer, the reflective dielectric film adjacent to an end face of the optical fiber; and
 - an absorptive coating disposed over the second surface of the silicon layer, the second surface distal to the end face of the optical fiber.
2. The fiber optic bolometer device of claim 1, wherein the optical fiber comprises at least one of a microstructured fiber, a photonic crystal fiber, a polarization-maintaining fiber, or a side-hole fiber.
 3. The fiber optic bolometer device of claim 1, wherein the optical fiber includes an expanded core disposed proximate to the end face of the optical fiber.
 4. The fiber optic bolometer device of claim 1, wherein the silicon layer includes a silicon pillar.
 5. The fiber optic bolometer device of claim 1, wherein the absorptive coating comprises at least one metal layer.
 6. The fiber optic bolometer device of claim 5, wherein the at least one metal layer comprises at least one of gold or platinum.
 7. The fiber optic bolometer device of claim 1, wherein the optical fiber includes a cavity disposed along at least a portion of the optical fiber and proximate to the end face of the optical fiber.
 8. The fiber optic bolometer device of claim 7, wherein the cavity is at least partially filled with a thermal conductor.
 9. The fiber optic bolometer device of claim 1, further comprising a mirror coating disposed between the optical fiber and the absorptive coating.
 10. The fiber optic bolometer device of claim 9, wherein the mirror coating is disposed between the silicon layer and the absorptive coating.
 11. The fiber optic bolometer device of claim 1, further comprising at least one of a graded-index lens or a section of graded-index fiber disposed between the end face of the optical fiber and the absorptive coating.
 12. A method for fabricating a fiber optic bolometer device, comprising:
 - receiving an optical fiber including a reflective dielectric film on a cleaved endface of the optical fiber;
 - forming at least one silicon pillar;

- placing an adhesive on the reflective dielectric film;
 - pressing the optical fiber with the adhesive onto the silicon pillar;
 - etching the silicon pillar; and
 - placing an absorptive coating on the silicon pillar.
13. The method for fabricating a bolometer device in claim 12, wherein the absorptive coating includes gold.
 14. A method for demodulating a fiber optic bolometer device array, comprising:
 - causing a light source to transmit light through an optical fiber and a circulator to a fiber optic bolometer device array including at least one fiber optic bolometer device, where the at least one fiber optic bolometer device includes a silicon layer and an absorptive layer disposed on an end face of the fiber optic bolometer device;
 - receiving reflected light from the fiber optic bolometer device array using at least one photodiode; and
 - analyzing an output from the at least one photodiode based on received reflected light to obtain a reflection spectrum of the bolometer.
 15. The method for demodulating a fiber optic bolometer device array of claim 14, wherein the optical fiber comprises at least one of a microstructured fiber, a photonic crystal fiber, a polarization-maintaining fiber, or a side-hole fiber.
 16. The method for demodulating a fiber optic bolometer device array of claim 14, wherein the optical fiber includes an expanded core disposed proximate to the end face.
 17. The method for demodulating a fiber optic bolometer device array of claim 14, wherein the optical fiber includes a cavity disposed along at least a portion of the optical fiber and proximate to the end face of the optical fiber.
 18. The method for demodulating a fiber optic bolometer device array of claim 17, wherein the cavity is at least partially filled with a thermal conductor.
 19. The method for demodulating a fiber optic bolometer device array of claim 14, further comprising a mirror coating disposed between the optical fiber and the absorptive coating.
 20. The method for demodulating a fiber optic bolometer device array of claim 14, further comprising at least one of a graded-index lens or a section of graded-index fiber disposed between the end face of the optical fiber and the absorptive coating.

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