



Title	Finite Element Analysis of Lamb Wave Scattering in an Elastic Plate
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Citation	IEEE Transactions on Sonics and Ultrasonics 31(1):18-24
Issue Date	1984-01
Doc URL	http://hdl.handle.net/2115/6067
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Type	article
Note URL	http://ieeexplore.ieee.org/xpl/freeabs/all.jsp?isnumber=32865&arnumber=1539532&count=15&index=7
File Information	ITSU3101.pdf



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Finite-Element Analysis of Lamb Wave Scattering in an Elastic Plate Waveguide

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Abstract—A method of the solution of scattering of the fundamental symmetric Lamb wave in an elastic plate waveguide is described. The approach is a combination of the finite-element and the analytical method. The numerical examples on the scattering by a wedge-shaped internal crack and a wedge-shaped surface crack in a plate are given. The reflection coefficient of the internal crack is considerably influenced by the wedge apex angle and the resonance phenomena arise in the region of the crack. On the other hand, the reflection coefficient of the surface crack is not very much affected by the wedge apex angle. The validity of the method is confirmed by comparing numerical results for an infinitely thin internal crack normal to the surface of a plate with the results of the variational method.

I. INTRODUCTION

THE scattering of guided modes by the discontinuities in an elastic waveguide is a basic problem in nondestructive evaluation and also has important implications with regard to electrical signal-processing functions [1]–[4], and the scattering of Lamb waves by cracks in an elastic plate has been investigated extensively [5]–[10]. Auld *et al.* have analyzed the scattering of Lamb waves by an infinitely thin crack normal to the surface of a plate using the variational method [5]–[7]. Rokhlin has analyzed the scattering of Lamb waves by an infinitely thin crack parallel to the surface of a plate using the modified Wiener-Hopf method [8] or the method

of multiple diffractions [9], [10]. Although these methods are useful for the discontinuities of regular shape, it seems to be difficult to apply these methods to those of arbitrary shape. Recently the numerical method based on the finite-element method has been developed for the analysis of the scattering of horizontally polarized shear (SH) waves with a single particle-velocity component parallel to the plate surface [11]–[13]. This approach is useful for the analysis of the scattering by the arbitrarily shaped discontinuities.

In this paper, this numerical approach based on the finite-element method is extended to the analysis of the scattering of Lamb waves with two particle-velocity components, lying in the plane perpendicular to the plate surface. Numerical examples on the scattering by a wedge-shaped internal crack and a wedge-shaped surface crack in a plate are given. The reflection coefficient of the internal crack is considerably influenced by the wedge apex angle and the resonance phenomena arise in the region of the crack. On the other hand, the reflection coefficient of the surface crack is not very much affected by the wedge apex angle. The validity of the method is confirmed by comparing numerical results for an infinitely thin internal crack normal to the surface of a plate with the results of the variational method [7].

II. BASIC EQUATIONS

In order to minimize the details, we consider the symmetric Lamb wave excitation of a symmetric plate waveguide as shown in Fig. 1, where the boundaries Γ_1 and Γ_2 connect

Manuscript received May 4, 1983; revised October 11, 1983.

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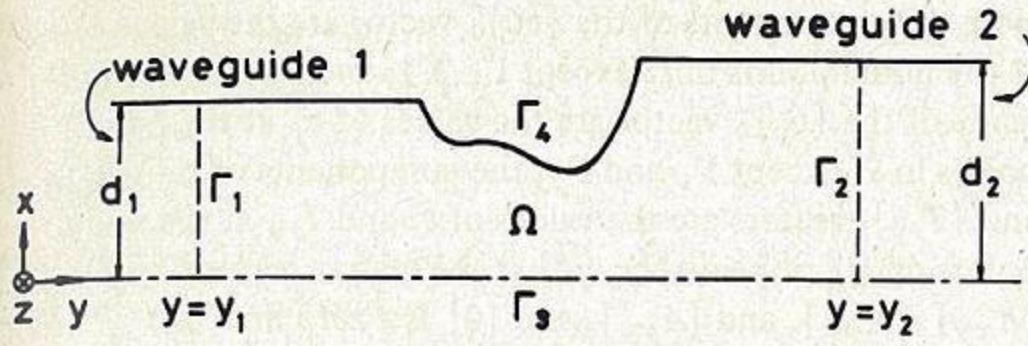


Fig. 1. Discontinuity in elastic plate waveguide.

the discontinuities to the waveguides 1 and 2, respectively, the x component of the particle velocity v_x and the y component of the particle velocity v_y are antisymmetric and symmetric about the midplane Γ_3 ($x = 0$), respectively, the plane Γ_4 is the stress-free surface, and the region Ω with the boundaries Γ_1 to Γ_4 completely encloses the discontinuities. The plate waveguide is assumed to have some discontinuities which are symmetric about the midplane Γ_3 .

Assuming that there is no variation in the z direction, we have the following basic equations [1]:

$$\partial T_{rx}/\partial x + \partial T_{ry}/\partial y - j\omega\rho v_r = 0, \quad r = x, y, \quad (1)$$

$$\begin{bmatrix} j\omega T_{xx} \\ j\omega T_{yy} \\ j\omega T_{xy} \end{bmatrix} = \begin{bmatrix} \lambda + 2\mu & \lambda & 0 \\ \lambda & \lambda + 2\mu & 0 \\ 0 & 0 & \mu \end{bmatrix} \begin{bmatrix} \partial v_x/\partial x \\ \partial v_y/\partial y \\ \partial v_x/\partial y + \partial v_y/\partial x \end{bmatrix}, \quad (2)$$

where T_{xx} , T_{yy} , and $T_{xy} = T_{yx}$ are the stresses, ω is the angular frequency, ρ is the mass density, and λ and μ are the Lamé constants.

III. MATHEMATICAL FORMULATION

A. Finite-Element Approach

Dividing the region Ω into a number of second-order triangular elements [14], [15] as shown in Fig. 2, the particle velocity v_r within each element is defined in terms of the particle velocity $v_{r,k}$ at the nodal point k ($k = 1, 2, \dots, 6$):

$$v_r = \{N\}^T \{v_r\}_e, \quad r = x, y, \quad (3)$$

where

$$\{v_r\}_e = [v_{r,1} v_{r,2} v_{r,3} v_{r,4} v_{r,5} v_{r,6}]^T, \quad r = x, y, \quad (4)$$

$$\{N\} = [N_1 N_2 N_3 N_4 N_5 N_6]^T. \quad (5)$$

Here $\{v_r\}_e$ is the particle-velocity vector corresponding to the nodal points within each element, T , $\{\cdot\}$, and $\{\cdot\}^T$ denote a transpose, a column vector, and a row vector, respectively, and shape functions N_1 to N_6 are given by

$$N_1 = L_1(2L_1 - 1) \quad (6a)$$

$$N_2 = L_2(2L_2 - 1) \quad (6b)$$

$$N_3 = L_3(2L_3 - 1) \quad (6c)$$

$$N_4 = 4L_1L_2 \quad (6d)$$

$$N_5 = 4L_2L_3 \quad (6e)$$

$$N_6 = 4L_3L_1 \quad (6f)$$

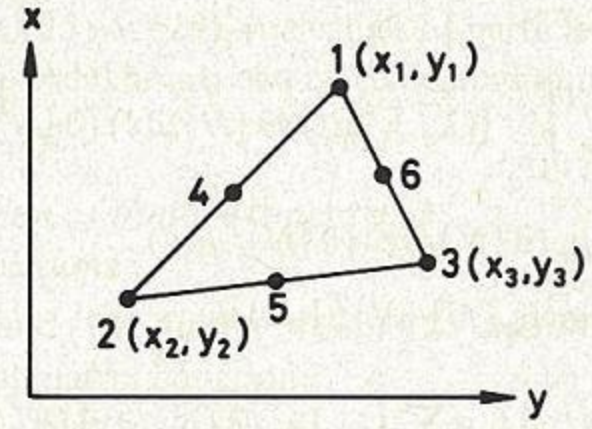


Fig. 2. Second-order triangular element.

with the area coordinates L_1 , L_2 , and L_3 [14], [15]. The relation equation between the area coordinates and Cartesian coordinates is given by

$$\begin{bmatrix} x \\ y \\ 1 \end{bmatrix} = \begin{bmatrix} x_1 & x_2 & x_3 \\ y_1 & y_2 & y_3 \\ 1 & 1 & 1 \end{bmatrix} \begin{bmatrix} L_1 \\ L_2 \\ L_3 \end{bmatrix}, \quad (7)$$

where (x_j, y_j) are the Cartesian coordinates of the vertex j ($j = 1, 2, 3$) of the triangle.

Using a Galerkin procedure on (1), we obtain

$$\int_{\Omega_e} \{N\} (\partial T_{rx}/\partial x + \partial T_{ry}/\partial y - j\omega\rho_e v_r) d\Omega = \{0\}, \quad r = x, y, \quad (8)$$

where Ω_e represents an element subdomain and $\{0\}$ is a null vector.

Integrating by parts, we obtain for (8)

$$\begin{aligned} & \int_{\Omega_e} [(\partial\{N\}/\partial x)T_{rx} + (\partial\{N\}/\partial y)T_{ry} + j\omega\rho_e\{N\}v_r] d\Omega \\ & - \int_{\Gamma_e} \{N\}T_{rn} d\Gamma = \{0\}, \quad r = x, y, \end{aligned} \quad (9)$$

where

$$T_{rn} = T_{rx}n_x + T_{ry}n_y, \quad r = x, y. \quad (10)$$

Here Γ_e represents the contour of the triangular element, and n_x and n_y are the x and y components of an outward normal unit-vector to Γ_e , respectively.

Noting that T_{xn} and T_{yn} are continuous across Γ_e (boundary conditions at the interface between two different media), $v_x = T_{yx} = 0$ on Γ_3 (midplane), and $T_{xn} = T_{yn} = 0$ on Γ_4 (stress-free surface), from (2), (3), and (9) the following global matrix equation is derived:

$$\begin{bmatrix} [A_{xx}] & [A_{xy}] \\ [A_{yx}] & [A_{yy}] \end{bmatrix} \begin{bmatrix} \{v_x\} \\ \{v_y\} \end{bmatrix} = \sum_{i=1}^2 \sum_{e'} (-1)^i j\omega \begin{bmatrix} \int_{\Gamma_{i,e'}} \{N\}_i T_{xy,i}(x, y_i) dx \\ \int_{\Gamma_{i,e'}} \{N\}_i T_{yy,i}(x, y_i) dx \end{bmatrix} \quad (11)$$

where

$$[A_{xx}] = \sum_e \int_{\Omega_e} [(\lambda_e + 2\mu_e) (\partial \{N\} / \partial x) (\partial \{N\}^T / \partial x) + \mu_e (\partial \{N\} / \partial y) (\partial \{N\}^T / \partial y) - \omega^2 \rho_e \{N\} \{N\}^T] dx dy, \quad (12a)$$

$$[A_{xy}] = [A_{yx}]^T = \sum_e \int_{\Omega_e} [\lambda_e (\partial \{N\} / \partial x) (\partial \{N\}^T / \partial y) + \mu_e (\partial \{N\} / \partial y) (\partial \{N\}^T / \partial x)] dx dy, \quad (12b)$$

$$[A_{yy}] = \sum_e \int_{\Omega_e} [\mu_e (\partial \{N\} / \partial x) (\partial \{N\}^T / \partial x) + (\lambda_e + 2\mu_e) (\partial \{N\} / \partial y) (\partial \{N\}^T / \partial y) - \omega^2 \rho_e \{N\} \{N\}^T] dx dy. \quad (12c)$$

Here the components of the $\{v_x\}$ vector are the values of v_x at all nodal points in Ω except Γ_3 , the components of the $\{v_y\}$ vector are the values of v_y at all nodal points in Ω , Σ_e and $\Sigma_{e'}$ extend over all different elements and the elements related to Γ_i ($i = 1, 2$), respectively, $T_{xy,i}(x, y_i)$ and $T_{yy,i}(x, y_i)$ are the stresses on Γ_i , and $\{N\}_i$ is the shape function vector on Γ_i , namely, $\{N\}_i = \{N(x, y_i)\}$.

Using the shape function $\{N\}_i$, the particle velocity $v_{r,i}(x, y_i)$ and the stress $T_{ry,i}(x, y_i)$ on Γ_i may be discretized as follows:

$$v_{r,i}(x, y_i) = \{N\}_i^T \{v_r\}_{i,e'}, \quad r = x, y, \quad (13a)$$

$$T_{ry,i}(x, y_i) = \{N\}_i^T \{T_{ry}\}_{i,e'}, \quad r = x, y, \quad (13b)$$

where $\{v_r\}_{i,e'}$ and $\{T_{ry}\}_{i,e'}$ are the particle-velocity vector and the stress vector corresponding to the nodal points within each element related to Γ_i , respectively.

Substituting (13) into (11), we obtain

$$[A] \begin{bmatrix} \{v_x\}_0 \\ \{v_y\}_0 \\ \{v_x\}_{12} \\ \{v_y\}_{12} \end{bmatrix} = \begin{bmatrix} \{0\} \\ [B] \{T_{xy}\}_{12} \\ [B] \{T_{yy}\}_{12} \end{bmatrix}, \quad (14)$$

where

$$\{v_r\}_{12} = \begin{bmatrix} \{v_r\}_1 \\ \{v_r\}_2 \end{bmatrix}, \quad r = x, y, \quad (15)$$

$$\{T_{ry}\}_{12} = \begin{bmatrix} \{T_{ry}\}_1 \\ \{T_{ry}\}_2 \end{bmatrix}, \quad r = x, y, \quad (16)$$

$$[B] = \begin{bmatrix} [B]_1 & [0] \\ [0] & [B]_2 \end{bmatrix}, \quad (17)$$

and

$$[B]_i = (-1)^i j \omega \sum_{e'} \int_{\Gamma_{i,e'}} \{N\}_i \{N\}_i^T dx, \quad i = 1, 2. \quad (18)$$

Here the components of the $\{v_x\}_0$ vector are the values of v_x at the nodal points in Ω except Γ_1 , Γ_2 , and Γ_3 , the components of the $\{v_y\}_0$ vector are the values of v_y at the nodal points in Ω except Γ_1 and Γ_2 , the components of the $\{v_r\}_i$ and $\{T_{ry}\}_i$ vectors are the values of v_r and T_{ry} at the nodal points on Γ_i , respectively, $[A]$ is the matrix formed by $[A_{xx}]$, $[A_{xy}]$, $[A_{yx}]$, and $[A_{yy}]$, and $[0]$ is a zero matrix.

B. Analytical Approach

In (14), the values of the stresses T_{xy} and T_{yy} on Γ_i ($i = 1, 2$) are unknown, so that it is necessary to introduce the compatibility conditions for the interface boundary Γ_i between the interior region ($y_1 \leq y \leq y_2$) and the exterior region ($y \leq y_1$, $y \geq y_2$). Considering the analytical relation between $[-T_{xy} \ v_y]^T$ on Γ_i and $[v_x \ T_{yy}]^T$ on Γ_i which can be obtained by use of the orthogonality relation [1], [2], [5] of the normal modes in an elastic plate waveguide, the values of particle velocities and stresses at the nodal points can be calculated numerically from (14). The solutions $[v_x \ T_{yy}]^T$ (or $[-T_{xy} \ v_y]^T$) on Γ_i allow the determination of the reflection coefficient and the transmission coefficient. The details will be discussed later.

The internal fields in the waveguide i ($i = 1, 2$) in Fig. 1 are represented by the sum of normal modes as [1], [2], [5]

$$\begin{bmatrix} v_{x,i}(x, y) \\ T_{yy,i}(x, y) \end{bmatrix} = \sum_m [a_{im} \exp(-j\beta_{im}y) + b_{im} \exp(j\beta_{im}y)] \cdot \{f_{im}(x)\} \quad (19a)$$

$$\begin{bmatrix} -T_{xy,i}(x, y) \\ v_{y,i}(x, y) \end{bmatrix} = \sum_m [a_{im} \exp(-j\beta_{im}y) - b_{im} \exp(j\beta_{im}y)] \cdot \{g_{im}(x)\}, \quad (19b)$$

where

$$\{f_{im}(x)\} = [f_{x,im}(x) \ f_{y,im}(x)]^T \quad (20a)$$

and

$$\{g_{im}(x)\} = [g_{x,im}(x) \ g_{y,im}(x)]^T. \quad (20b)$$

Here a_{im} and b_{im} are the amplitudes of the m th mode ($m = 0, 1, 2, \dots$) in the waveguide i propagating (or decaying) toward the $+y$ and $-y$ directions, respectively, and β_{im} is the wavenumber in the y direction. The mode functions $\{f_{im}(x)\}$ and $\{g_{im}(x)\}$ satisfy the following orthonormalization condition [1]:

$$\int_0^{d_i} \{f_{im}(x)\}^T \{g_{im'}(x)\} dx = \int_0^{d_i} \{g_{im}(x)\}^T \cdot \{f_{im'}(x)\} dx = \delta_{mm'}, \quad (21)$$

where $\delta_{mm'}$ is the Kronecker δ . The dispersion relation for β_{im} and the mode functions are given in the Appendix.

Now, assuming that the fundamental Lamb wave ($m = 0$) of unit amplitude is incident from the left of waveguide 1 in Fig. 1, the amplitudes of normal modes may be written as

$$a_{1m} = \begin{cases} 1, & m = 0; \\ 0, & m = 1, 2, 3, \dots, \end{cases} \quad (22a)$$

$$b_{2m} = 0 \quad m = 0, 1, 2, \dots \quad (22b)$$

Considering (19), (21), and (22), $T_{xy,i}(x, y_i)$ and $v_{y,i}(x, y_i)$ on Γ_i may be expressed as

$$\begin{bmatrix} -T_{xy,i}(x, y_i) \\ v_{y,i}(x, y_i) \end{bmatrix} = 2\delta_{i1} \exp(-j\beta_{10}y_1) \{g_{10}(x)\} \\ + (-1)^i \int_0^{d_i} \sum_m \{g_{im}(x)\} \{g_{im}(x')\}^T \\ \cdot \begin{bmatrix} v_{x,i}(x', y_i) \\ T_{yy,i}(x', y_i) \end{bmatrix} dx'. \quad (23)$$

Similarly, $v_{x,i}(x, y_i)$ and $T_{yy,i}(x, y_i)$ on Γ_i may be expressed as

$$\begin{bmatrix} v_{x,i}(x, y_i) \\ T_{yy,i}(x, y_i) \end{bmatrix} = 2\delta_{i1} \exp(-j\beta_{10}y_1) \{f_{10}(x)\} \\ + (-1)^i \int_0^{d_i} \sum_m \{f_{im}(x)\} \{f_{im}(x')\}^T \\ \cdot \begin{bmatrix} -T_{xy,i}(x', y_i) \\ v_{y,i}(x', y_i) \end{bmatrix} dx'. \quad (24)$$

Using (3) and (13), (23) can be discretized as follows:

$$\begin{bmatrix} -\{T_{xy}\}_i \\ \{v_y\}_i \end{bmatrix} = \delta_{i1} \begin{bmatrix} \{g_x\}_1 \\ \{g_y\}_1 \end{bmatrix} + \begin{bmatrix} [G_{xx}]_i & [G_{xy}]_i \\ [G_{yx}]_i & [G_{yy}]_i \end{bmatrix} \begin{bmatrix} \{v_x\}_i \\ \{T_{yy}\}_i \end{bmatrix} \quad (25)$$

where

$$\{g_r\}_1 = 2 \exp(-j\beta_{10}y_1) \{g_{r,0}\}_1, \quad r = x, y, \quad (26)$$

$$[G_{rr'}]_i = (-1)^i \sum_m \{g_{r,m}\}_i \sum_{e'} \int_{\Gamma_{i,e'}} g_{r',im}(x') \{N(x', y_i)\}^T dx', \\ r, r' = x, y. \quad (27)$$

Here the components of the $\{g_{r,m}\}_i$ vector are the values of $g_{r,im}(x)$ at the nodal points on Γ_i .

Similarly, (24) can be discretized as follows:

$$\begin{bmatrix} \{v_x\}_i \\ \{T_{yy}\}_i \end{bmatrix} = \delta_{i1} \begin{bmatrix} \{f_x\}_1 \\ \{f_y\}_2 \end{bmatrix} + \begin{bmatrix} [F_{xx}]_i & [F_{xy}]_i \\ [F_{yx}]_i & [F_{yy}]_i \end{bmatrix} \begin{bmatrix} -\{T_{xy}\}_i \\ \{v_y\}_i \end{bmatrix} \quad (28)$$

where

$$\{f_r\}_1 = 2 \exp(-j\beta_{10}y_1) \{f_{r,0}\}_1, \quad r = x, y, \quad (29)$$

$$[F_{rr'}]_i = (-1)^i \sum_m \{f_{r,m}\}_i \sum_{e'} \int_{\Gamma_{i,e'}} f_{r',im}(x') \{N(x', y_i)\}^T dx', \\ r, r' = x, y. \quad (30)$$

Here the components of the $\{f_{r,m}\}_i$ vector are the values of $f_{r,im}(x)$ at the nodal points on Γ_i .

Using either (25) or (28), the values of particle velocities and stresses at the nodal points can be calculated numerically from (14).

C. Combination of Finite-Element and Analytical Relations

Using (15) and (16), from (14) and (25) we obtain the following final matrix equation:

$$\begin{bmatrix} [A] & [0] \\ [0] & -[G_{xx}] & [0] & [1] & -[G_{xy}] \\ & -[G_{yx}] & [1] & [0] & -[G_{yy}] \end{bmatrix} \begin{bmatrix} \{v_x\}_0 \\ \{v_y\}_0 \\ \{v_x\}_{12} \\ \{v_y\}_{12} \\ -\{T_{xy}\}_{12} \\ \{T_{yy}\}_{12} \end{bmatrix} = \begin{bmatrix} \{0\} \\ \{0\} \\ \{g_x\}_{12} \\ \{g_y\}_{12} \end{bmatrix} \quad (31)$$

where

$$\{g_r\}_{12} = \begin{bmatrix} \{g_r\}_1 \\ \{0\} \end{bmatrix}, \quad r = x, y, \quad (32)$$

$$[G_{rr'}] = \begin{bmatrix} [G_{rr'}]_1 & [0] \\ [0] & [G_{rr'}]_2 \end{bmatrix}, \quad r, r' = x, y. \quad (33)$$

Here [1] is a unit matrix.

Similarly, from (14) and (28) we obtain the following final matrix equation:

$$\begin{bmatrix} [A] & [0] \\ [0] & [1] & -[F_{xy}] & -[F_{xx}] & [0] \\ & [0] & -[F_{yy}] & -[F_{yx}] & [1] \end{bmatrix} \begin{bmatrix} \{v_x\}_0 \\ \{v_y\}_0 \\ \{v_x\}_{12} \\ \{v_y\}_{12} \\ -\{T_{xy}\}_{12} \\ \{T_{yy}\}_{12} \end{bmatrix} = \begin{bmatrix} \{0\} \\ \{0\} \\ \{f_x\}_{12} \\ \{f_y\}_{12} \end{bmatrix} \quad (34)$$

where

$$\{f_r\}_{12} = \begin{bmatrix} \{f_r\}_1 \\ \{0\} \end{bmatrix}, \quad r = x, y, \quad (35)$$

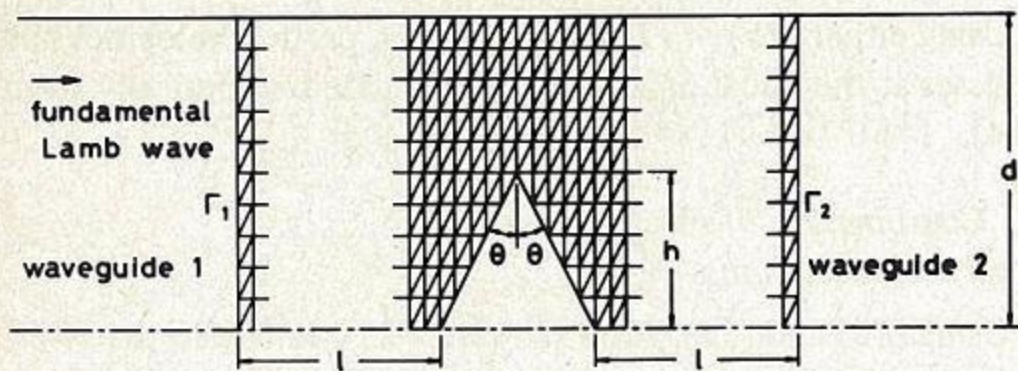


Fig. 3. Typical division of wedge-shaped internal crack.

$$[F_{rr'}] = \begin{bmatrix} [F_{rr'}]_1 & [0] \\ [0] & [F_{rr'}]_2 \end{bmatrix}, \quad r, r' = x, y. \quad (36)$$

The values of the particle velocity v_x and the stress T_{yy} at the nodal points on Γ_i ($i = 1, 2$), namely, $\{v_x\}_i$ and $\{T_{yy}\}_i$, are computed from (31) or (34), and then, by using (13), $v_{x,i}(x, y_i)$ and $T_{yy,i}(x, y_i)$ are calculated from these values. The solutions $v_{x,i}(x, y_i)$ and $T_{yy,i}(x, y_i)$ allow the determination of the reflection coefficient r at $y = y_1 \equiv 0$ and the transmission coefficient t at $y = y_2$ of the fundamental Lamb wave. Considering (19), (21), and (22), r and t may be written as

$$r \equiv b_{10} = -1 + \int_0^{d_1} \{g_{10}(x)\}^T \begin{bmatrix} v_{x,1}(x, y_1 = 0) \\ T_{yy,1}(x, y_1 = 0) \end{bmatrix} dx, \quad (37)$$

$$t \equiv a_{20} \exp(-j\beta_{20}y_2) = \int_0^{d_2} \{g_{20}(x)\}^T \begin{bmatrix} v_{x,2}(x, y_2) \\ T_{yy,2}(x, y_2) \end{bmatrix} dx. \quad (38)$$

IV. ANALYSIS OF LAMB WAVE SCATTERING BY A CRACK

In this section, we present the computed results for the fundamental Lamb wave reflection coefficient of a wedge-shaped crack with stress-free surfaces in a plate of thickness $2d$. A typical division of an internal crack into second-order triangular elements is shown in Fig. 3, where 2θ is the wedge apex angle. If the boundaries Γ_1 and Γ_2 are located slightly away from the discontinuity, the evanescent higher modes with pure imaginary and complex wavenumbers [1], [5]–[10] have little effect on the fields on Γ_1 and Γ_2 due to rapidly decaying modes from the discontinuity and the influence of the evanescent higher modes is involved in the finite-element region Ω . Hence it is usually sufficient to consider the propagating modes only in (27) and (30), and, if necessary, a few evanescent higher modes for a reasonable approximation. Convergence of the solution is checked by increasing a value of l in Fig. 3. In this calculation, a Poisson's ratio $\sigma = 0.31$ and $2k_s d/\pi = 1.0$, where $k_s = \omega\sqrt{\rho/\mu}$. All the higher modes are nonpropagating evanescent modes. In order to present the numerical verification of the method, Fig. 4 shows the magnitude and the phase of the reflection coefficient of an infinitely thin internal crack ($\theta = 0$) normal to the surface of a plate as a function of l/λ_{L0} , where λ_{L0} is the wavelength of the fundamental Lamb wave and the crack to plate thickness ratio $h/d = 0.5$. The phase is evaluated at the position

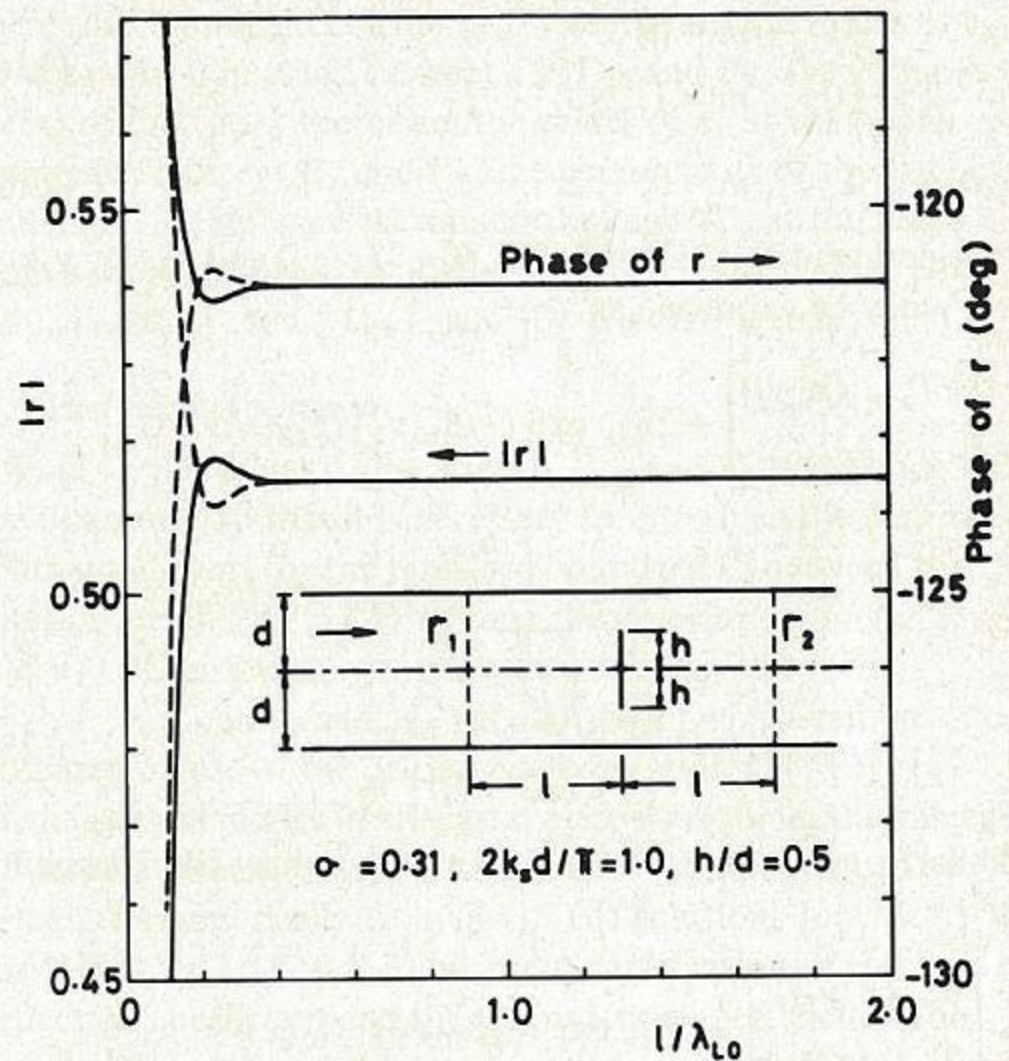
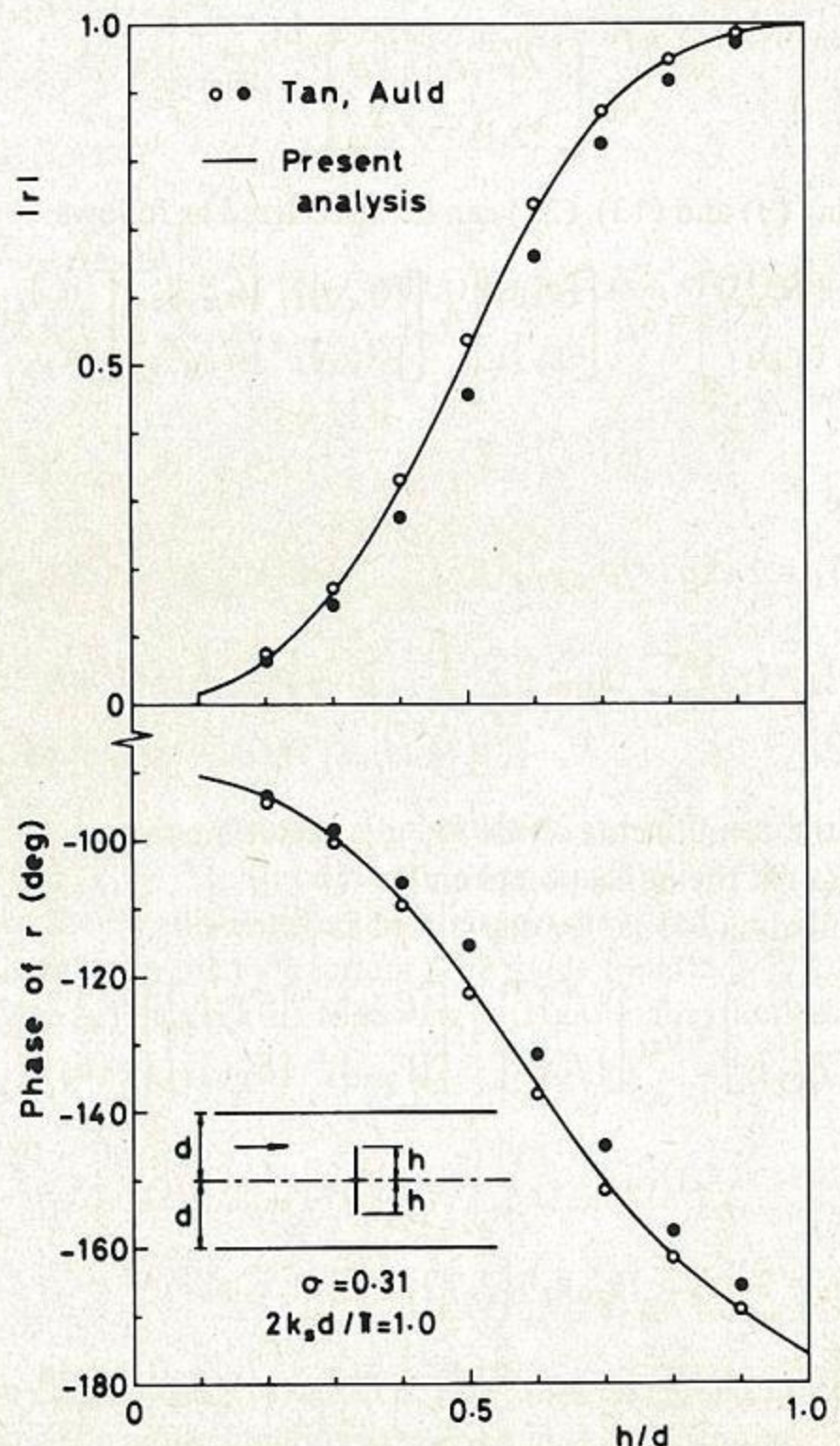


Fig. 4. Convergence behavior in calculation of reflection coefficients of an infinitely thin internal crack. The solid line is the results obtained by using (31). The broken line is the results obtained by using (34).

Fig. 5. Reflection coefficient of an infinitely thin internal crack. \circ results [7] of variational method with the trial function $v_y = \sqrt{1 - (x/h)^2}$ and $v_x = 0$. \bullet results [7] of variational method with the trial function $v_y = \cos(\pi x/2h)$ and $v_x = 0$.

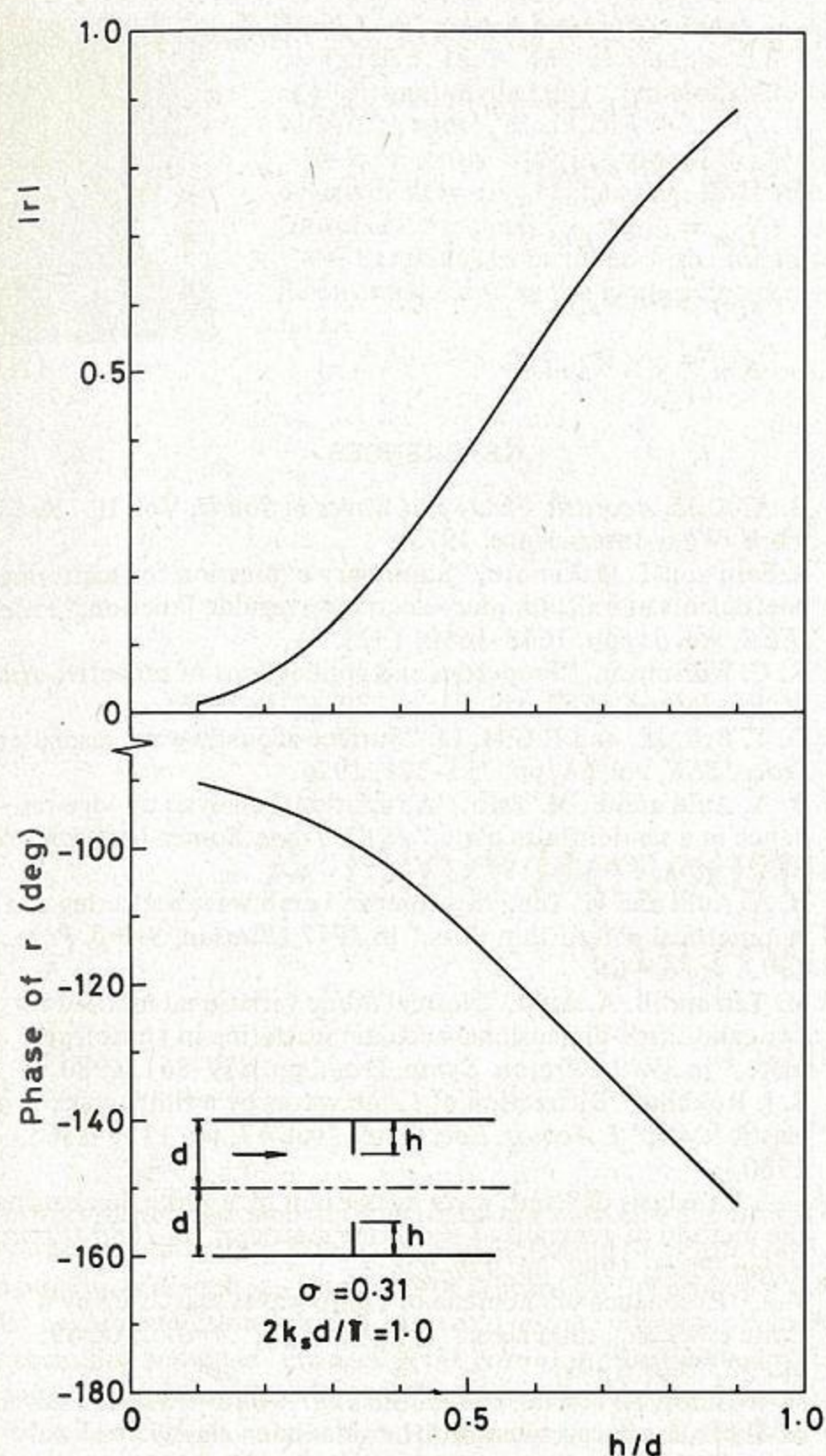


Fig. 6. Reflection coefficient of infinitely thin surface crack.

of a crack. The difference between the value (solid lines) calculated from (31) and the value (dashed lines) calculated from (34) can be distinguished only for the range of $l/\lambda_{L0} \lesssim 0.5$, and the two values converge with $l/\lambda_{L0} \approx 0.5$. Therefore, we set l equal to $2\lambda_{L0}$ and present only the results obtained by using (31).

Fig. 5 shows the magnitude and the phase of the reflection coefficient of an infinitely thin internal crack normal to the surface of a plate as a function of h/d . Agreement between our results and the results (circles) of the variational method with the trial function $v_y = \sqrt{1 - (x/h)^2}$ and $v_x = 0$ [7] is seen to be excellent. The results are in good agreement with the results (dots) of the variation method with the trial function $v_y = \cos(\pi x/2h)$ and $v_x = 0$ [7] at small values of h/d .

Fig. 6 shows the magnitude and the phase of the reflection coefficient of an infinitely thin surface crack normal to the surface of a plate as a function of h/d . It is seen that the magnitude of the reflection coefficient of the infinitely thin surface crack is smaller than that of the infinitely thin internal crack.

Figs. 7 and 8 show the magnitude of the reflection coefficient of a wedge-shaped internal crack and a wedge-shaped surface crack as a function of the wedge apex angle $\tan \theta$,

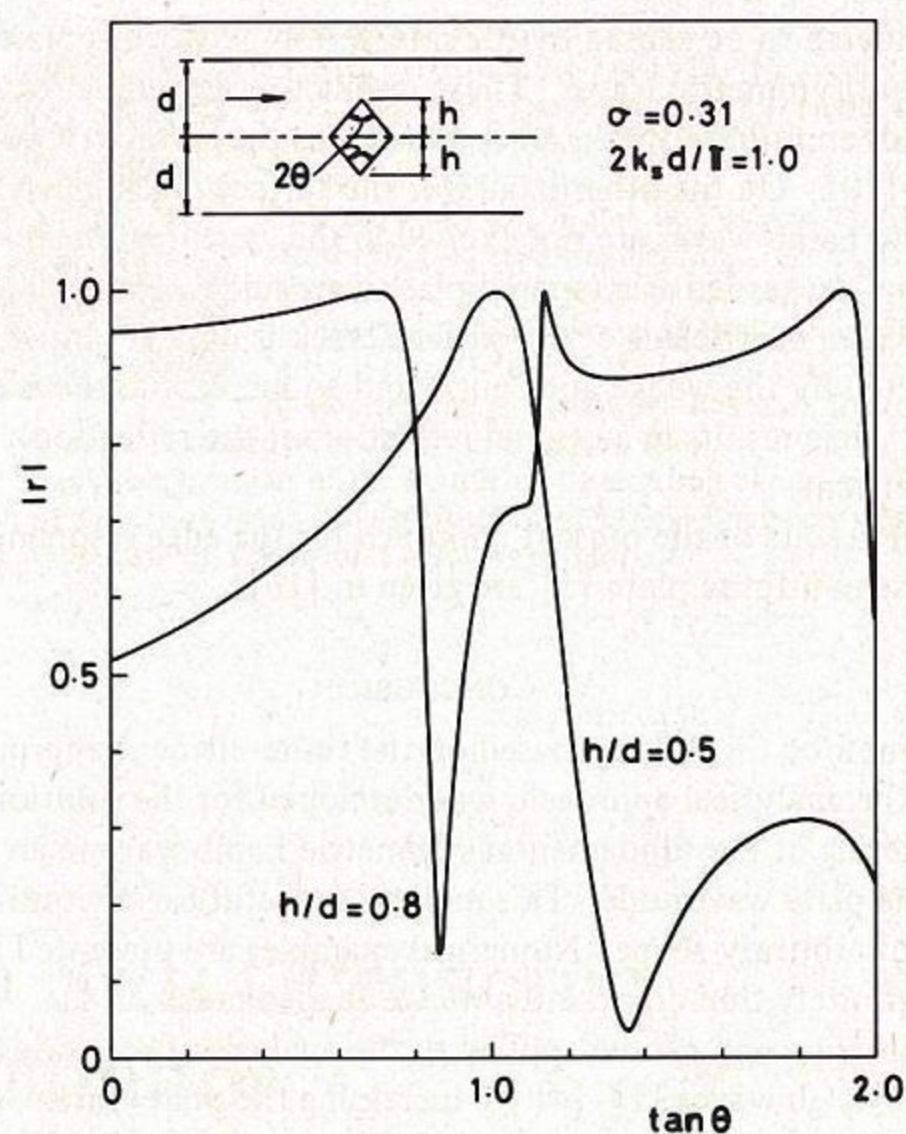


Fig. 7. Reflection coefficient of wedge-shaped internal crack.

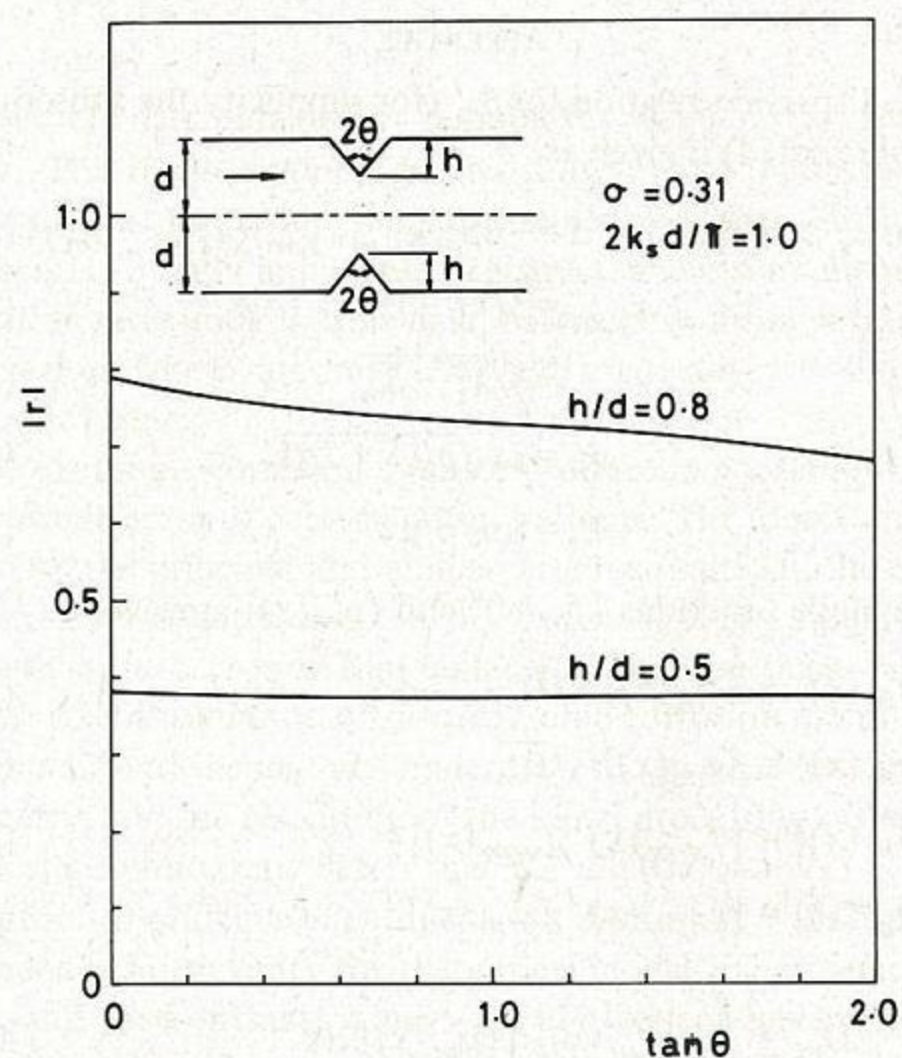


Fig. 8. Reflection coefficient of wedge-shaped surface crack.

respectively. The reflection coefficient of the internal crack is considerably influenced by the wedge apex angle and the curves exhibit resonances, resulting in complete reflection of the incident wave. By virtue of the problem's symmetry, for the incidence of the fundamental symmetric Lamb wave the antisymmetric Lamb waves are not excited in a plate except the region occupied by the crack. In the crack-region the plate waveguide branches into two waveguides, and both symmetric and antisymmetric Lamb waves are excited in each separated waveguide of length $2h \tan \theta$. The resonances are

considered to be caused by the interaction between symmetric and antisymmetric waves. These resonances are similar to the case of an infinitely thin crack parallel to the surface of a plate [8]–[10]. On the other hand, for the surface crack antisymmetric Lamb waves are not excited in the crack-region and this region is regarded as a tapered plate waveguide. Therefore, the reflection coefficient of the surface crack is not very much affected by the wedge apex angle and an increase in the wedge apex angle results in a general reduction of the reflection coefficient.

The results of the present approach for the edge resonance in a semi-infinite plate [5] are given in [16].

V. CONCLUSION

A method of analysis, based on the finite-element approach and the analytical approach, was developed for the solution of scattering of the fundamental symmetric Lamb wave in an elastic plate waveguide. This method is useful for discontinuities of arbitrary shape. Numerical examples are presented for an infinitely thin crack and a wedge-shaped crack.

This approach can be applied to the analysis of scattering of Rayleigh waves [1]–[4] by increasing the plate thickness in the same manner as the case of SH-type piezoelectric surface waves [12].

APPENDIX

The dispersion relation for β_m (for simplicity the subscript i is abbreviated) is given as

$$\tan \kappa_{s,m} d / \tan \kappa_{l,m} d = -4\beta_m^2 \kappa_{l,m} \kappa_{s,m} / (\kappa_{s,m}^2 - \beta_m^2) \quad (A1)$$

$$\kappa_{l,m} = \sqrt{k_l^2 - \beta_m^2} \quad (A2)$$

$$\kappa_{s,m} = \sqrt{k_s^2 - \beta_m^2} \quad (A3)$$

$$k_l = \omega \sqrt{\rho / (\lambda + 2\mu)} \quad (A4)$$

$$k_s = \omega \sqrt{\rho / \mu} \quad (A5)$$

The mode functions $\{f_m(x)\}$ and $\{g_m(x)\}$ are given as

$$\{f_m(x)\} = \{\bar{f}_m(x)\} / \sqrt{D_m} \quad (A6)$$

$$\{g_m(x)\} = \{\bar{g}_m(x)\} / \sqrt{D_m} \quad (A7)$$

$$\{\bar{f}_m(x)\} = [\bar{f}_{x,m}(x) \quad \bar{f}_{y,m}(x)]^T \quad (A8)$$

$$\{\bar{g}_m(x)\} = [\bar{g}_{x,m}(x) \quad \bar{g}_{y,m}(x)]^T \quad (A9)$$

$$D_m = \int_0^d \{\bar{f}_m(x)\}^T \{\bar{g}_m(x)\} dx \quad (A10)$$

$$\begin{aligned} \bar{f}_{x,m}(x) &= \sin \kappa_{l,m} x - [2\beta_m^2 / (\beta_m^2 - \kappa_{s,m}^2)] \\ &\quad \cdot (S_{l,m} / S_{s,m}) \sin \kappa_{s,m} x \end{aligned} \quad (A11)$$

$$\begin{aligned} \bar{f}_{y,m}(x) &= -j(\mu / \omega \kappa_{l,m}) [(k_s^2 - 2\kappa_{l,m}^2) \\ &\quad \cdot \cos \kappa_{l,m} x - (\beta_m^2 - \kappa_{s,m}^2) \\ &\quad \cdot (C_{l,m} / C_{s,m}) \cos \kappa_{s,m} x] \end{aligned} \quad (A12)$$

$$\bar{g}_{x,m}(x) = (2\mu\beta_m / \omega) [\sin \kappa_{l,m} x - (S_{l,m} / S_{s,m}) \sin \kappa_{s,m} x] \quad (A13)$$

$$\begin{aligned} \bar{g}_{y,m}(x) &= j(\beta_m / \kappa_{l,m}) (\cos \kappa_{l,m} x - [(\beta_m^2 - \kappa_{s,m}^2) / 2\beta_m^2] \\ &\quad \cdot (C_{l,m} / C_{s,m}) \cos \kappa_{s,m} x) \end{aligned} \quad (A14)$$

$$S_{l,m} = \sin \kappa_{l,m} d \quad (A15)$$

$$C_{l,m} = \cos \kappa_{l,m} d \quad (A16)$$

$$S_{s,m} = \sin \kappa_{s,m} d \quad (A17)$$

$$C_{s,m} = \cos \kappa_{s,m} d \quad (A18)$$

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